

Mathematical Modelling

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Contents

1	Lecture 1	2
1.1	Practical Information	2
1.2	Dimensional Analysis	2
1.3	Fundamental Units	2
1.4	Trinity of the first atomic blast	3
1.5	Steady-state single phase flow in a uniform straight pipeline . . .	4
2	Lecture 2	5
2.1	Practical Information	5
2.2	Recall	5
2.3	Scaling	5
2.4	Buckinghams Pi-Theorem	5
2.5	Scaling	6
3	References	8

1 Lecture 1

1.1 Practical Information

You need to know

- Separable 1. order equations.
- Linear 1. order equations.
- 2. order linear equations with constant coefficients.

1.2 Dimensional Analysis

Basic facts

- Any physical relation has to make sense dimensionally.
- Any physical relation must be valid for any choice of fundamental units.

Remark.

- **Forbidden** $3m + 2kg = ?$
- $m = f(x, t)$ is legal
- e^{-t} and $s = 5t^2$, is nonsense
- **Dimension** is length, mass, energy, etc.
- **Unit** is meter, feet, year, etc

Make sure
remark looks
better

Given a variable R , we write $R = \overbrace{v(R)}^{\text{numerical value}} \underbrace{[R]}_{\text{unit}}.$

If we have a physical relation that is dimensionally correct that

$$f(R_1, R_2, \dots, R_n) = 0 \rightarrow f(v(R_1), v(R_2), \dots, v(R_n)) = 0$$

1.3 Fundamental Units

Given units F_1, F_2, \dots, F_m for fundamental if

$$F_1^{\alpha_1}, F_2^{\alpha_2}, \dots, F_m^{\alpha_m} = 0 \rightarrow \alpha_1 = \alpha_2 = \dots = 0$$

This units are then independent.

Example 1. The units kg, m, s are independent.

Example 2. In a right angle triangle with angle α and hypotenuse c . We know the area A is uniquely determined by α and c

$$A = f(c, \alpha)$$

α is dimensionless since $\alpha = \frac{s}{r}$. Since A scales as the square of the length, then is

$$\begin{aligned} f(ac, \alpha) &= a^2 f(c, \alpha) \\ c = 1 &\rightarrow f(a, \alpha) = a^2 f(1, \alpha) = a^2 h(\alpha) \end{aligned}$$

Which then ends up with the relation

$$A = a^2 h(\alpha)$$

Make corollary environment

Lets derive $A = a^2 h(\alpha)$ somewhat differently. We know there is a relation $f(A, c, \alpha) = 0$. We want to introduce new variables.

$$\Pi_1 = \frac{A}{c^2}, \quad c = c_1, \quad \alpha = \alpha_1$$

which means $f(c^2 \Pi_1, c, \alpha) = 0$ and $h(\Pi_1, \alpha, c) = 0$. h must be dimensionally consistent $\rightarrow h$ must be independent of c .

$$\begin{aligned} h(\Pi_1, \alpha) &= 0 \leftrightarrow \Pi_1 = k(\alpha) \\ \rightarrow \frac{A}{c^2} &= k(\alpha) \quad \leftrightarrow \quad A = c^2 k(\alpha) \end{aligned}$$

1.4 Trinity of the first atomic blast

We assume there is a relation

$$f(E, \rho, r, t) = 0$$

- Energy: $E, [E] = kgm^2s^{-2}$
- Mass density of air: $\rho, [\rho] = kg^{-3}$
- Radius: $r, [r] = m$
- Time: $t, [t] = s$

We choose 3 independent variables, say r, t, ρ . Also we call r, t, ρ **core variables**. Let us define a dimensionless number Π_1 such that

$$[\Pi_1] = 0$$

The relation is now given by $h(\Pi, t, r, \rho) = 0$, where h is independent of t, r and ρ . Which in fact is $h(\Pi) = 0$, where $\Pi_1 = c$ s.t. $[c] = 1$.

Given by the definition is

$$\frac{Et^2}{\rho r^5} = c \quad \rightarrow \quad E = \frac{c\rho r^5}{t^2}$$

Using $\rho = 12 \text{ kg m}^{-3}$, $r = 110 \text{ m}$, $t = 6 \cdot 10^{-3}$ do we end up with the relation

$$E = c \cdot 7.5 \cdot 10^{13} \text{ J}$$

1.5 Steady-state single phase flow in a uniform straight pipeline

Figure of a pipe

Pipe with flow u , length L and pressure drop Δp Then there is a relation between

- L : length, $[L] = m$
- D : diameter $[D] = m$
- u : flow rate $[u] = \text{m s}^{-1}$
- Δp : Pressure drop, $[\Delta p] = \text{kg m}^{-1} \text{ s}^{-2}$
- μ : (Shear) viscosity $[\mu] = \text{kg m}^{-1} \text{ s}^{-1}$
- ρ : mass density: $[\rho] = \text{kg m}^{-3}$
- E : Wall roughness: $[E] = m$

We have to choose 3 core variables and they are not unique. Since we have 3 independent units ρ, u, D are independent such that it can be a core variable:

$$\Pi_1 = \frac{L}{D} \quad , \quad \Pi_2 = \frac{\Delta p}{\rho u^2} \quad , \quad \Pi_3 = \frac{\rho}{\mu} \quad , \quad \Pi_4 = \frac{E}{D}$$

Then the relation is

$$\begin{aligned} f(\Pi_1, \Pi_2, \Pi_3, \Pi_4, \rho, D, u) &= 0 \quad \Pi_2 = h(\Pi_1, \Pi_3, \Pi_4) \leftrightarrow \frac{\Delta p}{\rho u^2} = h(\Pi_1, \Pi_3, \Pi_4) \\ &\rightarrow \frac{\Delta p}{u^2 \rho} = \Pi_1 k(\Pi_3, \Pi_4) \\ \Delta p &= u^2 \rho \frac{L}{D} k\left(\frac{\rho D u}{\mu}, \frac{E}{D}\right) \\ \text{measure } \frac{\rho D \mu}{\mu} \quad , \quad k &= \frac{\Delta p D}{u^2 \rho} \end{aligned}$$

2 Lecture 2

2.1 Practical Information

Ask for zoom meeting. ola.mahlen@ntnu.no, wednesday 13-14.

2.2 Recall

Last time did we consider steady-state single phase in a flow in a pipe.

- Assuming $f(L, \Delta p, u, \mu, D, E, \rho) = 0$ we arrive with this formula

$$\frac{\Delta p D}{u^2 \rho L} = k \left(\underbrace{\frac{\rho u D}{\mu}}_{\text{Reynhold number}}, \underbrace{\frac{E}{D}}_{\text{Relative wall roughness}} \right)$$

- Dimensionless numbers are often called **dimensionless groups**. Such numbers are independent of choice of fundamental units. They have real physical meaning. **Reynholds number** R_e essentially define what type of flow. Usually $R_e < 2000$ is it laminar flow and $R_e > 4000$ turbulent flow.

2.3 Scaling

Let a pipe have diameter D and flow rate u such that $t_v = \frac{D}{u}$. Then can we describe

$$t_\alpha = \frac{D^2}{\frac{\mu}{\rho}}$$

where μ is the kinematic viscosity. Then is R_e defined such that

$$R_e = \frac{t_\alpha}{t_v}$$

Assume we have the relation

$$R_1 = f(R_2, \dots, R_m)$$

Such that it exist an

$$\Pi_1 = g(\Pi_2, \Pi_2, \dots, \Pi_{m-k}).$$

2.4 Buckingham's Pi-Theorem

Assume we have a dimensionally valid relation $f(R_1, \dots, R_m) = 0$ and a set of fundamental units F_1, F_2, \dots, F_n such that

$$[R_j] = F_1^{a_{j1}} F_2^{a_{j2}} \dots F_n^{a_{jn}} \quad j = 1, 2, \dots, m$$

This then defines the dimension matrix A given by

Table 1: caption				
	F_1	F_2	\dots	F_n
R_1	a_{11}	a_{11}		a_{1n}
R_2	a_{21}	a_{21}		a_{2n}
\vdots		\ddots		
R_n	a_{m1}	\dots		a_{mn}

Fix better table environment.

Let $\text{rank}(A) = \dim(\text{row}(A)) = k$. This translates to that we have k dimensionally independent variables. Choosing k linearly independent row vectors, corresponds to choosing core variables. Let this basis be $\mathbf{a}_{i1}, \mathbf{a}_{i2}, \dots, \mathbf{a}_{ik}$. Let the rest of the row vectors be

$$\mathbf{a}_{j_1}, \mathbf{a}_{j_2}, \dots, \mathbf{a}_{j_{m-k}}$$

Then is $\mathbf{a}_{j_r} = \sum_{s=1}^k C_{j_r,s} \mathbf{a}_{i_s}$ where $r = 1, \dots, m-k$. We end up with the equation

$$\Pi_r = \frac{R_{j_r}}{R_{i_1}^{r_{j_r,1}} R_{j_2}^{a_{j_r,2}} \dots R_{j_k}^{a_{j_r,k}}}$$

Are dimensionally numbers.

Our relation becomes

$$g(\Pi_1, \dots, \Pi_{m-k}) = 0, \quad \begin{cases} i_1, i_2, \dots, i_k \\ j_1, \dots, j_{m-k} \end{cases}$$

Example. Swinging pendulum

Assume there is a relation

$$f(w, \alpha_0, L, M, g) = 0$$

where w is the frequency, g gravitational acceleration, M mass, α_0 the swinging angle. We can set L, M, g as core variables such that

$$\left[\frac{L}{g} \right] = s^2 \quad \rightarrow \quad \left[\frac{L}{g} w^2 \right] = 1$$

$$f(w, \alpha_0, L, M, g) = 0 \implies g \left(\alpha_0, \frac{L w^2}{g} \right) = 0$$

2.5 Scaling

We have a problem at hand, usually differential equations. Then we try to find representative scales for the various variables, and then write the equation on so-called dimensionless form. This has several advantages

- Our dimensionless variables are of order 1 .
- We get rid of a lot of physical constants.
- It makes us able to see what terms are "small" in the equation. The idea is to introduce dimensionless variables by introducing appropriate scales. If we have a stick of length L , we choose L as length scale i.e

$$x^* = Lx \quad \text{Where } x \text{ is dimensionless}$$

Example. Heat flow in a rod with length L . Let $u^*(x^*, t^*)$ be the temperature with the boundary conditions

$$u^*(0, t^*) = 0 \quad u^*(L, t^*) = 0$$

If we let the model be

$$\frac{\partial u^*}{\partial t^*} = D \cdot \frac{\partial^2 u^*}{\partial x^{*2}}, \quad u^*(0, t^*) = 0 \quad u^*(L, t^*) = 0$$

$$u^*(x^*, 0) = u_0 \sin\left(\pi \frac{x^*}{L}\right)$$

We find the time scale T by scales **balancing the equation** .

Let $x^* = Lx$, and $t^* = Tt$, where T is to be determined $u^* = u_0 u$. If we find $u(x, t)$, then the physical temperature is given by

$$u^*(x^*, t^*) = u_0 u\left(\frac{x^*}{L}, \frac{t^*}{T}\right)$$

We have $u(0, t) = u(1, t) = 0$

$$\frac{\partial u^*}{\partial t^*} = D \frac{\partial^2 u^*}{\partial x^{*2}} \implies \frac{u_0}{T} \frac{\partial u}{\partial t} = \frac{u_0}{L^2} D \frac{\partial^2 u}{\partial x^2}$$

$$\leftrightarrow \frac{\partial u}{\partial t} = \left(\frac{TD}{L^2}\right) \frac{\partial^2 u}{\partial x^2} \quad \text{Balancing the equation}$$

$$\frac{TD}{L^2} = 1 \implies T = \frac{L^2}{D}$$

$$u^*(x^*, 0) = u_0 \sin\left(\pi \frac{x^*}{L}\right)$$

$$u(x, 0) = \sin(\pi x)$$

which fulfills the condition

$$\frac{\partial u}{\partial t} = \frac{\partial^2 u}{\partial x^2}, \quad u(0, t) = u(1, t) = 0$$

3 References