



High-Q R&D at FNAL

Mattia Checchin

Performance frontier group, SRF sector, TD

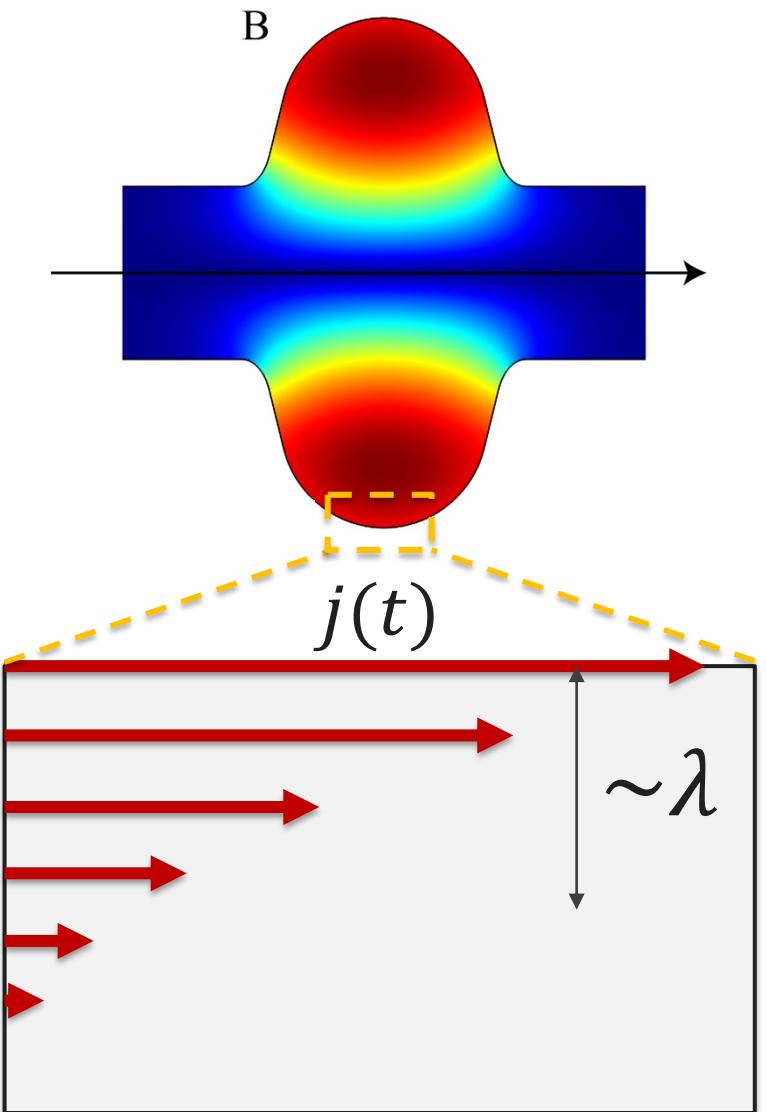
ERL 2017

20 June 2017



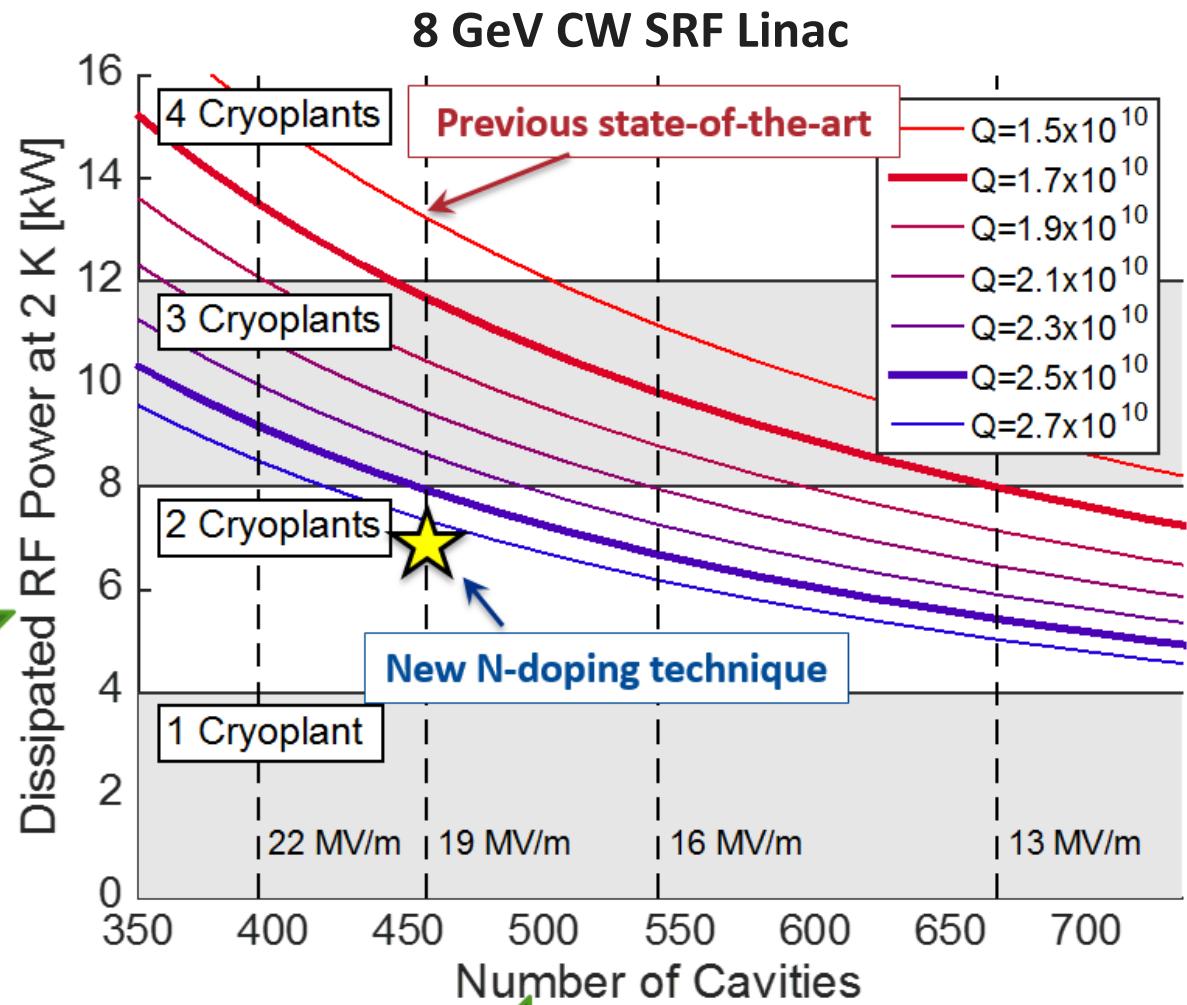
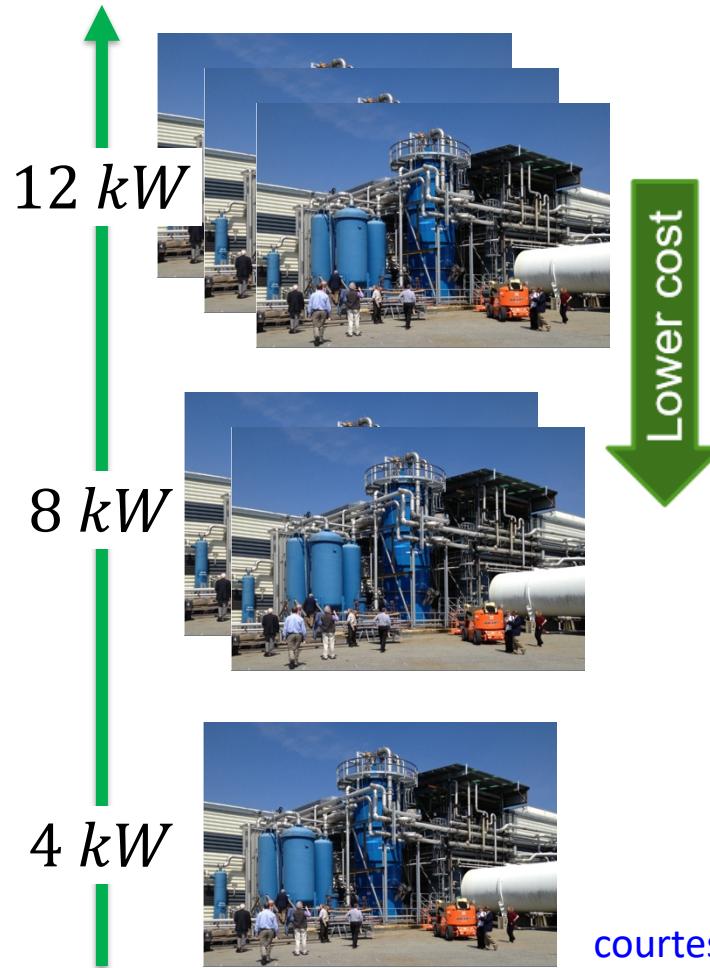
Superconducting RF resonators

- EM field resonates efficiently with very low dissipation
- Performance defined by the first hundreds of nanometers from the RF surface (λ), where the current flows
- $R_s(T) = R_{BCS}(T) + R_{res}$
- High $Q_0 \Rightarrow$ minimization of $R_{BCS}(T)$ and R_{res}



Why high-Q?

$$P_{diss} \sim E_{acc}/Q_0$$

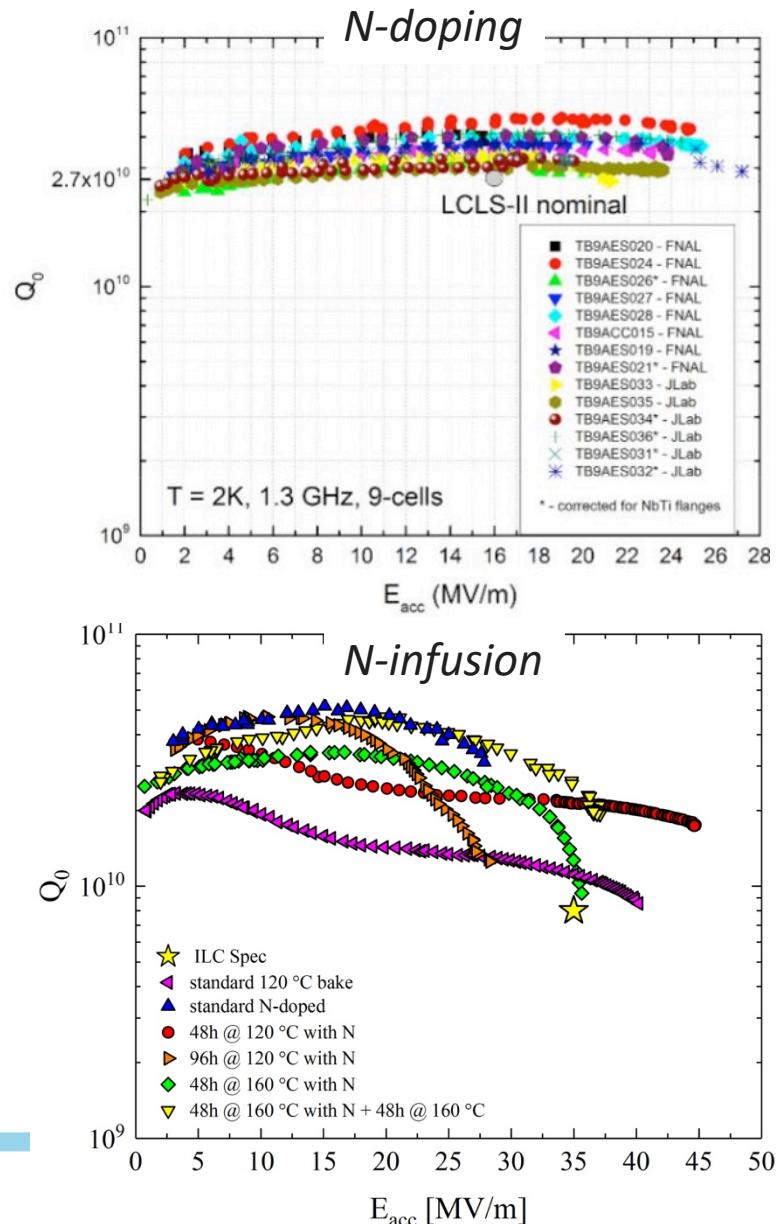


courtesy of A. Grassellino

High Q_0 studies at FNAL
N-doping & N-infusion

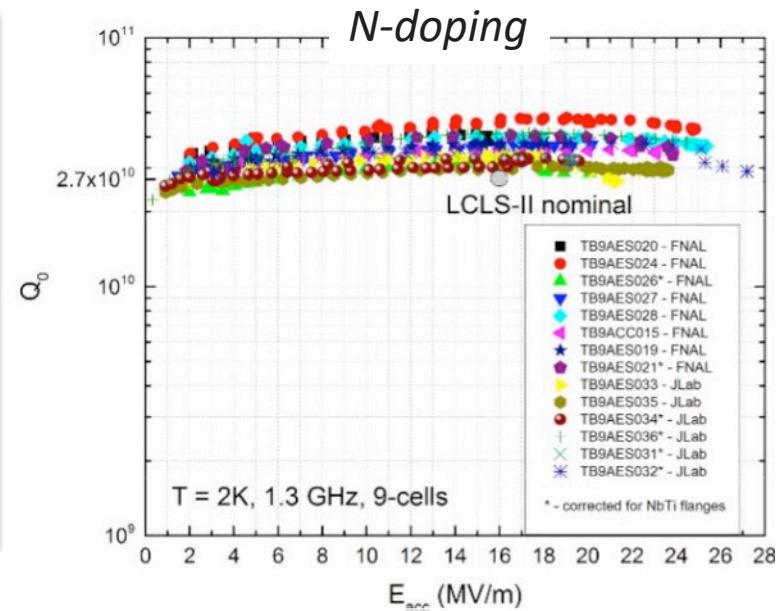
High Q_0 treatments studied at FNAL

- N-doping
 - High T treatment in HV with N_2
 - N_2 injection done at $T = 800 - 1000\text{ C}$ for $2 - 20\text{ min}$
 - Successfully implemented on large scale production (LCLS-II)
- N-infusion
 - Low T treatment in HV with N_2
 - N_2 injection done at $T = 120 - 160\text{ C}$ for $48 - 96\text{ h}$
 - Being deeply investigated

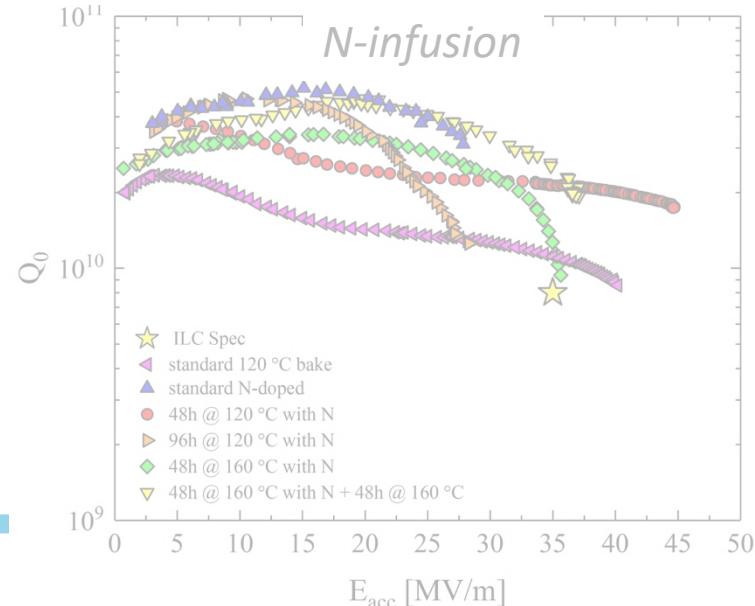


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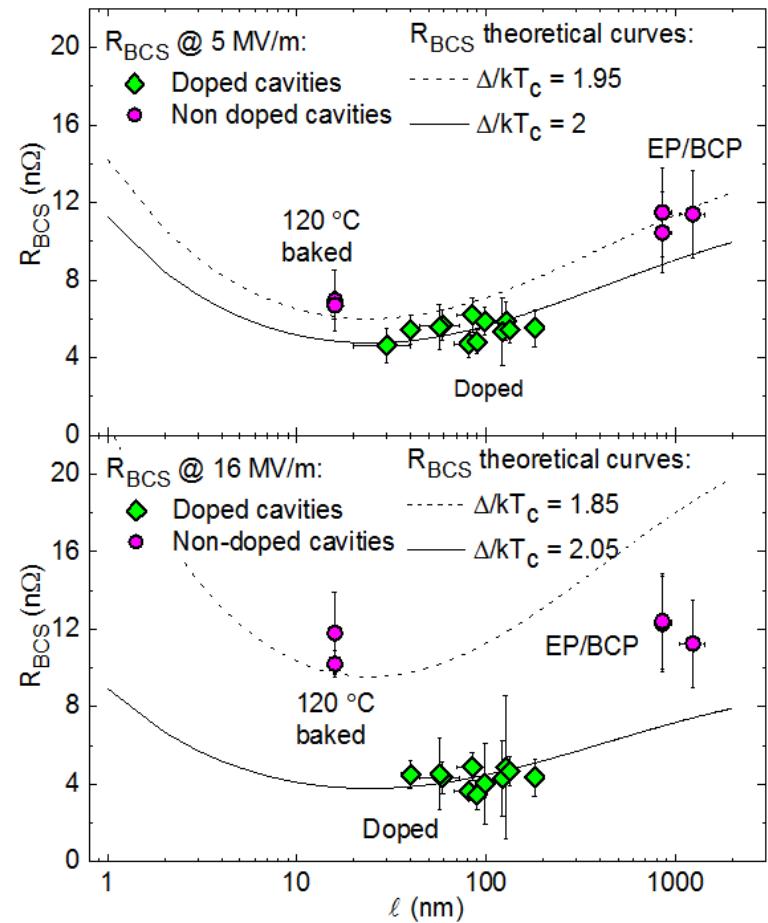
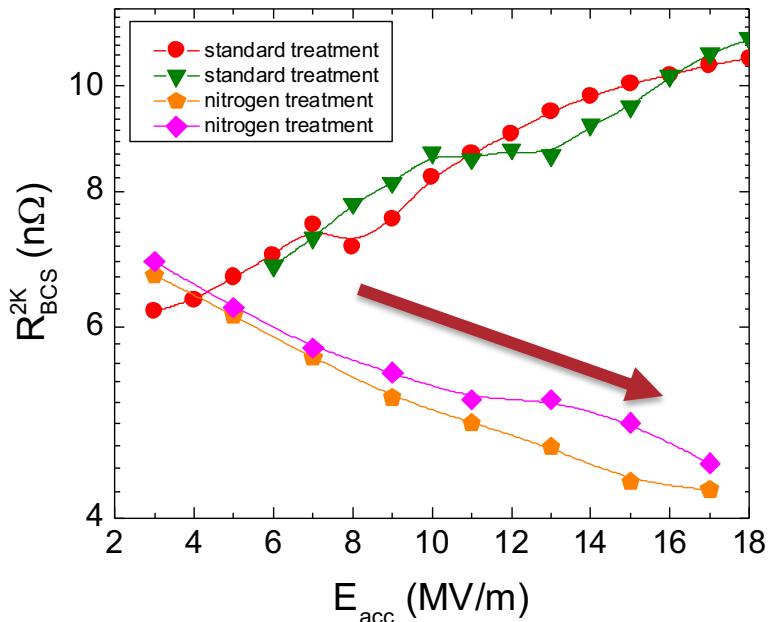
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N-doping: reversal of BCS surface resistance

$$R_s(T) = R_{BCS}(T) + R_{res}$$

Anti-Q-slope emerges from the BCS surface resistance decreasing with RF field



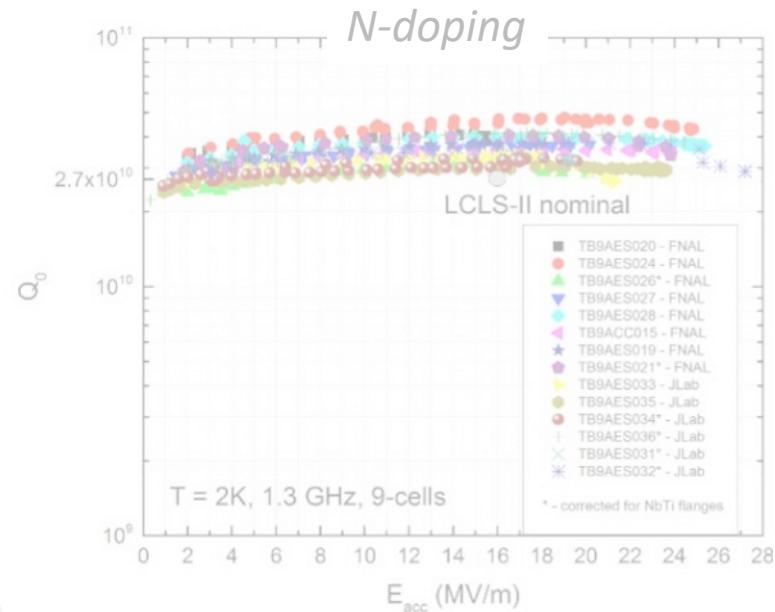
A. Grassellino *et al.*, Supercond. Sci. Technol. **26** 102001 (2013) - Rapid Communications

A. Romanenko and A. Grassellino, Appl. Phys. Lett. **102**, 252603 (2013)

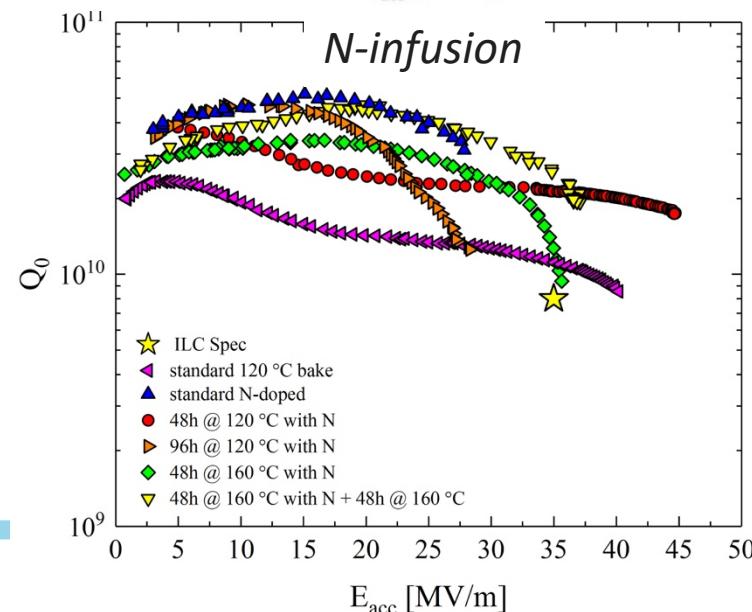
M. Martinello *et al.*, App. Phys. Lett. **109**, 062601 (2016)

High Q_0 treatments studied at FNAL

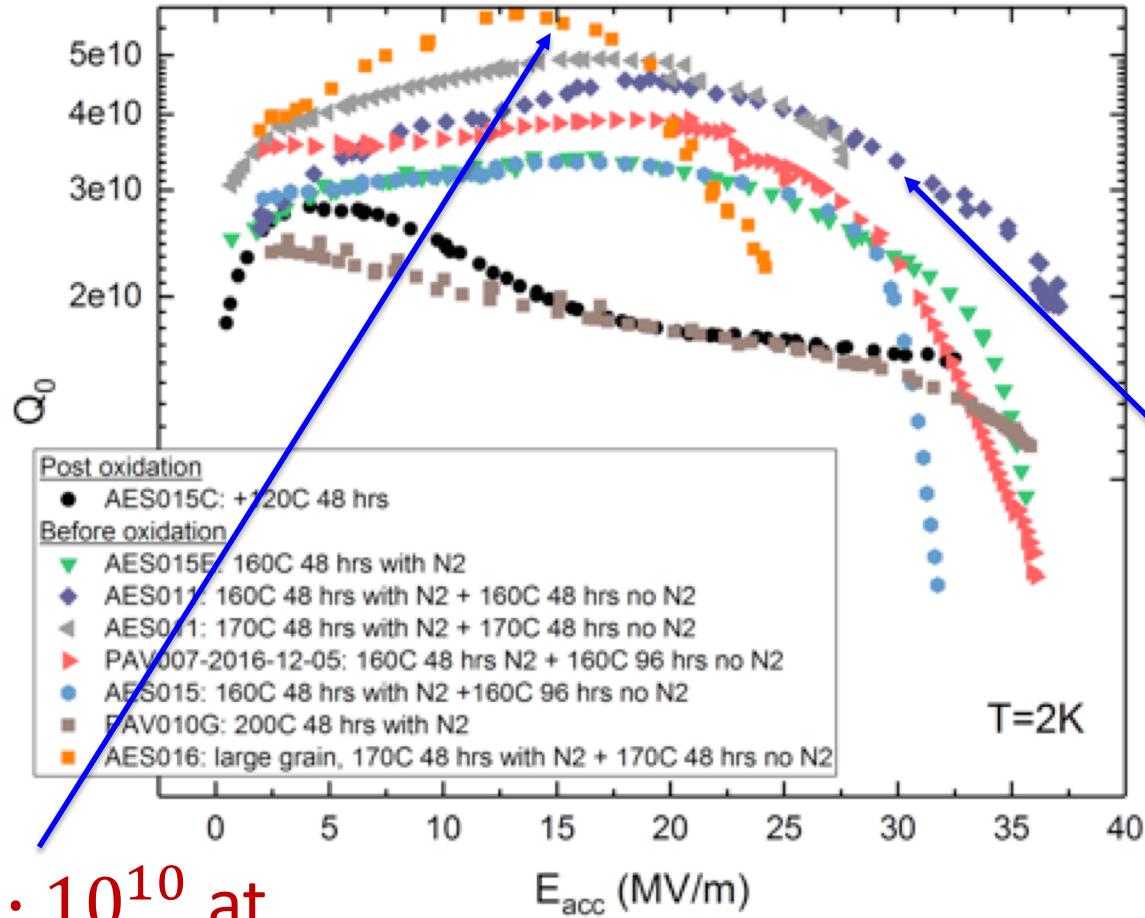
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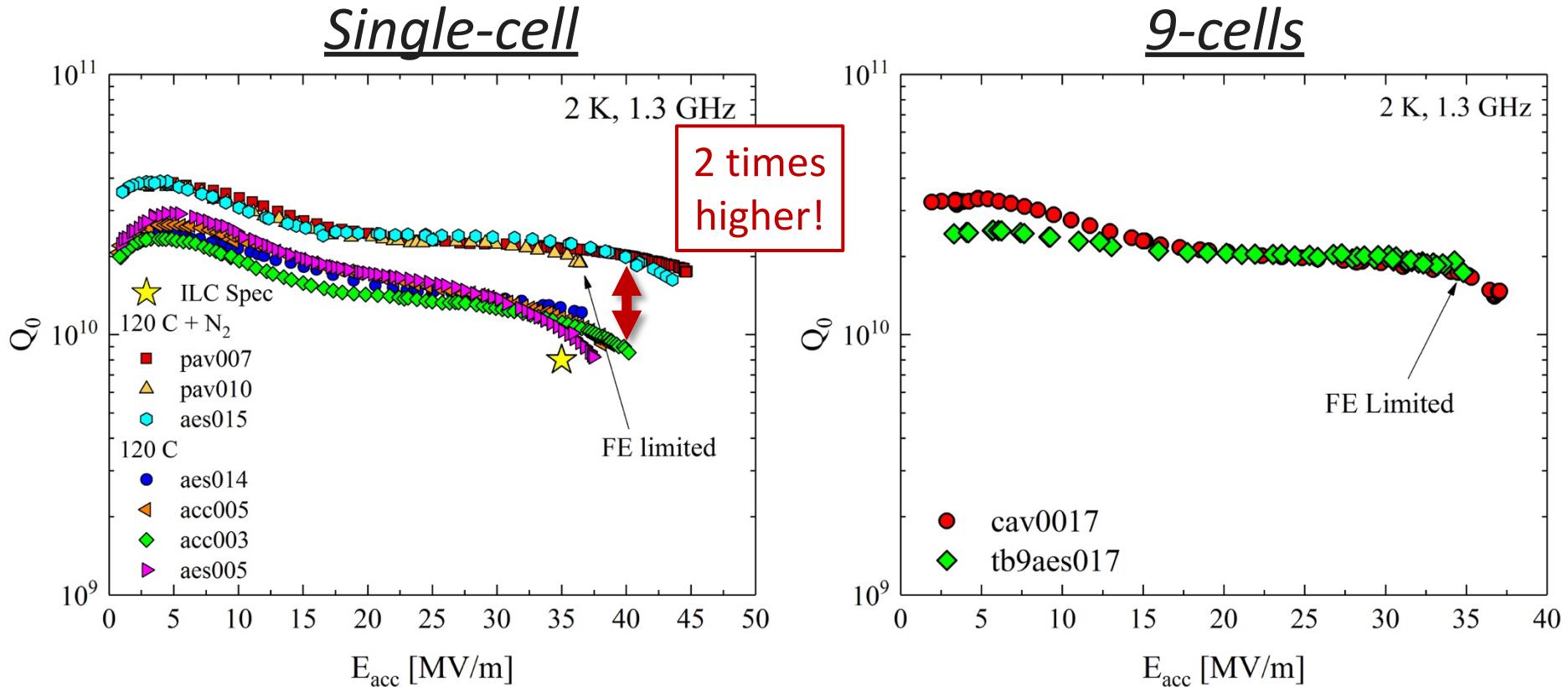


N-infusion: a larger parameter space to be explored



A. Grassellino *et al.*, arXiv:1701.06077 (submitted to SUST)

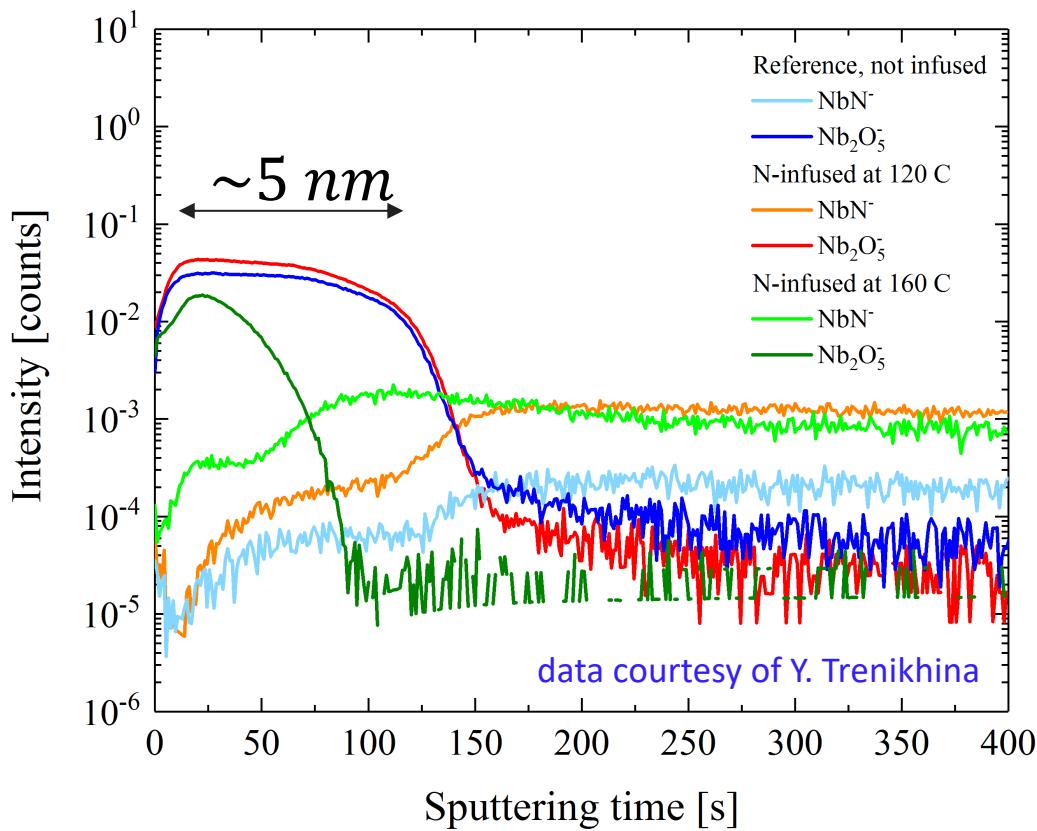
120 C N-infusion: high Q_0 at high gradients



Higher Q-factor at higher field may allow for higher duty-cycles and therefore higher luminosity!

A. Grassellino *et al.*, arXiv:1701.06077 (submitted to SUST)

Nitrogen role in N-infusion



No nitrides formation
at the RF surface

A. Grassellino *et al.*, arXiv:1701.06077 (submitted to SUST)

- Higher N_2 background than not infused samples
- Small ($\sim 1 - 2 \text{ nm}$) N_2 enriched layer below native oxide
- SIMS data suggest that performances are related to the first nm from the RF surface
- Being investigated with subsequent HF rinsing experiment

Q_0 preservation

Understanding the trapped flux surface resistance

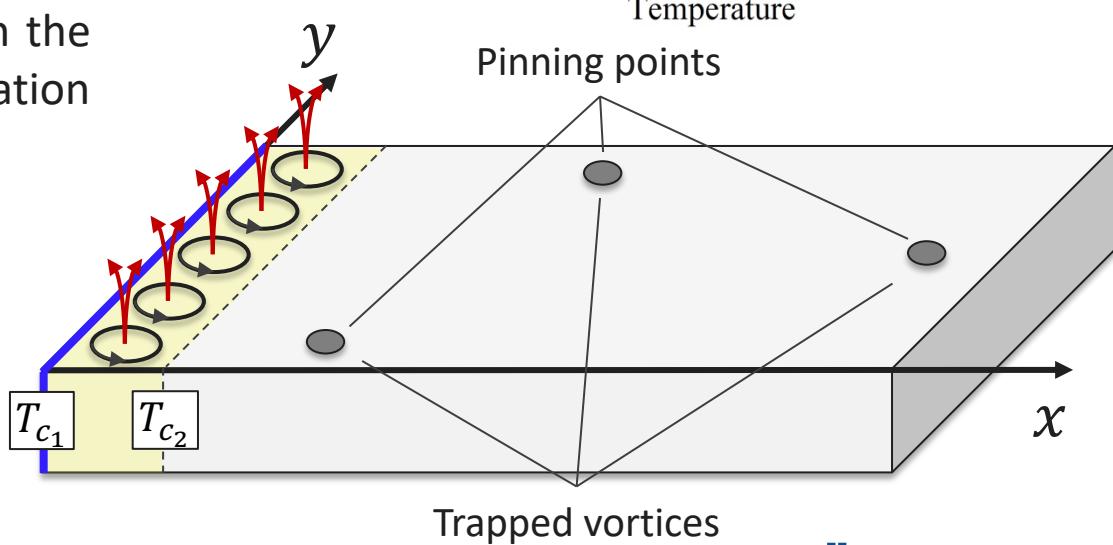
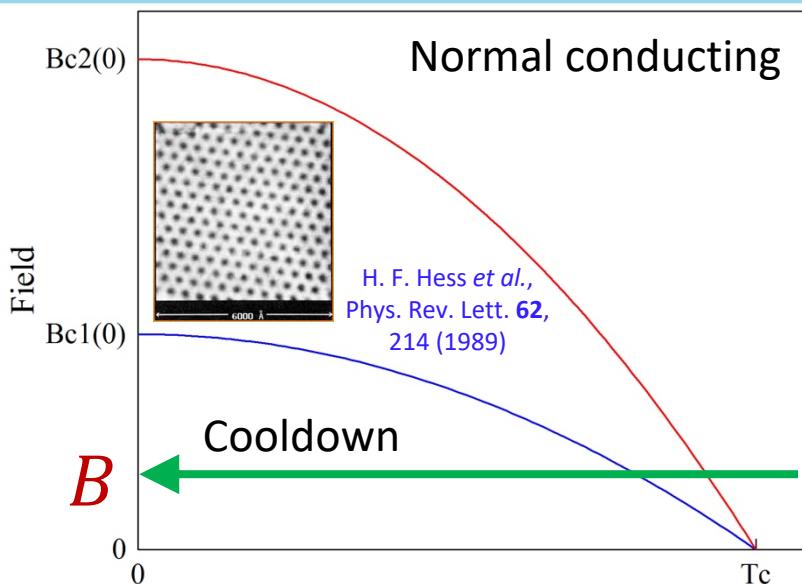
Trapped flux surface resistance

$$R_s(T, B) = R_{BCS}(T) + \underbrace{R_{fl}(B)}_{R_{res}} + R_0$$

$R_0 \Rightarrow$ intrinsic residual resistance

$R_{fl} = \eta_t S B \Rightarrow$ trapped magnetic flux surface resistance:

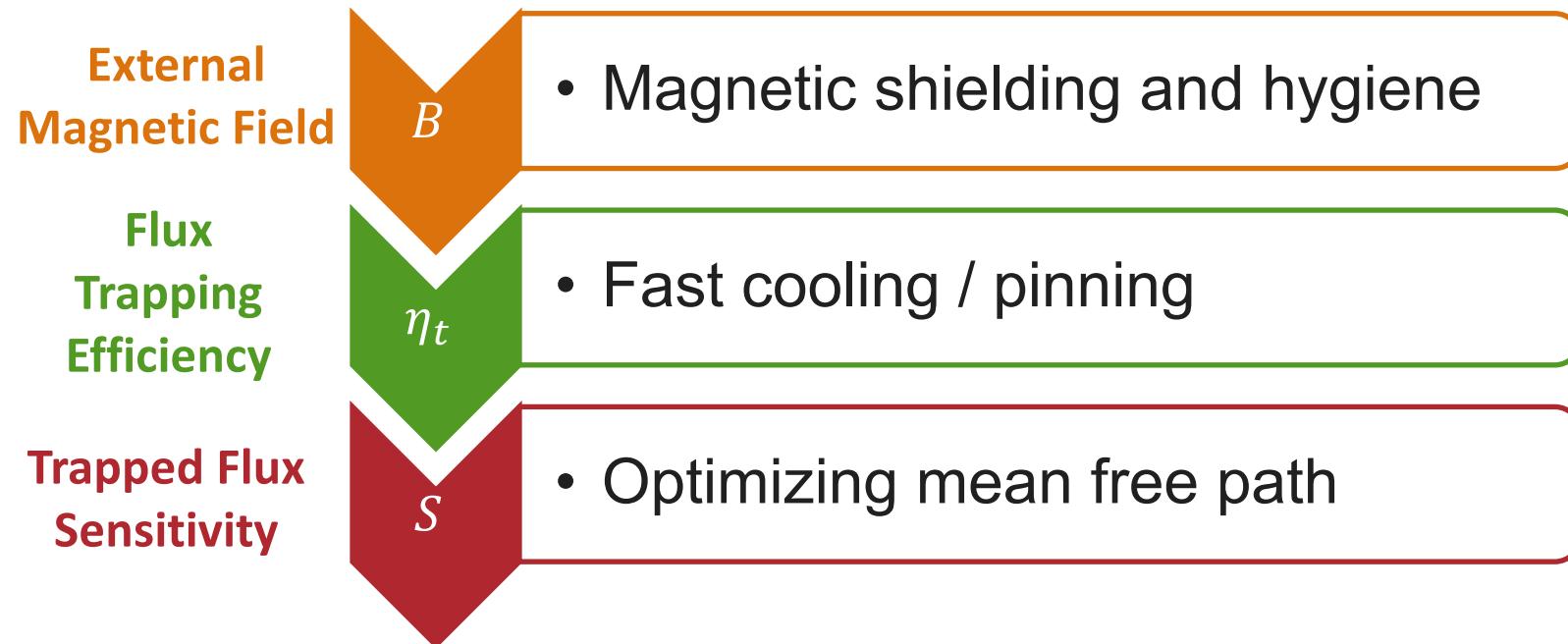
- If pinned, vortices may survive in the Meissner state introducing dissipation
- η_t —flux trapping efficiency
- S —trapped flux sensitivity
- B —external magnetic field



Trapped flux surface resistance contributions

$$R_{fl} = \eta_t S B$$

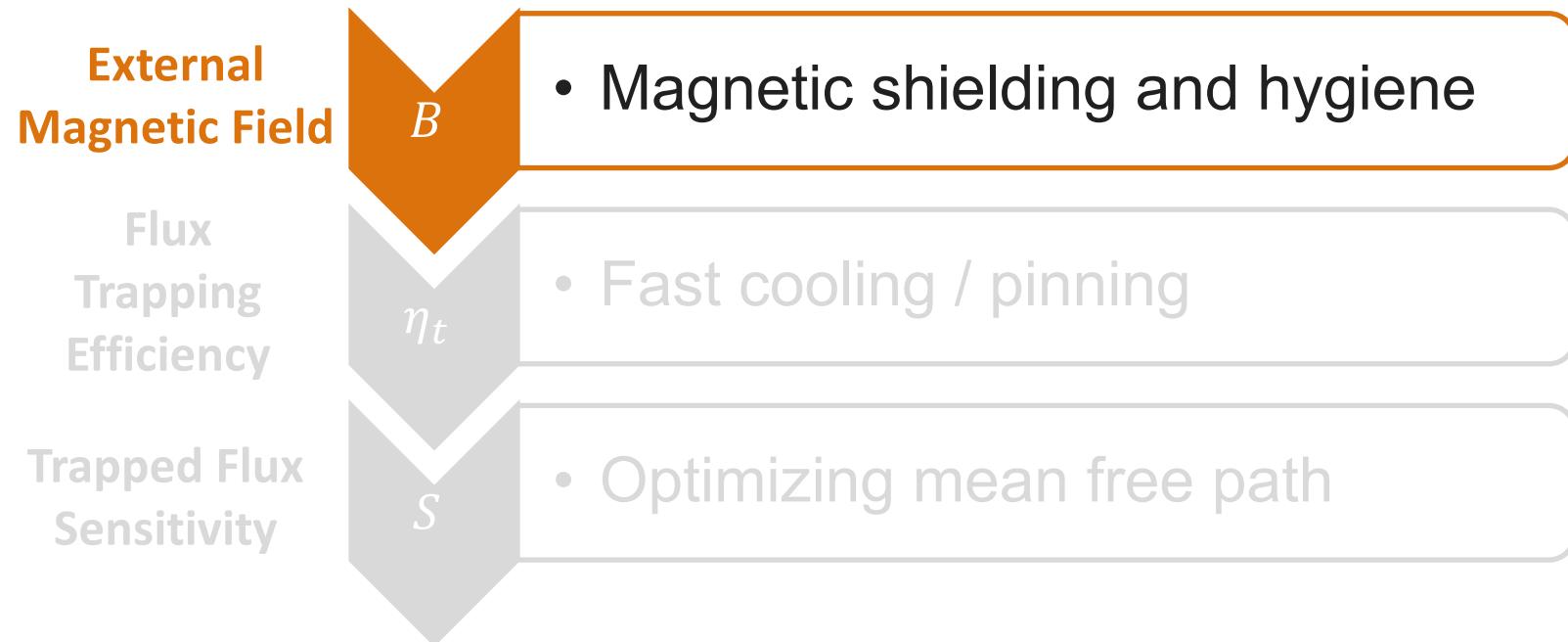
R_{fl} can be reduced by minimizing these contributions:



Trapped flux surface resistance contributions

$$R_{fl} = \eta_t S B$$

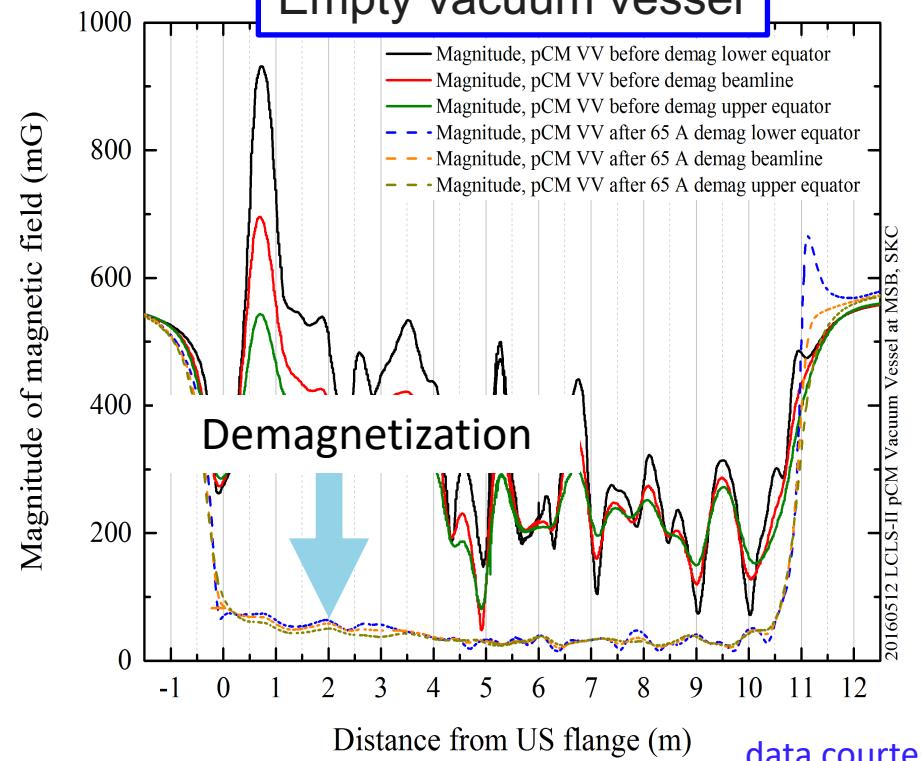
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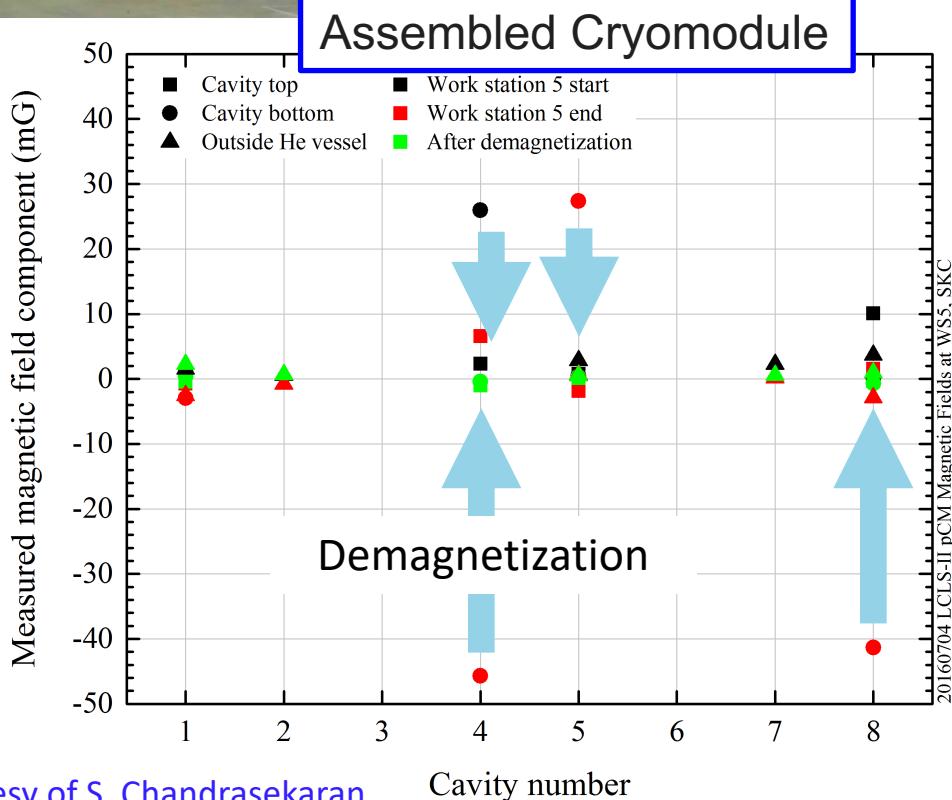
Minimization of remnant field in the cryomodule



Empty vacuum vessel



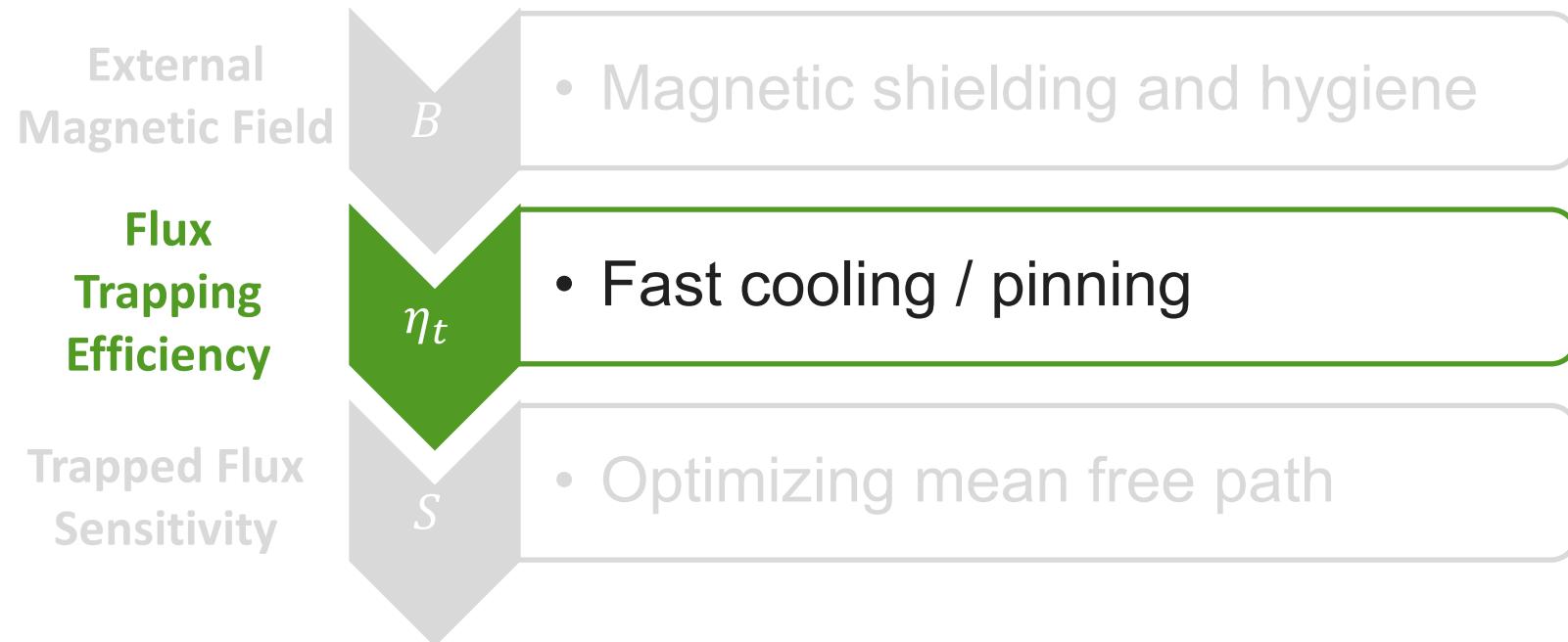
data courtesy of S. Chandrasekaran



Trapped flux surface resistance contributions

$$R_{fl} = \eta_t S B$$

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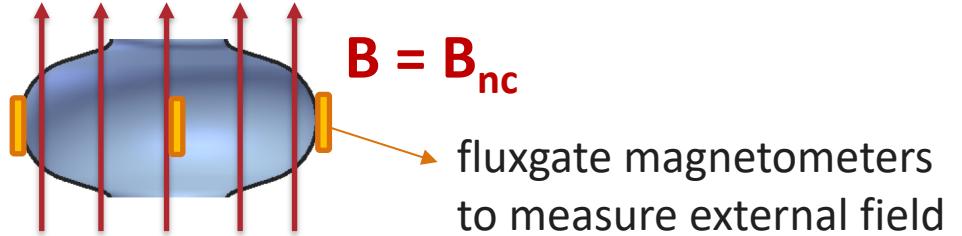


Magnetic field redistribution after SC transition

$$\eta_t = B_t/B = f(B_{sc}/B_{nc})$$

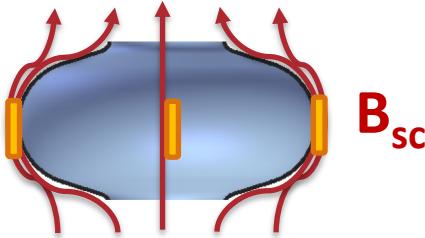
B_t : trapped magnetic field
 B_{sc}/B_{nc} : expulsion ratio

Before the SC transition:



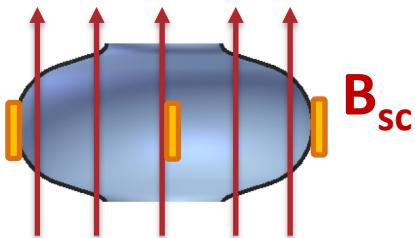
After the SC transition:

- Field completely expelled



$B_{sc}/B_{nc} = 1.74$ after complete Meissner effect (COMSOL simulation)

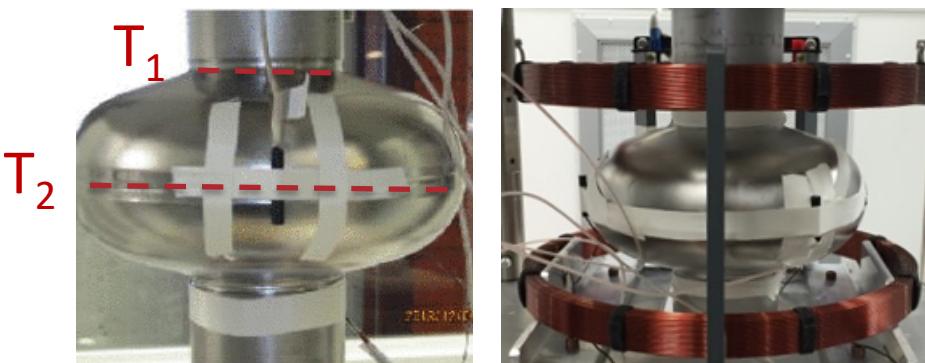
- Field completely trapped



$B_{sc}/B_{nc} = 1$ after full flux trapped

Fast cooldown helps flux expulsion

- *Fast cool-down:* large thermal gradients
→ efficient flux expulsion
- *Slow cool-down:* small thermal gradients
→ poor flux expulsion



A. Romanenko *et al.*, Appl. Phys. Lett. **105**, 234103 (2014)

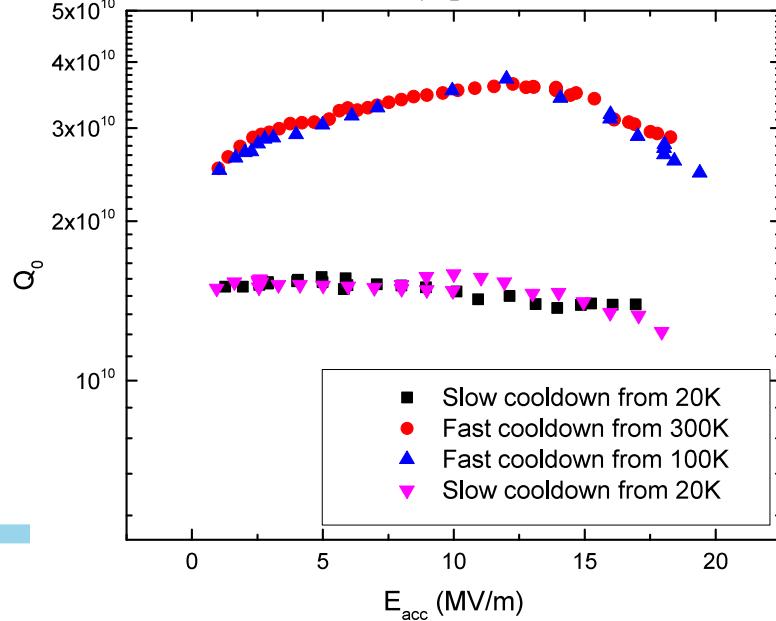
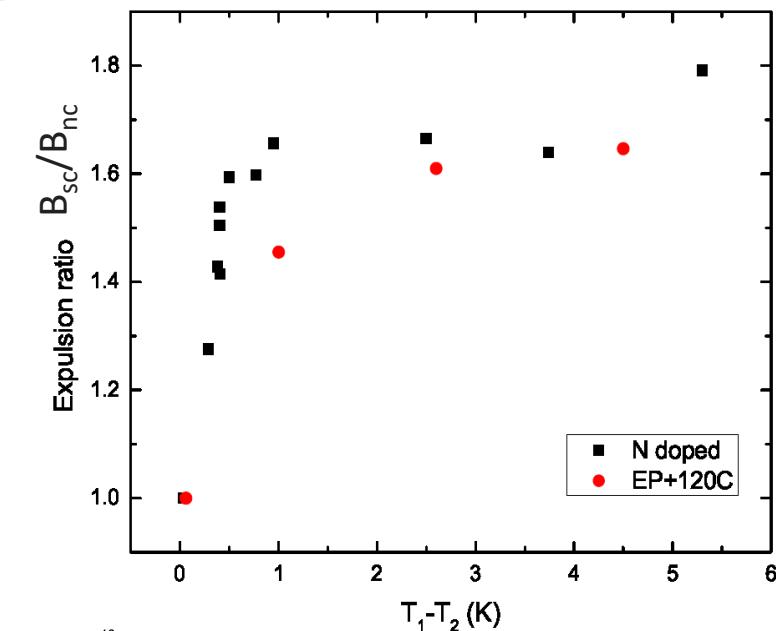
A. Romanenko *et al.*, J. Appl. Phys. **115**, 184903 (2014)

D. Gonnella *et al.*, J. Appl. Phys. **117**, 023908 (2015)

M. Martinello *et al.*, J. Appl. Phys. **118**, 044505 (2015)

S. Posen *et al.*, J. Appl. Phys. **119**, 213903 (2016)

S. Huang *et al.*, Phys. Rev. Accel. Beams **19**, 082001 (2016)



Thermodynamic force during cooldown

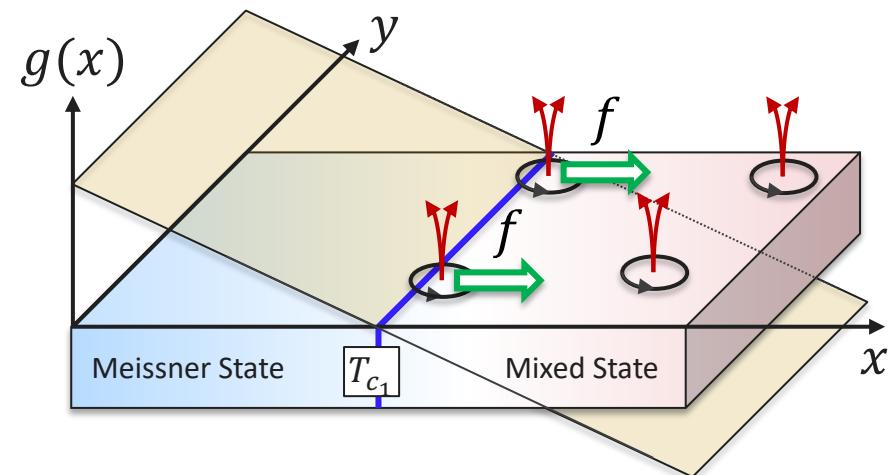
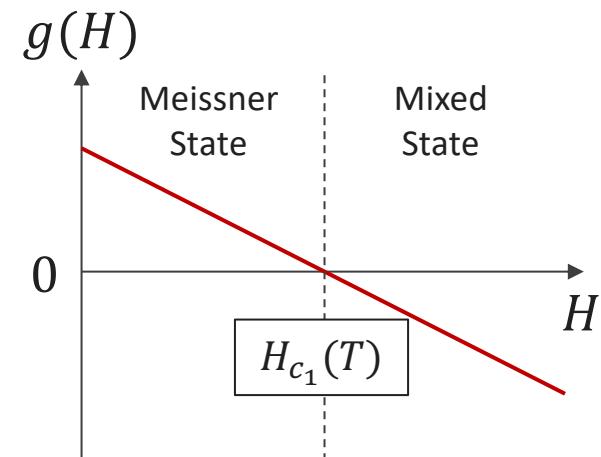
The Gibbs free energy density defines the stability of vortices in the SC:

$$g = B(H_{c_1}(T) - H)$$

We can define the *thermodynamic force* acting on the vortex as:

$$f = -\frac{\partial g}{\partial x} = -\frac{\partial g}{\partial T} \frac{\partial T}{\partial x}$$

$$f = \frac{2BH_{c_1}(0)T}{T_c^2} \nabla T$$



Critical thermal gradient

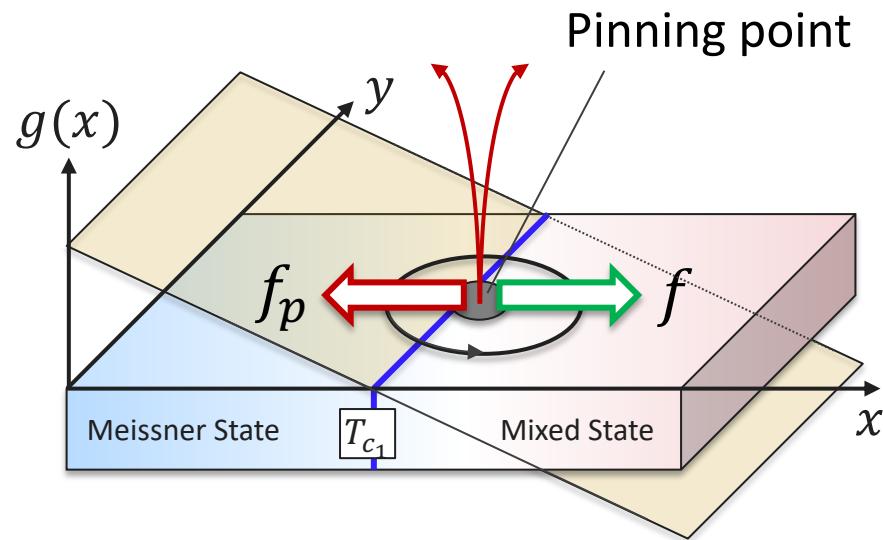
The *pinning force acting against the expulsion* is defined in terms of critical current density J_c :

$$f_p = |\bar{J}_c \times n\bar{\Phi}_0| = J_c B$$

The *minimum thermal gradient needed to expel vortices* is the critical thermal gradient ∇T_c :

$$\nabla T_c = \frac{J_c T_c^2}{2H_{c1}(0)T}$$

$$\nabla T_c \propto J_c \propto f_p$$



Statistical model for the expulsion ratio

Let's define a probability density function for flux expulsion:

→ the *probability of expelling vortices with the thermal gradient ∇T_{c_i} is $P(\nabla T_{c_i})$* , hence the expulsion ratio is:

For TESLA shape

$$B_{sc}/B_{nc} = 1 + 0.74 \cdot P(\nabla T_{c_i})$$

The model predicts $\langle J_c \rangle$ in agreement with literature^{1,2}:

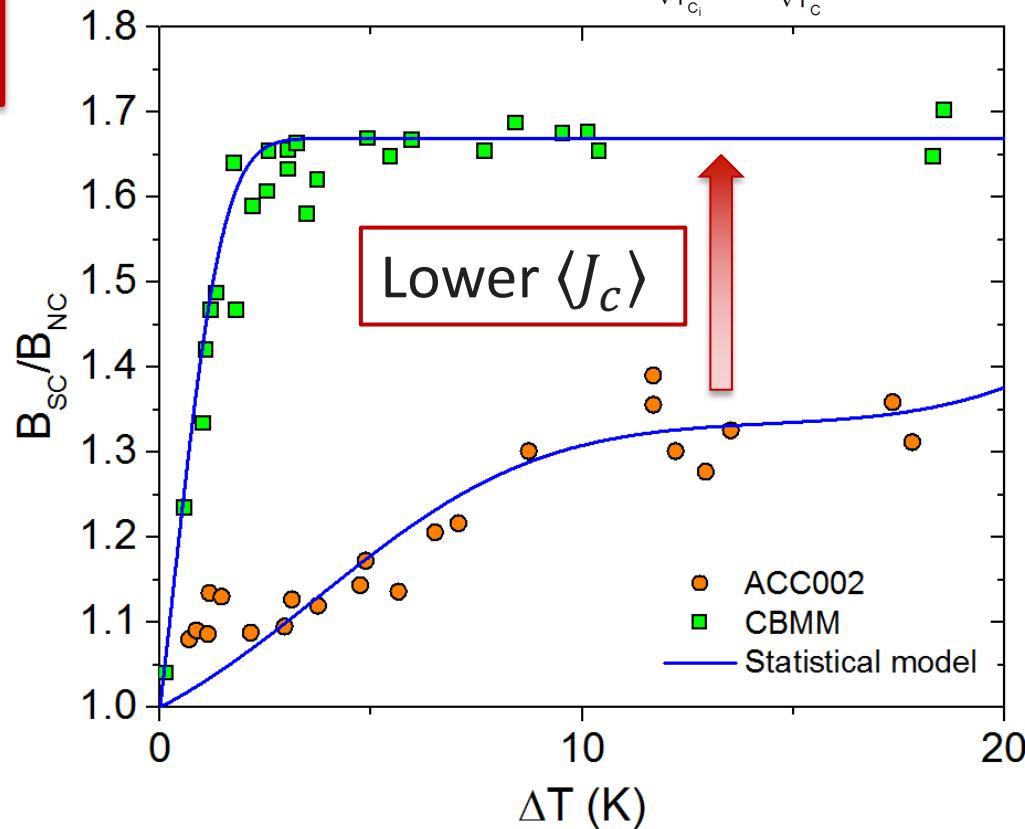
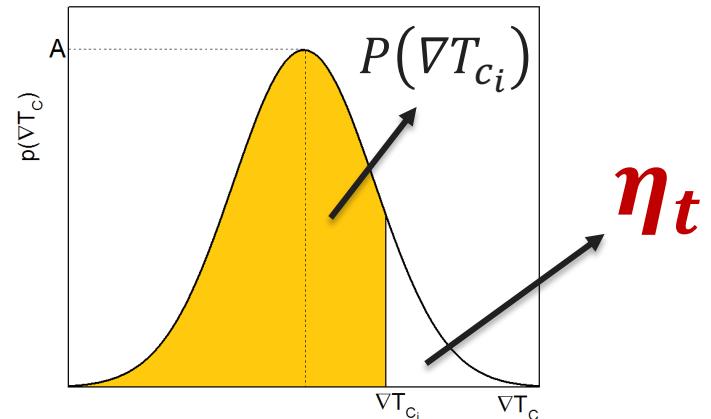
Cavity name	$\langle J_c \rangle$ (A/mm^2)
CBMM	0.3
ACC002	1.6

M. Martinello, M. Checchin *et al.*, to be published

Data: S. Posen *et al.*, J. Appl. Phys. **119**, 213903 (2016)

¹ G. Park *et al.*, Phys. Rev. Lett. **68**, 12 (1992)

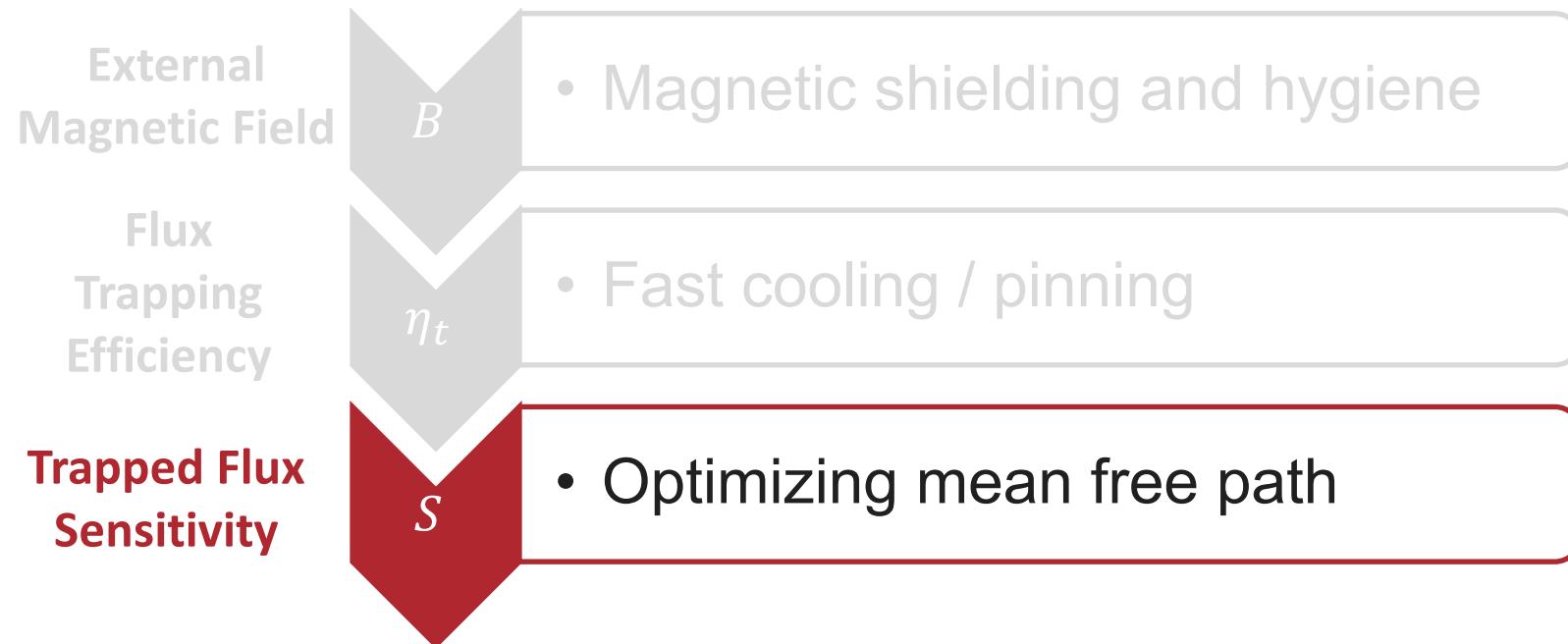
² L. H. Allen and J. H. Claassen, Phys. Rev. B **39**, 4 (1989)



Trapped flux surface resistance contributions

$$R_{fl} = \eta_t S B$$

R_{fl} can be reduced by minimizing these contributions:

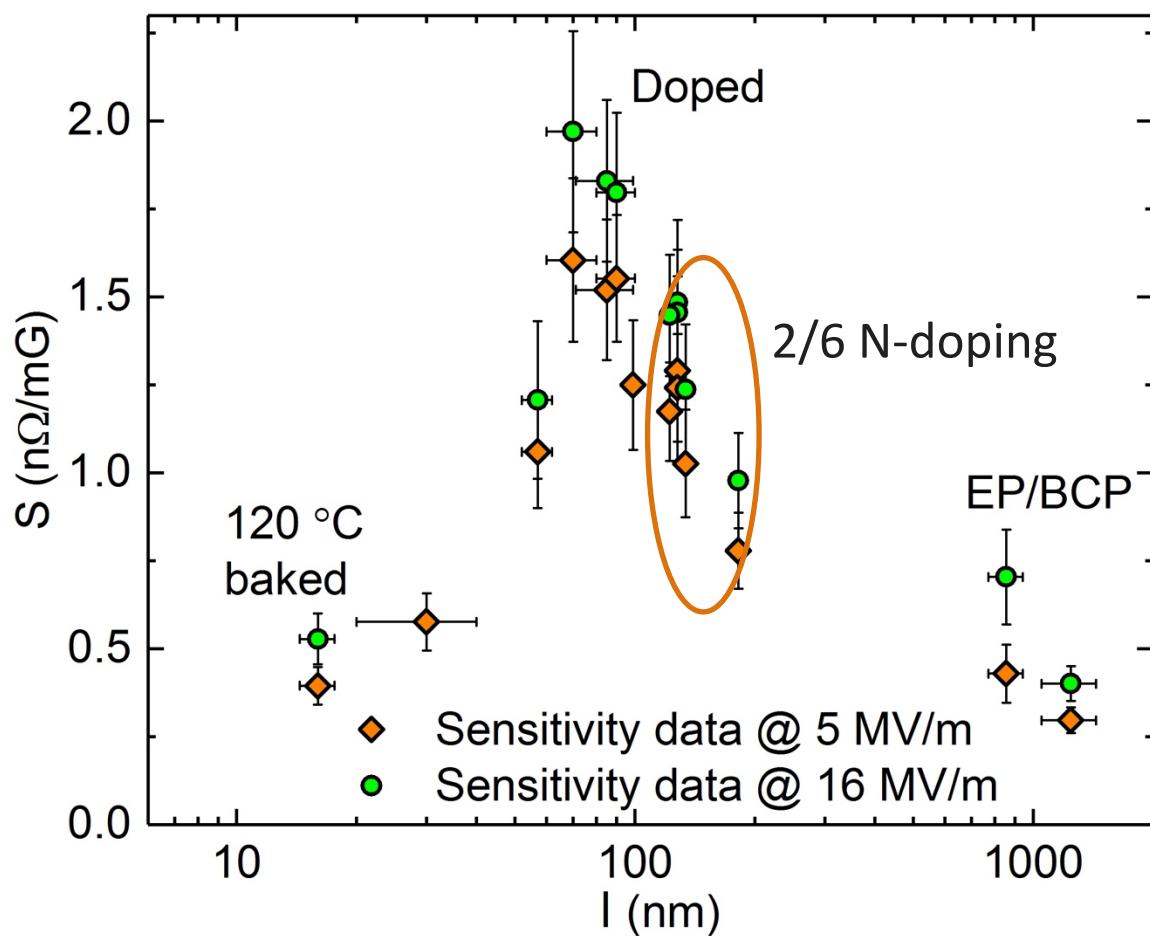


Light doping to minimize trapped flux sensitivity

Trapped flux sensitivity:

$$S = \frac{R_{fl}}{\eta_t B}$$

- Bell-shaped trend of S as a function of mean free path
- N-doping cavities present higher sensitivity than standard treated cavities
- *Light doping* is needed to *minimize* trapped flux sensitivity



M. Martinello et al., App. Phys. Lett. **109**, 062601 (2016)

D. Gonnella et al., J. Appl. Phys. **119**, 073904 (2016)

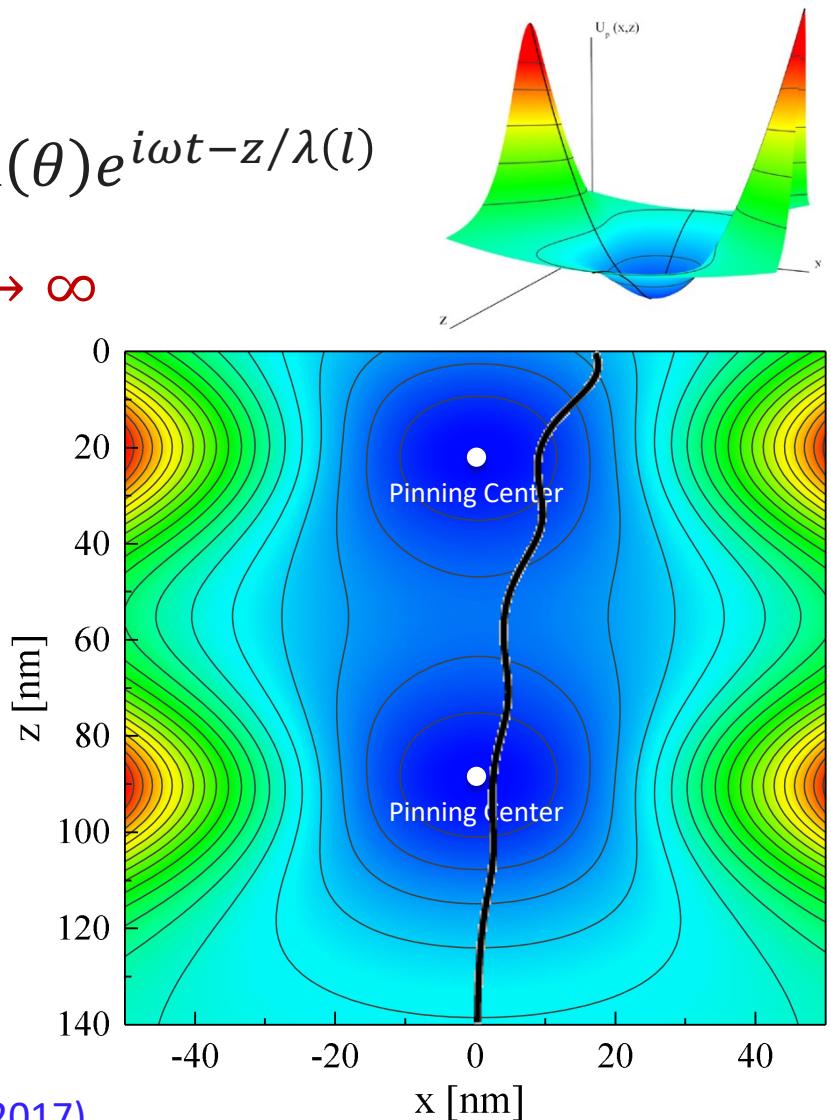
Single vortex equation of motion

The motion equation has form:

$$M(l)\ddot{x} + \eta(l)\dot{x} + p(z, l)x = j_0\phi_0 \sin(\theta) e^{i\omega t - z/\lambda(l)}$$

The solution is valid from $z = 0$ to $z \rightarrow \infty$

- The pinning potential assumed is a 2D Lorentzian function
 \Rightarrow *parabolic approximation along x*
- The pinning constant $p(z, l)$ is depth-dependent
 \Rightarrow *flexible vortex line*
- Multiple pinning centers can be considered



Sensitivity vs mean-free-path

- Small l – pinning regime $\eta \ll p$:

$$\rho_1(l, U_0) \approx \frac{\eta(l)}{p(l, U_0)^2}$$

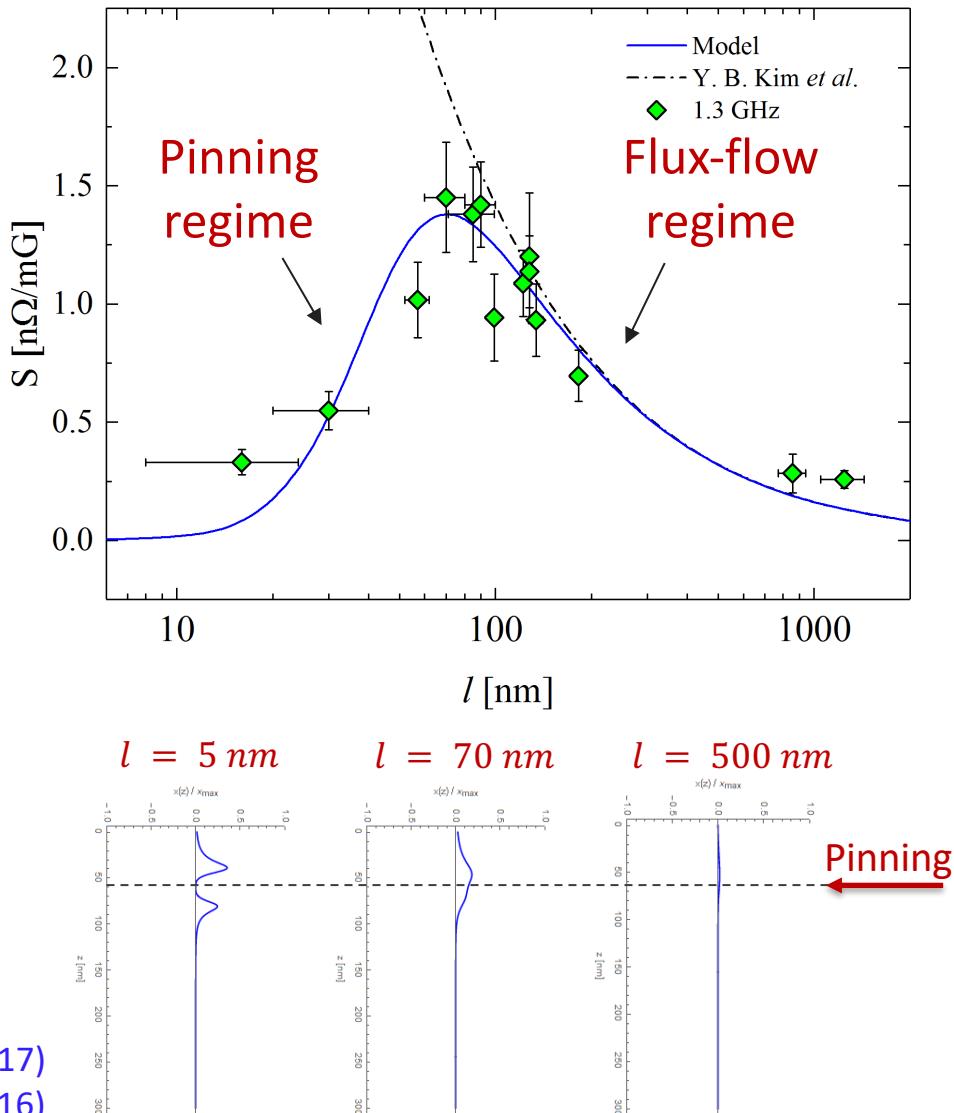
ρ_1 increases with l and ω^2 , decreases with the increasing of U_0

- Large l – flux-flow regime $\eta \gg p$:

$$\rho_1(l) \approx \frac{1}{\eta(l)}$$

ρ_1 decreases with l , independent on ω and U_0

M. Checchin et al., Supercond. Sci. Technol. **30**, 034003 (2017)
 Data: M. Martinello et al., App. Phys. Lett. **109**, 062601 (2016)



Sensitivity vs frequency

- Small l – pinning regime $\eta \ll p$:

$$\rho_1(\omega) \approx \omega^2$$

ρ_1 increases with ω^2

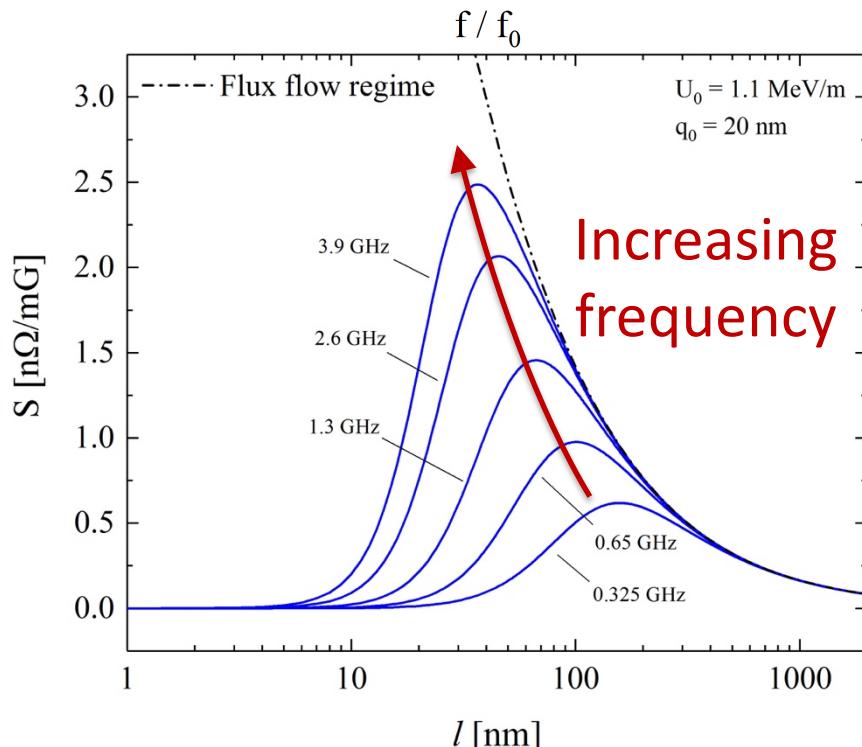
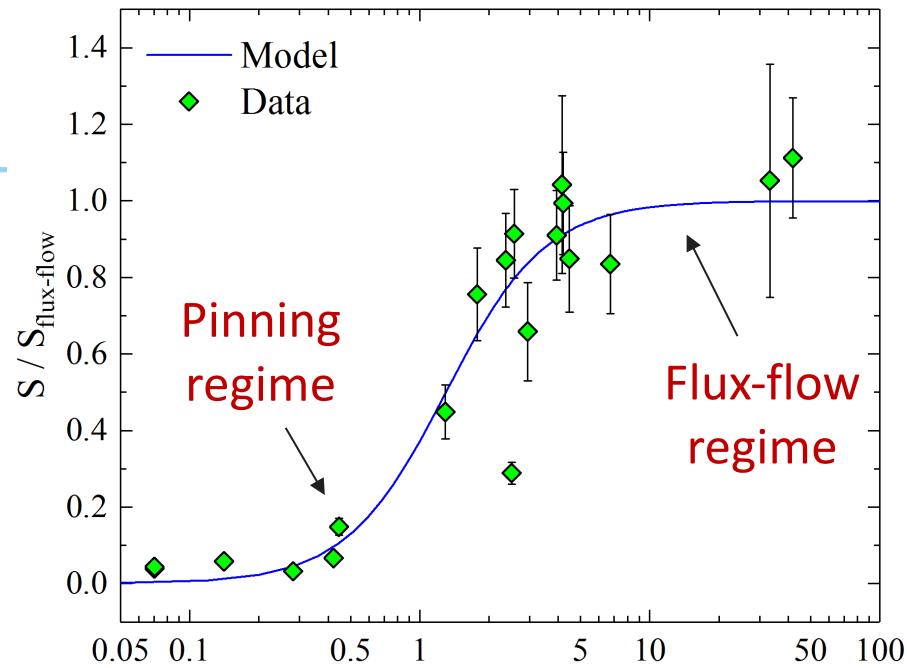
- Large l – flux-flow regime $\eta \gg p$:

$$\rho_1 = \text{constant}$$

ρ_1 independent on ω

- The higher f the higher the sensitivity peak
- *Lower frequencies* are favorable to *minimize the sensitivity*

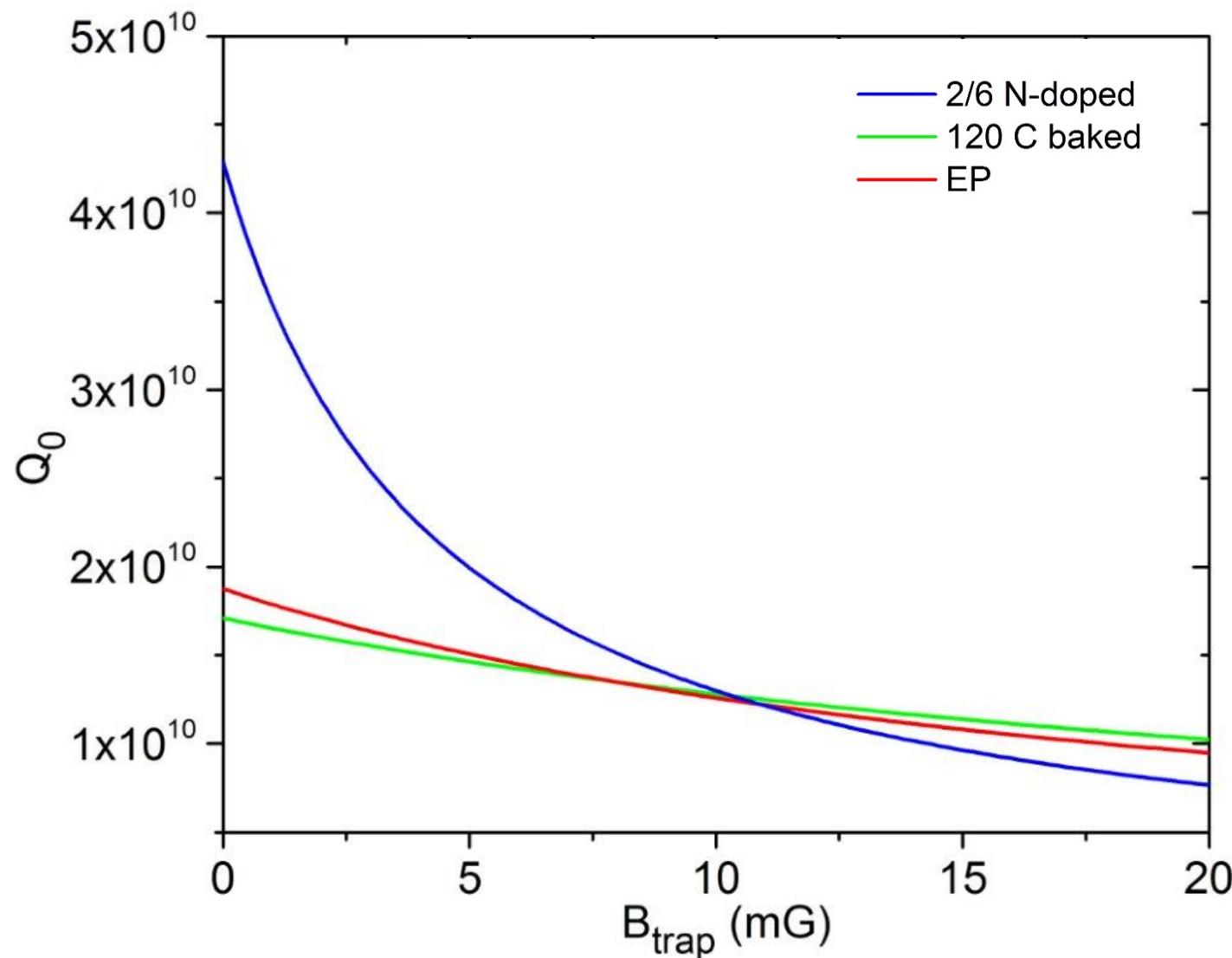
M. Checchin *et al.*, Supercond. Sci. Technol. **30**, 034003 (2017)



Summary

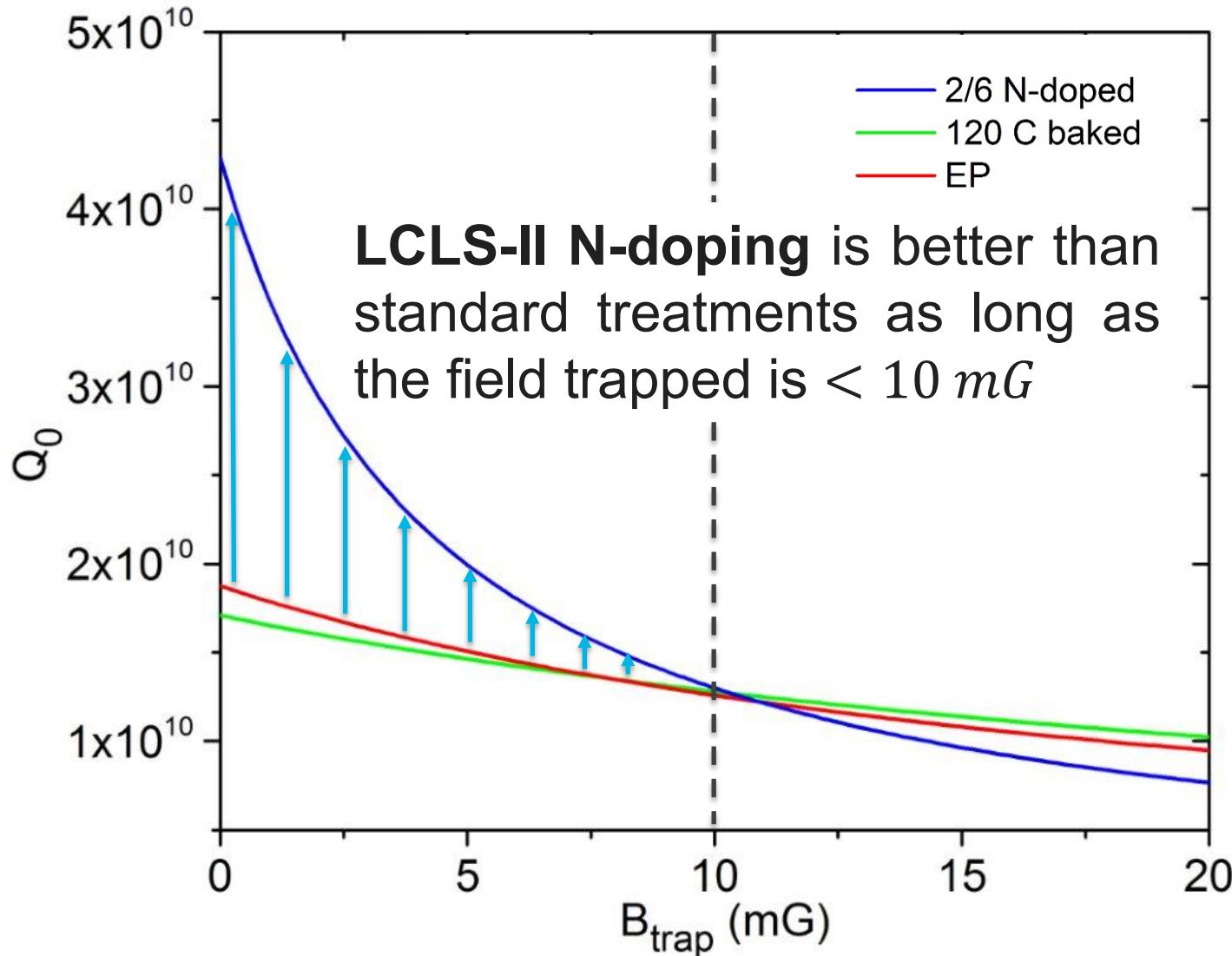
State-of-the-art surface treatment for high Q_0 at 1.3 GHz

Q_0 in condition of full flux-trapping @ 1.3 GHz



M. Martinello *et al.*, App. Phys. Lett. **109**, 062601 (2016)

Q_0 in condition of full flux-trapping @ 1.3 GHz



M. Martinello *et al.*, App. Phys. Lett. **109**, 062601 (2016)

LCLS-II prototype cryomodule test at FNAL

LCLS-II spec: 2.7×10^{10} at 16 MV/m

Cavity	Usable Gradient* [MV/m]	Cryomodule Q ₀ @16MV/m** Fast Cool Down
TB9AES021	18.2	2.6e10
TB9AES019	18.8	3.1e10
TB9AES026	19.8	3.6e10
TB9AES024	20.5	3.1e10
TB9AES028	14.2	2.6e10
TB9AES016	16.9	3.3e10
TB9AES022	19.4	3.3e10
TB9AES027	17.5	2.3e10
Average	18.2	3.0e10
Total Voltage	148.1 MV	

Acceptance = 128 MV

* Radiation <50 mR/h

** TB9AES028 Q₀ was at 14 MV/m

courtesy of G. Wu



Frequency dependence study

We are now extending the same study to *different frequencies* and *many surface treatments* (EP, 120 C bake, N-doping and N-infusion)....



The initial results are extremely interesting....**STAY TUNED!**

Conclusions

Conclusions

- N-doping and N-infusion both increases Q_0
- $R_{fl} = \eta_t S B$ can be minimized by:
 - Efficient magnetic field shielding (low B)
 - Fast cooling, minimize pinning (low η_t)
 - Decreasing as much as possible the sensitivity (low S)
- Two different regimes of vortex dissipation
 - Small l , *pinning regime*: ρ_1 increases if $l \uparrow$, $\omega^2 \uparrow$ and $U_0 \downarrow$
 - Large l , *flux-flow regime*: ρ_1 decreases if $l \uparrow$, but independent on ω and U_0
- Only by understanding R_{fl} N-doping could be successfully implemented to mass production
 - LCLS-II cryomodule specification exceeded

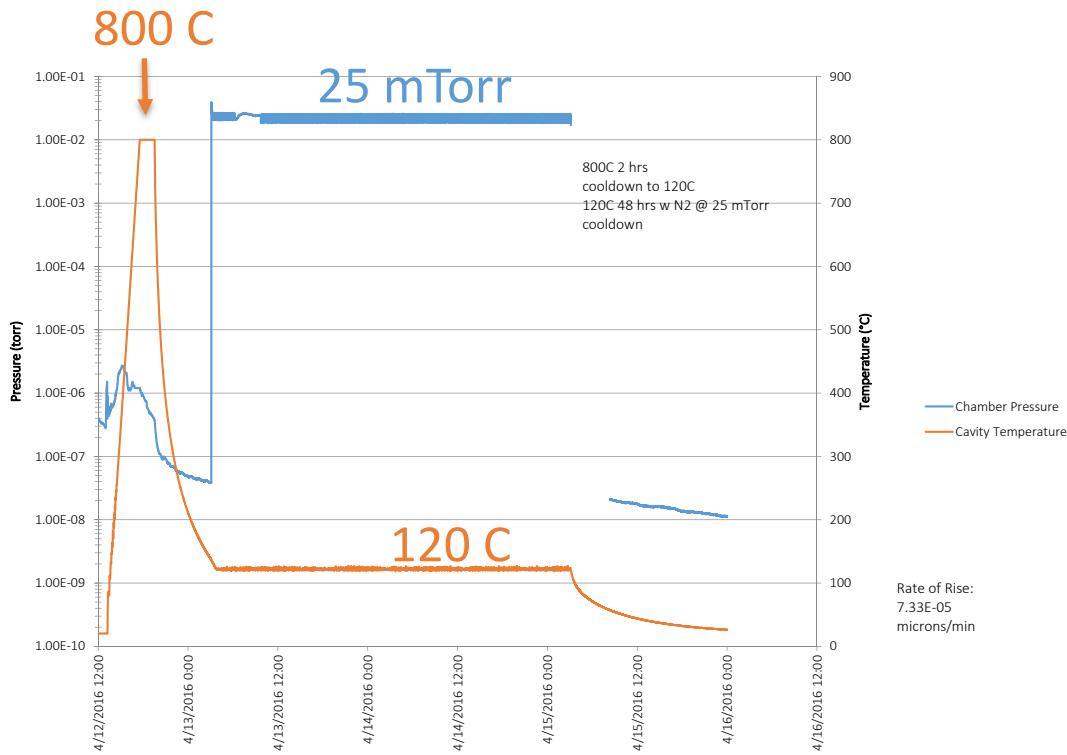
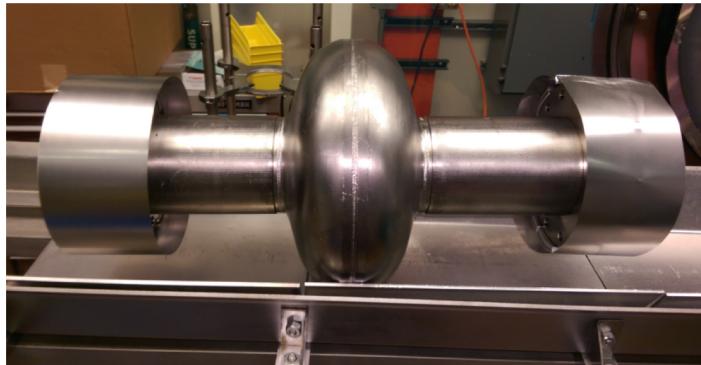
Thank you for the attention



Back-up slides

N-infusion thermal process

- Bulk electro-polishing
- High T furnace with caps to avoid furnace contamination:
 - 3h @ 800C in HV
 - 48h @ 120-160 C with N₂ (25 mTorr)
 - Optional annealing 48h @ 120-160 C
- NO chemistry post furnace
- HPR, VT assembly



Protective caps and foils are BCP'd prior to every furnace cycle and assembled in clean room, prior to transporting the cavity to furnace area

Statistical definition of trapping efficiency

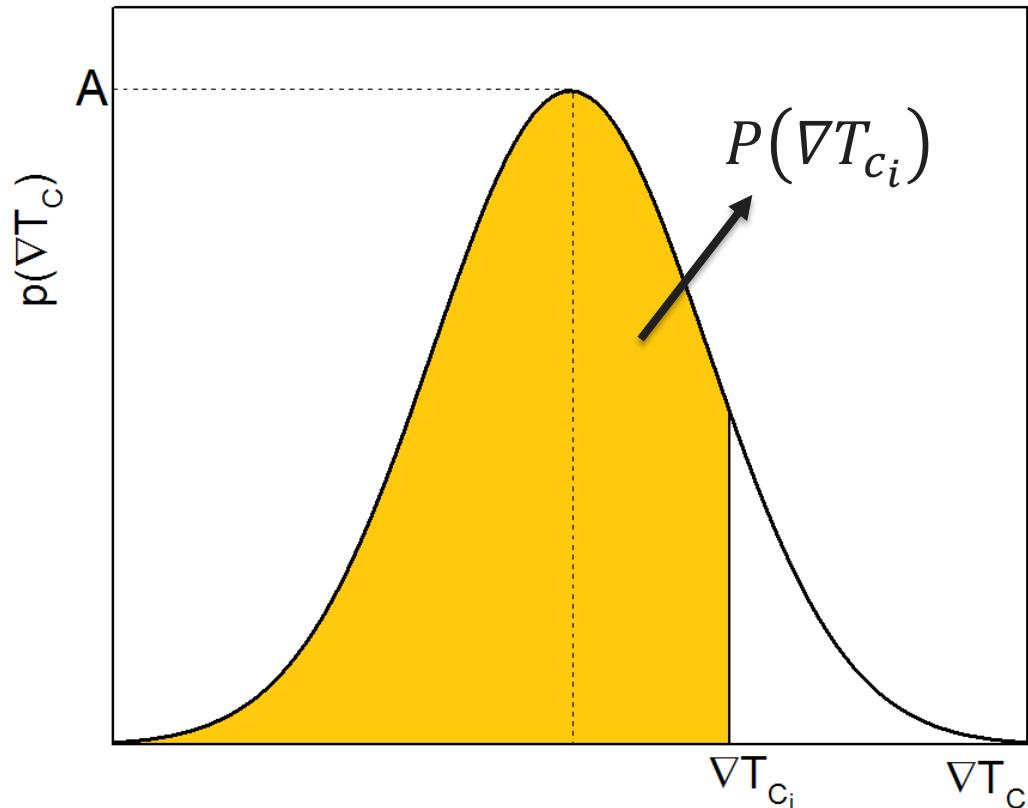
- The probability of expelling vortices with the thermal gradient ∇T_{c_i} is $P(\nabla T_{c_i})$
- The trapping efficiency η_t is function of ∇T_{c_i} :

$$\eta_t = [1 - P(\nabla T_{c_i})]$$

$$P(\nabla T_{c_i}) = \int_0^{\nabla T_{c_i}} p(\nabla T_c) d\nabla T_c$$

- The trapped field is then:

$$B_t = \eta_t B = B[1 - P(\nabla T_{c_i})]$$

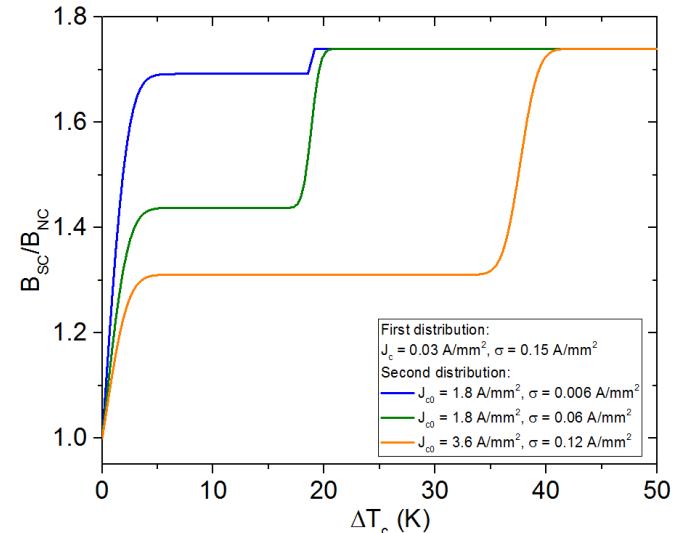
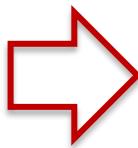
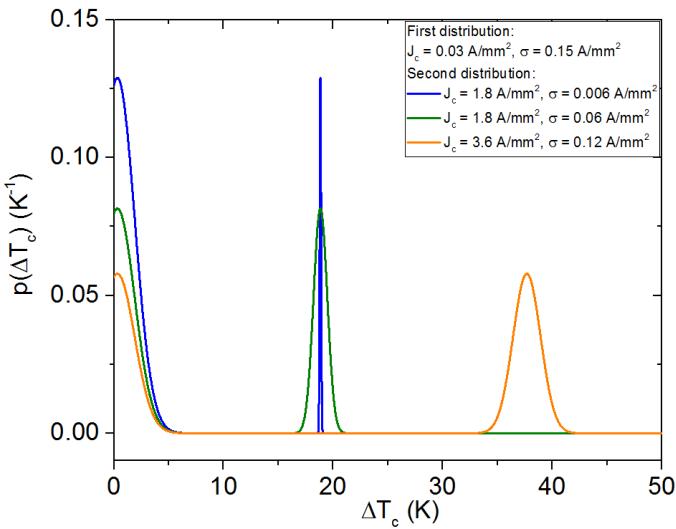


For TESLA shape



$$\frac{B_{sc}}{B_{nc}} = 1 + 0.74 \cdot P(\nabla T_{c_i})$$

Double-peaked probability density function

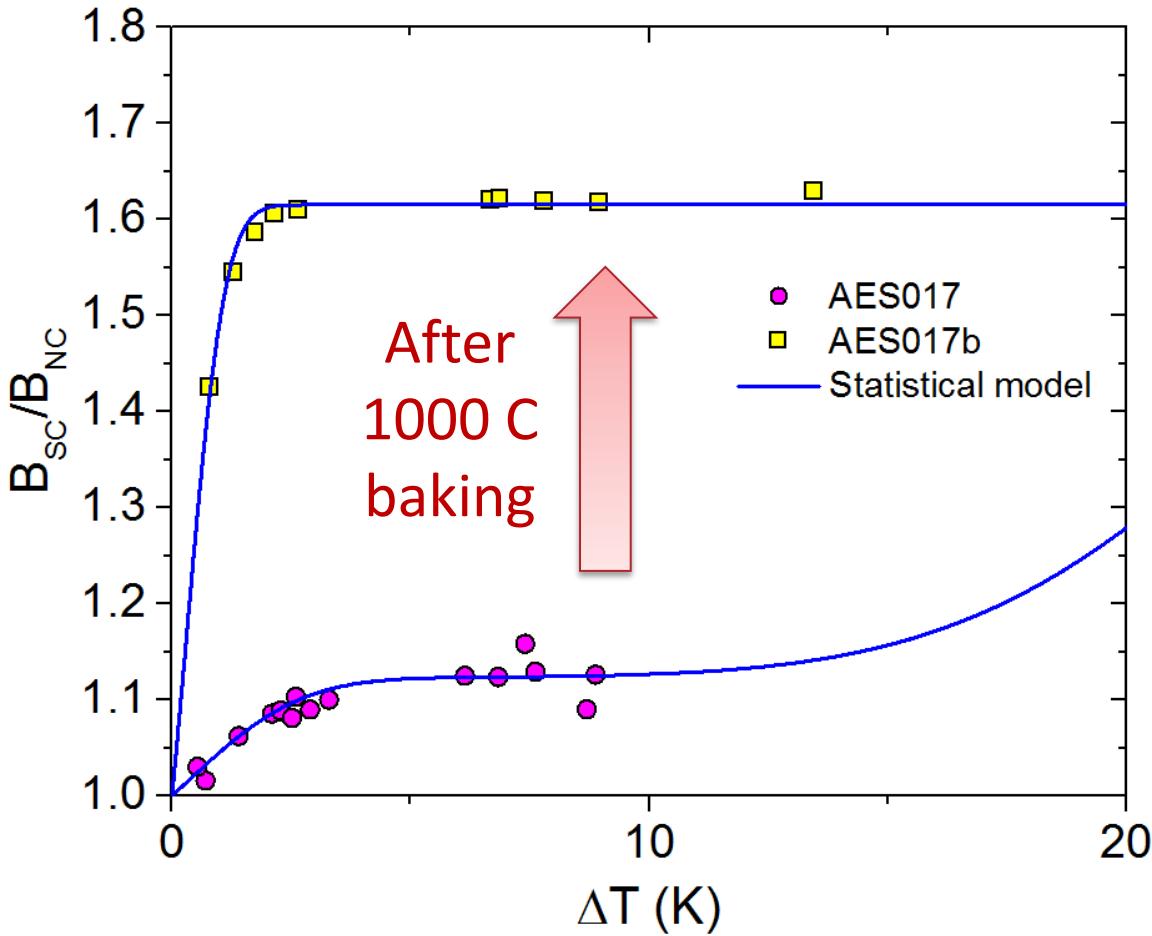
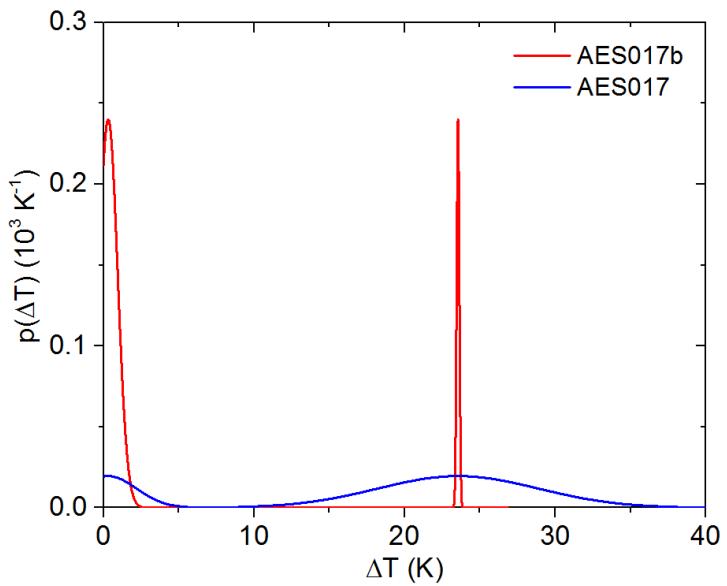


- Double distribution of pinning centers (e.g. dislocations + grain boundaries)
- $p(\Delta T_c \rightarrow 0) \neq 0 \Rightarrow$ finite probability that vortices are not pinned
- First plateau defined by the ratio of the two peaks' area
- Complete flux expulsion reached when ΔT_c is larger enough so that $P(\Delta T_c) = 1$

High T baking effects

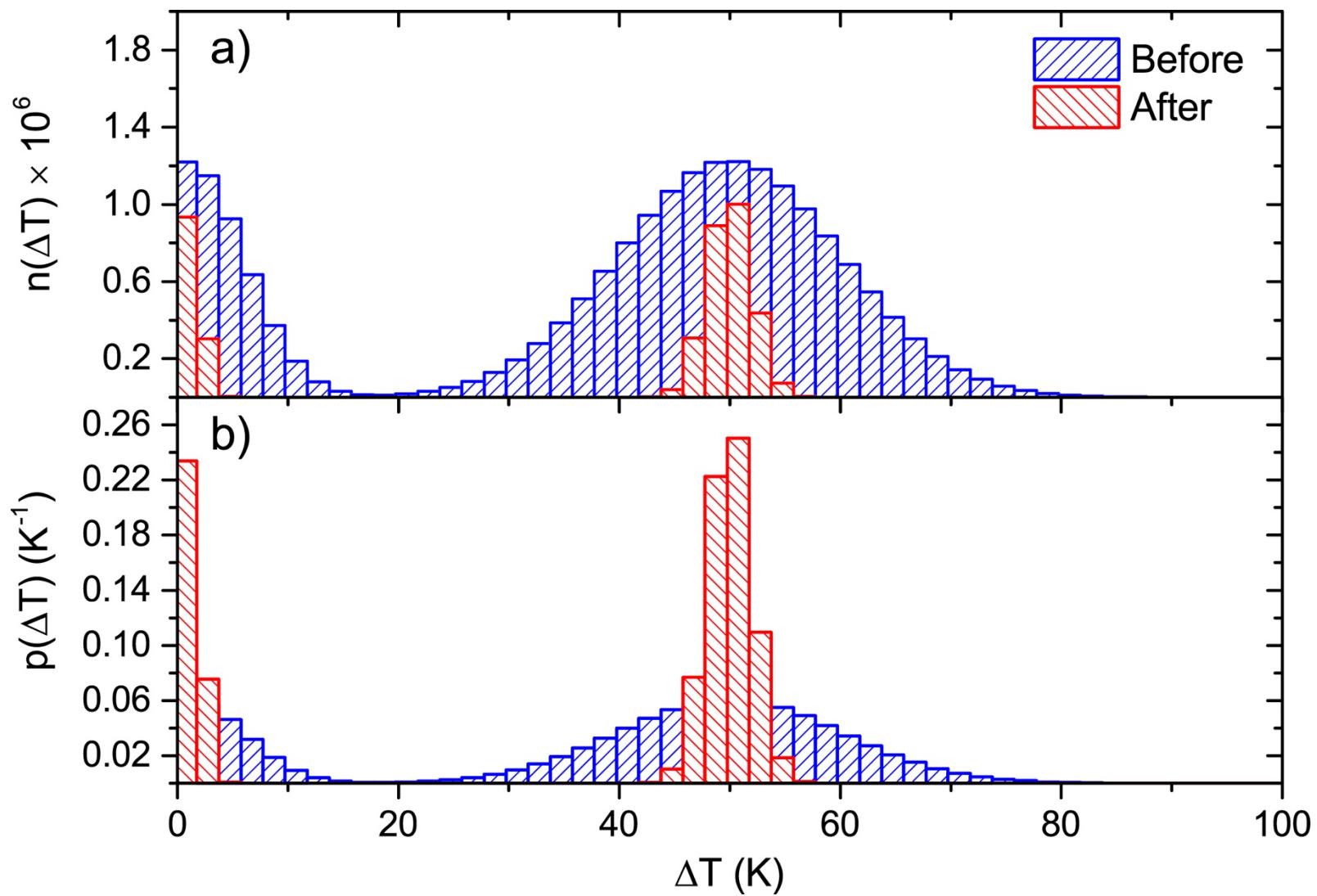
High T baking effects:

- Decreases the number of pinning points
→ pdf narrowing
- Smaller J_c



M. Martinello, M. Checchin *et al.*, to be published
Data: S. Posen *et al.*, J. Appl. Phys. **119**, 213903 (2016)

Pdf before/after 1000 C annealing example

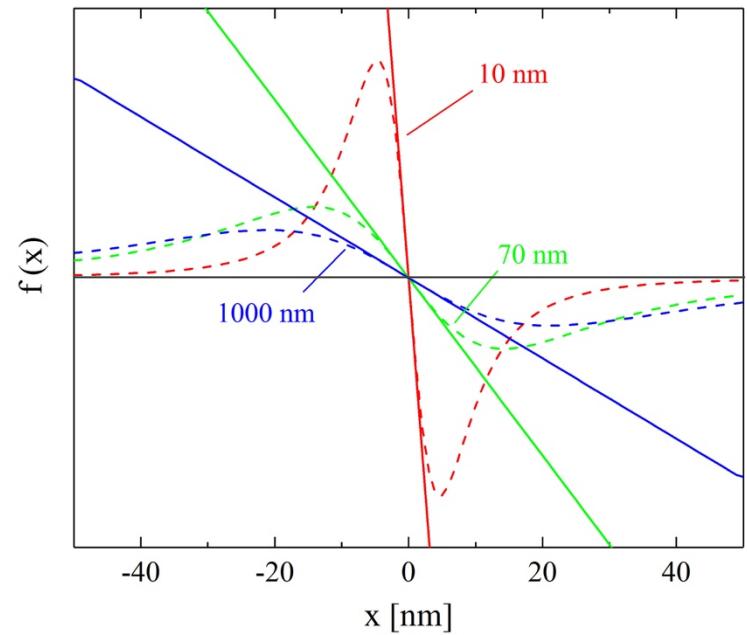
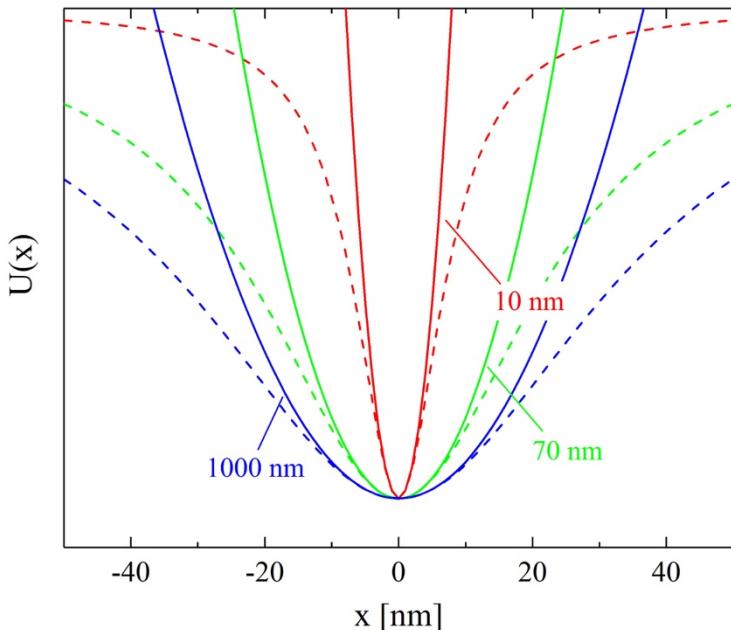


M. Martinello, M. Checchin *et al.*, to be published

Pinning potential

The smaller l , the steeper the potential:

$$\begin{aligned} U_p(z) &= - \sum_{i=0}^n \frac{U_{0i}\xi^2}{\xi^2 + x^2 + (z - q_i)^2} \\ &\approx - \sum_{i=0}^n \frac{U_{0i}\xi^2}{\xi^2 + (z - q_i)^2} + \sum_{i=0}^n \frac{U_{0i}\xi^2}{[\xi^2 + (z - q_i)^2]^2} x^2 \end{aligned}$$



M. Checchin *et al.*, Supercond. Sci. Technol. **30**, 034003 (2017)

Vortex surface impedance

The *complex resistivity* of the vortex line follows from the calculation of the apparent power (active plus reactive power) :

$$\rho(z, l) = \rho_1 + i\rho_2 = \frac{\phi_0^2 \sin^2(\theta)}{\pi \xi_0^2 [(p - M\omega^2)^2 + (\eta\omega)^2]} [\eta\omega + i(p - M\omega^2)]$$

The vortex surface impedance (using the classic definition of Z) is then:

$$Z(l) = \frac{\pi \xi_0^2 B}{\phi_0} \int_0^{q_0^\vee} \int_{U_{00}^\wedge}^{U_{00}^\vee} \cdots \int_0^{q_n^\vee} \int_{U_{0n}^\wedge}^{U_{0n}^\vee} \frac{\prod_{i=0}^n \Gamma(q_i) \Lambda(U_{0i})}{\int_0^L \frac{e^{-z/\lambda}}{\rho(z, l)} dz} dU_{00} dq_0 \cdots dU_{0n} dq_n$$

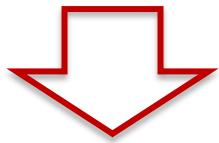
Number of
vortices B/B_{vortex}

Vortex impedance weighted over normal
distributions of pinning positions and strengths

Pinning strength dependence

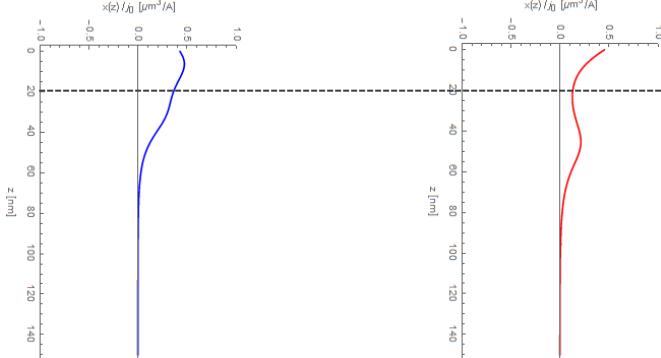
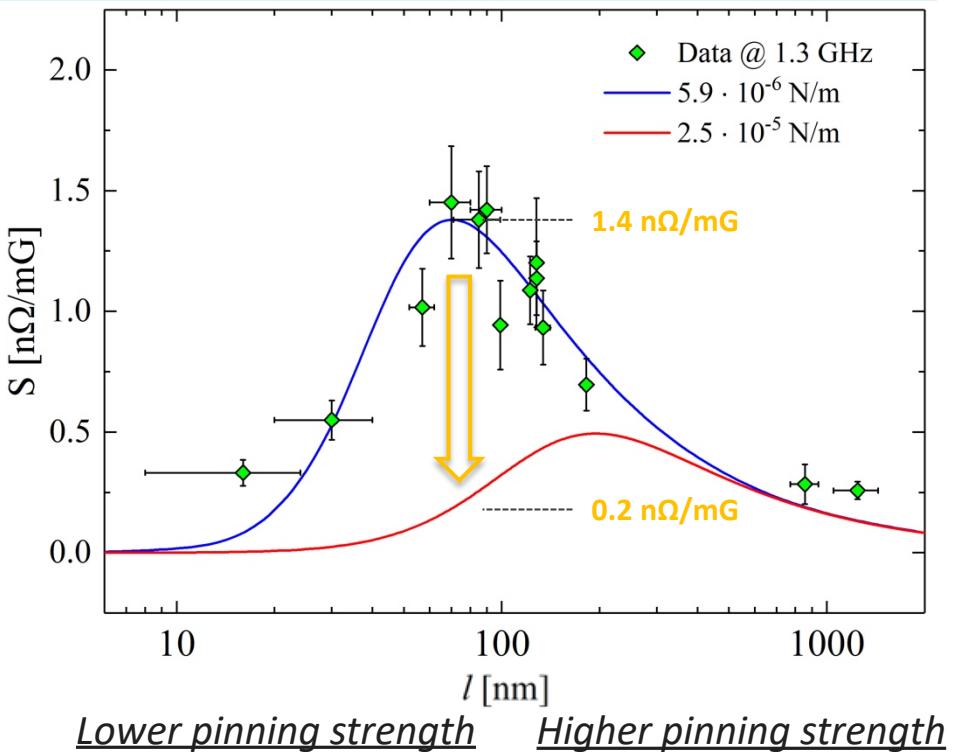
The higher the pinning force, the more constrained the oscillation

Dirtier or more defective materials (e.g. thin films) have larger pinning strength



Lower sensitivity!

By increasing the pinning force of one order of magnitude the sensitivity is 7 times smaller!

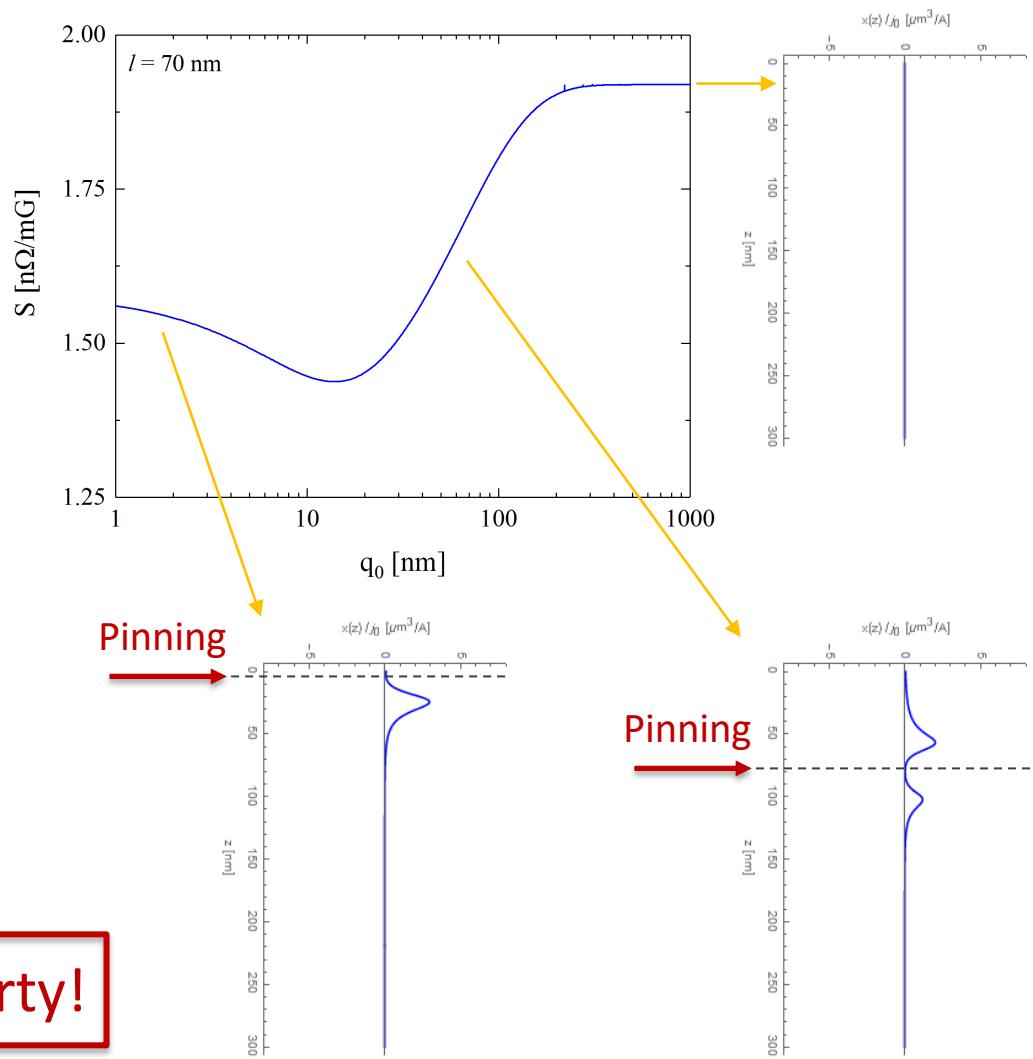


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Sensitivity vs pinning site depth

- Vortex dissipation is a *near-surface property*
- The pinning site distance from the surface q_0 determines the resistance
- For instance, if $l = 70 \text{ nm}$:
 - $q_0 \cong 15 \text{ nm} \Rightarrow$ *sensitivity is the lowest*
 - $q_0 > 400 \text{ nm} \Rightarrow$ *constant sensitivity*
 - bulk pinning does not affect the vortex oscillation!*

⇒ S is a near surface property!



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