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Electron Cooler Introduced Perturbations on Ion Beam

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- General requirements of e-cooling Parallel and similar velocity of e-beam and ion-beam
- Lower electron beam temperature
- Adequate cooling force (n_e, L_e)
- Neglectable or compensable influence on ion beam
- List of perturbations and their compensations (to 1st order)
- Main solenoid → coupling and focusing ← solenoid
- Toroids → transversal bending ← correction dipoles
- Space charge and current of e-beam -> focusing Fring Quadrupoles



- The perturbation of e-beam may help to understand the following problems:
- Why high e-beam current not be used to cool low energy beam?
 - Large tune shift and tune shift change during acceleration
- Low ac/deceleration efficiency.
 - Change of tune shift and matching condition
- Effects induced by the pulsed electron beam cooling.
- Electron cooler perturbations (solenoid and e-beam) in Hamiltonian representations:

The perturbation of e-beam field

Electron-beam space charge → e-field focusing, acc. and deacc. at ends

$$\vec{E}(\vec{r}) = -\frac{n e}{2\varepsilon_0} \vec{r}$$
, $K_E = \frac{n e}{2\varepsilon_0 \beta c B \rho}$ (main) (cooling is also from the E-field, with decreasing emittance)

Electron-beam current → magnet field defocusing

$$\vec{B}(\vec{r}) = \frac{\mu_0}{2 \pi r^2} \vec{I} \times \vec{r} = \frac{\mu_0 n e c}{2 r} \vec{\beta} \times \vec{r} ,$$

$$K_B = -\frac{\mu_0 n e \beta c}{2 R \rho} = -\beta^2 K_E$$

• Total electromagnetic field:

$$k = K_E + K_B = (1 - \beta^2) \frac{n e}{2\epsilon_0 \beta c B \rho}$$
 for ion beam

End and bending parts of e-beam field: higher order and short length, neglected

Transport Matrix of Independent Components

Solenoid:

$$R_{so} = \begin{pmatrix} \cos^2(k_s L) & \sin(2k_s L)/2k_s & \sin(2k_s L)/2 & \sin^2(k_s L)/k_s & 0 & 0 \\ -k_s \sin(2k_s L)/2 & \cos^2(k_s L) & -k_s \sin^2(k_s L) & \sin(2k_s L)/2 & 0 & 0 \\ -\sin(2k_s L)/2 & -\sin^2(k_s L)/k_s & \cos^2(k_s L) & \sin(2k_s L)/2k_s & 0 & 0 \\ k_s \sin^2(k_s L) & -\sin(2k_s L)/2 & -k_s \sin(2k_s L)/2 & \cos^2(k_s L) & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & L/\gamma^2 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

$$L \text{ is the length of solenoid or e-beam} \quad k_s = \frac{Bs}{2B\rho} \quad k = \frac{n \, e(1 - \beta^2)}{2\epsilon_0 \, \beta \, c \, B\rho}$$

Electron beam field:

$$R_{ef} = \begin{bmatrix} \cos(\sqrt{k}L) & \frac{1}{\sqrt{k}}\sin(\sqrt{k}L) & 0 & 0 \\ -\sqrt{k}\sin(\sqrt{k}L) & \cos(\sqrt{k}L) & 0 & 0 \\ 0 & 0 & \cos(\sqrt{k}L) & \frac{1}{\sqrt{k}}\sin(\sqrt{k}L) \\ 0 & 0 & -\sqrt{k}\cdot\sin(\sqrt{k}L) & \cos(\sqrt{k}L) \end{bmatrix} \begin{array}{c} \textbf{Drift:} \\ R_f = \begin{bmatrix} 1 & L & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & L \\ 0 & 0 & 0 & 1 \end{bmatrix} \end{array}$$

Transport Matrix of e-cooler

- The combined transport matrix in the electron cooler should be analyzed.
- Lie algebraic method was used to find the polynomial expression of each matrix

elements. Here, $f = -L \cdot H = -L \cdot \left[\frac{(x' + ksy)^2 + (y' + ksx)^2}{2} + k \frac{x^2 + y^2}{2} \right]$. Lie operator $[f,g] = \sum_{k=1}^{\infty} \left(\frac{\partial f}{\partial q_k} \frac{\partial g}{\partial p_k} - \frac{\partial f}{\partial p_k} \frac{\partial g}{\partial q_k} \right) \quad : f:g = [f,g] \text{ and } e^{:f:}g = \sum_{k=0}^{\infty} \frac{:f:^k}{k!}g.$

Then we found the transport matrix of solenoid + e-beam field as:

 $\cos(KL)\cos(k_sL)$ $\sin(KL)\cos(k_sL)/K$ $\cos(KL)\sin(k_sL)$: - $K\sin(KL)\cos(k_sL)$ $\cos(KL)\cos(k_sL)$ - $K\sin(KL)\sin(k_sL)$ $\sin(Kz)\sin(k_sz)/K$ $-K\sin(KL)\cos(k_sL)$ $\cos(KL)\sin(k_sL)$ $\begin{array}{cccc} \sin(Kz)\sin(k_sz)/K & \cos(KL)\cos(k_sL) \\ -\cos(KL)\sin(k_sL) & -K\sin(KL)\cos(k_sL) \\ K & 0 & \sqrt{\cos(k_sL)} \end{array}$ $-\cos(KL)\sin(k_sL)$ $\sin(KL)\cos(k_sL)/K$ $\begin{array}{ccc} K \sin(KL)\sin(k_sL) & -\\ \cos(KL) & \sin(KL)/K \\ -K \sin(KL) & \cos(KL) \end{array}$ $\cos(KL)\cos(k_sL)$ $\int \sin(k_sL)$ 0 $\cos(k_s L)$ $\sin(k_s L)$ $\begin{vmatrix}
\cos(KL) & \sin(KL)/K \\
-K\sin(KL) & \cos(KL)
\end{vmatrix} - \sin(k_sL)$ 0 $-\sin(k_s L)$ $\cos(k_s L)$ Focusing

 $k_S = \frac{BS}{2B\rho}$, $k = k_E + k_B = \frac{n \ e(1-\beta^2)}{2\varepsilon_0 \ \beta c \ B\rho}$ Where: $K = \sqrt{k + k_s^2}$,







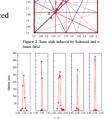
Hint: a hollow e-beam is preferred to reduce the perturbation, if cooling was sufficient in this case.

The Applications of the Transport Matrix

- The perturbation of e-beam may introduce additional tune shift and change the acceptance. The tune shift and acceptance change continuously during ac/deceleration or "mismatched" pulse cooling. This help to understand the following problems:
- 1. Why high e-beam current not be used to cool low energy beam? Example, CSRm 395G, L_e =2.56m/ r_e =3cm / I_e =0.33A / $\langle \beta_x \rangle$ =10m Case 1:²³⁸U³⁰-1.0 MeV/u \Rightarrow k=0.03/m², k_s ²=0.0003/m², $\Delta Q_{x,y}$ =0.061 Case 2: ${}^{12}C^{6+}$ -7.0 MeV/u $\Rightarrow k$ =0.0064/m², k_s ²=0.0007/m², $\Delta Q_{x,y}$ =0.013

k Tune X Tune Y Max βx (m) Max βy (m) 0 3.630 2.624 14.99 30.16 0.01 3.679 2.695 16.95 53.89 0.02 3.709 2.736 0.03 3.735 2.773 19.53 2. Instability and fast decay effects induced

- by the pulsed electron beam cooling. (L.J.Mao et al. COOL2007). This 'naturally' explained the experimental
- Low de/acceleration efficiency.
 Example: Deceleration of Ni²⁸⁺ from 400MeV/u to 4MeV/u at ESR/GSI. 1/6 efficiency to theory one. e-beam field may limit the efficiency. (Frank Herfurth, report, 2017)



Summary

