

Radiation damage calculation in PHITS and benchmarking experiment for cryogenic-sample high-energy proton irradiation

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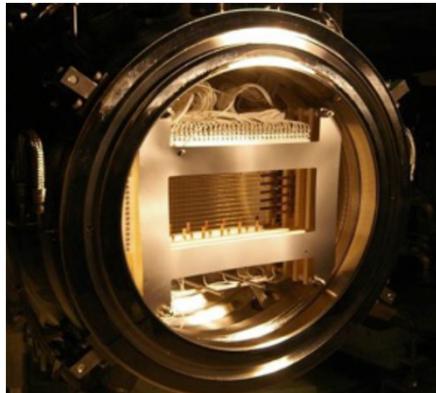
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2. Radiation damage model in PHITS
3. Benchmarking experiments of displacement cross section
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Introduction

Prediction of usable lifetime of materials under high-energy ($E>100$ MeV) particle irradiation is essential for the accelerator design.



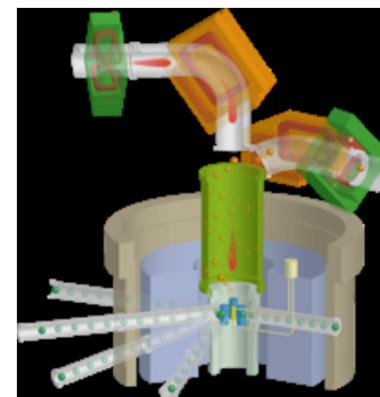
Beam windows in J-PARC MLF (Al alloy)



Beam window in neutrino facility (Ti alloy)



CERN LHC superconducting magnet (Nb alloy)



2nd target in J-PARC MLF (W)

Displacement per atom (DPA) value is used as a damage-based exposure unit.

Microscopic effects on material

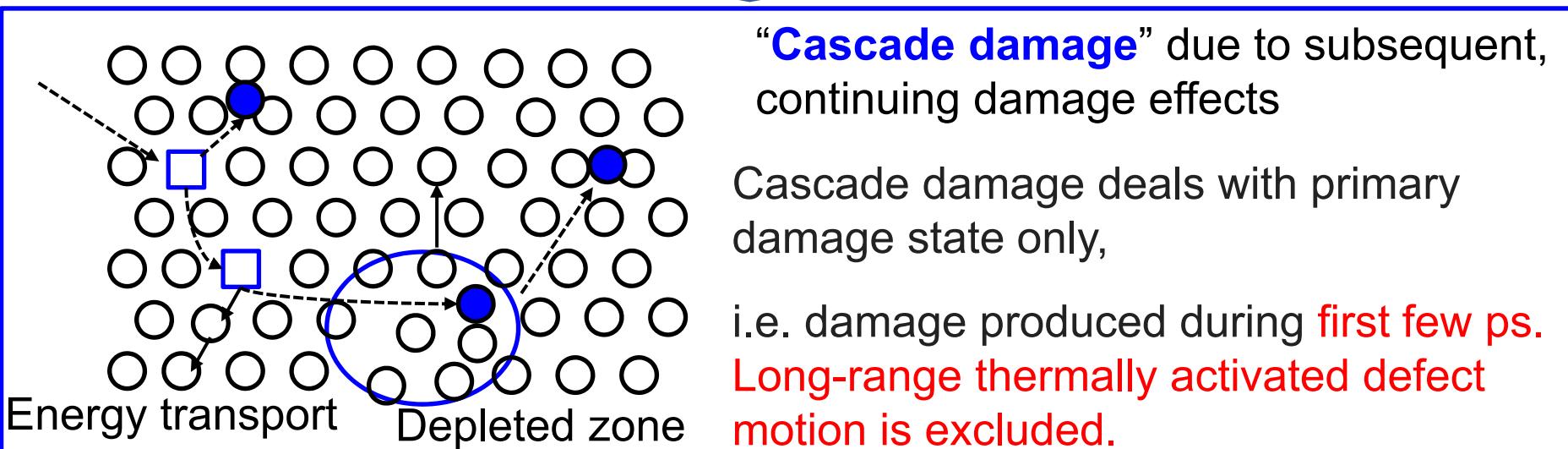
DPA: average number of displaced atoms per atom of a material

$$\text{DPA} = \sigma_d \phi$$

σ_d : displacement cross-section (m^2)

ϕ : irradiation fluence (particles/ m^2)

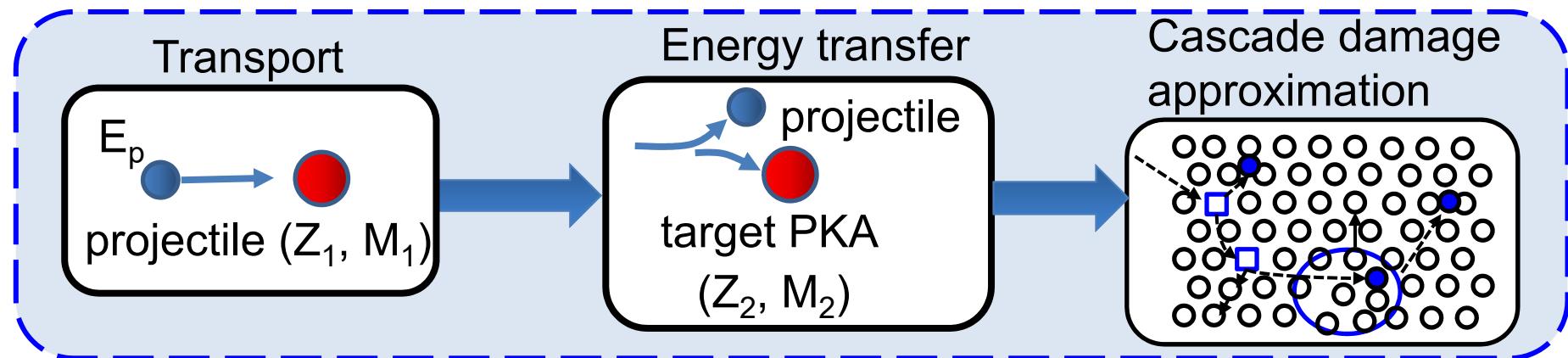
i.e. 1 dpa mean each atom has been displaced from its lattice site an average of 1 times.



Radiation damage model

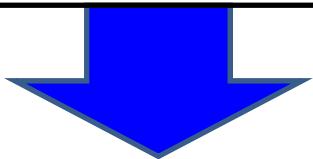
SRIM (Transport of Ions in Material): Major code for radiation damage

J.F. Ziegler, et al, see www.srim.org



no treatment of nuclear reaction in high-energy region

no production of PKAs created by the secondary particles



extend to high-energy region

Radiation damage model in advanced Monte Carlo particle transport codes.
e.g. PHITS, MARS, FLUKA, MCNP

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Overview of PHITS

Particle and Heavy Ion Transport code System

Development

JAEA (Japan), RIST (Japan), KEK (Japan), Technische Universitat Wien(Austria)
RIKEN (Japan), CEA (France), Kyushu Univ. (Japan)

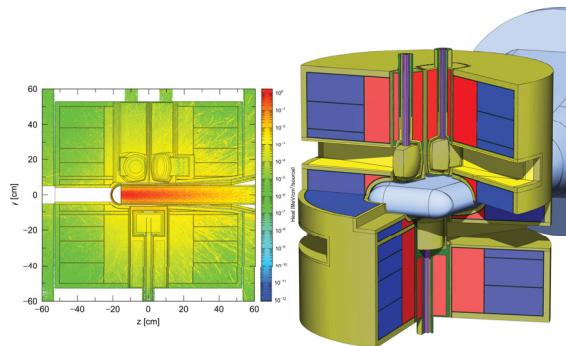
Capability

Transport and collision of various particles over wide energy range

in 3D phase space

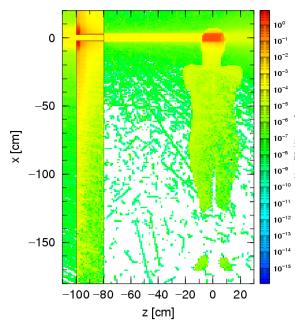
neutron, proton, meson, baryon
electron, photon, heavy ions

up to 100 GeV/u

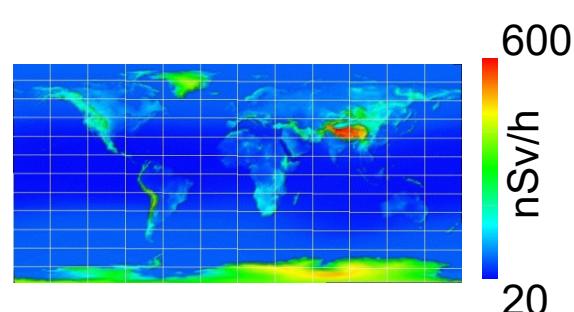


Accelerator Design

Application Fields

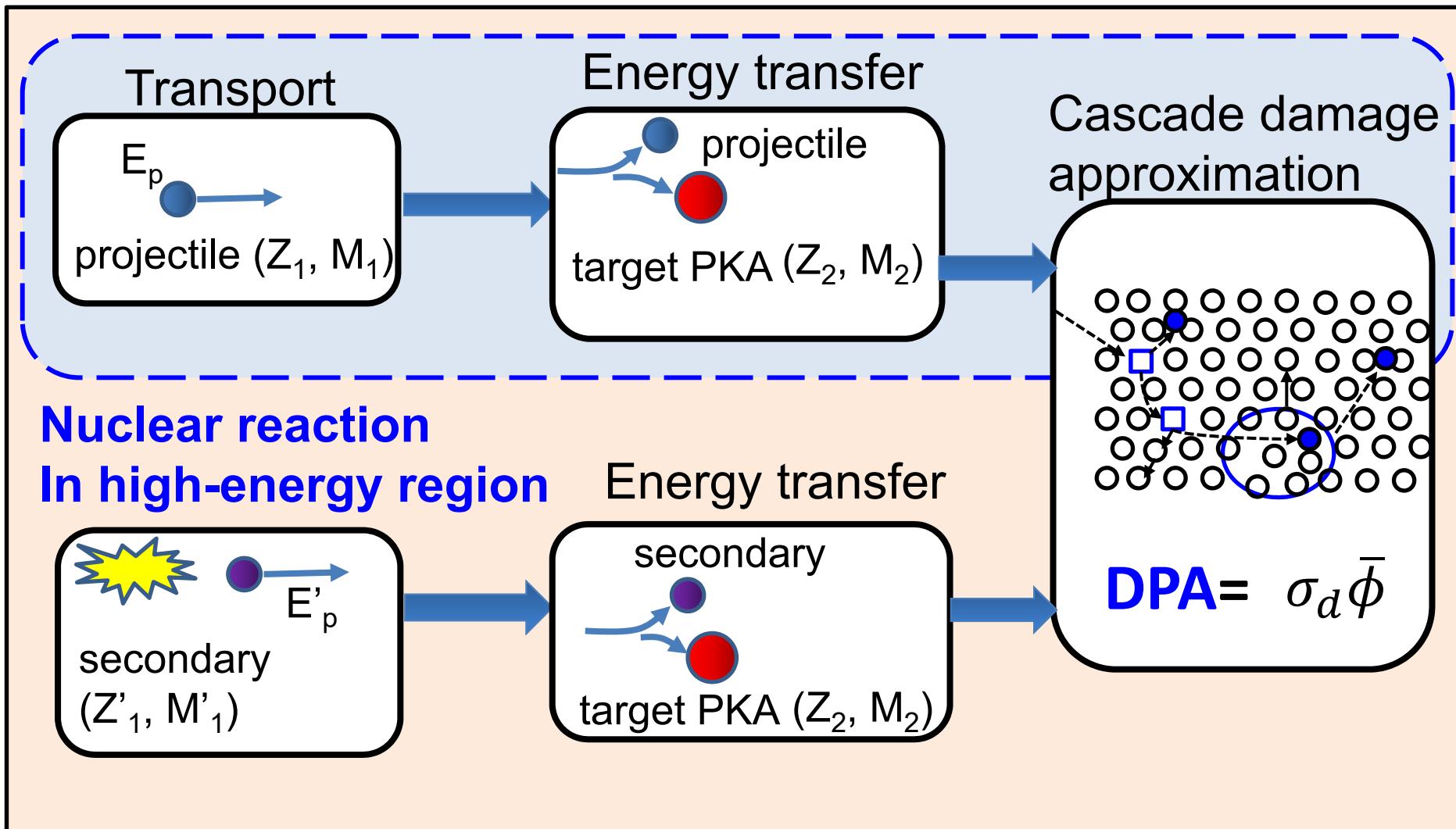


Radiation Therapy



Space Application

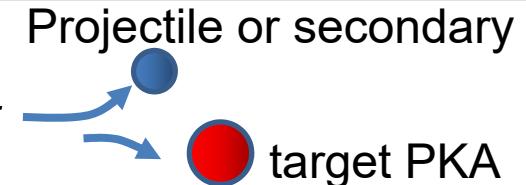
Radiation damage model in PHITS



Displacement cross-section with standard approximation

$$\sigma_{\text{NRT}} = \int_{t_d}^{t_{\max}} d\sigma_{sc}/dt \cdot N_{\text{NRT}} dt$$

$d\sigma_{sc}/dt$: Coulomb scattering cross section
using dimensionless collision parameter t



N_{NRT} : Number of displaced atoms using phenomenological approach

Norgett, Robinson and Torrens, Nuclear Engineering and Design, 33 (1975) 50-54.

The standard approach has been a simple equation for more than 40 years.

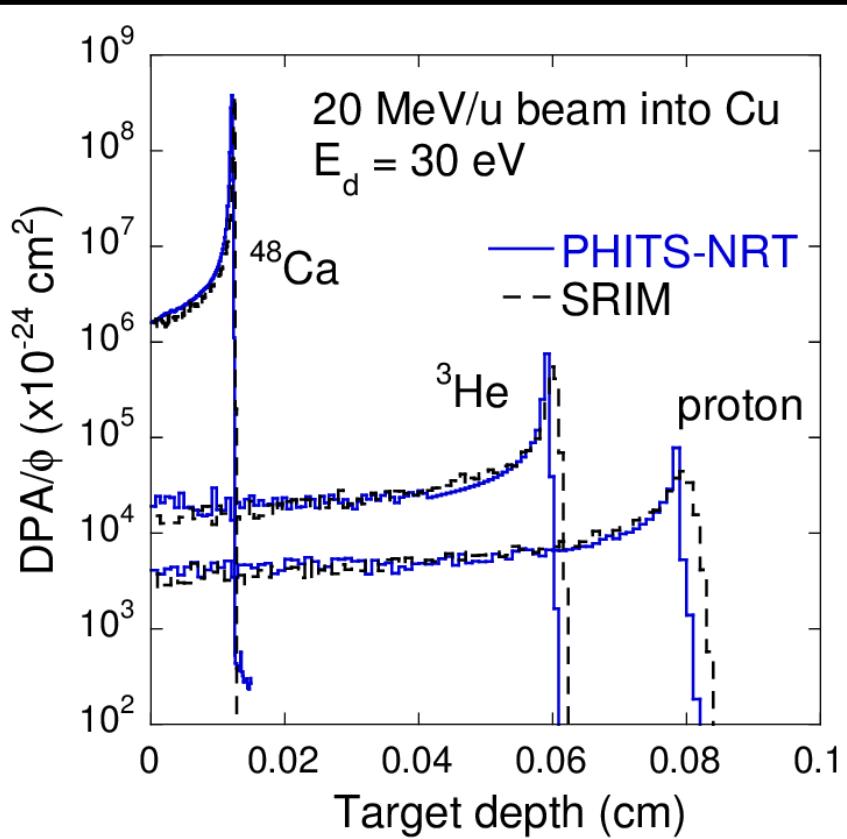
$$N_{\text{NRT}} = (0.8 \cdot T_d) / (2 \cdot E_d)$$

T_d : damage energy available to generate atomic displacements
by elastic collisions

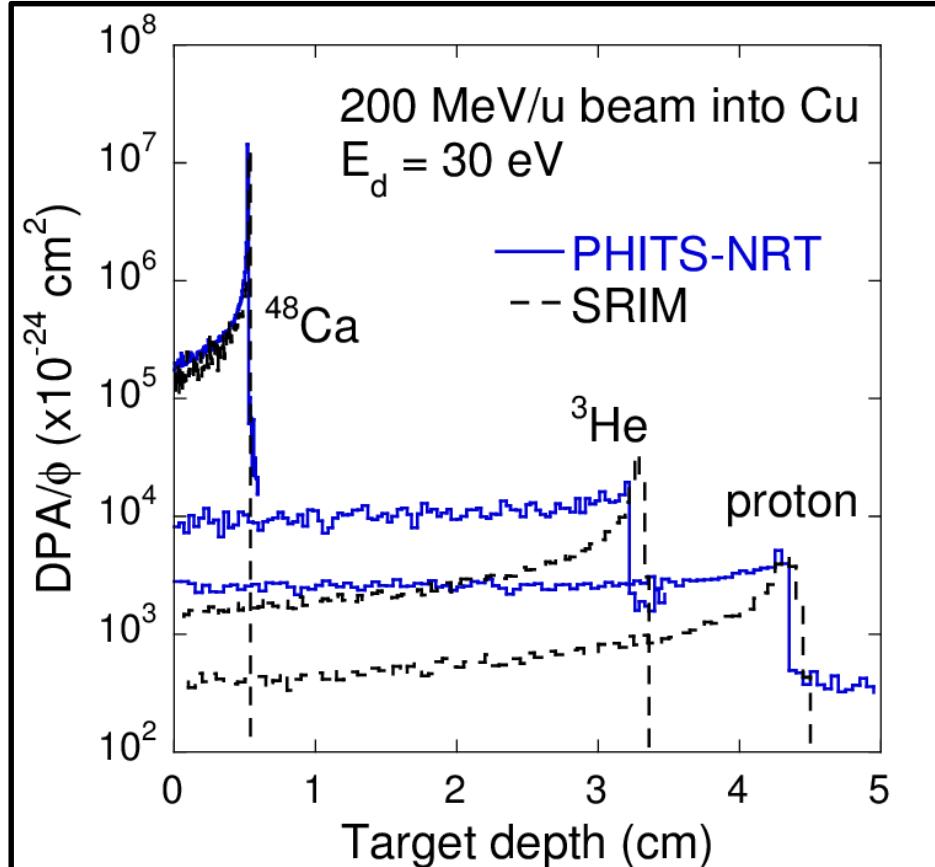
$$T_d = T / (1 + k_{\text{cascade}} \cdot g(\varepsilon)) \quad T: \text{PKA recoil energy}$$

E_d : Displacement threshold energy. e.g. varies 15 – 90 eV for each atom.

Target depth dependence of DPA values in copper



Target depth distribution for 20 MeV/u proton, ^3He and ^{48}Ca



Target depth distribution for 200 MeV/u proton, ^3He and ^{48}Ca

Secondary particles produced by sequential nuclear reactions

Advanced Monte Carlo particle transport codes are essential for DPA calculations in high-energy region.

Displacement cross-section with new approximation

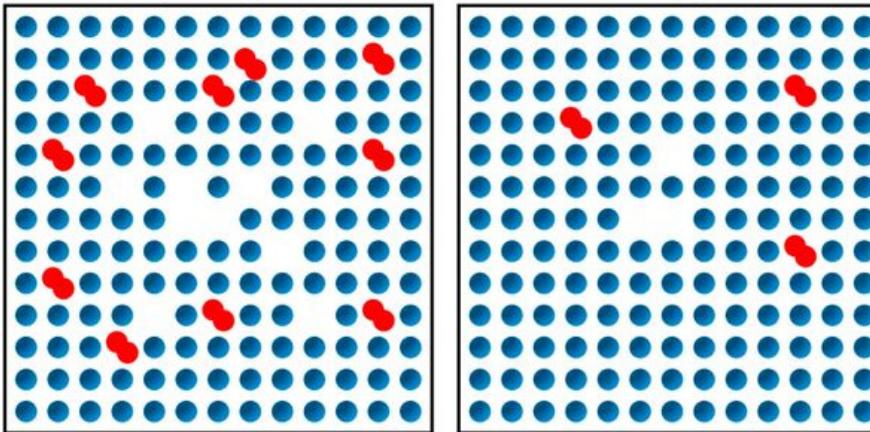


Figure 2 in the paper: K. Nordlund et al., Nature Communications 9 (2018) 1084.

Molecular Dynamic simulation study
athermal recombination between
interstitial atom and vacancy

NRT-dpa damage model Actual damage production

Schematic illustration of the damage for ~ 1 keV damage energy in a metal

addressed by new athermal recombination
correction (arc-dpa) equation

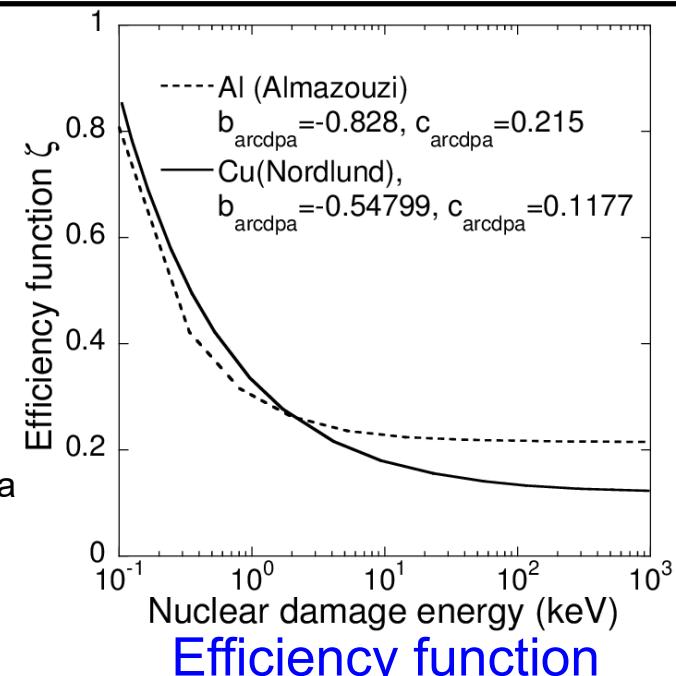
$$\sigma_{\text{arc-dpa}} = \int_{t_d}^{t_{\max}} d\sigma_{\text{sc}}/dt \cdot N_{\text{NRT}} \cdot \zeta dt$$

$$\zeta = \frac{1 - C_{\text{arcdfa}}}{(2 E_d / 0.8)^{b_{\text{arcdfa}}}} T_d^{b_{\text{arcdfa}}} + C_{\text{arcdfa}}$$

based on tabulated parameters: b_{arcdfa} , and c_{arcdfa}
for Fe, Cu, Ni, Pd, Pt, W (Nordlund)
Al (Almazouzi)

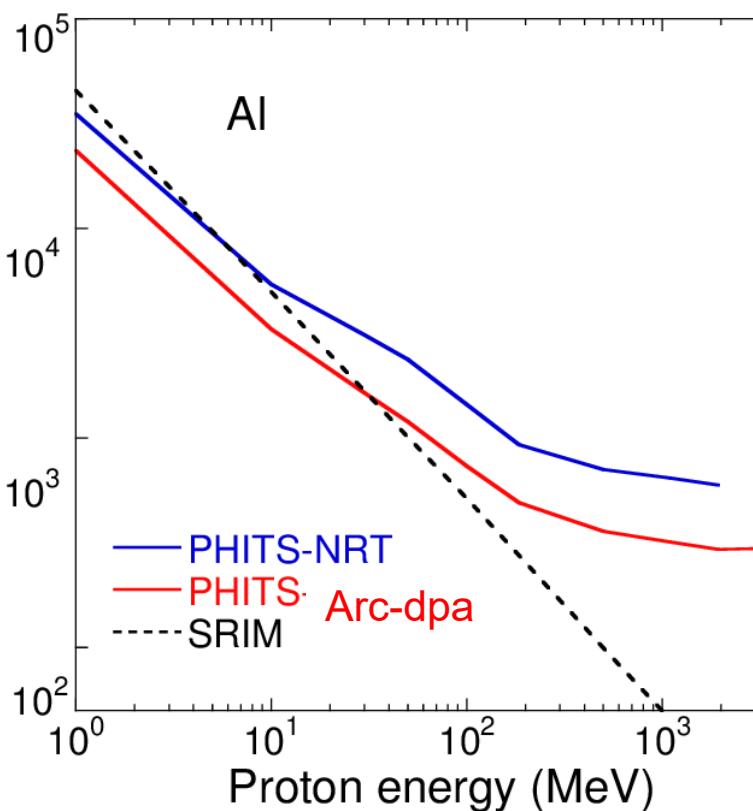


Implement into PHITS code



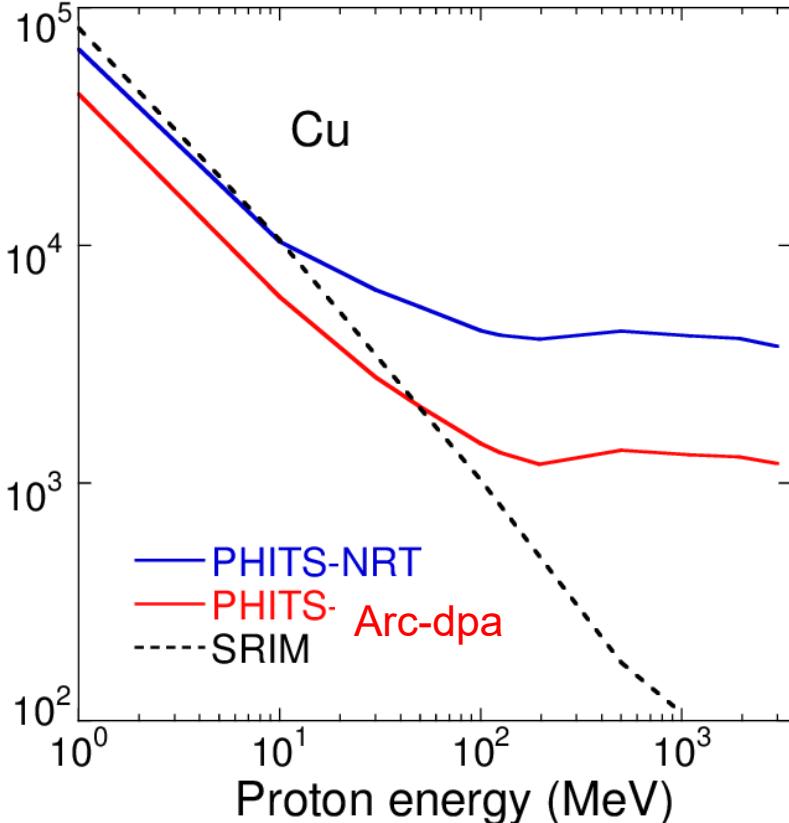
Calculated displacement cross sections

Displacement cross section (b)



Displacement cross section for $p + Al$

Displacement cross section (b)



Displacement cross section for $p + Cu$

NRT(standard) is larger than arc-dpa(new) by roughly a factor of 3.

To Validate calculated results, experimental data is needed.

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Irradiation on metal at cryogenic temperature

Recombination of Frenkel pairs by thermal motion is well suppressed.

Damage rate

$$\sigma_{\text{exp}} = \frac{1}{\rho_{FP}} \left(\frac{\Delta\rho_{\text{metal}}}{\overline{\phi}} \right)$$

$\Delta\rho_{\text{metal}}$: Electrical resistivity change(Ωm)

$\overline{\phi}$: Average Beam fluence($1/\text{m}^2$)

ρ_{FP} : Frenkel-pair resistivity (Ωm)

Resistivity increase is the sum of resistivity per Frenkel pair

BNL data (1.1, 1.9 GeV): Cryostat assembly for sample irradiation consisted of complicated system to deliver a flow of liquid cryogen.

Hard to measure systematic data at other facilities with same device.

Development of liquid cryogen-free cooling system

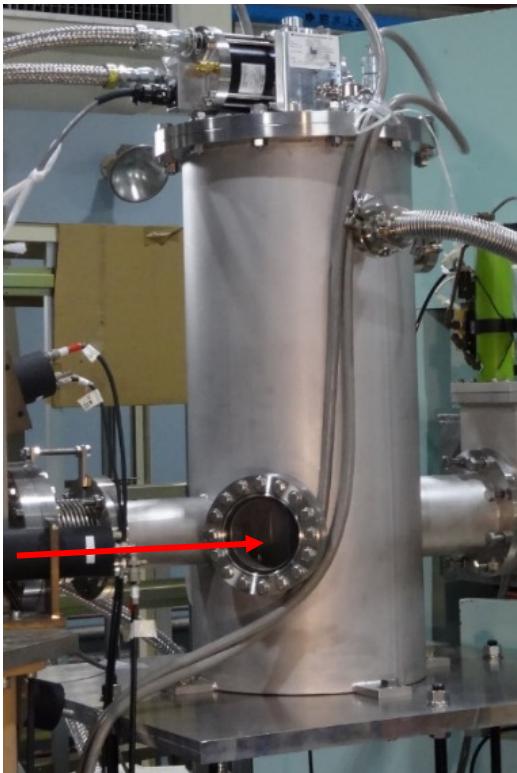
Measurements of displacement cross sections of Al and Cu

Measurements of displacement cross section in Japan



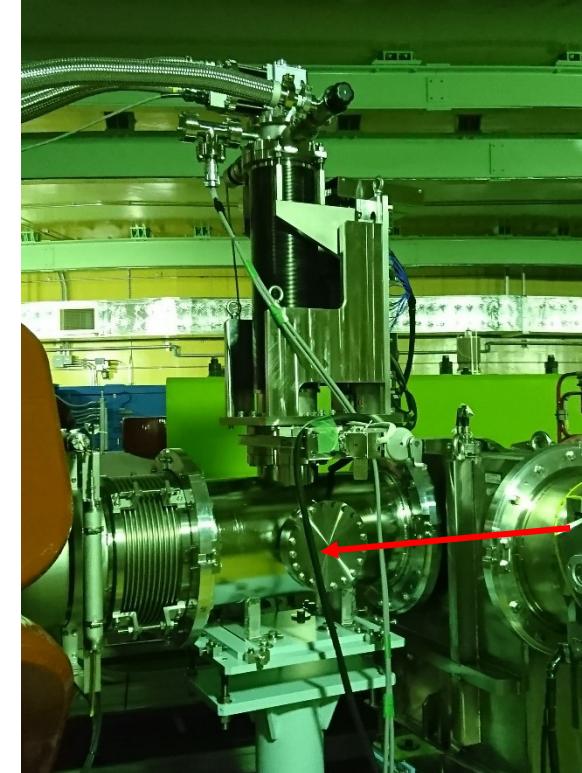
125 MeV proton+Cu
FFAG facility, Kyoto Univ.

Y. Iwamoto et al., J. Nucl. Mater.,
458, (2015) 369-375.



200 MeV proton+Cu, Al
RCNP, Osaka Univ.

Y. Iwamoto et al., J. Nucl. Mater.,
508, (2018) 195-202.

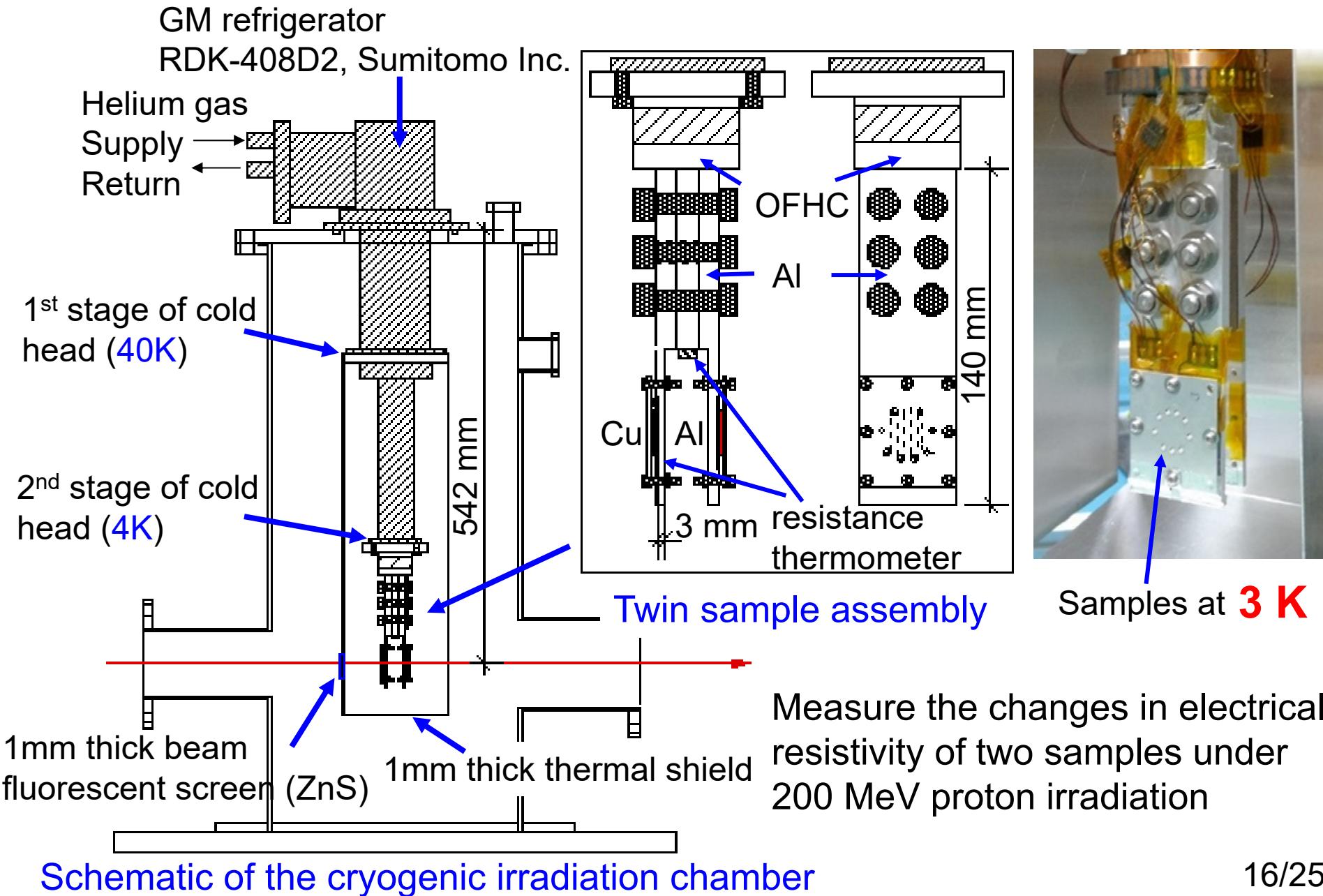


3 GeV proton+Cu
J-PARC

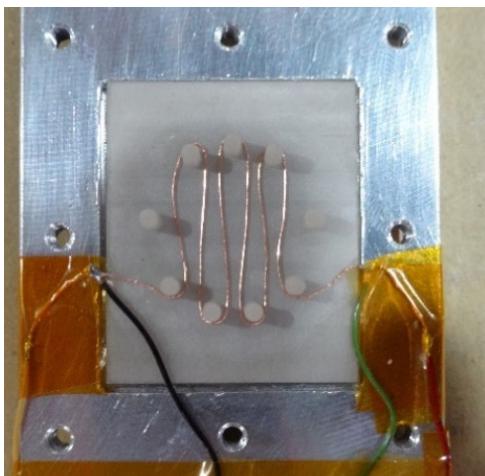
S. Meigo et al., presented at
IPAC'18, 2018, MOPML045

S. Meigo et al., presented at
HB2018, 2018, TUP1WE03

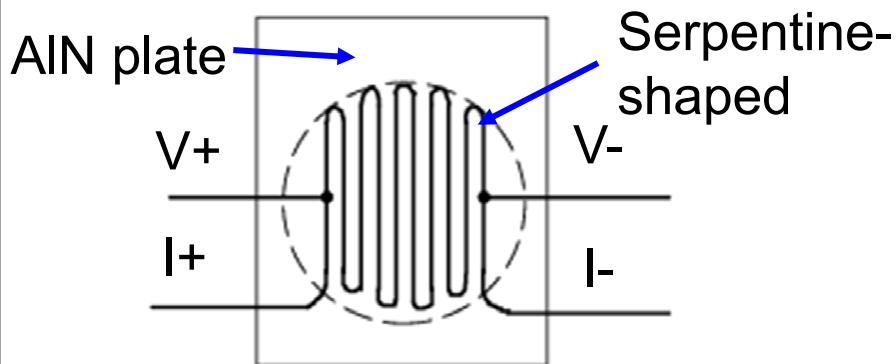
Irradiation chamber and target assembly



Sample and electrical resistance measurement

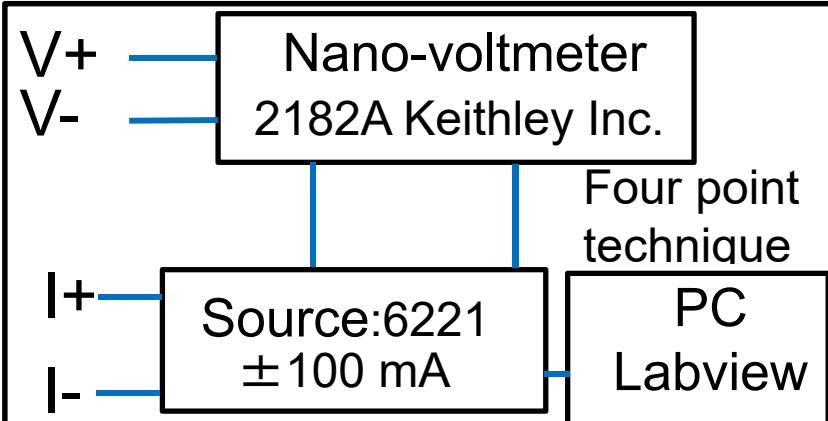


Material	Aluminum	Copper
Diameter (mm)	0.25	0.25
Length (mm)	123	134
Purity (%)	99.99	99.999
Electrical resistivity at room temperature(Ω m)	2.19×10^{-8}	1.47×10^{-8}
Electrical resistivity at 3 K(Ω m)	4.43×10^{-11}	2.02×10^{-11}



Cross section of wire

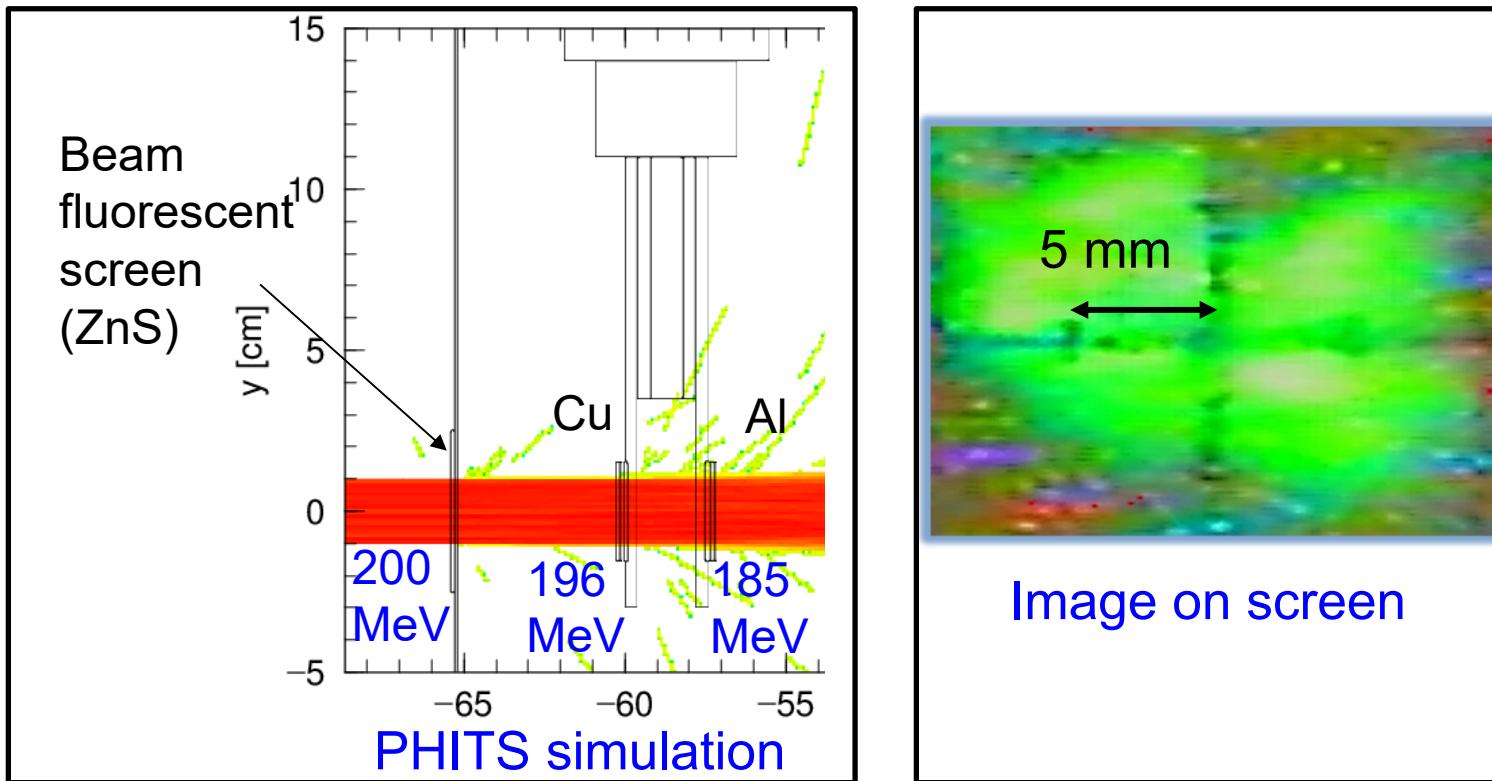
$$\text{Electrical resistivity } \rho(\Omega\text{m}) = \frac{S(\text{m}^2)}{L(\text{m})} * R(\Omega) \quad \text{Resistance}$$



Cancel effects of thermal electromotive force

Precision $\pm 0.001 \mu\Omega$ @ 3 K

Beam profile



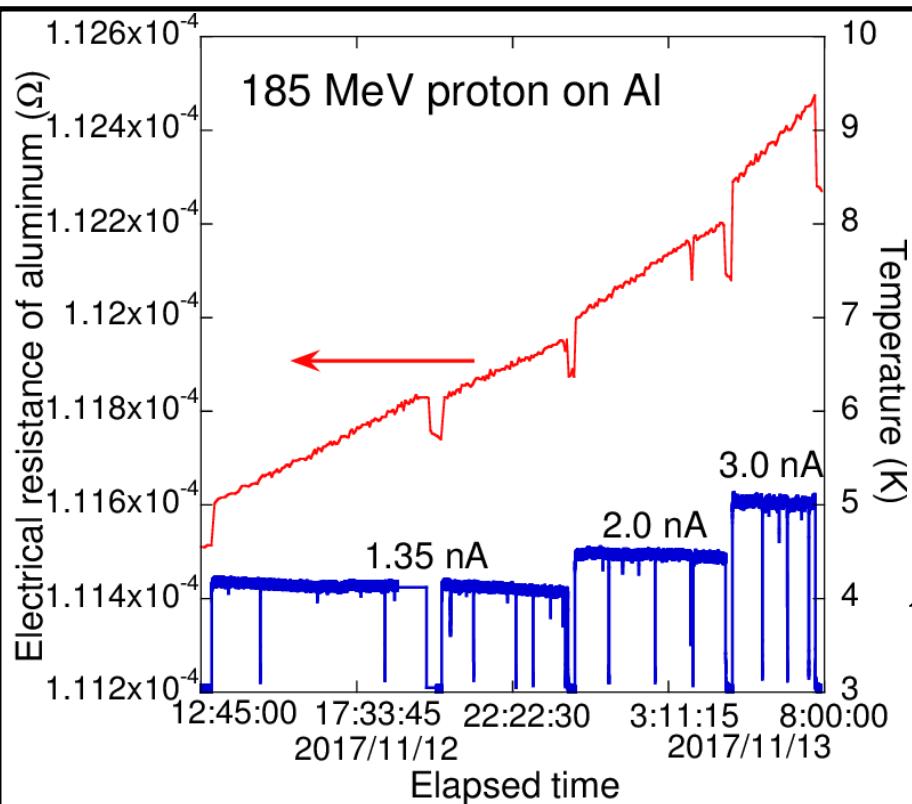
Adjusted beam area to cover sample with controlling magnetic field of magnets
Captured the beam shape on screen by portable camera.

Estimation of uncertainty of displacement cross section due to beam profile
(FWHM = 9.5 ± 2.5 mm) using PHITS

$$\sigma_d = \frac{DPA}{\bar{\Phi}} \quad \sim 4 \%$$

→ In future, beam profile monitor will be used at RCNP.

Electrical resistivity changes of wires during irradiation



- ✓ 5 K during 3 nA beam irradiation
- ✓ Total increase in resistance at 3 K: 0.76 $\mu\Omega$ for Al, 2.34 $\mu\Omega$ for Cu
- ✓ Total fluence: 3.89×10^{18} proton/m²

Damage rate

$$D(\Omega \text{m}^3) = \frac{\Delta \rho(\Omega \text{m})}{\bar{\Phi}(1/\text{m}^2)}$$

Electrical resistivity
Average beam fluence

Experimental damage rate

Beam		fusion neutron	125 MeV proton	200 MeV proton	1.94 GeV proton	3 GeV proton
		RTNS-II	KURRI-FFAG	RCNP	BNL	J-PARC
Damage rate ($10^{-31} \Omega \text{ m}^3/\text{particle}$)	Al	4.18	-	1.31	-	-
	Cu	2.48	3.41	3.60	3.66	2.35

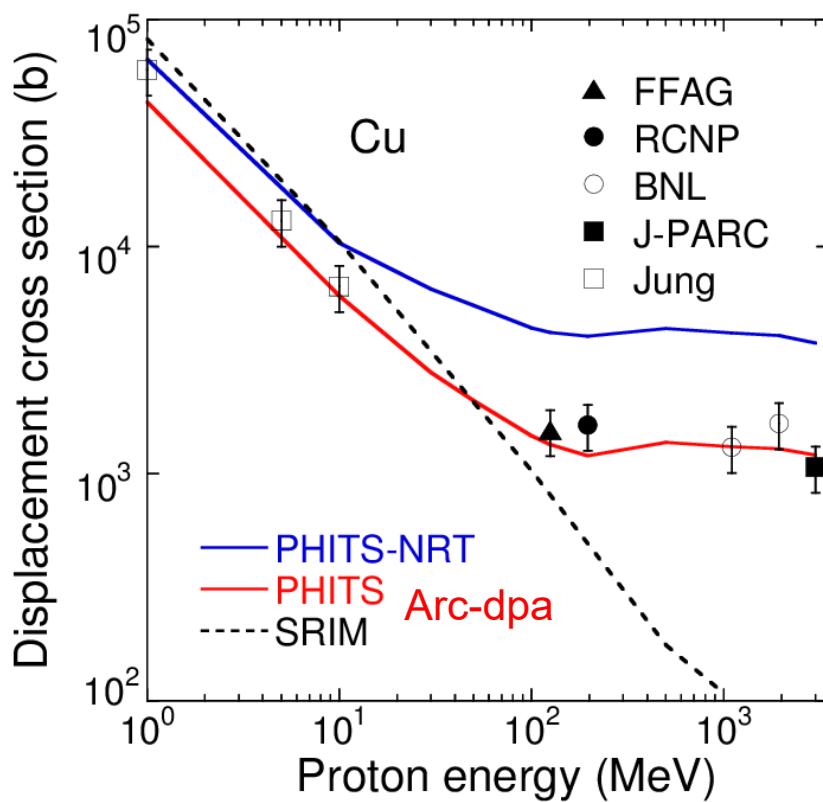
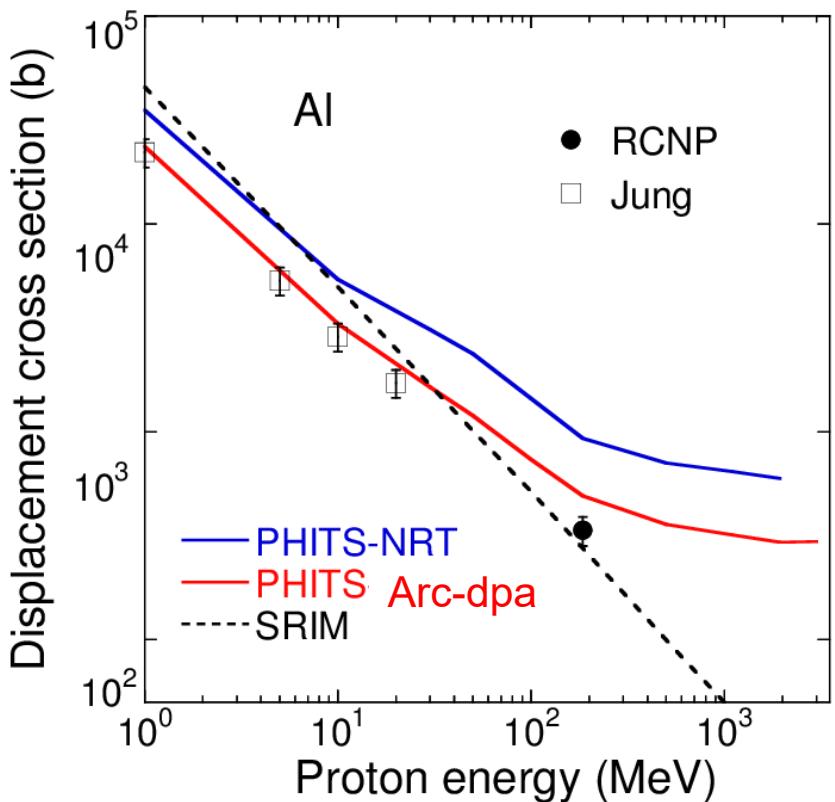
Comparison of experimental displacement cross sections with PHITS results

$$\sigma_{\text{exp}}(\text{m}^2) = \frac{1}{\rho_{\text{FP}}(\Omega\text{m})} D(\Omega\text{m}^3) \rightarrow \text{Damage rate}$$

\rightarrow Change in resistivity per Frenkel-pair density

Al: $3.9 \pm 0.6 \mu\Omega\text{m}$ 15 % uncertainty
 Phys. Rev. B 8 (1973) 2604-2621.

Cu: $2.2 \pm 0.5 \mu\Omega\text{m}$ 23 % uncertainty
 J. Nucl. Mater. 69&70 (1978) 644-649.



Results calculated by standard model (NRT) overestimates the data by a factor of ~3.
 New model(arc-dpa) gives good agreements with the data well.
 The arc-dpa will be a basis for formulating more reliable.

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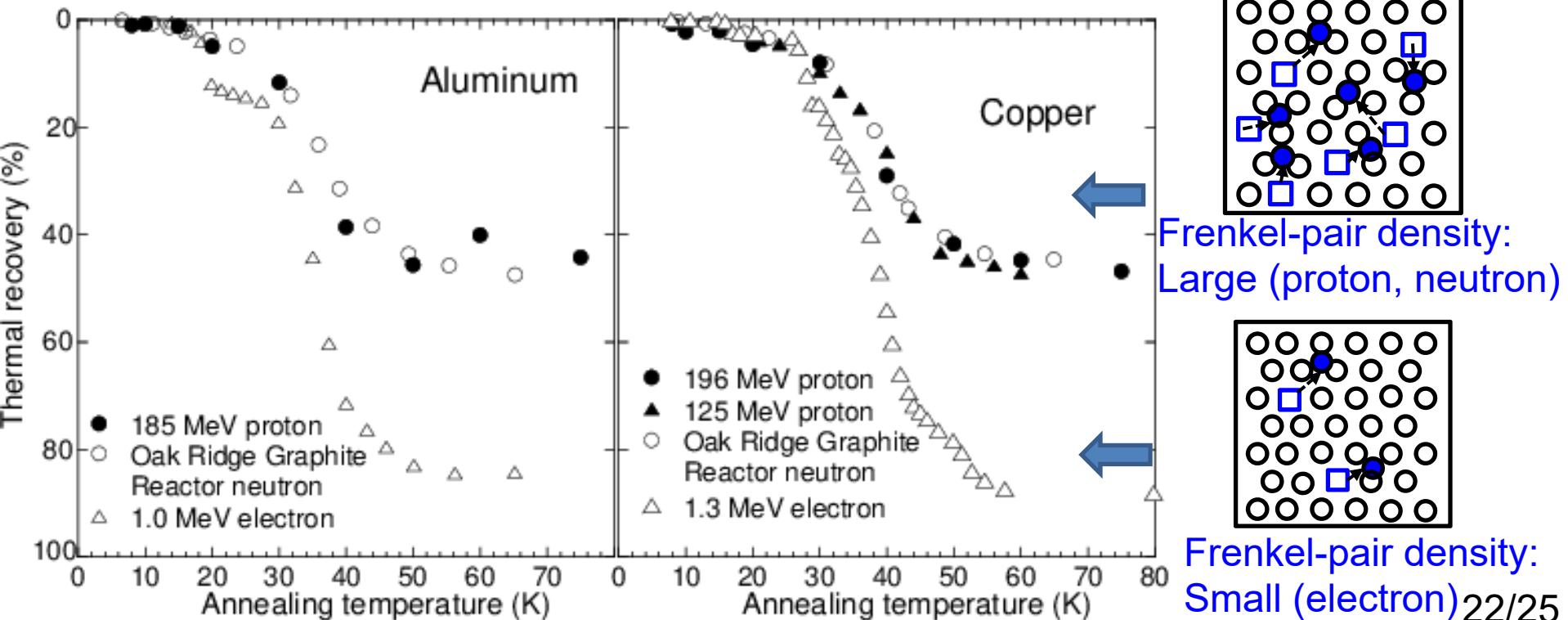
Recovery of defects through annealing after beam irradiation

Annealing effects were observed up to certain temperatures by isochronal schedule.

- (1) Warming the sample to the annealing temperature using an electric heater.
- (2) Holding sample temperature constant for about 10 min.
- (3) Cooling the sample to 3 K.
- (4) Measuring electrical resistivity of the sample at 3 K.

$$\text{Thermal recovery} = 1 - \frac{\Delta\rho}{\Delta\rho_0} (\%)$$

remaining radiation-induced resistivity increase
initial radiation-induced resistivity increase



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Conclusion

The radiation damage model in PHITS has been developed.

In the high energy region ($> \sim 100$ MeV) for proton beams,
DPA created by secondaries increase due to nuclear reactions.

The NRT-dpa(standard) is larger than the arc-dpa(new) by roughly a factor of 3.

We have developed cryogenic irradiation system and measured displacement cross sections of Al and Cu for 125, 200 MeV and 3 GeV proton irradiation.

The arc-dpa(new) reproduces the experimental data well for Cu and Al.

The arc-dpa will be used for efficient predictions of the usable lifetime.

Future plan

Continue to measure the data for various metals.
pure metal (Al, Fe, Ti, Nb, W), alloy

Arc-dpa parameters for various metals will be implemented in PHITS, when these parameters are opened.

(2) Energy transfer with Coulomb scattering in PHITS

M. Nastasi et al., "Ion-Solid Interaction: Fundamentals and Applications "



E_p : kinetic energy, (Z_1, M_1)

leads to the deflection of the particles

T : transferred energy, (Z_2, M_2)

Coulomb scat. cross section: one parameter

$$d\sigma_{sc} / dt(t) = \frac{\pi a_{TF}^2}{2} \frac{f(t^{1/2})}{t^{3/2}}$$

dimensionless collision parameter:

$$t \equiv \epsilon^2 \frac{T}{T_{max}} = \epsilon^2 \sin^2\left(\frac{\theta}{2}\right)$$

T : Transferred energy to target atom

T_{max} : maximum transferred energy

$$= \frac{4M_1 M_2 E_p}{(M_1 + M_2)^2}$$

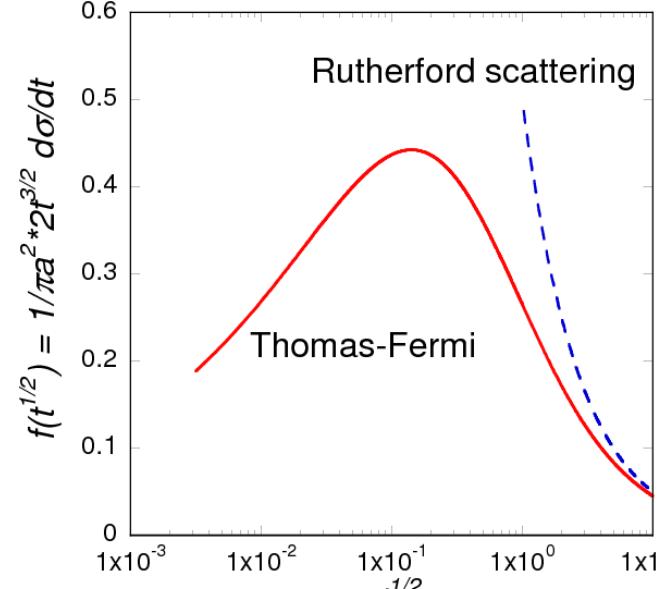
ϵ : dimensionless energy

$$= \frac{E a_{TF} M_2}{Z_1 Z_2 e^2 (M_1 + M_2)}$$

Screening functions:

$$f(t^{1/2}) = \lambda t^{1/2-m} [1 + (2\lambda t^{1-m})^q]^{-1/q}$$

Thomas-Fermi $\lambda=1.309$, $m=1/3$, $q=2/3$



Large t → large T in close collisions

Small t → small T in distance collisions