Secondary Structure Assignement

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1 Introduction

DSSP is a database of secondary structure assignments (and much more) for all protein entries in the Protein Data Bank (PDB). DSSP is also the program that calculates DSSP entries from PDB entries.

1.1 General Purpose

The purpose of this project is to generate a pattern-recognition program that assigns secondary structure elements (SSE) to a protein by using the dictionary of protein secondary structures (dssp)1 fixed by Kabsch and Sander in the mid-80's. SSE are based on hydrogen-bonded and geometrical features extracted from atomic coordinates.

1.2 Secondary structure Assignment

As Kabsch and Sander described in their paper¹, the implemented dssp program assigns the SSE according to a specific priority order. First α -helices (**H**) are assign, follow by isolated β -bridges (**B**), extended strands (**E**), 3_{10} -helices (**G**), π -helices (**I**), H-bonded turns **T** and then bend (**S**). The assignment of a SSE depends mainly on H-bonded features.

2 Material & methods

2.1 GANTT Diagram

we used GANTT to plannify our time.

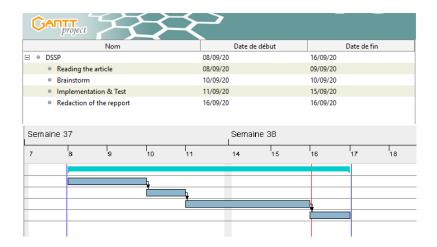


Figure 1: GANTT Diagram

2.2 Programming tools

All scripts are written in Python 3.6. PDB files are easily manage thanks to the BioPython² library. Adding hydrogens to a Protein DataBank (PDB) molecular structure file was done by Reduce program GitHub has been used for the development of this program. It is a web-based hosting service for version control using Git. Therefore, this project (its documentation and source code) is available online at the following address: https://github.com/saad272/Projet1.

2.3 Code structure

In addition to the main function (projet.py file), three modules are implemented: management (argument management and display of results), classes (Residue class and its methods to calculate supplement parameters) and structures (Secondary structures assignment) (see Figure 1).

2.4 Input data

The input file must be in PDB (Protein Data Bank) format. We used three examples to test:

- - 1E9O Crystal structure of bovine SOD
- - 3OGB Sperm whale myoglobin mutant H64W deoxy-form (see Results section).

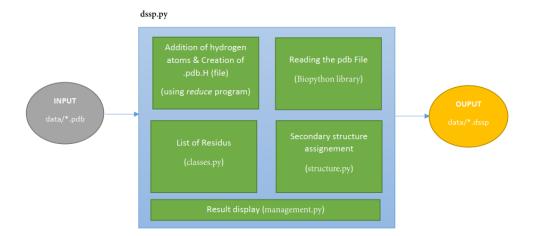


Figure 2: Schema of the implemented dssp program that assigns secondary structures from a pdb file.

2.5 Output data

Each line of a dssp output describes a residue and its assigned secondary structure .

- **RESIDUE**: Residue sequence number and chain identifier.
- AA: One letter amino acid code.
- STRUCTURE :
 - Secondary structure element: 'H', 'B', 'E', 'G', 'I', 'T', 'S' or ','
 - 3-turn/helix pattern : '>' (start), '<' (end), 'X' (start/end), '3' (middle), or ' '
 - 4-turn/helix pattern: '>', 'X', '<', '4', or ', '
 - 5-turn/helix pattern: '>', 'X', '<', '5' or ','
 - Geometrical bend: 'S' or ','
 - Chirality : '+' or '-'
 - Bridge label: 'a,b,c.' for parallel β-bridge, 'A,B,C.' for antiparallel β-bridge
- BP1 BP2 : Residue number of first and second bridge partner.
- TCO: Cosine of angle between C=O of residue i and C=O of residue i-1. TCO is near +1 for α -helices, TCO is near -1 for β -sheets.
- **KAPPA**: Virtual bond angle (bend angle) defined by the three C_{α} atoms of residues i-2, i, i+2. Used to define bend.

- **ALPHA**: Virtual torsion angle (dihedral angle) defined by the C_{α} atoms of residues i-1, i, i+1 and i+2. Used to define chirality.
- PHI PSI: Peptide backbone torsion angles (dihedral angles).
- X-CA Y-CA Z-CA : C_{α} atom coordinates.

2.6 Web server to calculate dssp files

The server is available at: https://www3.cmbi.umcn.nl/xssp/

3 Results

3.1 3OGB: Sperm whale myoglobin

3OGB is a is a dimensional structure with four -helices and does not contain β -sheets. the α helices are indicated in deferent colors, and the random ball regions are in white(see Figure 2). this protein is the first whose structure was resoled by crystallography in 1958 by Max Perutz and John Kendrew, which earned them the nobel Prize in chemistry in 1962. By comparing our dssp output (see Annexe section) with the result generated by dssp web (https://www3.cmbi.umcn.nl/xssp/), we notice the same assignment of the secondary structures for each residues except an isolated beta-bridge at residue number 59 that is not determined by the original program.

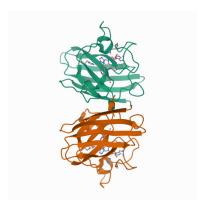


Figure 3: Structure of 1E90

3.2 1E9O: Crystal structure of bovine SOD

1E9O is a more complex example because the central part of these domains contains from 4 to more than 10 β strands the arrangement of these strands is most often antiparallel: the strands form 2 β sheets linked and compacted against each other The β sheets have a classic torsion and when 2 of these β

sheets are assembled, they form a barrel structure (" β barrel"). As before the main secondary structures (helices and strands) are well attributed. However, there are some differences/mistakes at some points.

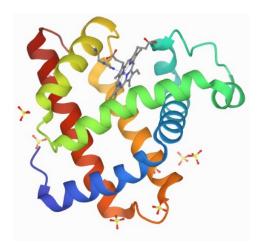


Figure 4: Structure of 3OGB

4 Conclusion

Our programme was inspired from the programme done by kabsch ans Sander in C++, we tried to implement it in python to get assigns secondary structure elements for each residues, this means you do need to have a full and valid 3D structure for a protein to be able to calculate the secondary structure.

5 References and webography

- 1. Kabsch, W., and C. Sander. "Secondary structure definition by the program DSSP." Biopolymers 22 (1983): 2577-2637.
- 2. Peter JA, et al. "Biopython: freely available Python tools for computational molecular biology and bioinformatics." Bioinformatics 25.11 (2009): 1422-1423.
- 3. https://www3.cmbi.umcn.nl/xssp/
- 4. https://www.rcsb.org/structure/1E9O
- 5. https://www.rcsb.org/structure/3OGB

6 Annexe

| 1 | (| base) in | nane | | | | | | | | | | ta/1e9o. | pdb |
|--------|---|--|--------------|-----|-----|-----|----|----------------|-------|------------------|---------|--------|----------|-----|
| 2 3 | | RESIDUE | AA | | | | | ure Ass TCO | | t using ALPHA | | PSI | X–CA | |
| 4 | Y-CA 1 30.0 | Z-CA 1 A 58.2 | A | | | 0 | 0 | 0.000 | 360.0 | 360.0 | 360.0 | 146.8 | -5.1 | |
| 5 | 28.6 | 2 A 60.5 | Т | | + | 0 | 0 | 0.453 | 360.0 | 35.2 - | -108.3 | -18.2 | -7.8 | |
| 6 | 3 25.3 | 3 A 61.1 | \mathbf{S} | E | +A | 21 | 0 | -0.999 | 62.7 | 174.2 - | -144.5 | 143.5 | -6.1 | |
| 7 | 24.1 | 4 A 61.5 | A | E | –B | 149 | 0 | -0.913 | 8.9 | -161.2- | -143.7 | 164.4 | -2.5 | |
| 8 | 5 20.9 | 5 A 62.3 | V | E | -C | 148 | 0 | -0.991 | 2.0 | -167.2- | -147.0 | 156.3 | -0.6 | |
| 9 | 6 20.0 | 6 A 63.4 | $^{\rm C}$ | E | –D | 18 | 0 | -0.987 | 11.1 | -151.4- | -148.5 | 133.6 | 2.8 | |
| 10 | 7 16.6 | 7 A 63.6 | V | E | –D | 17 | 0 | -0.958 | 20.3 | -145.9- | -107.0 | 121.4 | 4.6 | |
| 11 | 8 | 8 A 66.3 | L | E | +D | 16 | 0 | -0.728 | 27.3 | 162.6 | -92.0 | 125.6 | 7.2 | |
| 12 | 9 | 9 A 65.7 | S | E | +E | 144 | 0 | -0.988 | 4.8 | 164.1- | -138.6 | 154.6 | 10.3 | |
| 13 | $\begin{smallmatrix} 10\\14.1\end{smallmatrix}$ | 10 A 67.3 | G | | - | 0 | 0 | -0.787 | 53.2 | -83.4 | -149.5 | -167.2 | 13.7 | |
| 14 | $\begin{smallmatrix} 11\\12.1\end{smallmatrix}$ | 11 A 67.6 | D | S | S+ | 0 | 0 | 0.508 | 110.1 | 48.3 | -82.7 | -7.1 | 16.9 | |
| 15 | 9.9^{12} | 12 A 70.4 | G | S | S- | 0 | 0 | -0.248 | 110.4 | -75.3 | -112.5 | -154.6 | 15.3 | |
| 16 | 8.1 | 13 A 70.7 | Р | S | S+ | 0 | 0 | 0.358 | 86.8 | 116.9 | -90.2 | 2.0 | 11.9 | |
| 17 | $\begin{smallmatrix} 14\\11.2\end{smallmatrix}$ | 14 A 71.4 | V | | + | 0 | 0 | -0.639 | 36.0 | 154.3 | -76.0 | 128.5 | 9.8 | |
| 18 | $\frac{15}{11.8}$ | 15 A 68.7 | Q | E | + F | 0 | 34 | -0.958 | 8.3 | 156.1- | -146.1 | 162.4 | 7.2 | |
| 19 | $\frac{16}{13.5}$ | 16 A 68.4 | G | E | –DF | 8 | 33 | -0.984 | 33.4 | -125.8- | -176.4 | 167.2 | 3.8 | |
| 20 | $\begin{smallmatrix} 17\\15.2\end{smallmatrix}$ | 17 A 66.5 | Т | E | –DF | 7 | 32 | -0.998 | 23.6 | -171.1 - | -131.8 | 126.5 | 1.1 | |
| 21 | $\begin{array}{c} 18 \\ 18.6 \end{array}$ | 18 A 67.5 | Ι | E | –DF | 6 | 31 | -0.968 | 3.7 | -162.1 - | -120.1 | 134.3 | -0.2 | |
| 22 | $\begin{smallmatrix} 19\\20.3\end{smallmatrix}$ | 19 A 65.9 | Η | Ε | –CF | 5 | 30 | -0.839 | 2.7 | -161.2- | -116.0 | 150.8 | -3.3 | |
| 23 | $\begin{smallmatrix}20\\24.0\end{smallmatrix}$ | 20 A 66.1 | F | E | –AF | 4 | 29 | -0.998 | 8.4 | -179.7- | -133.2 | 138.1 | -4.1 | |
| 24 | $\begin{smallmatrix}21\\25.6\end{smallmatrix}$ | 21 A 65.5 | Е | Ε | –AF | 3 | 28 | -0.986 | 25.1 | -130.5 - | -143.4 | 127.8 | -7.5 | |
| 25 | $\begin{smallmatrix}22\\29.3\end{smallmatrix}$ | $\begin{array}{c} 22 \ \mathrm{A} \\ 65.6 \end{array}$ | A | Е | + F | 0 | 27 | -0.547 | 31.6 | 171.2 | -72.5 | 132.9 | -8.5 | |
| 26 | $\begin{array}{c} 23 \\ 29.8 \end{array}$ | 23 A 67.7 | K | E > | – F | 0 | 26 | -0.886 | 60.8 | -41.6 | -147.0 | 110.0 | -11.6 | |
| 27 | $\frac{24}{33.3}$ | 24 A 68.6 | G | Т 3 | S- | 0 | 0 | -0.530 | 121.8 | -29.9 | 71.8- | -132.6 | -12.7 | |
| 28 | $\begin{smallmatrix}25\\35.3\end{smallmatrix}$ | $\begin{array}{c} 25 \ \mathrm{A} \\ 69.5 \end{array}$ | D | Т 3 | S+ | 0 | 0 | -0.061 | 127.5 | 82.4 - | -108.0 | 30.2 | -9.6 | |
| 29 | $\begin{smallmatrix}26\\32.1\end{smallmatrix}$ | 26 A 70.8 | Т | E < | S–F | 23 | 0 | -0.846 | 70.8 | -132.8- | -123.1 | 167.3 | -7.9 | |
| 30 | $\begin{smallmatrix}27\\29.2\end{smallmatrix}$ | 27 A 69.4 | V | Е | –FG | 22 | 99 | -0.987 | 18.2 | -148.8 - | -122.4 | 125.6 | -5.9 | |
| 31 | $\begin{smallmatrix}28\\25.7\end{smallmatrix}$ | 28 A 70.6 | | | –FG | 21 | 98 | -0.865 | | -162.2 | | | -6.9 | |
| 32 | $\begin{array}{c} 29 \\ 23.3 \end{array}$ | 29 A 70.7 | | | +FG | 20 | 97 | -0.937 | | 162.8- | | | -4.0 | |
| 33 | $\begin{array}{c} 30 \\ 19.6 \end{array}$ | 30 A 70.9 | | | +FG | 19 | 96 | -0.897 | | 91.6 - | | | -4.7 | |
| 34 | 31 | 31 A | G | E | –FG | 18 | 95 | -0.931 | 55.8 | -93.7 | 144.9 - | -170.2 | -2.8 | |

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16.4
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              32 A S E
                               -FG
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              39 A G E
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              41 A H E
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              42 A G E
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              43 A F E
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              46 A H B
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              47 A Q S
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              48 A F
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              49 A G
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              51 A N
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                                                 0.043
                                                          42.8 \quad 115.4 - 105.1 \quad 23.4
                                                                                         15.3
     22.3
             61.1
                                                          90.2 \quad 30.5 \quad -63.3 \quad -29.9
55
        52
              52 A T T 3
                              S+
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                                                 0.818
                                                                                         18.7
     22.4
             59.3
56
        53
              53 A Q T >
                              S-
                                       0
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     21.5
             62.6
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                                                          82.0 - 27.8 \quad 62.9 - 139.7
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                              S-
                                       0
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                                                -0.293
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     19.5
             64.2
              55 A C T >
                                                 0.666\ 129.2\ 76.9\ -81.6\ -17.3
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                              S+
                                       0
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                                                                                         15.8
        55
     21.4
             66.9
59
              56 A T G X
                              S+
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                                            0
                                                 0.871
                                                          87.8 \quad 58.5 \quad -62.9 \quad -36.4
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        56
     23.5
             67.8
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        57
              57 A S G 3
                              S+
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                                                 0.553
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    25.7
             64.7
              58 A A G <
                              S-
                                                          86.2 - 149.5 - 75.4 - 13.7
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                                            0
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     26.7
             65.8
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              59 A G
                                       0
                                                -0.347
                                                          33.4 - 30.4 81.8 - 165.1
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        59
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     29.5
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              60 A P S
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        60
     31.0
             71.1
              61 A H B
64
                                -K
                                      46
                                            0
                                                -0.410
                                                          64.1 - 96.8 - 68.0 146.0
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    31.3
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                                +
                                                          58.8 \ 163.0 \ -63.7 \ 111.5
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              64 A P T 3
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                              S+
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                                                 0.764
                                                          80.2 \quad 51.1 \quad -68.4 \quad -22.7
     39.5
             69.3
              65 A L T 3
68
                             S-
                                       0
                                            0
                                                 0.323\ 107.7 - 123.7\ - 97.1
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        65
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| | | | | | | | | | | 9 | 72. | 41.8 | |
|------|--------|--------|----------|-------|--------|---|-----|----|-----|----------|-------------------|---|-----|
| 10.6 | 55.6 | 53.0 | 150.3 | 56.0 | 0.879 | 0 | 0 | + | < | A S | 66 | 66 | 69 |
| 9.4 | 176.1 | -106.0 | -99.1 | 48.7 | -0.506 | 0 | 0 | _ | | A K | 73. 67 | $41.3 \\ 67$ | 70 |
| 10.9 | 166.6 | -87.6 | -84.0 | 52.3 | -0.510 | 0 | 0 | _ | | 3 A K | 77. 68 | 40.1 68 | 71 |
| | | | | | | | | | | 8 | 79. | 37.8 | |
| 9.8 | 139.0 | -70.1 | 152.6 | 60.3 | -0.381 | 0 | 0 | + | | АН | 69 80. | $\frac{69}{34.1}$ | 72 |
| 6.7 | -171.3 | -147.6 | -79.7 | 45.5 | -0.810 | 0 | 0 | _ | | A G | | $70 \\ 33.2$ | 73 |
| 3.9 | 171.0 | -91.9 | -98.0 | 53.0 | -0.549 | 0 | 0 | _ | > | A G | 71 | 71 | 74 |
| 0.9 | -25.5 | -64.1 | 51.1 | 122.9 | 0.779 | 0 | 0 | S+ | Т 3 | ΑP | | $\frac{30.7}{72}$ | 75 |
| -1.3 | -0.2 | -89.9 | 102.6 | 91.4 | 0.502 | 0 | 0 | S+ | Т 3 | 9 A K | 79. 73 | $\frac{30.9}{73}$ | 76 |
| 1.4 | 145.4 | -82.8 | -144.2 | 67.1 | -0.529 | 0 | 0 | _ | < | 4 A D | 82. 74 | $32.8 \\ 74$ | 77 |
| 1.3 | | -73.5 | | 97.4 | 0.863 | 0 | 0 | S+ | S | | 83. | $35.4 \\ 75$ | 78 |
| | 02.0 | | | | | | · · | | D | 7 | 81. | 38.9 | |
| 5.1 | 96.9 | -99.6 | 112.2 | 83.7 | -0.833 | 0 | 0 | S+ | S | АЕ 4 | $\frac{76}{81}$. | $\frac{76}{38.8}$ | 79 |
| 5.7 | 165.7 | -154.3 | -97.2 | 69.4 | -0.975 | 0 | 0 | _ | | A R | 77 | 77 | 80 |
| 6.9 | 159.3 | -80.5 | -119.2 | 35.6 | -0.672 | 0 | 0 | _ | > | A H | | 35.9 78 | 81 |
| 4.2 | -38.2 | -61.4 | 53.4 | 117.2 | 0.913 | 0 | 0 | S+ | Т 3 | A V | | $35.1 \\ 79$ | 82 |
| 5.6 | 4.8 | -79.8 | 113.7 | 78.4 | 0.416 | 0 | 0 | S+ | Т 3 | 9 A G | 72. 80 | 34.6 80 | 83 |
| 5.4 | 93.1 | | 158.9 | | -0.648 | 0 | 44 | +J | В < | | 72. | $31.1 \\ 81$ | 84 |
| | | | | | | | | | D | 2 | 76. | 30.2 | |
| 2.7 | 10.9 | | -136.0- | | 0.261 | 0 | 0 | _ | | | 76. | $\begin{array}{c} 82 \\ 27.5 \end{array}$ | 85 |
| 3.8 | -139.4 | 80.7 - | -27.4 | 45.3 | -0.506 | 0 | 0 | _ | | AG 8 | 83 79. | $83 \\ 26.1$ | 86 |
| 4.1 | 152.6 | -120.5 | -150.8 | 39.2 | -0.935 | 0 | 42 | –Н | E | A N 4 | 84 80. | $\frac{84}{22.3}$ | 87 |
| 2.5 | 156.0 | -108.1 | -133.9 | 24.8 | -0.791 | 0 | 41 | –Н | E | A V | | 85 19.2 | 88 |
| 2.3 | 122.0 | -119.3 | -157.0- | 12.2 | -0.945 | 0 | 40 | –Н | E | АТ | 86 | 86 | 89 |
| 3.2 | 142.5 | -94.2 | -140.3 | 12.8 | -0.738 | 0 | 93 | -L | E | A A | | 16.2 87 | 90 |
| 1.8 | -176.3 | -86.3 | -79.0 | 41.3 | -0.327 | 0 | 0 | _ | > | A D | 80. 88 | 12.6 88 | 91 |
| 3.6 | -24.7 | -57.2 | 54.3 | 131.8 | 0.739 | 0 | 0 | S+ | Т 3 | A S | 82.3 89 | 9.6 | 92 |
| 3.3 | 3.9 | | -109.3 | | | 0 | 0 | S- | Т 3 | A N | 83.4 | 6.4 | 93 |
| | | | | | | | | | | | 79.8 | 5.0 | |
| 5.0 | 19.5 | 78.8 | 141.1 | 72.4 | 0.651 | 0 | 0 | S+ | S < | A G | $\frac{91}{78.5}$ | 91 8.2 | 94 |
| 1.9 | 119.9 | -101.7 | -166.8 | 32.4 | -0.799 | 0 | 0 | _ | | A V | $\frac{92}{76.9}$ | $92 \\ 9.5$ | 95 |
| 1.1 | 130.7 | -104.5 | -153.2 | 7.7 | -0.909 | 0 | 87 | -L | E | A A | | $93 \\ 13.2$ | 96 |
| -2.3 | 124.8 | -100.1 | -149.0 | 13.7 | -0.843 | 0 | 32 | -G | E | A I | 94 | 94 | 97 |
| -2.3 | 131.9 | -99.8 | 148.3 | 32.4 | -0.853 | 0 | 31 | +G | E | A V | | 14.5 95 | 98 |
| -5.2 | 88.4 | -161.4 | 151.3- | 16.3 | -0.674 | 0 | 30 | +G | E | A D | | 18.1 96 | 99 |
| -4.4 | 141 5 | -121.1 | -157 8 - | 20 1 | -0.969 | 0 | 29 | –G | E | 4 A I | 75. 97 | $\frac{20.5}{97}$ | 100 |
| -4.4 | 141.0 | 141.1 | 101.0 | 23.4 | 0.303 | U | 43 | -G | L | | 75. | 24.2 | 100 |