

Vibrational isolation of pump unit

Project description

A pump unit on an industrial floor causes vibrations that spread to the building's structure and disturb nearby equipment. The assignment is to model the system as a 1-DOF mass-spring system assuming a machine weight of 150 kg and a rotational speed of 1800 rpm. The goal is to reduce the force transmission to the structure by at least 70%. Identify critical operating modes and dimension a new isolating mount (spring constant and potential damping).

Assumptions

1. Pump is not in the isolated region, meaning the force transmissibility is ≥ 1 . This will act as our reference in order to reduce the force by at least 70%. In reality we might want to experimentally or theoretically determine the natural frequency and thereby also the actual force transmissibility.
2. The original pump mount (spring) is replaced by a new mount and therefore the original spring constant doesn't affect the new system.
3. The rotating unbalance is the dominating vibration, and other vibrations from the environment can be neglected.

Data

```
In[1]:= Remove["Global`*"]
m = 150; (*kg*)
N = 1800; (*rpm*)
g = 981 * 10^-2; (*m/s^2*)
```

Force frequency

$$\text{In[2]:= } \omega = N \frac{2\pi}{60}; (\text{rad/s})$$

Force transmissibility

$$T_f = r^2 \sqrt{\frac{1 + (2\xi r)^2}{(1 - r^2)^2 + (2\xi r)^2}};$$

(*For rotating unbalance. r = Frequency ratio, ξ = Damping ratio*)

```
In[3]:= $Assumptions = {r > 0, \xi > 0};
```

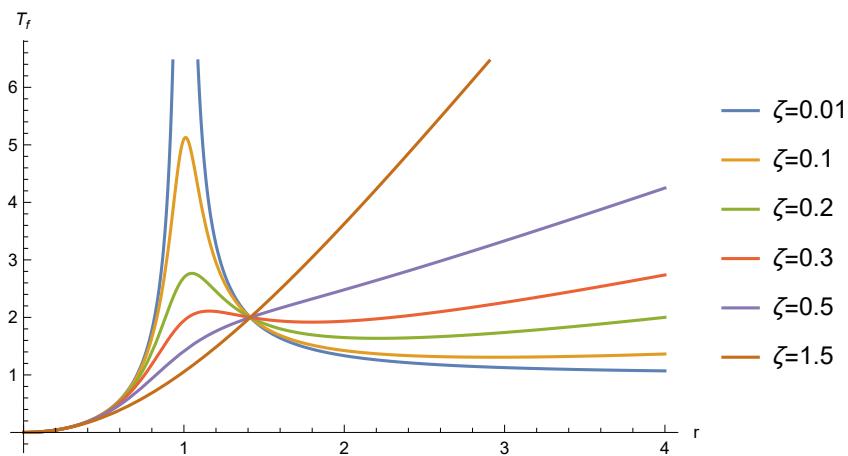
Damping ratio

Although damping is not required in this case, some damping is recommended as to not result in extremely high force transmissibility in the case that the pump is subject to its resonance frequency. Surrounding machines and other vibration sources in the operating environment should

be taken into account. For this example we choose a moderate damping ratio of $\zeta = 0.3$.

```
In[6]:= Plot[{Tf /. ζ → 0.01, Tf /. ζ → 0.1, Tf /. ζ → 0.2,
          Tf /. ζ → 0.3, Tf /. ζ → 0.5, Tf /. ζ → 1.5}, {r, 0, 4},
          PlotLegends → {"ζ=0.01", "ζ=0.1", "ζ=0.2", "ζ=0.3", "ζ=0.5", "ζ=1.5"},

Out[6]=
```



```
In[7]:= ζ = 0.3;
```

Required frequency ratio

```
In[8]:= solr = Solve[Tf == 0.3, r, PositiveReals] // Normal // Flatten // Quiet
Out[8]=
```

Frequency ratio

```
In[9]:= ωn = ω / . solr;
```

Spring constant

```
In[10]:= k = ωn^2 m
```

```
Out[10]=
```

$$2.26205 \times 10^7$$

Damping constant

Critical

```
In[11]:= Cc = 2 √(k m);
```

Actual

```
In[1]:= C = \(\mathbf{C}\) \(\mathbf{C}^T\)
Out[1]=
34950.
```

Static displacement

```
In[2]:= \(\delta\)st = \(\frac{m g}{k}\) // EngineeringForm
Out[2]//EngineeringForm=
65.0517 \(\times 10^{-6}\)
( \(\approx 0\))
```

Resonance speed

$r = 1$ gives

```
In[3]:= solwr = Solve[1 == \(\frac{\omega r}{\omega n}\), \(\omega r\)] // Flatten
Out[3]=
\{\(\omega r \rightarrow 388.334\)\}
```

In rpm

```
In[4]:= wr \(\frac{60}{2 \pi}\) /. solwr
Out[4]=
3708.31
```

Solution

Spring constant: $k \geq 22.6 \text{ MN/m}$

Damping constant: $c = 35.0 \text{ kNs/m}$

Resonance speed: $\sim 3710 \text{ rpm}$

If our assumptions are applicable, we will see $\geq 70\%$ reduction in the force transmitted into the surroundings. The static deflection is almost zero as not to exceed elastic limits of the new springs. The pump should always operate well below 3700 rpm.