

# 計算固体力学入門 (5)

Introduction to Computational Solid Mechanics (5)

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# Today's topic

The contents of this course will be as follows:

1. FEM for a one-dimensional problem.
2. Mathematical preliminaries
  - Gauss-Legendre quadrature
  - Einstein's summation convention
3. Continuum mechanics
  - Deformation of continuum
  - **Balance of continuum**
  - **Basic equations**
4. Weak form
5. Discretization
6. FEM implementations

# Tensor product

Let us consider fixed two vectors  $\mathbf{a}$  and  $\mathbf{b} \in \mathbb{R}^3$ , and another vector  $\mathbf{u} \in \mathbb{R}^3$ . By using these vectors, let us define another vector  $\mathbf{v} \in \mathbb{R}^3$  as

$$\mathbf{v} = (\mathbf{b} \cdot \mathbf{u})\mathbf{a}. \quad \cdots (1)$$

With this procedure, we have defined a “map”:  $\mathbf{u} \rightarrow \mathbf{v}$ . Such a map is called a **tensor product** of the vectors  $\mathbf{a}$  and  $\mathbf{b}$ , and will be denoted as

$$\mathbf{v} = (\mathbf{a} \otimes \mathbf{b})[\mathbf{u}] \quad (= (\mathbf{b} \cdot \mathbf{u})\mathbf{a}). \quad \cdots (2)$$

Note: We have not used the components of the relevant vectors to define (2), i.e. it can be defined without coordinate system.

Note: Tensor product is the tensor (which will be defined in the next page).

# Tensor

Let us consider a map  $L : \mathbb{R}^3 \ni \mathbf{u} \rightarrow \mathbf{v} \in \mathbb{R}^3$ , i.e.  $\mathbf{v}$  is defined as

$$\mathbf{v} = L[\mathbf{u}]. \quad \cdots (3)$$

When  $L$  is linear, i.e.  $L[a\mathbf{u} + b\mathbf{v}] = aL[\mathbf{u}] + bL[\mathbf{v}]$  holds, it is called the linear transform of a vector, or the (second-order) **tensor**. Again,  $L$  is independent of the choice of coordinate. Once we fix the coordinate system, (3) is represented as

$$v_i = L_{ij}u_j \Leftrightarrow \mathbf{v} = \mathbf{L}\mathbf{u}. \quad \cdots (4)$$

The matrix  $\mathbf{L} \in \mathbb{R}^{3 \times 3}$  is called the **representation matrix** of the tensor  $L$ .

(example)

the  $ij$ -component of representation matrix of  $\mathbf{a} \otimes \mathbf{b}$  is given as  $a_i b_j$ .

# Examples

Q1:

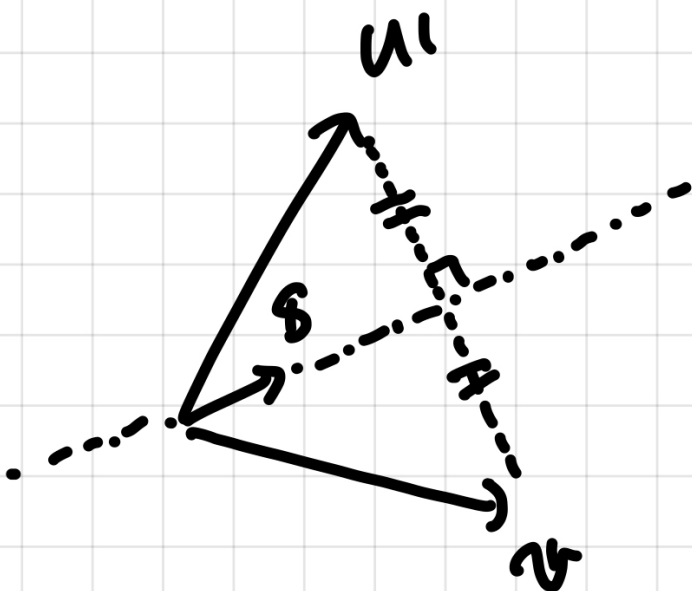
find the representation matrix of the identity map  $I$  which maps a vector  $u$  to  $u$  itself, i.e.  $u = I[u]$

Q2:

show that the “reflection”  $v$  of the vector  $u$  with respect to a unit vector  $s$  is given as follows:

$$v = (2n \otimes n - I)u,$$

and show the corresponding representation matrix.



# Adjoint linear transformation

## Definition: adjoint linear transformation

The tensor  $\tilde{L}$  satisfying

$$L[\mathbf{u}] \cdot \mathbf{v} = \mathbf{u} \cdot \tilde{L}[\mathbf{v}] \quad \cdots (5)$$

is called the adjoint linear transformation.

(example):

Let us consider the tensor product  $L = \mathbf{a} \otimes \mathbf{b}$ . Its adjoint  $\tilde{L}$  is given as  $\tilde{L} = \mathbf{b} \otimes \mathbf{a}$ .

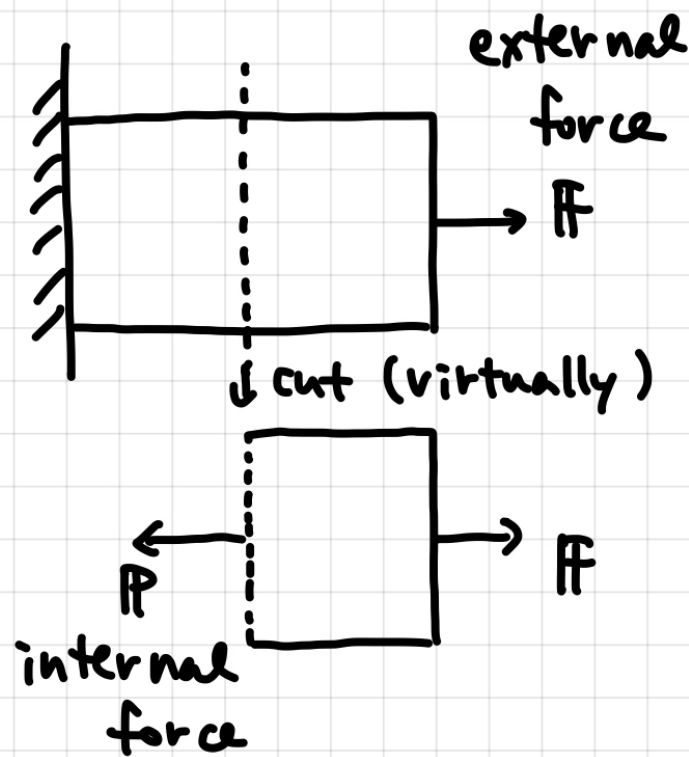
$$(L[\mathbf{u}] \cdot \mathbf{v} = (\mathbf{a} \otimes \mathbf{b})[\mathbf{u}] \cdot \mathbf{v} = ((\mathbf{b} \cdot \mathbf{u})\mathbf{a}) \cdot \mathbf{v} = \mathbf{u} \cdot (\mathbf{b}(\mathbf{a} \cdot \mathbf{v})) = \mathbf{u} \cdot (\mathbf{b} \otimes \mathbf{a})[\mathbf{v}] = \mathbf{u} \cdot \tilde{L}[\mathbf{v}])$$

(Quiz):

Show the representation matrix of  $\tilde{L} = \mathbf{b} \otimes \mathbf{a}$ .

# Stress tensor $\sigma$ 1/2

Let us consider a uniform bar subject to an external force  $F$ .



Then, at an arbitrary cross section of the bar, we observe the corresponding internal force  $P$ .

(Otherwise, the bar cannot be balanced!)

Stress vector (or traction)  
= internal force per unit area.

## Definition: Stress tensor

The linear transformation  $\sigma$  whose adjoint generates the traction  $P$  on a surface from the unit normal vector  $n$ , i.e.

$$P = \tilde{\sigma}[n] \quad \cdots (6)$$

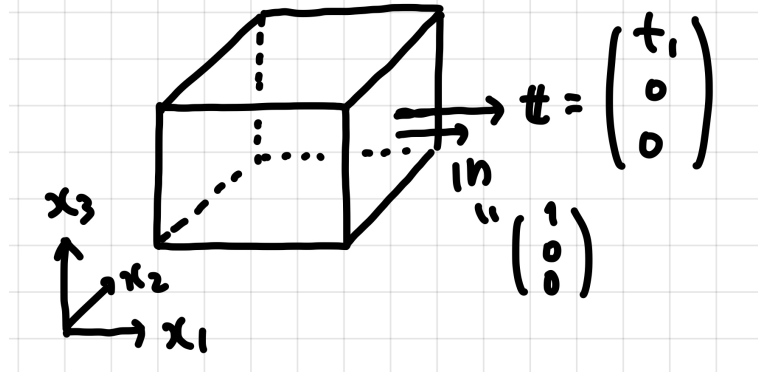
is called the **stress tensor**.

(6) is called the Cauchy stress formula.

# Stress tensor $\sigma$ 2/2

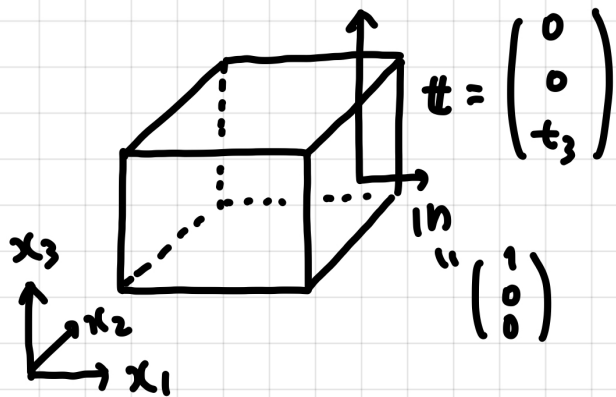
Let us consider a rectangular box (whose edges are parallel to given axes).

Let us consider the traction  $\mathbf{t} = (t_1, 0, 0)^t$  acting on the surface having the normal  $\mathbf{n} = (1, 0, 0)^t$ . The Cauchy stress formula gives



$$t_1 = \sigma_{j1}n_j = \sigma_{11}n_1 + \sigma_{21}n_2 + \sigma_{31}n_3 = \sigma_{11}.$$

Similarly, the traction  $\mathbf{t} = (0, 0, t_3)^t$  acting on the surface and the normal  $\mathbf{n} = (1, 0, 0)^t$  have the following relation:



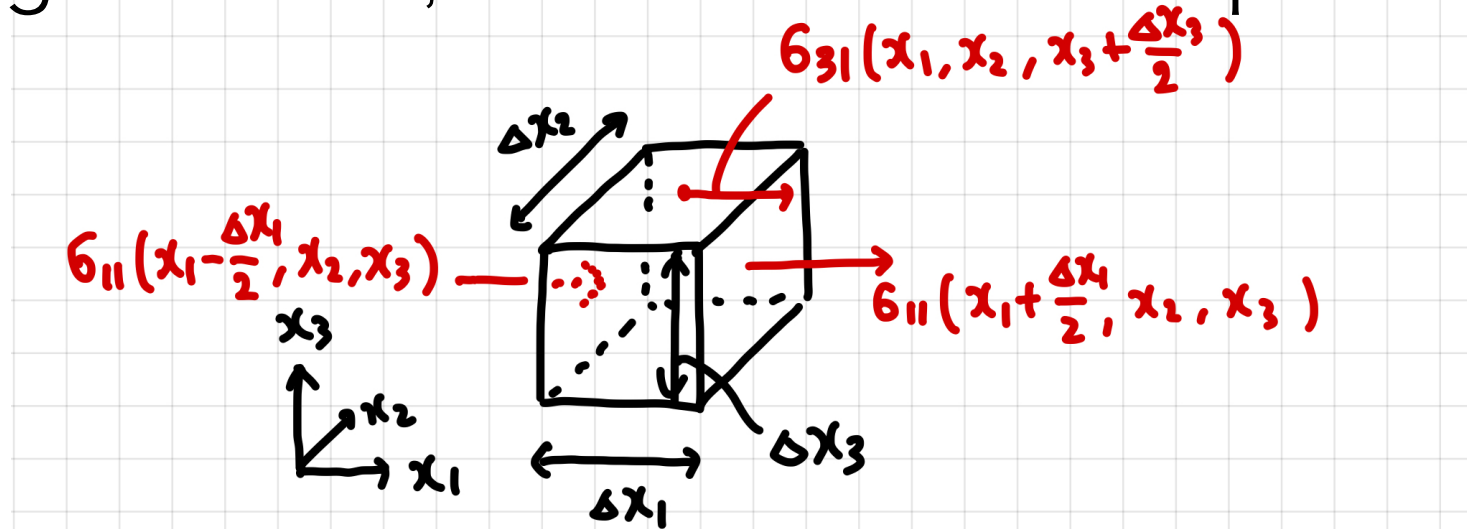
$$t_3 = \sigma_{j3}n_j = \sigma_{13}n_1 + \sigma_{23}n_2 + \sigma_{33}n_3 = \sigma_{13}.$$

→  $\sigma_{ij}$  provides  $j^{\text{th}}$  component of a traction acting on the surface perpendicular to  $x_i$  axis.



# Balance equation 1/3

Let us consider a rectangular box (whose edges (of length  $\Delta x_i$ ) are parallel to given axes, and the “centre” is put at the origin).



The 1st component of traction working on the “left” and “right” surface can be written as

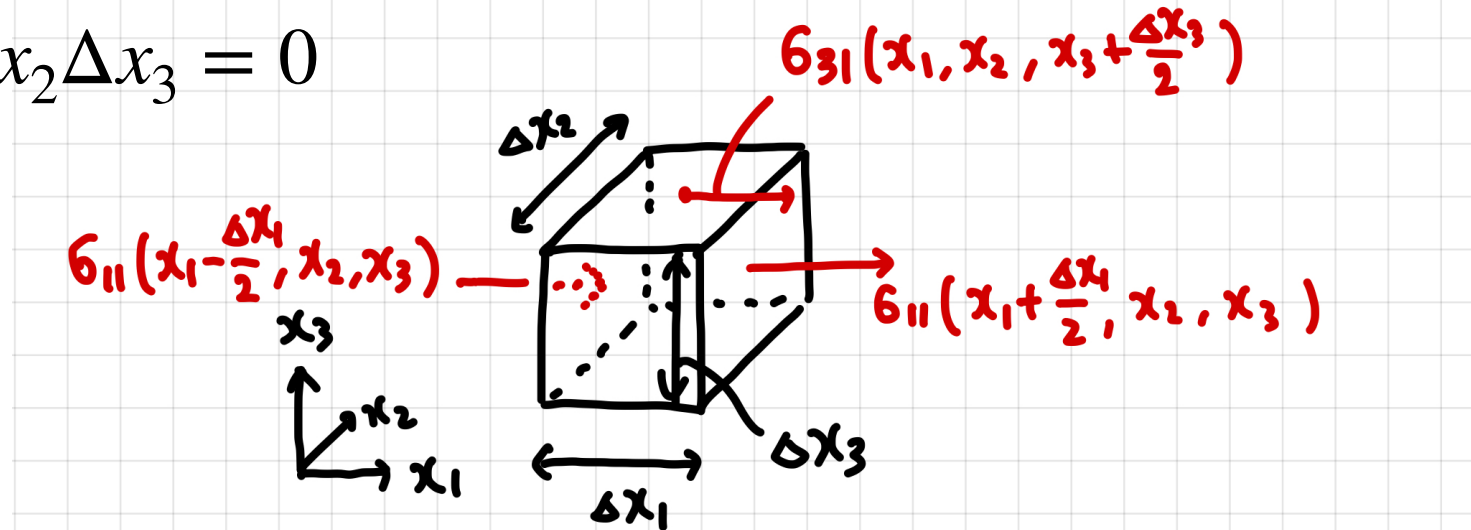
$$\sigma_{11}(x_1 \pm \Delta x_1/2, x_2, x_3) \simeq \sigma_{11}(x_1, x_2, x_3) \pm \partial \sigma_{11}(x_1, x_2, x_3) / \partial x_1 \times \Delta x_1 / 2$$

Quiz: present the 1st comp. of traction working on the “top”, “bottom”, “front” and “back” surfaces.

# Balance equation 2/3

When this box is subject to a body force  $F = (F_1, F_2, F_3)^t$ , the balance equation in  $x_1$  direction can be obtained as

$$\begin{aligned} & \sigma_{11}(x_1 + \Delta x_1/2, x_2, x_3) \Delta x_2 \Delta x_3 - \sigma_{11}(x_1 - \Delta x_1/2, x_2, x_3) \Delta x_2 \Delta x_3 \\ & + \sigma_{21}(x_1, x_2 + \Delta x_2/2, x_3) \Delta x_3 \Delta x_1 - \sigma_{21}(x_1, x_2 - \Delta x_2/2, x_3) \Delta x_3 \Delta x_1 \\ & + \sigma_{31}(x_1, x_2, x_3 + \Delta x_3/2) \Delta x_1 \Delta x_2 - \sigma_{31}(x_1, x_2, x_3 - \Delta x_3/2) \Delta x_1 \Delta x_2 \\ & + F_i \Delta x_1 \Delta x_2 \Delta x_3 = 0 \end{aligned}$$



By using the approximations in the previous page, and taking the limit of  $\Delta x_1 \Delta x_2 \Delta x_3 \rightarrow 0$ , we have the balance equation as  $\sigma_{j1,j} + F_1 = 0$ .

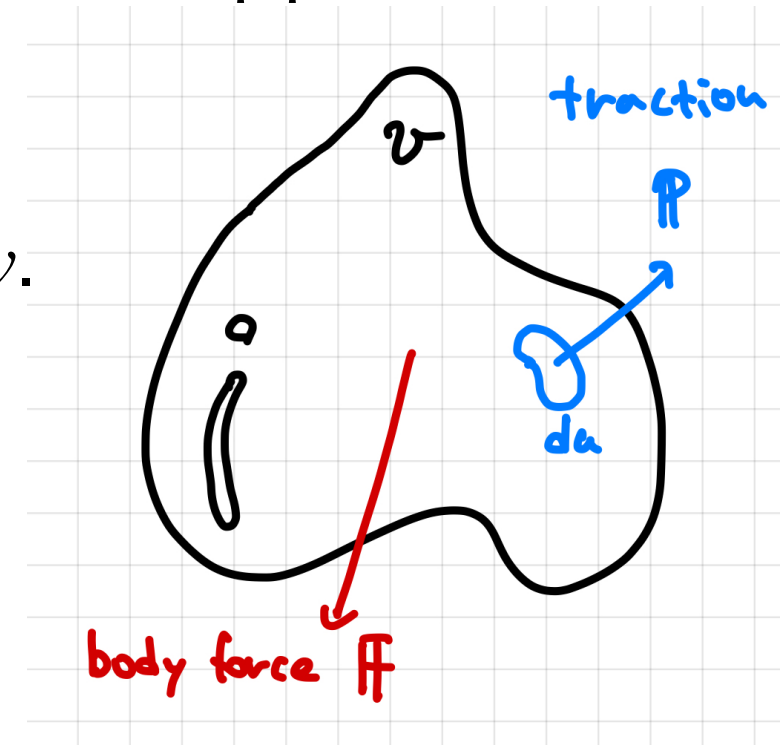
By repeating the above procedure for  $i = 2$  and  $3$ , we have the following balance equation of the continuum:

$$\sigma_{ji,j} + F_i = 0.$$

# Balance equation 3/3

The balance equation can be derived by a different approach.

Let us take an arbitrary partial domain  $v$  of the continuum, and consider the forces acting on  $v$ . The forces are divided into two parts: the **body force**  $F$  and **the traction**  $P$ .



The balance equation for  $v$  is written as

$$\int_{\partial v} p_i da + \int_v F_i dv = 0$$

$$\Leftrightarrow \int_{\partial v} \sigma_{ji} n_j da + \int_v F_i dv = 0$$

$$\Leftrightarrow \int_v \sigma_{ji,j} da + \int_v F_i dv = 0. \quad \rightarrow \text{Since } v \text{ is arbitrary, we have}$$

$$\sigma_{ji,j} + F_i = 0.$$

# Constitutive equation 1/2

We then discuss the constitutive equation which relates the stress tensor  $\sigma_{ij}$  and strain tensor  $\varepsilon_{ij}$ .

## Linear elastic material

When  $\sigma_{ij} = C_{ijkl}\varepsilon_{kl}$  holds in a material, such a material is called linear elastic (c.f.  $f = kx$ ).

Note: The elastic tensor  $C_{ijkl}$  is (a representation of) a linear map from a second order tensor  $\varepsilon_{ij}$  to another one  $\sigma_{ij}$ . In this sense,  $C_{ijkl}$  is called 4th order tensor.

In this lecture, we focus on the material whose elastic tensor has the following form:

$$C_{ijkl} = \lambda\delta_{ij}\delta_{kl} + \mu\delta_{ik}\delta_{jl} + \mu\delta_{il}\delta_{jk},$$

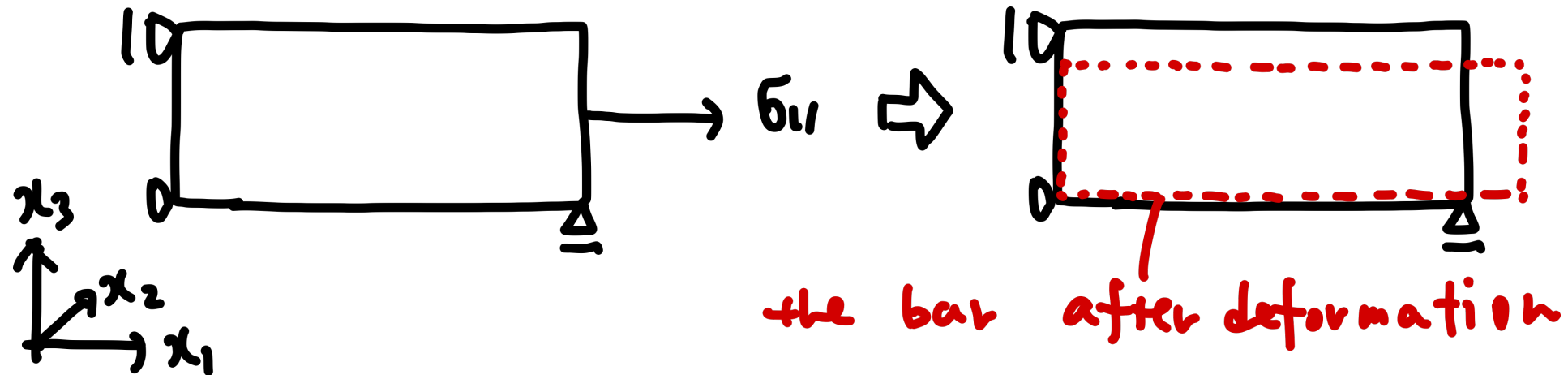
i.e. the isotropic elastic material, where  $\lambda$  and  $\mu$  are the Lamé constants.

# Constitutive equation 2/2

Quiz: show that the constitutive equation for isotropic material is give as  $\sigma_{ij} = \lambda \delta_{ij} \varepsilon_{kk} + 2\mu \varepsilon_{ij}$ .

# Poisson's ratio

Let us consider a bar subject to uniaxial tension.



The constitutive equations give

$$\sigma_{11} = \lambda \varepsilon_{kk} + 2\mu \varepsilon_{11}, \quad \dots (7)$$

$$0 = \sigma_{22} = \lambda \varepsilon_{kk} + 2\mu \varepsilon_{22}, \quad \dots (8)$$

$$0 = \sigma_{33} = \lambda \varepsilon_{kk} + 2\mu \varepsilon_{33}. \quad \dots (9)$$

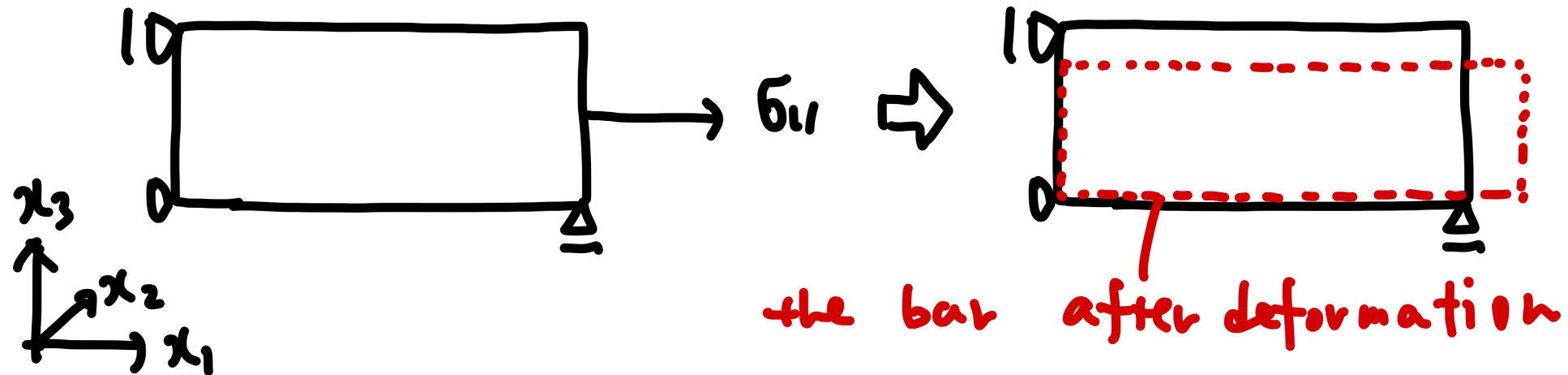
From (8) and (9), it is obvious that  $\varepsilon_{22} = \varepsilon_{33}$ . We then substitute this

into (8) to have  $\varepsilon_{22} = -\frac{\lambda}{2(\lambda + \mu)} \varepsilon_{11}$ .

The poisson ratio  $\nu$

# Young's modulus

Let us consider a bar subject to uniaxial tension.



The constitutive equations give

$$\sigma_{11} = \lambda \varepsilon_{kk} + 2\mu \varepsilon_{11}, \quad \dots (7)$$

$$0 = \sigma_{22} = \lambda \varepsilon_{kk} + 2\mu \varepsilon_{22}, \quad \dots (8)$$

$$0 = \sigma_{33} = \lambda \varepsilon_{kk} + 2\mu \varepsilon_{33}. \quad \dots (9)$$

$\varepsilon_{22} = -\frac{\lambda}{2(\lambda + \mu)} \varepsilon_{11}$  is substituted into (7) to have  $\sigma_{11} = \frac{(3\lambda + 2\mu)\mu}{\lambda + \mu} \varepsilon_{11}$

The Young's modulus  $E$

Note: The isotropic elastic material can be characterised by two material constants.

# Two-dimensional elasticity 1/2

Suppose that  $u_3(\mathbf{x}) = 0$ , and  $u_1(\mathbf{x})$  and  $u_2(\mathbf{x})$  are independent of  $x_3$ .  
e.g. the object is “very” thick in  $x_3$  direction, and the external force is uniform in this direction.

→ Such a mechanical system is called in **plane-strain state**.

According to the definition of the plane-strain state, we have  
 $u_3 = 0$ ,  $u_{i,3} = 0$ , and thus we also have  $\varepsilon_{33} = \varepsilon_{13} = \varepsilon_{23} = \varepsilon_{31} = \varepsilon_{32} = 0$ .

Quiz: derive the constitutive equations for such a material.



# Two-dimensional elasticity 2/2

Similarly, if the stress in a mechanical system admits  $\sigma_{33} = \sigma_{13} = \sigma_{23} = \sigma_{31} = \sigma_{32} = 0$ , it is in plane-strain state.

Homework: derive the constitutive equations for a material in the plane-strain state.