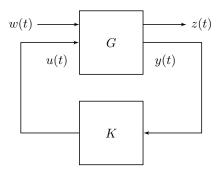
Output Feedback Control

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\mathcal{H}_2 Optimal Controller

\mathcal{H}_2 Optimal Controller

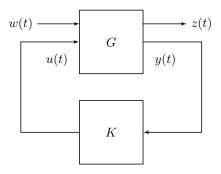


Let

$$\hat{G}(s) = \begin{bmatrix} A & B_1 & B_2 \\ \hline C_1 & \mathbf{0} & D_{12} \\ C_2 & D_{21} & D_{22} \end{bmatrix}, \qquad \hat{K}(s) = \begin{bmatrix} A_K & B_K \\ \hline C_K & D_K \end{bmatrix}.$$

K(s) is essentially full-state feedback with \mathcal{H}_2 estimator.





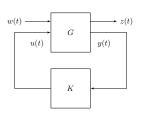
Let

$$\hat{G}(s) = \begin{bmatrix} A & B_1 & B_2 \\ \hline C_1 & D_{11} & D_{12} \\ C_2 & D_{21} & D_{22} \end{bmatrix}, \qquad \hat{K}(s) = \begin{bmatrix} A_K & B_K \\ \hline C_K & D_K \end{bmatrix}.$$

Find K(s) that minimizes $\|\hat{G}_{w\to z}\|_{\infty}$.



Simpler case with $D_{22} = 0$



System

$$\hat{G}(s) = \begin{bmatrix} A & B_1 & B_2 \\ \hline C_1 & D_{11} & D_{12} \\ C_2 & D_{21} & \mathbf{0} \end{bmatrix},$$

$$\hat{K}(s) = \begin{bmatrix} A_K & B_K \\ \hline C_K & D_K \end{bmatrix}.$$

Closed-loop transfer function is

$$\begin{split} \mathcal{F}_l(\hat{G}, \hat{K}) &= \begin{bmatrix} A_{\mathsf{cl}} & B_{\mathsf{cl}} \\ C_{\mathsf{cl}} & D_{\mathsf{cl}} \end{bmatrix}, \\ &= \begin{bmatrix} A + B_2 D_K C_2 & B_2 C_K & B_1 + B_2 D_K D_{21} \\ B_K C_2 & A_K & B_K D_{21} \\ \hline C_1 + D_{12} D_K C_2 & D_{12} C_K & D_{11} + D_{12} D_K D_{21} \end{bmatrix}. \end{split}$$

Simpler case with $D_{22} = 0$ (contd.)

Define matrices

$$J = \begin{bmatrix} A_K & B_K \\ C_K & D_K \end{bmatrix},$$

and

$$\bar{A} = \begin{bmatrix} A & 0 \\ 0 & 0 \end{bmatrix}, \qquad \qquad \bar{B} = \begin{bmatrix} B_1 \\ 0 \end{bmatrix},
\bar{C} = \begin{bmatrix} C_1 & 0 \end{bmatrix}, \qquad \qquad \underline{C} = \begin{bmatrix} 0 & I \\ C_2 & 0 \end{bmatrix},
\underline{B} = \begin{bmatrix} 0 & B_2 \\ I & 0 \end{bmatrix}, \qquad \qquad \underline{D}_{12} = \begin{bmatrix} 0 & D_{12} \end{bmatrix},
\underline{D}_{21} = \begin{bmatrix} 0 \\ D_{21} \end{bmatrix}.$$

These will be useful in reconstructing controller from LMI solution.



Simpler case with $D_{22} = 0$ (contd.)

Therefore

$$A_{cl} = \bar{A} + \underline{B}J\underline{C},$$

$$C_{cl} = \bar{C} + D_{12}JC,$$

$$B_{cl} = \bar{B} + \underline{B}J\underline{D}_{21}$$

$$D_{cl} = D_{11} + \underline{D}_{12}J\underline{D}_{21}.$$

Simpler case with $D_{22} = 0$ (contd.)

Theorem $A_{\rm cl}$ is Hurwitz and $\|\mathcal{F}_l(\hat{G},\hat{K})\|_{\infty} < \gamma$, iff there exists symmetric matrices X>0 and Y>0 such that

$$\begin{bmatrix} N_{o} & 0 \\ 0 & I \end{bmatrix}^{*} \begin{bmatrix} A^{*}X + XA & XB_{1} & C_{1}^{*} \\ B_{1}^{*}X & -\gamma I & D_{11}^{*} \\ C_{1} & D_{11} & -\gamma I \end{bmatrix} \begin{bmatrix} N_{o} & 0 \\ 0 & I \end{bmatrix} < 0,$$

$$\begin{bmatrix} N_{c} & 0 \\ 0 & I \end{bmatrix}^{*} \begin{bmatrix} A^{*}Y + YA & YC_{1} & B_{1}^{*} \\ C_{1}^{*}Y & -\gamma I & D_{11}^{*} \\ B_{1} & D_{11} & -\gamma I \end{bmatrix} \begin{bmatrix} N_{c} & 0 \\ 0 & I \end{bmatrix} < 0,$$

$$\begin{bmatrix} X & I \\ I & Y \end{bmatrix} \ge 0,$$

where N_o and N_c are full rank matrices satisfying

$$\operatorname{Im} N_o = \operatorname{Ker} \begin{bmatrix} C_2 & D_{21} \end{bmatrix}, \text{ and } \operatorname{Im} N_c = \operatorname{Ker} \begin{bmatrix} B_2^* & D_{12}^* \end{bmatrix}.$$

Simpler case with $D_{22} = 0$ (contd.)

Proof: See A Linear Matrix Inequality Approach to \mathcal{H}_{∞} Control – Pascal Gahinet, Pierre Apkarian, 1994.

Main Ingredients:

- KYP Lemma
- Projection Lemmas

\mathcal{H}_{∞} Controller Reconstruction

Suppose we have solved the LMIs and have obtained X,Y. Define X_{cl} as

$$X_{\mathsf{cl}} = \begin{bmatrix} X & X_2^* \\ X_2 & I \end{bmatrix},$$

such that

$$X - Y^{-1} = X_2 X_2^*.$$

The LMI in the synthesis enforces

$$\begin{bmatrix} X & I \\ I & Y \end{bmatrix} \ge 0$$

implies

$$X - Y^{-1} \ge 0.$$

Therefore, we can set

$$X_2 := \sqrt{X - Y^{-1}}$$
. symmetric

\mathcal{H}_{∞} Controller Reconstruction

contd.

With X_2 determined, X_{cl} is defined.

Define matrices,

$$\begin{split} P_{X_{\text{cl}}} &= \begin{bmatrix} \underline{B}^* & 0 & \underline{D}_{12}^* \end{bmatrix}, \; Q = \begin{bmatrix} \underline{C} & \underline{D}_{21} & 0 \end{bmatrix}, \\ H_{X_{\text{cl}}} &= \begin{bmatrix} \bar{A}^* X_{\text{cl}} + X_{\text{cl}} \bar{A} & X_{\text{cl}} \bar{B} & \bar{C}^* \\ \bar{B}^* X_{\text{cl}} & -\gamma I & D_{11}^* \\ \bar{C} & D_{11} & -\gamma I \end{bmatrix}. \end{split}$$

Controller matrix J can be obtained using reciprocal projection lemma (see Gahinet, Apkarian 1994)

$$H_{X_{cl}} + Q^*J^*P_{X_{cl}} + P_{X_{cl}}JQ < 0.$$

- Many solutions for *J* exists!
- A family of γ optimal \mathcal{H}_{∞} controllers exists.
- Formulation is LMI feasibility



Few Comments about \mathcal{H}_{∞}

- \blacksquare We do not seek optimal γ as the computations become singular instead we seek suboptimal γ
- lacktriangle Bisection algorithm is used to reduced γ and LMIs are solved
- Issue with controller-plant pole-zero cancellation
- Poles in $j\omega$ axis

LMI framework provides a flexibility to address/circumvent these issues

(see Gahinet, Apkarian 1994)

Application of \mathcal{H}_{∞} Controller

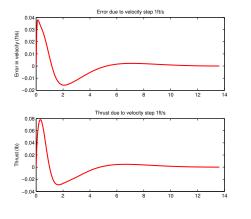
 (V,γ) Tracking Controller for Longitudinal F16 Model

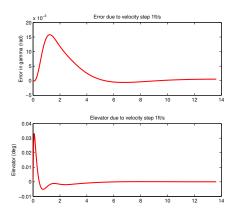
```
clc: clear:
% Define F16 Model
% =========
load f16LongiLinear.mat
wd = 1; % Scaling to adjust alpha disturbance
A = f16ss.a:
Bu = f16ss.b;
Bd = [0; wd; 0; 0];
B = [Bu Bd1:
Cy = [1 0 0 0; % Velocity
     0 -1 1 01; % gamma
[ns,nul = size(B);
F16 = ss(A,B,Cy,zeros(2,nu));
% Define Weights
§ =========
s = tf('s'):
Wr = blkdiag(1/(s/1+1), 1/(s/5+1));
Wu = blkdiag(1/5000, 1/25);
We = blkdiag(1, 1):
Wd = 0.1/(s/.1+1):
Wn = 0.01*blkdiag(1,1);
Wm = blkdiag(1, 1);
```

```
% System Interconnection
  _____
r = icsignal(2);
d = icsignal(1):
n = icsignal(2);
u = icsignal(2);
v = F16*[u:Wd*d1:
e = (Wr*r - y);
G = iconnect;
G.input = [r;d;n;u];
G.output = [We*e;Wu*u;Wr*r-y-Wn*n];
[K,F16cl,gam,info] = hinfsyn(G.System,2,2,...
                            'method','lmi'):
disp(sprintf('Minimum gamma = %f',gam));
```

Application of \mathcal{H}_{∞} Controller

 (V, γ) Tracking Controller for Longitudinal F16 Model





 $\gamma^* = 0.971881$