

工程电磁场

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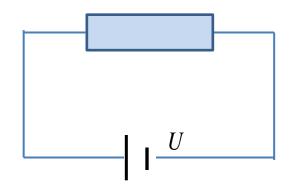


3.1 恒定电场基本方程与场的特性

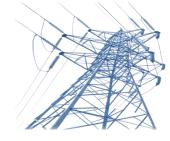
恒定电场: 与恒定电流相伴随的电场,该电场不随时间变化。

分析: 导体两端施加电压U,导体中形成电场,驱使其中的自由电子持续定向运动,呈现直流即恒定电流,此时导体中 $E\neq 0$ 。

静电场与恒定电场的差异与联系:



- (1) 为何静电场中电荷静止而恒定电场中电荷持续移动形成电流?
- (2) 导体特征有何差异?
- (3) 场的特征的差异?



3.1.1 恒定电场基本方程:无散、无旋

电荷守恒:
$$\oint_{S} \boldsymbol{J}_{c} \cdot d\boldsymbol{S} = -\frac{\partial q}{\partial t} = -\frac{\partial}{\partial t} \int_{V} \rho dV = -\int_{V} \frac{\partial \rho}{\partial t} dV$$

分析: 导体当中 ρ 为常数,不随时间变化,故右端为零,即

$$\oint_{c} \boldsymbol{J}_{c} \cdot d\boldsymbol{S} = 0 \quad \Longrightarrow \quad \nabla \cdot \boldsymbol{J}_{c} = 0 \quad \Xi \mathbf{B} \mathbf{E}$$

另一方面,恒定电场可看作是电源极板上驻定电荷引起的静态电场,

$$\oint_{\mathbf{r}} \mathbf{E} \cdot d\mathbf{l} = 0 \qquad \Rightarrow \qquad \nabla \times \mathbf{E} = 0 \qquad \mathbf{E} \mathbf{E} \mathbf{E}$$

媒质构成方程: $J_c = \gamma E$



3.1.1 恒定电场基本方程:无散、无旋

由无旋性**:** $\nabla \times \mathbf{E} = 0$



$$E = -\nabla \varphi$$ 类似于静电场可引入标量电位

$$U_{PQ} = \int_{P}^{Q} \mathbf{E} \cdot d\mathbf{l} \qquad \varphi_{P} = \int_{P}^{\infty} \mathbf{E} \cdot d\mathbf{l}$$

$$\varphi_P = \int_P^\infty \boldsymbol{E} \cdot d\boldsymbol{l}$$

$$abla \cdot oldsymbol{J}_c = 0$$
 $oldsymbol{E} = -\nabla \varphi$
 $abla c = \gamma E$
 $abla c = 0$
 $abla c = 0$
可基于边值问题求恒定电场



(t+dt)

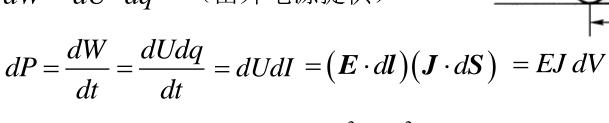
3.1.2 电功率 电动势

导体电流热效应: 电荷运动,与晶格相碰撞,产生热,此部分的能量 由电源提供,具体是电源通过电场力作功输送电子,

供热能消耗。

电功率: 取一元电流管,设电场作用下, dt时间内,电荷dq由导体左端面 移动到右端面,电场力作功为

$$dW = dU \cdot dq$$
 (由外电源提供)





3.1.2 电功率 电动势

$$p = E \cdot J$$

电功率体密度

电动势: (<u>与感应电动势完全不同的概念</u>)

<u>电池</u>:通过化学作用,使得溶液中的正负电荷分开,并分别趋向于正负 <u>电极</u>,维持板间电压,从而建立恒定电场,本质上将化学能转为电能。

定义: 电源中将正负电荷分开的力为局外力 $F_{\rm e}$, 进而引入局外场强

$$\boldsymbol{E}_{e} = \boldsymbol{F}_{e} / q$$

等效场强

为了衡量电源将其他能量转化为电能的能力,

定义:

$$e = \int_{e}^{+} E_{e} \cdot dl$$

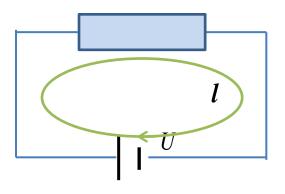
积分在电源内部由负极到正极



3.1.2 电功率 电动势

注意: 电源内部也有库仑电场

思考题:沿闭合路径1作电场的积分,结果?





3.1.3 不同媒质分界面的边界条件

(1) 两种不同导电媒质

由

$$\oint_{I} \mathbf{E} \cdot d\mathbf{l} = 0$$



$$E_{1t} = E_{2t}$$

$$\boldsymbol{e}_{n} \times (\boldsymbol{E}_{2} - \boldsymbol{E}_{1}) = 0$$

$$\oint_{S} \boldsymbol{J}_{c} \cdot d\boldsymbol{S} = 0$$



$$\boldsymbol{J}_{2n} = \boldsymbol{J}_{1n}$$

$$\boldsymbol{e}_n \cdot (\boldsymbol{J}_2 - \boldsymbol{J}_1) = 0$$

$$E_1 \sin \alpha_1 = E_2 \sin \alpha_2$$

$$\gamma_1 E_1 \cos \alpha_1 = \gamma_2 E_2 \cos \alpha_2$$



$$\frac{\tan \alpha_1}{\tan \alpha_2} = \frac{\gamma_1}{\gamma_2}$$

折射定理



3.1.3 不同媒质分界面的边界条件

(2) 良导体和不良导体 $\gamma_1 \gg \gamma_2$

$$\pm \frac{\tan \alpha_1}{\tan \alpha_2} = \frac{\gamma_1}{\gamma_2} \rightarrow \infty$$



$$\alpha_2 \approx 0 \implies$$
 电流垂直于交界面,流入不良导体

由于
$$E_{1t} = E_{2t} \approx 0$$

例:
$$\gamma_{steel} = 5 \times 10^6 \text{S/m}$$
 $\gamma_{soil} = 1 \times 10^{-2} \text{S/m}$

$$\alpha_1 = 89^{\circ}59'50''$$
 $\alpha_2 = 8''$ $J_{2t} = \gamma_2 E_{2t} \approx 0$



$$J_{2t} = \gamma_2 E_{2t} \approx 0$$







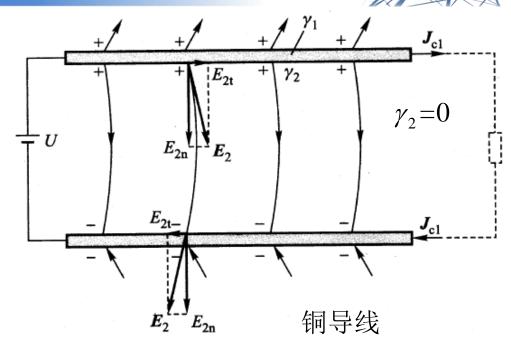
3.1.3 不同媒质分界面的边界条件

(3) 导体和理想介质 $\gamma_1 \gg \gamma_2 = 0$

$$\gamma_2 = 0$$
 $J_2 = 0$

$$E_{1t} = E_{2t} J_{1n} = J_{2n}$$

$$J_{2n} = 0 = J_{1n}$$



媒质1:
$$J_{1n} = 0$$
 \longrightarrow $E_{1n} = 0$ \longrightarrow $J_1 = J_{1t}$ $E_{1t} = J_1 / \gamma_1 = 0.086 \, \text{V} / \text{m}$

媒质2:
$$J_{2n} = 0$$
 \longrightarrow $E_{2n} = J_{2n} / \gamma_2$? $U = \int_{+}^{-} E_{2n} \cdot dl$ $E_{2n} = 3 \times 10^6 \, \text{V/m}$



导体近似为等位体







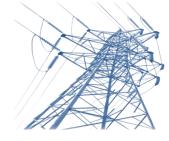
3.1.3 不同媒质分界面的边界条件

(4) 两种有损电介质

有损: 介质不是理想的,有导体的性质,可以导电

可解得,
$$\sigma = \frac{\varepsilon_2 \gamma_1 - \varepsilon_1 \gamma_2}{\gamma_1 \gamma_2} J_{2n}$$

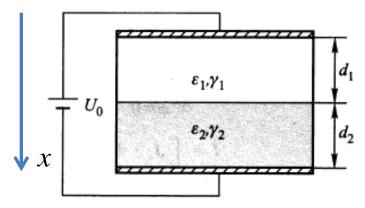
可知, 当
$$\varepsilon_2 \gamma_1 = \varepsilon_1 \gamma_2 \sim \frac{\varepsilon_1}{\varepsilon_2} = \frac{\gamma_1}{\gamma_2}$$
 $\sigma = 0$



3.1.3 不同媒质分界面的边界条件

例3-2: 两层非理想介质(有损电介质)构成的平板电容器,如图所示,介电常数和电导率已知,外施电压为 U_0 ,求:

- (1) 两层非理想介质中的电场强度;
- (2) 单位体积中的电场能量及功率 损耗;
- (3) 两层介质分界面上的自由电荷面密度。



$$J_{1n} = J_{2n}$$
 $J_1 = J_{1n} = J_{2n} = J_2$ $\gamma_1 E_1 = \gamma_2 E_2$



3.1.3 不同媒质分界面的边界条件

可解得
$$\boldsymbol{E}_{1} = \frac{\gamma_{2}U_{0}}{\gamma_{1}d_{2} + \gamma_{2}d_{1}}\boldsymbol{e}_{x}$$
 $\boldsymbol{E}_{2} = \frac{\gamma_{1}U_{0}}{\gamma_{1}d_{2} + \gamma_{2}d_{1}}\boldsymbol{e}_{x}$

$$(2)$$

$$w_{e1} = \frac{1}{2}\boldsymbol{D}_{1} \cdot \boldsymbol{E}_{1} = \frac{1}{2}\varepsilon_{1}E_{1}^{2} \quad w_{e2} = \frac{1}{2}\boldsymbol{D}_{2} \cdot \boldsymbol{E}_{2} = \frac{1}{2}\varepsilon_{2}E_{2}^{2}$$

$$p_{1} = \boldsymbol{J}_{1} \cdot \boldsymbol{E}_{1} = \gamma_{1}E_{1}^{2} \qquad p_{2} = \boldsymbol{J}_{2} \cdot \boldsymbol{E}_{2} = \gamma_{2}E_{2}^{2}$$

(3) 分界面自由电荷面密度

$$\sigma = \frac{\varepsilon_2 \gamma_1 - \varepsilon_1 \gamma_2}{\gamma_1 \gamma_2} J_{2n} = \frac{\varepsilon_2 \gamma_1 - \varepsilon_1 \gamma_2}{\gamma_1 \gamma_2} J_2 = \frac{\varepsilon_2 \gamma_1 - \varepsilon_1 \gamma_2}{\gamma_1 \gamma_2} \gamma_2 \frac{\gamma_1 U_0}{\gamma_1 d_2 + \gamma_2 d_1} = \frac{\varepsilon_2 \gamma_1 - \varepsilon_1 \gamma_2}{\gamma_1 d_2 + \gamma_2 d_1} U_0$$



- 3.2 恒定电场与静电场的比拟 接地系统
- 3.2.1 静电比拟

	$\nabla \cdot \boldsymbol{J}_c = 0$	
均 匀	$\nabla \times \boldsymbol{E} = 0$	
导电	$E = -\nabla \varphi$	
媒	$oldsymbol{J}_{c}=\gamma oldsymbol{E}$	
质 中	$\nabla^2 \varphi = 0$	
	$oldsymbol{I} = \int_S oldsymbol{J}_c \cdot doldsymbol{S}$	

$$\nabla \cdot \mathbf{D} = 0 \ (\rho = 0)$$

$$\nabla \times \mathbf{E} = 0$$

$$\mathbf{E} = -\nabla \varphi$$

$$\mathbf{D} = \varepsilon \mathbf{E}$$

$$\nabla^2 \varphi = 0$$

$$\psi(q) = \int_{S} \mathbf{D} \cdot d\mathbf{S}$$

均匀电介质中

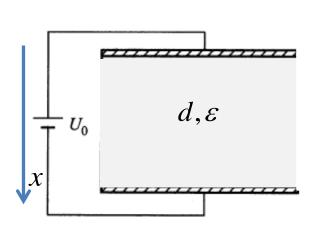


- (1) 两种场均可基于边值问题(BVP) 求解和分析
- (2) 由唯一性定理,当边界条件相同时, φ 同,E同,J,D分布规律一致

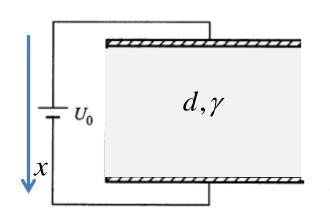


3.2.1 静电比拟

单一均匀电介质:
$$\text{BVP:} \quad \left\{ \begin{array}{l} \nabla^2 \varphi = 0 \\ \varphi\big|_{x=0} = U_0 \\ \varphi\big|_{x=d} = 0 \end{array} \right.$$



单一均匀导电媒质: BVP:
$$\left\{ \begin{array}{l} \nabla^2 \varphi = 0 \\ \varphi\big|_{x=0} = U_0 \\ \varphi\big|_{x=d} = 0 \end{array} \right.$$

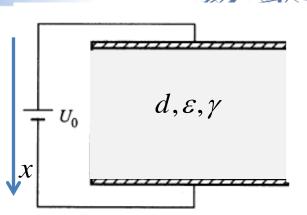


 \longrightarrow 由唯一性定理,arphi同, $oldsymbol{I}$, $oldsymbol{D}$ 分布相似



3.2.1 静电比拟

a.单一媒质(极化+导电):
$$\left\{ \begin{array}{l} \nabla^2\varphi=0 \\ \varphi\big|_{x=0}=U_0 \\ \varphi\big|_{x=d}=0 \end{array} \right.$$

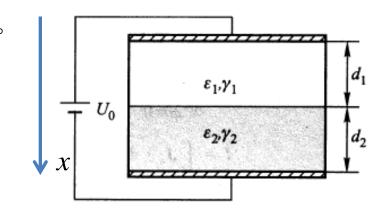


解出 φ ,得到E,再得到J,D,二者分布相似。

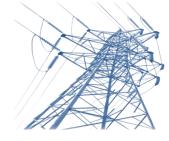
b.非单一媒质(分块均匀):

$$\frac{\tan \alpha_1}{\tan \alpha_2} = \frac{\varepsilon_1}{\varepsilon_2}$$
 静电场

$$\frac{\tan \alpha_1'}{\tan \alpha_2'} = \frac{\gamma_1}{\gamma_2}$$
 恒定电场



$$\frac{\varepsilon_1}{\varepsilon_2} = \frac{\gamma_1}{\gamma_2}$$
 」))) 力 布相似



3.2.1 静电比拟

静电比拟: 基于场分布的相似性,可将一种场的计算和实验结果(**场量**, **参数**等),推广应用于另一种场,将这种方法称之为静电比拟。

电容:
$$C = \frac{q}{U} = \frac{\int_{s} \mathbf{D} \cdot d\mathbf{S}}{\int_{l} \mathbf{E} \cdot d\mathbf{l}} = \frac{\varepsilon \int_{s} \mathbf{E} \cdot d\mathbf{S}}{\int_{l} \mathbf{E} \cdot d\mathbf{l}}$$

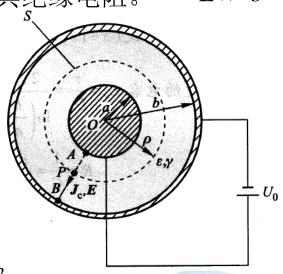
中导: $G = \frac{I}{U} = \frac{\int_{s} \mathbf{J}_{c} \cdot d\mathbf{S}}{\int_{l} \mathbf{E} \cdot d\mathbf{l}} = \frac{\gamma \int_{s} \mathbf{E} \cdot d\mathbf{S}}{\int_{l} \mathbf{E} \cdot d\mathbf{l}}$

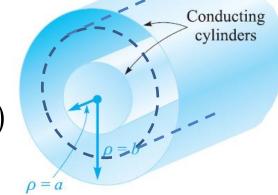
例3-3: 内外导体半径分别为a,b的同轴电缆,外施电压U0,试求因绝缘介质老化(不完善)而引起的电缆内泄漏电流密度及其绝缘电阻。 $L\gg b$

解1: 取长度为l的一段进行分析,由对称性可知,E,J都沿 e_ρ 方向,设总电流为I,建立圆柱坐标系分析,作半径为 ρ ,长度为l的圆柱面S,则有

由已知
$$U_0 = \int_a^b \mathbf{E} \cdot d\mathbf{\rho} = \int_a^b \frac{I}{\gamma 2\pi \rho l} d\rho = \gamma 2\pi l \ln \frac{b}{a}$$

$$I = \frac{U_0 \gamma 2\pi l}{\ln(b/a)} \longrightarrow J_c = \frac{U_0 \gamma}{\rho \ln(b/a)} e_{\rho} \quad (a < \rho < b)$$





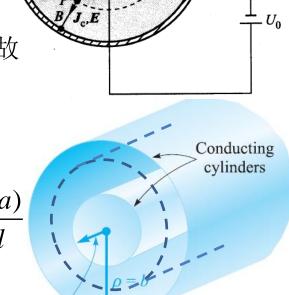


例3-3: 内外导体半径分别为a,b的同轴电缆,外施电压U0,试求因绝缘介质老化(不完善)而引起的电缆内泄漏电流密度及其绝缘电阻。 $L\gg b$

$$R = \frac{U_0}{I} = \frac{\ln(b/a)}{\gamma 2\pi l}$$

解2: 由高斯定理可求得,静电场中 $E = \frac{U_0}{\rho \ln(b/a)} e_{\rho}$

由静电比拟可知,对于恒定电场中E与此相同,故





3.2.2 接地电阻

接地: 将金属导体埋入地内,与系统中需要接地的部分相连,此接地导体称之为接地器。

接地作用: a 保障人身和设备安全; b 为系统提供零电位参考点。

接地电阻: 电流流经大地遇到的电阻;

- a. 接地器本身的电阻;
- b. 接地导线电阻;
- c. 接地器与大地间的接触电阻;
- d. 接地器间的土壤电阻; 最主要部分

3.2.2 接地电阻

深埋地下的球形接地器接地电阻:

由静电场可知,带电导体球的电容为,

$$C = \frac{q}{U} = q / (\varphi_a - \varphi_\infty) = q / (q / 4\pi\varepsilon a) = 4\pi\varepsilon a$$

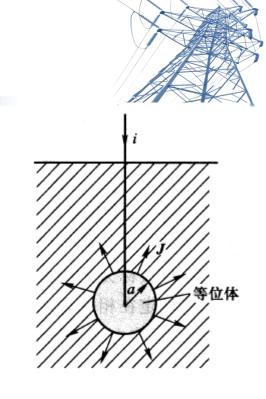
由静电比拟可得, $G = C\gamma / \varepsilon = 4\pi\gamma a$

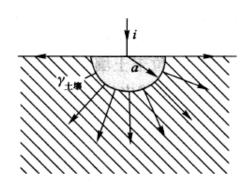


$$R=1/G=1/(4\pi\gamma a)$$

埋于地下的半球形接地器接地电阻:

空间中既有土壤,也有空气,介质不均匀,可采用镜像法







3.2.2 接地电阻

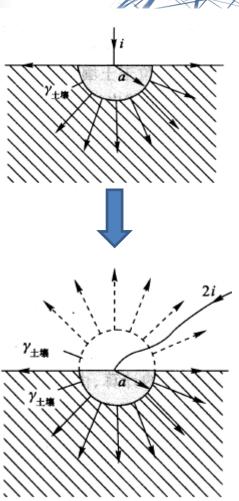
埋于地下的半球形接地器接地电阻:

$$\boldsymbol{J}_c = \frac{2i}{4\pi r^2} \boldsymbol{e}_r \quad \Longrightarrow \quad \boldsymbol{E} = \frac{2i}{4\pi r^2 \gamma_S} \boldsymbol{e}_r$$

$$C = \frac{q}{U} = q / (\varphi_a - \varphi_\infty)$$

$$\varphi_a = \int_a^\infty \mathbf{E} \cdot d\mathbf{r} = \frac{i}{2\pi\gamma_s a}$$

$$R = U / I = \varphi_a / i = \frac{1}{2\pi\gamma_s a}$$





3.2.3 跨步电压

人体所能承受的安全临界电压: $U_0=50\sim70\text{V}$ 求人体的跨步电压 U_{AB} 和安全距离 r_0

$$\boldsymbol{J}_c = \frac{I}{2\pi r^2} \boldsymbol{e}_r \quad \Longrightarrow \quad \boldsymbol{E} = \frac{I}{2\pi r^2 \gamma_S} \boldsymbol{e}_r$$

$$U_{AB} = \int_{A}^{B} \mathbf{E} \cdot d\mathbf{r} = \int_{r-b}^{r} \frac{I}{2\pi r^{2} \gamma_{s}} dr$$

$$=\frac{I}{2\pi\gamma_{S}}\left(\frac{1}{r-b}-\frac{1}{r}\right) = \frac{I}{2\pi\gamma_{S}}\left[\frac{r-r+b}{r(r-b)}\right] \approx \frac{Ib}{2\pi r^{2}\gamma_{S}} < U_{0} \implies r > \sqrt{\frac{Ib}{2\pi U_{0}\gamma_{S}}} = r_{0}$$

若已知
$$R = \frac{1}{2\pi\gamma_s a}$$
 $r_0 = \sqrt{\frac{abIR}{U_0}}$ 若要减小危险区域面积怎么办?

(I,R)







3.3 恒定磁场

3.3.1 基本方程

积分方程

微分方程

全电流定律:

$$\oint_{l} \boldsymbol{H} \cdot d\boldsymbol{l} = \int_{S} \left(\boldsymbol{J} + \frac{\partial \boldsymbol{D}}{\partial t} \right) \cdot d\boldsymbol{S}$$

$$\nabla \times \boldsymbol{H} = \boldsymbol{J} + \frac{\partial \boldsymbol{D}}{\partial t}$$

$$\nabla \times \boldsymbol{E} = -\frac{\partial \boldsymbol{B}}{\partial t}$$

电磁感应定律:

$$\oint_{l} \mathbf{E} \cdot d\mathbf{l} = -\int_{s}^{l} \frac{\partial \mathbf{B}}{\partial t} d\mathbf{S}$$

$$\nabla \times \boldsymbol{E} = -\frac{\partial \boldsymbol{B}}{\partial t}$$

磁通连续性:

$$\oint_{S} \mathbf{B} \cdot d\mathbf{S} = 0$$

$$\nabla \cdot \boldsymbol{B} = 0$$

高斯定理:

$$\oint_{S} \mathbf{D} \cdot d\mathbf{S} = \int_{V} \rho dV$$

$$\nabla \cdot \boldsymbol{D} = \rho$$

静态:与时间无关

磁场: 与电场无关



3.3.1 基本方程

积分方程

微分方程

安培环路定律:

$$\oint_{I} \boldsymbol{H} \cdot d\boldsymbol{l} = \int_{S} \boldsymbol{J} \cdot d\boldsymbol{S}$$

$$\nabla \times \boldsymbol{H} = \boldsymbol{J}$$

有旋

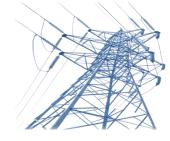
磁通连续性原理:

$$\oint_{S} \mathbf{B} \cdot d\mathbf{S} = 0$$

$$\nabla \cdot \boldsymbol{B} = 0$$

本构关系:

$$B = \mu H$$



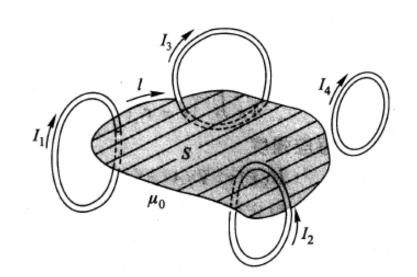
3.3.2 真空中的安培环路定律 (有旋)

在真空中, $\mathbf{B} = \mu_0 \mathbf{H}$ 代入前式中,

$$\oint_{l} \frac{\boldsymbol{B}}{\mu_{0}} \cdot d\boldsymbol{l} = \int_{S} \boldsymbol{J}_{c} \cdot d\boldsymbol{S} \qquad \Longrightarrow \quad \oint_{l} \boldsymbol{B} \cdot d\boldsymbol{l} = \mu_{0} \int_{S} \boldsymbol{J}_{c} \cdot d\boldsymbol{S} = \mu_{0} \sum I_{i}$$

微分形式: $\nabla \times \boldsymbol{B} = \mu_0 \boldsymbol{J}_c$

$$\oint_{I} \mathbf{B} \cdot d\mathbf{l} = \mu_0 \left(I_1 + I_2 - I_3 \right)$$

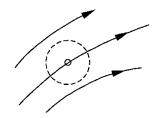




3.3.3 磁通连续性原理 恒定磁场的无散性

$$\oint_{S} \mathbf{B} \cdot d\mathbf{S} = 0$$

$$\nabla \cdot \boldsymbol{B} = 0$$



$$\nabla \cdot \boldsymbol{B} = 0, \quad \rho = 0$$



3.3.4 毕奥萨伐尔定律

赫姆霍兹定理: $B(r) = -\nabla \varphi(r) + \nabla \times A(r)$

$$\varphi(\mathbf{r}) = \frac{1}{4\pi} \int_{V'} \frac{\nabla' \cdot \mathbf{B}(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} dV'$$

$$A(r) = \frac{1}{4\pi} \int_{V'} \frac{\nabla' \times B(r')}{|r - r'|} dV'$$

曲
$$\nabla \times \mathbf{B} = \mu_0 \mathbf{J}_c$$
 \Longrightarrow $\mathbf{A}(\mathbf{r}) = \frac{\mu_0}{4\pi} \int_{V'} \frac{\mathbf{J}_c(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} dV'$ \Longrightarrow $\mathbf{A} = \mathbf{J}$ 的方向一致



3.3.4 毕奥萨伐尔定律

由此可得到

$$B(r) = \nabla \times A(r)$$

$$\boldsymbol{A}(\boldsymbol{r}) = \frac{\mu_0}{4\pi} \int_{V'} \frac{\boldsymbol{J}_c(\boldsymbol{r}')}{|\boldsymbol{r} - \boldsymbol{r}'|} dV'$$

$$\boldsymbol{B}(\boldsymbol{r}) = \nabla \times \left| \frac{\mu_0}{4\pi} \int_{V'} \frac{\boldsymbol{J}_c(\boldsymbol{r}')}{|\boldsymbol{r} - \boldsymbol{r}'|} dV' \right| = \frac{\mu_0}{4\pi} \int_{V'} \nabla \times \left| \frac{\boldsymbol{J}_c(\boldsymbol{r}')}{|\boldsymbol{r} - \boldsymbol{r}'|} \right| dV'$$

由矢量恒等式,
$$\nabla \times \frac{\boldsymbol{J}_{c}(\boldsymbol{r}')}{R} = \nabla \left(\frac{1}{R}\right) \times \boldsymbol{J}_{c}(\boldsymbol{r}') + \frac{1}{R} \nabla \times \boldsymbol{J}_{c}(\boldsymbol{r}')$$

$$= \nabla \left(\frac{1}{R}\right) \times \boldsymbol{J}_{c}\left(\boldsymbol{r}'\right) = -\frac{\boldsymbol{e}_{R}}{R^{2}} \times \boldsymbol{J}_{c}\left(\boldsymbol{r}'\right) = \boldsymbol{J}_{c}\left(\boldsymbol{r}'\right) \times \frac{\boldsymbol{e}_{R}}{R^{2}}$$

$$\boldsymbol{B}(\boldsymbol{r}) = \frac{\mu_0}{4\pi} \int_{V'} \frac{\boldsymbol{J}_c(\boldsymbol{r}') \times \boldsymbol{e}_R}{R^2} dV' = \frac{\mu_0}{4\pi} \int_{V'} \frac{\boldsymbol{J}_c(\boldsymbol{r}') \times (\boldsymbol{R} / R)}{R^2} dV'$$



3.3.4 毕奥萨伐尔定律

$$= \frac{\mu_0}{4\pi} \int_{V'} \frac{\boldsymbol{J}_c(\boldsymbol{r}') \times \boldsymbol{R}}{R^3} dV' = \frac{\mu_0}{4\pi} \int_{V'} \frac{\boldsymbol{J}_c(\boldsymbol{r}') \times (\boldsymbol{r} - \boldsymbol{r}')}{|\boldsymbol{r} - \boldsymbol{r}'|^3} dV'$$
$$= \frac{\mu_0}{4\pi} \int_{V'} \frac{\boldsymbol{J}_c(\boldsymbol{r}') \times \boldsymbol{e}_R}{\boldsymbol{P}^2} dV'$$

$$B(r) = \frac{\mu_0}{4\pi} \int_{V'} \frac{J_c(r') \times e_R}{R^2} dV'$$

$$= \frac{\mu_0}{4\pi} \int_{S'} \frac{K_c(r') \times e_R}{R^2} dS' \qquad A(r) = \frac{\mu_0}{4\pi} \int_{S'} \frac{K_c(r')}{R} dV'$$

$$= \frac{\mu_0}{4\pi} \int_{I'} \frac{Idl' \times e_R}{R^2} dS' \qquad A(r) = \frac{\mu_0}{4\pi} \int_{I'} \frac{I}{R} dl'$$



3.4 自由空间的磁场

3.4.1 基于场量B的分析

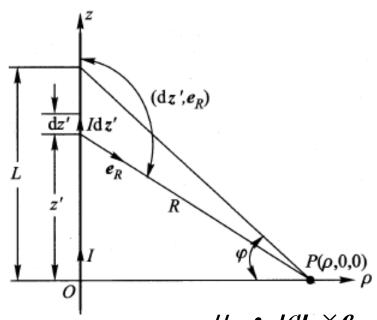
例3-4: 计算真空中有限长(L)直载流导线 产生的磁感应强度。

取元电流 Idl' = Idz' 其在P点处产生的场

$$d\mathbf{B} = \frac{\mu_0}{4\pi} \frac{Id\mathbf{z}' \times \mathbf{e}_R}{R^2} = \frac{\mu_0 I}{4\pi} \frac{d\mathbf{z}' \times \mathbf{e}_R}{\rho^2 + {z'}^2}$$

$$= \frac{\mu_0 I}{4\pi} \frac{dz'}{\rho^2 + z'^2} \boldsymbol{e}_z \times \boldsymbol{e}_R = \frac{\mu_0 I}{4\pi} \frac{dz'}{\rho^2 + z'^2} \sin(\boldsymbol{e}_z, \boldsymbol{e}_R) \boldsymbol{e}_\phi$$

$$= \frac{\mu_0 I}{4\pi} \frac{dz'}{\rho^2 + z'^2} \frac{\rho}{\sqrt{\rho^2 + z'^2}} e_{\phi} = \frac{\mu_0 I}{4\pi} \frac{\rho dz'}{(\rho^2 + z'^2)^{3/2}} e_{\phi}$$



$$\boldsymbol{B}(\boldsymbol{r}) = \frac{\mu_0}{4\pi} \int_{l'} \frac{I d\boldsymbol{l} \times \boldsymbol{e}_R}{R^2}$$



3.4.1 基于场量B的分析

$$\mathbf{B} = \int_{l} d\mathbf{B} = \frac{\mu_{0}I}{4\pi} \int_{l} \frac{\rho}{\left(\rho^{2} + z'^{2}\right)^{3/2}} dz' \mathbf{e}_{\phi}$$

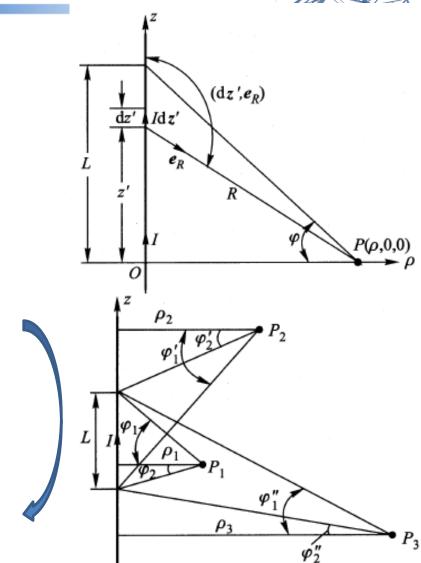
$$= \frac{\mu_{0}I}{4\pi} \frac{z'}{\sqrt{\rho^{2} + z'^{2}}} \Big|_{0}^{L} \mathbf{e}_{\phi} = \frac{\mu_{0}I}{4\pi} \sin \varphi \mathbf{e}_{\phi}$$

$$P_1 \stackrel{\rightleftharpoons}{\bowtie} : \qquad \boldsymbol{B}_{P1} = \frac{\mu_0 I}{4\pi \rho_1} \left(\sin \varphi_1 + \sin \varphi_2\right) \boldsymbol{e}_{\phi}$$

$$P_2$$
点:
$$\boldsymbol{B}_{P2} = \frac{\mu_0 I}{4\pi\rho_2} \left(\sin \varphi_1' - \sin \varphi_2'\right) \boldsymbol{e}_{\phi}$$

$$P_3$$
点:
$$\boldsymbol{B}_{P3} = \frac{\mu_0 I}{4\pi\rho_2} \left(\sin \varphi_1'' - \sin \varphi_2''\right) \boldsymbol{e}_{\phi}$$

当
$$L$$
趋于无穷大时 $\mathbf{B} = \frac{\mu_0 I}{2\pi o} \mathbf{e}_{\phi}$ 应用

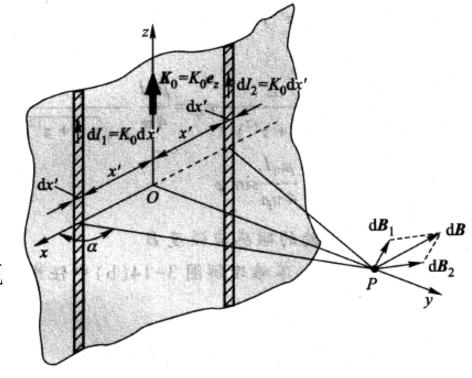


3.4.1 基于场量B的分析

例3-5: 真空中载有恒定面电流密度 K_0 的无限大导电片,在任意点P所产生的的磁感应强度B。

解1: 如图建立直角坐标系,电流沿z 方向,将面电流看作无数线电流

$$d\mathbf{B}_{1} = \frac{\mu_{0}(K_{0}dx')}{2\pi(x'^{2} + y^{2})^{1/2}} \mathbf{e}_{\phi}$$



$$e_{\phi} = -e_x \sin \phi + e_y \cos \phi = -e_x \sin \alpha + e_y \cos \alpha$$

对于P点磁场,在z轴两侧取对称的线电流,磁场只有x方向的分量,即有

3.4.1 基于场量*B*的分析

$$B = B_{x}e_{x} = -\int_{-\infty}^{+\infty} \frac{\mu_{0}K_{0} \sin \alpha}{2\pi(x'^{2} + y^{2})^{1/2}} dx'e_{x}$$

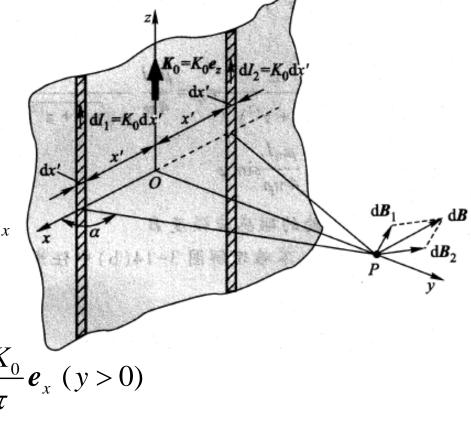
$$= -\int_{-\infty}^{+\infty} \frac{\mu_{0}K_{0}}{2\pi(x'^{2} + y^{2})^{1/2}} \frac{y}{(x'^{2} + y^{2})^{1/2}} dx'e_{x}$$

$$= -\frac{\mu_{0}K_{0}y}{2\pi} \int_{-\infty}^{+\infty} \frac{dx'}{2\pi(x'^{2} + y^{2})} e_{x}$$

$$= -\frac{\mu_{0}K_{0}}{2\pi} \arctan\left(\frac{x'}{y}\right)\Big|_{-\infty}^{+\infty} e_{x} = \begin{cases} -\frac{\mu_{0}K_{0}}{2\pi}e_{x} & (y < 0) \\ \frac{\mu_{0}K_{0}}{2\pi}e_{x} & (y < 0) \end{cases}$$

$$= -\frac{\mu_0 K_0 y}{2\pi} \int_{-\infty}^{+\infty} \frac{dx}{2\pi (x'^2 + y^2)} \boldsymbol{e}_x$$

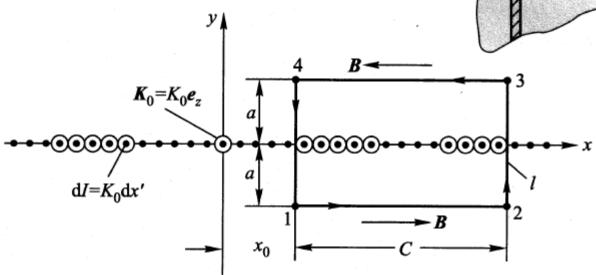
$$= -\frac{\mu_0 K_0}{2\pi} \arctan\left(\frac{x'}{y}\right)\Big|_{-\infty}^{+\infty} \boldsymbol{e}_x$$

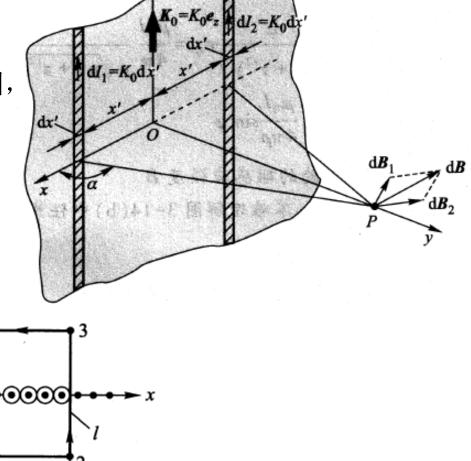


3.4.1 基于场量B的分析

解2: 安培环路定理进行求解,如下图,

- (1) 由前可知B的方向及对称性;
- (2) **B**的数值与x无关;
- (2) B为关于z轴的平行平面场;





恒定电流的电场和磁场 3. 静态电磁场



3.4.1 基于场量B的分析

取如图所示矩形回路,则有 解2:

$$=2B_{x}C = \mu_{0} \int_{x_{0}}^{x_{0}+C} dI = \mu_{0} \int_{x_{0}}^{x_{0}+C} K_{0} dx = \mu_{0} K_{0}C$$

 $\oint_{l} \mathbf{B} \cdot d\mathbf{l} = \int_{1}^{2} \mathbf{B}_{1} \cdot d\mathbf{l} + \int_{3}^{4} \mathbf{B}_{2} \cdot d\mathbf{l} = B_{1} \int_{1}^{2} dl + B_{2} \int_{3}^{4} dl$ $=2B_{1}C=2B_{r}C=\mu_{0}K_{0}C$



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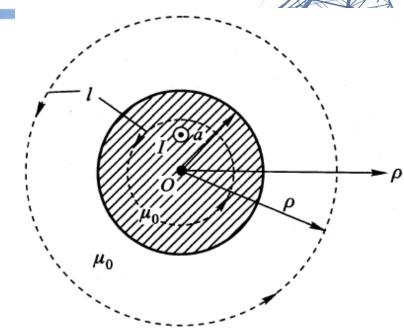
3.4.1 基于场量*B*的分析

例: 3-7 计算真空中半径为a,载流为I的 无限长圆柱形导体内外磁场。

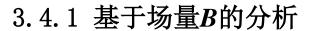
导体内: $(\rho < a)$

$$\oint_{l} \mathbf{B} \cdot d\mathbf{l} = \int_{l} B\mathbf{e}_{\phi} \cdot dl\mathbf{e}_{\phi} = B \int_{l} (\mathbf{e}_{\phi} \cdot \mathbf{e}_{\phi}) dl$$

$$=2\pi\rho B=\mu_0\frac{\pi\rho^2}{\pi a^2}I \implies B=\frac{\mu_0I\rho}{2\pi a^2}e_{\phi}$$



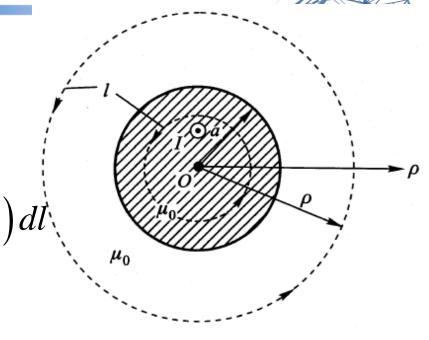
$$\boldsymbol{B} = \frac{\mu_0 I \rho}{2\pi a^2} \boldsymbol{e}_{\phi}$$



导体外:
$$(\rho > a)$$

$$\oint_{l} \mathbf{B} \cdot d\mathbf{l} = \int_{l} B\mathbf{e}_{\phi} \cdot dl\mathbf{e}_{\phi} = B \int_{l} (\mathbf{e}_{\phi} \cdot \mathbf{e}_{\phi}) d\dot{l}$$

$$=2\pi\rho B = \mu_0 I \implies B = \frac{\mu_0 I}{2\pi\rho} e_{\phi}$$



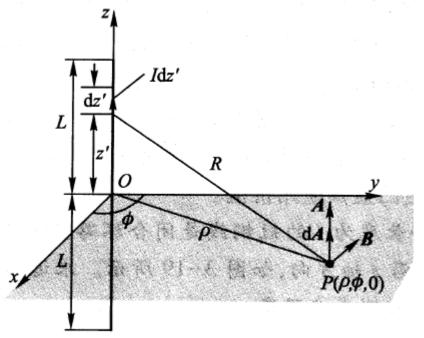


3.4.2 基于场量A的分析

$$A(r) = \frac{\mu_0}{4\pi} \int_{V'} \frac{J_c(r')}{R} dV'$$

$$= \frac{\mu_0}{4\pi} \int_{S'} \frac{K_c(r')}{R} dS'$$

$$= \frac{\mu_0}{4\pi} \int_{l'} \frac{I}{R} dl'$$



例3-9: 空气中长为2L的长直载流导线,在其中截面任意点处矢量磁位A,及B。



3.4.2 基于场量A的分析

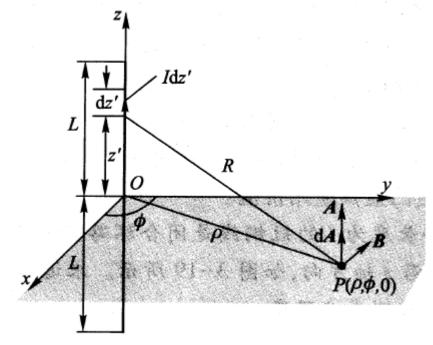
解: 建立直角坐标系,取元电流,可得

$$A(\mathbf{r}) = A_z \mathbf{e}_z = \frac{\mu_0 I}{4\pi} \int_{-L}^{L} \frac{dz}{R} \mathbf{e}_z$$

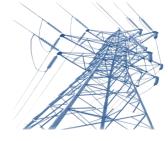
$$= \frac{\mu_0 I}{4\pi} \int_{-L}^{L} \frac{dz'}{\sqrt{\rho^2 + z'^2}} \mathbf{e}_z$$

$$= \frac{\mu_0 I}{2\pi} \left[\ln\left(L + \sqrt{\rho^2 + L^2}\right) - \ln\rho \right] \mathbf{e}_z$$

当L无限大时,即 $L \gg \rho$



$$A = \frac{\mu_0 I}{2\pi} \ln \frac{2L}{\rho} e_z$$
???
$$B = \nabla \times A = \frac{\mu_0 I}{2\pi\rho} e_\phi$$



3.4.2 基于场量A的分析

分析: 当导线无限长,即L趋于无穷大时,源分布在整个空间。但是磁矢量位的计算式实际上依据的是亥姆霍兹定理,其中规定源分布于有限区域,也就是相当于无穷远处是参考点。故上述情况不成立。此时必须把参考点选择非无穷远的某一点Q,设其与电流相距为 ρ_0

慘正:
$$A(\mathbf{r}) = \frac{\mu_0}{4\pi} \int_{l'} \frac{I}{R} d\mathbf{l'} + \mathbf{C} = \frac{\mu_0 I}{2\pi} \ln \frac{2L}{\rho} \mathbf{e}_z + \mathbf{C}$$

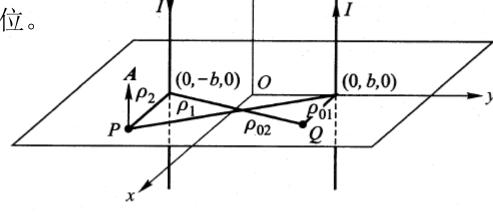
对*Q*点:
$$A_Q = \frac{\mu_0 I}{2\pi} \ln \frac{2L}{\rho_0} e_z + C = 0$$
 \longrightarrow $C = -\frac{\mu_0 I}{2\pi} \ln \frac{2L}{\rho_0} e_z$

$$A = \frac{\mu_0 I}{2\pi} \ln \frac{\rho_0}{\rho} e_z \qquad \Longrightarrow \qquad B = \nabla \times A = \frac{\mu_0 I}{2\pi\rho} e_\phi$$



例3-10 无限长直平行输电线,半径a,相距2b, 且b远大于a,求空间磁矢量位。

$$A = \left[\frac{\mu_0 I}{2\pi} \ln \frac{\rho_{01}}{\rho_1} - \frac{\mu_0 I}{2\pi} \ln \frac{\rho_{02}}{\rho_2}\right] \boldsymbol{e}_z$$
$$= \left[\frac{\mu_0 I}{2\pi} \ln \frac{\rho_2}{\rho_1} - \frac{\mu_0 I}{2\pi} \ln \frac{\rho_{01}}{\rho_{02}}\right] \boldsymbol{e}_z$$



为了简化计算结果,可考虑将参考点选择在x轴上,则有 $\rho_{01} = \rho_{02}$

磁通:
$$\Phi = \int_{S} \mathbf{B} \cdot d\mathbf{S} = \int_{S} (\nabla \times \mathbf{A}) \cdot d\mathbf{S} = \oint_{I} \mathbf{A} \cdot d\mathbf{I}$$

基于A求磁通



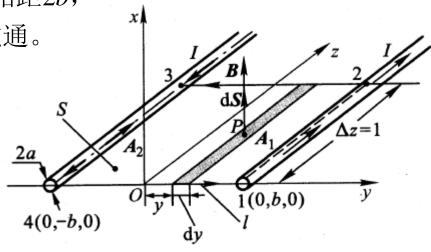
例3-11 无限长直平行输电线,半径a,相距2b,

且b远大于a, 求两线间单位长磁通。

分析: 本题与上题模型一致, 故结论可用

解1: 由安培环路和叠加定理

$$\mathbf{B} = \frac{\mu_0 I}{2\pi\rho_1} \mathbf{e}_x + \frac{\mu_0 I}{2\pi\rho_2} \mathbf{e}_x$$
$$= \frac{\mu_0 I}{2\pi(b-y)} \mathbf{e}_x + \frac{\mu_0 I}{2\pi(b+y)} \mathbf{e}_x$$



磁通:

$$\Phi = \int_{S} \mathbf{B} \cdot d\mathbf{S} = \int_{S} \mathbf{B} \cdot \Delta z dy \mathbf{e}_{x} = 2 \int_{0}^{b-a} \left[\frac{\mu_{0}I}{2\pi (b-y)} + \frac{\mu_{0}I}{2\pi (b+y)} \right] dy$$

$$= \frac{\mu_{0}I}{\pi} \left[-\ln(b-y) + \ln(b+y) \right]_{0}^{b-a} = \frac{\mu_{0}I}{\pi} \ln \frac{2b-a}{a}$$



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解2: 基于A进行求解

选取有向闭合曲线l(曲面S的边界):

 $=\frac{\mu_0 I}{2\pi} \ln \frac{\left(2b-a\right)^2}{a^2} = \frac{\mu_0 I}{\pi} \ln \frac{2b-a}{a}$

$$1 \rightarrow 2 \rightarrow 3 \rightarrow 4$$

$$\Phi = \oint_{l} \mathbf{A} \cdot d\mathbf{l} = \int_{1}^{2} \mathbf{A}_{1} \cdot d\mathbf{l} + 0 + \int_{3}^{4} \mathbf{A}_{2} \cdot d\mathbf{l} + 0$$

$$= \mathbf{A}_{1} \Delta z + \mathbf{A}_{2} \left(-\Delta z \right) = \frac{\mu_{0} I}{4\pi} \ln \frac{\left(b - a + b\right)^{2}}{\left(b - a - b\right)^{2}} - \frac{\mu_{0} I}{4\pi} \ln \frac{\left(-b + a + b\right)^{2}}{\left(-b + a - b\right)^{2}}$$



例3-12: 磁偶极子远区磁场A, B。 $r \gg a$

分析: 首先磁场具有轴对称特征,A只有 ϕ 方向

分量,即
$$\mathbf{A} = A_{\phi}(r,\theta)\mathbf{e}_{\phi}$$

定义: 磁偶极矩: m=IdS

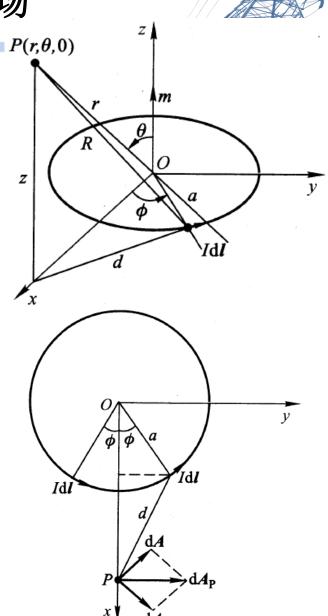
解: 要求A,先取元电流Idl,建立球坐标系,

$$dA = \frac{\mu_0 I dl}{4\pi R}$$

在子午面两侧取对称的元电流,使得P点dA只有 ϕ 方向分量,

1

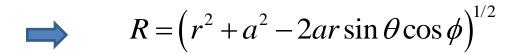
$$d\mathbf{A}_{p} = 2d\mathbf{A}\cos\phi = 2\frac{\mu_{0}Iad\phi}{4\pi R}\cos\phi\mathbf{e}_{\phi}$$



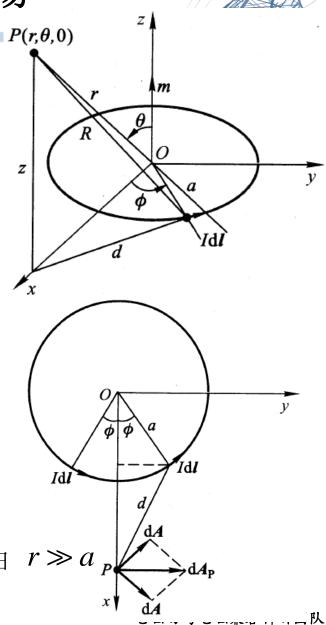
$$A_{p} = \int_{0}^{\pi} dA_{p} = \int_{0}^{\pi} 2dA \cos \phi = \int_{0}^{\pi} 2 \frac{\mu_{0} Iad\phi}{4\pi R} \cos \phi e_{\phi}$$
$$= \frac{\mu_{0} Ia}{2\pi} \int_{0}^{\pi} \frac{\cos \phi}{R} d\phi e_{\phi}$$

$$\exists R = \sqrt{z^2 + d^2} = \sqrt{(r\cos\theta)^2 + d^2}$$

$$d^2 = (a\sin\phi)^2 + (r\sin\theta - \cos\phi)^2$$



$$\frac{1}{R} = \frac{1}{\sqrt{r^2 + a^2 - 2ar\sin\theta\cos\phi}}$$





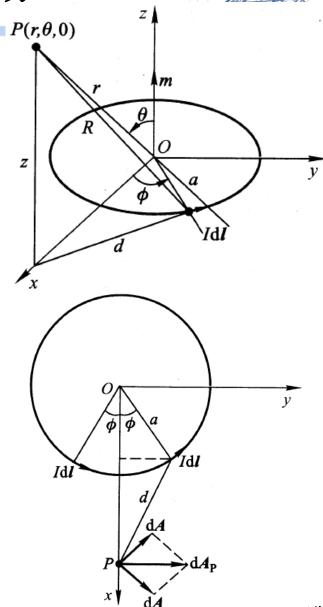
$$\frac{1}{R} = \frac{1}{r\sqrt{1 + \frac{a^2}{r^2} - \frac{2a}{r}\sin\theta\cos\phi}}$$

$$\frac{1}{R} = \frac{1}{r} \left(1 + \frac{a^2}{r^2} - \frac{2a}{r} \sin \theta \cos \phi \right)^{-1/2}$$

$$\oplus r \gg a \qquad \Longrightarrow R \gg a$$

$$\frac{1}{R} \approx \frac{1}{r} \left(1 - \frac{2a}{r} \sin \theta \cos \phi \right)^{-1/2}$$

$$\approx \frac{1}{r} \left(1 + \frac{a}{r} \sin \theta \cos \phi \right)$$
代入前式





$$A_{p} = \frac{\mu_{0}Ia}{2\pi} \int_{0}^{\pi} \frac{\cos\phi}{R} d\phi e_{\phi}$$

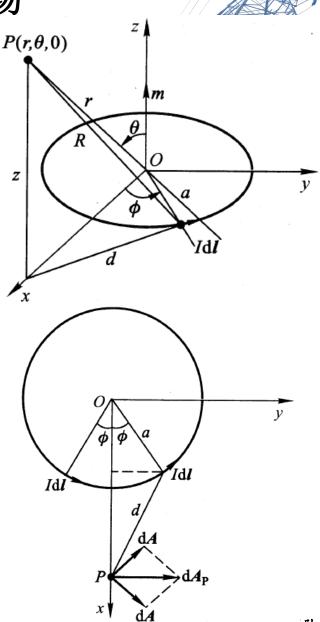
$$= \frac{\mu_{0}Ia}{2\pi} \int_{0}^{\pi} \frac{1}{r} \left(1 + \frac{a}{r} \sin\theta \cos\phi \right) \cos\phi d\phi e_{\phi}$$

$$= \frac{\mu_{0}I\pi a^{2}}{4\pi r^{2}} \sin\theta e_{\phi} = \frac{\mu_{0}}{4\pi} \frac{m \times e_{r}}{r^{2}}$$

$$B = \nabla \times A$$

$$= \frac{1}{r \sin\theta} \frac{\partial}{\partial \theta} (\sin\theta A_{\phi}) e_{r} - \frac{1}{r} \frac{\partial}{\partial r} (rA_{\phi}) e_{\theta}$$

$$= \frac{\mu_{0}m}{4\pi r^{3}} (2\cos\theta e_{r} + \sin\theta e_{\theta})$$





磁偶极子:
$$A_p = \frac{\mu_0}{4\pi} \frac{m \times e_r}{r^2}$$
$$B = \frac{\mu_0 m}{4\pi r^3} (2\cos\theta e_r + \sin\theta e_\theta)$$

磁偶极子远区的磁场,与电偶极子远区的电场具有相同的分布形态;不同 的是所不同的是电场线起始于正电荷,终止于负电荷,而磁场线自身闭合。



3.4.3 磁场线

与电力线的定义类似,对于描述磁场B分布的磁力线有

$$\boldsymbol{B} \times d\boldsymbol{l} = 0$$

$$(B_x \mathbf{e}_x + B_y \mathbf{e}_y + B_z \mathbf{e}_z) \times (dx \mathbf{e}_x + dy \mathbf{e}_y + dz \mathbf{e}_z)$$

$$= (B_y dz - B_z dy) \mathbf{e}_x + (B_z dx - B_x dz) \mathbf{e}_y + (E_x dy - E_y dx) \mathbf{e}_z = 0$$

$$\frac{dx}{B_x} = \frac{dy}{B_y} = \frac{dz}{B_z}$$

对于平行平面场,当给定 $\boldsymbol{J} = \boldsymbol{J}_z(x,y)\boldsymbol{e}_z$ \Rightarrow $\boldsymbol{A} = \boldsymbol{A}_z(x,y)\boldsymbol{e}_z$

$$\mathbf{B} = \nabla \times \mathbf{A}$$



3.4.3 磁场线

与电力线的定义类似,对于描述磁场B分布的磁力线有

$$\boldsymbol{B} \times d\boldsymbol{l} = 0$$

$$B_{x} = \frac{\partial A_{z}}{\partial y} \qquad B_{y} = -\frac{\partial A_{z}}{\partial x} \qquad B_{z} = 0$$

$$B_{y} = -\frac{CA_{z}}{\partial x}$$

$$B_z = 0$$



$$\frac{dx}{B_x} = \frac{dy}{B_y}$$

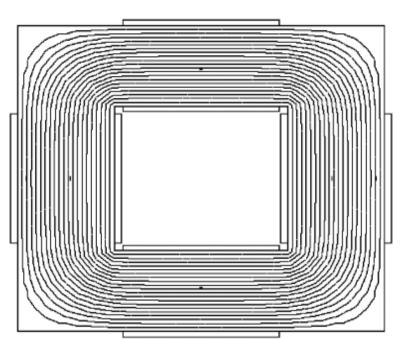
$$\frac{\partial A_z}{\partial x} dx + \frac{\partial A_z}{\partial y} dy = 0 \qquad \Rightarrow \qquad dA_z = 0$$

$$dA_z = 0$$



$$A_{-} = C$$

 $A_r = C$ A_r 取定值的轨迹,即为**B**线。





- 3.5 媒质中的磁场
- 3.5.1 媒质磁化

磁偶极子:

电子围绕原子核轨道运动 🔷 环形电流 🗬 磁偶极子 🗬 轨道磁矩

原子、电子自旋 📦 磁偶极子 📦 自旋磁矩

为描述媒质的宏观磁化状态, 定义,

磁化强度
$$M$$
: $M = \lim_{\Delta V \to 0} \frac{\sum m}{\Delta V}$ (A/m)

意义:单位体积中微观磁偶极矩m矢量之和。



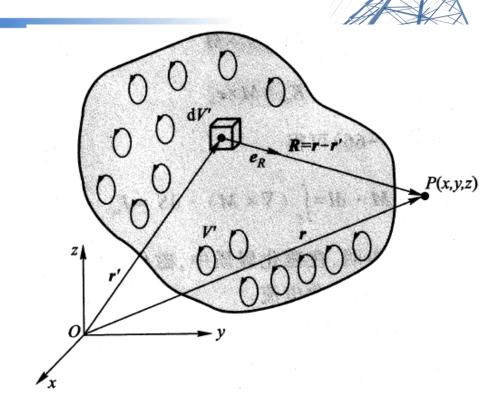
单个磁偶极子:
$$A = \frac{\mu_0}{4\pi} \frac{\mathbf{m} \times \mathbf{e}_r}{r^2}$$

$$A = \frac{\mu_0}{4\pi} \frac{\mathbf{m} \times \mathbf{e}_R}{R^2}$$

$$A_1 = \frac{\mu_0}{4\pi} \frac{\boldsymbol{m}_1 \times \boldsymbol{e}_R}{R^2}$$
 $A_2 = \frac{\mu_0}{4\pi} \frac{\boldsymbol{m}_2 \times \boldsymbol{e}_R}{R^2} \dots$

dV' 对应于P点处的场,

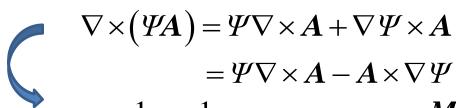
$$d\mathbf{A} = \frac{\mu_0}{4\pi} \frac{\sum_{i=1}^{\infty} \mathbf{m} \times \mathbf{e}_R}{R^2} = \frac{\mu_0}{4\pi} \frac{\mathbf{M} \times \mathbf{e}_R}{R^2} dV' = \frac{\mu_0}{4\pi} \mathbf{M} \times \nabla' \left(\frac{1}{R}\right) dV'$$





$$\boldsymbol{A} = \int_{V'} \frac{\mu_0}{4\pi} \boldsymbol{M} \times \nabla' \left(\frac{1}{R}\right) dV'$$

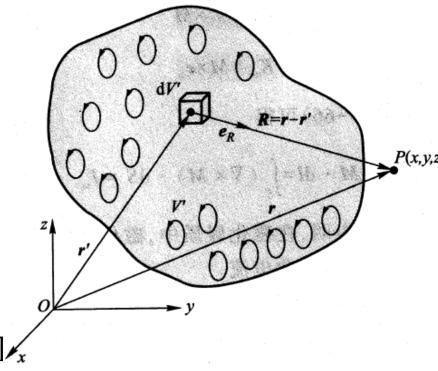
由矢量恒等式



$$M(r') \times \nabla'(\frac{1}{R}) = \frac{1}{R} \nabla' \times M(r') - \nabla' \times \left[\frac{M(r')}{R}\right] \times \left[\frac{M(r')}{R}\right]$$

$$A = \frac{\mu_0}{4\pi} \int_{V'} \frac{\nabla' \times \boldsymbol{M}(\boldsymbol{r}')}{R} dV' - \int_{V'} \nabla' \times \left[\frac{\boldsymbol{M}(\boldsymbol{r}')}{R}\right] dV'$$

由矢量恒等式
$$\int_{V} (\nabla \times \mathbf{A}) dV = \oint_{S} (\mathbf{e}_{n} \times \mathbf{A}) dS$$





$$\mathbf{A} = \frac{\mu_0}{4\pi} \int_{V'} \frac{\nabla' \times \mathbf{M}(\mathbf{r}')}{R} dV' + \oint_{S'} \frac{\mathbf{M}(\mathbf{r}') \times \mathbf{e}_n}{R} dS'$$

自由空间传导电流产生磁场,

$$\mathbf{A} = \frac{\mu_0}{4\pi} \int_{V'} \frac{\mathbf{J}_c(\mathbf{r}')}{R} dV' \quad \mathbf{A} = \frac{\mu_0}{4\pi} \int_{S'} \frac{\mathbf{K}_c(\mathbf{r}')}{R} dS'$$

比较发现,规律一致,故定义如下

$$\boldsymbol{J}_{m} = \nabla' \times \boldsymbol{M}(\boldsymbol{r}')$$

磁化体电流密度

$$\boldsymbol{K}_{m} = \boldsymbol{M}(\boldsymbol{r}') \times \boldsymbol{e}_{n}$$

磁化面电流密度

$$\oint_{S} \boldsymbol{M}(\boldsymbol{r}') \cdot d\boldsymbol{l} = \int_{S} \left[\nabla \times \boldsymbol{M}(\boldsymbol{r}') \right] \cdot d\boldsymbol{S} = \int_{S} \boldsymbol{J}_{m} \cdot d\boldsymbol{S} = \boldsymbol{I}_{m}$$



3.5.2 一般形式的安培环路定律

自由空间:
$$\oint_I \mathbf{B} \cdot d\mathbf{l} = \mu_0 \sum I$$

媒质空间:
$$\oint_{I} \mathbf{B} \cdot d\mathbf{l} = \mu_0 \left(\sum I + \sum I_m \right)$$

对多数媒质:
$$M = \chi_m H$$
 ض 磁化率

$$\boldsymbol{B} = \mu_0 (\boldsymbol{H} + \boldsymbol{M}) = \underline{\mu_0 (1 + \chi_m) \boldsymbol{H}} = \underline{\mu \boldsymbol{H}} \qquad \mu_r = \frac{\mu}{\mu_0} = (1 + \chi_m)$$

磁导率 相对磁导率





 $K=Ke'_n$

3.5.3 不同媒质分界面的边界条件

(1) 两种不同磁媒质

$$\oint_{l} \boldsymbol{H} \cdot d\boldsymbol{l} = \sum_{S} \boldsymbol{I} = \int_{S} \boldsymbol{J} \cdot d\boldsymbol{S}$$

设分界面上,电流密度 $K = Ke_n' \left(e_n' = e_t \times e_n \right)$

分界面两侧作一个狭小的矩形回路

$$\oint_{l} \boldsymbol{H} \cdot d\boldsymbol{l} = H_{1t} \Delta l_{1} - H_{2t} \Delta l_{1} = K \Delta l_{1}$$

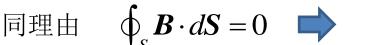


$$H_{1t} - H_{2t} = K$$

通常情况下,不同磁媒质分界面处,不存在自由面电流,即K=0



$$H_{1t} = H_{2t}$$



$$B_{1n} = B_{2n}$$

$$\boldsymbol{e}_{n} \times (\boldsymbol{H}_{2} - \boldsymbol{H}_{1}) = \boldsymbol{K}$$

 B_1, H_1

$$\boldsymbol{e}_n \cdot (\boldsymbol{B}_2 - \boldsymbol{B}_1) = 0$$







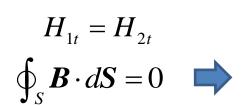
3.5.3 不同媒质分界面的边界条件

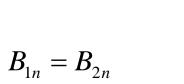
折射定理:
$$\frac{\tan \alpha_1}{\tan \alpha_2} = \frac{\mu_1}{\mu_2}$$

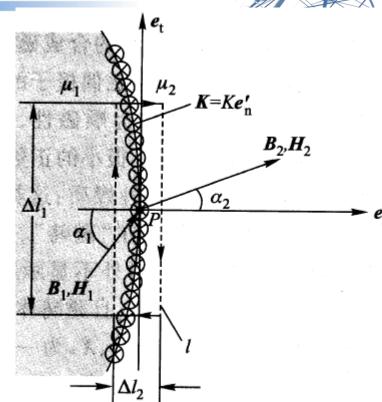
(2) 铁磁媒质与空气分界面 $\mu_1 \gg \mu_2 \approx \mu_0$ 由折射定理可知,只要 $\alpha_1 \neq \pi/2$,则 $\alpha_2 \rightarrow 0$ 即空气侧场线近似垂直于分界面



$$B_{1n} = B_{2n} \quad H_{1t} = H_{2t} \approx 0$$







$$\boldsymbol{e}_{n} \times (\boldsymbol{H}_{2} - \boldsymbol{H}_{1}) = \boldsymbol{K}$$

$$\boldsymbol{e}_n \cdot (\boldsymbol{B}_2 - \boldsymbol{B}_1) = 0$$



3.5.3 不同媒质分界面的边界条件

(3) 基于A的表述

$$\begin{cases} A_1 = A_2 \\ \frac{1}{\mu_1} (\nabla \times A_1)_t - \frac{1}{\mu_2} (\nabla \times A_2)_t = K \end{cases}$$

3.5.4 场的分布

(1) 基于场量H的分析

例3-15 截面半径a «R, 磁导率为 μ , 求 铁心及气隙中H,B

解:设 铁心中:H,B 气隙中: H_{δ} , B_{δ}

由安培环路定理,

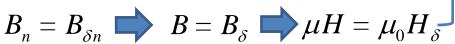
$$\oint_{I} \boldsymbol{H} \cdot d\boldsymbol{l} = NI$$

$$H_{\delta}d + H(2\pi R - d) = NI$$

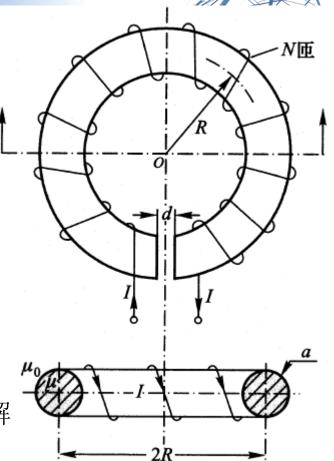
由分界面边界条件,

$$B_n = B_{\delta n}$$

$$B = B_{\delta}$$



- 联立求解





3.5.4 场的分布

(1) 基于场量H的分析



$$\boldsymbol{H} = \frac{NI}{\mu_r d + (2\pi R - d)} \boldsymbol{e}_{\phi} \qquad \boldsymbol{B} = \mu \boldsymbol{H}$$

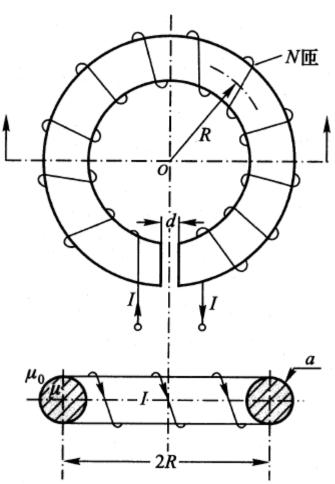
$$H_{\delta} = \frac{\mu}{\mu_0} H = \frac{\mu_r NI}{\mu_r d + (2\pi R - d)} \qquad B_{\delta} = \mu_0 H_{\delta}$$

$$\boldsymbol{H}_{\delta} = H_{\delta} \boldsymbol{e}_{\phi}$$

$$B = \mu H$$

$$B_{\delta} = \mu_0 H_{\delta}$$

$$\boldsymbol{B}_{\delta} = \mu_0 \boldsymbol{H}_{\delta}$$





3.5.4 场的分布

(2) 基于边值问题

前面关于磁场的求解:

前面关于磁场的方程:

$$\mathbf{B} = \frac{\mu_0}{4\pi} \int_{V'} \frac{\mathbf{J}_c(\mathbf{r}') \times \mathbf{e}_R}{R^2} dV'$$

$$\oint_l \mathbf{B} \cdot d\mathbf{l} = \mu_0 \sum I$$

$$\oint_l \mathbf{H} \cdot d\mathbf{l} = \int_S \mathbf{J} \cdot d\mathbf{S} = \sum I$$

$$abla imes H = J$$
 $B = \mu H$
 $\otimes \mathcal{B} = \nabla \times A$



3.5.4 场的分布

(2) 基于边值问题

$$\nabla \times \boldsymbol{H} = \boldsymbol{J}_{c}$$

$$\boldsymbol{B} = \mu_{0} \boldsymbol{H}$$

$$\boldsymbol{B} = \nabla \times \boldsymbol{A}$$

$$\nabla \times \nabla \times \boldsymbol{A} = \nabla (\nabla \cdot \boldsymbol{A}) - \nabla^{2} \boldsymbol{A} = \mu_{0} \boldsymbol{J}_{c}$$

分析: 对于矢量场A,需由其散度和旋度唯一确定,故由 $B = \nabla \times A$ 可知,仍需要定义其散度

规定: $\nabla \cdot \mathbf{A} = 0$ 库仑规范

$$\nabla^2 A = -\mu_0 J_c$$

$$\nabla^2 A_x = -\mu_0 J_{cx}$$

$$\nabla^2 A_y = -\mu_0 J_{cy}$$

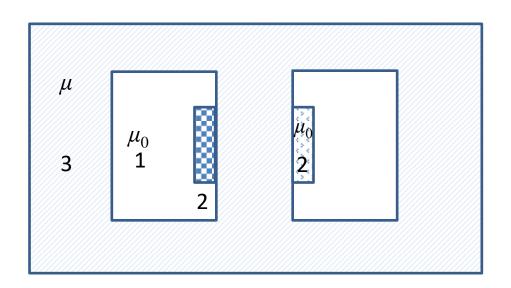
$$\nabla^2 A_z = -\mu_0 J_{cz}$$



3.5.4 场的分布

(2) 基于边值问题

思考题: 对1,2,3区域分别列写关于 A_z 的边值问题,大致画出B线走势。





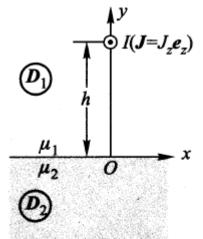
3.5.4 场的分布

(3) 镜像法 与静电场中类似,根据恒定磁场解的唯一性,计算和分析无限长直载流导线在空间的磁场问题

$$\nabla^{2} A_{z} = -\mu_{0} J_{cz}$$

$$A_{z1}|_{y=0} = A_{z2}|_{y=0} \quad (H_{1t} = H_{2t})$$

$$\frac{1}{\mu_{1}} \frac{\partial A_{z1}}{\partial n} = \frac{1}{\mu_{2}} \frac{\partial A_{z2}}{\partial n} \quad (B_{1n} = B_{2n})$$





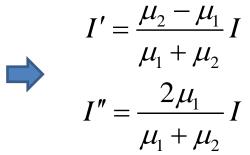
如何取镜像?

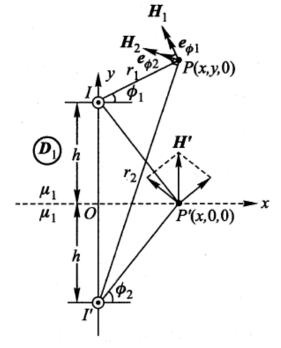
(a) 线电流-无限大 平表面媒质系统



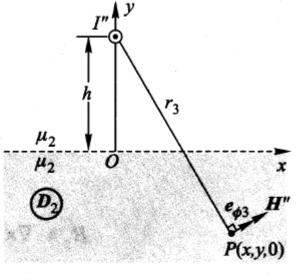
3.5.4 场的分布

(3) 镜像法 与静电场中类似,根据恒定磁场解的唯一性,计算和分析无限长直载流导线在空间的磁场问题





(b) 上半空间磁场 的镜像法图示



(c) 下半空间磁场 的镜像法图示

EMF&EMC



设一根载流为I的无限长直导线平行放置在无限大铁磁媒质表面上 例3-18:

方,间距为h,试求空气中和铁磁媒质中的磁场

解: 由前面的分析可知, $\mu_1 = \mu_0$, $\mu_2 = \mu_\infty$

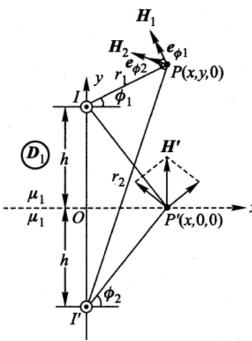
$$I' = \frac{\mu_2 - \mu_1}{\mu_1 + \mu_2} I = \frac{\mu_\infty - \mu_0}{\mu_0 + \mu_\infty} I \approx I$$

$$I'' = \frac{2\mu_1}{\mu_1 + \mu_2} I = \frac{2\mu_0}{\mu_0 + \mu_\infty} I \approx 0$$

(1) 上半空间:
$$H = H_1 + H_2 = \frac{I}{2\pi r_1} e_{\phi 1} + \frac{I}{2\pi r_2} e_{\phi 2}$$

其中
$$r_1 = \sqrt{x^2 + (y - h)^2}$$
 $r_2 = \sqrt{x^2 + (y + h)^2}$

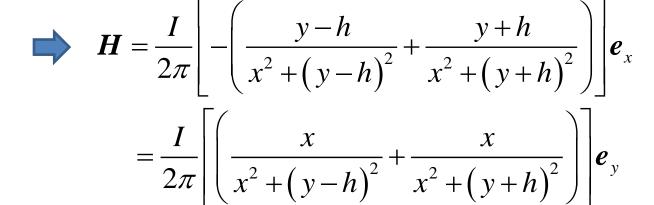
由单位矢量转换关系,
$$\begin{cases} e_{\phi 1} = -e_x \sin \phi_1 + e_y \cos \phi_1 \\ e_{\phi 2} = -e_x \sin \phi_2 + e_y \cos \phi_2 \end{cases}$$



(b) 上半空间磁场 的镜像法图示

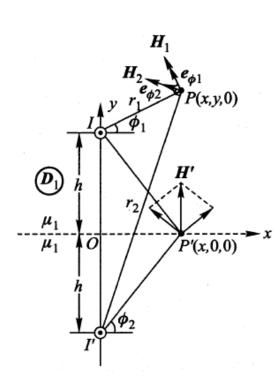
EMF&EMC





在边界上(y=0)任意一点处:

$$\boldsymbol{H}\big|_{y=0} = \frac{\boldsymbol{I}x}{\pi(x^2 + h^2)}\boldsymbol{e}_y$$



(b) 上半空间磁场 的镜像法图示



(2) 下半空间

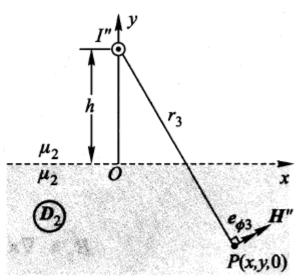


$$\boldsymbol{H} \approx 0$$

$$\boldsymbol{B} = \mu \boldsymbol{H} = \mu_{\infty} \boldsymbol{H} = ??$$

$$\mathbf{B} = \mu_{\infty} \mathbf{H} = \mu_{\infty} \frac{I''}{2\pi r_{3}} \mathbf{e}_{\phi 3} = \mu_{\infty} \frac{2\mu_{0}}{\mu_{0} + \mu_{\infty}} \frac{I}{2\pi r_{3}} \mathbf{e}_{\phi 3}$$

$$= \frac{\mu_{0} I}{2\pi r_{3}} \mathbf{e}_{\phi 3}$$



(c) 下半空间磁场 的镜像法图示



3.6 电感

3.6.1 自电感

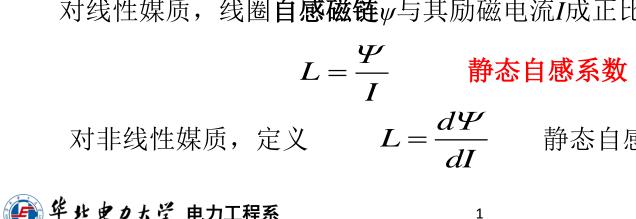
载有电流1的线圈,其各匝交链的磁通总和, 磁链: 称之为磁链ψ, 也称自感磁链

线圈各匝交链的磁通往往并不相同(由于漏磁存在等)

$$\mathbf{\Psi} = \sum_{i=1}^{M} N_{i} \mathbf{\Phi}_{i}$$

对线性媒质,线圈**自感磁链** ψ 与其励磁电流I成正比,定义 I

静态自感系数





3.6.1 自电感

自感磁链: 外磁链+内磁链 (载流导体截面较大,不可忽略时)

- a. 外磁链: 与电流完全交链的磁通之和
- b. 内磁链: 与电流部分交链的磁通之和
- a. 外磁链对应磁通: $dS_1 \rightarrow d\Phi_1 \rightarrow I$
- b. 内磁链对应磁通: $dS_2 \rightarrow d\Phi_2 \rightarrow I' \frac{I'}{r} \times 1$

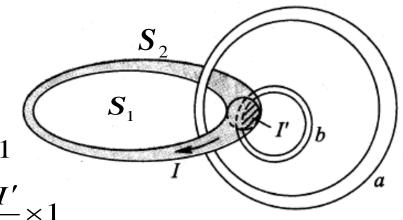
$$d\Psi_0 = d\Phi_1 \times 1$$



$$d\mathcal{\Psi}_{o} = d\mathcal{\Phi}_{1} \times 1 \quad \Longrightarrow \quad \mathcal{\Psi}_{o} = \int_{S_{1}} d\mathcal{\Phi}_{1} \times 1$$

$$d\Psi_{\rm i} = d\Phi_{\rm 2} \times \frac{I'}{I}$$

$$d\Psi_{i} = d\Phi_{2} \times \frac{I'}{I} \quad \Longrightarrow \quad \Psi_{i} = \int_{S_{2}} d\Phi_{2} \times \frac{I'}{I}$$



$$L = \frac{\Psi}{I} = \frac{\Psi_i + \Psi_o}{I}$$

$$=L_i+L_o$$



3.6.1 自电感

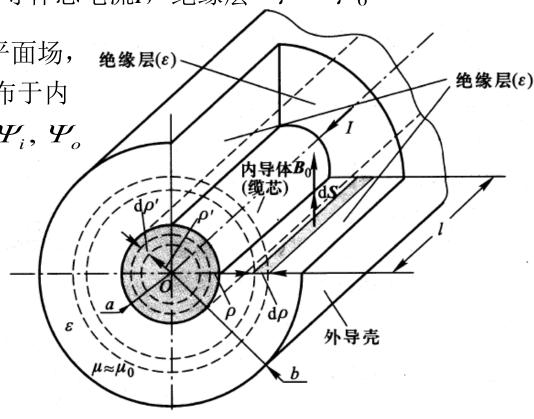
例3-19: 求同轴电缆的自感。外壳厚度可忽略,导体内外径分别为a,b,长度为L,远大于a,b,内导体总电流I,绝缘层 $\mu \approx \mu_0$

解: 由于 $L \gg b$,可视为平行平面场, 场具有圆柱对称性,磁场分布于内 导体和绝缘层,分别对应于 Ψ_i , Ψ_o

(1) 外磁链 ψ_0 :

$$\mathcal{\Psi}_{o} = \int_{S_{1}} d\mathcal{\Psi}_{o} = \int_{S_{1}} d\mathcal{\Phi}_{o} \times 1$$
$$= \int_{S_{1}} \mathbf{B}_{o} \cdot d\mathbf{S}$$

求 B_0 和 H_0 ,确定面元dS



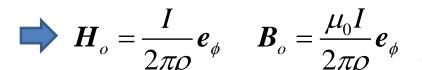


求 $\boldsymbol{B}_{\mathrm{o}}$ 和 $\boldsymbol{H}_{\mathrm{o}}$

作半径为 ρ 的环形路径 $l(a < \rho < b)$

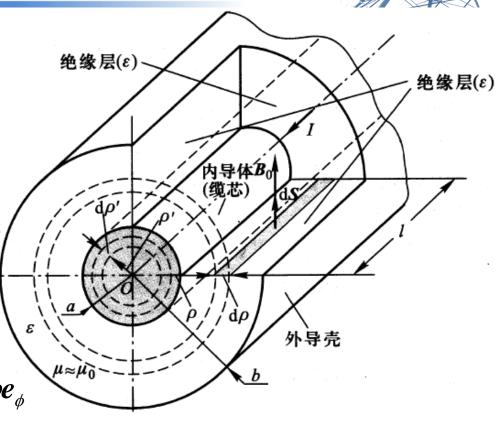
$$\oint_{l} \boldsymbol{H}_{o} \cdot d\boldsymbol{l} = \oint_{l} H_{o} \boldsymbol{e}_{\phi} \cdot dl \boldsymbol{e}_{\phi}$$

$$= \oint_{l} H_{o} dl = H_{o} \oint_{l} dl = I$$



取长度为l,宽为 $d\rho$ 的面元 $dS = ld \rho e_{\phi}$

$$\Psi_{o} = \int_{S_{1}} d\Psi_{o} = \int_{S_{1}} d\Phi_{o} = \int_{S_{1}} \mathbf{B}_{o} \cdot d\mathbf{S} = \int_{a}^{b} \frac{\mu_{o}I}{2\pi\rho} ld\rho = \frac{\mu_{o}Il}{2\pi} \ln \frac{b}{a}$$





求 \mathbf{B}_{i} 和 \mathbf{H}_{i} : 作半径为 ρ 的环形路径 $l\left(a<\rho< b\right)$

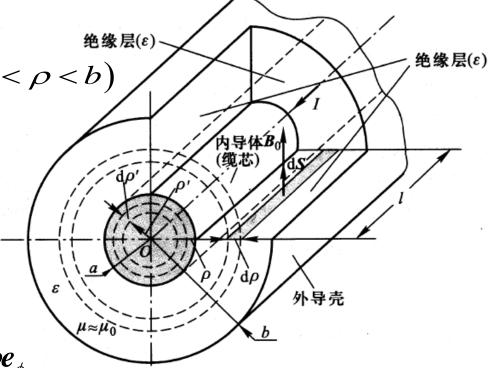
$$\oint_{l} \boldsymbol{H}_{i} \cdot d\boldsymbol{l} = \oint_{l} H_{i} \boldsymbol{e}_{\phi} \cdot dl \boldsymbol{e}_{\phi} = \oint_{l} H_{i} dl$$

$$= H_{i} \oint_{l} dl = I' = \frac{\pi \rho^{2}}{\pi a^{2}} I$$

取长度为l,宽为 $d\rho$ 的面元 $dS = ld \rho e_{\phi}$

$$\Psi_{i} = \int_{S_{2}} d\Psi_{i} = \int_{S_{2}} d\Phi_{i} \times \frac{I}{I'} = \int_{S_{2}} \frac{I}{I'} \mathbf{B}_{i} \cdot d\mathbf{S} = \int_{0}^{a} \frac{\rho^{2}}{a^{2}} \frac{\mu_{0} I \rho}{2\pi a^{2}} l d\rho = \frac{\mu_{0} I l}{8\pi}$$

自感:
$$L = \frac{\Psi}{I} = \frac{\Psi_i + \Psi_o}{I} = L_i + L_o = \frac{\mu_0 l}{2\pi} \ln \frac{b}{a} + \frac{\mu_0 l}{8\pi}$$





例3-20: 计算下图所示两线传输线的自感,线长为1, 且远大于导线半

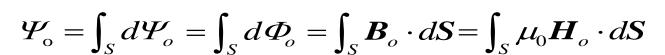
径a和线间距D。

解:

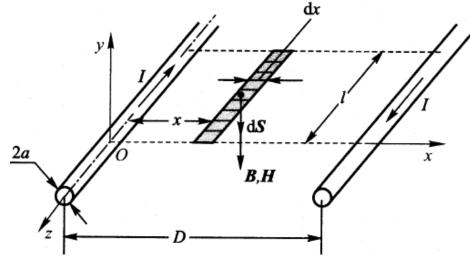
(1)由前面分析可知,双线传输线的内 自感只与长度有关,

$$L_i = \frac{\mu_0}{8\pi} 2l = \frac{\mu_0 l}{4\pi}$$

(2) 外自感,可按照如下求解



由安培环路和叠加定理,坐标为x处的H





$$\boldsymbol{H}_{o} = \left[\frac{I}{2\pi x} + \frac{I}{2\pi (D-x)}\right] \left(-\boldsymbol{e}_{y}\right)$$

取长度为l,宽为dx的面元 $dS = ldx \left(-e_y\right)^{\frac{2a}{3}}$

$$\boldsymbol{\mathcal{\Psi}}_{o} = \int_{S} d\boldsymbol{\mathcal{\Psi}}_{o} = \int_{S} \boldsymbol{B}_{o} \cdot d\boldsymbol{S} = \int_{S} \mu_{0} \boldsymbol{H}_{o} \cdot d\boldsymbol{S}$$

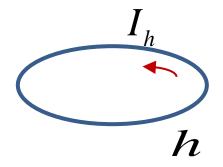
$$= \frac{\mu_0 I l}{2\pi} \int_a^{D-a} \left(\frac{1}{x} + \frac{1}{D-x} \right) dx = \frac{\mu_0 I l}{\pi} \ln \frac{D-a}{a}$$

$$L = L_i + L_o = \frac{\Psi_i + \Psi_o}{I} = \frac{\mu_0 l}{4\pi} + \frac{\mu_0 l}{\pi} \ln \frac{D - a}{a}$$



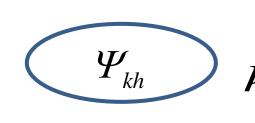
3.6.2 互电感

线性媒质中,若一个线圈k的磁链由另一个线圈h的电流 I_h 产生,记为互感磁链 ψ_{kh} ,定义线圈h对线圈k的静态互感系数

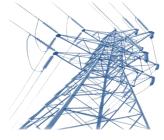


$$M_{kh} = \frac{\Psi_{kh}}{I_{h}}$$





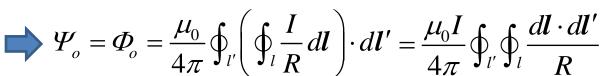
$$M_{hk} = rac{arPsi_{hk}}{I_k}$$



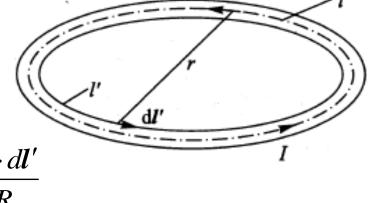
3.6.3 线形回路电感(截面可忽略)

由于截面可忽略,线电流I可看作集中在单匝回路中心轴线I上流动,

$$\Psi_o = \Phi_o = \int \mathbf{B}_o \cdot d\mathbf{S} = \oint_{l'} \mathbf{A} \cdot d\mathbf{l'}$$



对于多匝细导线绕制的线圈,其通过电流I时所产生的的磁通,可近似认为是,单匝电流I所产生的磁通的N倍,且该磁通与全部N匝线圈交链,

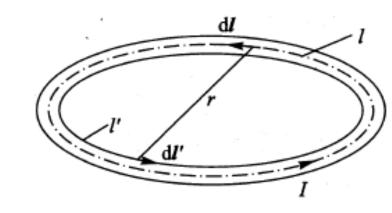




3.6.3 线形回路电感(截面可忽略)

外自感为

$$L_o = \frac{\Psi'}{I} = \frac{N\Phi_o'}{I} = N\frac{N\Phi_o}{I} = \frac{N^2\Phi_o}{I}$$
$$= \frac{N^2\mu_o I}{4\pi} \oint_{l'} \oint_{l} \frac{d\mathbf{l} \cdot d\mathbf{l'}}{R}$$



内自感:

当回路任何部位的曲率半径都大于截面半径时,其内自感等同于无限长直导线,只与其长度*l*有关,

$$L_i = \frac{\mu_0 l}{8\pi I} \qquad (\ll L_o)$$

$$L = L_i + L_o \approx L_o$$



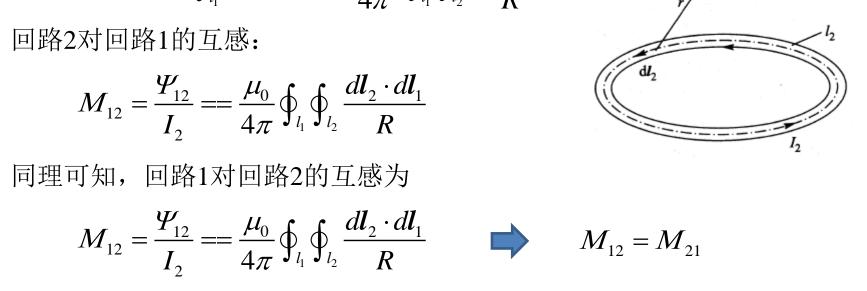
3.6.3 线形回路电感(截面可忽略)

两线形回路互感:

$$\Psi_{12} = \Phi_{12} = \oint_{l_1} \mathbf{A}_P \cdot d\mathbf{l}_1 = \frac{\mu_0 I_2}{4\pi} \oint_{l_1} \oint_{l_2} \frac{d\mathbf{l}_2 \cdot d\mathbf{l}_1}{R}$$

当两个回路的匝数分别为 N_1 和 N_2 时,

$$M_{12} = M_{21} = \frac{N_1 N_2 \mu_0}{4\pi} \oint_{l_1} \oint_{l_2} \frac{d\mathbf{l}_2 \cdot d\mathbf{l}_1}{R}$$





磁场能量 3. 7

3.7.1 载流回路系统中的磁场能量

设电流i由零逐渐增加至终值,并引起感应电动势 $e = -d\Psi/dt$, 外电 源克服感应电动势提供给线圈能量 dW = uidt (u = -e)

$$dW = i\left(\frac{d\Psi}{dt}\right)dt = id\left(Li\right) = Lidi$$

假设过程中无能量损失(机械能、焦耳热等),电源作功转化为磁 场能量,

$$dW_m = dW = Lidi$$

$$W_{m} = \int dW_{m} = \int_{0}^{I} Lidi = \frac{1}{2}LI^{2} \begin{cases} \text{单个回路电感:} \ L = 2W_{m}/I^{2} \\ \text{磁场能量:} \ W_{m} = LI^{2}/2 = I\Psi/2 \end{cases}$$





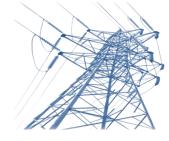
3.7.1 载流回路系统中的磁场能量

N个载流回路系统:

设磁场建立过程如下:各回路电流按照同一比例增长($0\rightarrow I_k$),增长的比例系数为m($0\leq m\leq 1$),则增长过程中某一时刻k回路电流为 $i_k(t)=m(t)\ I_k$,与回路k交链的磁通 $\Psi'_k=m\Psi_k$,在dt时间内,外源在m个载流回路中作功,

$$dW_{m} = dW = \sum_{k=1}^{n} i_{k} d\Psi'_{k} = \sum_{k=1}^{n} mI_{k} d(m\Psi_{k})$$
$$= \sum_{k=1}^{n} mI_{k} \Psi_{k} dm$$

当回路达到最终状态,外源所作总功:



3.7.1 载流回路系统中的磁场能量

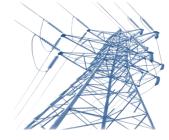
$$W_{m} = \int dW_{m} = \sum_{k=1}^{n} I_{k} \Psi_{k} \int_{0}^{1} m dm = \frac{1}{2} \sum_{k=1}^{n} I_{k} \Psi_{\underline{k}}$$

对于第k个载流回路, ψ_k 为自感磁链与互感磁链之和,即

$$\begin{aligned} \Psi_{k} &= (\Psi_{L})_{k} + (\Psi_{M})_{k} = L_{k}I_{k} + M_{k1}I_{1} + M_{k2}I_{2} + \dots + M_{kn}I_{n} \\ &= L_{k}I_{k} + \sum_{h=1, h \neq k}^{n} M_{kh}I_{h} \end{aligned}$$

对于第k个载流回路, ψ_k 为自感磁链与互感磁链之和,即

$$W_{m} = \frac{1}{2} L_{1} I_{1}^{2} + \frac{1}{2} L_{2} I_{2}^{2} + \dots + \frac{1}{2} L_{n} I_{n}^{2} + \left(M_{12} I_{1} I_{2} + M_{13} I_{1} I_{3} + \dots + M_{n-1,n} I_{n-1} I_{n} \right)$$



3.7.1 载流回路系统中的磁场能量

$$= \frac{1}{2} \sum_{k=1}^{n} L_k I_k^2 + \frac{1}{2} \sum_{k=1}^{n} \sum_{h=1, h \neq k}^{n} M_{kh} I_k I_h$$

由前一节分析可知,对于某个单匝的线形回路,以k回路为例,其磁 链Ψμ为

$$\Psi_k = \oint_{l_k} \mathbf{A}_k \cdot d\mathbf{l}_k'$$
 \mathbf{A}_k : 各回路电流在 k 号回路上 $d\mathbf{l}_k'$ 处产生的合磁矢量位

$$W_{m} = \frac{1}{2} \sum_{k=1}^{n} I_{k} \Psi_{k} = \frac{1}{2} \sum_{k=1}^{n} I_{k} \oint_{l_{k}'} A_{k} \cdot dl_{k}' = \frac{1}{2} \sum_{k=1}^{n} \oint_{l_{k}'} A_{k} \underbrace{I_{k} dl_{k}'} \longrightarrow \overline{\pi} \stackrel{\text{le}}{\pi}$$



静电场:

$$W_e = \frac{1}{2} \int_{V'} \rho \varphi dV'$$





3.7.2 磁场能量分布及其密度

$$A \leftrightarrow B = \nabla \times A$$
 $J \leftrightarrow \nabla \times H = J$

$$J \leftrightarrow \nabla \times H = J$$



$$W_m = \frac{1}{2} \int_V \boldsymbol{B} \cdot \boldsymbol{H} dV$$

$$W_m = \frac{1}{2} \int_V \mathbf{B} \cdot \mathbf{H} dV \qquad w_m = \frac{1}{2} \mathbf{B} \cdot \mathbf{H} \qquad = \frac{1}{2} \mu H^2 = \frac{B^2}{2\mu}$$

$$W_{m} = \frac{1}{2} \sum_{k=1}^{n} I_{k} \Psi_{k}$$

$$W_{m} = \frac{1}{2} \sum_{k=1}^{n} L_{k} I_{k}^{2} + \frac{1}{2} \sum_{k=1}^{n} \sum_{h=1, h \neq k}^{n} M_{kh} I_{k} I_{h}$$
 电路参数

求磁场能量:

$$W_m = \frac{1}{2} \int_V \boldsymbol{B} \cdot \boldsymbol{H} dV$$
 场空间 $W_m = \frac{1}{2} \int_{V'} \boldsymbol{A} \cdot \boldsymbol{J} dV'$ 源空间

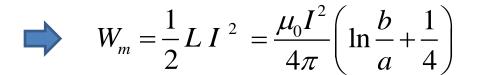
$$W_m = \frac{1}{2} \int_{V'} \boldsymbol{A} \cdot \boldsymbol{J} dV'$$
 源空间



例3-23: 求同轴电缆的单位长磁场能量。

解(1)基于电路参数计算,前面已经求出 过同轴电缆单位长电感为,

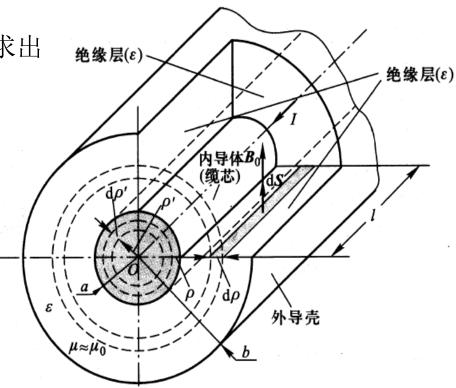
$$L = \frac{\mu_0}{2\pi} \left(\ln \frac{b}{a} + \frac{1}{4} \right)$$



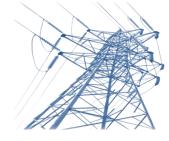
(2) 基于场分布计算,

内导体:
$$\boldsymbol{H}_{i} = \frac{I\rho}{2\pi a^{2}}\boldsymbol{e}_{\phi}$$

外导体:
$$H_o = \frac{I}{2\pi o} e_{\phi}$$

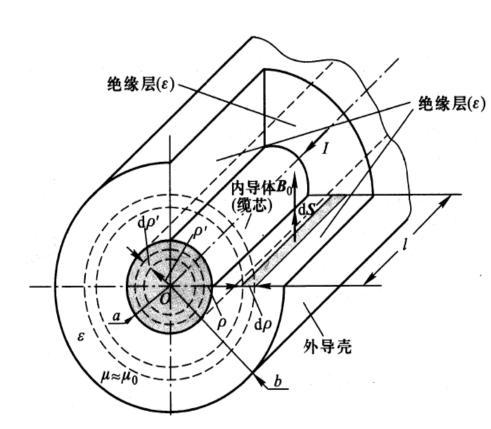


$$W_{mi} = \frac{1}{2} \int_{V} \boldsymbol{B}_{i} \cdot \boldsymbol{H}_{i} dV = \frac{1}{2} \int_{V} \mu H_{i}^{2} dV$$

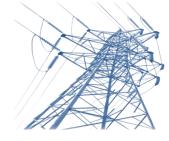


$$= \int_0^a \int_0^{2\pi} \frac{\mu_0}{2} \left(\frac{I\rho}{2\pi a^2} \right) \rho d\phi d\rho = \frac{\mu_0 I^2}{16\pi}$$

$$W_{mo} = \frac{1}{2} \int_{V} \boldsymbol{B}_{o} \cdot \boldsymbol{H}_{o} dV = \frac{1}{2} \int_{V} \mu H_{o}^{2} dV$$
$$= \int_{a}^{b} \int_{0}^{2\pi} \frac{\mu_{0}}{2} \left(\frac{I}{2\pi\rho} \right) \rho d\phi d\rho$$
$$= \frac{\mu_{0} I^{2}}{4\pi} \ln \frac{b}{a}$$



$$W_{m} = W_{mi} + W_{mo} = \frac{\mu_{0}I^{2}}{16\pi} + \frac{\mu_{0}I^{2}}{4\pi} \ln \frac{b}{a} = \frac{\mu_{0}I^{2}}{4\pi} \left(\ln \frac{b}{a} + \frac{1}{4} \right)$$



3.8 磁场力

磁场对运动电荷的力: $d\mathbf{F} = dq(\mathbf{v} \times \mathbf{B})$

磁场对元电流的力: $d\mathbf{F} = Id\mathbf{l} \times \mathbf{B}$

对整个载流回路: $d\mathbf{F} = \oint_{l} \mathbf{I} d\mathbf{l} \times \mathbf{B} = -\mathbf{I} \oint_{l} \mathbf{B} \times d\mathbf{l}$

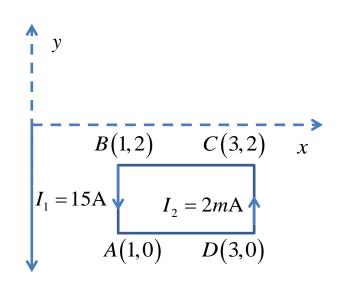
例: 求载流回路受合力

解:设回路是刚性的,总力为各边受力之和,

$$d\mathbf{F} = \oint_{l_2} Id\mathbf{l}_2 \times \mathbf{B} = -I_2 \oint_{l_2} \mathbf{B} \times d\mathbf{l}$$

$$= -2 \times 10^{-3} \left(\int_{BA} \mathbf{B}_1 \times d\mathbf{l} + \int_{DC} \mathbf{B}_1 \times d\mathbf{l} \right)$$

$$= -2 \times 10^{-3} \times \left(\int_{BA} \frac{\mu_0 I_1}{2\pi \times 1} \mathbf{e}_z \times dl \left(-\mathbf{e}_y \right) + \int_{DC} \frac{\mu_0 I_1}{2\pi \times 3} \mathbf{e}_z \times dl \left(-\mathbf{e}_y \right) \right)$$





3.8 磁场力

$$= -2 \times 10^{-3} \times 4\pi \times 10^{-7} \left(\int_{BA} \frac{I_1}{2\pi \times 1} dl \boldsymbol{e}_x + \int_{DC} \frac{I_1}{2\pi \times 3} dl \boldsymbol{e}_x \right)$$

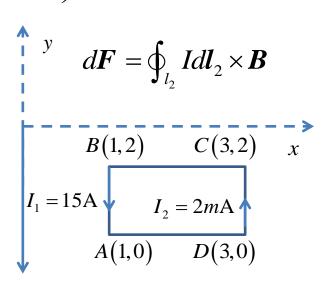
$$= -2 \times 10^{-3} \times 4\pi \times 10^{-7} \times 15 \times \left(\int_{BA} \frac{1}{2\pi \times 1} dl + \int_{DC} \frac{1}{2\pi \times 3} dl \right) e_{x}$$

$$=-8\times10^{-9}e_{x}(N)=-8e_{x}(nN)$$

思考: 求载流直导线为载流回路?

$$\boldsymbol{B}(\boldsymbol{r}) = \frac{\mu_0}{4\pi} \oint_{l_1} \frac{Id\boldsymbol{l}_1 \times \boldsymbol{e}_R}{R^2}$$

$$\boldsymbol{F}(\boldsymbol{r}) = \frac{\mu_0}{4\pi} \oint_{l_2} \oint_{l_1} (I_2 d\boldsymbol{l}_2) \times \frac{I_1 d\boldsymbol{l}_1 \times \boldsymbol{e}_R}{R^2}$$





磁场力 3.8

虚位移法:

由功能守恒可得

$$dW = dW_m + Fdg$$

$$dW = uidt = id\Psi \left(= \sum_{k=1}^{\infty} i_k d\Psi_k \right)$$
 外源输入系统的能量

$$dW_m = \frac{1}{2} \sum i_k d\Psi_k$$

广义坐标dg变化引起磁场能量变化

Fdg

dg方向的广义力作功



3.8 磁场力

(1) 常电流系统 I_{k} 不变,磁链变化量为 $d\psi_{k}$

外源提供能量,故由 $dW = dW_m + Fdg$

$$dW = dW_m + Fdg$$

$$\begin{cases} dW = \sum_{k} i_{k} d\Psi_{k} \\ dW_{m} = \frac{1}{2} \sum_{k} i_{k} d\Psi_{k} \end{cases} \Rightarrow Fdg = dW_{m}|_{I_{k} = C} \Rightarrow F = \frac{dW_{m}}{dg}|_{I_{k} = C}$$

(2) 常磁链系统 I_{ν} 变化,磁链不变,即 $d\psi_{\nu}$

广义力F的方向:广义坐标dg增大的方向

例3-24: 两线传输线系统, 求导线所受到的力

解:基于电路参数计算,前面已经求出过同

轴电缆单位长电感为,

$$L = \frac{\mu_0 l}{\pi} \left(\frac{1}{4} + \ln \frac{D - a}{a} \right)$$
$$\approx \frac{\mu_0 l}{\pi} \left(\frac{1}{4} + \ln \frac{D}{a} \right)$$

系统能量
$$W_m = \frac{1}{2}LI^2 \approx \frac{\mu_0 I^2 l}{2\pi} \left(\frac{1}{4} + \ln \frac{D}{a}\right)$$

设系统为常电流系统,由虚位移法,若取广义坐标为D,导线1受力为

$$F_1 = \frac{dW_m}{dD}\Big|_{I=C} = \frac{1}{2}I^2 \frac{dL}{dD} = \frac{\mu_0 I^2 l}{2\pi D}$$

正方向 e_x ,即D增大的方向

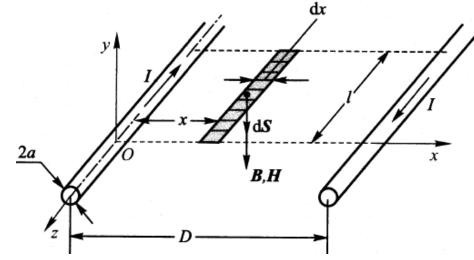




若取广义坐标为a,导线1受力为

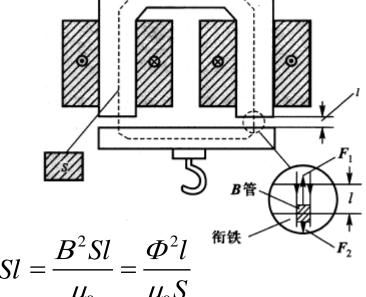
$$F_2 = \frac{dW_m}{da}\Big|_{I_k=C} = \frac{1}{2}I^2 \frac{dL}{da} = -\frac{\mu_0 I^2 l}{2\pi a}$$

正方向 e_{ρ} , 即a增大的方向



例3-26: 求电磁铁对衔铁的吸力,已知铁心截 面面积为S,空气气隙长度为l,忽略边 缘效应,认为气隙中磁密B均匀分布

解:由于已知尺寸等参数,磁密*B*亦可认为均匀分布,故可以假定系统是常磁链系统,



系统能量:
$$W_m = \frac{B^2}{2\mu} \times 2Sl' + \frac{B^2}{2\mu_0} \times 2Sl \approx \frac{B^2}{2\mu_0} \times 2Sl = \frac{B^2Sl}{\mu_0} = \frac{\Phi^2l}{\mu_0S}$$

由虚位移法, 若取广义坐标为1, 衔铁受力为

$$F = -\frac{dW}{dg}\Big|_{\sigma=C} = -\frac{dW}{dl} = -\frac{\Phi^2}{\mu_0 S} = -\frac{B^2 S}{\mu_0}$$
 正方向 \mathbf{e}_y , 即 l 增大的方向