


① → Equivalent volume sphere diameter, the surface-volume equivalent sphere/diane

① → equivalent volume sphere diameter.
Surface-volume sphere diameter.

Projected area diameter of Cuboid Particles.

Equivalent circle diameter

 circle with area equal to projected area.

Martini's Diameter.

↳ line Bisecting Projected Area.

Feret's diameter.

↳ Distance between parallel tangents

$$\begin{aligned} \rightarrow \frac{4}{3}\pi \frac{d^3}{8} &= 1 \times 2 \times 4 \\ \frac{d^3 \pi}{6} &= 8 \text{ mm}^3 \end{aligned}$$

$$d = \left(\frac{8 \times 6}{\pi} \right)^{\frac{1}{3}} = \left(\frac{48}{\pi} \right)^{\frac{1}{3}} = 2.481 \text{ mm}$$

Diameter having same surface to volume ratio

$$\begin{aligned} \frac{\frac{\pi d^2}{2}}{\frac{\pi d^3}{6}} &= \frac{2(1 \times 2 + 2 \times 4 + 1 \times 4)}{(1 \times 2 \times 4)} = \frac{2(2+8+4)}{8} = \frac{28}{8} = \frac{14}{4} = \frac{7}{2} = \frac{3}{d} \\ d &= \frac{6}{7} = 0.857 \end{aligned}$$

$$A_1 = 1 \times 2 = 2 \Rightarrow \frac{\pi d_1^2}{4}$$

$$A_2 = 2 \times 4 = 8 \Rightarrow \frac{\pi d_2^2}{4}$$

$$A_3 = 1 \times 4 = 4 \Rightarrow \frac{\pi d_3^2}{4}$$

$$d_1 \Rightarrow \sqrt{\frac{8}{\pi}} = 1.59 \text{ mm}$$

$$d_2 \Rightarrow \sqrt{\frac{32}{\pi}} = 3.19 \text{ mm}$$

$$d_3 \Rightarrow \sqrt{\frac{16}{\pi}} = 2.25 \text{ mm}$$

(2) Sphericity $\Rightarrow \frac{(\text{Surface area of Sphere of Same Volume})}{\text{actual Surface Area}}$

\rightarrow ~~volume of cube~~ $= L^3 = 0.3$

~~Sphere volume~~ $= \frac{\pi}{6}$

$$\frac{\pi d^2}{6L^2} = \frac{\pi d^2}{6\pi^2}$$

$$L^3 = \frac{\pi d^3}{6}$$

$$L = \left(\frac{\pi}{6}\right)^{1/3} \text{ (D)}$$

$$\begin{aligned} \frac{\pi d^2}{6L^2} &= \left(\frac{\pi}{6}\right) \left(\frac{1}{\pi/6}\right)^{2/3} \\ &= \left(\frac{\pi}{6}\right)^{1/3} \\ &= \boxed{0.805} \checkmark \end{aligned}$$

③ → Sand mixture was screened through 12 mesh.

Screen Analysis → Each screen is identified in meshes per inch.

According to Tyler Screen Series

200 mesh screen \Rightarrow 0.074 mm.

↳ Area of next screen smaller screen is twice the next smaller screen.

Ideal Screen

↳ Smallest

Particle in overflow $>$ largest particle in underflow.

Cut diameter

$D_{pc} \Rightarrow$ equal to mesh opening.

Screen effectiveness Feed.

Material Balance \Rightarrow

$F = D + B$

$$F x_F = D x_D + B x_B$$

$$\frac{D}{F} = \frac{x_F - x_B}{x_D - x_B}$$

$$\frac{B}{F} = \frac{x_D - x_F}{x_D - x_B}$$

$$E_A = \frac{\text{Oversize material A in the overflow}}{\text{Total entering in feed.}}$$

$$= \frac{D x_D}{F x_F}$$

→ Effectiveness based on undersize

$$E_B = \frac{B(1-x_B)}{F(1-x_F)} \Rightarrow \frac{\text{Undersize material in underflow}}{\text{Total entering in feed.}}$$

$$E = E_A E_B \Rightarrow \frac{D B x_D (1-x_B)}{F^2 x_F (1-x_F)}$$

$$\frac{D}{F} = \frac{x_F - x_B}{x_D - x_B}$$

$$\frac{B}{F} = \frac{x_D - x_F}{x_D - x_B}$$

$$\Rightarrow \frac{(x_F - x_B)}{(x_D - x_B)} \times \frac{(x_D - x_F)}{(x_D - x_B)} \times \frac{x_D (1-x_B)}{x_F x (1-x_F)}$$

③ →

$$E = \frac{D}{P} \times \frac{B}{F} \times \frac{(x_D)(1-x_B)}{x_F(1-x_F)}$$

$$x_F = 0.4$$

$$x_D = 0.8$$

$$x_B = 0.2$$

$$= \left(\frac{x_D - x_B}{x_D - x_F} \right) \times \left(\frac{x_D - x_F}{x_D - x_B} \right) \times \left(\frac{x_D}{x_F} \right) \left(\frac{1-x_B}{1-x_F} \right)$$

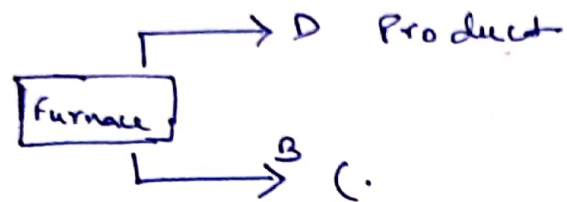
$$= \left(\frac{0.4 - 0.2}{0.8 - 0.2} \right) \times \left(\frac{0.8 - 0.4}{0.8 - 0.2} \right) \times \left(\frac{0.8}{0.4} \right) \left(\frac{0.8}{0.6} \right)$$

$$= \frac{0.2}{0.6} \times \frac{0.4}{0.6} \times (2) \times \frac{0.8}{0.6}$$

$$= \frac{2 \times 4 \times 2 \times 8}{6 \times 6 \times 6} = \frac{16}{27}$$

$$= \boxed{0.59}$$

④ → we have $x_F \Rightarrow$



$$F = \underline{100 \text{ tonne/h}}$$

$$x_B = \underline{0.05}$$

$$x_F = \underline{0.75}$$

we have efficiency.

$$E = \frac{D}{F} \times \frac{B}{F} \times \frac{(x_D)}{(x_F)} \times \left(\frac{1-x_B}{1-x_F} \right)$$

$$E = \frac{(x_F - x_B)}{(x_D - x_B)} \times \frac{(x_D - x_F)}{(x_D - x_B)} \times \left(\frac{x_D}{x_F} \right) \times \left(\frac{1-x_B}{1-x_F} \right)$$

$$0.5 = \frac{(\cancel{0.05} - x_B)}{(\cancel{0.05} - x_B)} = \frac{0.7}{(x_D - 0.05)} \times \frac{(x_D - 0.75)}{(x_D - 0.05)} \times \frac{x_D}{0.75} \times \frac{0.95}{0.25}$$

$$0.5 = 3.54 \left(\frac{x_D^2 - 0.75x_D}{x_D^2 - 0.1x_D + 0.0025} \right)$$

estimation \Rightarrow 2

$$0.5 = 3.54 \left(\frac{x_D (x_D - 0.75)}{x_D (x_D - 0.1)} \right)$$

$$0.5 x_D - 0.05 = 3.54 x_D - 2.655$$

$$2.605 = 3.04 x_D$$

$$x_D = \left(\frac{2.64}{3.04} \right) = \boxed{0.868}$$

$1 - x_D \Rightarrow$ fines concentration in overflow
 $\rightarrow 14\%$

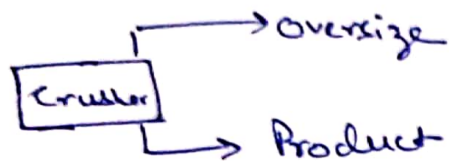
$F \Rightarrow 100 \text{ tonne/hr}$

$$\frac{D}{F} = \frac{x_B - x_D}{(x_D - x_B)} = \frac{0.75 - 0.05}{0.86 - 0.05}$$

$$= \frac{0.7}{0.81} = 0.864$$

$$D = 86.4 \text{ tonne/hr.}$$

⑥ → ⑤



$$B = 100 \text{ kg/h}$$

$$X_F = \cancel{0.146} \quad 0.694$$

$$X_D = \cancel{0.168} \quad 0.764$$

$$X_B = \underline{0.113}$$

$$E = \left(\frac{D}{F} \right) \left(\frac{B}{F} \right) \left(\frac{X_D}{X_F} \right) \left(\frac{1-X_B}{1-X_F} \right)$$

$$= \left(\frac{X_F - X_B}{X_D - X_B} \right) \left(\frac{X_D - X_F}{X_D - X_B} \right) \left(\frac{X_D}{X_F} \right) \left(\frac{1-X_B}{1-X_F} \right)$$

$$= \left(\frac{0.694 - 0.113}{0.764 - 0.113} \right) \left(\frac{0.764 - 0.694}{0.764 - 0.113} \right) \left(\frac{0.168}{0.146} \right) \left(\frac{1 - 0.113}{1 - 0.146} \right)$$

$$= \left(\frac{0.581}{\cancel{0.033}} \right) \times \left(\frac{0.070}{\cancel{0.022}} \right) \times \left(\frac{0.764}{0.694} \right) \left(\frac{0.887}{\cancel{0.854}} \right)$$

$$= \frac{3}{5} \times \frac{2}{5} \times 1.195 = \underline{0.306}$$

$$\frac{B}{F} = \frac{X_D - X_F}{X_D - X_B} = \frac{0.070}{0.651}$$

$$F = \frac{B}{\frac{0.070}{0.651}} = \frac{100}{0.1077} = 930 \text{ kg/hr.}$$

⑥ → Cumulative $x_F = 55\%$ $x_B = 0$ $x_D = 76\%$

$$E_{76} = \left(\frac{x_F - x_B}{x_D - x_B} \right) \left(\frac{x_D - x_F}{x_D - x_B} \right) \left(\frac{x_D}{x_F} \right) \left(\frac{1 - x_B}{1 - x_F} \right)$$

$$= \left(\frac{0.55}{0.76} \right) \left(\frac{0.76 - 0.55}{0.76} \right) \left(\frac{0.76}{0.55} \right) \left(\frac{1}{0.45} \right)$$

$$= \frac{0.55}{0.76} \times \frac{0.21}{0.76} \times \left(\frac{0.76}{0.55} \right) \times \left(\frac{1}{0.45} \right)$$

$$= \frac{21 \times 100}{76 \times 45} = \boxed{0.61}$$

$$B \Rightarrow \underline{\underline{2 \text{ tonne/h}}}$$

$$\frac{B}{F} = \frac{x_D - x_F}{x_D - x_B}$$

$$= \frac{0.76 - 0.55}{0.76 - 0}$$

$$\frac{2}{F}$$

$$F = \frac{0.76}{0.21} \times 2 = 7.23 \text{ tonne/h}$$

⑦ →	Mesh No	% Retained	Screen Opening 4.699	(Dpi) avg (mm)	$w_i/5p_i$
	4				
6	-4+6	5 (0.05)	3.327	4.013	0.01245
8	-6+8	6.2 (0.062)	2.362	2.8445	0.02179
10	-8+10	13.0 (0.13)	1.651	2.0065	0.06478
14	-10+14	16.6 (0.166)	1.168	1.4095	0.11777
20	-14+20	15.0 (0.150)	0.833	1.0005	0.14992
28	-20+28	12.4 (0.124)	0.589	0.711	0.17440
35	-28+35	9.0 (0.09)	0.417	0.503	0.17892
48	-35+48	8.2 (0.082)	0.295	0.356	0.23033
65	-48+65	5.0 (0.05)	0.208	0.2515	0.19880
100	-65+100	4.8 (0.048)	0.147	0.1775	0.27042
150	-100+150	3.3 (0.033)	0.104	0.1255	0.26244
200	-150+200	1.5 (0.015)	0.074	0.089	0.16854

$$\sum \frac{x_i}{D_i} = 1.85106$$

Specific
Surface
Area \Rightarrow

$$\frac{6}{\phi_s \rho_p} \sum \frac{x_i}{D_{pi}}$$

$$\Rightarrow \frac{6 \times 1.85106}{5 \times 10^{-2} \times 0.38} = 59 \text{ cm}^2/\text{g}$$

$$74 \text{ cm}^2/\text{g}$$

taking Sphericity
as 0.38

Varies from 0.079 - 0.437
mean value \Rightarrow 0.297