

ELCE 705

DIGITAL SIGNAL PROCESSING

Sampling of
continuous-time signals
(4.6- 4.8 exclude 4.7.6)

Contents

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- Change the sampling Rate
- Multirate signal processing
- Digital Processing of Analog Signals

Changing the Sampling Rate

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- A continuous-time signal can be represented by its samples as

$$x[n] = x_c(nT)$$

- Some applications require us to change the sampling rate
 - ▢ To obtain a new discrete-time signal from the same CT signal

$$x'[n] = x_c(nT') \quad \text{where } T \neq T'$$

- One way of accomplishing this is to
 - ▢ Reconstruct the continuous-time signal from $x[n]$
 - ▢ Resample the continuous-time signal using new rate to get $x'[n]$
 - ▢ This requires analog processing which is often undesired
- **Target: get $x'[n]$ directly from $x[n]$**

Downsampling (Compressor)

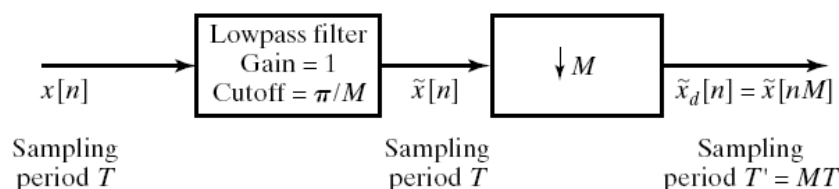
- Sampling Rate Reduction by an Integer Factor

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- Reduce the sampling rate of a sequence by “**sampling**” it

$$x_d[n] = x[nM] = x_c(nMT) \quad T_d = MT$$

- This is accomplished with a **sampling rate compressor**



- $x_d[n]$ is identical to what being got by reconstructing the signal and resampling it with $T'=MT$
- There will be no aliasing if $\frac{\pi}{T'} = \frac{\pi}{MT} > \Omega_N$

Frequency Domain Representation

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- Recall the DTFT of $x[n]=x_c(nT)$

$$X(e^{j\omega}) = \frac{1}{T} \sum_{k=-\infty}^{\infty} X_c \left(j \left(\frac{\omega}{T} - \frac{2\pi k}{T} \right) \right)$$

- The DTFT of the downsampled signal can similarly written as

$$X_d(e^{j\omega}) = \frac{1}{T'} \sum_{r=-\infty}^{\infty} X_c \left(j \left(\frac{\omega}{T'} - \frac{2\pi r}{T'} \right) \right) = \frac{1}{MT} \sum_{r=-\infty}^{\infty} X_c \left(j \left(\frac{\omega}{MT} - \frac{2\pi r}{MT} \right) \right)$$

- Let's represent the summation index as

$$r = i + kM \quad \text{where} \quad -\infty < k < \infty \quad \text{and} \quad 0 \leq i < M$$

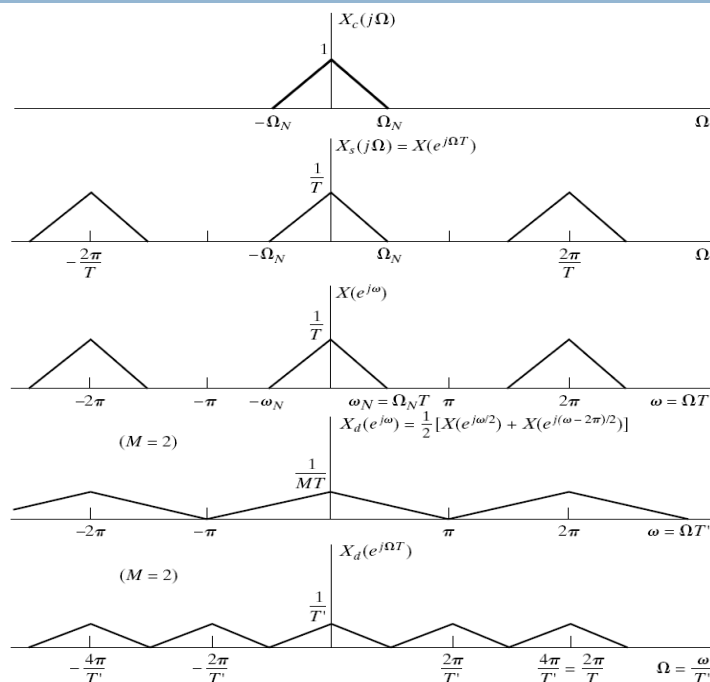
$$X_d(e^{j\omega}) = \frac{1}{M} \sum_{i=0}^{M-1} \left[\frac{1}{T} \sum_{k=-\infty}^{\infty} X_c \left(j \left(\frac{\omega}{MT} - \frac{2\pi k}{T} - \frac{2\pi i}{MT} \right) \right) \right]$$

- And finally

$$X_d(e^{j\omega}) = \frac{1}{M} \sum_{i=0}^{M-1} X \left(e^{j \left(\frac{\omega}{M} - \frac{2\pi i}{M} \right)} \right)$$

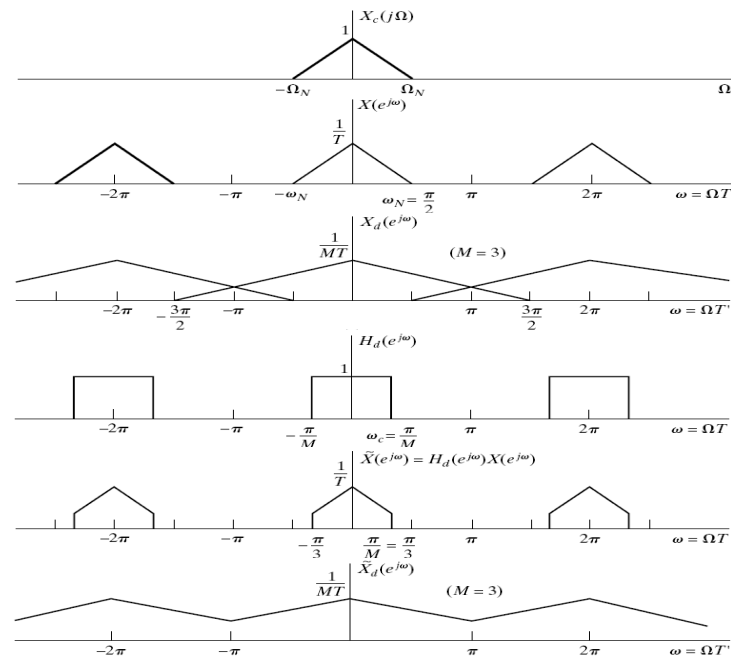
Frequency Domain Representation of Downsampling: No Aliasing

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Frequency Domain Representation

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Upsampling

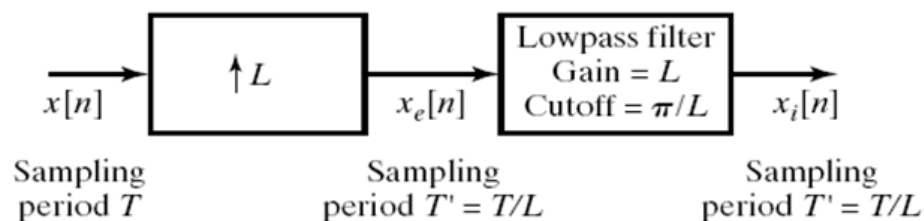
-Increasing the Sampling Rate by an Integer Factor

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- Increase the sampling rate of a sequence interpolating it

$$x_i[n] = x[n/L] = x_c(nT/L) \quad T_i = T/L$$

- This is accomplished with a sampling rate expander



- $x_i[n]$ is identical to sample with $T_i = T/L$

Upsampling

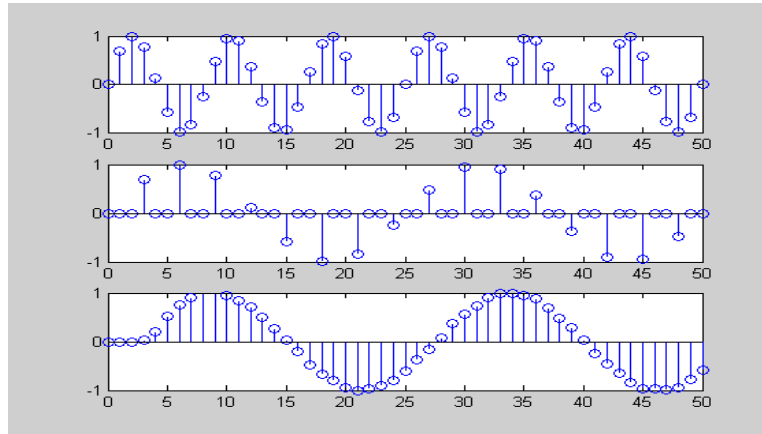
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□ Upsampling consists of **two steps**

➤ **Expander**

$$x_e[n] = \begin{cases} x[n/L] & n = 0, \pm L, \pm 2L, \dots \\ 0 & \text{else} \end{cases} = \sum_{k=-\infty}^{\infty} x[k] \delta[n - kL]$$

➤ **Interpolating** (Low pass filter)



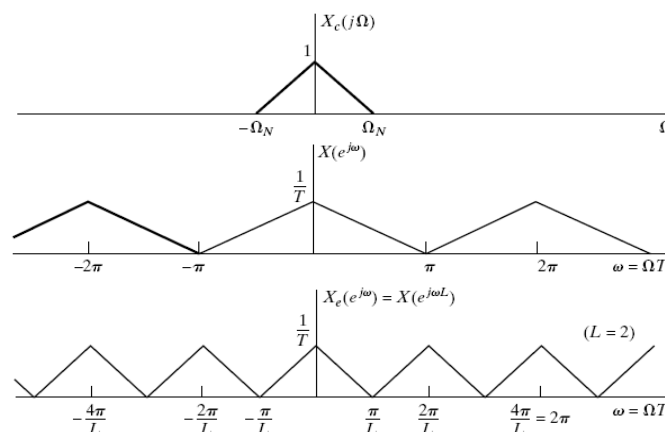
Frequency Domain Representation of Expander

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□ The DTFT of $x_e[n]$ can be written as

$$X_e(e^{j\omega}) = \sum_{n=-\infty}^{\infty} \left(\sum_{k=-\infty}^{\infty} x[k] \delta[n - kL] \right) e^{-j\omega n} = \sum_{k=-\infty}^{\infty} x[k] e^{-j\omega Lk} = X(e^{j\omega L})$$

□ The output of the expander is frequency-scaled

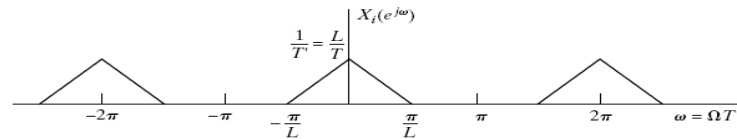


$$\omega = \Omega T_i$$

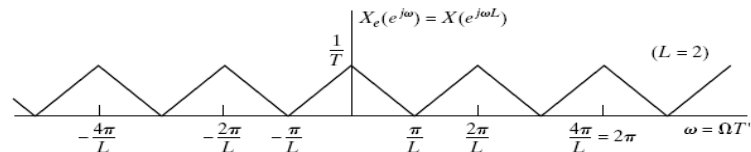
Frequency Domain Representation of Interpolator

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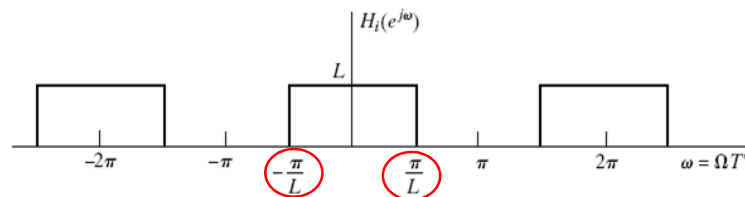
- The DTFT of the **desired interpolated signals** is



- The **extrapolator output** is given as



- Apply the LPF



Interpolator in Time Domain

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- Get an interpolation formula for $x_i[n]$ in terms of $x[n]$
- The low-pass filter impulse response is

$$h_i[n] = \frac{\sin(\pi n / L)}{\pi n / L}$$

- Hence the interpolated signal is written as

$$x_i[n] = \sum_{k=-\infty}^{\infty} x[k] \frac{\sin(\pi(n - kL) / L)}{\pi(n - kL) / L}$$

- Note that

$$\begin{aligned} h_i[0] &= 1 \\ h_i[n] &= 0 \quad n = \pm L, \pm 2L, \dots \end{aligned}$$

- Therefore the filter output can be written as

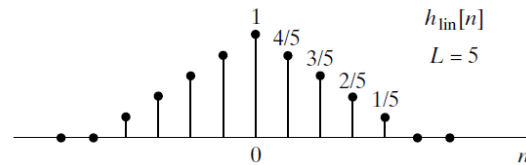
$$x_i[n] = x[n/L] = x_c(nT/L) = x_c(nT') \quad \text{for } n = 0, \pm L, \pm 2L, \dots$$

Linear Interpolation

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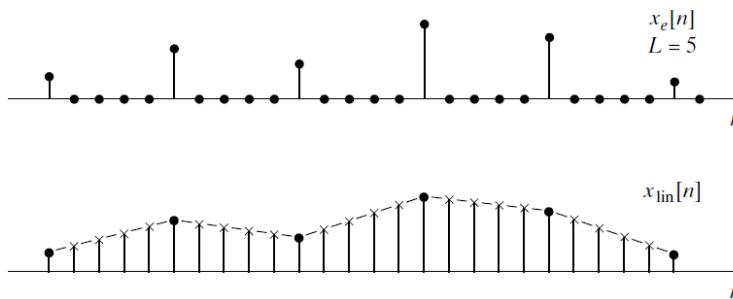
- The **impulse response** of the filter is

$$h_{lin}[n] = \begin{cases} 1 - |n|/L & |n| \leq L \\ 0 & \text{otherwise} \end{cases}$$



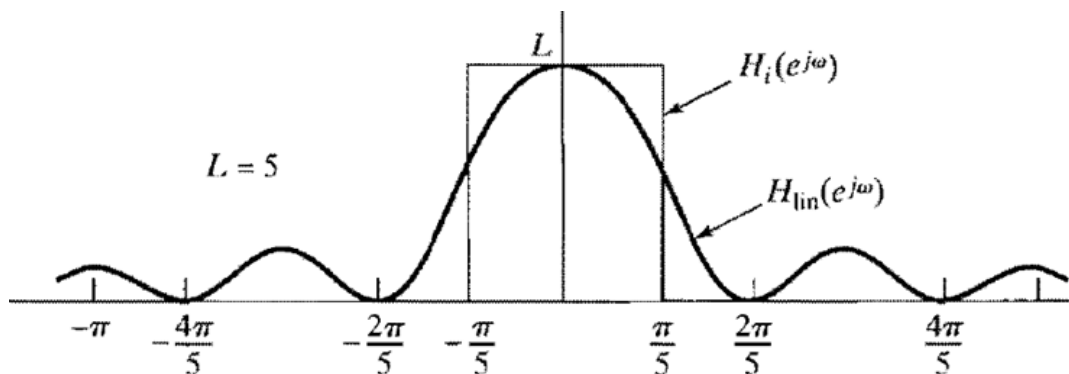
- The interpolated output

$$x_i[n] = \sum_{k=-\infty}^{\infty} x_e[k] h_{lin}[n-k] = \sum_{k=n-L+1}^{k=n+L-1} x_e[k] h_{lin}[n-k]$$



Compare the frequency response

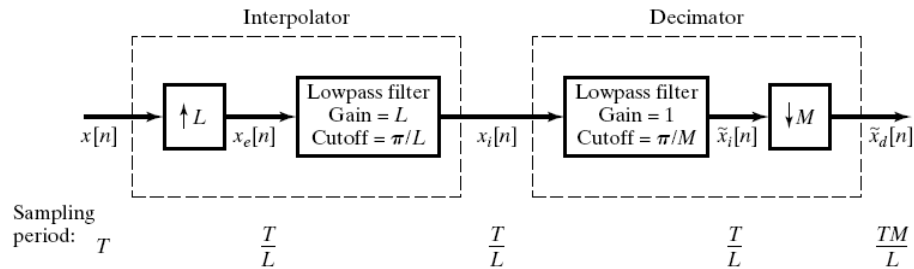
$$H_{lin}(e^{j\omega}) = \frac{1}{L} \left[\frac{\sin(\omega L / 2)}{\sin(\omega / 2)} \right]^2$$



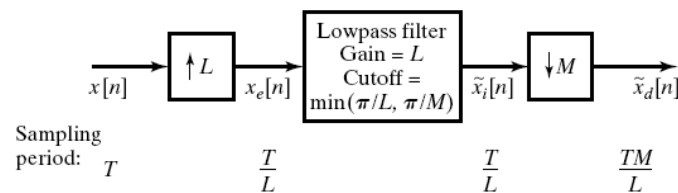
Changing the Sampling Rate by Non-Integer Factor

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- Combine decimation and interpolation for non-integer factors

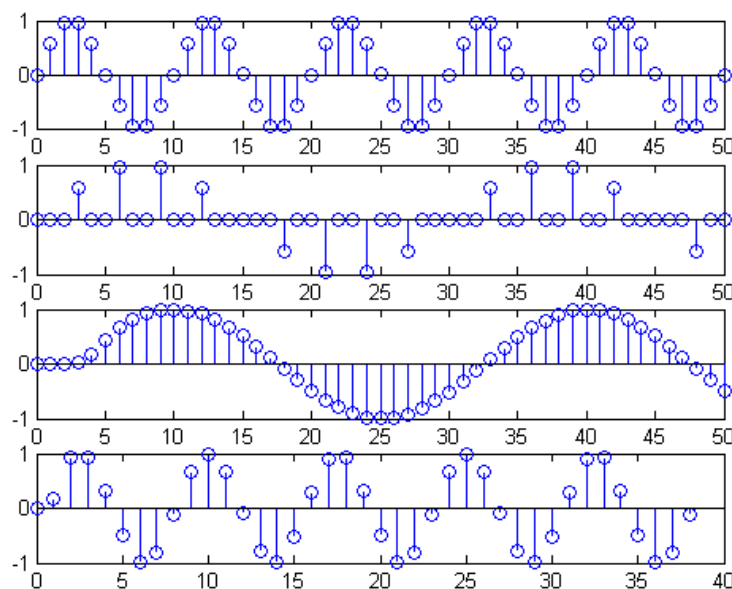


- The two low-pass filters can be combined into a single one



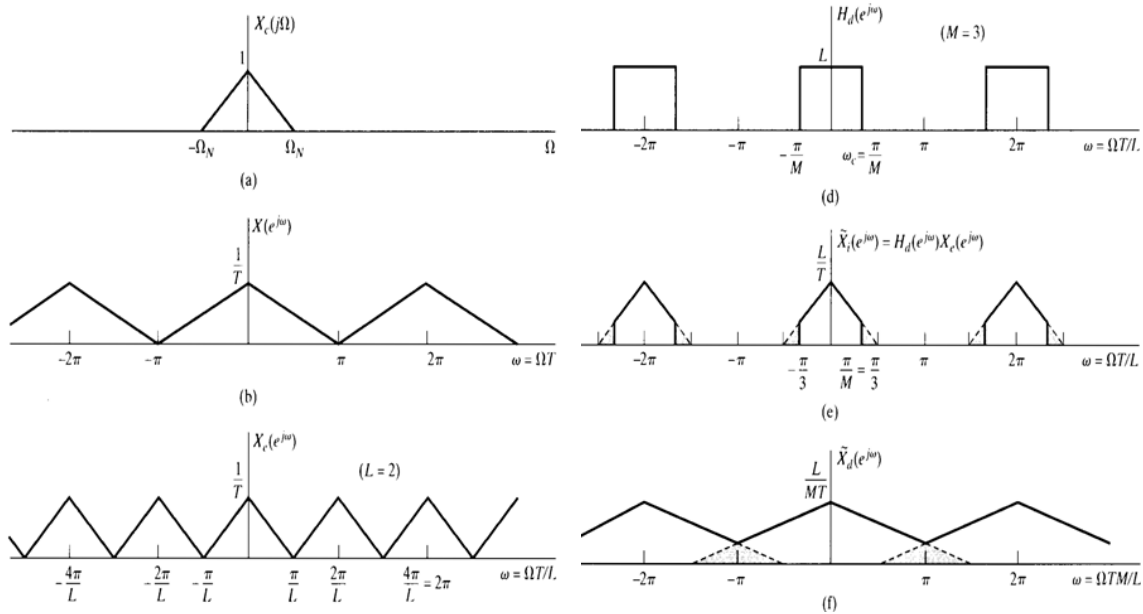
Changing the sampling rate by 4/3

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Example

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- Changing the sampling Rate
- Multirate signal processing
- Digital Processing of Analog Signals

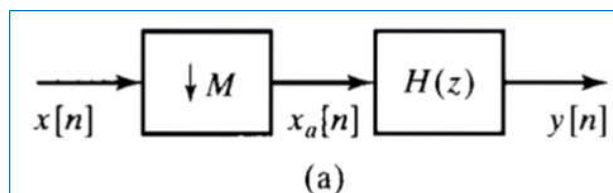
Multirate Signal Processing

- Change sampling rate by
 - ▣ Interpolation
 - ▣ Decimation
 - ▣ Combine them
- Multirate signal processing
 - ▣ Reduce the amount of computation required by sampling rate conversion
 - ▣ Two basic methods are discussed

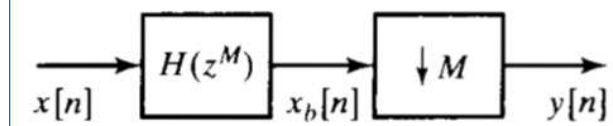
Interchange of filtering with compressor

$$Y(e^{j\omega}) = H(e^{j\omega}) \frac{1}{M} \sum_{i=0}^{M-1} X(e^{j(\omega/M - 2\pi i/M)})$$

$$= H(e^{j\omega}) X_a(e^{j\omega}).$$



$$X_b(e^{j\omega}) = H(e^{j\omega M}) X(e^{j\omega})$$

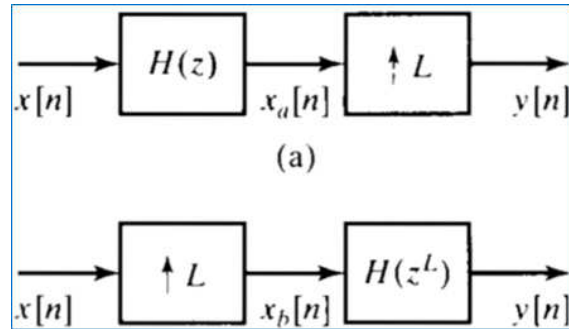


$$Y(e^{j\omega}) = \frac{1}{M} \sum_{i=0}^{M-1} X(e^{j(\omega/M - 2\pi i/M)}) H(e^{j(\omega - 2\pi i)})$$

Interchange of filtering with expander

$$Y(e^{j\omega}) = X_a(e^{j\omega L})$$

$$= X(e^{j\omega L})H(e^{j\omega L})$$



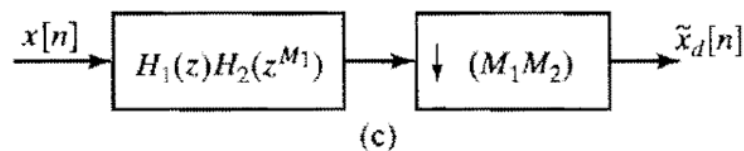
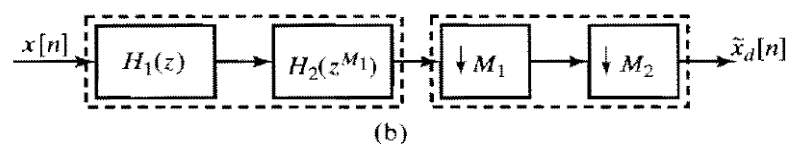
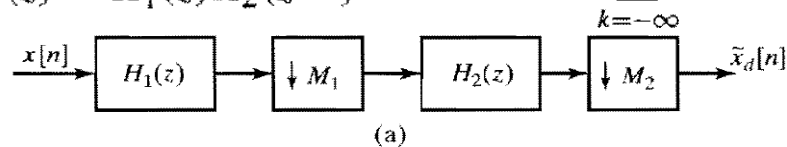
$$Y(e^{j\omega}) = H(e^{j\omega L})X_b(e^{j\omega})$$

Multistage Interpolation

□ Decimation or interpolation ratios are large

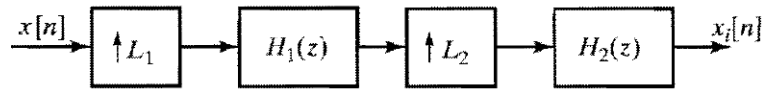
- ▣ Significant reduction in computation through multistage
- ▣ Interpolated FIR filter

$$H(z) = H_1(z)H_2(z^{M_1}) \quad h[n] = h_1[n] * \sum_{k=-\infty}^{\infty} h_2[k]\delta[n - kM_1]$$

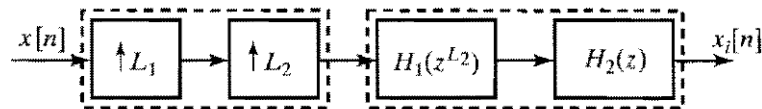


Multistage Decimation

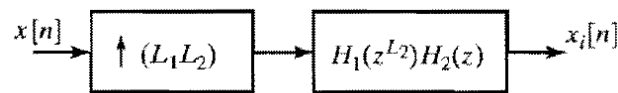
- Low pass filter: pass band gain 0dB, stop band gain -40dB
- $L=100$: transition band $0.008\pi \sim 0.012\pi$, FIR order **709**
- $L=10$: transition band $0.09\pi \sim 0.11\pi$, FIR order **142**



(a)



(b)



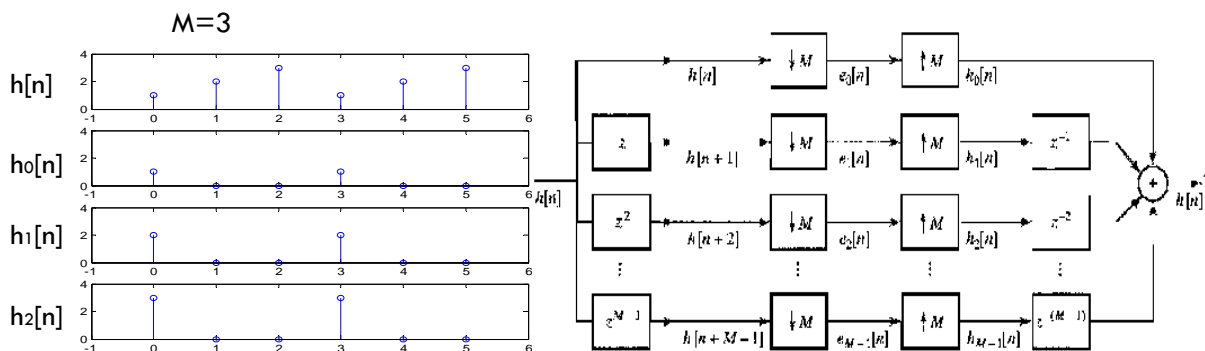
(c)

Polyphase decompositions

- $h[n]$ as superposition of M subsequences

$$h[n] = \sum_{k=0}^{M-1} h_k[n-k] \quad k=0, 1, \dots, M-1$$

$$h_k[n] = \begin{cases} h[n+k], & n = \text{integer multiple of } M \\ 0, & \text{otherwise.} \end{cases}$$

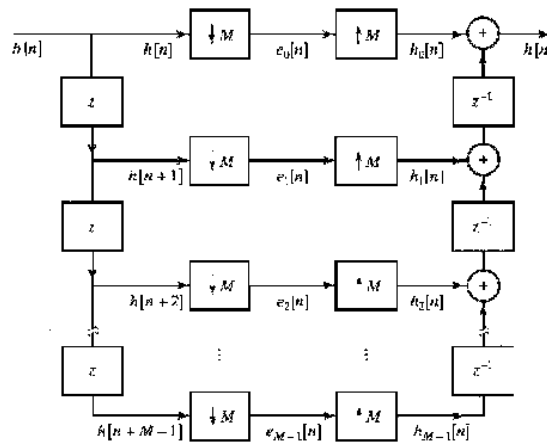
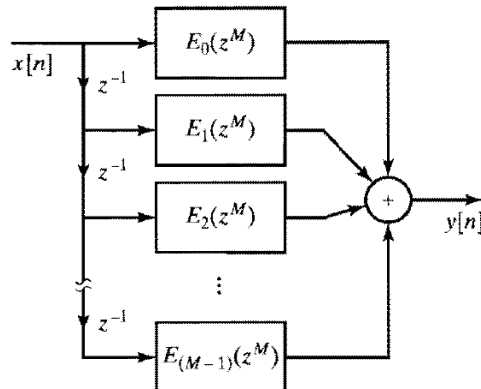


Polyphase decompositions

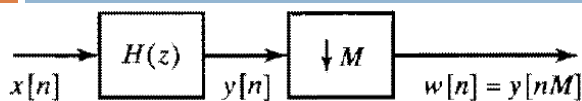
- Decompose to M parallel filters

$$H(z) = \sum_{k=0}^{M-1} E_k(z^M) z^{-k}$$

$$e_k[n] = h[nM + k] = h_k[nM]$$

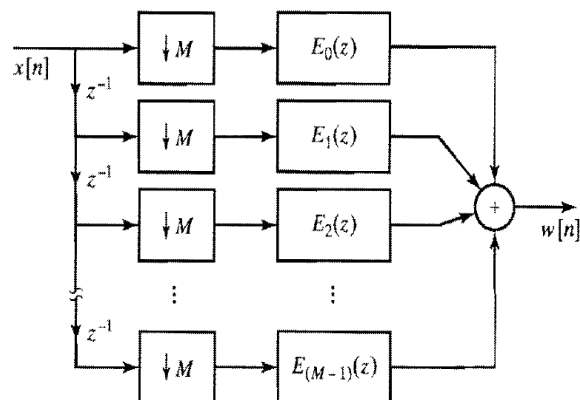
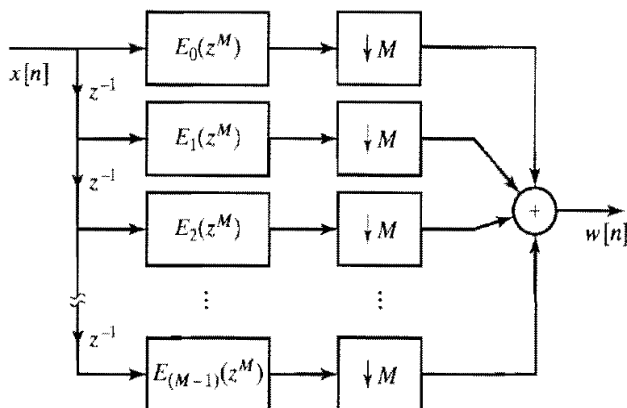


Polyphase implementation of decimation filters



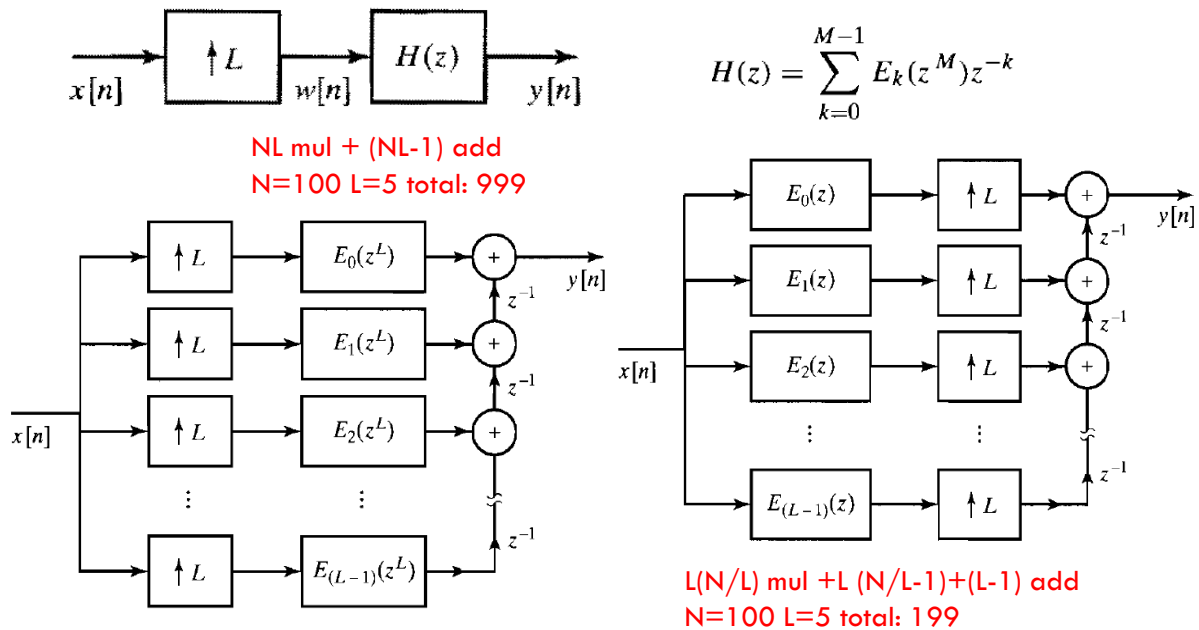
N mul + (N-1) add
N=100 total: 199

$$H(z) = \sum_{k=0}^{M-1} E_k(z^M) z^{-k}$$



N/M mul + (N/M-1)+(M-1)/M add
N=100 M=10 total: 20

Polyphase implementation of interpolation filters



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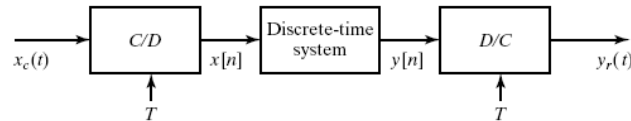
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- Changing the sampling Rate
- Multirate signal processing
- Digital Processing of Analog Signals

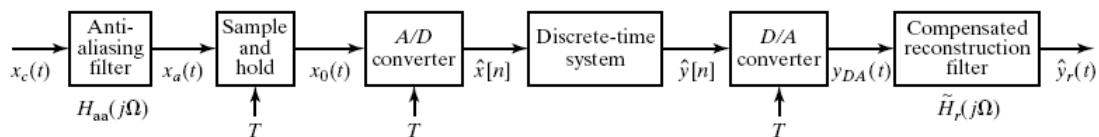
Ideal Conversion

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- Assume ideal D/C and C/D conversion



- In practice, however
 - Continuous-time signals are **not perfectly bandlimited**
 - D/C and C/D converters can only be **approximated with D/A and A/D converters**
- A more realistic model for digital signal processing



Prefiltering to Avoid Aliasing

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- Desirable to **minimize sampling rate**
 - Minimizes amount of data to process
 - Remove high frequencies (noises) that are not of interest
- A **low-pass anti-aliasing filter** would improve both aspects

- An ideal **anti-aliasing filter**

$$H_{aa}(j\Omega) = \begin{cases} 1 & |\Omega| < \Omega_c < \pi/T \\ 0 & |\Omega| > \Omega_c \end{cases}$$

- The effective response is

$$H_{eff}(j\Omega) = \begin{cases} H(e^{j\Omega T}) & |\Omega| < \Omega_c \\ 0 & |\Omega| > \Omega_c \end{cases}$$

- In practice an ideal low-pass filter is not possible hence

$$H_{eff}(j\Omega) \approx H_{aa}(j\Omega)H(e^{j\Omega T})$$

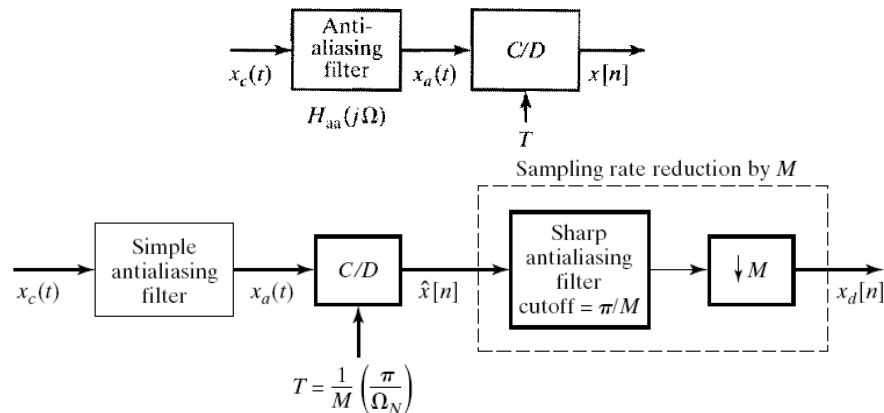
- This would require sharp-cutoff analog filters which are expensive

Oversampled A/D Conversion

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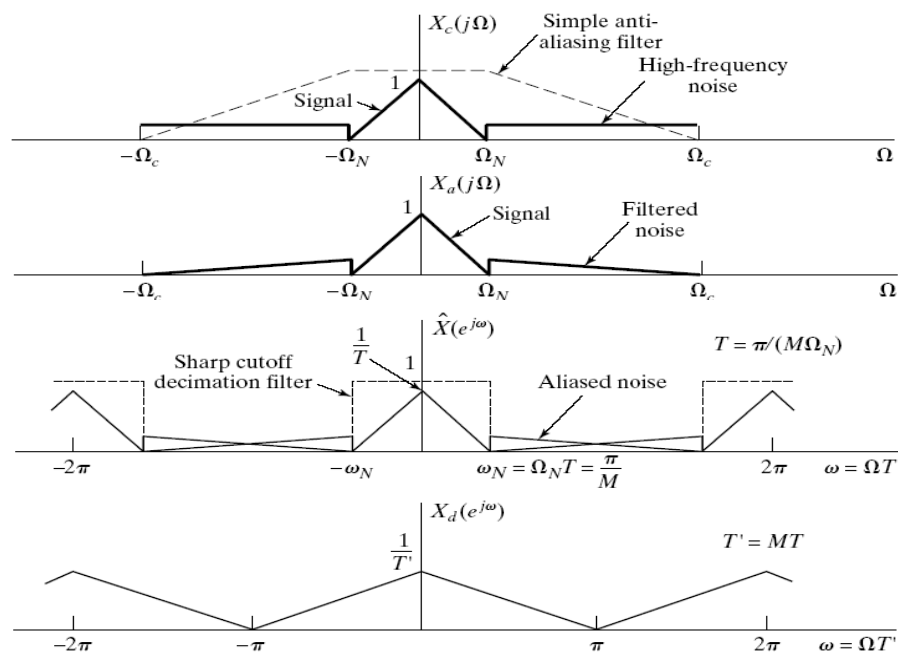
□ The idea is

- ▣ to use a **simple analog anti-aliasing filter**
- ▣ Use **higher** than required **sampling rate**
- ▣ implement **sharp anti-aliasing filter** in discrete-time
- ▣ Downsample to desired sampling rate



Example

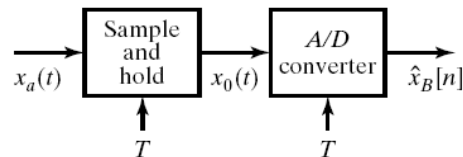
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Analog-to-Digital (A/D) Conversion

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- Ideal C/D converters convert continuous-time signals into infinite-precision discrete-time signals
- In practice, implement C/D converters as the cascade of



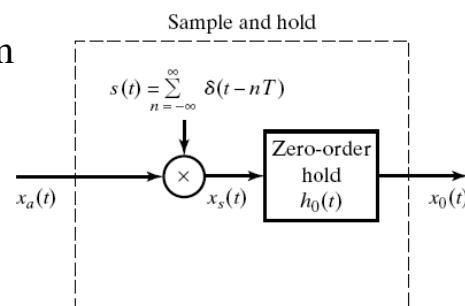
- The **sample-and-hold device** holds current/voltage constant
- The A/D converter converts current/voltage into finite-precisions number
- The ideal sample-and-hold device has the output

$$x_0(t) = \sum_{n=-\infty}^{\infty} x[n] h_0(t - nT) \quad h_0(t) = \begin{cases} 1, & 0 < t < T \\ 0, & \text{else} \end{cases}$$

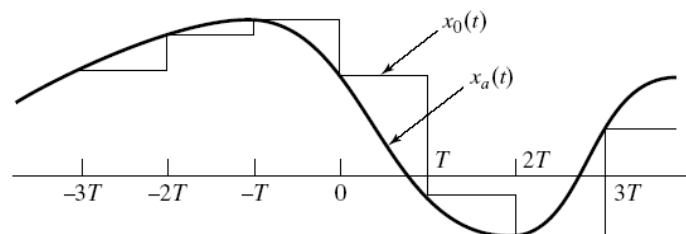
Sample and Hold

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- An ideal **sample-and-hold** system



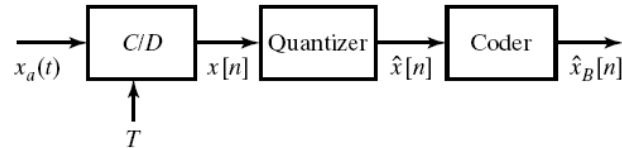
- Time-domain representation of sample-and-hold operation



A/D Converter Model

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- An **practical A/D converter** can be modeled as



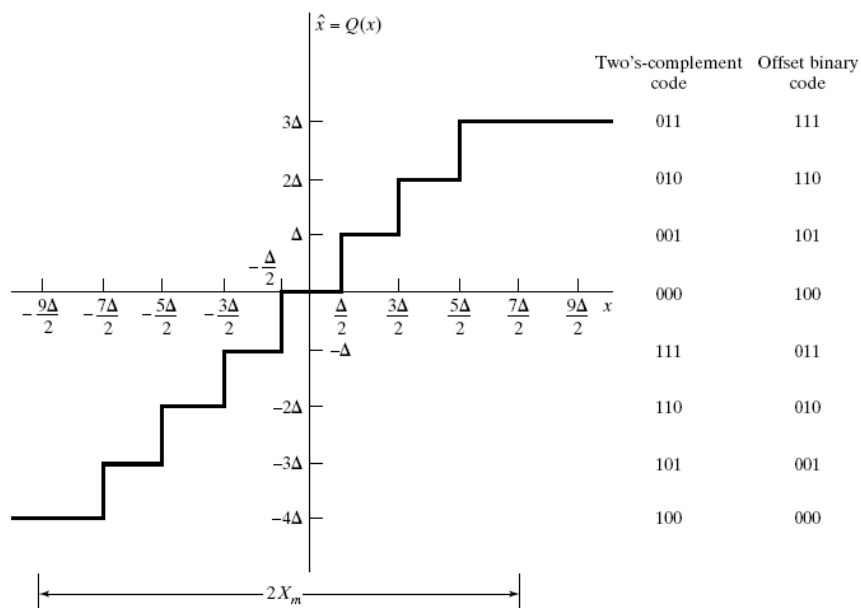
- The C/D converter represent the sample-and-hold-operation
- Quantizer transforms input into a finite set of numbers

$$\hat{x}[n] = Q(x[n])$$

- Most of the time uniform quantizers are used

Uniform Quantizer

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Two's Complement Numbers

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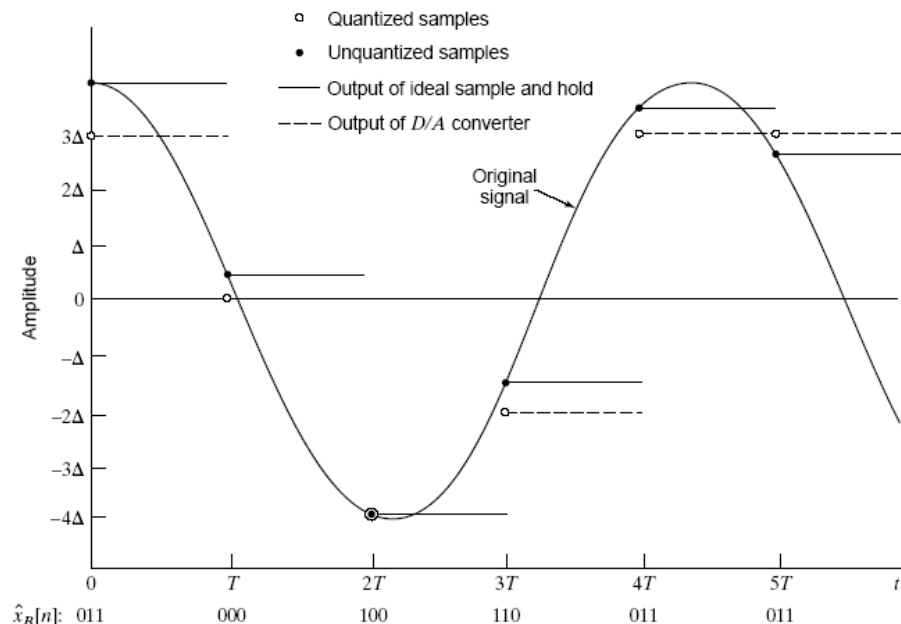
- Representation for signed numbers in computers
- Integer two's-complement $-a_0 2^B + a_1 2^{B-1} + \dots + a_B 2^0$
- Fractional two's-complement $-a_0 2^0 + a_1 2^{-1} + \dots + a_B 2^{-B}$
- Example $B+1=3$ bit two's-complement numbers

$-a_0 2^2 + a_1 2^1 + a_2 2^0$	
Binary Symbol	Numerical Value
011	3
010	2
001	1
000	0
111	-1
110	-2
101	-3
100	-4

$-a_0 2^0 + a_1 2^{-1} + a_2 2^{-2}$	
Binary Symbol	Numerical Value
0.11	3/4
0.10	2/4
0.01	1/4
0.00	0
1.11	-1/4
1.10	-2/4
1.01	-3/4
1.00	-4/4

Example

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Quantization Error

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- Quantization error: $e[n] = \hat{x}[n] - x[n]$
 - difference between the original and quantized value

- If quantization step is Δ the **quantization error** :

$$-\Delta/2 < e[n] < \Delta/2$$

- As long the input does not clip

- Based on this fact we may use the following simplified model with assumption:

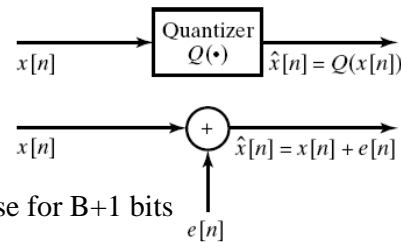
- $e[n]$ is uniformly distributed random variable
- Is uncorrelated with the signal $x[n]$

- The variance of $e[n]$ is then

$$\sigma_e^2 = \frac{\Delta^2}{12}$$

- And the **signal-to-noise ratio** of quantization noise for B+1 bits

$$\text{SNR} = 6.02B + 10.8 - 20 \log_{10} \left(\frac{X_m}{\sigma_x} \right)$$



D/C Conversion

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- Perfect reconstruction requires filtering with ideal LPF

$$X_r(j\Omega) = X(e^{j\Omega T})H_r(j\Omega)$$

$$X(e^{j\Omega T}): \text{FT of sampled signal}$$

$$X_r(j\Omega): \text{FT of reconstructed signal}$$

- The ideal reconstruction filter

$$H_r(j\Omega) = \begin{cases} T & |\Omega| < \pi/T \\ 0 & |\Omega| > \pi/T \end{cases}$$

- The time domain reconstructed signal is

$$x_r(t) = \sum_{n=-\infty}^{\infty} x[n] \frac{\sin[\pi(t - nT)/T]}{\pi(t - nT)/T}$$

- In practice we **cannot implement an ideal reconstruction filter**

D/A Conversion

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- The practical way of D/C conversion is an D/A converter



- It takes a binary code and converts it into continuous-time output

$$x_{DA}(t) = \sum_{n=-\infty}^{\infty} X_m \hat{x}_B[n] h_0(t - nT) = \sum_{n=-\infty}^{\infty} \hat{x}[n] h_0(t - nT)$$

- Using the additive noise model for quantization

$$x_{DA}(t) = \sum_{n=-\infty}^{\infty} x[n] h_0(t - nT) + \sum_{n=-\infty}^{\infty} e[n] h_0(t - nT) = x_0(t) + e_0(t)$$

- The signal component in frequency domain can be written as

$$X_0(j\Omega) = X(e^{j\Omega T}) H_0(j\Omega)$$

- To recover the desired signal component, a compensated reconstruction filter is needed:

$$\tilde{H}_r(j\Omega) = \frac{H_r(j\Omega)}{H_0(j\Omega)}$$

Compensated Reconstruction Filter

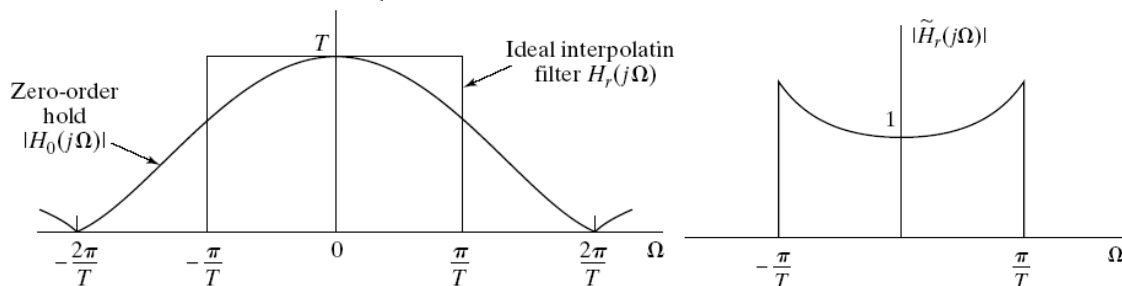
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- The frequency response of zero-order hold is

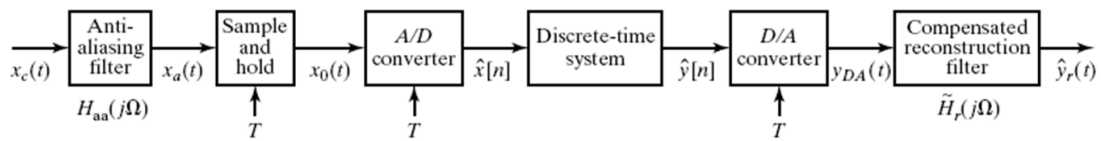
$$H_0(j\Omega) = \frac{2 \sin(\Omega T / 2)}{\Omega} e^{-j\Omega T / 2}$$

- Therefore the compensated reconstruction filter should be

$$\tilde{H}_r(j\Omega) = \begin{cases} \frac{\Omega T / 2}{\sin(\Omega T / 2)} e^{j\Omega T / 2} & |\Omega| < \pi / T \\ 0 & |\Omega| > \pi / T \end{cases}$$



Digital processing of analog signals



$$Y_d(j\Omega) = \tilde{H}_r(j\Omega)H_0(j\Omega)H(e^{j\Omega T})H_{aa}(j\Omega)X_c(j\Omega)$$

$$H_{\text{eff}}(j\Omega) = \tilde{H}_r(j\Omega)H_0(j\Omega)H(e^{j\Omega T})H_{aa}(j\Omega)$$

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THE END