

工程电磁场

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4.1 动态电磁场基本方程与边界条件

4.1.1 动态电磁场的基本方程

积分方程

微分方程

$$\oint_{l} \boldsymbol{H} \cdot d\boldsymbol{l} = \int_{S} \left(\boldsymbol{J} + \frac{\partial \boldsymbol{D}}{\partial t} \right) \cdot d\boldsymbol{S}$$

$$\nabla \times \boldsymbol{H} = \boldsymbol{J} + \frac{\partial \boldsymbol{D}}{\partial t}$$

电磁感应定律:

$$\oint_{l} \mathbf{E} \cdot d\mathbf{l} = -\int_{S} \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{S}$$

$$\nabla \times \boldsymbol{E} = -\frac{\partial \boldsymbol{B}}{\partial t}$$

磁通连续性:

$$\oint_{S} \mathbf{B} \cdot d\mathbf{S} = 0$$

$$\nabla \cdot \boldsymbol{B} = 0$$

高斯定理:

$$\oint_{S} \mathbf{D} \cdot d\mathbf{S} = \int_{V} \rho dV$$

$$\nabla \cdot \boldsymbol{D} = \rho$$

本构关系:

$$J = \gamma E$$

$$D = \varepsilon E$$

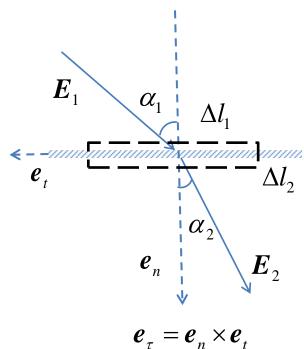
$$B = \mu H$$

参数与频率也有关系



4.1.2 动态电磁场的边界条件

(1) 不同媒质分界面



同理由
$$\oint_l \boldsymbol{H} \cdot d\boldsymbol{l} = \int_S \left(\boldsymbol{J} + \frac{\partial \boldsymbol{D}}{\partial t} \right) \cdot d\boldsymbol{S}$$
 \Longrightarrow $H_{1t} - H_{2t} = K$

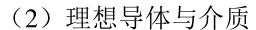
对于**B**, **D**的边界条件,同理可得 $B_{1n} = B_{2n}$ $D_{2n} - D_{1n} = \sigma$



4.1.2 动态电磁场的边界条件

矢量形式:

$$e_n \times (\boldsymbol{H}_2 - \boldsymbol{H}_1) = \boldsymbol{K}$$
 $e_n \times (\boldsymbol{E}_2 - \boldsymbol{E}_1) = 0$
 $e_n \cdot (\boldsymbol{B}_2 - \boldsymbol{B}_1) = 0$
 $e_n \cdot (\boldsymbol{D}_2 - \boldsymbol{D}_1) = \sigma$



理想导体内: $\gamma_1 \rightarrow \infty$ $J_{c1} = C < \infty$ \Longrightarrow $E_1 = 0$

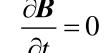
$$J_{c1} = C < \infty$$



$$\boldsymbol{E}_{\scriptscriptstyle 1} = 0$$

曲
$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$
 \Rightarrow $\frac{\partial \mathbf{B}}{\partial t} = 0$ \Rightarrow $\mathbf{B} = 0$ 或者 $\mathbf{B} = \mathbf{C}$ 静态场不考虑







 $\boldsymbol{e}_{\tau} = \boldsymbol{e}_{n} \times \boldsymbol{e}_{t}$



4.1.2 动态电磁场的边界条件

曲此可得
$$\boldsymbol{B}_1 = \boldsymbol{H}_1 = 0$$
 $\boldsymbol{D}_1 = \varepsilon \boldsymbol{E}_1 = 0$

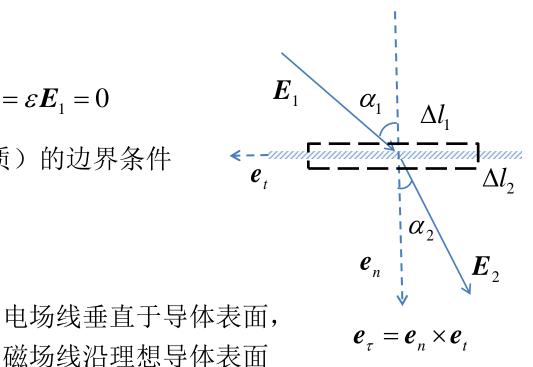
结合一般条件下(两种不同介质)的边界条件适量形式,

$$\mathbf{e}_{n} \times \mathbf{H}_{2} = \mathbf{K}$$

$$\mathbf{e}_{n} \times \mathbf{E}_{2} = \mathbf{e}_{n} \times \mathbf{E}_{1} = 0$$

$$\mathbf{e}_{n} \cdot \mathbf{B}_{2} = \mathbf{e}_{n} \cdot \mathbf{B}_{1} = 0$$

 $e_n \cdot D_2 = \sigma$





例4-1: 无限大理想导体平板间的无源自由空间中,动态电磁场的磁场

强度为

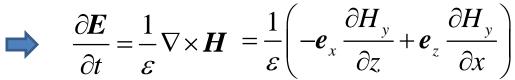
$$\boldsymbol{H} = \boldsymbol{e}_{y} H_{0} \cos \left(\frac{\pi}{d} z \right) \cos \left(\omega t - \beta x \right)$$

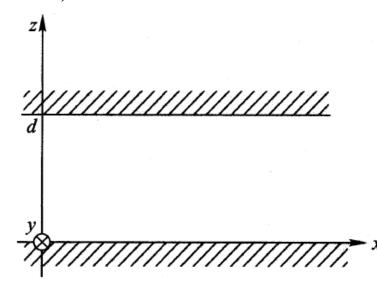
求: (1) 板间时变的电场强度 E:

(2) 两导体表面上时变的面电流密度 K和电荷面密度 σ 。

解(1):

1):
由无源空间以及
$$\nabla \times \boldsymbol{H} = \boldsymbol{J} + \frac{\partial \boldsymbol{D}}{\partial t}$$



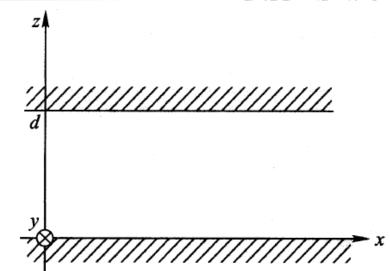




$$\Rightarrow \mathbf{E} = \frac{1}{\varepsilon} \int \left(-\mathbf{e}_x \frac{\partial H_y}{\partial z} + \mathbf{e}_z \frac{\partial H_y}{\partial x} \right) dt$$

$$= \frac{H_0}{\omega \varepsilon} \left[\frac{\pi}{d} \sin \left(\frac{\pi}{d} z \right) \sin \left(\omega t - \beta x \right) \mathbf{e}_x \right]$$

$$-\beta \cos \left(\frac{\pi}{d} z \right) \cos \left(\omega t - \beta x \right) \mathbf{e}_z$$



(2)

两个导体表面,即导体真空交界面,分别讨论。当z=0时

交界面的法向: $\mathbf{e}_n = \mathbf{e}_z$

由理想导体与介质交界面连续性条件, $e_n \times H_2 = K$,可得

$$\boldsymbol{K}' = \boldsymbol{e}_n \times \boldsymbol{H}_2 = \left(\boldsymbol{e}_z \times \boldsymbol{e}_y\right) H_0 \cos\left(\frac{\pi}{d}z\right) \cos\left(\omega t - \beta x\right) \bigg|_{z=0} = -\boldsymbol{e}_x H_0 \cos\left(\omega t - \beta x\right)$$



$$\sigma' = \mathbf{e}_{n} \cdot \mathbf{D}_{2} = \mathbf{e}_{n} \cdot (\varepsilon \mathbf{E}_{2})$$

$$= \mathbf{e}_{z} \cdot \varepsilon \frac{H_{0}}{\omega \varepsilon} \left[\frac{\pi}{d} \sin \left(\frac{\pi}{d} z \right) \sin (\omega t - \beta x) \mathbf{e}_{x} \right]$$

$$-\beta \cos \left(\frac{\pi}{d} z \right) \cos (\omega t - \beta x) \mathbf{e}_{z}$$

$$= -\frac{\varepsilon H_{0}}{\omega \varepsilon} \beta \cos \left(\frac{\pi}{d} z \right) \cos (\omega t - \beta x) = -\frac{\beta H_{0}}{\omega} \cos (\omega t - \beta x)$$

当z=d时 交界面的法向: $e_n = -e_z$

$$\mathbf{K''} = \mathbf{e}_n \times \mathbf{H}_2 = -\mathbf{e}_x \mathbf{H}_0 \cos(\omega t - \beta x) \qquad \sigma'' = \mathbf{e}_n \cdot \mathbf{D}_2 = -\frac{\beta \mathbf{H}_0}{\omega} \cos(\omega t - \beta x)$$



- 4.2 时谐电磁场
- 4.2.1 时谐场的复数表示

背景: 工程中,场源及其所产生的电场、磁场都随时间作正弦变化, 非正弦变化也可以分解为基波及高次谐波分量的叠加。

时谐电磁场: 随时间作正弦变化的时变电磁场

瞬时矢量:
$$E(r,t) = e_x E_{xm}(r) \left[\cos \omega t + \phi_x(r)\right] + e_y E_{ym}(r) \left[\cos \omega t + \phi_y(r)\right] + e_z E_{zm}(r) \left[\cos \omega t + \phi_z(r)\right]$$
 (1)

$$E_{xm}(\mathbf{r})$$
 振幅 $\phi_{x}(\mathbf{r})$ 初相位

采用正弦量的相量表示法,上式可以表示为如下复矢量(相量):



4.2.1 时谐场的复数表示

$$\dot{\boldsymbol{E}}_{m}(\boldsymbol{r}) = \boldsymbol{e}_{x} \dot{\boldsymbol{E}}_{xm}(\boldsymbol{r}) + \boldsymbol{e}_{y} \dot{\boldsymbol{E}}_{ym}(\boldsymbol{r}) + \boldsymbol{e}_{y} \dot{\boldsymbol{E}}_{ym}(\boldsymbol{r})$$
(2)

其中
$$\dot{E}_{xm}(\mathbf{r}) = E_{xm}e^{j\phi_x}$$
 $\dot{E}_{ym}(\mathbf{r}) = E_{ym}e^{j\phi_y}$ $\dot{E}_{zm}(\mathbf{r}) = E_{zm}e^{j\phi_z}$

考虑(1)与(2)的关系,

- $(1) \rightarrow (2)$:
 - a. 将(1)式中各方向的分量加上虚部,

$$E'(r,t) = e_x E_{xm}(r) \{\cos \omega t + \phi_x(r) + j [\sin \omega t + \phi_x(r)] \}$$
$$+ e_y E_{ym}(r) \{\cos \omega t + \phi_y(r) + j [\sin \omega t + \phi_y(r)] \} + \dots$$



4.2.1 时谐场的复数表示

$$\boldsymbol{E}_{m}'(\boldsymbol{r},t) = \boldsymbol{e}_{x} E_{xm}(\boldsymbol{r}) e^{j\omega t} e^{j\phi_{x}} + \boldsymbol{e}_{y} E_{ym}(\boldsymbol{r}) e^{j\omega t} e^{j\phi_{y}} + \boldsymbol{e}_{z} E_{zm}(\boldsymbol{r}) e^{j\omega t} e^{j\phi_{z}}$$

b. 去掉与时间相关的指数项,记作,

$$\dot{\boldsymbol{E}}_{m}(\boldsymbol{r}) = \boldsymbol{e}_{x} E_{xm}(\boldsymbol{r}) e^{j\phi_{x}} + \boldsymbol{e}_{y} E_{ym}(\boldsymbol{r}) e^{j\phi_{y}} + \boldsymbol{e}_{z} E_{zm}(\boldsymbol{r}) e^{j\phi_{z}}$$

$$= \boldsymbol{e}_{x} \dot{\boldsymbol{E}}_{xm}(\boldsymbol{r}) + \boldsymbol{e}_{y} \dot{\boldsymbol{E}}_{ym}(\boldsymbol{r}) + \boldsymbol{e}_{z} \dot{\boldsymbol{E}}_{zm}(\boldsymbol{r})$$

 $(2) \rightarrow (1)$:

$$\mathbf{E}_{m}(\mathbf{r},t) = \operatorname{Re}\left[\dot{\mathbf{E}}_{m}(\mathbf{r})e^{j\omega t}\right] = \operatorname{Re}\left[\sqrt{2}\dot{\mathbf{E}}(\mathbf{r})e^{j\omega t}\right]$$

基于峰值的表示 基于有效值的表示



4.2.1 时谐场的复数表示

例4-2: 写出下列与时谐电磁场对应的复矢量(有效值)或瞬时矢量

(1)
$$\dot{H}_x = jH_0 \sin \theta \cos(\beta x \cos \theta) e^{-j\beta z \sin \theta}$$

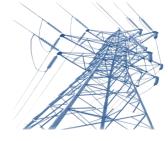
(2)
$$\mathbf{E} = \mathbf{e}_{y} E_{ym} \cos(\omega t - \beta x + \alpha) + \mathbf{e}_{z} E_{zm} \sin(\omega t - \beta x + \alpha)$$

解:

$$(1)H_{x} = \operatorname{Re}\left[\sqrt{2} \dot{H}_{x} e^{j\omega t}\right] = \operatorname{Re}\left[\sqrt{2} jH_{0} \sin\theta \cos(\beta x \cos\theta) e^{j\omega t - j\beta z \sin\theta}\right]$$

$$= \operatorname{Re}\left\{\sqrt{2} jH_{0} \sin\theta \cos(\beta x \cos\theta) \left[\cos(\omega t - \beta z \sin\theta) + j\sin(\omega t - \beta z \sin\theta)\right]\right\}$$

$$= -\sqrt{2}H_{0} \sin\theta \cos(\beta x \cos\theta) \sin(\omega t - \beta z \sin\theta)$$



4.2.1 时谐场的复数表示

(2)
$$E'_{m}(\mathbf{r},t) = \mathbf{e}_{y} E_{ym} \left[\cos(\omega t - \beta x + \alpha) + j \sin(\omega t - \beta x + \alpha) \right]$$

$$+ \mathbf{e}_{z} E_{zm} \left[\cos(\omega t - \beta x + \alpha - \frac{\pi}{2}) + j \sin(\omega t - \beta x + \alpha - \frac{\pi}{2}) \right]$$

$$= \mathbf{e}_{y} E_{ym} e^{j[\omega t + (\alpha - \beta x)]} + \mathbf{e}_{z} E_{zm} e^{j[\omega t + (\alpha - \beta x) - \frac{\pi}{2}]}$$

$$= \mathbf{e}_{y} E_{ym} e^{j[\omega t + (\alpha - \beta x)]} + \mathbf{e}_{z} E_{zm} e^{j[\omega t + (\alpha - \beta x)]} e^{-j\frac{\pi}{2}}$$

$$\overset{\cdot}{\Longrightarrow} \dot{E}(r,t) = e_y \frac{E_{ym}}{\sqrt{2}} e^{-j(\beta x - \alpha)} - e_z j \frac{E_{zm}}{\sqrt{2}} e^{-j(\beta x - \alpha)}$$

$$\dot{\boldsymbol{E}}(\boldsymbol{r},t) = \boldsymbol{e}_{y} E_{y} e^{-j(\beta x - \alpha)} - \boldsymbol{e}_{z} j E_{z} e^{-j(\beta x - \alpha)}$$



u, i

4.2.2 有损媒质的复数表示

复介电常数:

右图所示为理想无损电容器(板间为真空),设其电容为 C_0 , 当其两极板上加有角频率为 ω 的正弦电压u时,有

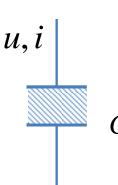
$$\dot{I} = j\omega C_0 \dot{U}$$
 $\left(i = C_0 \frac{\partial u}{\partial t}\right)$



若将极板间充满相对介电常数为 ε_r 的电介质,则电容器电容 $C = \varepsilon_r C_0$

$$\dot{I} = j\omega C \dot{U} = j\omega \varepsilon_r C_0 \dot{U}$$
 **

理论上, ※式中电压、电流应相差90度, 但测量发现小于 90度,导致该问题的应该是相对介电常数。



4.2.2 有损媒质的复数表示

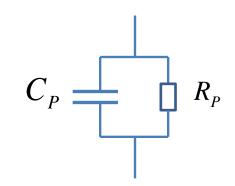
$$\dot{I} = \omega \varepsilon_r'' C_0 \dot{U} + j\omega \varepsilon_r' C_0 \dot{U}
= j\omega \left(\varepsilon_r' - j\varepsilon_r''\right) C_0 \dot{U} \qquad \text{\times \times}$$

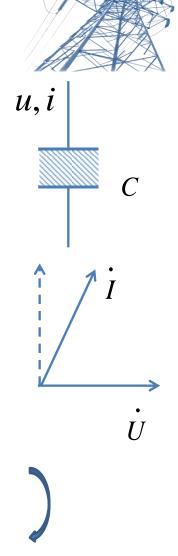
将※式与※※式比较,可得 $\varepsilon_r = \varepsilon_r' - j\varepsilon_r'' \implies$ 复相对介电常数

$$\varepsilon = \varepsilon_r \varepsilon_0 = \varepsilon' - j \varepsilon''$$
 复介电常数

由以上分析,可得

$$C_P = \varepsilon_r' C_0$$
 $R_P = \frac{1}{\omega \varepsilon_r'' C_0}$





介质有损耗,是极化时产生,但这种损耗不是欧姆损耗,称之为<mark>极化损耗</mark>



4.2.2 有损媒质的复数表示

从场的角度来看,

$$\nabla \times \boldsymbol{H} = \boldsymbol{J}_c + \frac{\partial \boldsymbol{D}}{\partial t}$$

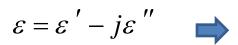
对于时谐场,有
$$\nabla \times \dot{\boldsymbol{H}} = \gamma \boldsymbol{E} + j\omega \varepsilon \boldsymbol{E}$$

$$= j\omega\varepsilon\,\dot{\boldsymbol{E}} + j\omega\left(-j\frac{\gamma}{\omega}\right)\dot{\boldsymbol{E}}$$

$$= j\omega \left(\varepsilon - j\frac{\gamma}{\omega}\right)\dot{E}$$

$$= j\omega \left[\varepsilon' - j\left(\varepsilon'' + \frac{\gamma}{\omega}\right) \right] \dot{\boldsymbol{E}} = j\omega\varepsilon_e \dot{\boldsymbol{E}}$$

$$\varepsilon_e = \varepsilon' - j \left(\varepsilon'' + \frac{\gamma}{\omega} \right)$$
 等效复介电常数





4.2.2 有损媒质的复数表示

等效复介电常数的虚部与损耗相关,工程中引入介质损耗角表征损耗 的特性,

$$\tan \delta = \frac{\varepsilon'' + \frac{\gamma}{\omega}}{\varepsilon'}$$
 表征电介质特性的重要参数

工程上希望该值越小越好,即意味着绝缘特性越好。

(1) 微波炉加热面食,菜,肉: $\tan \delta = 0.073$

聚苯乙烯泡沫: $\tan \delta = 3 \times 10^{-5}$

(2) 导电媒质:
$$\varepsilon'' = 0$$
 $\tan \delta = \frac{\gamma}{\varepsilon' \omega} = \frac{\gamma E}{\varepsilon' \omega E} = \frac{|\boldsymbol{J}|}{|j\omega \boldsymbol{D}|}$

显然导体中传导电流远大于位移电流 \implies tan $\delta \gg 1$







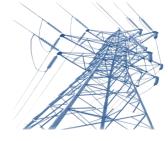
4.2.2 有损媒质的复数表示

工频50赫兹条件下, $\tan \delta = 2.085 \times 10^{16}$ 铜

$$\tan \delta = 1.366 \times 10^{16}$$
 铝

类似地, 当媒质处于磁场中时, 有

$$\mu = \mu' - j\mu''$$



4.3 电磁场能量 坡印廷定理

回顾: 静态场
$$W_e = \frac{1}{2} \int_V \mathbf{D} \cdot \mathbf{E} dV$$
 $W_m = \frac{1}{2} \int_V \mathbf{B} \cdot \mathbf{H} dV$ $P = \int_V \mathbf{E} \cdot \mathbf{J} dV$

思考: 动态场 能量变化 能量流动 (转化) 能量守恒

单位体积内,动态电磁场在导电媒质中消耗的电功率为:

$$E \cdot J = E \cdot \left(\nabla \times H - \frac{\partial D}{\partial t} \right)$$

曲散度定理
$$-\oint_{S} (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{S} = \frac{d}{dt} \int_{V} (w_{e} + w_{m}) dV + \int_{V} (\mathbf{E} \cdot \mathbf{J}) dV$$

$$=\frac{d}{dt}(W_e + W_m) + P$$

坡印廷定理积分形式





4.3 电磁场能量 坡印廷定理

$$-\oint_{S} (\boldsymbol{E} \times \boldsymbol{H}) \cdot d\boldsymbol{S} = \frac{d}{dt} \int_{V} (w_{e} + w_{m}) dV + \int_{V} (\boldsymbol{E} \cdot \boldsymbol{J}) dV$$

 $S_P = E \times H$ 坡印廷矢量: 单位时间内穿过单位面积的电磁能量

坡印廷定理:单位时间内穿过闭合面S流入体积V的电磁能量,等于该体积内电磁能量W的增加率和电磁能量的消耗率。

对于时谐场,有

$$-\oint_{S} \left(\dot{\boldsymbol{E}} \times \dot{\boldsymbol{H}}^{*} \right) \cdot d\boldsymbol{S} = \int_{V} \left[\dot{\boldsymbol{E}} \cdot \dot{\boldsymbol{J}}^{*} + j\omega \left(\dot{\boldsymbol{B}} \cdot \dot{\boldsymbol{H}}^{*} - \dot{\boldsymbol{E}} \cdot \dot{\boldsymbol{D}}^{*} \right) \right] dV$$

对于有损媒质,上式可进一步写为

$$-\oint_{S} \left(\dot{E} \times \dot{H}^{*} \right) \cdot dS = \int_{V} \left[\gamma E^{2} + \omega \varepsilon'' E^{2} + \omega \mu'' H^{2} + j\omega \left(\mu' H^{2} - \varepsilon' E^{2} \right) \right] dV$$



4.3 电磁场能量 坡印廷定理

$$-\oint_{S} \left(\dot{\boldsymbol{E}} \times \dot{\boldsymbol{H}}^{*} \right) \cdot d\boldsymbol{S} = \int_{V} \left[\gamma E^{2} + \omega \varepsilon'' E^{2} + \omega \mu'' H^{2} + j\omega \left(\mu' H^{2} - \varepsilon' E^{2} \right) \right] dV$$

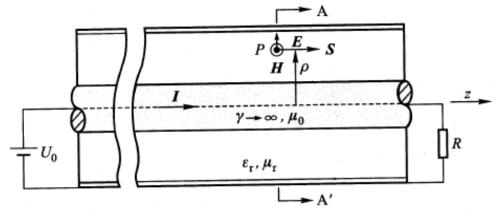
 $\tilde{S}_{P} = E \times H^{*}$ 复坡印廷矢量:实部对应于媒质吸收的有功功率,等于电磁功率面密度矢量的平均值,即下式

$$S_{av} = \frac{1}{T} \int_0^T S(\mathbf{r}, t) dt = \text{Re} \left[\dot{\mathbf{E}} \times \dot{\mathbf{H}}^* \right]$$



4.3 电磁场能量 坡印廷定理

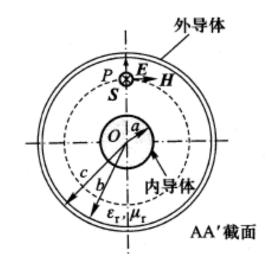
例4-3: 直流电压源 U_0 经下图所示同轴电缆,向负载R供电,求同轴电缆传输功率 P_R ,内导体半径a,外导体内外半径分别为b、c。基于坡印廷定理分析其能量传输过程。



分析: 由动态下的坡印廷矢量定理,

$$-\oint_{S} (\boldsymbol{E} \times \boldsymbol{H}) \cdot d\boldsymbol{S} = \frac{d}{dt} (W_{e} + W_{m}) + \int_{V} (\boldsymbol{E} \cdot \boldsymbol{J}) dV$$

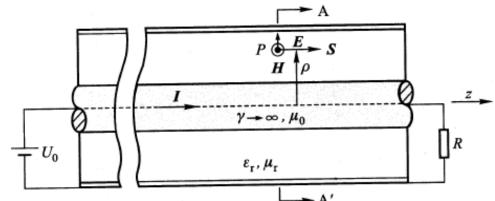






解:

内导体电位为 U_0 ,外导体电位为零,电流 $I=U_0/R$ 。

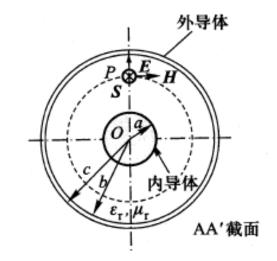


<u>电场:</u>

导体:

对于内导体 $(0 \le \rho < a)$ 和外导体 $(b < \rho \le c)$,可 认为 $\gamma \to \infty$,而 \mathbf{J}_c 有限,故 $\mathbf{E} = 0$ 。

媒质:
$$E = \frac{U_0}{\rho \ln \frac{b}{a}} e_{\rho} \quad (a \le \rho \le b)$$





磁场:

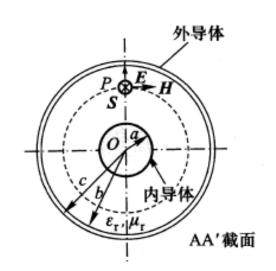
内导体:

$$\boldsymbol{H} = \frac{I\rho}{2\pi a^2} \boldsymbol{e}_{\phi} = \frac{U_0 \rho}{R2\pi a^2} \boldsymbol{e}_{\phi} \quad (0 \le \rho < a)$$

媒质:
$$H = \frac{U_0}{R2\pi\rho} e_{\phi} \quad (a \le \rho \le b)$$

外导体:

$$\boldsymbol{H} = \frac{U_0}{R2\pi\rho} \left(1 - \frac{\rho^2 - b^2}{c^2 - b^2} \right) \boldsymbol{e}_{\phi} \quad (b < \rho < c)$$



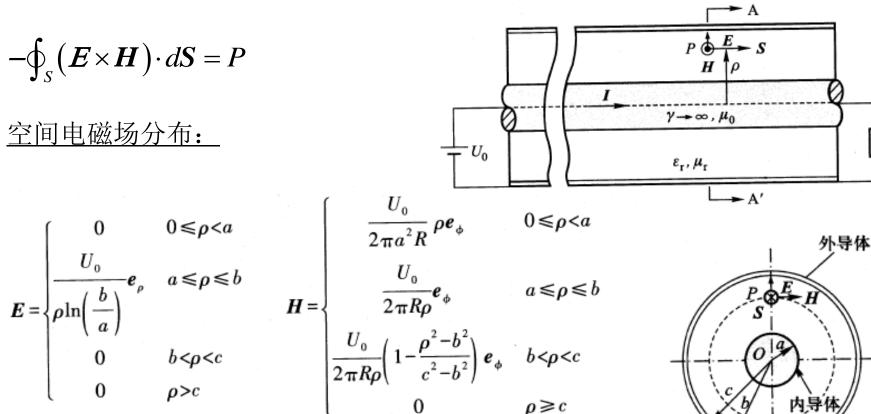


$$-\oint_{S} (\boldsymbol{E} \times \boldsymbol{H}) \cdot d\boldsymbol{S} = P$$

空间电磁场分布:

$$\boldsymbol{E} = \begin{cases} 0 & 0 \leq \rho < a \\ \frac{U_0}{\rho \ln\left(\frac{b}{a}\right)} \boldsymbol{e}_{\rho} & a \leq \rho \leq b \\ 0 & b < \rho < c \\ 0 & \rho > c \end{cases}$$

代入上式,可得



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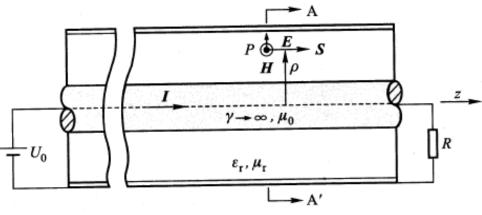
AA'截面



$$S_{P} = E \times H$$

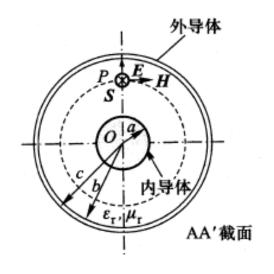
$$= \frac{U_{0}}{\rho \ln \frac{b}{a}} e_{\rho} \times \frac{U_{0}}{R2\pi\rho} e_{\phi}$$

$$= \frac{U_{0}^{2}}{2\pi R \ln \frac{b}{\rho}} \frac{1}{\rho^{2}} e_{z} \quad (a \le \rho \le b)$$



S: 选择半径为 ρ =c的电缆最外层圆柱面

$$-\oint_{S} (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{S} = -\left[\int_{S_{l}} (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{S} + \int_{S_{r}} (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{S} + \int_{S_{r}} (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{S} + \int_{S_{r}} (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{S} \right]$$
$$= -\int_{S_{l}} \mathbf{S}_{P} \cdot d\mathbf{S} - \int_{S_{r}} \mathbf{S}_{P} \cdot d\mathbf{S}$$



$$-\oint_{S} (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{S}$$

$$= -\int_{S_{l}} \mathbf{S}_{P} \cdot d\mathbf{S} - \int_{S_{r}} \mathbf{S}_{P} \cdot d\mathbf{S}$$

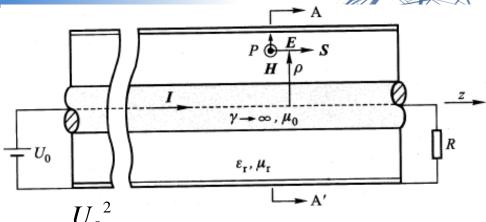
$$-\int_{S} \mathbf{S}_{P} \cdot d\mathbf{S}$$

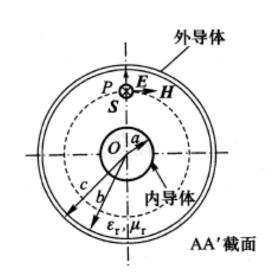
$$= -\int_{a}^{b} \frac{U_0^2}{2\pi R \ln \frac{b}{a}} \frac{1}{\rho^2} \boldsymbol{e}_z \cdot (-\boldsymbol{e}_z) 2\pi \rho d\rho = \frac{U_0^2}{R}$$

$$-\int_{S_r} S_P \cdot dS = -\int_a^b \frac{U_0^2}{2\pi R \ln \frac{b}{r}} \frac{1}{\rho^2} e_z \cdot (e_z) 2\pi \rho d\rho = -\frac{U_0^2}{R}$$

$$\rightarrow$$
 $-\oint_{c}(E \times H) \cdot dS = P = 0$ 电缆中电功率损耗为零

电缆提供给电阻的功率







- 4.4 电磁位
- 4.4.1 电磁位 洛伦兹规范

由无旋场的特性可知 $\mathbf{E} = -\nabla \varphi - \frac{\partial \mathbf{A}}{\partial t}$ (2)

即可基于位函数组 $A-\varphi$ 描述动态电磁场,将(1)(2)及媒质构成方程代入如下麦克斯韦方程,



4.4.1 电磁位 洛伦兹规范

思考:

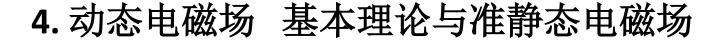
- (1) 要求解A,需要确保A的唯一性,即要规定A的散度和旋度;
- (2) 要求解A、 φ ,需要对方程进行解耦;

只有令:
$$\nabla \cdot \mathbf{A} = -\mu \varepsilon \frac{\partial \varphi}{\partial t}$$
 洛伦兹规范

$$\nabla^{2} \mathbf{A} - \mu \varepsilon \frac{\partial^{2} \mathbf{A}}{\partial t^{2}} = -\mu \mathbf{J}$$
 (5) 电磁位非齐次波动方程
$$\nabla^{2} \varphi - \mu \varepsilon \frac{\partial^{2} \varphi}{\partial t^{2}} = -\frac{\rho}{\varepsilon}$$
 (6)

$$abla^2 \varphi - \mu \varepsilon \frac{\partial^2 \varphi}{\partial t^2} = -\frac{\rho}{\varepsilon}$$
 (6)







4.4.2 非齐次波动方程

对于时谐场,非齐次波动方程的复数形式为



4.4.3 电磁位积分解

令
$$v = \frac{1}{\sqrt{\mu \varepsilon}}$$
 称之为电磁波在媒质空间的传播速度

自由空间中:
$$v = \frac{1}{\sqrt{\mu_0 \varepsilon_0}} \approx 3.0 \times 10^8 \ (m/s)$$

将波速表达式代入前面(6)式,有 $\nabla^2 \varphi - \frac{1}{v^2} \frac{\partial^2 \varphi}{\partial t^2} = -\frac{\rho}{\varepsilon}$

分析: 上式为线性方程, 且 $\varphi = \varphi(\mathbf{r}, t)$, 与 ρ 有关。

求解思路: 可以先求一个处于坐标原点的时变元电荷*dq=pdV*在空间产生的动态标量电位,再基于叠加原理,推导出任意分布的时变体电荷对于的空间动态标量位。



4.4.3 电磁位积分解

假设坐标原点处有一时变元电荷dq,场分布具有对称性,即

$$\varphi(\mathbf{r},t) = \varphi(r,t)$$

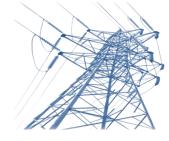
除坐标原点以外,空间中有

$$\nabla^2 \varphi - \frac{1}{v^2} \frac{\partial^2 \varphi}{\partial t^2} = \frac{1}{r} \frac{\partial^2 (r\varphi)}{\partial r^2} - \frac{1}{v^2} \frac{\partial^2 \varphi}{\partial t^2} = 0 \quad 0 < r < \infty \quad 美于r\varphi$$
一维齐次波动方程

通解为:
$$r\varphi(r,t) = f_1\left(t-\frac{r}{v}\right) + f_2\left(t+\frac{r}{v}\right)$$
 位滯后于源 位超前于源

$$\varphi(\mathbf{r},t) = \frac{f_1(t-r/v)}{r}$$
 显然 f_1 与媒质特性、元电荷量 dq 等参数相关。





4.4.3 电磁位积分解

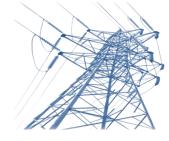
当dq与时间无关时,即为静电场中电位表达式 $d\varphi(r) = \frac{\rho a v}{4\pi r \varepsilon}$ 将其与前式比较, $\varphi(\mathbf{r},t) = \frac{f_1(t-r/v)}{r}$

$$\Rightarrow d\varphi(\mathbf{r},t) = \frac{\rho(t-r/v)}{4\pi r \varepsilon} dV \quad \text{区别应该只在时间延迟效应方面}$$

若dq不在原点,而是位于r'处,则令 R=r-r' R=|r-r'|

$$\Rightarrow d\varphi(\mathbf{r},t) = \frac{\rho\left(\mathbf{r}',t - \frac{|\mathbf{r} - \mathbf{r}'|}{v}\right)}{4\pi\varepsilon|\mathbf{r} - \mathbf{r}'|}dV = \frac{\rho\left(\mathbf{r}',t - \frac{R}{v}\right)}{4\pi\varepsilon R}dV$$

由此可知,场域 V' 中,任意分布的体电荷 $\rho(\mathbf{r}',t)$,在场点 \mathbf{r} 处产生的标量位可由上式积分求得



4.4.3 电磁位积分解

$$\varphi(\mathbf{r},t) = \frac{1}{4\pi\varepsilon} \int_{V} \frac{\rho\left(\mathbf{r}',t-\frac{R}{V}\right)}{R} dV \qquad A(\mathbf{r},t) = \frac{\mu}{4\pi} \int_{V} \frac{J\left(\mathbf{r}',t-\frac{R}{V}\right)}{R} dV'$$

动态标量位、动态矢量位(除时间上延迟以外,与静态规律一致)

对于时谐场,为简化分析,时间延迟项仍以坐标原点为基点,记作t-r/v,则有

$$\omega\left(t - \frac{r}{v}\right) = \omega t - \frac{\omega}{v}r = \omega t - \left(\omega\sqrt{\varepsilon\mu}\right)r = \omega t - kr$$

➡ 时间上的延迟,对应于相位上的滞后,因此可知复数形式的电磁位



4.4.3 电磁位积分解

$$\dot{\varphi}(\mathbf{r}) = \frac{1}{4\pi\varepsilon} \int_{V} \frac{\dot{\rho}(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} e^{-jk|\mathbf{r} - \mathbf{r}'|} dV = \frac{1}{4\pi\varepsilon} \int_{V} \frac{\dot{\rho}(\mathbf{r}')}{R} e^{-jkR} dV$$

$$\dot{\boldsymbol{A}}(\boldsymbol{r}) = \frac{\mu}{4\pi} \int_{V} \frac{\dot{\boldsymbol{J}}(\boldsymbol{r}')}{|\boldsymbol{r} - \boldsymbol{r}'|} e^{-jk|\boldsymbol{r} - \boldsymbol{r}'|} dV' = \frac{\mu}{4\pi} \int_{V} \frac{\dot{\boldsymbol{J}}(\boldsymbol{r}')}{R} e^{-jkR} dV'$$

$$v = \frac{\omega}{k} = \frac{1}{\sqrt{\mu\varepsilon}} \qquad k = \omega\sqrt{\mu\varepsilon} \qquad \lambda = \frac{2\pi}{k}$$

非齐次亥姆霍兹方程的解



- 4.5 准静态电磁场
- 4.5.1 电准静态场与磁准静态场
 - (1) 电准静态场

$$\nabla \times \boldsymbol{E} = -\frac{\partial \boldsymbol{B}}{\partial t}$$

$$\nabla \cdot \boldsymbol{D} = \rho$$

对于低频电磁场,感应电场 E_i 远小于库仑电场 E_a ,可以忽略时间导数项, 可见课本中例4-4。

$$\nabla \times \boldsymbol{E} = 0$$

$$\nabla \cdot \boldsymbol{D} = \rho$$

电准静态场(变压器、输电线路等)

$$\Rightarrow$$

$$\nabla \cdot \boldsymbol{B} = 0$$



4.5.1电准静态场与磁准静态场

(2) 磁准静态场

$$\nabla \times \boldsymbol{H} = \boldsymbol{J}_c + \frac{\partial \boldsymbol{D}}{\partial t} \qquad \nabla \cdot \boldsymbol{B} = 0$$

对于低频电磁场,当位移电流 J_D 远小于传导电流 J_c 时,可以忽略时间导数项。

$$ightharpoonup$$
 $\nabla imes \mathbf{H} = \mathbf{J}_c$ $\nabla \cdot \mathbf{B} = 0$ 磁准静态场(电机、变压器)

⇒
$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$
 $\nabla \cdot \mathbf{D} = \rho$ 与磁准静态场共存的电场

例4-4,例4-5一定要好好自学,重要。



4.5.2 导电媒质中的自由电荷驰豫过程

电荷驰豫过程:自由电荷体密度随时间衰减的过程

(1) 均匀导电媒质中的电荷驰豫过程:

$$\oint_{S} \boldsymbol{J}_{c} \cdot d\boldsymbol{S} = -\frac{d}{dt} \int_{V} \rho dV = \int_{V} -\frac{\partial \rho}{\partial t} dV \quad \Longrightarrow \quad \nabla \cdot \boldsymbol{J}_{c} = -\frac{\partial \rho}{\partial t}$$

对于良导体、驰豫时间很小、很快衰减为零、该过程为自由电荷驰豫过程。

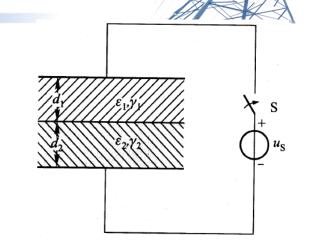
基本理论与准静态电磁场 4. 动态电磁场

4.5.2 导电媒质中的自由电荷驰豫过程

(2) 分块均匀导电媒质分界面处电荷驰豫:

$$\varepsilon_2 E_{2n} - \varepsilon_1 E_{1n} = \sigma$$

$$J_{2n} - J_{1n} = -\frac{\partial \sigma}{\partial t} \quad \longleftarrow \left(\oint_{S} \boldsymbol{J}_{c} \cdot d\boldsymbol{S} = \int_{V} -\frac{\partial \rho}{\partial t} \, dV \right)$$



$$\gamma_2 E_{2n} - \gamma_1 E_{1n} + \frac{\partial}{\partial t} \left(\varepsilon_2 E_{2n} - \varepsilon_1 E_{1n} \right) = 0$$

$$\tau_e = \frac{d_2 \varepsilon_1 + d_1 \varepsilon_2}{d_2 \gamma_1 + d_1 \gamma_2}$$



$$\gamma_{2}E_{2} - \gamma_{1}E_{1} + \frac{\partial}{\partial t}\left(\varepsilon_{2}E_{2} - \varepsilon_{1}E_{1}\right) = 0$$

$$C = \frac{\varepsilon_{2}\gamma_{1} - \varepsilon_{1}\gamma_{2}}{d_{2}\gamma_{1} - d_{1}\gamma_{2}}u_{s}\left(1 - e^{-\frac{t}{\tau_{e}}}\right)$$

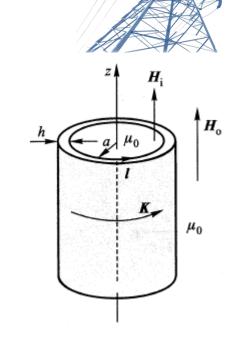
$$E_{1}d_{1} + E_{2}d_{2} = u_{s}$$

$$\sigma = \frac{\varepsilon_2 \gamma_1 - \varepsilon_1 \gamma_2}{d_2 \gamma_1 - d_1 \gamma_2} u_s \left(1 - e^{-\frac{t}{\tau_e}} \right)$$

刚充电时=0,随着时间t增加,面电荷逐渐积累,至电路达到稳态时为常数。

4.5.3 导电媒质中的磁扩散与磁屏蔽

磁扩散:恒定外磁场突然施加在导电媒质中,由于电磁感应,必然在导电媒质中产生感应电流,其去磁效应将使得导电媒质中磁场不会突变。随时间增加,感应电流逐渐衰减为零。最终去磁效应消失,形成恒定磁场。该过程称之为磁扩散(驰豫)过程。



(1) 轴向磁场向导体内的磁扩散

圆柱形导体壳受轴向外磁场激励,为 $H_{o}(t)$ 。令t=0时,突然建立恒定磁场 H_{o}

$$e_n$$
: 导体(1)指向空气(2) $e_n = e_\rho$

4.5.3 导电媒质中的磁扩散与磁屏蔽

由于: $K = hJ = h\gamma E$ 导体壳很薄 $\rightarrow E$, J, K均匀

由电磁感应定律, 在导体壳中取回路

$$\oint_{l} \mathbf{E} \cdot d\mathbf{l} = -\int_{S} \frac{\partial \mathbf{B}_{i}}{\partial t} \cdot d\mathbf{S} \quad \Longrightarrow \quad \oint_{l} \frac{K}{h\gamma} dl = -\int_{S} \frac{\partial \mathbf{B}_{i}}{\partial t} \cdot d\mathbf{S}$$

$$\frac{1}{h\gamma} (H_i - H_o) 2\pi a = -\mu_0 \pi a^2 \frac{dH_i}{dt}$$

$$\frac{dH_i}{dt} + \frac{2}{ah\mu_0 \gamma} H_i = \frac{2H_o}{ah\mu_0 \gamma} \qquad \Longrightarrow \qquad K = -H_o e^{-\frac{t}{\tau_m}} \qquad \tau_m = \frac{1}{2} ah\mu_0 \gamma$$

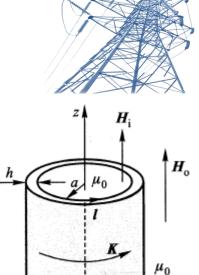
$$H_i = H_o \left(1 - e^{-t/\tau_m} \right) \qquad K: -H_o \to 0$$



$$K = -H_o e^{-}$$

$$K:-H_o\to 0$$

$$H_i: 0 \to H_o$$

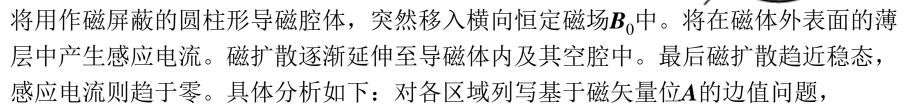


磁扩散(驰豫)时间

$$\tau_m = \frac{1}{2}ah\mu_0\gamma$$

4.5.3 导电媒质中的磁扩散与磁屏蔽

- (2) 横向磁场向导体壳内的磁扩散(**自学**)
- (3) 磁屏蔽



$$A_{z1} = B_0 \rho \sin \phi + \frac{F_1}{\rho} \sin \phi \ (\rho \ge b)$$

$$A_{z2} = F_2 \rho \sin \phi + \frac{F_3}{\rho} \sin \phi \ (b < \rho \le a)$$

$$A_{z3} = F_4 \rho \sin \phi \quad (0 < \rho \le a)$$

结合分界面边界条件,由计算推导可得到各个系数。



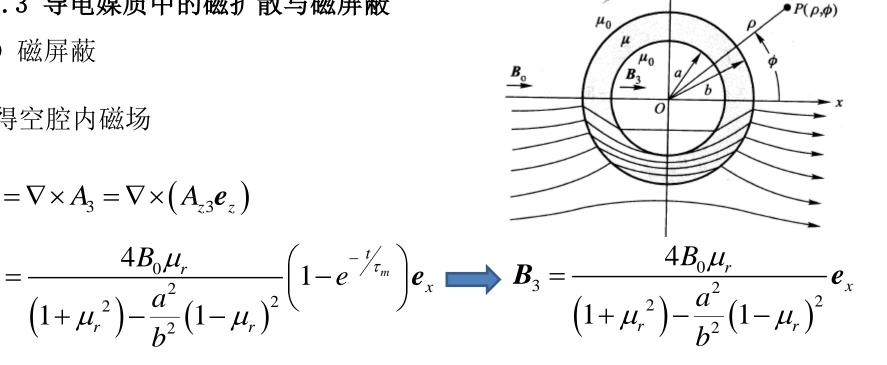


(3) 磁屏蔽

可得空腔内磁场

$$\boldsymbol{B}_{3} = \nabla \times A_{3} = \nabla \times \left(A_{z3}\boldsymbol{e}_{z}\right)$$

$$= \frac{4B_{0}\mu_{r}}{\left(1 - e^{-\frac{t}{\tau_{n}}}\right)}$$



当
$$\mu_r \gg 1$$
 $B_3 = \frac{4B_0}{\mu_r \left(1 - a^2/b^2\right)} e_x$ 导磁腔体具有明显的磁屏蔽作用



4.5.4 集肤效应 涡流

(1) 集肤效应:导电媒质中通以正弦电流后,变化磁场 在导电媒质中产生于磁场交链的感应电磁场和感应电流, 称之为涡流。涡流使导电媒质中场量(电流密度)趋于表 面分布,且沿着纵深方向衰减,称之为集肤效应。

磁准静态场

$$\nabla \times \boldsymbol{H} = \gamma \boldsymbol{E}$$

$$\nabla \cdot \boldsymbol{B} = 0$$

$$\nabla \times \boldsymbol{H} = \gamma \boldsymbol{E} \qquad \nabla \times \boldsymbol{E} = -\frac{\partial \boldsymbol{B}}{\partial t}$$

$$\nabla \cdot \boldsymbol{D} = 0$$



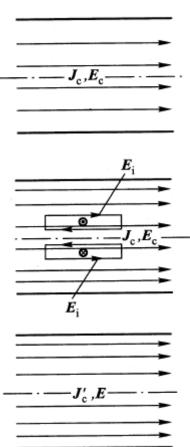
$$\nabla^2 \mathbf{E} = \mu \gamma \frac{\partial \mathbf{E}}{\partial t} \qquad \nabla^2 \mathbf{H} = \mu \gamma \frac{\partial \mathbf{H}}{\partial t}$$

$$\nabla^2 \boldsymbol{H} = \mu \gamma \frac{\partial \boldsymbol{H}}{\partial t}$$



$$\nabla^2 \dot{\mathbf{E}} = i\omega\mu\gamma\dot{\mathbf{E}} = p^2\dot{\mathbf{E}}$$

$$\nabla^2 \dot{\mathbf{E}} = j\omega\mu\gamma \dot{\mathbf{E}} = p^2 \dot{\mathbf{E}} \qquad \nabla^2 \dot{\mathbf{H}} = j\omega\mu\gamma \dot{\mathbf{H}} = p^2 \dot{\mathbf{H}}$$





4.5.4 集肤效应 涡流

$$p = \sqrt{j\mu\omega\gamma} = \sqrt{\frac{\mu\omega\gamma}{2}} (1+j) = \frac{1}{d} (1+j)$$

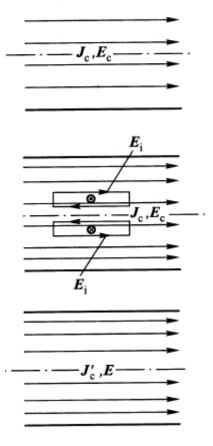
对于上述时谐场方程,假定有半无限大平面导体(x>0),电 流沿y方向流动,则此一维场有,

$$\dot{E} = \dot{E}_y(x)e_y$$
 代入前式可解

 $E_v = Ae^{-px} + Be^{px}$ 当x趋于无穷时,电场为有限值,故B=0

设在
$$x=0$$
处, $E_y = E_y(0) = A$ 则有

$$\dot{E}_{y} = Ae^{-px} = \dot{E}_{y}(0)e^{-\frac{1}{d}(1+j)x} = \dot{E}_{y}(0)e^{-\frac{x}{d}}e^{-j\frac{x}{d}}$$





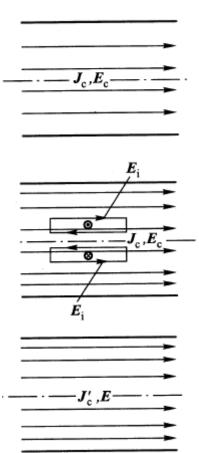
4.5.4 集肤效应 涡流

即距离表面x=d处,场强值相比x=0处,减小e倍。

则距离d称之为该导体的集肤深度,即为

$$d = \sqrt{\frac{2}{\mu\omega\gamma}}$$

频率/Hz	铝/mm	铜/mm	碳钢/mm
50	11.546	9.346	0.919
10 ³	2.582	2.090	0.205
10 ⁶	0.082	0.066	0.006



4.5.4 集肤效应 涡流

(2) 铁心叠片中的涡流

由于
$$h \gg a$$
, $l \gg a$ **i** $B = B_z(x)e_z$ 即涡流分布位于 xoy 平面

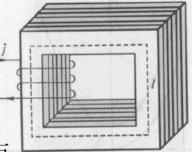
对于时谐磁场,应满足以下方程

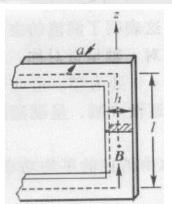
$$\frac{d^2 \dot{B}_z(x)}{dx^2} = j\omega\mu\gamma \dot{B}_z = p^2 \dot{B}_z$$

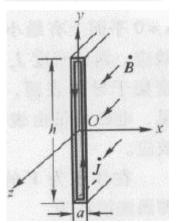
$$\Rightarrow B_z = B_0 \cosh(px)$$
 $B_0: x=0$ 处的磁感应强度

进一步可得
$$\dot{E}_y = -\frac{B_0 p}{\mu \gamma} \sinh(px) = \dot{E}_{y0} \sinh(px)$$

$$\dot{J}_y = -\frac{B_0 p}{\mu} \sinh(px) = \dot{J}_{y0} \sinh(px)$$







EMF&EMC



4.5.4 集肤效应 涡流

$$\begin{vmatrix} \dot{B}_z \end{vmatrix} = B_z = \begin{vmatrix} \dot{B}_0 \end{vmatrix} \sqrt{\frac{1}{2}} \left[\cosh(2Kx) + \cos(2Kx) \right]$$

$$\left| \dot{\boldsymbol{J}}_{z} \right| = \boldsymbol{J}_{z} = \left| \dot{\boldsymbol{J}}_{y0} \right| \sqrt{\frac{1}{2} \left[\cosh(2Kx) - \cos(2Kx) \right]}$$

进一步可得
$$K = \sqrt{\frac{\mu\omega\gamma}{2}}$$

$$P = \int_{V} \frac{J_{y}^{2}}{\gamma} dV = \frac{1}{12} \gamma \omega^{2} a^{2} V B_{zav}^{2}$$

 B_{rav} [-a/2, a/2]区间有效值的平均值

