Helical resonator

Goal

To trap ions within a Paul trap a high radio frequency voltage is applied to electrodes in order to provide the required electric potentials.

A helical resonator allows impedance matching between a radio frequency source and an ion tap enabling **high voltages** while reducing **the noise** injected into the system.

Goal

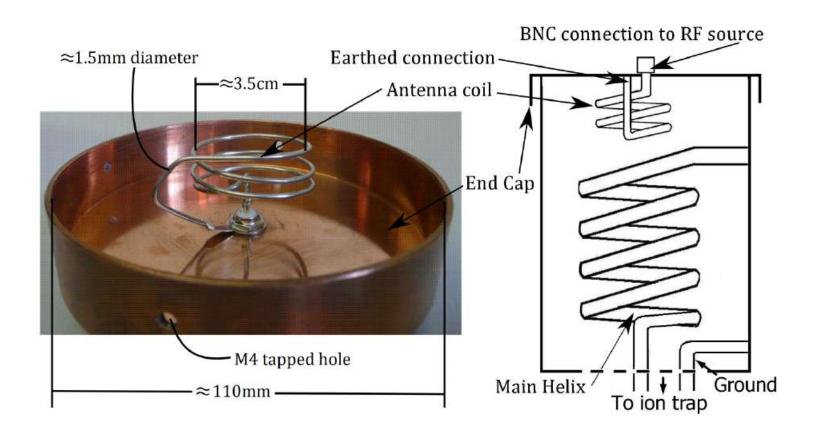
high voltage: *resonate frequency* → impedance matching

- → maximum power on load impedance
- → maximum voltage between the trap

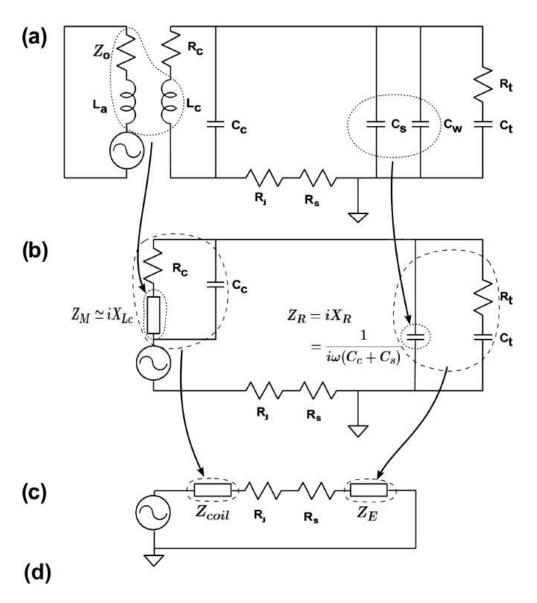
Less noise: $high Q \rightarrow$ frequency selectivity

→ less noise

structure



Structure



 Z_{coil} Equivalent impedance of the Helical coil due to:

 R_c Helical coil resistance

 C_c Helical coil self capacitance

 Z_M Helical coil total inductance due to:

 L_c Helical coil self inductance

 L_a Antenna coil self inductance

 Z_o RF voltage source impedance (typically 50Ω)

 Z_E Equivalent impedance of the experimental system due to:

 R_t Ion trap resistance

 C_t Ion trap capacitance

 X_R Equivalent capacitance due to:

 C_s Capacitance of Helical coil to surrounding shield

 C_w Capacitance of the ion trap connecting wires

 R_i Helical coil to shield junction resistance

 R_s Shield resistance

condition

At resonance: the imaginary part of the impedance is 0, which determines "b".

$$X_{tot} = 0$$

High Q:

$$Q = \frac{X_{L_c}}{R_{ESR}}$$

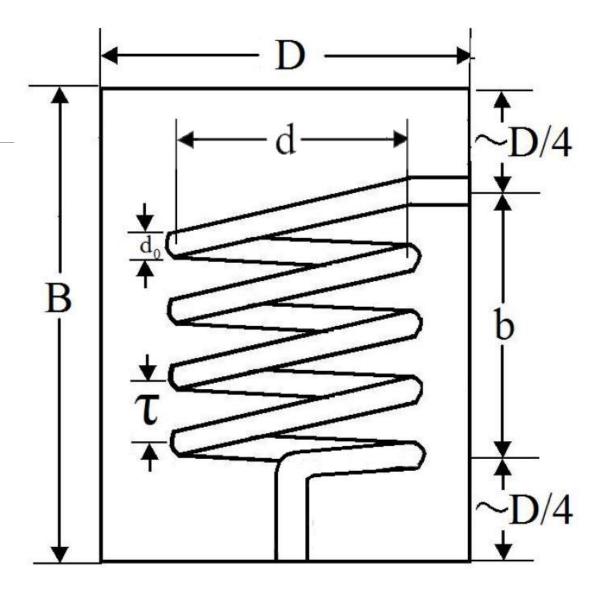
Empirical formula

If b>d

$$C_C \simeq (Hd/100) \times 10^{-12}$$

$$C_s \simeq 39.37b \frac{0.75}{\log\left(\frac{D}{d}\right)} \times 10^{-12} = K_C(d, D) b$$

$$L_C \simeq 39.37b \frac{0.025d^2(1-\frac{d}{D})^2}{\tau^2} \times 10^{-6} = K_L(d, D, \tau) b$$



resistance

$$R_n = \frac{\rho l}{C\delta_n}$$

$$\delta_n = \sqrt{(2\rho)/(\pi f_n \mu_0)}$$

$$R_0 = R_1 \sqrt{\frac{f_0}{f_1}}$$

Only valid: in a frequency regime where the solder joint is larger than the skin depth and when the resistivity, ρ , is constant over the two frequencies used.

Result of calculation

Resonate →

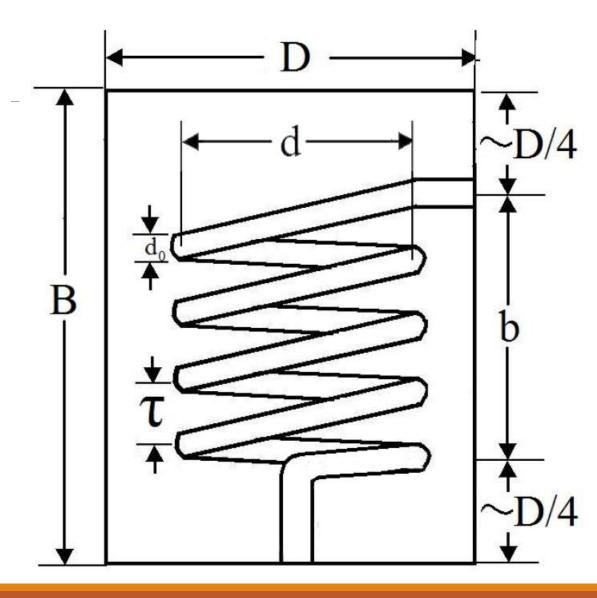
$$b \simeq \sqrt{\frac{1}{K_C K_L (2\pi f_0)^2} + \frac{C_{\Sigma}^2}{4K_C^2}} - \frac{C_{\Sigma}}{2K_C}$$

Size and frequency →

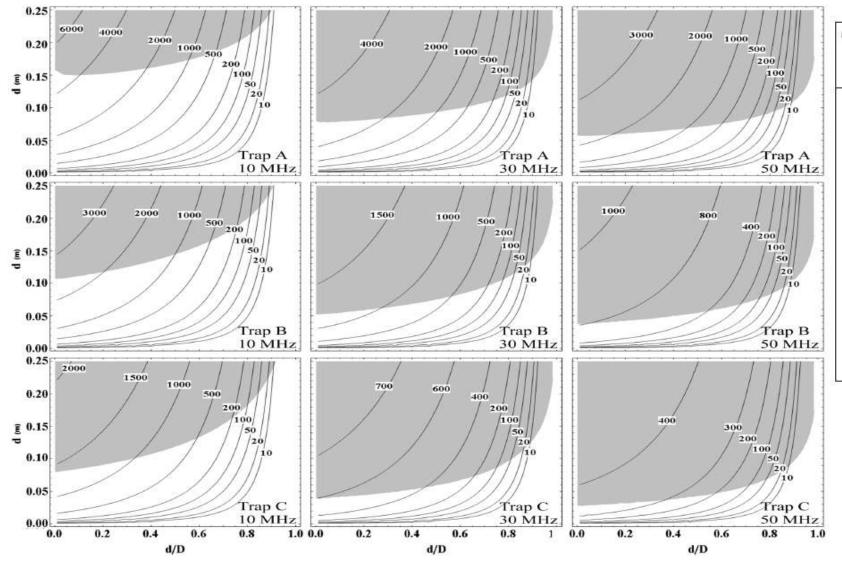
$$Q = \frac{X_{L_c}}{R_{_{ESR}}}$$

Specific process of calculation

- b(d, d/D) The coil length by using equation 27 and K_c and K_l from equation 25 and 26
- $C_s(d, d/D)$ The coil to shield capacitance by substituting b(d, d/D) into equation 25
- $C_c(d, d/D)$ The coil self capacitance by substituting b(d, d/D) into equation 25
- $R_s(d,d/D)$ The shield resistance by using equation 34
- $R_c(d,d/D)$ The coil resistance by using equation 33
- $R_{ESR}(d,d/D)$ The total resistance by using equation 23
- $L_c(d, d/D)$ The coil inductance by substituting b(d, d/D) into equation 26
- Q(d, d/D) The Q factor by substituting $L_c(d, d/D)$ & $R_{ESR}(d, d/D)$ into equation 21

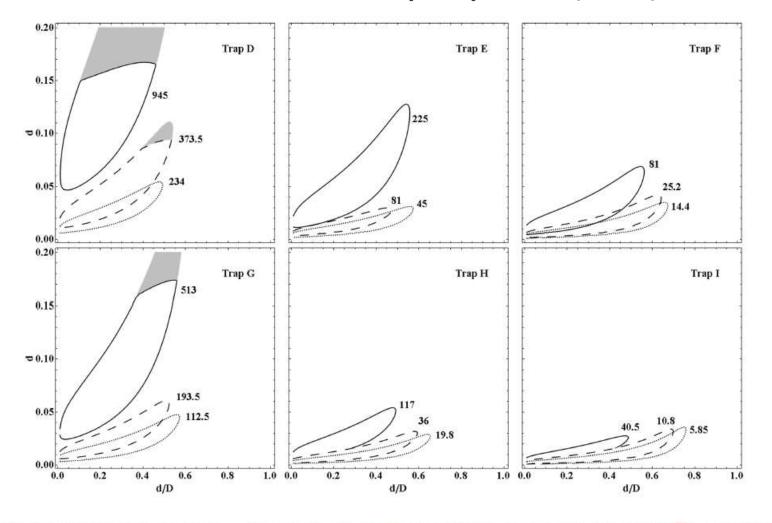


Result from the paper (?)



| Trap | Resistance | Capacitance | |
|--------------|------------|-------------|--|
| | Ω | pF | |
| A | 0.1 | 5 | |
| В | 0.1 | 20 | |
| \mathbf{C} | 0.1 | 50 | |
| D | 5 | 5 | |
| \mathbf{E} | 5 | 20 | |
| \mathbf{F} | 5 | 50 | |
| G | 15 | 5 | |
| \mathbf{H} | 15 | 20 | |
| I | 15 | 50 | |

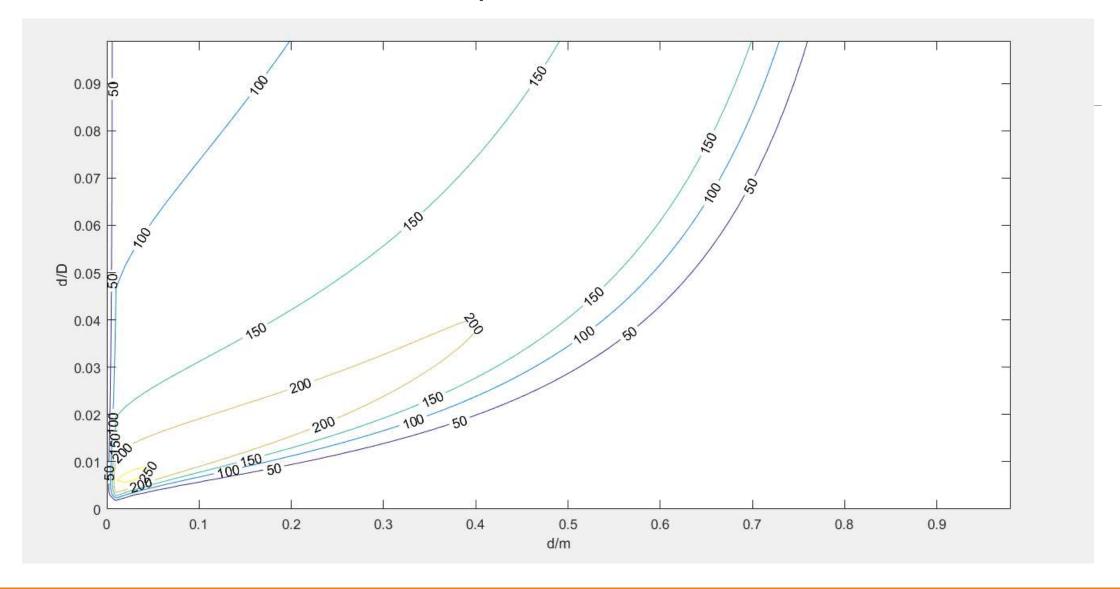
Result from the paper (?)



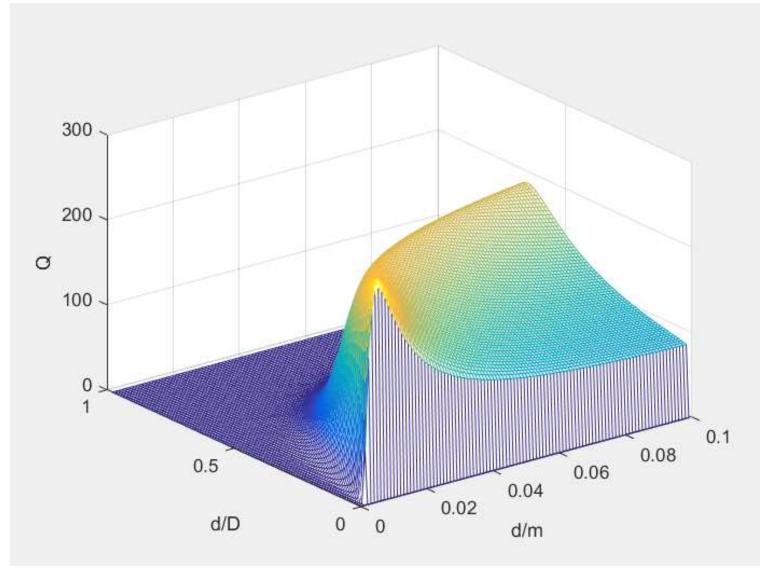
| Trap | Resistance | Capacitance | |
|--------------|------------|-------------|--|
| | Ω | pF | |
| A | 0.1 | 5 | |
| В | 0.1 | 20 | |
| \mathbf{C} | 0.1 | 50 | |
| D | 5 | 5 | |
| \mathbf{E} | 5 | 20 | |
| \mathbf{F} | 5 | 50 | |
| G | 1 5 | 5 | |
| \mathbf{H} | 15 | 20 | |
| \mathbf{I} | 15 | 50 | |

FIG. 11: Contour plots showing $Q_{90\%}$ for each set of paramters coresponding to traps D to I from table I for operating frequencies of 10 MHz (solid lines), 30 MHz (dashed lines) and 50 MHz (dotted lines). The grey areas indicate where b/d < 1 therefore invalidating the theory. The value of $Q_{90\%}$ is indicated next to the contour line.

Our result about trap D



Our result about trap D



pho= 1.678E-8; %电阻率

f0=50E6; %频率

t= 0.01; %线圈相邻圈间距

d0=0.005; %线圈直径

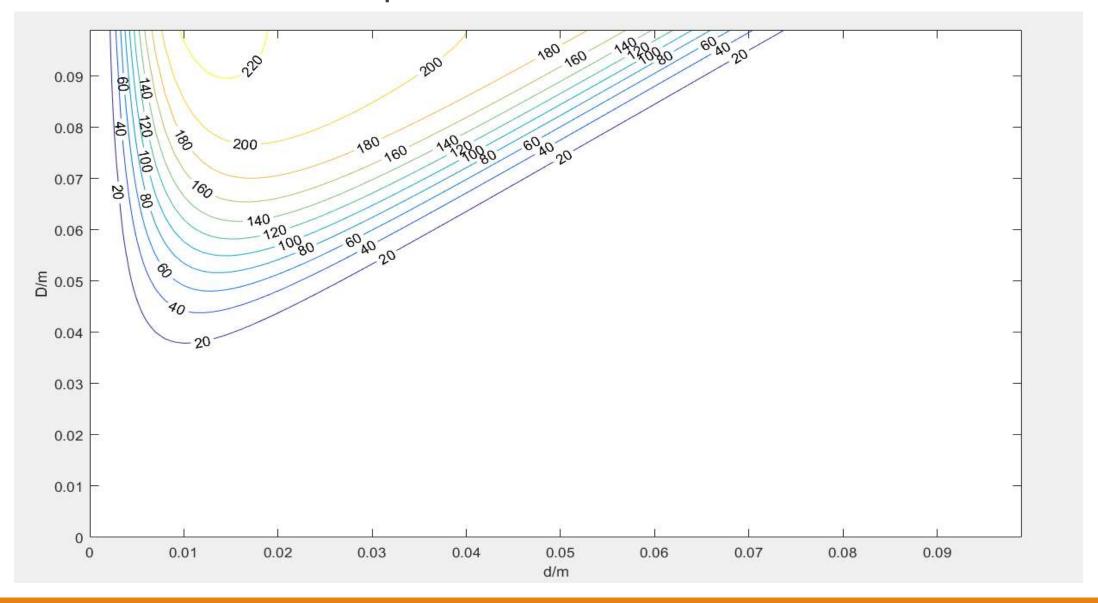
Rj=0; %连接点电阻

Ct=5E-12; %trap的电容

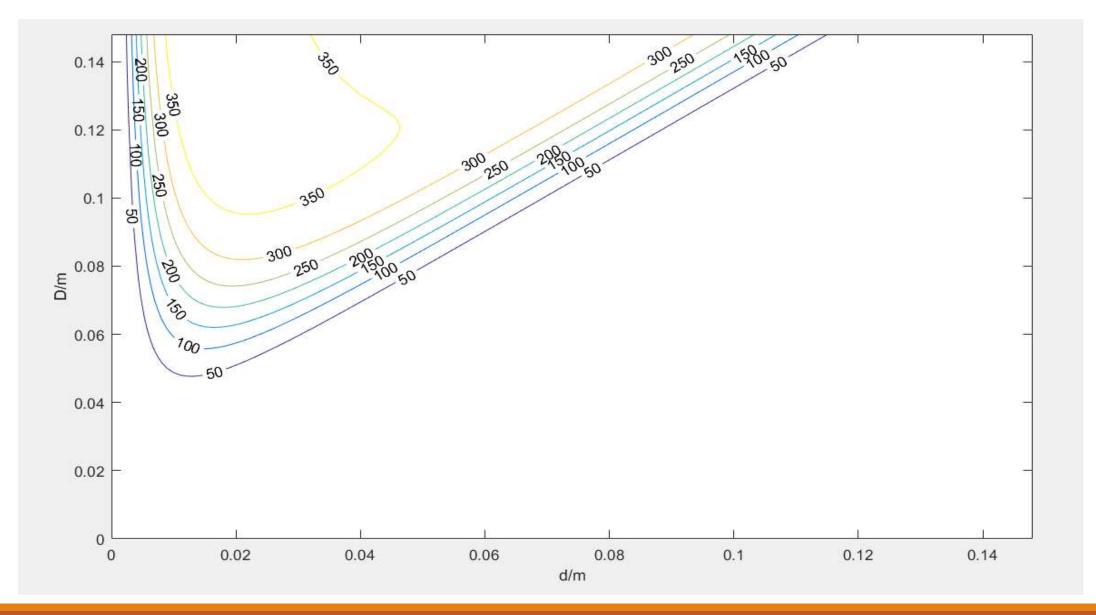
Rt=5; %trap的电阻

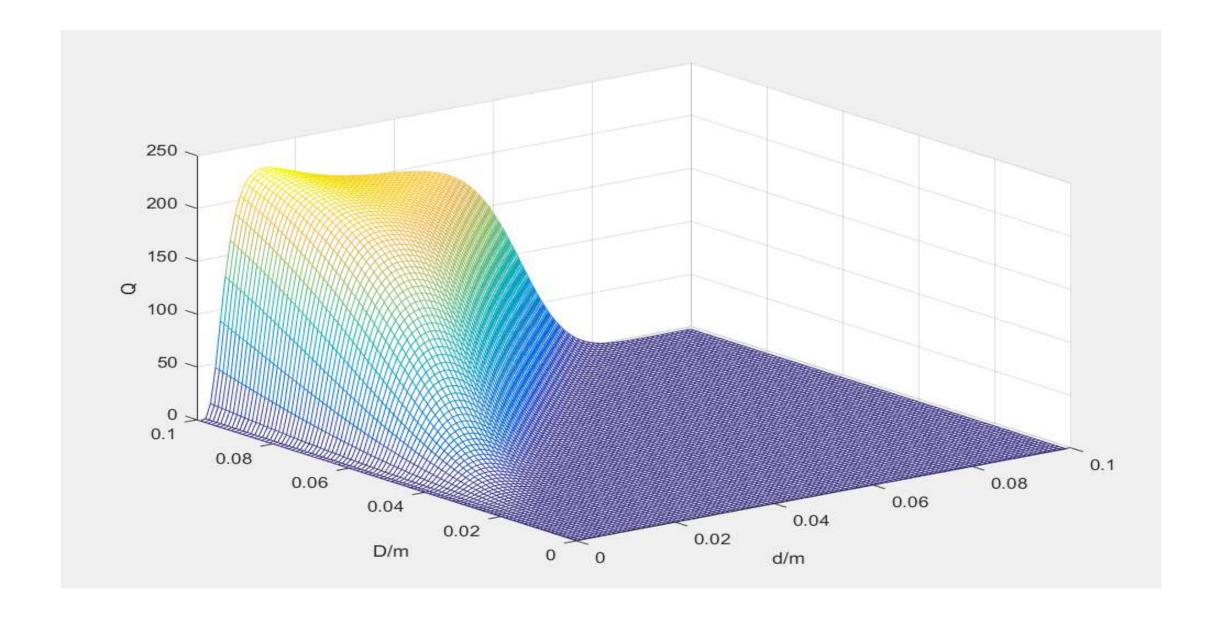
Cw=0; %连接线电容

Our result of trap D



Larger range



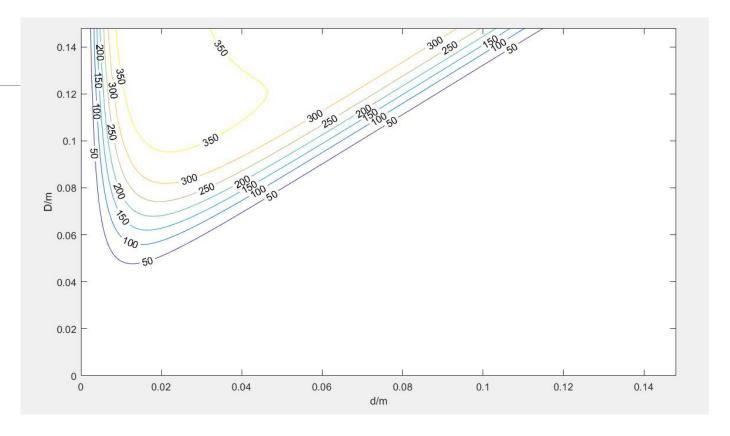


About the design

$$b \simeq \sqrt{\frac{1}{K_C K_L (2\pi f_0)^2} + \frac{C_{\Sigma}^2}{4K_C^2}} - \frac{C_{\Sigma}}{2K_C}$$

$$K_L \approx d^2 \cdot const$$

$$\rightarrow$$
 b · d $\approx \frac{1}{f_0} \cdot const$



About the design

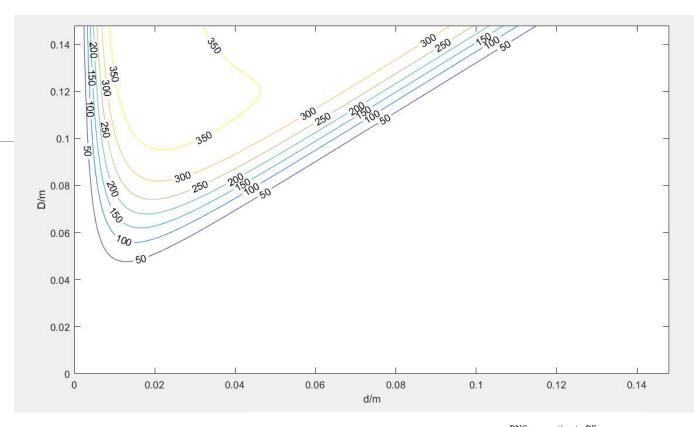
$$b \cdot d \approx \frac{1}{f_0} \cdot const$$

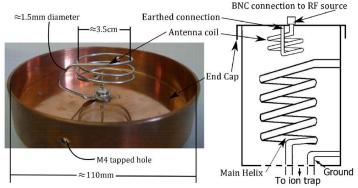
$$h = b + D/2$$

We want small size and a high Q:

So we choose a D less than 12cm so that we can choose a larger d and at the same time a Larger Q

★ Notice: Although a larger D will be more likely to bring a higher Q, It also may make h bigger and make the whole size bigger.





My design

```
f0=4e+007
                                       f0=5e+007
d=0.053m
                                       d=0.055m
D=0. 103m
                                       D=0.103m
Q=528. 535
                                       Q=679. 268
                                       b=0.0993721m
b=0.131594m
h=0. 183094m
                                       h=0.150872m
                                       检验信息:
检验信息:
                                       b=0.0993721m 满足b>d, valid!
b=0.131594m 满足b>d, valid!
                                       趋肤深度为1.30391e-005m<1mm. 足够小!
趋肤深度为1.45781e-005m<1mm. 足够小!
                                       resonator尺寸信息:
resonator尺寸信息:
                                       height=15.0872cm
height=18.3094cm
                                       Diameter=10.3cm
Diameter=10.3cm
                                       Vpeak=1395. 72
Vpeak=1323. 21
```

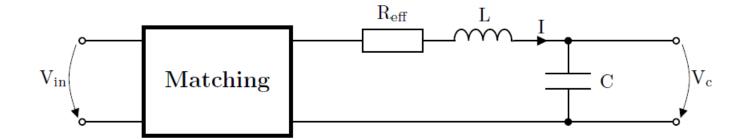
The end

About this design



Another design

OF RESONATORS WE MAY BE INTERESTED IN

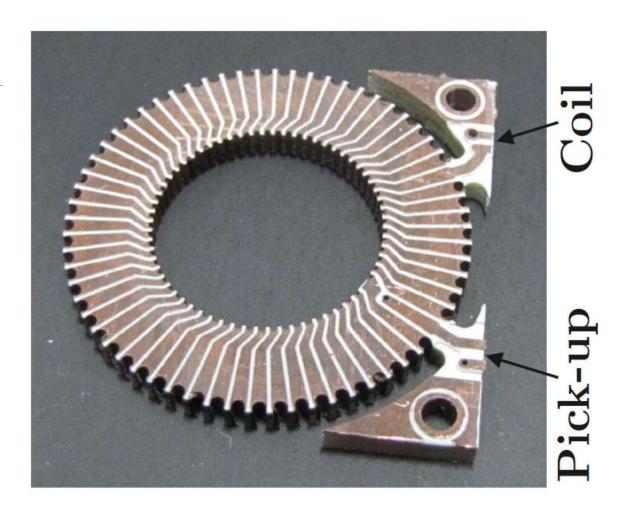


An *RLC*-series-resonator driven through a *matching* network

Coils produced with machines are desirable because the production process is reproducible. Furthermore, we prefer toroid coils as they guide the magnetic field in their center, making them less Sensitive to their environment.

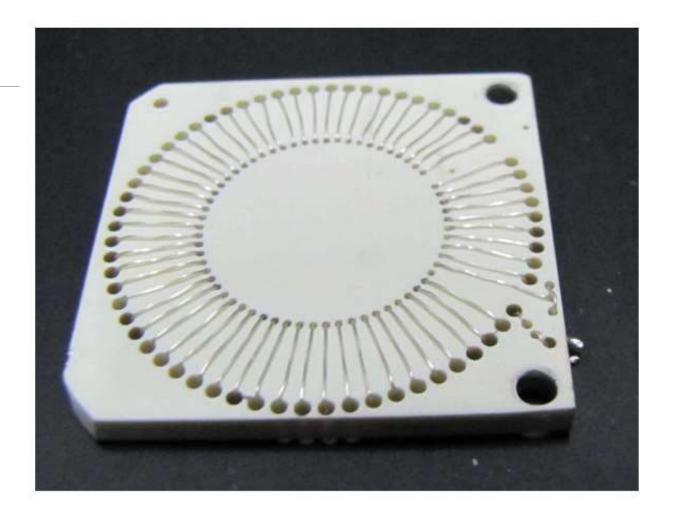
Different designs

1.PCB coils



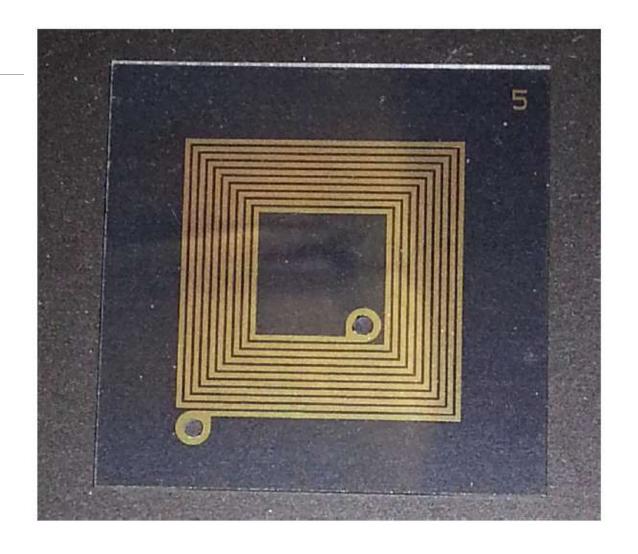
Different designs

2.wire coils

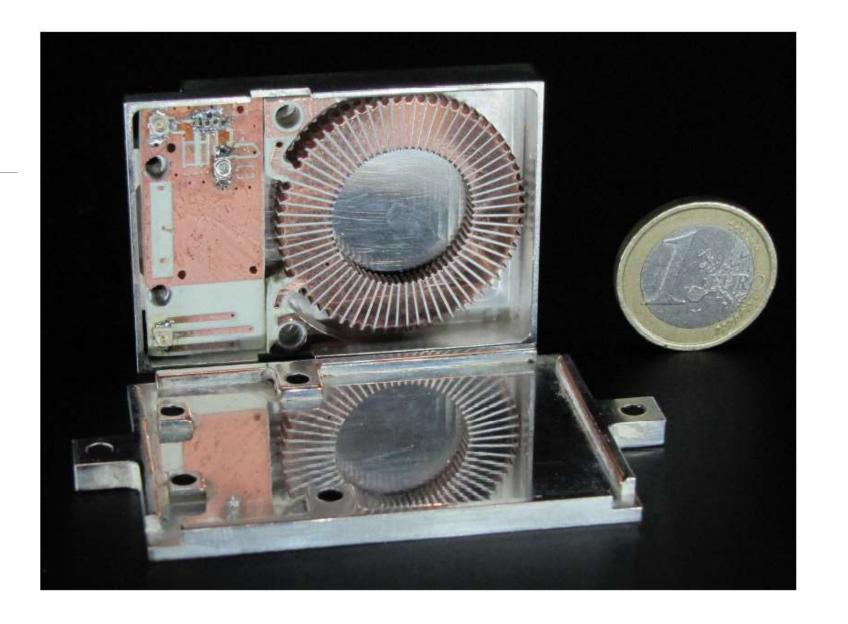


Different designs

3.Spiral coils



Small size



effective

| Name | ${f T}$ | $ m f_{res}$ | G_{V} | Q_{coil} |
|-----------|-------------------------|---------------------|---------|------------|
| PCB coil | 295K | 42.4MHz | 19.4 | 60 |
| PCB coil | $\sim \! 80 \mathrm{K}$ | $42.8 \mathrm{MHz}$ | 27.1 | 115 |
| PCB coil | $\sim 10 \mathrm{K}$ | $42.9 \mathrm{MHz}$ | 41.5 | 208 |
| Wire Coil | 295K | 36.8 MHz | 25.2 | 89 |
| Wire Coil | $\sim 80 \mathrm{K}$ | $37.2 \mathrm{MHz}$ | 36.5 | 184 |
| Wire Coil | $\sim 10 \mathrm{K}$ | $37.9 \mathrm{MHz}$ | 58.9 | 624 |
| HTS Coil | <88K | 44.3MHz | 92.1 | 1172 |

$$G_{
m V} = rac{V_{
m c}}{V_{
m in}}$$

Reference

[1] Siverns J D, Simkins L R, Weidt S, et al. On the application of radio frequency voltages to ion traps via helical resonators[J]. Applied Physics B, 2012, 107(4):921-934.

[2] Matthias F. Brandl, Philipp Schindler, Thomas Monz, Rainer Blatt, Cryogenic resonator design for trapped ion experiments in Paul traps, arxiv:1601.06699

The end

THANK YOU