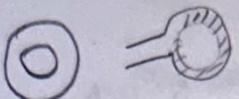
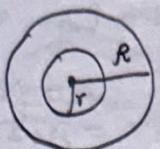


Inductance of Toroid



$$B = \frac{\mu NI}{l}$$

$$[B = \mu H]$$



$$H = \frac{NI}{l}$$

'N-turns' carrying I.

$$l = 2\pi R$$

circumference

$$B = \frac{\mu NI}{2\pi R}$$

$$B = \frac{\phi}{A}$$

$$N\phi = NBA$$

$$N\phi = \frac{\mu N^2 I}{2\pi R} A$$

$$B = \frac{\mu NI}{2\pi R}$$

$$N\phi = \frac{\mu N^2 I}{2\pi R} A$$

$$N\phi = \frac{\mu N^2 I}{2\pi R} (\pi r^2)$$

$$L = \frac{\mu N^2 I}{2\pi R} (\pi r^2)$$

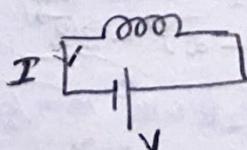
$$L = N \frac{\phi}{I}$$

$$\phi = \frac{\mu NI}{2\pi R} (\pi r^2)$$

$$L = \frac{N\phi}{I} = \frac{\mu N^2}{2\pi R} (\pi r^2)$$

$$L = \frac{\mu N^2 r^2}{2R}$$

R means radianc



$$V = L \frac{di}{dt}$$

$$P = V \times I = \frac{dw}{dt} = \frac{d\text{Energy}}{dt}$$

$$\int dw = \int V I dt$$

$$W = \int L \frac{dp}{dt} I dt$$

$$= L \int I \cdot d\theta$$

$$E = \frac{LI^2}{2}$$

$$E_{\text{stored}} (\text{Ind}) = \frac{LI^2}{2}$$

$$E_{\text{stored}} (\text{capa}) = \frac{1}{2} CV^2$$

Energy density

$$L = \frac{N^2 \mu A}{l}$$

$$E.D = \frac{E}{\text{Volume}} = \frac{LI^2}{2V} = \frac{\frac{N^2 \mu A}{l} I^2}{2Axl}$$

(Inductance)

$$\boxed{\text{Energy density} = \frac{N^2 \mu I^2}{2l^2}}$$

$$\text{Energy dens} = \frac{\mu}{2} \left(\frac{NI}{l} \right)^2$$

$$B = \mu H$$

$$E.D = \frac{\mu}{2} H^2$$

$$\boxed{E.D = \frac{1}{2} \frac{B^2}{\mu}}$$

$$H = \frac{B}{\mu}$$

$$H^2 = \frac{B^2}{\mu^2}$$

$$(\text{Energy density})_{\text{capacitors}} = \frac{1}{2} \epsilon E^2$$

H.W: Two mag materials - sep by a distance $z=0$, having perm

$\mu_1 = 4\mu_0 \text{ H/m}$, $\mu_2 = 7\mu_0 \text{ H/m}$ ($z < 0$) \rightarrow There exist surface

$$z > 0$$

current density $K_s = 60 \hat{i} \text{ A/m}$ at $z=0$ free field $\vec{B}_1 = 1\hat{i} - 2\hat{j} - 3\hat{k} \text{ mT}$

$$\boxed{\vec{B}_2 = ?} \rightarrow \text{find}$$

Soluⁿ:

$$\vec{B}_{E1} - \vec{B}_{E2} = \mu_0 (K_s \times \hat{n}) \quad B_1 = 1\hat{i} - 2\hat{j} - 3\hat{k} \text{ mT}$$

$$\mu_1 = 4\mu_0$$

$$\overline{z=0} \quad [K_s = 60 \hat{i}]$$

$$\mu_2 = 7\mu_0$$

$$B_{N_1} = B_{N_2}, H_{N_1} = \frac{\mu_2}{\mu_1} H_{N_2} \Rightarrow A_{k_1} - H_{k_2} = K_s$$

$$B_1 = \hat{r} - 2\hat{z} - 3\hat{x}$$

$$H_{k_1} = \frac{B_{k_1}}{\mu_1}$$

$$\boxed{B_{N_1} = B_{N_2} = -3\hat{x}}$$

$$A_{k_2} = \frac{B_{k_2}}{\mu_2}$$

$$H_N = n_N B = n_N \hat{B}$$

$$H_1 = \frac{B_1}{\mu_1} = \frac{(\hat{r} - 2\hat{z} - 3\hat{x})}{4\mu_0}$$

$$H_2 = \frac{B_2}{\mu_2} = \frac{B_{x_2}\hat{x} + B_{y_2}\hat{y} + B_{z_2}\hat{z}}{7\mu_0}$$

$$H_{tot} = \frac{1}{\mu_1} \left(\frac{n_N B}{(H_1 - H_2)} \times a_{n12} \right) K$$

$$(H_1 a_{n12}) = H_2 a_{n12} + K$$

$$\frac{\hat{r} - 2\hat{z} - 3\hat{x}}{4\mu_0} \times \frac{1}{H_2} = \frac{B_{x_2}\hat{x} + B_{y_2}\hat{y} + B_{z_2}\hat{z}}{7\mu_0} \times \hat{r} + 60\hat{z}$$

$$\vec{a} \times \vec{b} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ 1 & 1 & 1 \\ 1 & -2 & -3 \\ 0 & 0 & 1 \end{vmatrix} \quad \text{Note: } (\vec{a} \cdot \vec{b}) \text{ sum of diagonal elements} \leftarrow \vec{a} \cdot \vec{b} \text{ formula from notes}$$

$$\frac{1}{4\mu_0} \begin{vmatrix} 1 & 1 & 1 \\ 1 & -2 & -3 \\ 0 & 0 & 1 \end{vmatrix} = \frac{1}{7\mu_0} \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ B_{x_2} & B_{y_2} & B_{z_2} \\ 0 & 0 & 1 \end{vmatrix} + 60\hat{z}$$

$$\frac{1}{4\mu_0} \left(\hat{x}(-2+0) - \hat{y}(1+0) + \hat{z}(1) \right) = \frac{1}{7\mu_0} \left[\hat{x}(B_y) - \hat{y}(B_x) \right] + 60\hat{z}$$

$$\frac{1}{4\mu_0} \left(-2\hat{x} - \hat{y} \right) - 60\hat{z} = \frac{1}{7\mu_0} \left[B_y \hat{x} - B_x \hat{y} \right] + 60\hat{z}$$

$$2 \text{ am } P_{01} \times 8 \text{ SP} =$$

Evaluating

$$\left(\frac{1}{4\mu_0} \right) 8 \text{ SP} = \frac{1}{4\mu_0} (-2\hat{x}) - 60\hat{z} = \frac{1}{7\mu_0} B_y \hat{x}$$

$$\frac{1}{4\mu_0} \left(\frac{8 \text{ SP}}{2} \right) \text{ total} =$$

$$\frac{4 \cdot 2 \cdot (-2\hat{x})}{4\mu_0} = \frac{1}{7\mu_0} (-B_x \hat{y})$$

$$-\frac{8}{4\mu_0} - 60 = \frac{B_y}{7\mu_0}$$

$$\frac{8}{4\mu_0} = \frac{1}{7\mu_0} B_x \quad \checkmark$$

$$3G = 8 \text{ SP} = 98$$

$$8 \text{ SP} = 3G \quad B_y = 28$$

$$\frac{8}{4\mu_0} \left(\frac{-2}{4\mu_0} - 60 \right) = -3 \cdot 5 \cdot 28 = 60 \quad B_x = \frac{7}{4} = 1.75$$

$$B_2 = (B_x \hat{i} + B_y \hat{j} + B_z \hat{k}) = B_{k2} + B_{2N}$$

$$B_2 = 1.75 \hat{i} - 3.5 \hat{j} - 3 \hat{k}$$

$$B_1 = B_{1k} + B_{1n}$$

$$B_{1k} = B_1 - B_{1n}$$

$$\cdot = 1 \hat{i} - 2 \hat{j}$$

$$B_{1k} = B_{2n} = -3k$$

APP. another BC,

$$\frac{B_{1k}}{\mu_1} - \frac{B_{2k}}{\mu_2} = k_S$$

$$\left(\frac{9\hat{i} - 2\hat{j}}{4\mu_0} - \frac{B_{2k}}{7\mu_0} \right) \times \hat{k} = 60 \hat{i}$$

(vector)

$$\hat{i} \times \hat{j} = \hat{k}$$

Hemisphere \rightarrow Along $dR \rightarrow$ (area can't have dR).

$$P_V = -0.3 \text{ nC/mm}^3$$

a)

$$10^9 \rightarrow \text{milliampere}$$

$$J = -a_Z 2.4 \text{ A/mm}^2$$

$$R = 5 \text{ mm}$$

a) Total current passing through hemis cap ($k = 5 \text{ henry}$)

$$\begin{aligned} I &= \int J \cdot dS = - \int a_Z \cdot a_Z \cdot dS \\ &= \int_0^{2\pi} \int_0^{\pi/2} -2.4 \cos \theta (5^2 \sin \theta d\theta d\phi) \\ &= -2\pi \int_0^{\pi/2} 60 \sin \theta d\sin \theta \\ &= -120\pi \left(\frac{\sin^2 \theta}{2} \right)_0^{\pi/2} \\ &= -60\pi = -188.5 \text{ A} \end{aligned}$$

v = velocity of free charges $dS \sin \theta = \cos \theta$

$$u = \frac{J}{P_V} = a_Z \frac{-2.4}{-0.3 \times 10^{-9}}$$

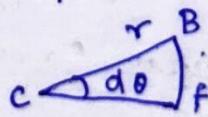
$$= a_Z 8 \times 10^9 \text{ mm/s}$$

$$= a_Z 8 \text{ (Mm/s)}$$



$$AB = AD = r \sin \theta$$

$$BD = r \sin \theta d\phi$$



$$CB = r$$

$$\angle BCF = d\theta$$

$$BF = r d\theta = DE$$

$$DE = r d\theta$$

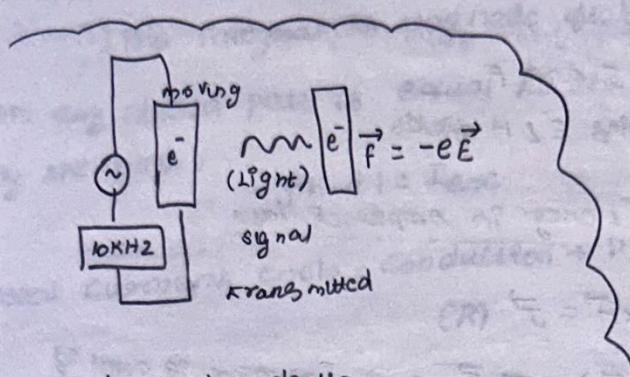
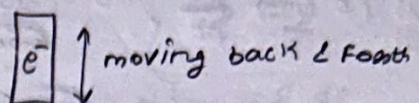
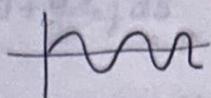
$$dS = BD \cdot BF$$

$$= r \sin \theta d\phi \cdot r d\theta = r^2 \sin \theta d\phi d\theta$$

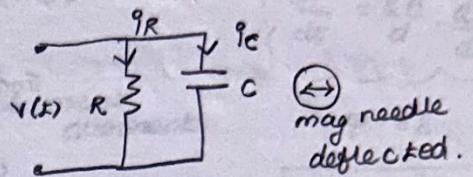
Faрадаевъ закон - Displacement I & Maxwell - Ampere law - Maxwell eqn -
potential functions - EM B.C

Unit - 4

$$\vec{E} = \frac{\vec{E}}{v}$$



Displacement Current



may needle deflected.

Infrared radiation.

Peta Hertz \rightarrow visible light (speed of light)
(transmitted \uparrow)

$$q_R(x) = \frac{V(x)}{R}, q_C(x) = C \frac{dV(x)}{dx}$$

'Current is also due to bound charges - Since capacitor has bound charges'.

through R - conduction current

C - displacement current.

$$\bar{J}_d(x) = \frac{d\bar{D}(x)}{dx}$$

$$q_C(x) = q_d(x) = \frac{dQ}{dx} = C \frac{dV(x)}{dx}$$

$$\boxed{\bar{J}_d(x) = \frac{\partial \bar{D}(x)}{\partial x}}$$

$$= EA \frac{d}{dx} \left[\frac{V(x)}{d} \right] = \frac{EA}{d} \frac{dV(x)}{dt} = \frac{EA}{d} \frac{dE(x)}{dt}$$

$$= A \frac{d}{dt} [E E(x)]$$

$$= A \frac{d}{dt} \bar{D}(x)$$

Intro

* Static E can exist without H

* Conductors with I has a H without E

* Time varying fields

* E & H can't exist without each other

* Discovered EM waves - Express by Faraday & Maxwell

Maxwells law - 4 laws

Derived from - Amp Ckt law,

Faraday's law

Gauss law of E

Gauss law of H

* used to describe EM fields

* Partial derivation law:

B/w B, E, D, H, J and P

Relation b/w changing E & H fields

Inconsistency in Ampere's law

$$\nabla \times \vec{H} = \vec{J}$$

$$\nabla \cdot (\nabla \times \vec{H}) = \nabla \cdot \vec{J} = 0$$

[Divergence of curl of any vector = 0]

$$\nabla \cdot \vec{J} = - \frac{\partial P}{\partial t} \neq 0$$

↓

Continuity equation

[contradiction]

Modified - Maxwell Amp law

$$\nabla \times \vec{H} = \vec{J} + \vec{J}_d$$

$$\nabla \cdot (\nabla \times \vec{H}) = \nabla \cdot \vec{J} + \nabla \cdot \vec{J}_d = 0$$

$$\nabla \cdot \vec{J}_d = - \nabla \cdot \vec{J} = \frac{\partial P}{\partial t} = \frac{\partial}{\partial t} (\nabla \cdot \vec{D}) = \nabla \cdot \frac{\partial \vec{D}}{\partial t}$$

$$\vec{J}_d = \frac{\partial \vec{D}}{\partial t}$$

$$\boxed{\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}}$$

Maxwell eqn - I

From Amp's ckt law:

$$I = \oint H \cdot dI$$

$$\oint H \cdot dI = \iint_S (J_c + J_d) \cdot dS$$

$$\oint H \cdot dI = \iint_S (\text{cond current} + \text{disp current}) \cdot dS$$

obtained from Ampere's

$$\nabla \times H = J + \frac{\partial D}{\partial t}$$

$$2\pi (H \times V) B = 1 b \cdot A$$

$$I_D = \frac{d\Phi}{dt} = \frac{\epsilon A}{d} \cdot \frac{dE}{dt}$$

$$\oint H \cdot dL = \iint (J + \frac{\partial D}{\partial t}) \cdot dS$$

$$2\pi (H \times V) B = 2b \left(\frac{I_D}{A} + \frac{dE}{dt} \right)$$

$$\frac{d\Phi}{dt} + \frac{d\Phi}{dt} = H \cdot V \quad = \epsilon \frac{dE}{dt}$$

Ampere's law:

Line integral of magnetic field intensity 'H'

on any closed path is equal to the current enclosed by the path.

$$\oint H \cdot dL = I_{enc}$$

$$V = E \cdot d$$

Total current enclosed = Conduction + Displacement current

(R)

(C)

$$\Phi = E \cdot E$$

$$\oint H \cdot dL = \iint (J_C + J_D) \cdot dS$$

$$I = J \cdot A$$

$$\frac{d\Phi}{dt} = \epsilon \frac{dE}{dt}$$

J_C = Conduction current density

From Ohm's law:

$$R = \frac{P_L}{A}$$

$$P_L = \frac{1}{\sigma}$$

$$V = J_C R$$

$$J_C = \frac{V}{R}$$

$$= \frac{V}{P_L} = \frac{V \times A}{P_L}$$

$$= \frac{V \times A \times \sigma}{l}$$

If E is the electric field,

$$E l \approx V$$

$$J_C = \frac{E \times l \times A \times \sigma}{l}$$

$$J_C = EA\sigma$$

$$J_C = \frac{I_C}{A} = \sigma E$$

current through capacitor (I_D)

$$I_D = \frac{d\Phi}{dt}$$

$$C = \frac{\epsilon A}{d}$$

$$Q = CV$$

$$\frac{dQ}{dt} = \epsilon \frac{dV}{dt}$$

$$\frac{dq}{dt} = \frac{\epsilon A}{d} \frac{d}{dt} (E \cdot d)$$

$$= \epsilon A \frac{dE}{dt}$$

$$J_D = \frac{\partial D}{\partial t}$$

$$\epsilon E = D$$

$$\oint H \cdot dL = \iint (\sigma E + \frac{\partial D}{\partial t}) \cdot dS$$

This is called Potential form

$$J_D = \frac{I_D}{A} = \epsilon \frac{dE}{dt}$$

To get the differential form, we apply Stokes theorem:

$$\oint \mathbf{H} \cdot d\mathbf{l} = \oint (\nabla \times \mathbf{H}) ds \quad \frac{\partial \mathbf{B}}{\partial t} + \mathbf{J}_e = \mathbf{H} \times \nabla$$

$$\iint_S (\sigma_E + \frac{\partial D}{\partial t}) ds = \iint_S (\nabla \times \mathbf{H}) ds \quad \left(\frac{\partial \mathbf{B}}{\partial t} + \mathbf{J}_e \right) \downarrow = \mathbf{H} \cdot \mathbf{d}$$

$$\nabla \times \mathbf{H} = \frac{\partial \mathbf{E}}{\partial t} + \frac{\partial \mathbf{D}}{\partial x}$$

This is the point of differential form of Maxwell's law I

Maxwell's equation II

* From Faraday's law: emf produced in a circuit is equal to the rate of decrease of the magnetic flux linkage of the circuit.

$$(P.E) \quad V_{emf} = - \frac{d\phi}{dt} = - \frac{d}{dt} \left[\iint_S \mathbf{B} \cdot d\mathbf{s} \right]$$

$$A \cdot \mathcal{I} = I$$

$$2b \cdot (\mathcal{I}t + \mathcal{I}t) \downarrow = \boxed{V_{emf}}$$

W.K.t

$$V_{emf} = \oint \mathbf{E} \cdot d\mathbf{l}$$

$$\oint \mathbf{E} \cdot d\mathbf{l} = - \frac{d}{dt} \left[\iint_S \mathbf{B} \cdot d\mathbf{s} \right] = - \iint_S \frac{\partial \mathbf{B}}{\partial t} d\mathbf{s} = - \iint_S \frac{\partial H}{\partial t} d\mathbf{s} = \mathcal{I}$$

From Stokes:

$$\oint \mathbf{E} \cdot d\mathbf{l} = \iint_S (\nabla \times \mathbf{E}) ds$$

$$2. \quad \nabla \times \mathbf{E} = - \frac{\partial \mathbf{B}}{\partial t}$$

$$\boxed{\nabla \times \mathbf{E} = - \mu \frac{\partial \mathbf{H}}{\partial t}}$$

$$A \cdot \mathcal{I} = V$$

$$\frac{V}{A} = \mathcal{I}$$

$$\frac{V}{A} = B$$

$$\frac{V}{A} = B$$

Emf around a closed path is equal to the magnetic flux density through that closed path

$$A \cdot \mathcal{I} = \frac{V}{A} = \mathcal{I}$$

Maxwell's equation - III

* From Gauss law: Electric flux through a closed surface is equal to the charge enclosed by the surface.

$$\oint \mathbf{D} \cdot d\mathbf{s} = Q = \iiint_V P_v \cdot dV$$

$$\psi = \phi \quad \frac{Q}{A} = \mathcal{I}$$

$$\frac{Q}{A} = \mathcal{I}$$

$$V \mathcal{I} = Q$$

→ This is Maxwell's form of Gauss' law in

Integral form

$$2b \left(\frac{\partial \mathbf{B}}{\partial t} + \mathbf{J}_e \right) \downarrow = \mathbf{H} \cdot \mathbf{d}$$

By app. Divergence theorem

$$(b.3) \quad \frac{b}{A} \frac{\partial B}{\partial t} = \frac{P_v}{A}$$

$$\text{From Ampere's law} \quad \iint_S \mathbf{D} \cdot d\mathbf{s} = \iiint_V (\nabla \cdot \mathbf{D}) dV = \iint_V P_v dV =$$

$$\nabla \cdot \mathbf{D} = P_v$$

$$\frac{P_v}{A} = \frac{b}{A} = \frac{I}{A}$$

This is the point form of div form

The total electric displacement through the surface enclosing a volume is equal to the charge (total) within the volume

maxwell eqn - IV

Magnetic flux through any closed surface is equal to zero $\oint \mathbf{B} \cdot d\mathbf{S} = 0$

$\oint \mathbf{B} \cdot d\mathbf{S} = 0 \rightarrow$ Integral form

App. Divergence theorem:

$$\oint \mathbf{B} \cdot d\mathbf{S} = \iiint_V (\nabla \cdot \mathbf{B}) dV$$

$$\oint \mathbf{B} \cdot d\mathbf{S} = \iiint_V (\nabla \cdot \mathbf{B}) dV = 0$$

$$\nabla \cdot \mathbf{B} = 0$$

Net magnetic flux emerging through any closed surface is zero.

Max eqn: Divergence & Integral form

Name of law	Divergence	Integral form
Gauss's law	$\nabla \cdot \mathbf{D} = P_V$	$\oint \mathbf{D} \cdot d\mathbf{S} = \iiint_V P_V dV = \Phi$
Faraday's law	$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$	$\oint \mathbf{E} \cdot d\mathbf{l} = -\frac{\partial}{\partial t} \iint_S \mathbf{B} \cdot d\mathbf{S}$
Gauss's law of magnetism	$\nabla \cdot \mathbf{B} = 0$	$\oint \mathbf{B} \cdot d\mathbf{S} = 0$
Ampere's law	$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}$	$\oint \mathbf{H} \cdot d\mathbf{l} = \iint_S (\mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}) \cdot d\mathbf{S}$

Boundary conditions across time varying fields

The B.C. derived in static fields remains valid across time varying fields.

B.C. b/w two dielectric materials [Arun monkey - 315]

Tangential components:

We have derived the tangential components of dielectric-dielectric boundary conditions using the dielectric-dielectric relation $\oint \mathbf{E} \cdot d\mathbf{l} = 0$ for a closed path in a static field.

Now we apply

$$\oint \mathbf{E} \cdot d\mathbf{l} = - \int \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{s}$$
 around a selected closed path

(closed) 1-2-3-4-1.

Hence, the integral must be broken into four parts

$$\oint \mathbf{E} \cdot d\mathbf{l} = \int_1^2 + \int_2^3 + \int_3^4 + \int_4^1 = - \int \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{s}$$

Let the long 1-2 and 3-4 be Δw , $\Delta h \rightarrow 0$ (keeping the surface b/w term)

$$\oint \mathbf{E} \cdot d\mathbf{l} = \int_P E_T \cdot \Delta w + \int_2^3 E_N \frac{\Delta h}{2} + \int_3^4 E_T \Delta w + \int_4^1 E_N \frac{\Delta h}{2} = - \int \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{s}$$

$$E_T(1-2) \Delta w - E_N(2-3) \frac{\Delta h}{2} - E_T(3-4) \Delta w + E_N(4-1) \frac{\Delta h}{2} = - \int \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{s}$$

$$\Delta h \rightarrow 0$$

E_N at b $\frac{1}{2} \Delta h \approx E_N$ at a $\frac{1}{2} \Delta h$ and as the area of rectangle approaches zero, the surface integral of $\frac{\partial \mathbf{B}}{\partial t}$ vanishes.

Thus,

$$E_{T_1} \Delta w - E_{T_2} \Delta w = 0$$

$$\boxed{E_{T_1} = E_{T_2}}$$

Boundary cond. stated above hold good across both static & time changing fields.

Normal Components:

For determining the normal component, we select a Gaussian surface & apply the Gauss law on it

$$\oint D \cdot d\mathbf{s} = \Delta \Phi = \int \rho_v \cdot d\mathbf{v}$$

Gauss law is same for both static & time changing fields, so boundary conditions are

$$D_{N_1} - D_{N_2} = \rho_s$$

$$\boxed{D_{N_1} = D_{N_2}}$$

[at polycond unit w/ additional preterm] [at polycond unit w/ additional preterm] charge at boundary

B.C b/w two diff mag materials?

Maxwell's law is used

: heterogeneous material

$$\oint H \cdot d\mathbf{l} = \int_S (J_c + \frac{\partial D}{\partial t}) ds$$
 instead of

$$\oint \mathbf{H} \cdot d\mathbf{l} = I = \int_S J_0 ds$$

It's assumed that $\Delta h \rightarrow 0$ the \int_S of $\frac{\partial D}{\partial z}$ vanishes, so the time changing \vec{D} normal to sheet path (half in medium) doesn't contribute.

From $\oint \mathbf{H} \cdot d\mathbf{l} = \int_S (J_c + \frac{\partial D}{\partial z}) ds$, the conduction current density J_c may also change with time. However the surface integral also vanishes as $\Delta h \rightarrow 0$.

$$H_{T_1} - H_{T_2} = K \times \hat{a}_{12} \quad (\text{current sheet at the boundary})$$

$$\boxed{H_{T_1} = H_{T_2}} \rightarrow \text{Absence of } K.$$

Normal components:

The normal comp. of B & H are same as that of static field boundary conditions

$$\boxed{B_{N1} = B_{N2}}$$

- 1) A $25\mu C$ charge is located at $(3, 4, 0)$ m. Evaluate the resulting field at the origin. a) spherical b) cylindrical

$$(0, 0, 0) \rightarrow (0, 0, 0)$$

Soln:

a) spherical:

$$r = \sqrt{x^2 + y^2 + z^2}$$

$$r = \sqrt{9 + 16 + 0}$$

$$r = 5$$

$$\vec{E}(\text{point charge}) = \frac{\varphi}{4\pi\epsilon r^2} \cdot \vec{a}_r$$

$$\theta = \cos^{-1} \left(\frac{z}{\sqrt{x^2 + y^2 + z^2}} \right)$$

$$\theta = \cos^{-1}(0)$$

$$\theta = (\pi/2)^{\circ}$$

$$\phi = \tan^{-1} \left(\frac{y}{x} \right)$$

$$\phi = \tan^{-1}(4/3)$$

$$\phi = 53.13^{\circ}$$

$$\vec{r} = -5\hat{a}_r - \frac{\pi}{2}\hat{a}_{\theta} - 53.13\hat{a}_{\phi}$$

$$\begin{aligned} &= \frac{4\pi\epsilon \times 25}{25\mu} \times \frac{5}{(-5\hat{a}_r - \frac{\pi}{2}\hat{a}_{\theta} - 53.13\hat{a}_{\phi})} \\ &= \frac{4\pi \times 8.854 \times 10^{-12} \times 25}{4\pi \times 25 \times 8.854 \times 10^{-6}} \times \frac{(-5\hat{a}_r - \frac{\pi}{2}\hat{a}_{\theta} - 53.13\hat{a}_{\phi})}{5} \end{aligned}$$

$$\begin{aligned} &= 1797.54 (-5\hat{a}_r - \frac{\pi}{2}\hat{a}_{\theta} - 53.13\hat{a}_{\phi}) \\ &= -8987.7\hat{a}_r - 161778\hat{a}_{\theta} - 95503.30\hat{a}_{\phi} \end{aligned}$$

$$\boxed{\vec{E} = -(8.987\hat{a}_r + 161778\hat{a}_{\theta} + 95503.30\hat{a}_{\phi}) V/m}$$

$$\begin{aligned} E &= \frac{\varphi}{4\pi\epsilon r^2} = \frac{25\mu}{4\pi \times 8.854 \times 10^{-12} \times 25} \\ &= \frac{25}{4\pi \times 8.854 \times 10^{-6} \times 25} \end{aligned}$$

$$\boxed{E = 8987.742438 V/m}$$

Cartesian coordinates

$$E = 8987.74 V/m$$

$$\vec{E} = 8987.74\hat{a}_r$$

$$= 8987.74 \left(-\frac{3\hat{a}_x - 4\hat{a}_y}{5} \right)$$

$$\vec{E} = +1797.54846 (-3\hat{a}_x - 4\hat{a}_y)$$

$$\vec{E} = (-5.392 \hat{a}_x - 7.190 \hat{a}_y) \text{ N/V/m}$$

Q) If $V = 2x^2y + 20z - \frac{4}{x^2+y^2}$ Volts. Find \vec{E} and \vec{D} at $P(6, -2.5, 3)$

Solu:

$$V = - \int E \cdot dL$$

$$E = -\nabla V \text{ (Potential gradient)}$$

$$\nabla V = \left(\frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z \right)$$

$$\nabla V = \left(4xy + \frac{4(2x)}{(x^2+y^2)^2} \right) \hat{a}_x + \left(2x^2 + \frac{4(2y)}{(x^2+y^2)^2} \right) \hat{a}_y + (20) \hat{a}_z$$

$$\nabla V = \left(4xy + \frac{8x}{(x^2+y^2)^2} \right) \hat{a}_x + \left(2x^2 + \frac{8y}{(x^2+y^2)^2} \right) \hat{a}_y + 20 \hat{a}_z$$

$$\vec{E} = -\nabla V \Big|_{(6, -2.5, 3)}$$

$$\vec{E} = - \left(\frac{(4 \times 6 \times -2.5) + \frac{8(6)}{(36 + (-2.5)^2)^2}}{(36 + (-2.5)^2)^2} \right) \hat{a}_x - \left(\frac{2 \times 36 + \frac{8(-2.5)}{(36 + (-2.5)^2)^2}}{(36 + (-2.5)^2)^2} \right) \hat{a}_y + 20 \hat{a}_z$$

$$\vec{E} = - \left(-60 + \frac{48}{1785.0625} \right) \hat{a}_x - \left(72 - \frac{20}{1785.0625} \right) \hat{a}_y + 20 \hat{a}_z$$

$$\vec{E} = 59.9731 \hat{a}_x - 71.988 \hat{a}_y - 20 \hat{a}_z \quad \text{V/m}$$

$$E = 95.807 \text{ V/m}$$

$$\vec{D} = \epsilon \vec{E}$$

$$\vec{D} = 8.854 \times 10^{-12} (\vec{E})$$

$$\vec{D} = (531.001 \hat{a}_x - 637.381 \hat{a}_y - 177.08 \hat{a}_z) \times 10^{-12}$$

$$\vec{D} = (0.531 \hat{a}_x - 0.637 \hat{a}_y - 0.177 \hat{a}_z) \text{ N} \left(\frac{\text{V}}{\text{m}} \times \frac{\text{F}}{\text{m}} \right)$$

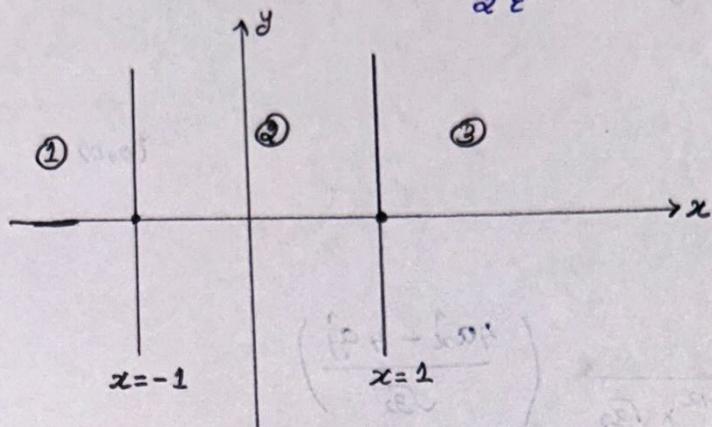
$$\vec{D} = (0.531 \hat{a}_x - 0.637 \hat{a}_y - 0.177 \hat{a}_z) \text{ N} \frac{\text{C}}{\text{m}^2}$$

$$= \frac{N}{C} \times \frac{C^2}{m^2 N} = \frac{C}{m^2}$$

3. Two infinite uniform sheets of charge each with density located at $x = \pm 1$ determine E in all regions.

solu:

E due to infinite sheet is $\vec{E} = \frac{\rho_s}{2\epsilon_0} \hat{a}_x$



Region 1:

$$\vec{E} = \left[\frac{\rho_s}{2\epsilon_0} + \frac{\rho_s}{2\epsilon_0} \right] (-\hat{a}_x)$$

$$\vec{E} = \frac{2\rho_s}{2\epsilon_0} (-\hat{a}_x)$$

$$\vec{E} = -\frac{\rho_s}{\epsilon_0} \hat{a}_x \quad |_{x < -1}$$

Region 2:

$$\vec{E} = \frac{\rho_s}{2\epsilon_0} \hat{a}_x + \frac{\rho_s}{2\epsilon_0} (-\hat{a}_x)$$

$$\vec{E} = 0 \quad |_{-1 < x < 1}$$

Region 3:

$$\vec{E} = \frac{\rho_s}{2\epsilon_0} \hat{a}_x + \frac{\rho_s}{2\epsilon_0} \hat{a}_x$$

$$\vec{E} = \frac{\rho_s}{\epsilon_0} \hat{a}_x \quad |_{x > 1}$$

4) Two straight wires (con conductors) parallel to z-axis passing through points O and A. The wires carry equal & uniform charges of density $0.4 \mu C/m$. Determine E at point P

Sol:

$$\vec{E} = \frac{\lambda}{2\pi\epsilon_0 r} \hat{a}_r \text{ (line charge)}$$

Point O:

$$\vec{r} = 4\hat{a}_x - 4\hat{a}_y$$

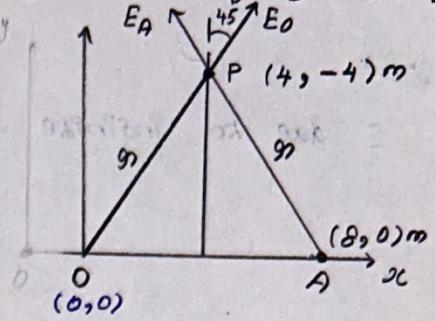
$$|\vec{r}| = \sqrt{32}$$

$$\vec{E}_O = \frac{0.4\mu}{2\pi \times 8.854 \times 10^{-12} \times \sqrt{32}} \left(\frac{4\hat{a}_x - 4\hat{a}_y}{\sqrt{32}} \right)$$

$$\vec{E}_O = \frac{0.4}{2\pi \times 32 \times 8.854 \times 10^{-6}} (4\hat{a}_x - 4\hat{a}_y)$$

$$\vec{E}_O = 0.2469356 (4\hat{a}_x - 4\hat{a}_y)$$

$$\boxed{\vec{E}_O = 898.77 \hat{a}_x - 898.77 \hat{a}_y \text{ V/m}}$$



Point A:

$$\vec{r} = -4\hat{a}_x - 4\hat{a}_y$$

$$|\vec{r}| = \sqrt{32}$$

$$\vec{E}_A = \frac{0.4\mu}{2\pi \times 8.854 \times 10^{-12} \times \sqrt{32}} \left(\frac{-4\hat{a}_x - 4\hat{a}_y}{\sqrt{32}} \right)$$

$$\vec{E}_A = -0.2469356 (4\hat{a}_x + 4\hat{a}_y)$$

$$\boxed{\vec{E}_A = -898.77 \hat{a}_x - 898.77 \hat{a}_y \text{ V/m}}$$

$$\boxed{\vec{E}_A = 1271.05 \text{ V/m}}$$

By superposition

$$\vec{E}_P = \vec{E}_O + \vec{E}_A$$

$$\boxed{\vec{E}_P = -1797.54 \hat{a}_y \text{ V/m}}$$