



Inferring phase and amplitude response of oscillatory systems exploiting test stimulation

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Motivation

- We need these characteristics for modelling oscillatory networks
- We need the phase and amplitude response to optimise control of oscillatory dynamics

Analysis of oscillatory systems

- Active analysis vs. passive analysis
- Model-based analysis vs. non-model-based one

Analysis of oscillatory systems

- Active analysis vs. passive analysis
 - ~ Passive analysis: we observe the system under free-running conditions
 - ~ Active analysis: we perturb the system by a specially designed perturbation and look for the response
- Model-based analysis vs. non-model-based one

Analysis of oscillatory systems

- Active analysis vs. passive analysis
- Model-based analysis vs. non-model-based one
 - ~ Non-model-based: no assumption about the origin of the signal
(an example: spectral analysis)
 - ~ Model-based: the validity of the technique crucially depends on the assumption about the system under investigation
(an example: coupling function reconstruction assumes that the signals come from interacting self-sustained oscillators)

Analysis of oscillatory systems

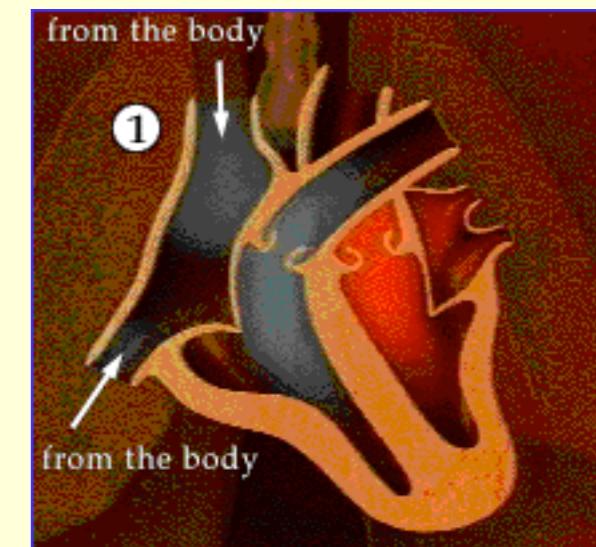
- Active analysis vs. passive analysis
- Model-based analysis vs. non-model-based one

We present an active analysis technique based
on the model of self-sustained oscillators

Self-sustained oscillators

Active oscillators

Biology: systems generating **endogenous** rhythms



Systems of this class:

- 1 generate stationary oscillations without periodic forces
- 2 are dissipative nonlinear systems
- 3 are described by autonomous differential equations
- 4 are represented by a limit cycle in the phase space



Self-sustained oscillator: limit cycle and phase

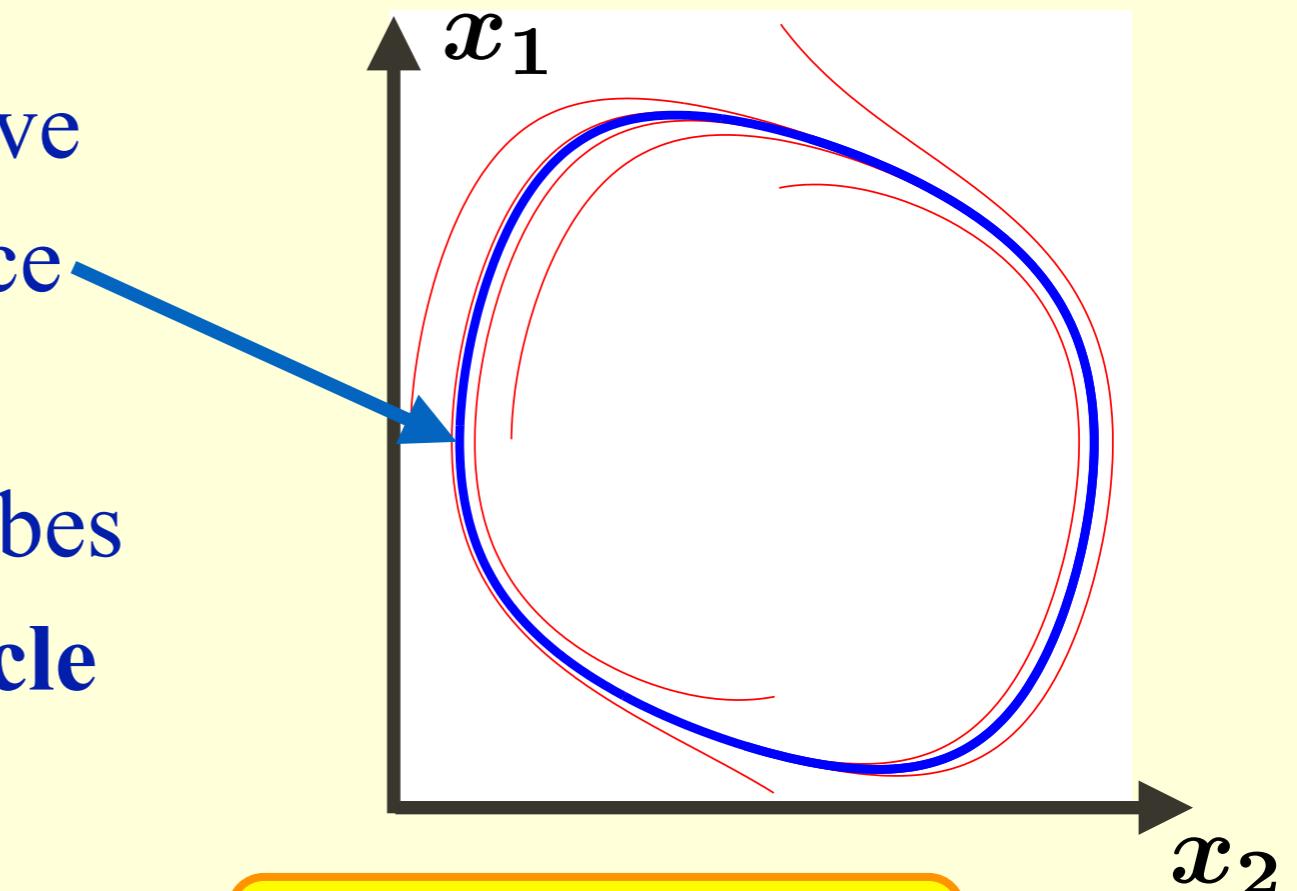
Stable limit cycle: an attractive closed curve in the phase space

Phase is a variable that describes the motion along the **limit cycle**

Phase is defined to obey the condition

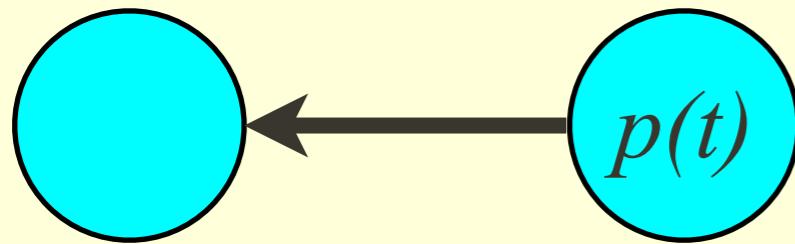
and can be introduced:

1. on the limit cycle
2. in the basin of attraction of the limit cycle



$$\dot{\phi} = \omega = 2\pi/T$$

Phase dynamics: the phase sensitivity function



Suppose the oscillator is driven by
weak perturbation $p(t)$

Then

$$\dot{\varphi} = \omega + Z(\varphi)p(t)$$

Phase Sensitivity function, or
Phase Response Curve (PRC)

Phase dynamics equation in the Winfree form

- PRC is a basic characteristic of a limit-cycle oscillator
- PRC description is widely used, e.g. in neuroscience

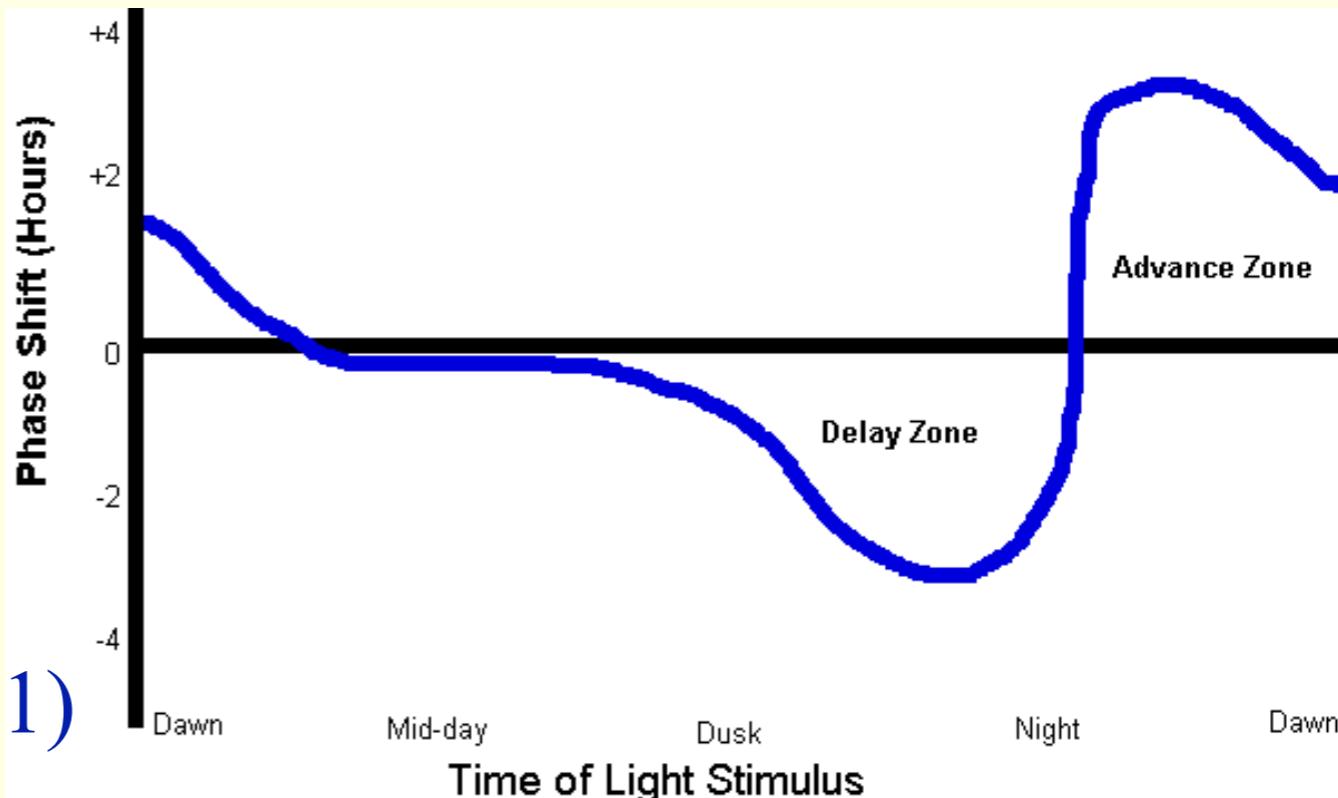
Phase response curve: examples

PRC quantifies response (phase shift) of an oscillator to a perturbation

Example: human circadian cycle

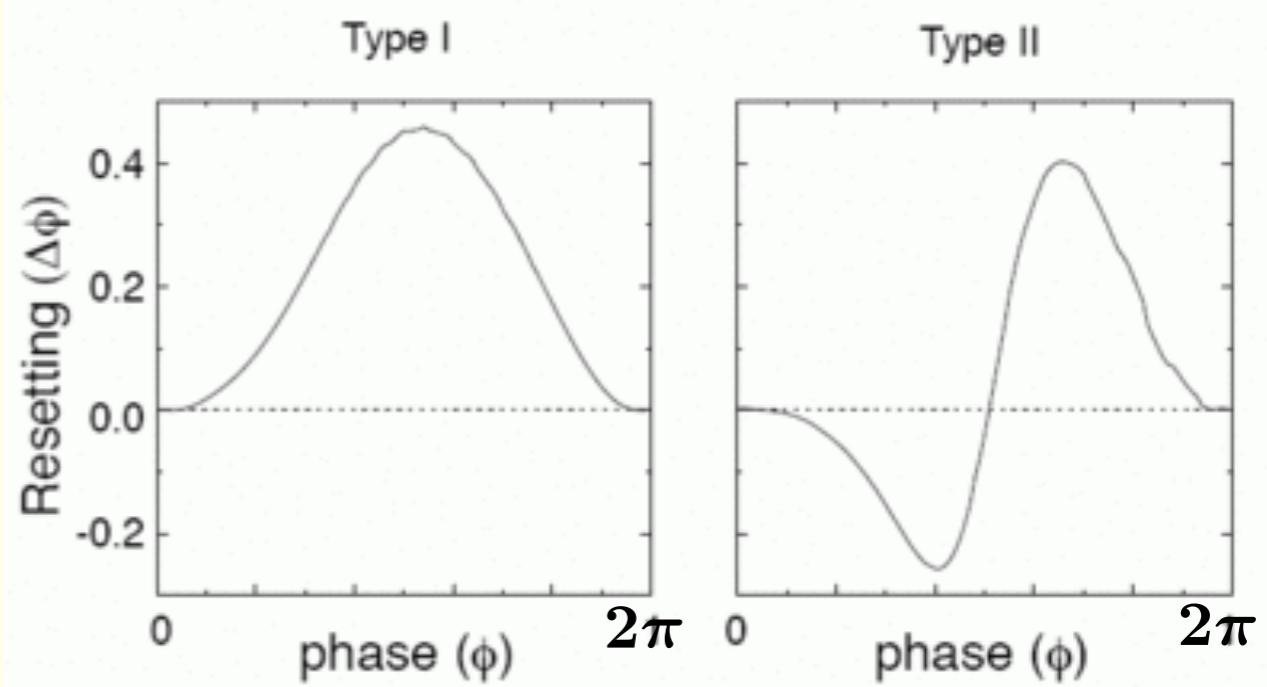
- *Delay region: evening light shifts sleepiness later and*
- *Advance region: morning light shifts sleepiness earlier.*

(Wikipedia; Kripke & Loving, 2001)



Example: neural PRCs

(Scholarpedia)

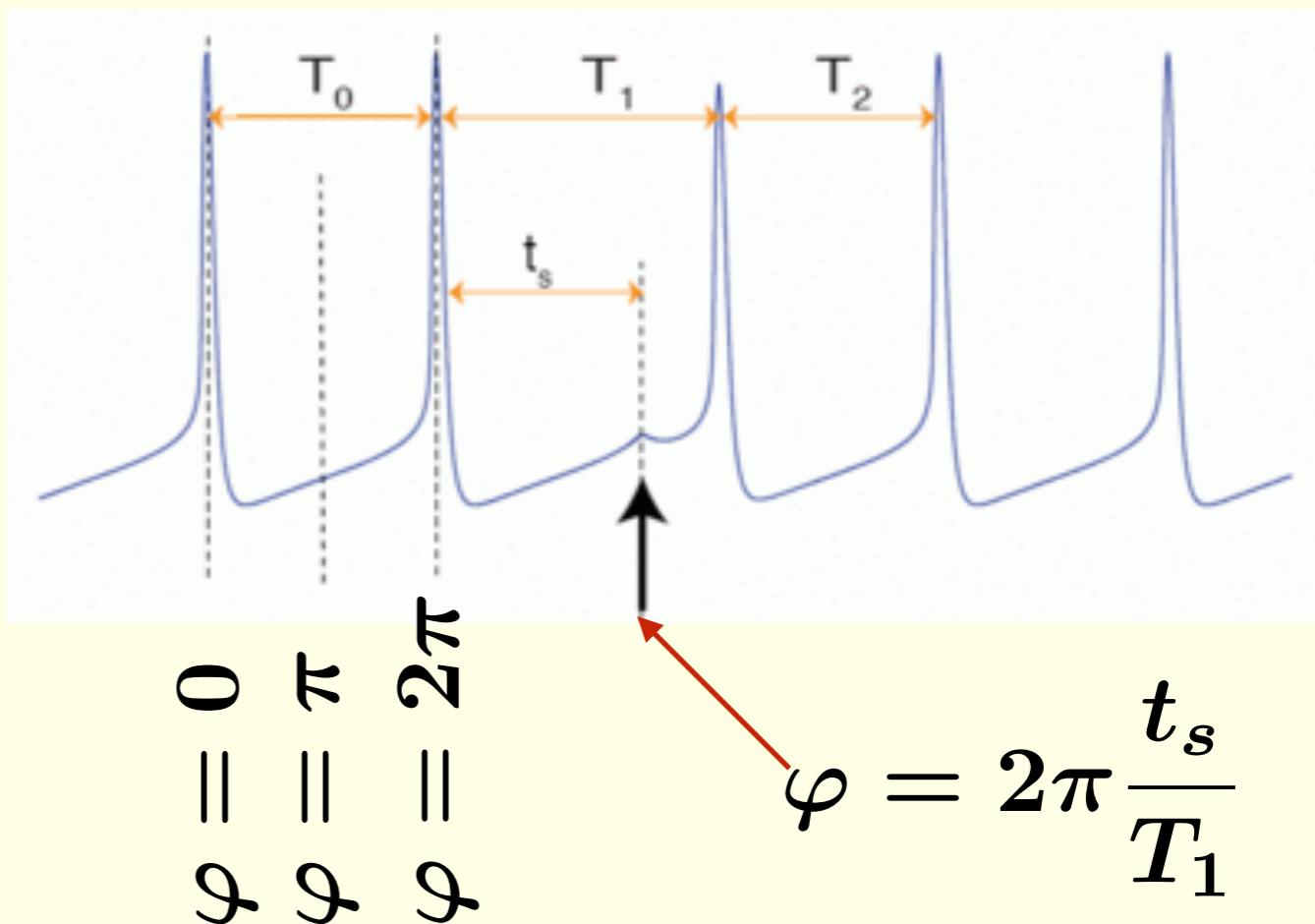


PRC determination

Traditional approach to PRC determination: repeated stimulation of an isolated oscillator by short pulses

(Picture from Scholarpedia)

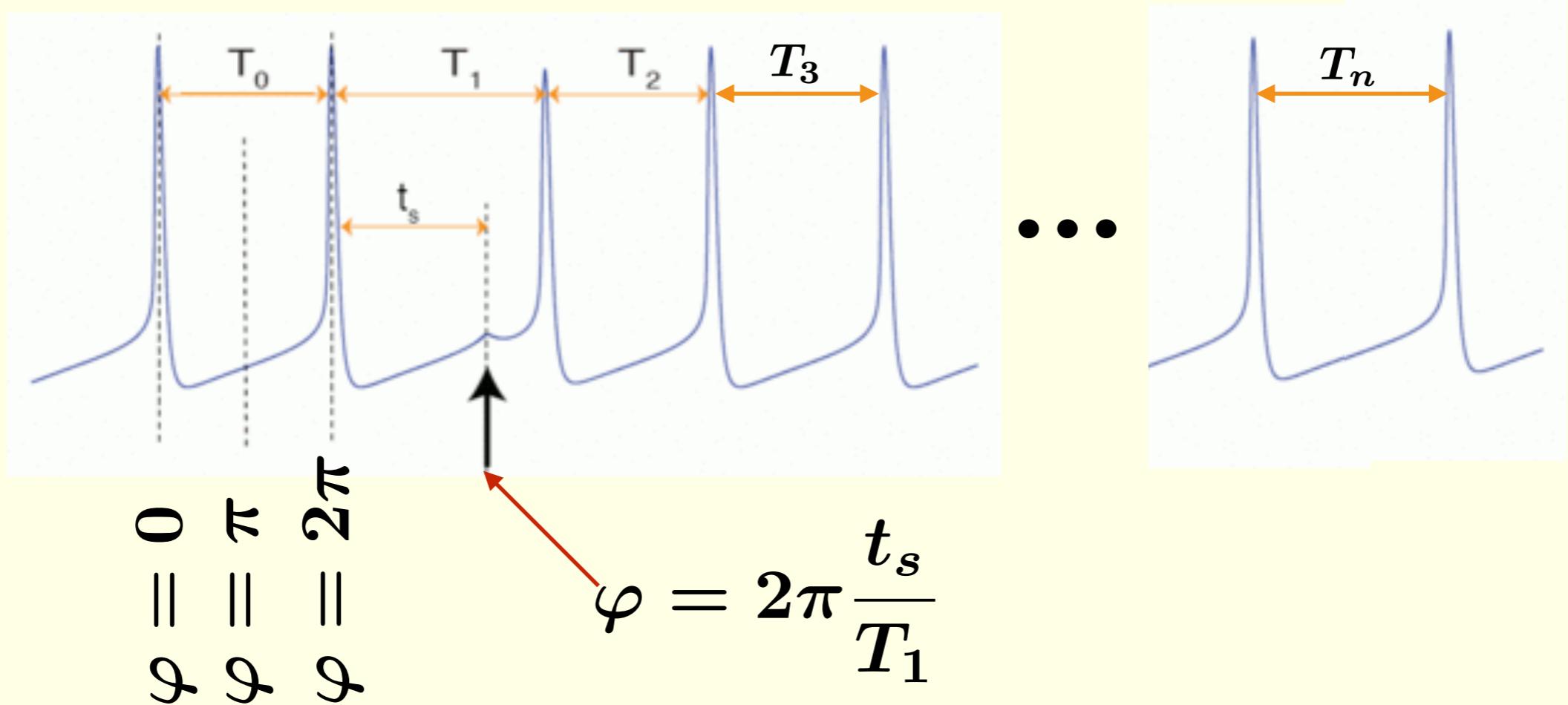
$$Z(\varphi) = 2\pi \frac{T_0 - T_1}{T_0}$$



This works well with neuronal system that are well-described by integrate-and-fire models

PRC determination II

Generally, one has to follow several periods after the kick



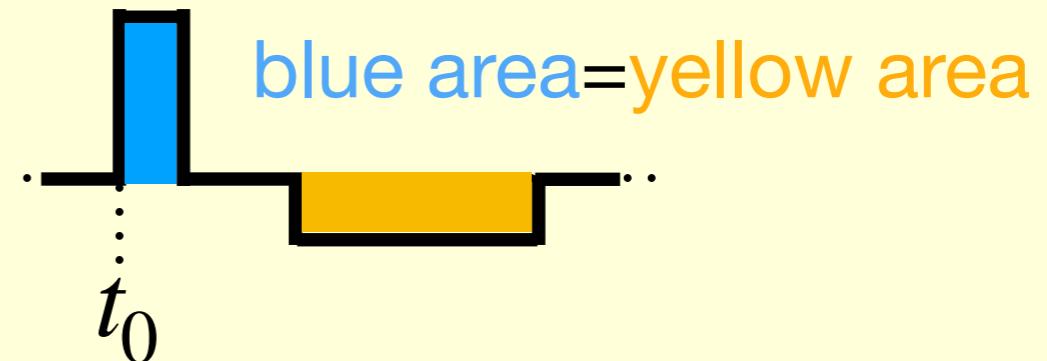
$$Z(\varphi) = 2\pi \frac{nT_0 - \sum_{j=1}^n T_j}{T_0}$$

(PRC is typically normalized by the amplitude of the kick)

PRC determination: problems

- The standard approach requires narrow pulses that reasonably approximate Dirac's delta function; however, in biological applications, the pulses frequently must be **charge-balanced**

Pulse $\mathcal{P}(t - t_0)$



We denote theoretical PRC (response to Dirac's delta) as $Z(\varphi)$

We denote effective PRC (response to arbitrary \mathcal{P}) as $Z_{\mathcal{P}}(\varphi)$

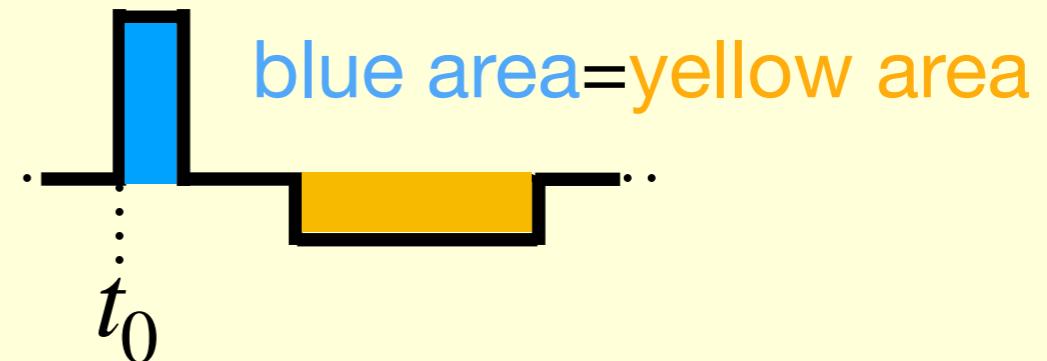


We need a technique for re-computation $Z_{\mathcal{P}}(\varphi) \rightarrow Z(\varphi)$

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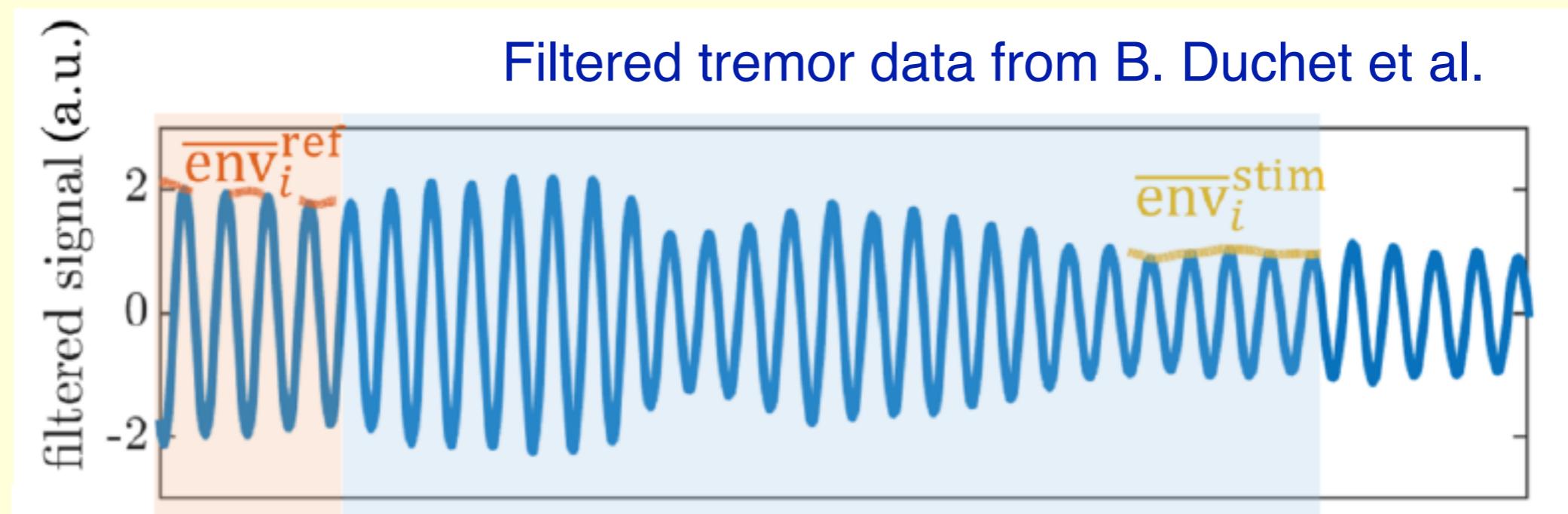


We need a technique for re-computation $Z_{\mathcal{P}}(\varphi) \rightarrow Z(\varphi)$

... and we provide it!

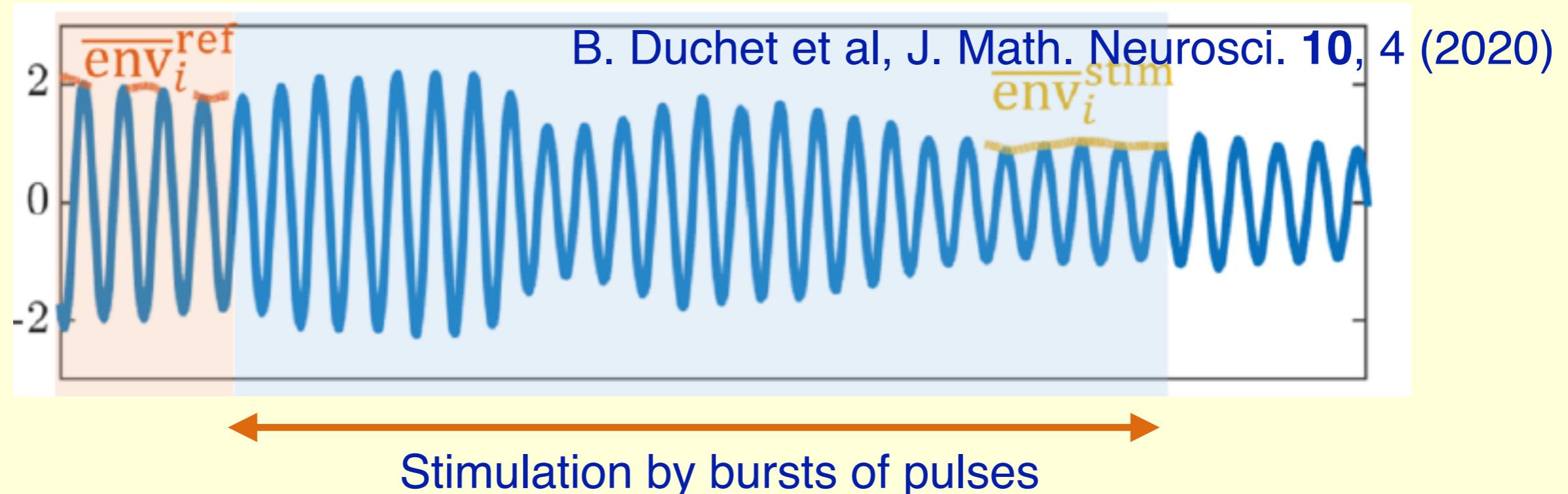
PRC determination: problems II

- The standard approach works well if the signal has well-defined marker events that can be assigned a specific phase value



We need a technique for arbitrary stimulation's and signal's shape

PRC determination: problems II



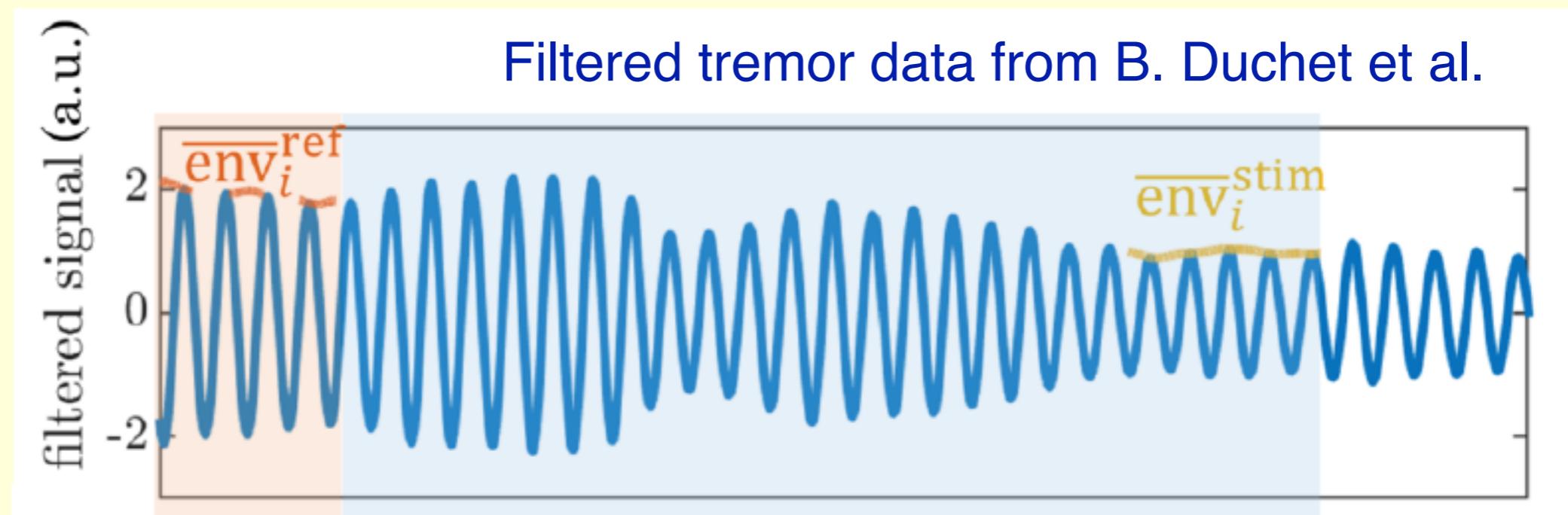
Amplitude changes due to stimulation



Weakly stable limit cycle

PRC determination: problems II

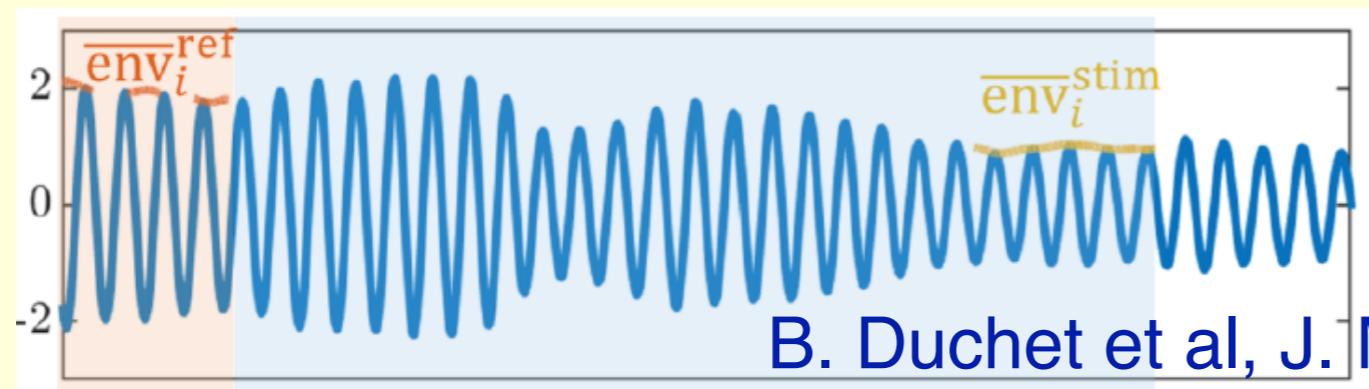
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We need a technique for arbitrary stimulation's and signal's shape

PRC determination in the context of Deep Brain Stimulation (DBS)

- Fitting sine-wave before and after the stimulus
 - A. Holt and T. Netoff, J Comput Neurosci **37**, 505 (2014)
 - A. Holt et al, PLoS Comput. Biol. **12**, e1005011 (2016)
- Using Hilbert Transform (HT) to evaluate phase (and amplitude) variation due to the pulse



B. Duchet et al, J. Math. Neurosci. **10**, 4 (2020)

Both techniques have never been tested on models with known PRC

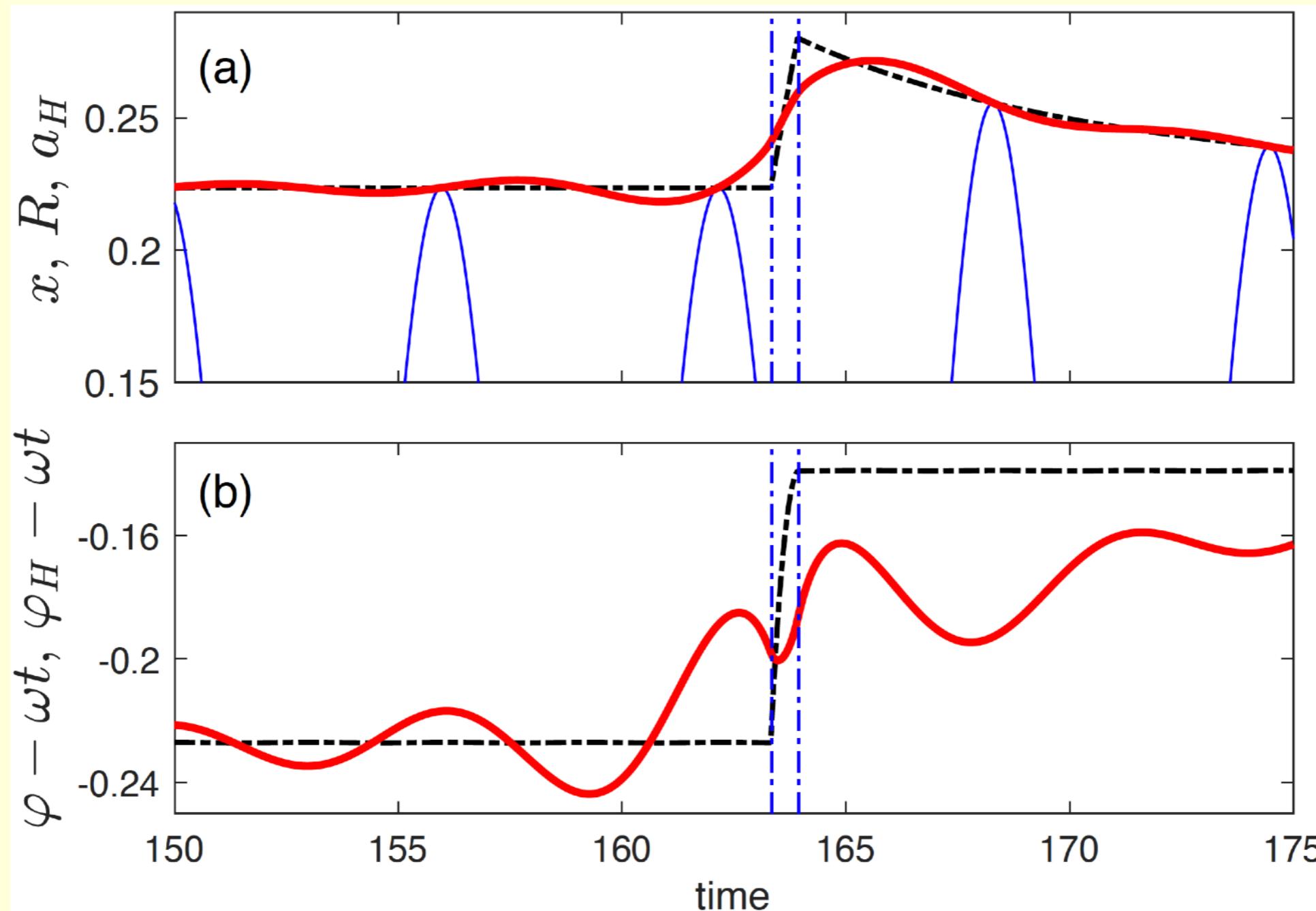
- We need test models
- We need a measure of goodness of the PRC determination

Amplitude response - an unexplored problem

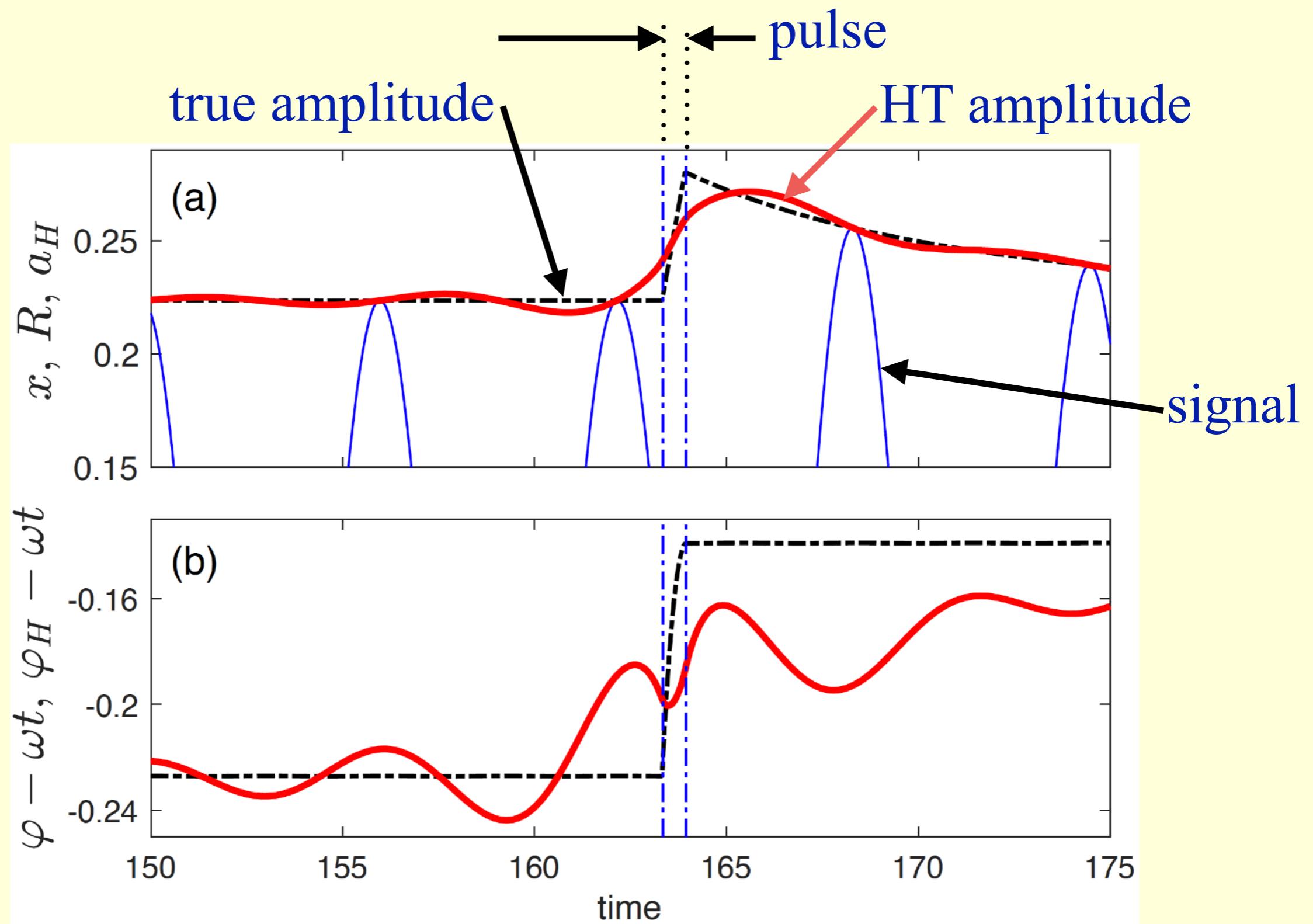
- Irrelevant for neuron-like systems (relaxational oscillators, strongly stable limit cycle); no effect of simulation on the amplitude
- Highly relevant in the context of DBS, where the goal of the stimulation is to suppress the oscillation, i.e., to affect the amplitude. This is possible for a weakly stable cycle only.
- The main problem is the amplitude's definition
- *Ad hoc* approach (B. Duchet et al.): to compute the amplitude response curve as $A(\varphi) = a_{\text{after pulse}}/a_{\text{before pulse}}$, where $a(t)$ is the instantaneous amplitude obtained via HT

Tests of known techniques: Hilbert-based

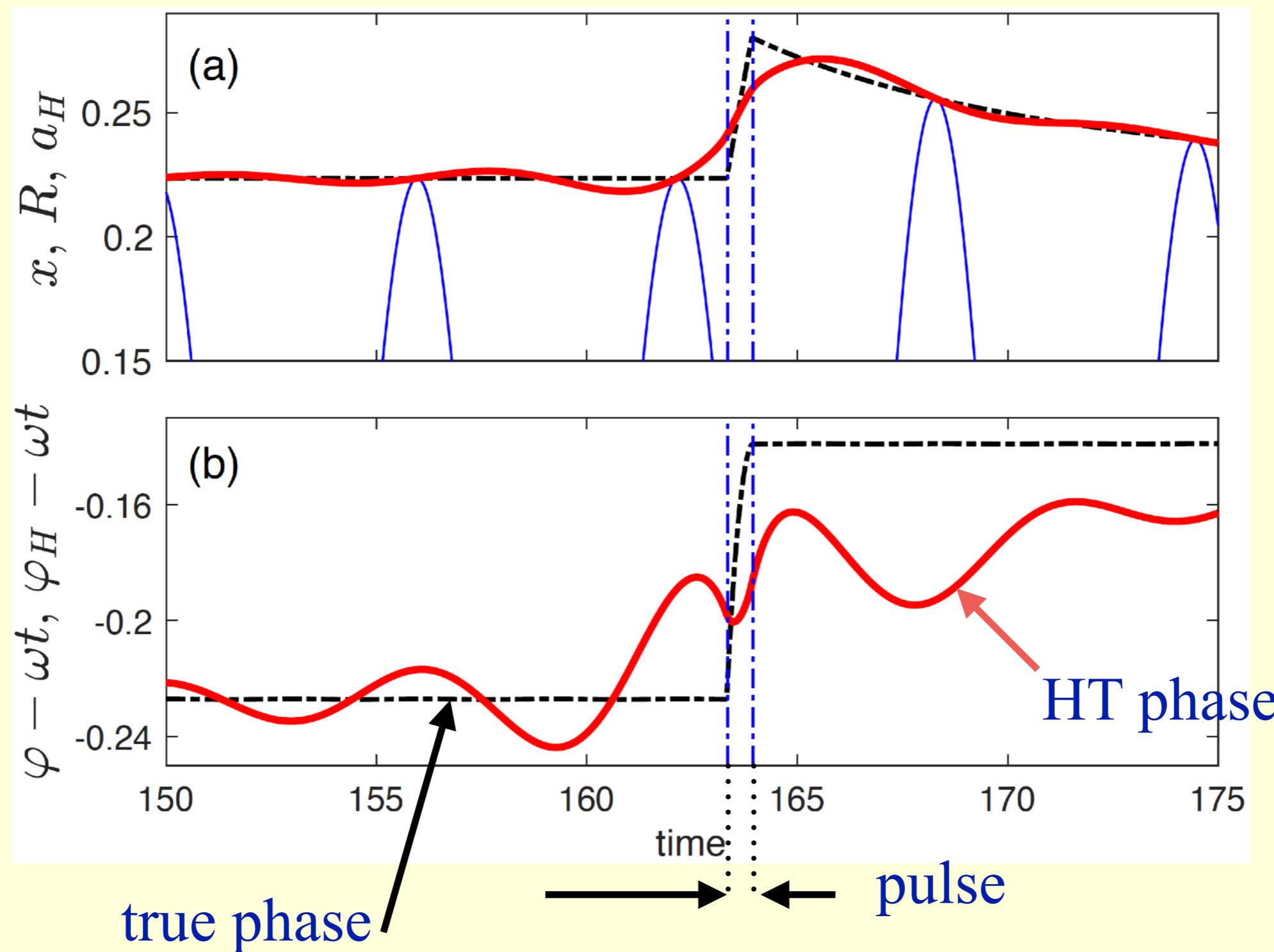
Hilbert transform is non-local, it is known to work poorly with pulse perturbation, here is the test for the SL system



Tests of known techniques: Hilbert-based



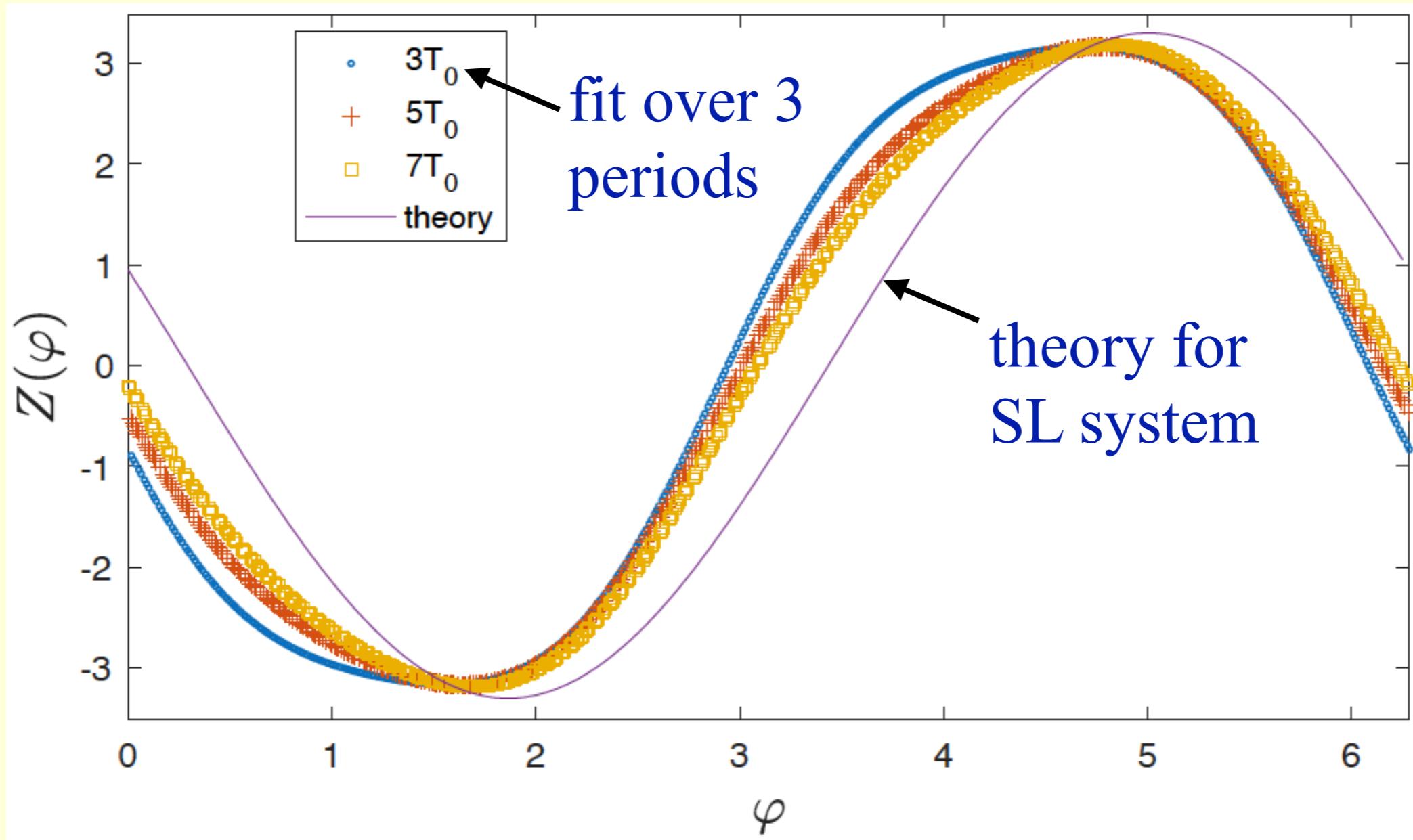
Tests of known techniques: Hilbert-based



Hilbert-based technique: summary

- the results depend on the observable (not shown)
- works only with nearly harmonic signals
- can be improved (not shown), but remains imprecise

Tests of known techniques: sine-fitting



- works only with nearly harmonic signals
- is imprecise
- requires long time series

Phase - isostable variable representation

For an autonomous 2-dimensional system:

$$\dot{\varphi} = \omega, \quad \dot{\psi} = \kappa\psi$$

Floquet exponent Isostable variable

ψ quantifies deviation from the limit cycle

For a perturbed system (1st approximation!):

$$\dot{\varphi} = \omega + Z(\varphi)p(t), \quad \dot{\psi} = \kappa\psi + I(\varphi)p(t)$$

Isostable response curve (IRC)

The description applies to multidimensional systems if relaxation in one direction is much slower than in others

For details, see Wilson and Moehlis, PRE 94, 052213 (2016)

Wilson and Ermentrout, SIAM J on Appl Dyn Sys 17, 2516 (2018)

Wilson, PRE 99, 022210 (2019)

Phase - isostable variable representation

For an autonomous 2-dimensional system:

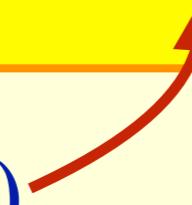
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For a perturbed system (1st approximation!):

$$\dot{\varphi} = \omega + Z(\varphi)p(t), \quad \dot{\psi} = \kappa\psi + I(\varphi)p(t)$$

Isostable response curve (IRC) 

We present an algorithm for inferring these equations
from an observation of the perturbed system

Computing PRC from a known input

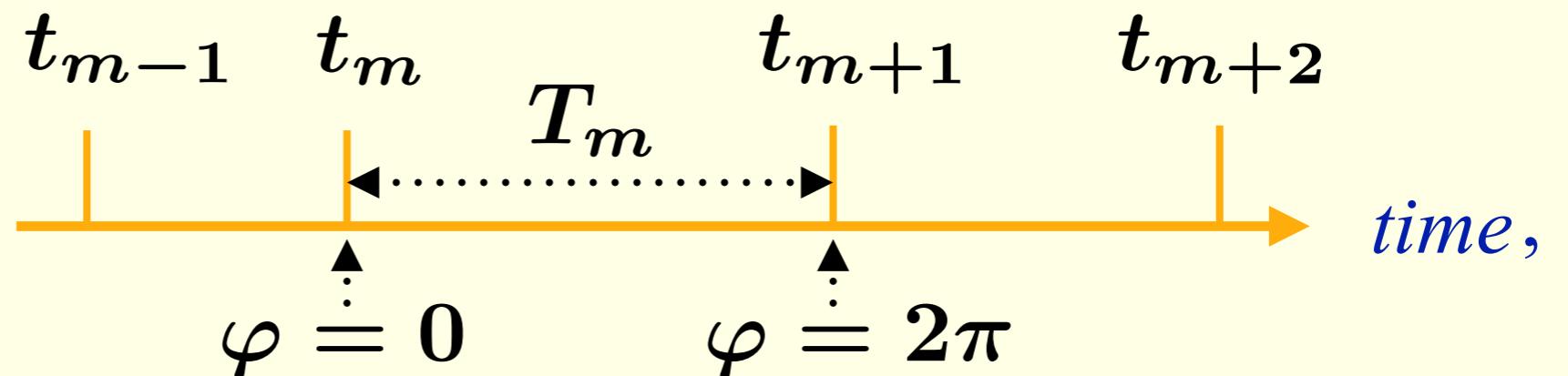
We adapt our approach from

Rok Cestnik & M. R. Sci Rep 8, 13606, 2018

We perturb the oscillator by the pulse train $p(t) = \sum_k \mathcal{P}(t - t_k)$

We define events via thresholding, e.g., $x(t) = x_{threshold}, \dot{x} > 0$

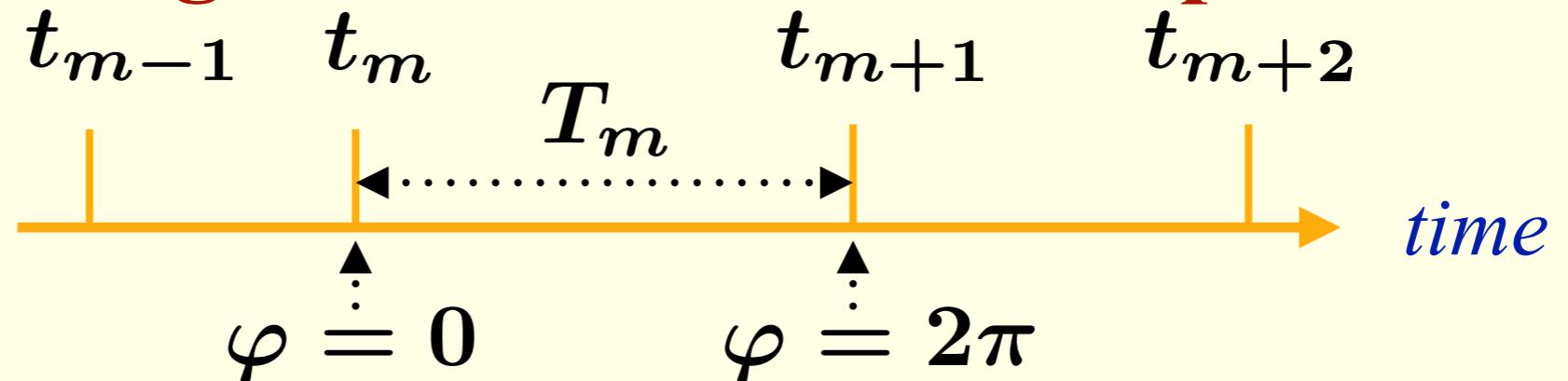
Notations



The choice of the threshold can be optimised

Computing PRC from a known input

Notations



Winfree model $\dot{\varphi} = \omega + Z(\varphi)p(t)$

$$\int_0^{2\pi} d\varphi = \int_{t_m}^{t_m + T_m} [\omega + Z(\varphi)p(t)] dt$$

Substituting PRC as a finite Fourier series,

$$Z(\varphi) = a_0 + \sum_{n=1}^N [a_n \cos(n\varphi) + b_n \sin(n\varphi)]$$

we obtain m equations:

$$2\pi = \omega T_m + a_0 \int_{t_m}^{t_m + T_m} p(t) dt + \sum_{n=1}^N \left[a_n \int_{t_m}^{t_m + T_m} p(t) \cos[n\varphi(t)] dt + b_n \int_{t_m}^{t_m + T_m} p(t) \sin[n\varphi(t)] dt \right]$$

Computing PRC from a known input

$$2\pi = \omega T_m + a_0 \int_{t_m}^{t_m+T_m} p(t) dt + \sum_{n=1}^N \left[a_n \int_{t_m}^{t_m+T_m} p(t) \cos[n\varphi(t)] dt + b_n \int_{t_m}^{t_m+T_m} p(t) \sin[n\varphi(t)] dt \right]$$

Eq.(*)

We solve the problem by iterations: first we take

$$\varphi^{(0)}(t) = 2\pi(t - t_m)/T_m \in [t_m, t_m + T_m]$$

Computing PRC from a known input

$$2\pi = \omega T_m + a_0 \int_{t_m}^{t_m+T_m} p(t) dt + \sum_{n=1}^N \left[a_n \int_{t_m}^{t_m+T_m} p(t) \cos[n\varphi(t)] dt + b_n \int_{t_m}^{t_m+T_m} p(t) \sin[n\varphi(t)] dt \right]$$

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iteration 

Computing PRC from a known input

$$Eq. (*) \quad 2\pi = \omega T_m + a_0 \int_{t_m}^{t_m+T_m} p(t) dt + \sum_{n=1}^N \left[a_n \int_{t_m}^{t_m+T_m} p(t) \cos[n\varphi(t)] dt + b_n \int_{t_m}^{t_m+T_m} p(t) \sin[n\varphi(t)] dt \right]$$

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$$\varphi^{(0)}(t) = 2\pi(t - t_m)/T_m \in [t_m, t_m + T_m]$$

iteration ↗

substitute into *Eq.(*)*, compute numerically all integrals

↓

system of M linear equations for $2N+2$ coefficients

↓

for $M > 2N+2$ we solve the system using l.m.s. optimisation

↓

first approximation for frequency and PRC $\omega^{(1)}, Z^{(1)}$

Next approximation for the phase

We integrate numerically $\dot{\varphi}^{(1)} = \omega^{(1)} + Z^{(1)}(\varphi^{(0)}(t)) p(t)$ for each inter-spike interval with initial condition $\varphi^{(1)}(t_m) = 0$

It is, for $0 \leq \tau \leq T_m$ we compute

$$\varphi^{(1)}(t_m + \tau) = \omega^{(1)}\tau + \int_{t_m}^{t_m + \tau} Z^{(1)}(\varphi^{(0)}(t)) p(t) dt$$

Since everything is approximate, generally

$$\varphi^{(1)}(t_m + T_m) = \psi_m^{(1)} \neq 2\pi$$

Therefore we **rescale the phase**: $\varphi^{(1)}(t) \rightarrow 2\pi\varphi^{(1)}(t)/\psi_m^{(1)}$

Quantities $\psi_m^{(k)}$ will be used to monitor convergence of iterations

Second iteration

$$Eq. (*) \quad 2\pi = \omega T_m + a_0 \int_{t_m}^{t_m+T_m} p(t) dt + \sum_{n=1}^N \left[a_n \int_{t_m}^{t_m+T_m} p(t) \cos[n\varphi(t)] dt + b_n \int_{t_m}^{t_m+T_m} p(t) \sin[n\varphi(t)] dt \right]$$

We obtained $\varphi^{(1)}(t)$



substitute into $Eq. (*)$, compute numerically all integrals

system of M linear equations for $2N+2$ coefficients

for $M > 2N+2$ we solve the system using l.m.s. optimisation



second approximation for frequency and PRC $\omega^{(2)}, Z^{(2)}$

Second and further iterations

$$Eq.(*) \quad 2\pi = \omega T_m + a_0 \int_{t_m}^{t_m+T_m} p(t) dt + \sum_{n=1}^N \left[a_n \int_{t_m}^{t_m+T_m} p(t) \cos[n\varphi(t)] dt + b_n \int_{t_m}^{t_m+T_m} p(t) \sin[n\varphi(t)] dt \right]$$

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second approximation for frequency and PRC $\omega^{(2)}, Z^{(2)}$



$\omega^{(k)}, Z^{(k)}, \psi_m^{(k)}$

Monitoring convergence

Recall:

$$\varphi^{(1)}(t_m + \tau) = \omega^{(1)}\tau + \int_{t_m}^{t_m + \tau} Z^{(1)} \left(\varphi^{(0)}(t) \right) p(t) dt$$

Since everything is approximate, generally

$$\varphi^{(1)}(t_m + T_m) = \psi_m^{(1)} \neq 2\pi$$

and similarly for further iterations, $\psi_m^{(k)}$

We introduce the average error $\Delta_\psi = \langle (\psi_m - 2\pi)^2 \rangle^{1/2}$

to be compared with

$$\Delta_{\psi_T} = \langle (\langle \omega \rangle T_m - 2\pi)^2 \rangle^{1/2} \text{ where } \langle \omega \rangle = \langle 2\pi/T_m \rangle$$

(error of trivial prediction with average period)

Quality of the PRC estimation

We introduce the average error $\Delta_\psi = \langle (\psi_m - 2\pi)^2 \rangle^{1/2}$

to be compared with

$$\Delta_{\psi_T} = \langle (\langle \omega \rangle T_m - 2\pi)^2 \rangle^{1/2} \text{ where } \langle \omega \rangle = \langle 2\pi/T_m \rangle$$

(error of trivial prediction with average period)

The measure $E = \Delta_\psi / \Delta_{\psi_T}$ quantifies the quality of the estimation

This measure can and shall be used with any inference technique!

Inferring 1st-order phase-isostable dynamics (IPID-1 technique)

First, we infer PRC; this also yields $\varphi(t)$.

From $\varphi(t)$ we obtain time events τ_i of equal phase, $\varphi(\tau_i) = \text{const}$

For a noise-free unperturbed system, the observed signal would be $s(\tau_i) = \text{const} = s_0$

For the perturbed system, we write in the 1st order:

$$\psi_i = c(\varphi(\tau_i) - s_0) \quad (*)$$

Generally, $c = c(\varphi)$, $s_0 = s_0(\varphi)$. However, at points τ_i phase is the same. Hence, c and s_0 in Eq. (*) are constants.

Additionally, ψ is defined up to a constant factor $\implies c = 1$

IPIID-1 technique

We integrate the isostable dynamics $\dot{\psi} = \kappa\psi + I(\varphi)p(t)$

$$\psi_{i+1} - \psi_i = \kappa \int_{\tau_i}^{\tau_{i+1}} \psi(t) dt + \int_{\tau_i}^{\tau_{i+1}} I(\varphi)p(t) dt$$

Using $\psi_i = c(\psi(\tau_i) - s_0)$, we write the l.h.s. as $s(\tau_{i+1}) - s(\tau_i)$

Substituting $I(\varphi)$ as a finite Fourier series, we obtain a linear

system, but we have to compute the integral $\kappa \int_{\tau_i}^{\tau_{i+1}} \psi(t) dt$

We write it as

$$\kappa \int_{\tau_i}^{\tau_{i+1}} \psi(t) dt = -\kappa s_0(\tau_{i+1} - \tau_i) + \kappa \int_{\tau_i}^{\tau_{i+1}} (\psi(t) + s_0) dt$$

IPID-1 technique II

We write it as

$$\kappa \int_{\tau_i}^{\tau_{i+1}} \psi(t) dt = -\kappa s_0(\tau_{i+1} - \tau_i) + \kappa \int_{\tau_i}^{\tau_{i+1}} (\psi(t) + s_0) dt$$

becomes another variable for the linear system

this function is known in endpoints:

$$\psi(\tau_i) + s_0 = s(\tau_i)$$

$$\psi(\tau_{i+1}) + s_0 = s(\tau_{i+1})$$

we approximate $\int_{\tau_i}^{\tau_{i+1}} (\psi(t) + s_0) dt \approx [s(\tau_i) + s(\tau_{i+1})]/2.$

we solve the linear system and obtain the 1st-approximation

$$s_0^{(1)}, \kappa^{(1)}, I^{(1)}(\varphi)$$

IPID-1 technique III

we solve the linear system and obtain the 1st-approximation

$$s_0^{(1)}, \kappa^{(1)}, I^{(1)}(\varphi)$$



again, we use iterations to obtain next approximations

starting with $s_0^{(m)}, \kappa^{(m)}, I^{(m)}(\varphi)$, we compute

$$\psi^{(m)}(t) = s(\tau_i) - s_0^{(m)} + \int_{\tau_i}^t [\kappa^{(m)} \psi^{(m)}(t') + I^{(m)}(\varphi)p(t')] dt'$$



$$\psi^{(m)}(\tau_i)$$



and solve the linear system to obtain $s_0^{(m+1)}, \kappa^{(m+1)}, I^{(m+1)}(\varphi)$

Monitoring the inference's error

starting with $s_0^{(m)}, \kappa^{(m)}, I^{(m)}(\varphi)$, we compute

$$\psi^{(m)}(t) = s(\tau_i) - s_0^{(m)} + \int_{\tau_i}^t [\kappa^{(m)} \psi^{(m)}(t') + I^{(m)}(\varphi) p(t')] dt'$$

$\psi^{(m)}(\tau_i)$

Our model is not exact, hence $\Psi_i^{(m)} = \lim_{t \uparrow \tau_{i+1}} \psi^{(m)}(t) \neq s(\tau_{i+1}) - s_0^{(m)}$.

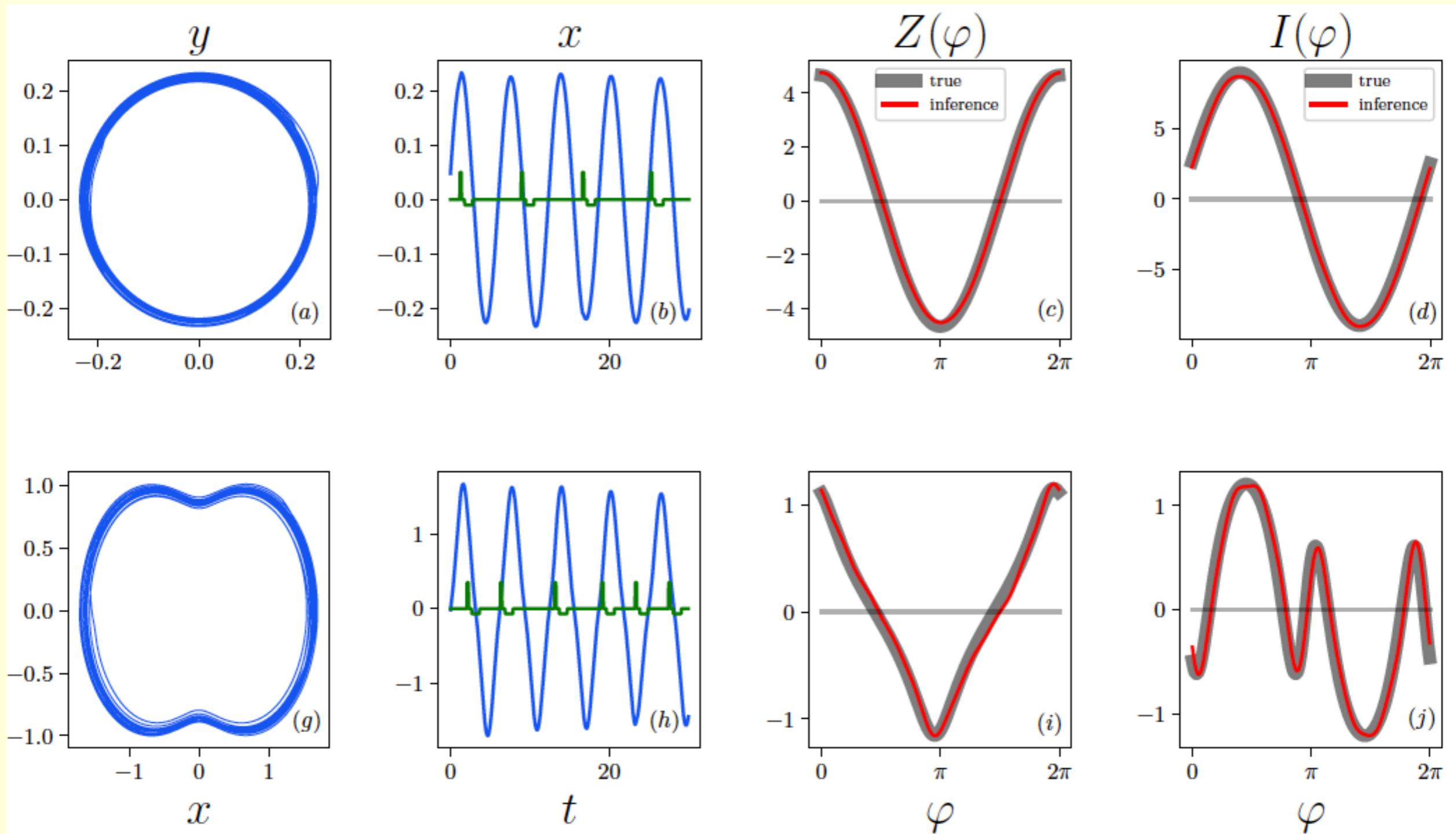
We define the error as

$$E_I^{(m)} = \langle (\Psi_i^{(m)} - (s(\tau_{i+1}) - s_0^{(m)}))^2 \rangle^{1/2}$$

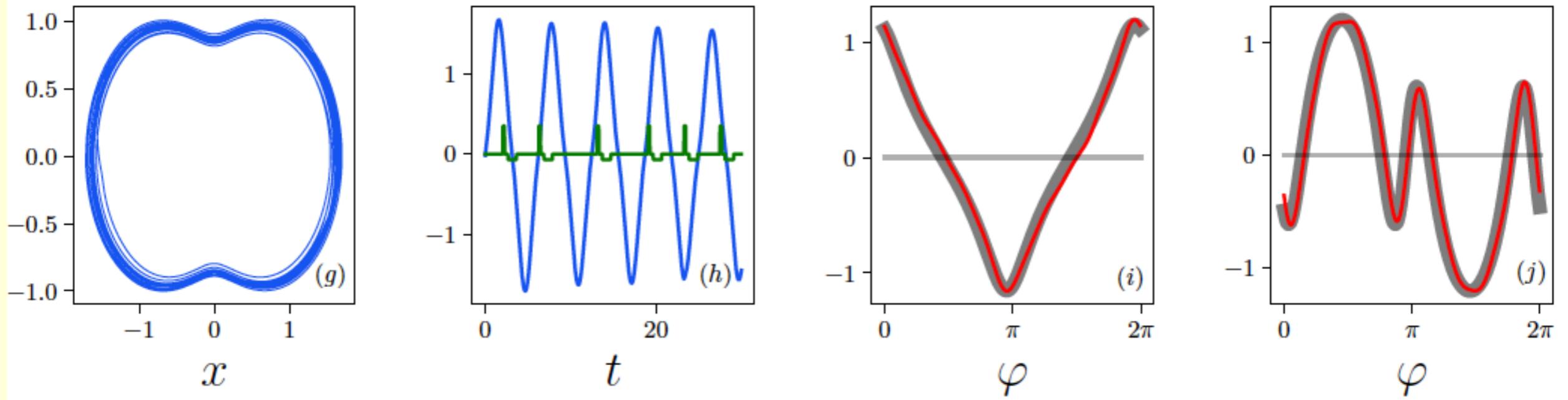
and compare it with the signal's variability at events

$$E_{I0} = \langle (s(\tau_i) - \langle s(\tau_i) \rangle)^2 \rangle^{1/2}$$

Results for test models with known $Z(\varphi)$, $I(\varphi)$

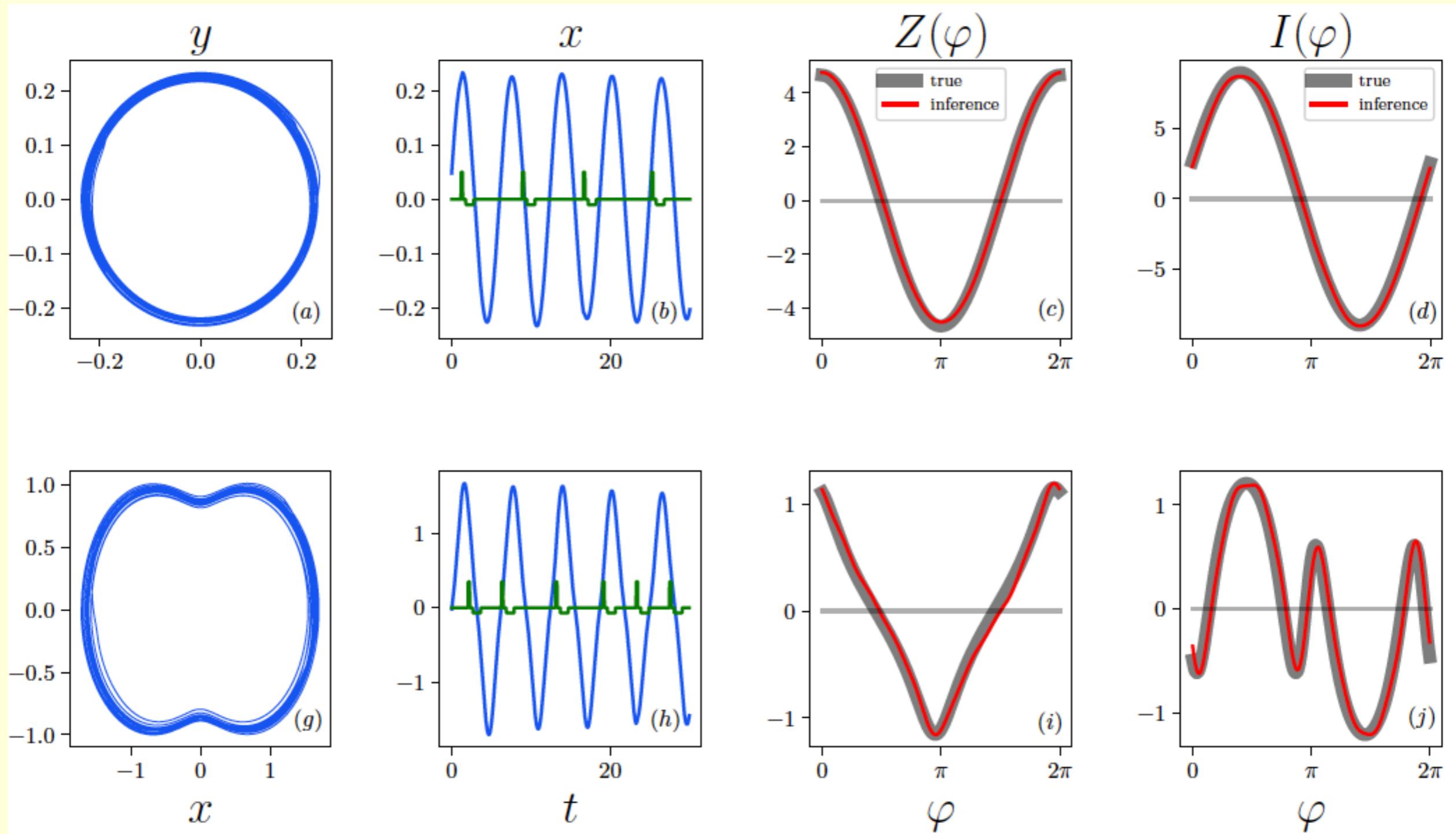


Results for test models with known $Z(\varphi)$, $I(\varphi)$



We constructed test models with known $Z(\varphi)$ and $I(\varphi)$
These models generate different waveforms

Results for test models with known $Z(\varphi)$, $I(\varphi)$

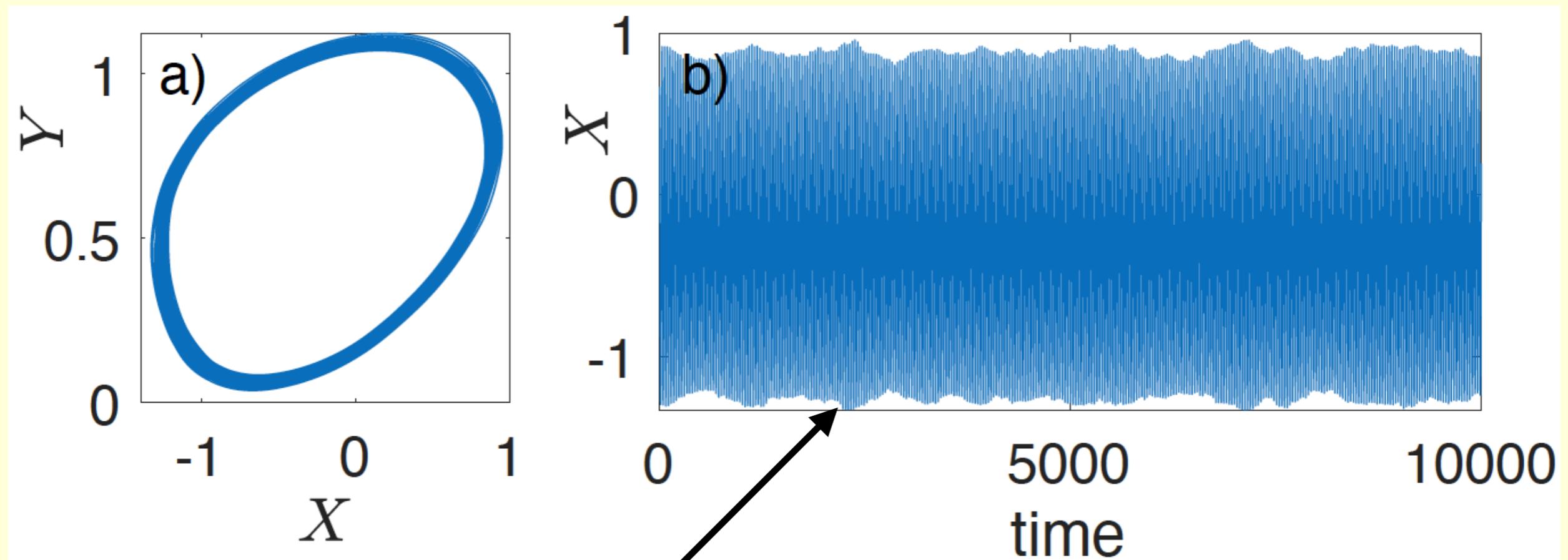


Further results for the IPID-1 technique

It is most reliable technique in the presence of noise

It performs better for a high-dimensional chaotic system

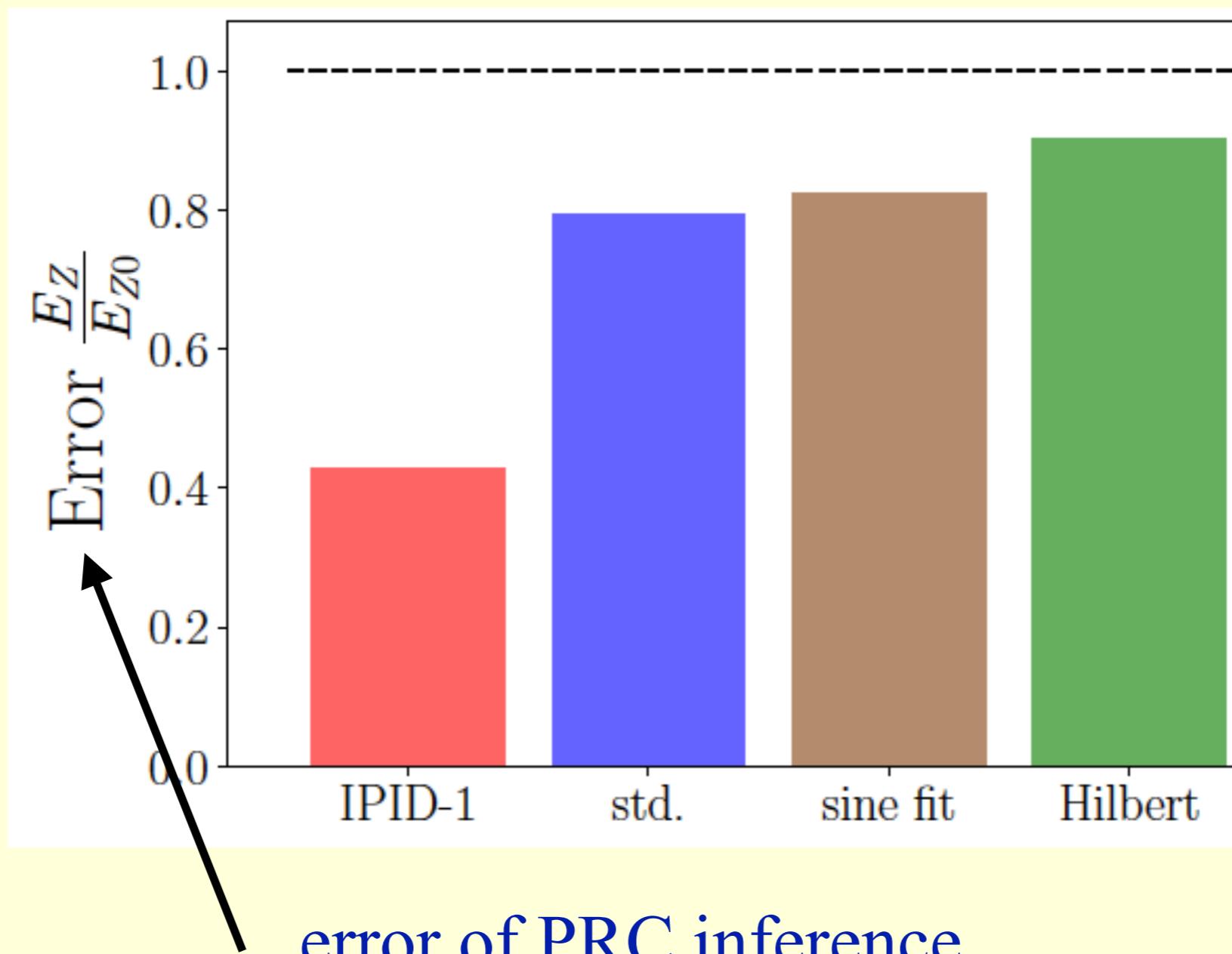
(ensemble of globally-coupled Bonhoeffer -van der Pol systems with chaotic mean field)



observable of the unperturbed system

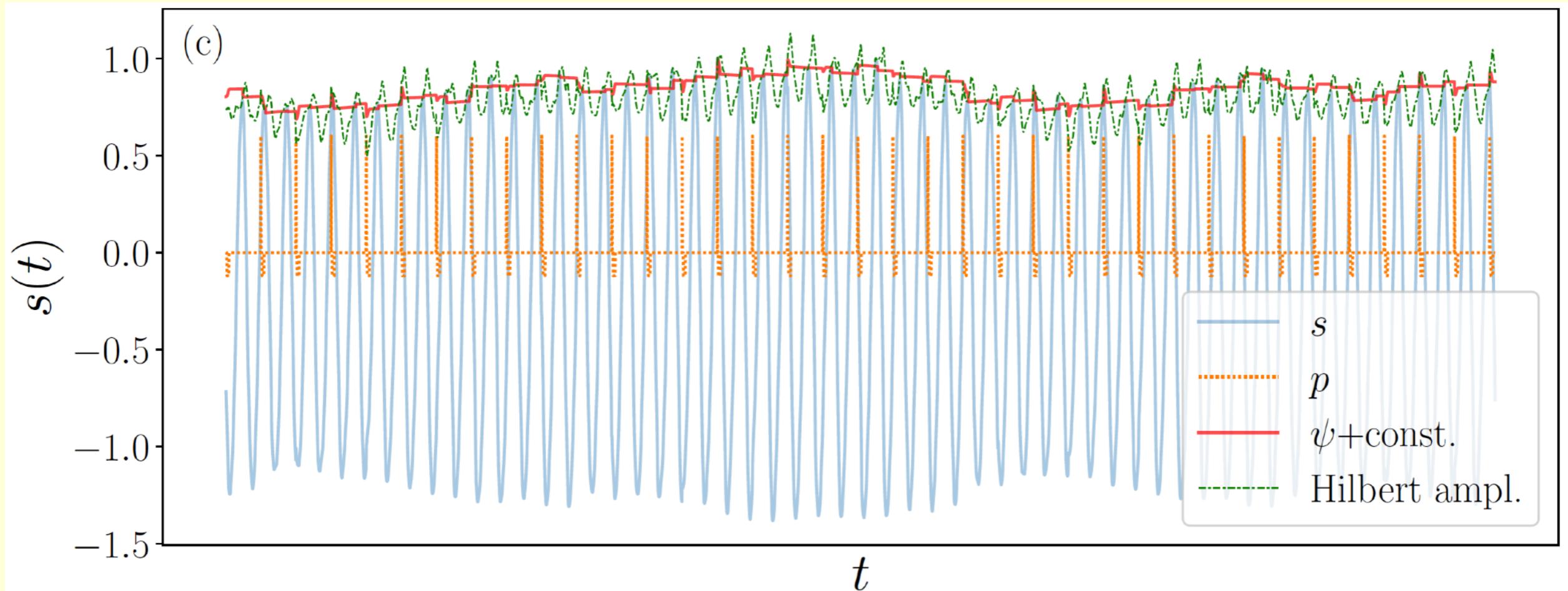
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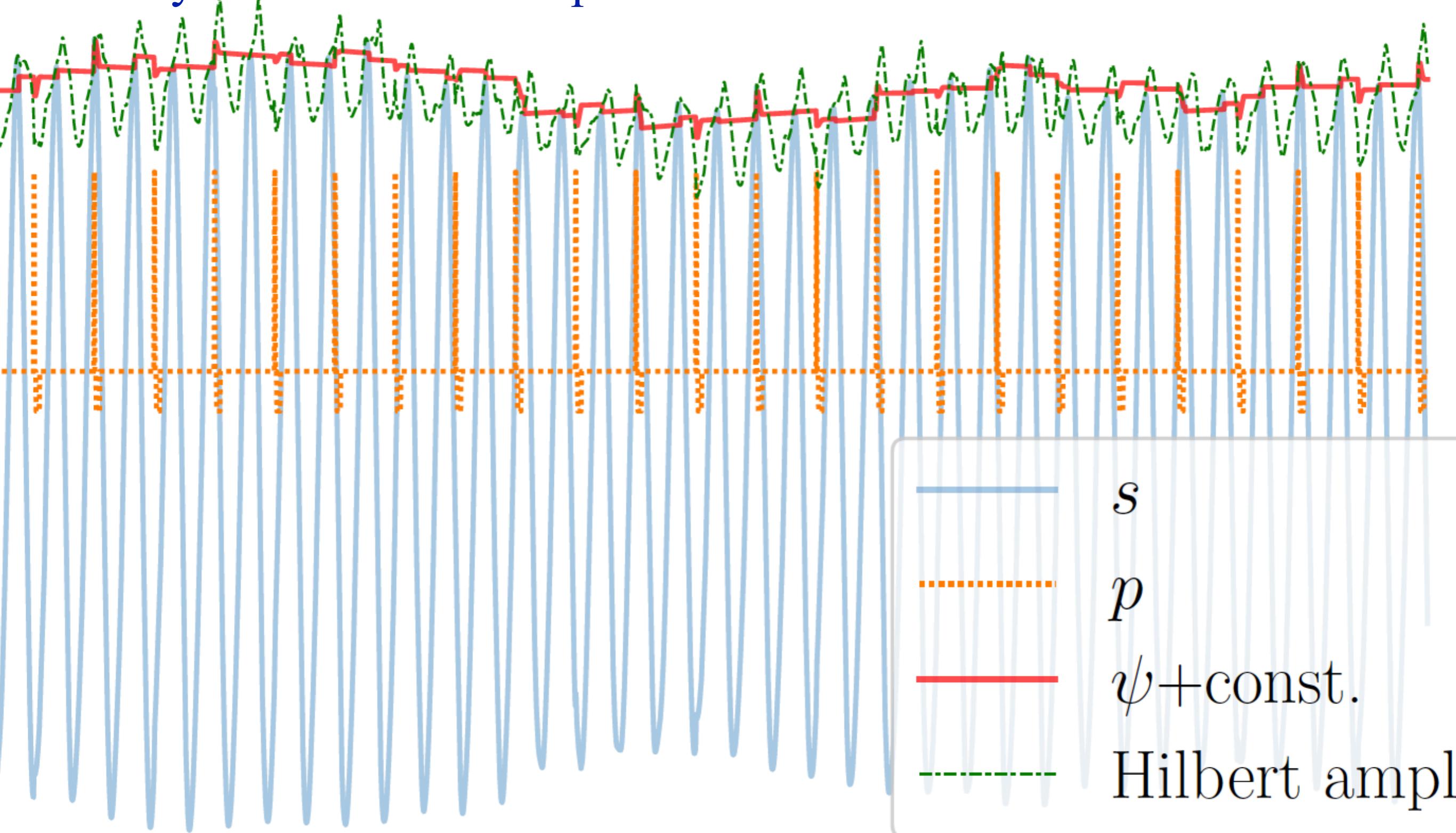
Further results for the IPID-1 technique

It yields better envelope than the Hilbert Transform



Further results for the IPID-1 technique

It yields better envelope than the Hilbert Transform



Conclusions

- Reconstruction of the phase - isostable dynamics
 - is independent of the observable
 - robust against noise
 - requires shorter time series
- Inference of the PRC for arbitrary pulse shape
- Test models with known ground truth
- Estimation of the inference error from data

Rok Cestnik, E. Mau, M. Rosenblum, arXiv:2206.09173 (June 2022)

