



BPM Technologies for Quadrupolar Moment Measurements

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Outline

- Introduction
- Problem Overview - Fundamental Limitations
- New Approach based on Movable BPMs
- Preliminary Tests
- Differential Measurements
- Conclusion

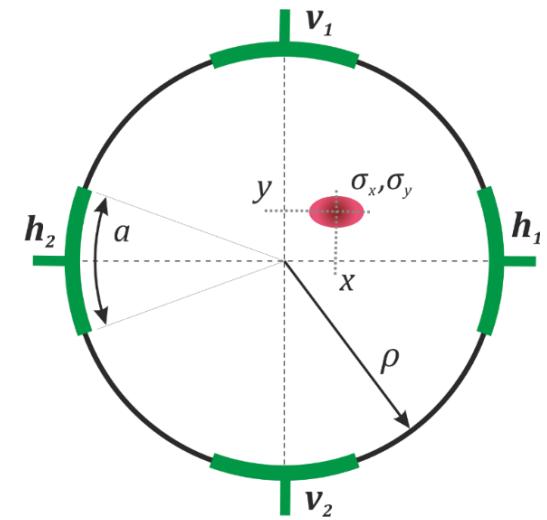
Introduction

What is a Quadrupolar Pick-Up (PU)?

- an **electromagnetic Pick-Up**, e.g. a *BPM*
- measures the 2nd order term (**quadrupolar moment**) of the electrode signals.

$$U_{h1} \propto \frac{a}{2\pi} + \frac{1}{\rho} \frac{2\sin(a/2)}{\pi} x \\ + \frac{1}{\rho^2} \frac{\sin(a)}{\pi} (\sigma_x^2 - \sigma_y^2 + x^2 - y^2) + \dots$$

Quadrupolar Term



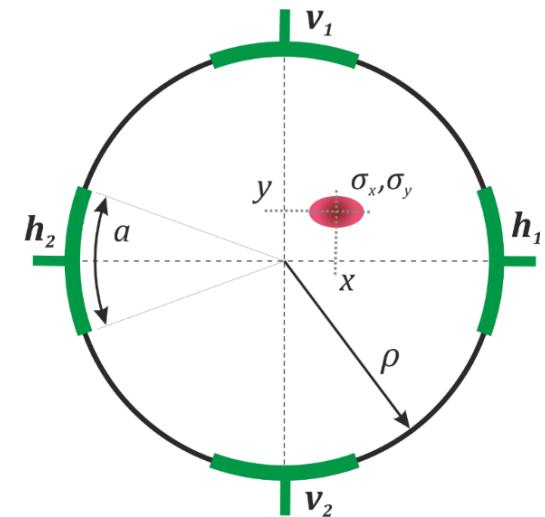
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Quadrupolar Term



Motivation

Support Beam Size / Emittance measurements

- Non-intercepting
- Existing PU technology (BPMs)
- Energy independent

Wire Scanners (WS)

- Partially distractive
- Limited by Intensity

Synchrotron Light Monitors (BSRT)

- Limitations during energy ramp
- Need WS for calibration

Standard Measurement Technique

PU signals as a **multipole expansion**

$$U_{h1} = i_b [c_0 + c_1 D_x + c_2 \mathbf{Q} + \dots]$$

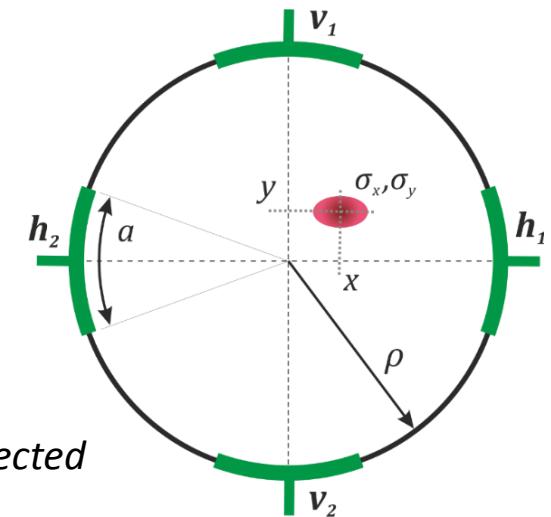
$$U_{h2} = i_b [c_0 - c_1 D_x + c_2 \mathbf{Q} + \dots]$$

$$U_{v1} = i_b [c_0 + c_1 D_y - c_2 \mathbf{Q} + \dots]$$

$$U_{v2} = i_b [c_0 - c_1 D_y - c_2 \mathbf{Q} + \dots]$$

↑ *Quadrupolar Term*

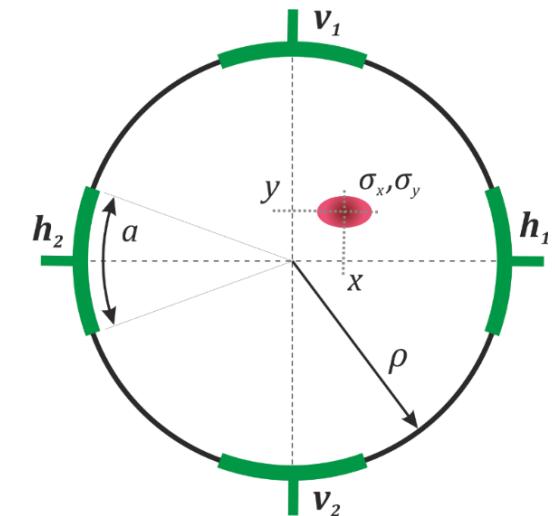
*High order terms
can be fairly neglected*



Standard Measurement Technique

PU signals as a **multipole expansion**

$$\begin{aligned} \Sigma_{hor} & \left\{ \begin{array}{l} U_{h1} = i_b [c_0 + c_1 D_x + c_2 \mathbf{Q} + \dots] \\ U_{h2} = i_b [c_0 - c_1 D_x + c_2 \mathbf{Q} + \dots] \end{array} \right. \\ \Sigma_{ver} & \left\{ \begin{array}{l} U_{v1} = i_b [c_0 + c_1 D_y - c_2 \mathbf{Q} + \dots] \\ U_{v2} = i_b [c_0 - c_1 D_y - c_2 \mathbf{Q} + \dots] \end{array} \right. \end{aligned}$$



Cancel Dipolar moments

$$\Sigma_{hor} = 2i_b c_0 + 2i_b c_2 \mathbf{Q}$$

$$\Sigma_{ver} = 2i_b c_0 - 2i_b c_2 \mathbf{Q}$$

Cancel Monopole moment

$$\Sigma_{hor} - \Sigma_{ver} = 4i_b c_2 \mathbf{Q}$$

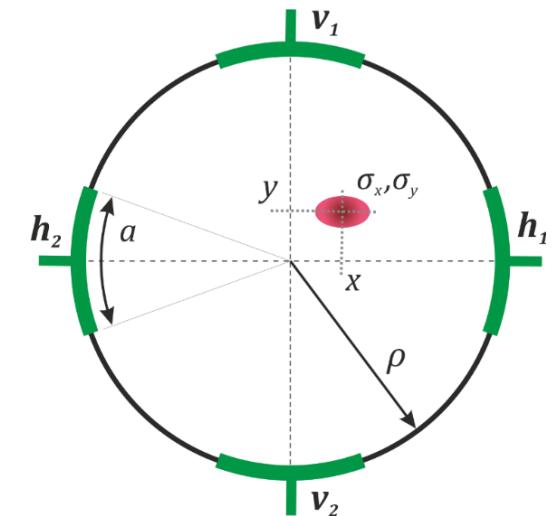
Normalize by intensity

$$R_q = \frac{\Sigma_{hor} - \Sigma_{ver}}{\Sigma_{hor} + \Sigma_{ver}} = \frac{c_2}{c_0} \mathbf{Q}$$

Standard Measurement Technique

PU signals as a **multipole expansion**

$$\begin{cases} \Sigma_{hor} \\ U_{h1} = i_b [c_0 + c_1 D_x + c_2 \mathbf{Q} + \dots] \\ U_{h2} = i_b [c_0 - c_1 D_x + c_2 \mathbf{Q} + \dots] \\ \Sigma_{ver} \\ U_{v1} = i_b [c_0 + c_1 D_y - c_2 \mathbf{Q} + \dots] \\ U_{v2} = i_b [c_0 - c_1 D_y - c_2 \mathbf{Q} + \dots] \end{cases}$$



Cancel Dipolar moments

$$\Sigma_{hor} = 2i_b c_0 + 2i_b c_2 \mathbf{Q}$$

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Normalize by intensity

$$R_q = \frac{\Sigma_{hor} - \Sigma_{ver}}{\Sigma_{hor} + \Sigma_{ver}} = \frac{c_2}{c_0} \mathbf{Q}$$

Pretty straightforward...
but very challenging!

Low Quadrupolar Sensitivity

Analytical 2D Case

$$U_{h1} \propto \frac{a}{2\pi} + \frac{1}{\rho} \frac{2\sin(a/2)}{\pi} x + \frac{1}{\rho^2} \frac{\sin(a)}{\pi} (\sigma_x^2 - \sigma_y^2 + x^2 - y^2) + \dots$$

General Case

$$U_{h1} \propto c_0 + c_1 D_x + c_2 Q + \dots$$

$$\frac{c_2}{c_0} Q \propto (\sigma_{\text{eff}}/\rho)^2 \ll 1$$

Quadrupolar moment constitutes only a
very small part of the total BPM signal



Typical values: *few per milles*

Challenges (1)

Low Quadrupolar Sensitivity

Analytical 2D Case

$$U_{h1} \propto \frac{a}{2\pi} + \frac{1}{\rho} \frac{2\sin(a/2)}{\pi} x + \frac{1}{\rho^2} \frac{\sin(a)}{\pi} (\sigma_x^2 - \sigma_y^2 + x^2 - y^2) + \dots$$

channel **asymmetries** $\xrightarrow{\text{low sensitivity}}$ large **offsets**

General Case

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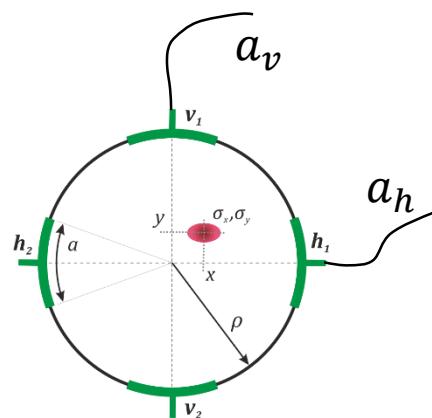
ideal world

symmetric channels

$$\Sigma_{hor} = 2i_b c_0 + 2i_b c_2 Q$$

$$\Sigma_{ver} = 2i_b c_0 - 2i_b c_2 Q$$

$$Q_m = \frac{c_0}{c_2} \frac{\Sigma_{hor} - \Sigma_{ver}}{\Sigma_{hor} + \Sigma_{ver}} = Q$$



realistic case

small asymmetry

$$\Sigma_{hor} = 2a_h i_b c_0 + 2a_h i_b c_2 Q$$

$$\Sigma_{ver} = 2a_v i_b c_0 - 2a_v i_b c_2 Q$$

$$Q_m = \frac{c_0}{c_2} \frac{\Sigma_{hor} - \Sigma_{ver}}{\Sigma_{hor} + \Sigma_{ver}} \approx Q + \frac{c_0}{c_2} \frac{a_h - a_v}{a_h + a_v}$$

Challenges (1)

Low Quadrupolar Sensitivity

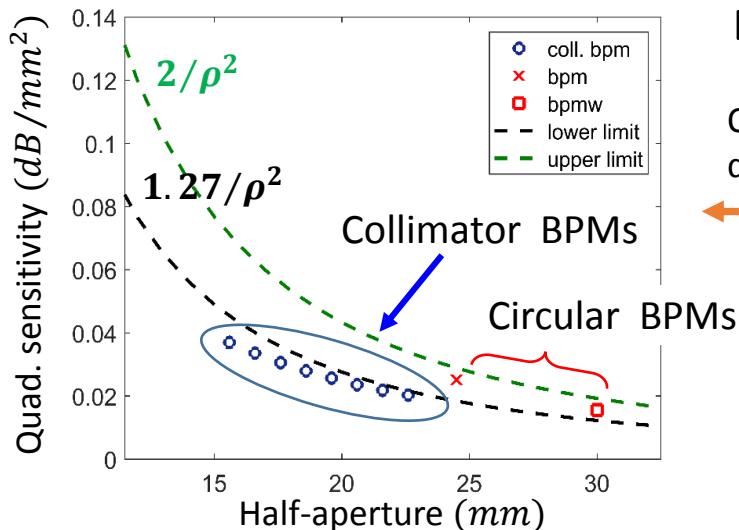
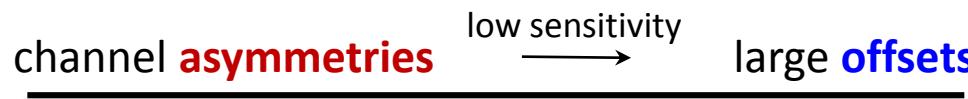
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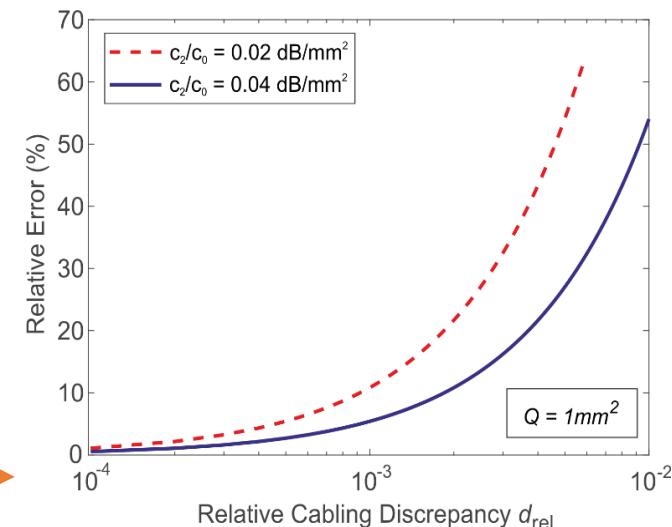
$$\frac{c_2}{c_0} Q \propto (\sigma_{\text{eff}}/\rho)^2 \ll 1$$



Example: LHC BPMs

Quad. sensitivity (c_2/c_0) for different types of LHC BPMs

Error considering a cabling discrepancy in one channel



Parasitic Position Signal

$$Q = \frac{\sigma_x^2 - \sigma_y^2}{Q_\sigma} + \frac{x^2 - y^2}{Q_p}$$

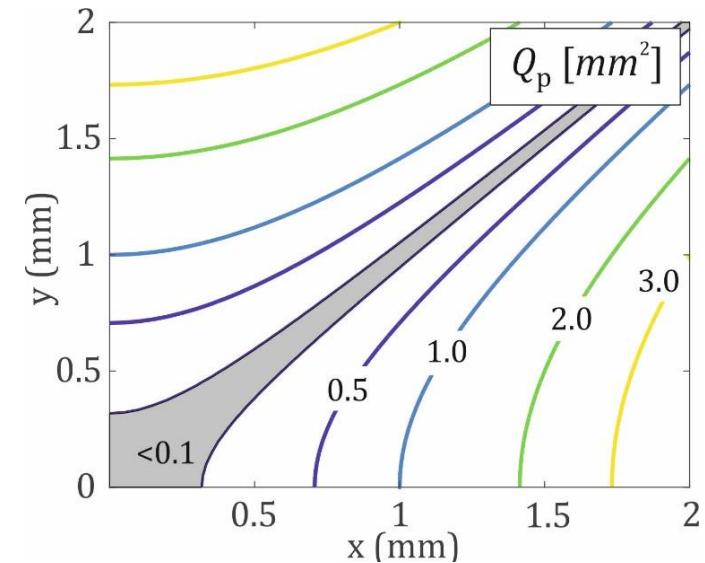
beam size signal
to be measured
position signal
parasitic

Typical values in LHC PUs

[450 GeV] → $Q_\sigma \sim 0.30 - 1.50 \text{ mm}^2$

[6.5 TeV] → $Q_\sigma \sim 0.05 - 0.30 \text{ mm}^2$

Even small beam displacements may result in large parasitic signal Q_p



Problem – Overview

Fundamental Limitations	<i>Unfavourable Conditions</i>	Destructive Measurement Effects
Low quadrupolar sensitivity $U_{h1} \propto c_0 + c_1 D_x + c_2 Q + \dots$ <div style="border: 1px solid black; padding: 5px; display: inline-block;"> $c_2 Q \ll c_0$ </div>	<i>asymmetries (electronics, cabling, geometrical)</i> <i>noise (electronics)</i>	<p>Beam size information lost in large offsets</p> <p>→ Beam size information lost in large offsets</p> <p>→ Low resolution**</p>
Parasitic Position Signal $Q = \sigma_x^2 - \sigma_y^2 + \boxed{x^2 - y^2}$	<i>off-centered beam</i>	<p>Beam size signal lost in parasitic position signal</p>

** Noise from electronics may significantly affect the quadrupolar measurements.

However, existing BPM acquisition systems typically achieve sufficient resolution.

Example: $\sim 1\mu\text{m}$ position resolution → $\sim 0.01\text{mm}^2$ quadrupolar resolution

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Example: $\sim 1\mu\text{m}$ position resolution → $\sim 0.01 - 0.02\text{mm}^2$ quadrupolar resolution

Subtract Position Signal

Direct subtraction

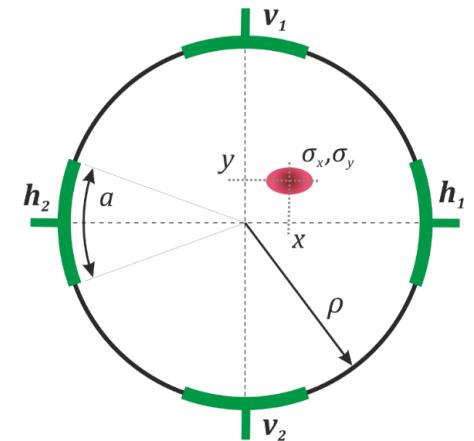
Manipulate PU as a beam position monitor (BPM)

1. Measure the beam position

$$x_m = P \left(\frac{U_{h1} - U_{h2}}{U_{h1} + U_{h2}} \right) \quad y_m = P \left(\frac{U_{v1} - U_{v2}}{U_{v1} + U_{v2}} \right)$$

2. Subtract the parasitic signal

$$Q_{\sigma,m} = Q - x_m^2 + y_m^2$$



Subtract Position Signal

Direct subtraction

Manipulate PU as a beam position monitor (BPM)

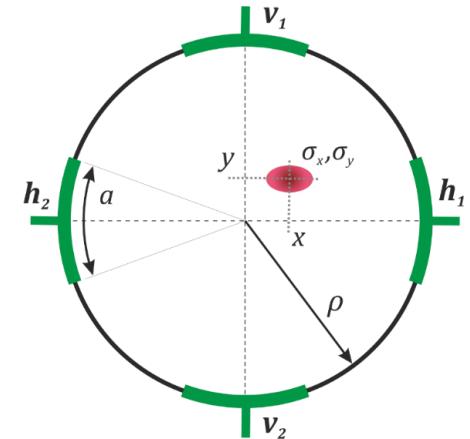
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2. Subtract the parasitic signal

$$Q_{\sigma,m} = Q - x_m^2 + y_m^2$$

Is this subtraction sufficient to cancel
the position signal?



Subtract Position Signal

Direct subtraction

Manipulate PU as a beam position monitor (BPM)

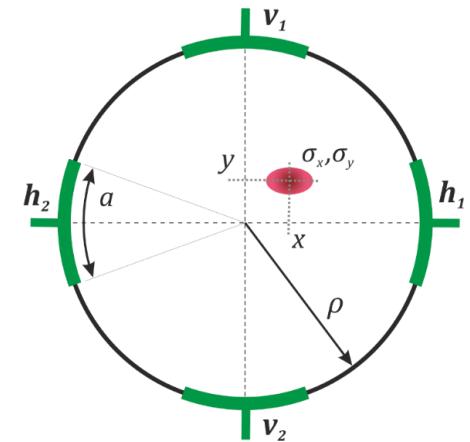
1. Measure the beam position, **with certain accuracy**

$$x_m = P \left(\frac{U_{h1} - U_{h2}}{U_{h1} + U_{h2}} \right) \quad y_m = P \left(\frac{U_{v1} - U_{v2}}{U_{v1} + U_{v2}} \right)$$

2. Subtract the parasitic signal

$$Q_{\sigma,m} = Q - x_m^2 + y_m^2$$

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Subtract Position Signal

Direct subtraction

Manipulate PU as a beam position monitor (BPM)

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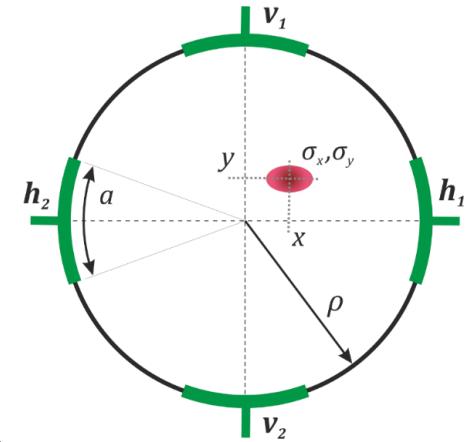
$$x_m = x + \Delta x \quad y_m = y + \Delta y$$

2. Subtract the parasitic signal

$$Q_{\sigma,m} = Q - x_m^2 + y_m^2$$

*Remaining Error:
 $Q_{x,rem} \approx 2x\Delta x$*

Significant for large offsets



Towards a Movable PU..

Direct subtraction

Manipulate PU as a beam position monitor (BPM)

1. Measure the beam position, **with certain accuracy**

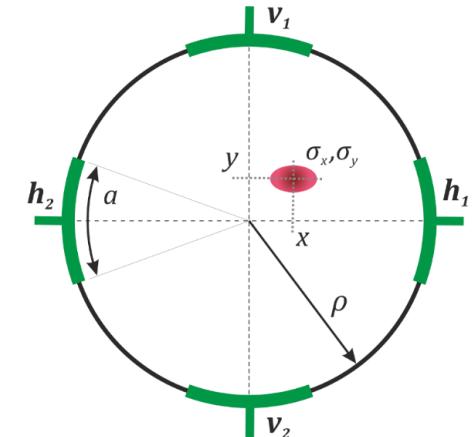
$$x_m = x + \Delta x \quad y_m = y + \Delta y$$

2. Subtract the parasitic signal

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Remaining Error:

$$Q_{x,rem} \approx 2x\Delta x$$



Subtraction by Alignment (Movable PU)

1. Measure the beam position, **with certain accuracy**

$$x_m = x + \Delta x \quad y_m = y + \Delta y$$

2. Align PU according to (x_m, y_m)

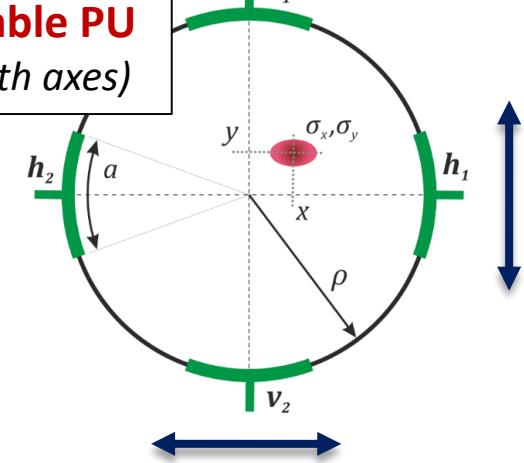
$$x' \approx \Delta x$$

$$y' \approx \Delta y$$

Movable PU
(in both axes)

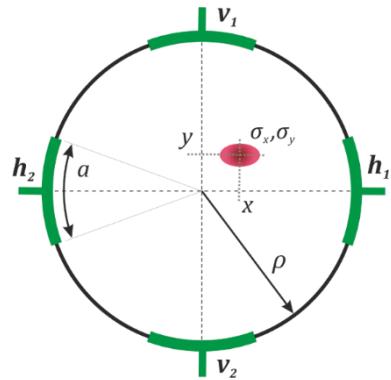
$$Remaining Error:$$

$$Q_{x,rem} \approx \Delta x^2$$



Towards a Movable PU..

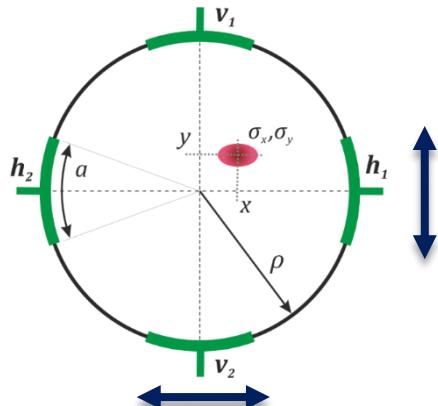
Direct subtraction (Fixed PU)



Measure & subtract beam position

$$\text{Remaining Error: } Q_{x,rem} \approx 2x\Delta x$$

Subtraction by Alignment (Movable PU)



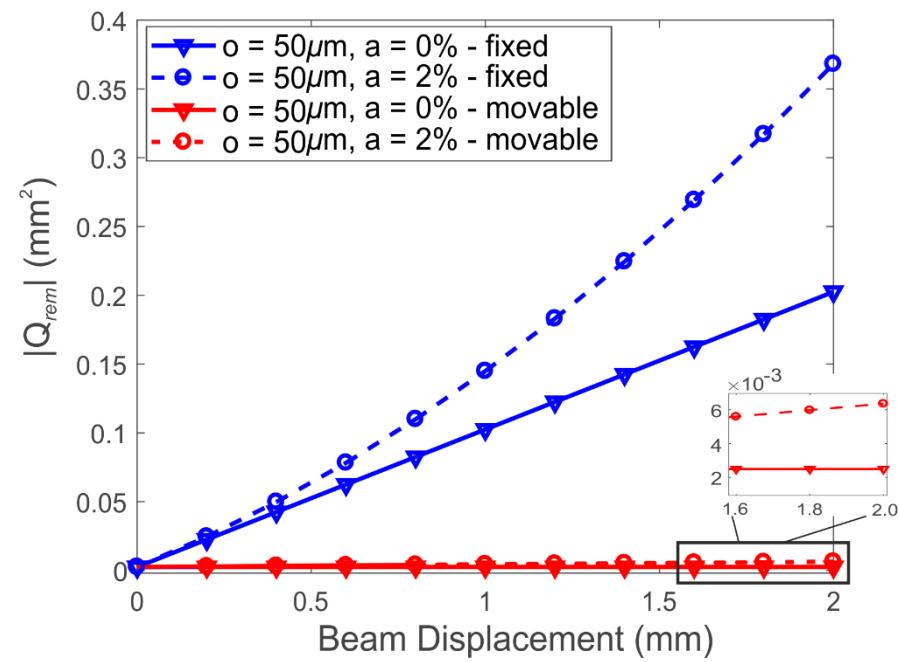
Measure beam position
& align PU

$$\text{Remaining Error: } Q_{x,rem} \approx \Delta x^2$$

Example

Remaining parasitic signal considering offset, o , & scaling, a , errors in position measurement:

$$\Delta x = o + ax$$



Problem – Overview

Fundamental Limitations	<i>Unfavourable Conditions</i>	Destructive Measurement Effects
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Parasitic Position Signal $Q = \sigma_x^2 - \sigma_y^2 + \boxed{x^2 - y^2}$	<i>off-centered beam</i>	<p>Beam size signal lost in parasitic position signal</p> <p>→ Beam size signal lost in parasitic position signal</p> <p><i>Align PU with the beam</i></p> <p>movable PU</p>

** Noise from electronics may significantly affect the quadrupolar measurements. However, existing BPM acquisition systems typically achieve sufficient resolution.
Example: $\sim 1\mu\text{m}$ position resolution $\rightarrow \sim 0.01 - 0.02\text{mm}^2$ quadrupolar resolution

Problem – Overview

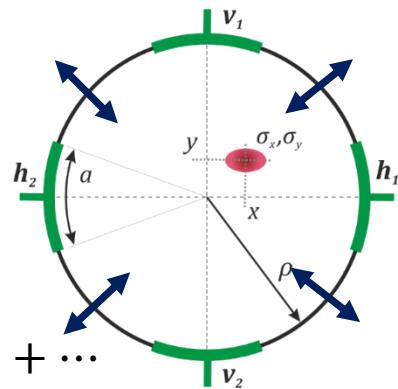
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Parasitic Position Signal $Q = \sigma_x^2 - \sigma_y^2 + \boxed{x^2 - y^2}$	<i>off-centered beam</i>	Beam size signal lost in parasitic position signal <i>Align PU with the beam</i>

movable PU

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Aperture Scans

Consider a (*theoretical*) circular PU able to change its aperture ρ

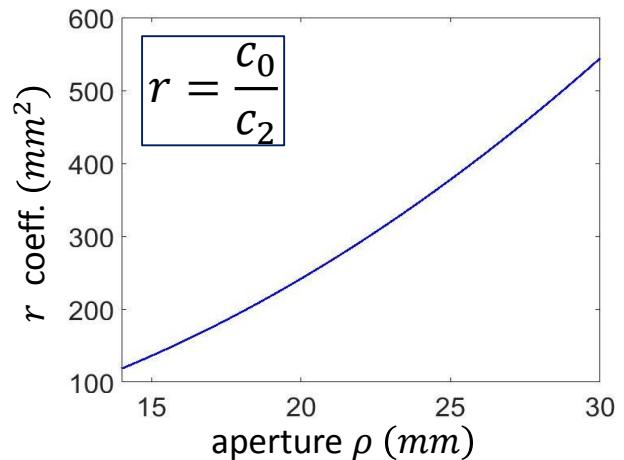
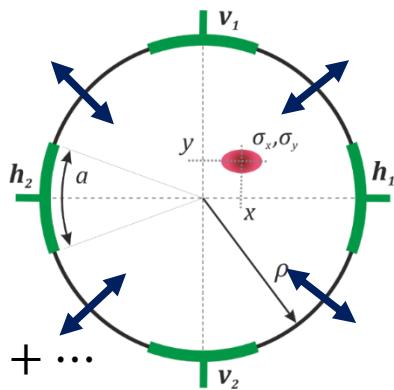


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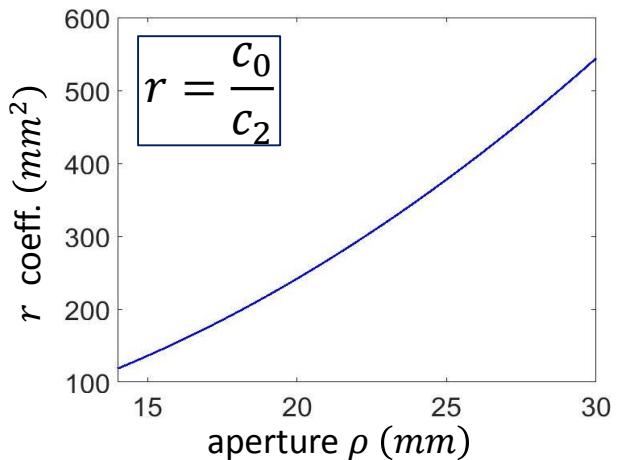
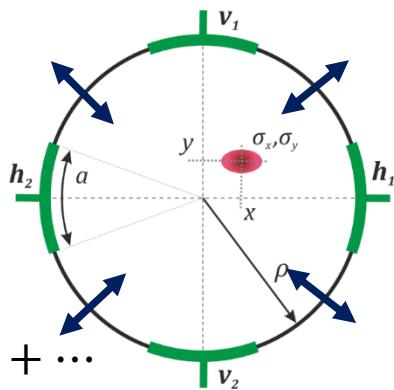
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Aperture Scans

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Monopole & Quadrupolar moments **change differently** w.r.t. to the aperture change

stable beam

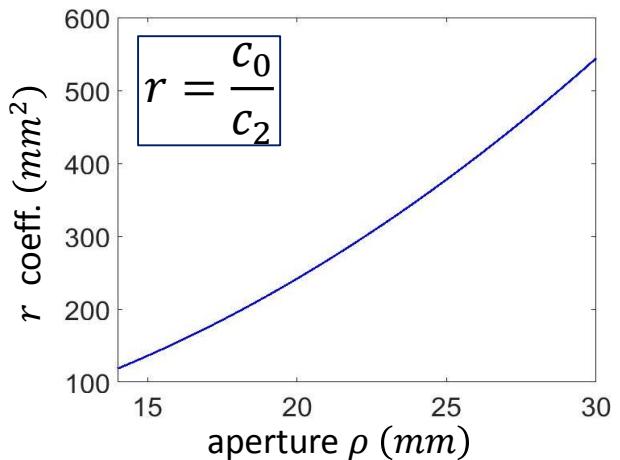
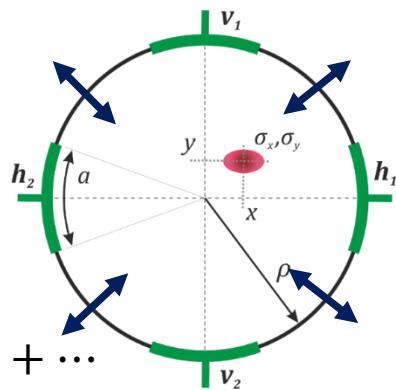
Calibrate PU system
(e.g. electronics/ cabling)

reference point

Aperture Scans

Consider a (*theoretical*) circular PU able to change its aperture ρ

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A more realistic example?



Monopole & Quadrupolar moments **change differently** w.r.t. to the aperture change

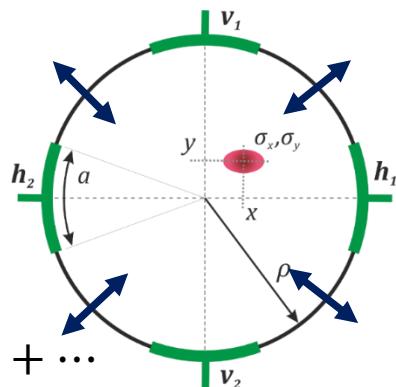
stable beam

Calibrate PU system
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Aperture Scans

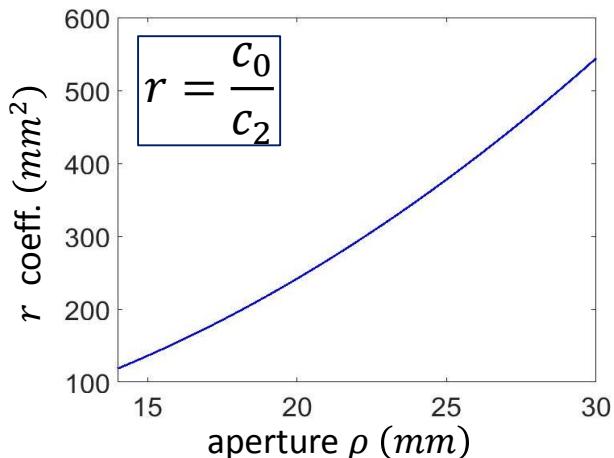
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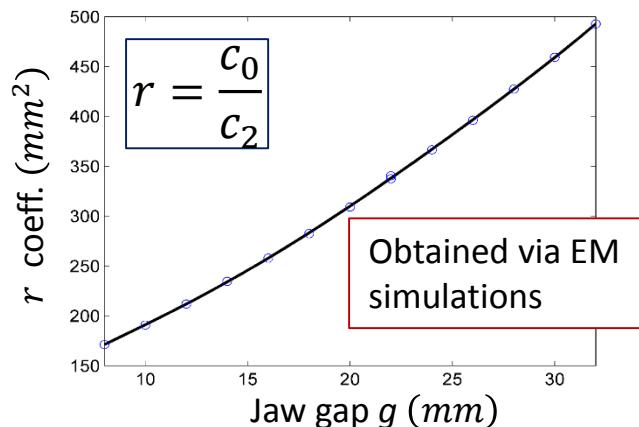
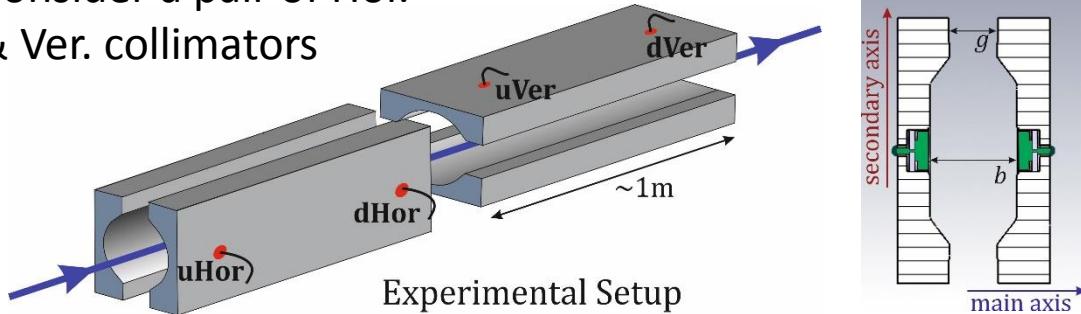
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stable beam

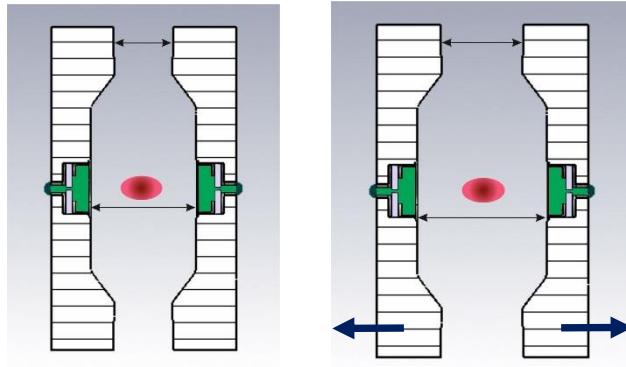
Calibrate PU system
(e.g. electronics/ cabling)

Consider a pair of Hor. & Ver. collimators



A New Approach: The d-Norm Method

Consider a movable PU, able to change the aperture



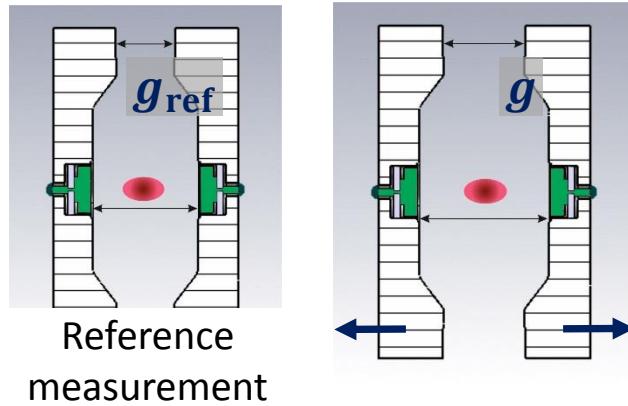
Consider some asymmetry
between the Hor. & Ver. channels

$$\Sigma_h = \textcolor{red}{a_h} i_b (c_0 + c_2 Q)$$

$$\Sigma_v = \textcolor{red}{a_v} i_b (c_0 - c_2 Q)$$

A New Approach: The d-Norm Method

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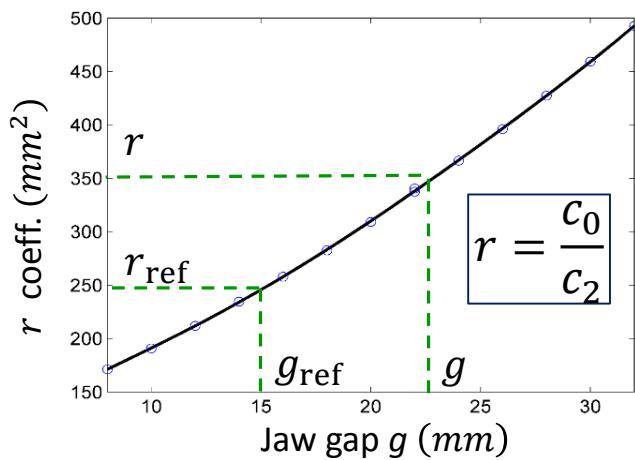


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$$\Sigma_h = \color{red}{a_h} i_b (c_0 + c_2 Q)$$

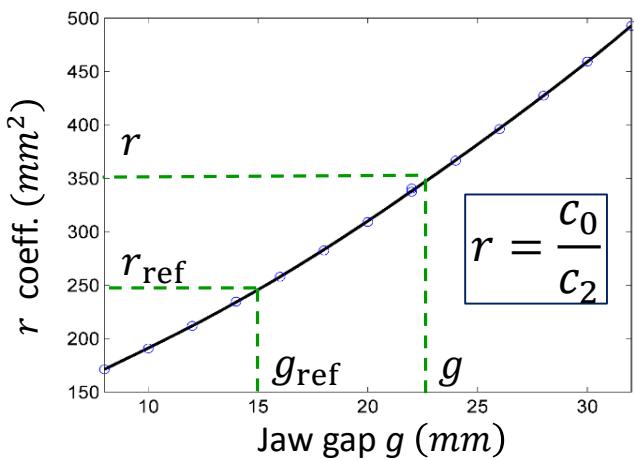
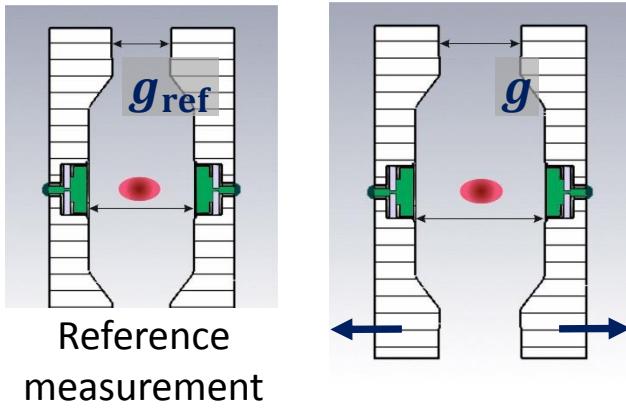
$$\Sigma_v = \color{red}{a_v} i_b (c_0 - c_2 Q)$$

Perform 2 measurements with different apertures



A New Approach: The d-Norm Method

Consider a movable PU, able to change the aperture



Consider some asymmetry between the Hor. & Ver. channels

$$\Sigma_h = a_h i_b (c_0 + c_2 Q)$$

$$\Sigma_v = a_v i_b (c_0 - c_2 Q)$$

Perform 2 measurements with different apertures

1st normalization

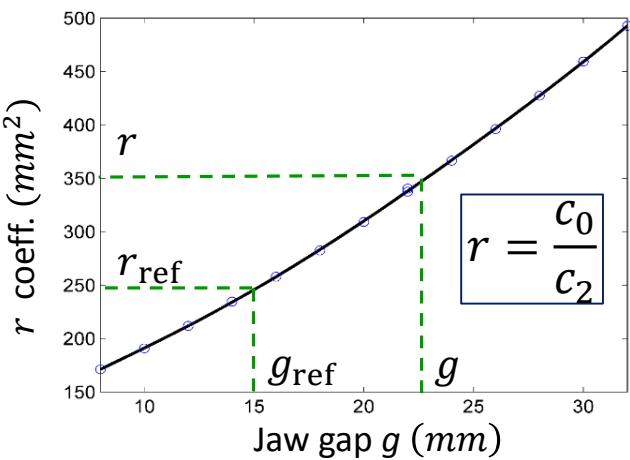
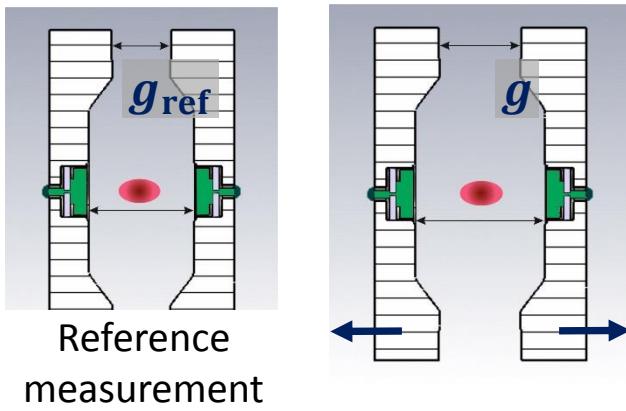
cancel the asymmetric gains a_h, a_v

$$S_h = \frac{\Sigma_h}{\Sigma_{h,\text{ref}}} = \frac{i_b(r + Q)}{i_{b,\text{ref}}(r_{\text{ref}} + Q)}$$

$$S_v = \frac{\Sigma_v}{\Sigma_{v,\text{ref}}} = \frac{i_b(r - Q)}{i_{b,\text{ref}}(r_{\text{ref}} - Q)}$$

A New Approach: The d-Norm Method

Consider a movable PU, able to change the aperture



Consider some asymmetry between the Hor. & Ver. channels

$$\Sigma_h = \mathbf{a}_h i_b (c_0 + c_2 Q)$$

$$\Sigma_v = \mathbf{a}_v i_b (c_0 - c_2 Q)$$

Perform 2 measurements with different apertures

1st normalization

$$S_h = \frac{\Sigma_h}{\Sigma_{h,ref}} = \frac{i_b(r + Q)}{i_{b,ref}(r_{ref} + Q)}$$

$$S_v = \frac{\Sigma_v}{\Sigma_{v,ref}} = \frac{i_b(r - Q)}{i_{b,ref}(r_{ref} - Q)}$$

cancel the asymmetric gains a_h, a_v

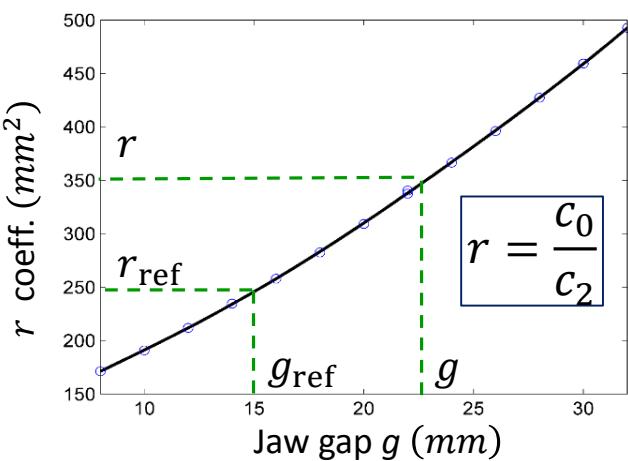
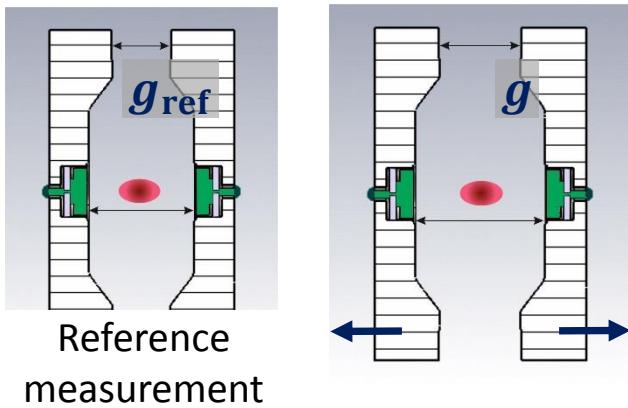
2nd normalization

$$R = \frac{S_h}{S_v} = \frac{r + Q}{r - Q} \frac{r_{ref} - Q}{r_{ref} + Q}$$

normalize intensity

A New Approach: The d-Norm Method

Consider a movable PU, able to change the aperture



Consider some asymmetry between the Hor. & Ver. channels

$$\Sigma_h = a_h i_b (c_0 + c_2 Q)$$

$$\Sigma_v = a_v i_b (c_0 - c_2 Q)$$

Perform 2 measurements with different apertures

1st normalization

cancel the asymmetric gains a_h, a_v

$$S_h = \frac{\Sigma_h}{\Sigma_{h,ref}} = \frac{i_b(r + Q)}{i_{b,ref}(r_{ref} + Q)}$$

$$S_v = \frac{\Sigma_v}{\Sigma_{v,ref}} = \frac{i_b(r - Q)}{i_{b,ref}(r_{ref} - Q)}$$

2nd normalization

normalize intensity

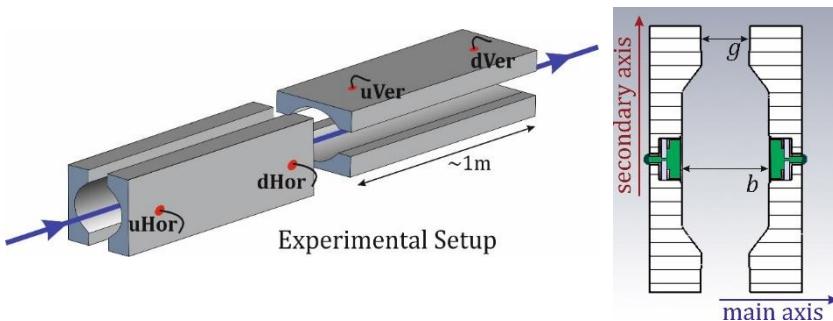
$$R = \frac{S_h}{S_v} = \frac{r + Q}{r - Q} \frac{r_{ref} - Q}{r_{ref} + Q}$$

Q obtained by **double-normalization (d-Norm)**

$$Q \approx \frac{rr_{ref}}{r - r_{v,ref}} \frac{1 - R}{1 + R}$$

First Observations

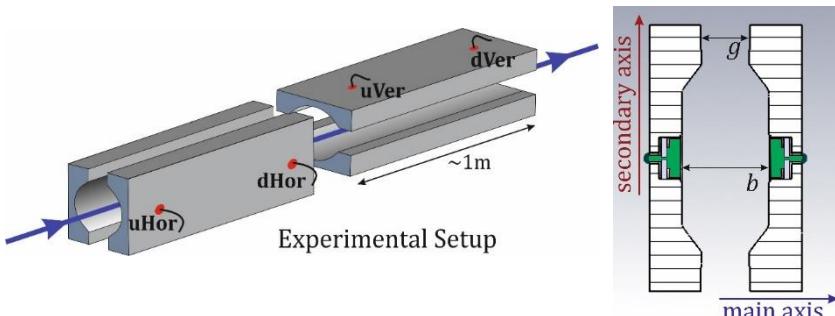
Experimental Setup: Collimator BPMs



- Dioded-based electronics (DOROS) – **high resolution** (better than $1\mu\text{m}$ for position measurements)
- BPM signals are **processed separately**
- Select a pair of Hor. – Ver. Collimators to form **4-electrodes PUs**
- **4 PUs in total** by combining upstream/downstream collimator BPMs

First Observations

1st phase: PU alignment



- **Main Axis:** direct alignment using position readings
- **Secondary Axis:** quadrupolar measurements

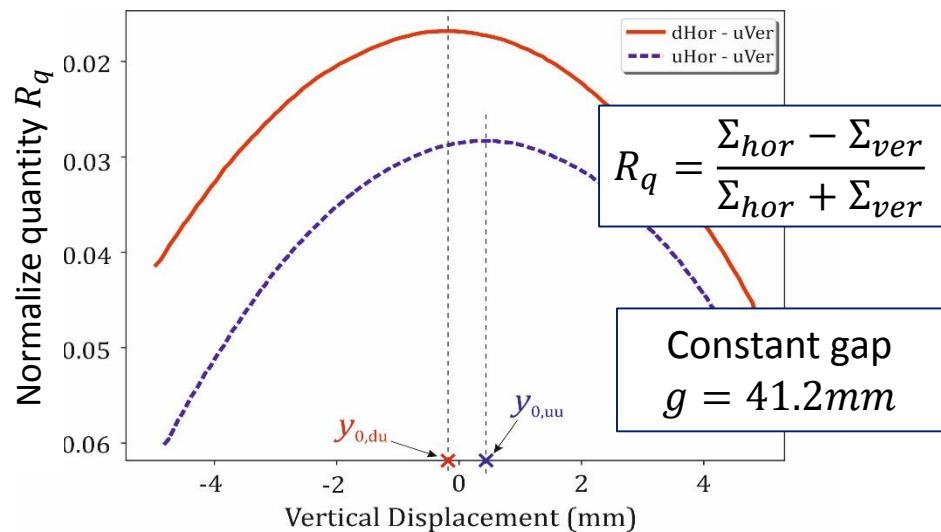
$$Q = \sigma_x^2 - \sigma_y^2 + x^2 - y^2$$

↓ During scans on the secondary axis

$$Q_h = Q_{h,0} - y^2 \quad \text{Hor. collimator}$$

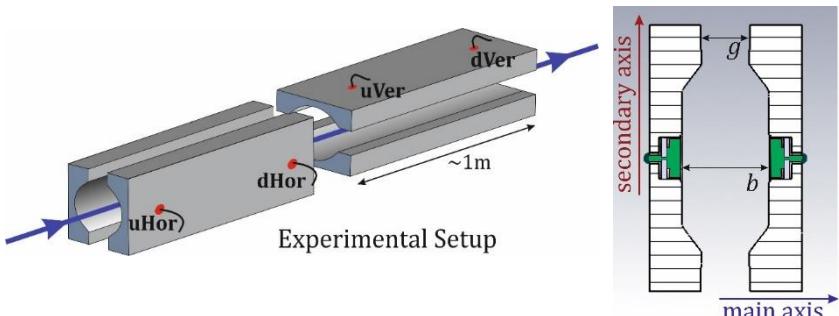
$$Q_v = Q_{v,0} + x^2 \quad \text{Ver. collimator}$$

Alignment process on the secondary axis



First Observations

1st phase: PU alignment



- **Main Axis:** direct alignment using position readings
- **Secondary Axis:** quadrupolar measurements

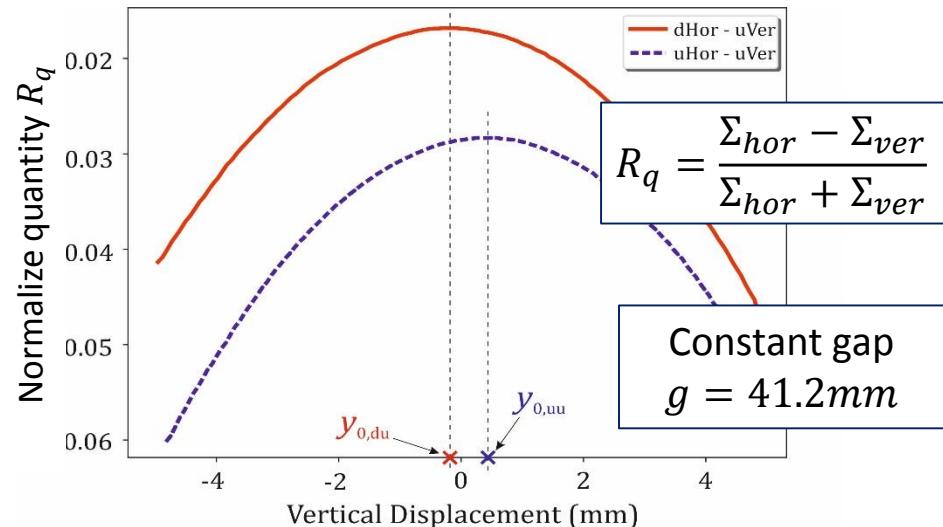
$$Q = \sigma_x^2 - \sigma_y^2 + x^2 - y^2$$

During scans on the secondary axis

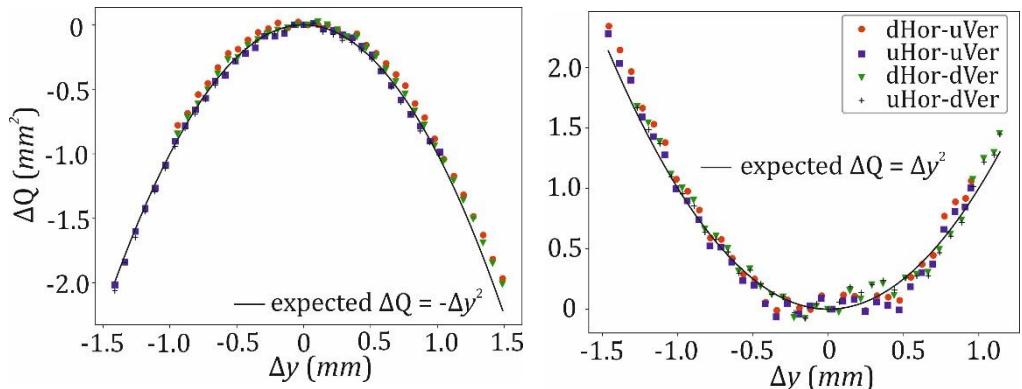
$$Q_h = Q_{h,0} - y^2 \quad \text{Hor. collimator}$$

$$Q_v = Q_{v,0} + x^2 \quad \text{Ver. collimator}$$

Alignment process on the secondary axis

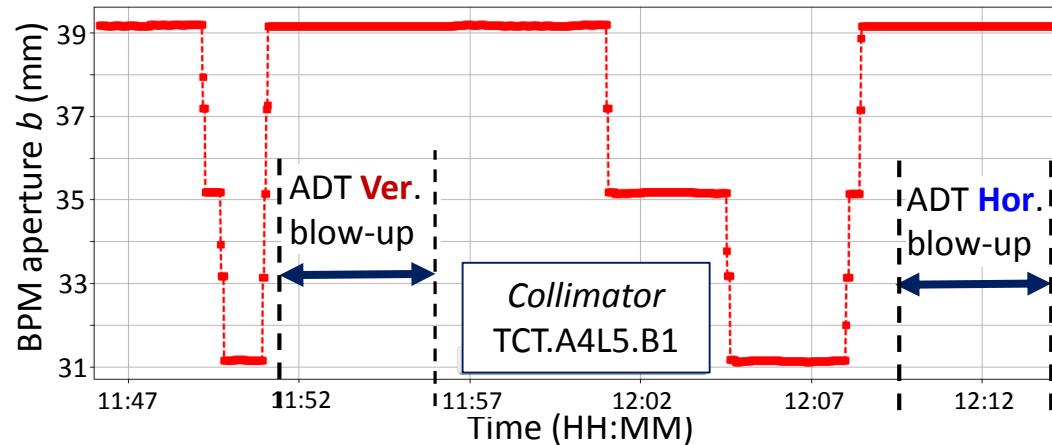
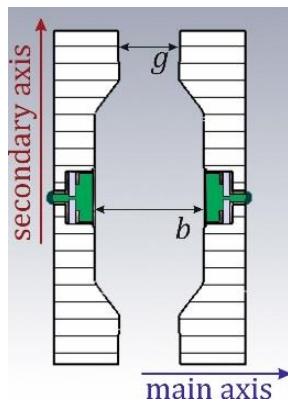


Scan around beam center after alignment



First Observations

2nd phase: aperture scans + emittance blow-up



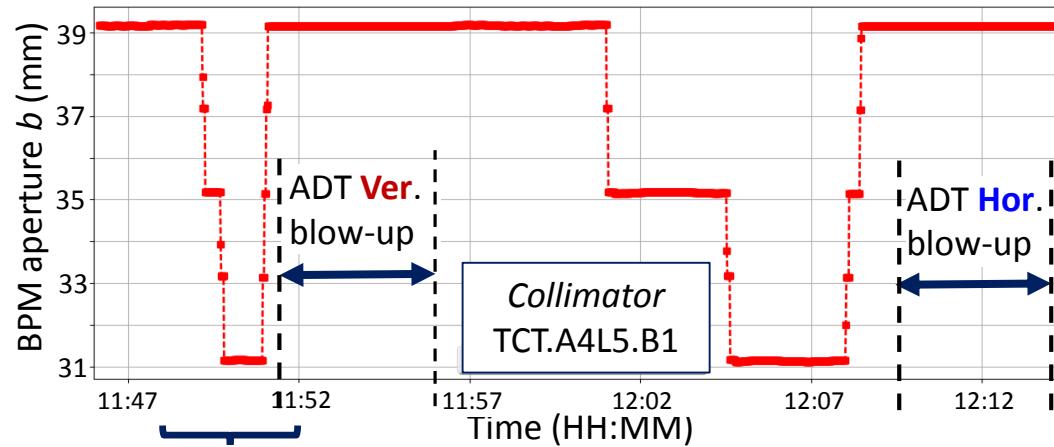
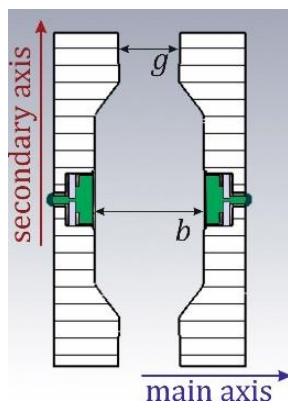
Injection energy
(450 GeV)

Nominal values:

- $\beta_x = 165m$
- $\beta_y = 79m$
- $Q_{nom} = 0.47mm^2$

First Observations

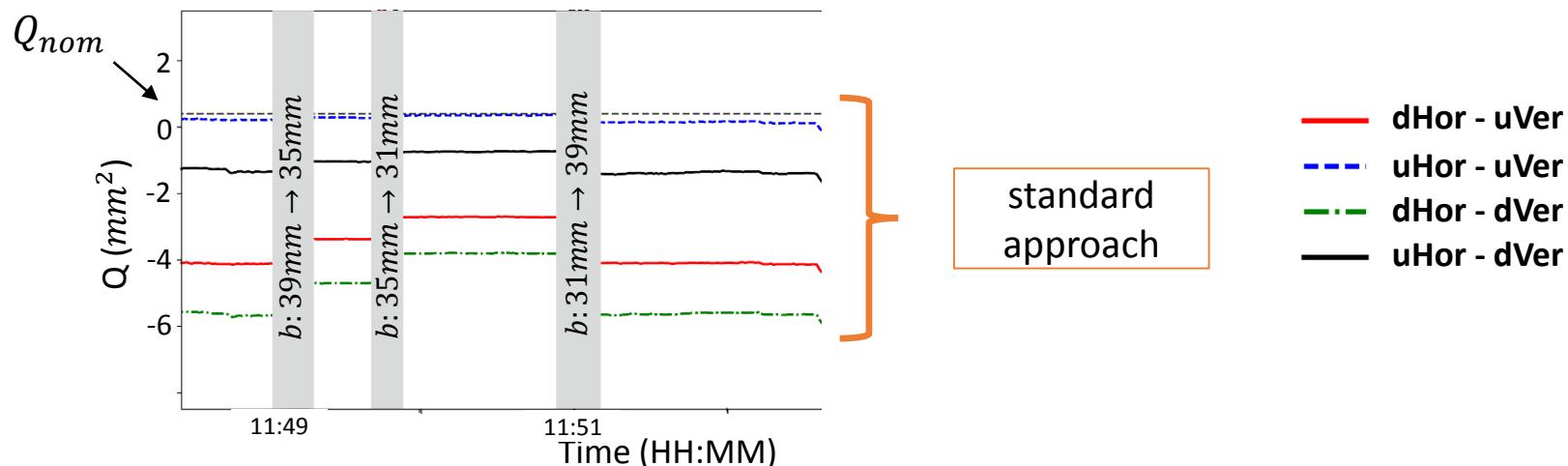
2nd phase: aperture scans + emittance blow-up



Injection energy
(450 GeV)

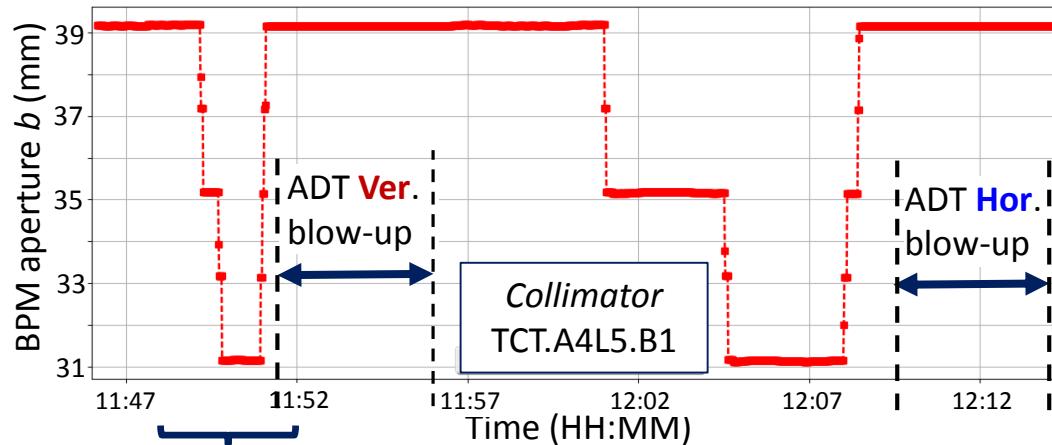
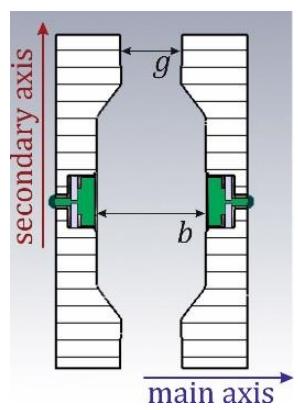
Nominal values:

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- $Q_{nom} = 0.47\text{mm}^2$



First Observations

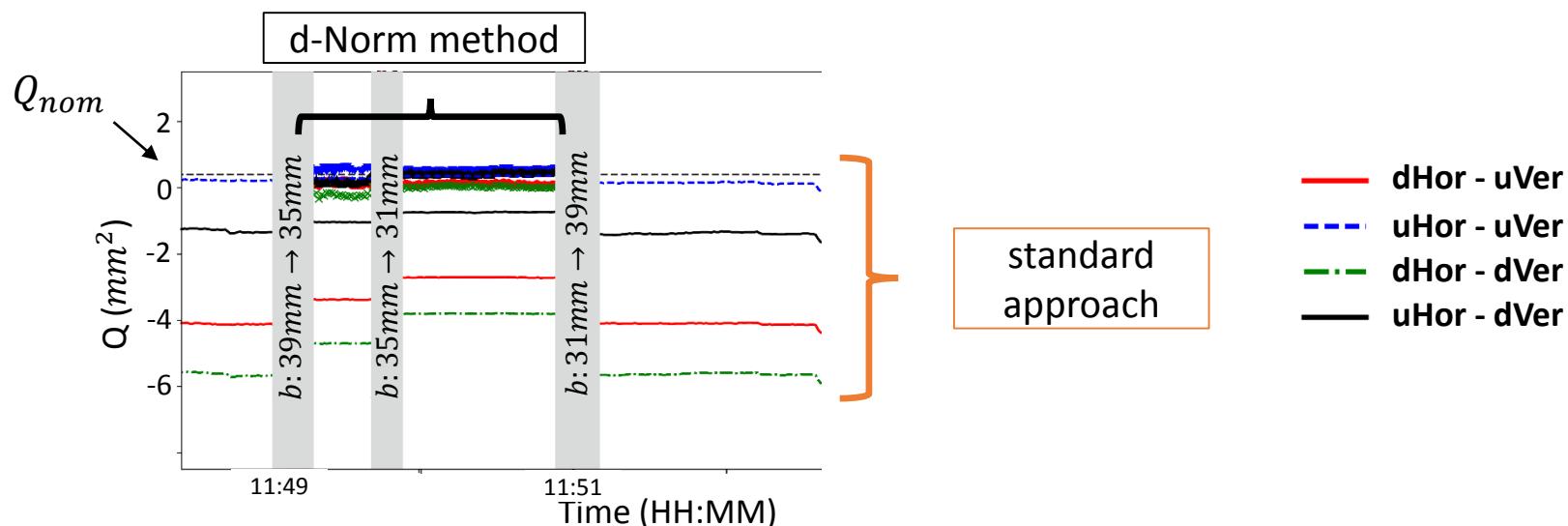
2nd phase: aperture scans + emittance blow-up



Injection energy
(450 GeV)

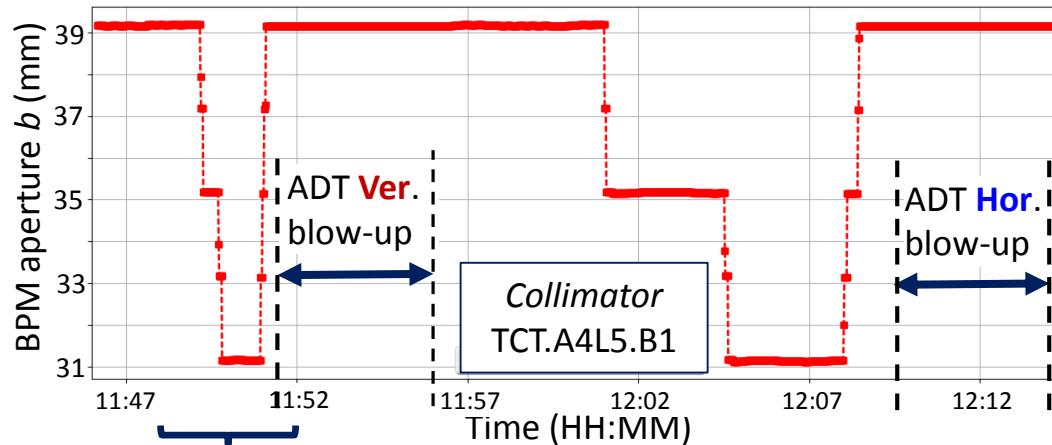
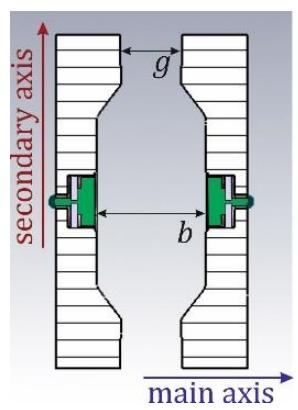
Nominal values:

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- $Q_{nom} = 0.47\text{mm}^2$



First Observations

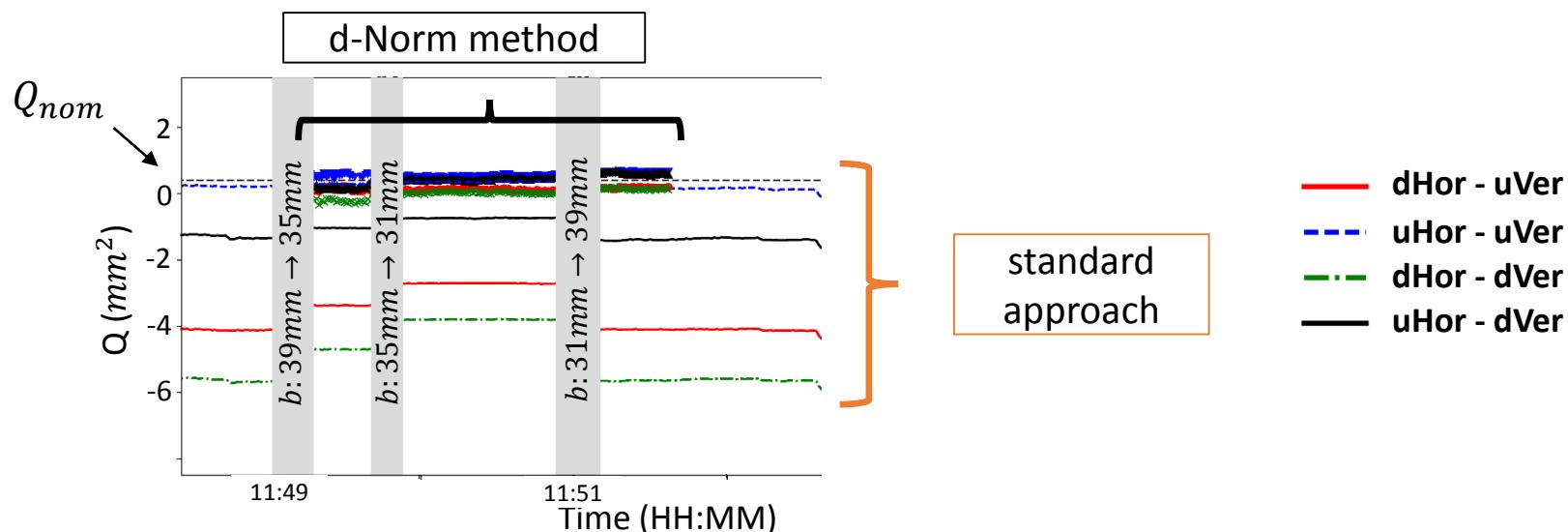
2nd phase: aperture scans + emittance blow-up



Injection energy
(450 GeV)

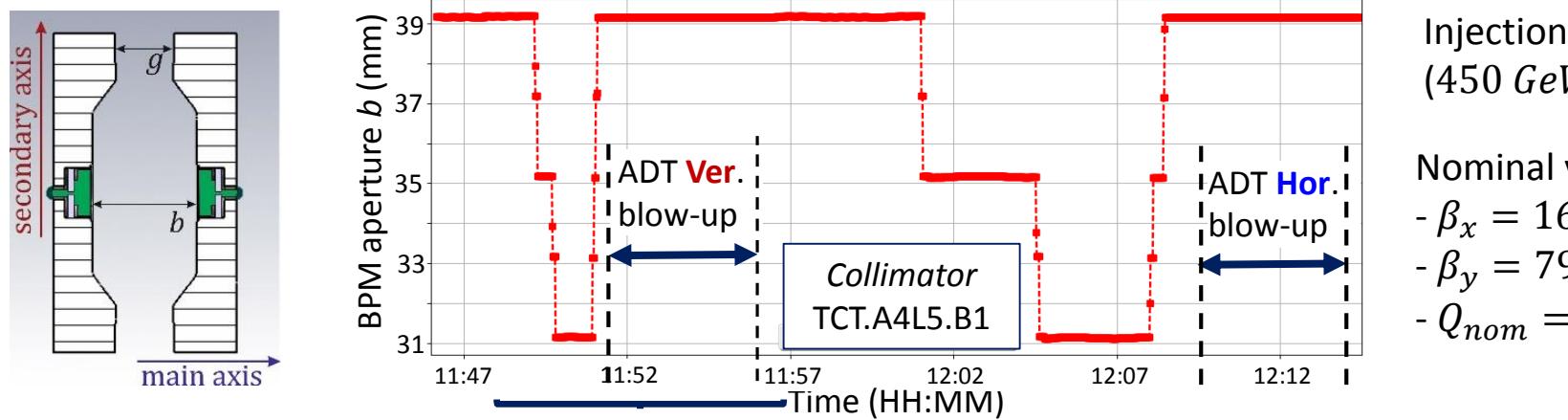
Nominal values:

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- $Q_{nom} = 0.47\text{mm}^2$



First Observations

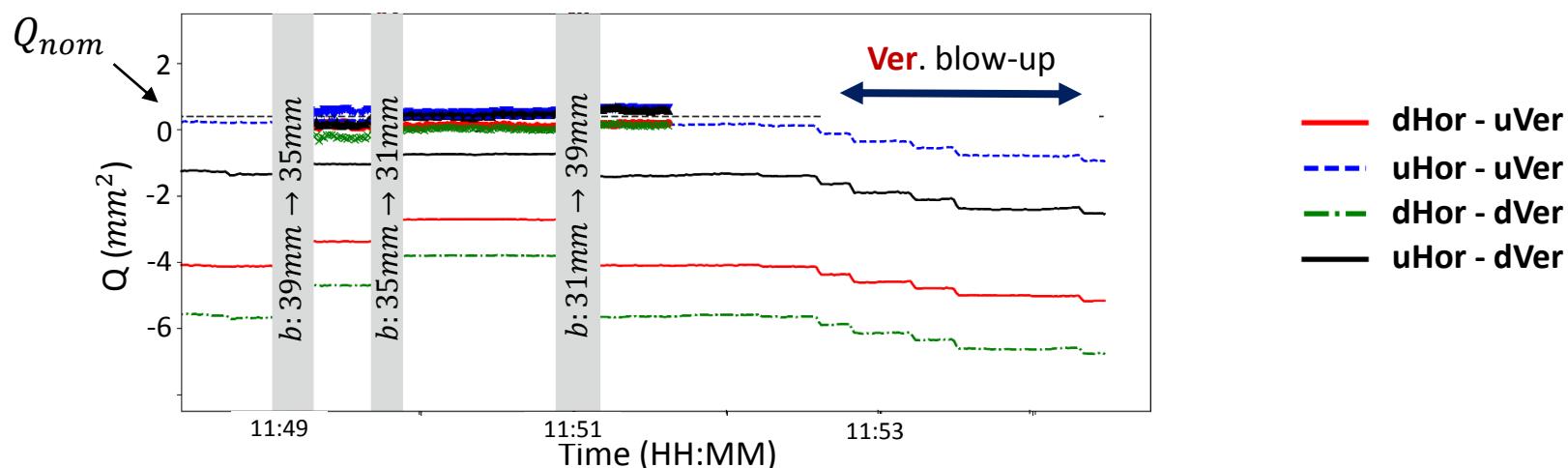
2nd phase: aperture scans + emittance blow-up



Injection energy
(450 GeV)

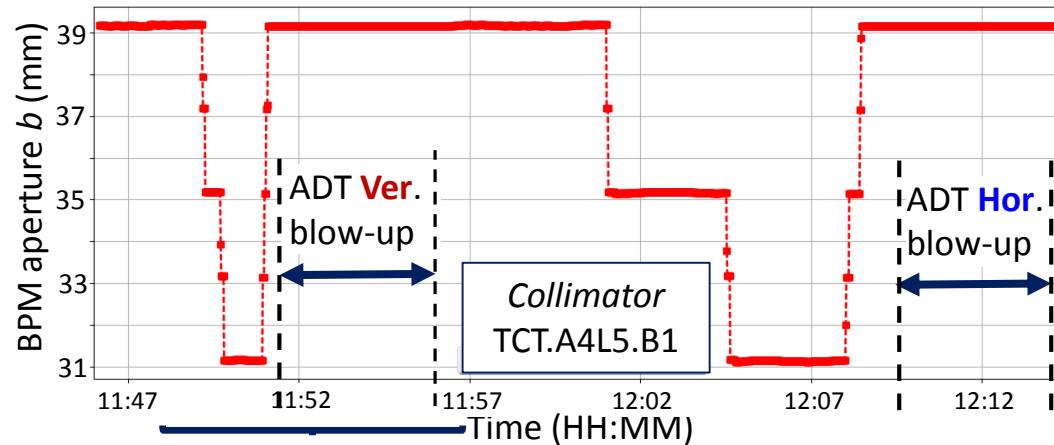
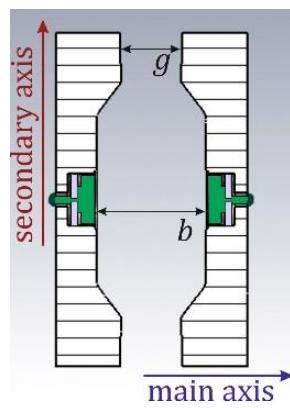
Nominal values:

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- $\beta_y = 79\text{m}$
- $Q_{nom} = 0.47\text{mm}^2$



First Observations

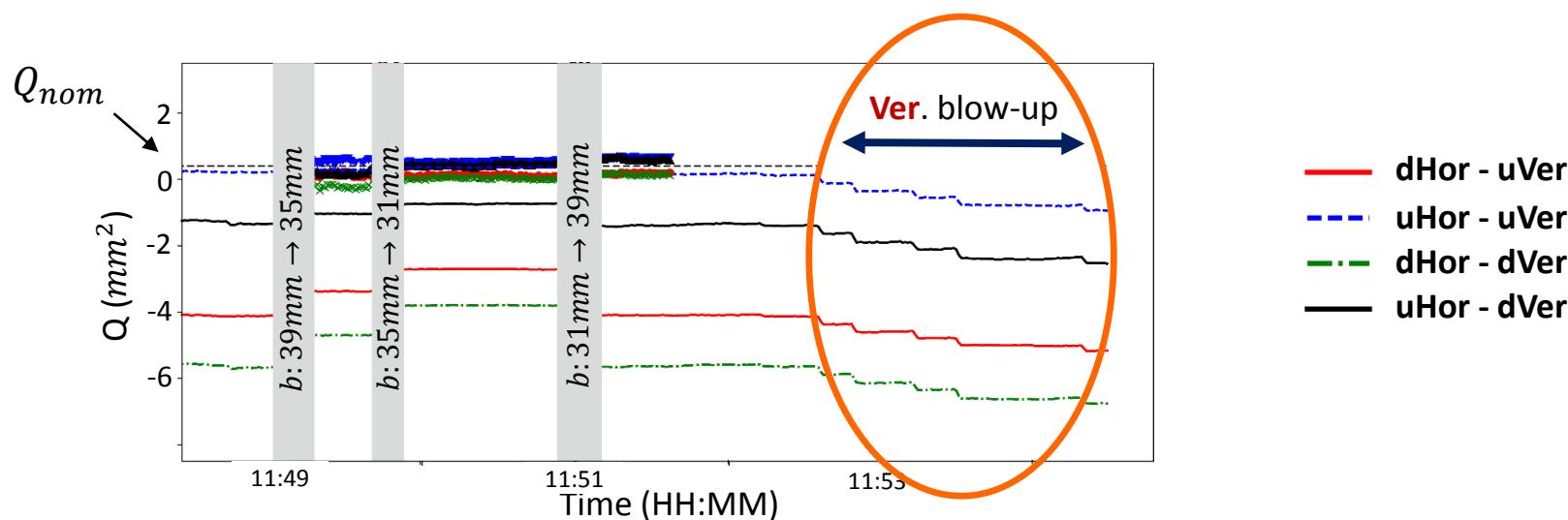
2nd phase: aperture scans + emittance blow-up



Injection energy
(450 GeV)

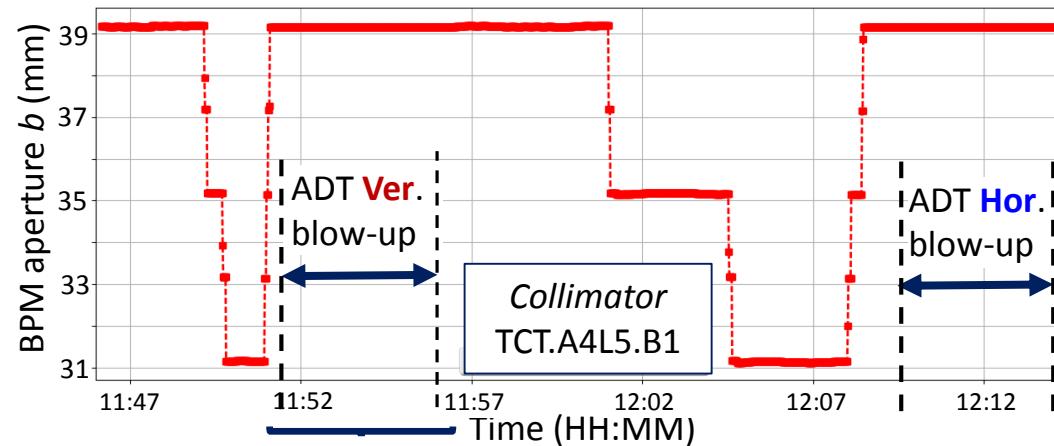
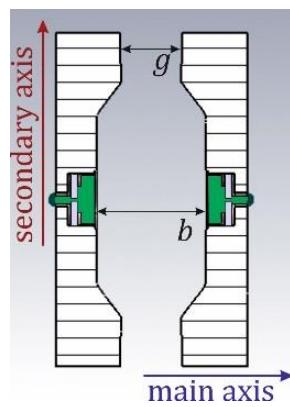
Nominal values:

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First Observations

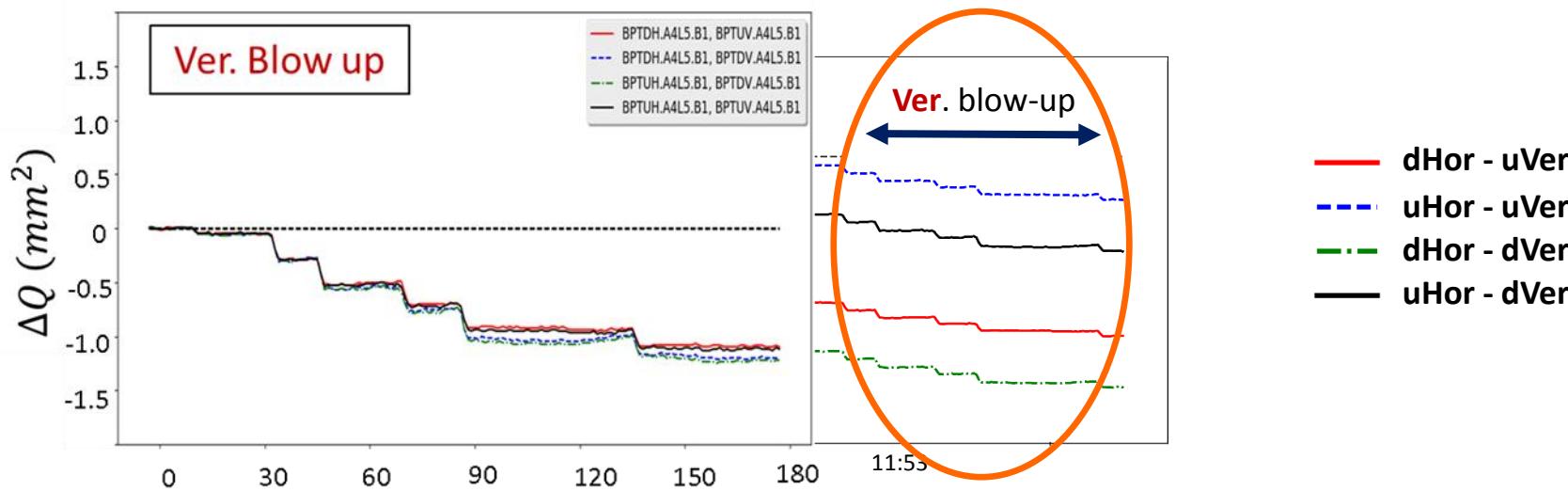
2nd phase: aperture scans + emittance blow-up



Injection energy
(450 GeV)

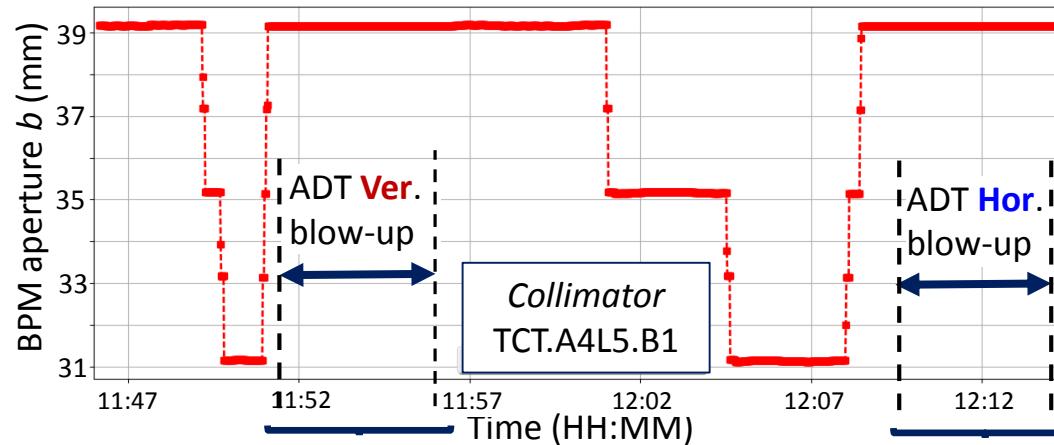
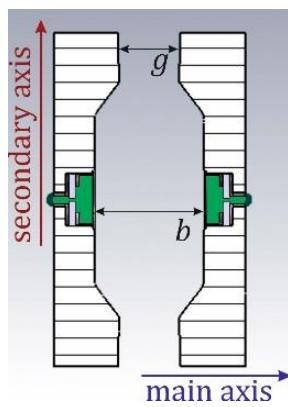
Nominal values:

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First Observations

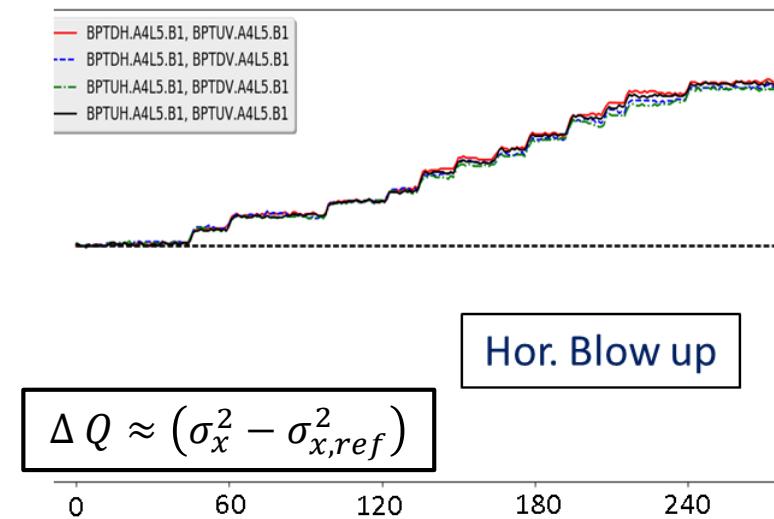
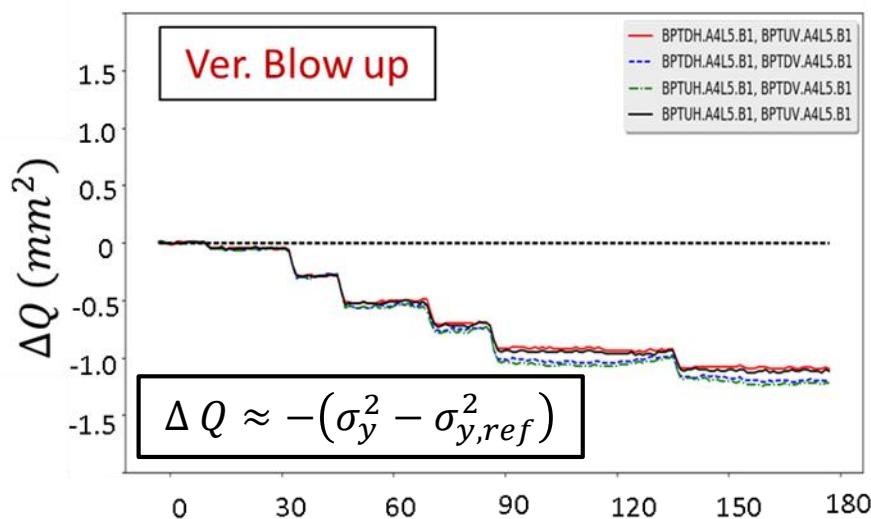
2nd phase: aperture scans + emittance blow-up



Injection energy
(450 GeV)

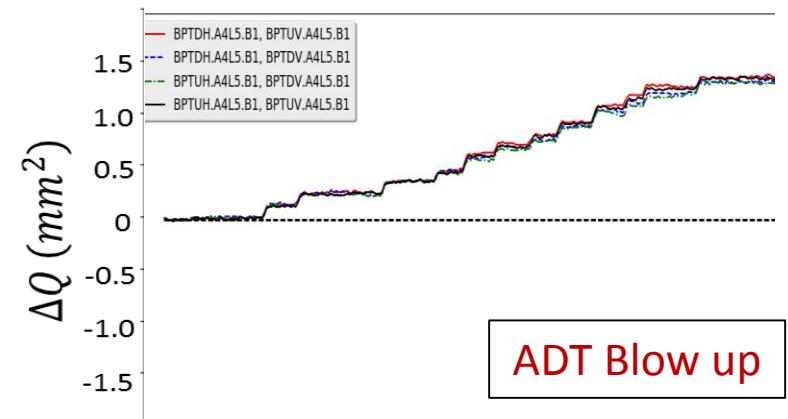
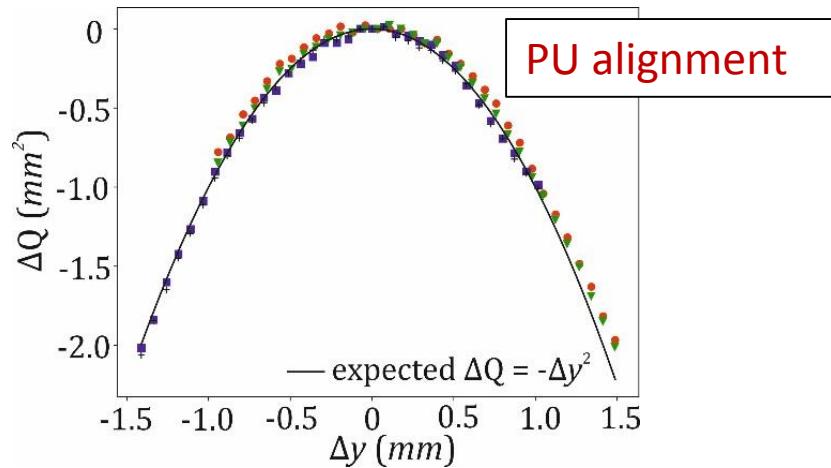
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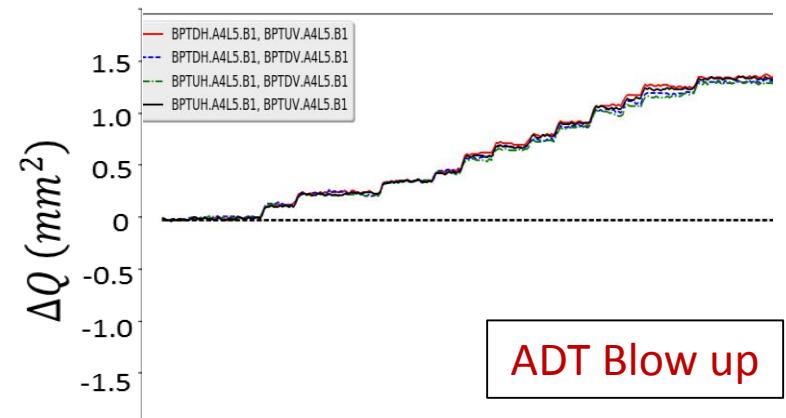
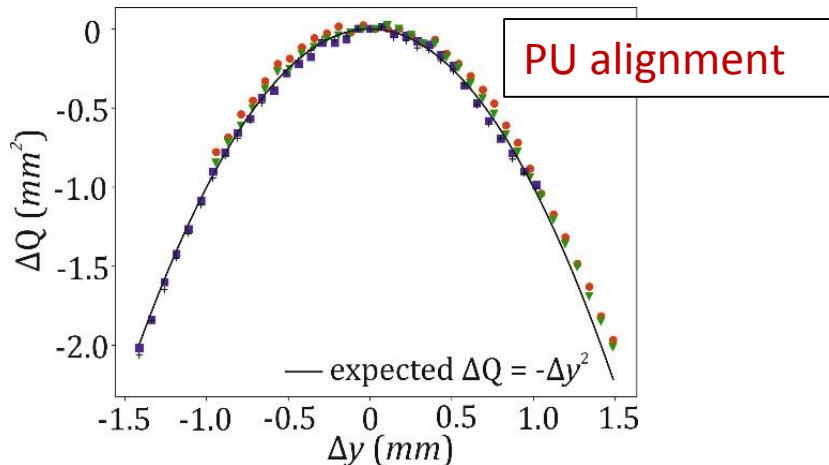
Last Point: Differential measurements

Promising differential measurements during PU alignment, during ADT blow-up

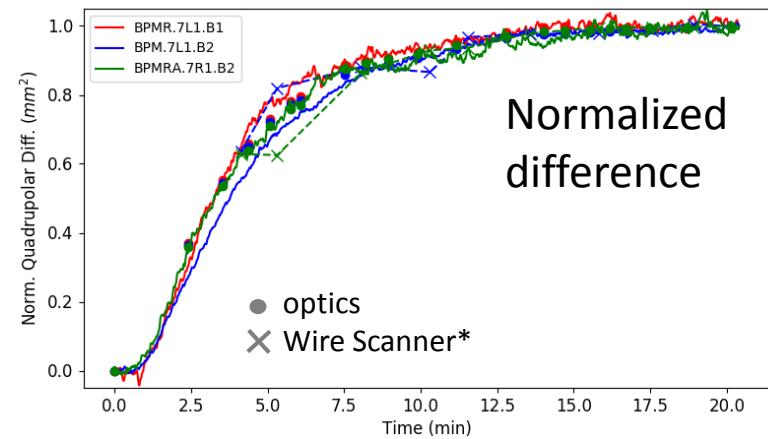
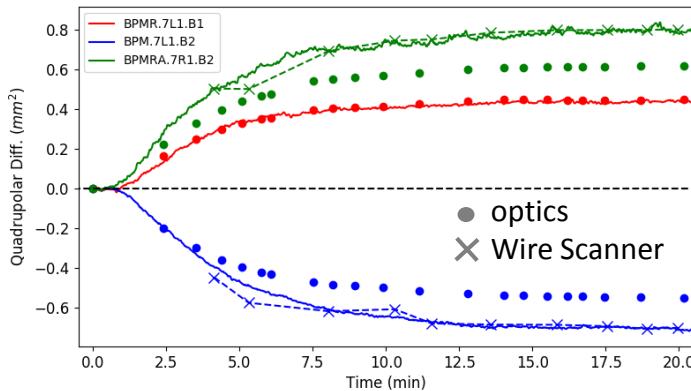


Last Point: Differential measurements

Promising differential measurements during PU alignment, during ADT blow-up

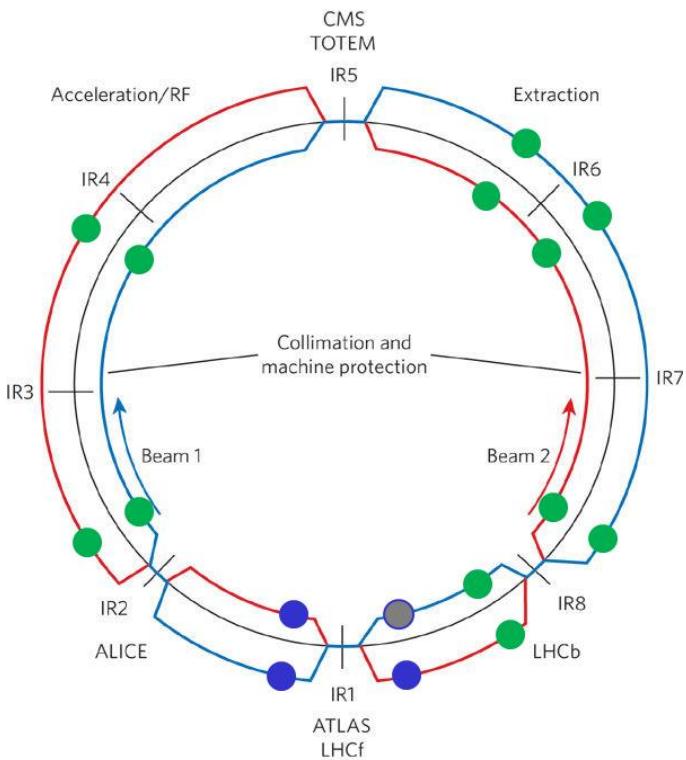


..and during the energy ramp



Emittance Measurements During the Ramp

12 BPMs all around LHC

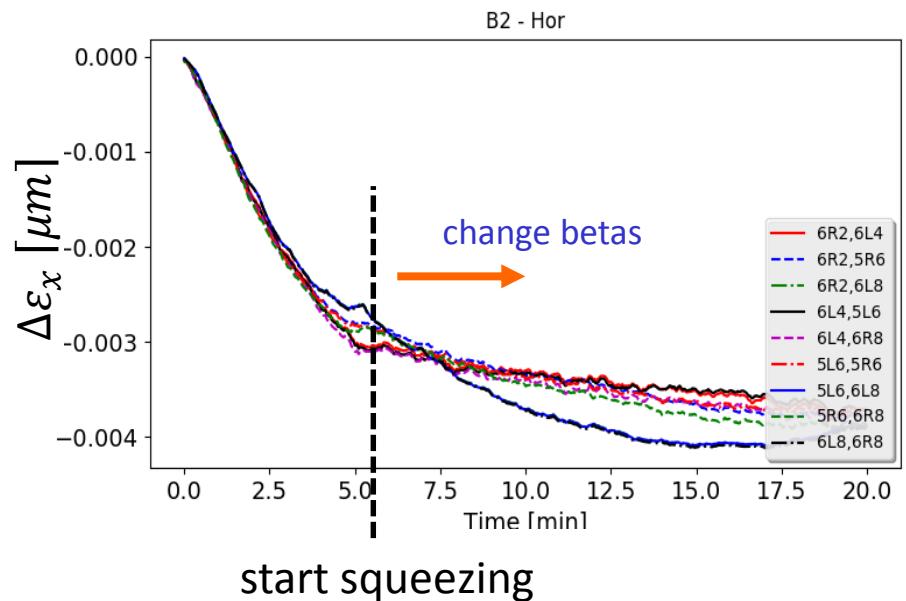


Absolute change on the geometric emittance

- Combine (at least) 2 BPMs with different beta functions

$$\Delta Q^{(1)} = \beta_x^{(1)} \Delta \varepsilon_x - \beta_y^{(1)} \Delta \varepsilon_y$$

$$\Delta Q^{(2)} = \beta_x^{(2)} \Delta \varepsilon_x - \beta_y^{(2)} \Delta \varepsilon_y$$

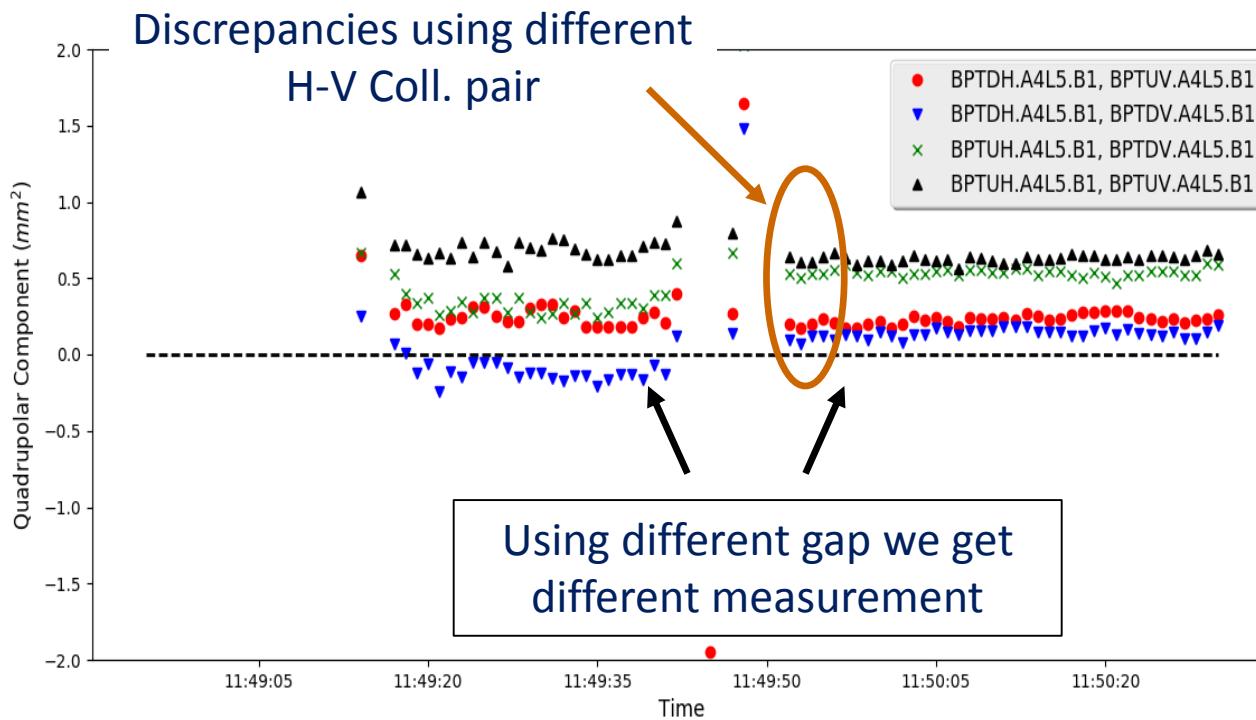


- **Quadrupolar Measurements**
 - simple concept but **very challenging** in reality
- **Fundamental Limitations**
 - Low quadrupolar sensitivity → *large offsets*
 - Parasitic Position Signal -> big errors when beam is displaced
- **Movable PUs**
 - Sufficiently cancel position signal (direct subtraction do not work for large beam displacements)
 - Calibrate the measurements system via **aperture scans**
- **Differential Measurements**
 - Use of existing BPM technologies
 - Promising results during the energy ramp

Thank You for your attention!

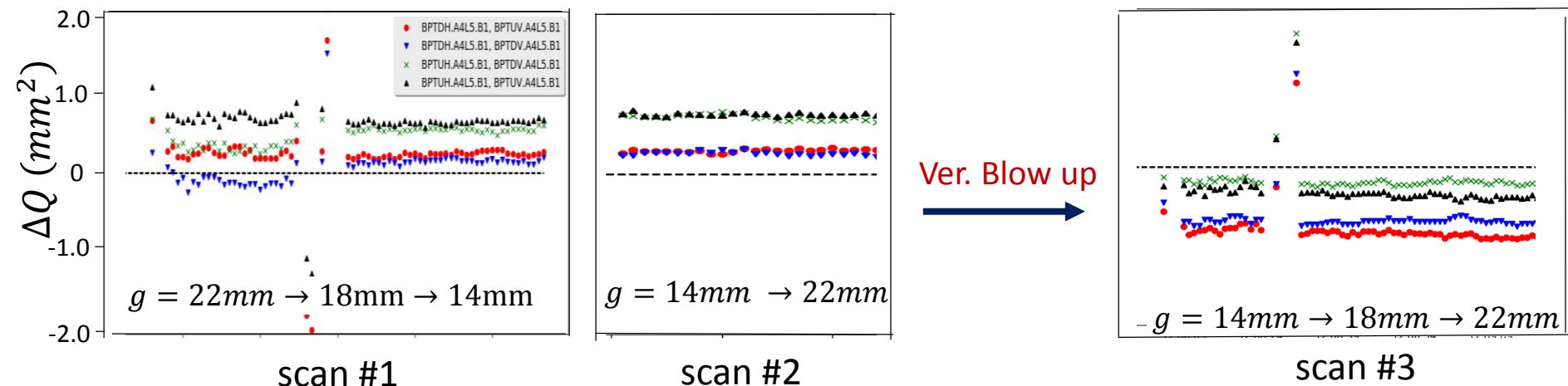
Spare slides

Understand the Uncertainties



First Observations

2nd phase: absolute & differential measurements

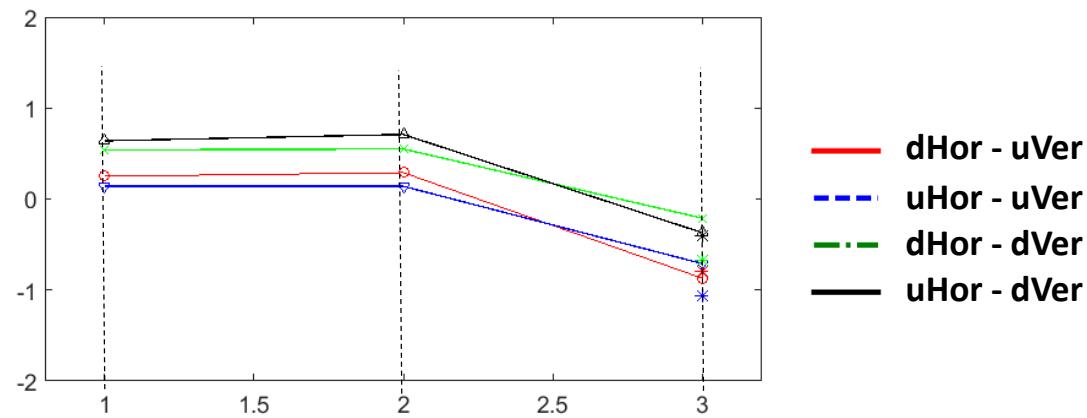
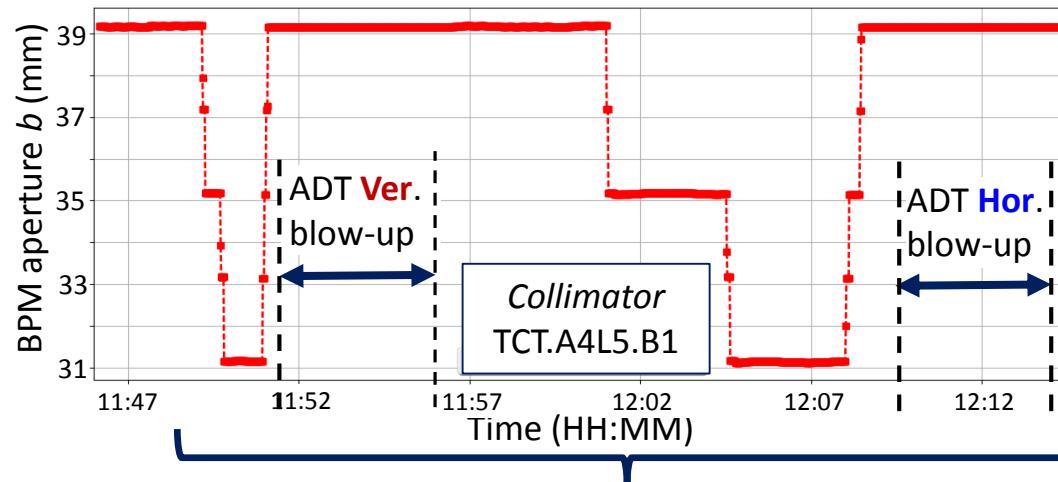
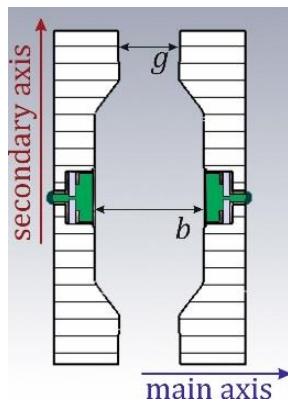


	Qabs1 (mm^2)	Qabs2 (mm^2)	Qdiff1 (mm^2)	Qabs3 (mm^2) Estimation**	Qabs3 (mm^2)	Diff. (mm^2)
DH - UV	0.25	0.29	-1.09	-0.80	-0.87	0.07
DH - DV	0.14	0.14	-1.20	-1.07	-0.71	-0.36
UH - DV	0.54	0.55	-1.22	-0.68	-0.21	-0.47
UH - UV	0.64	0.71	-1.12	-0.41	-0.37	-0.04

$$**Q_{3,\text{est}} = Q_2 + \Delta Q_1$$

First Observations

2nd phase: aperture scans + emittance blow-up



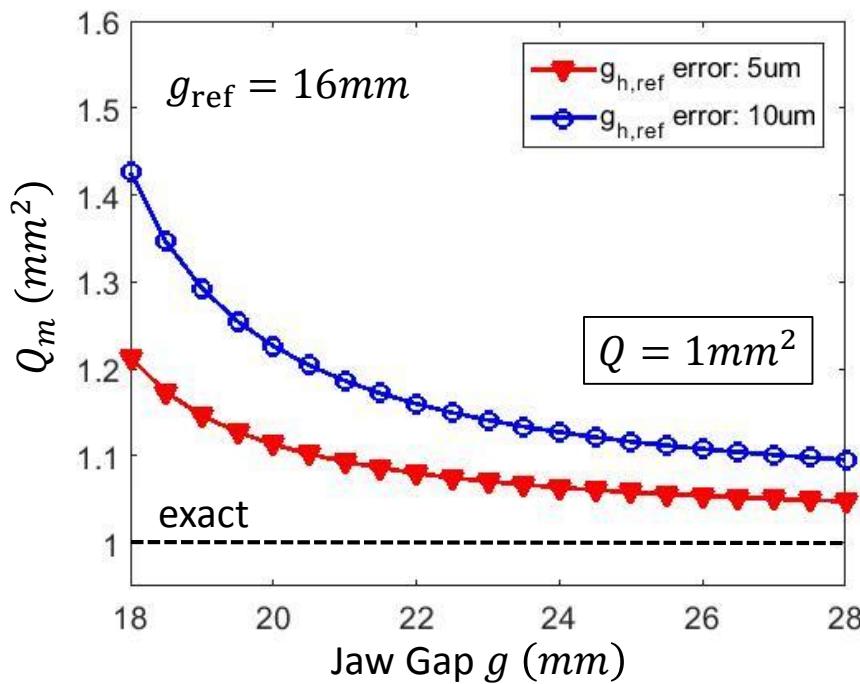
Injection energy
(450 GeV)

Nominal values:

- $\beta_x = 165m$
- $\beta_y = 79m$
- $Q_{nom} = 0.47mm^2$

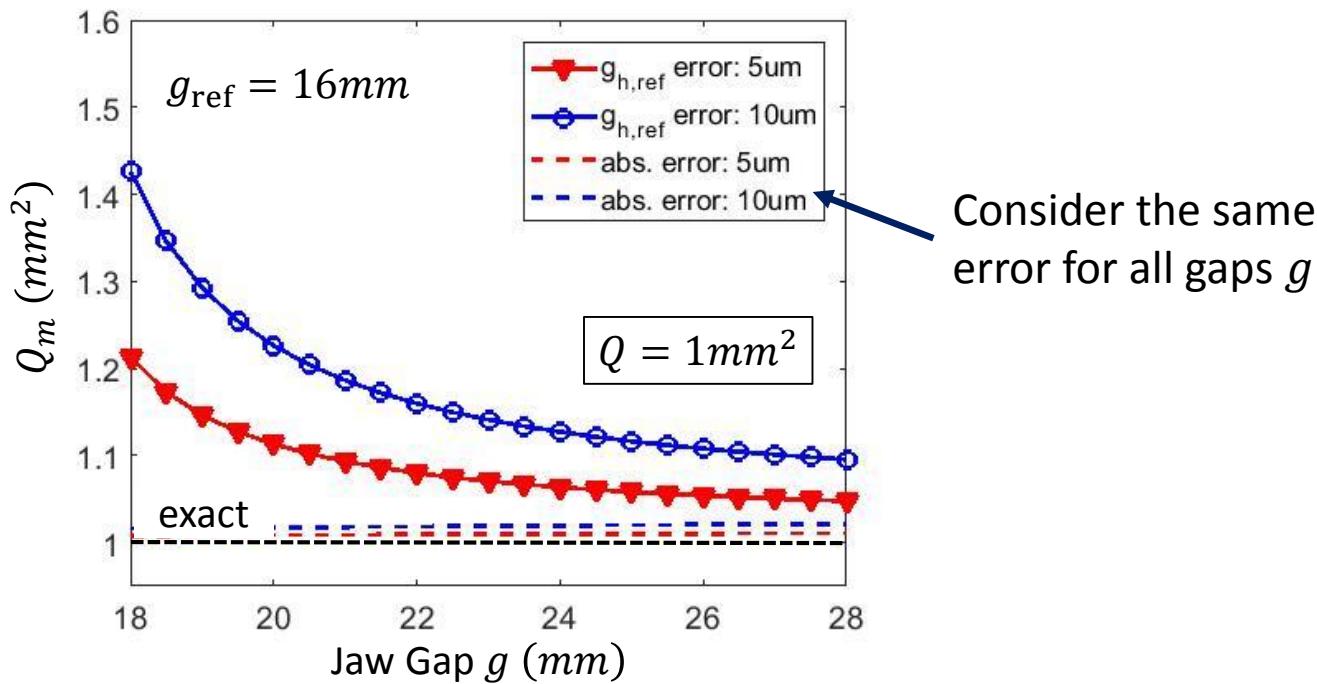
Aperture Measurement – Limitation?

Consider an error in the measurement
of the reference gap, g_{ref}



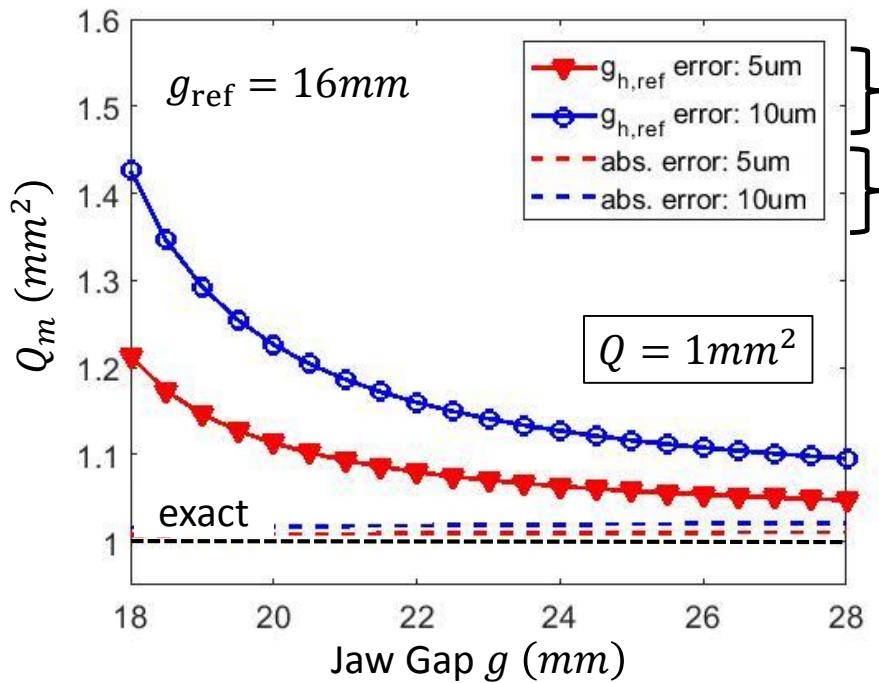
Aperture Measurement – Limitation?

Consider an error in the measurement
of the reference gap, g_{ref}



Aperture Measurement – Limitation?

Differential vs Absolute Error

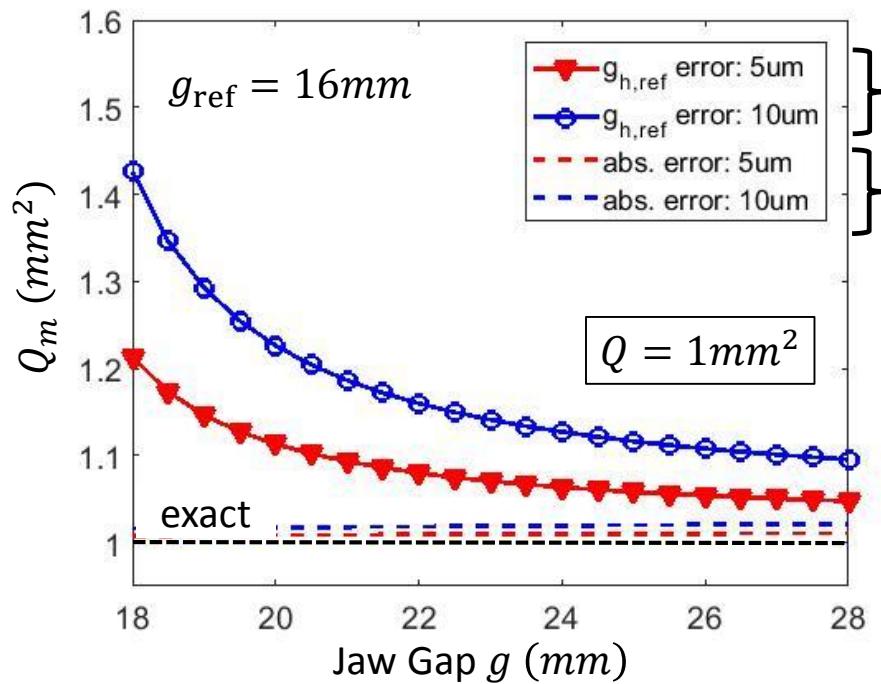


Differential errors are crucial

Absolute errors → acceptable

Aperture Measurement – Limitation?

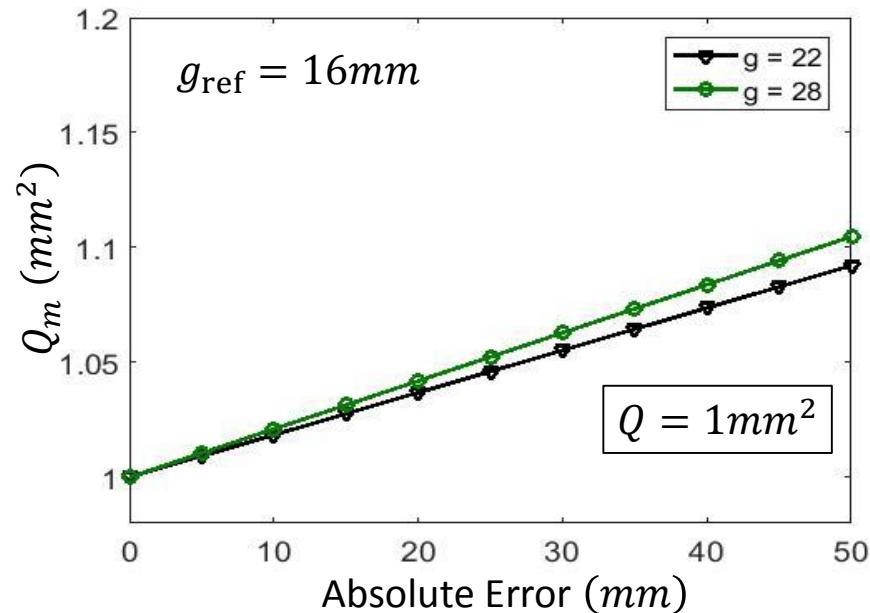
Differential vs Absolute Error



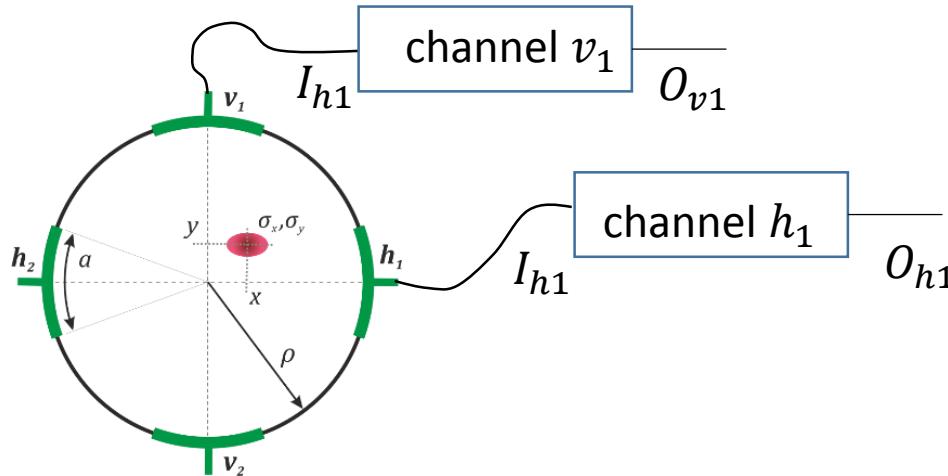
Less than 10% error for absolute aperture measurement errors up to 50 μm



Differential errors are crucial
Absolute errors → acceptable



What about Non-Linearities?

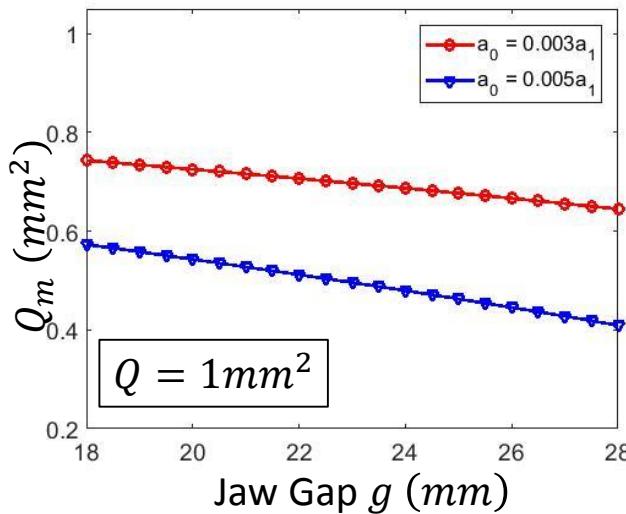


Active components may introduce offsets/ non-linear terms

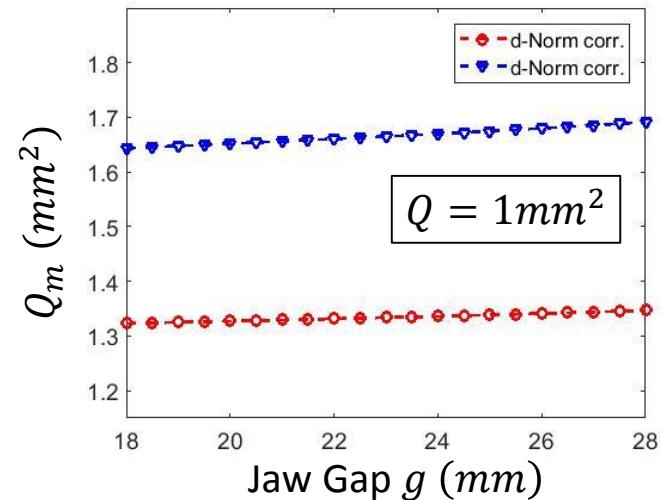
$$O = a_0 + a_1 I + a_2 I^2$$

d-Norm method is optimized to cancel linear asymmetries
(in the whole channel)

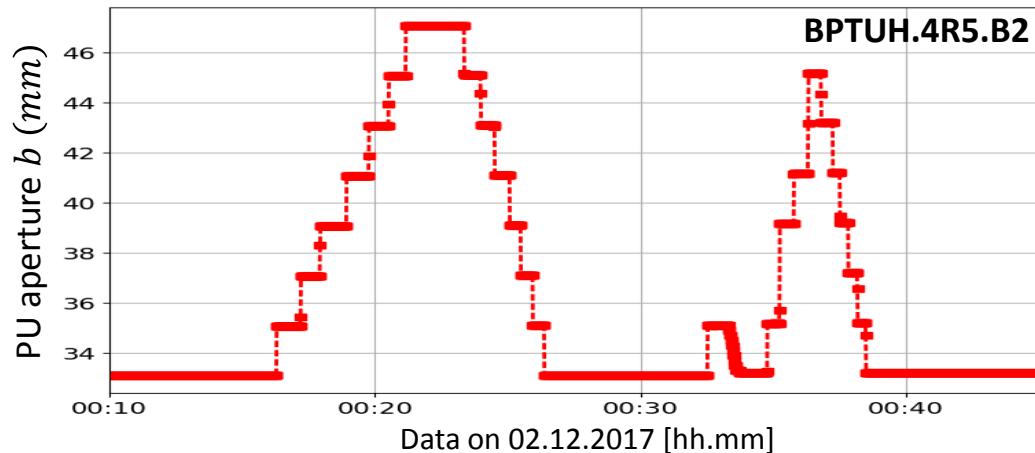
$$O_h = a_{0,h} + a_{1,h} I_h \quad O_v = a_{1,v} I_v$$



$$O_h = a_1 I_h + a_2 I_h^2 \quad O_v = a_{1,v} I_v$$

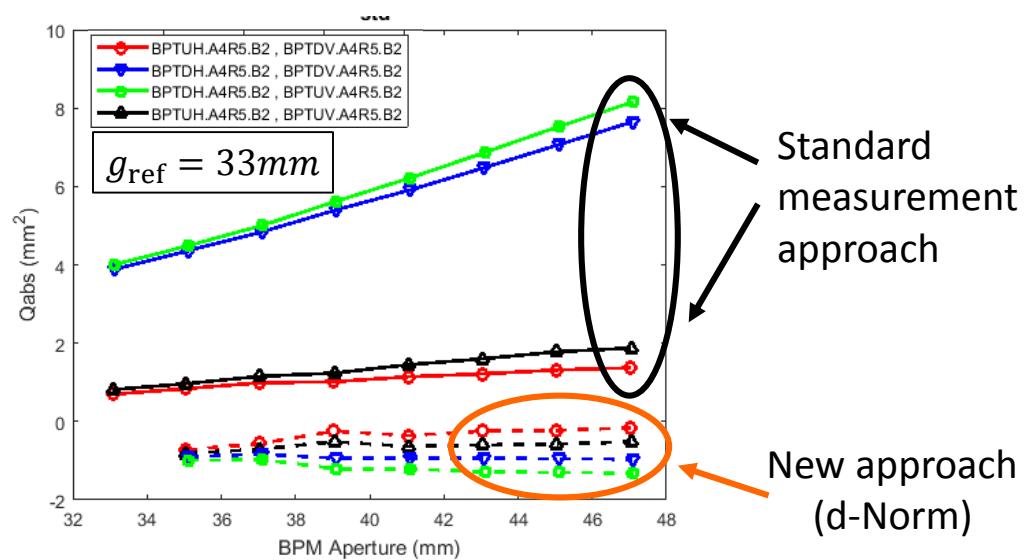


Further Tests

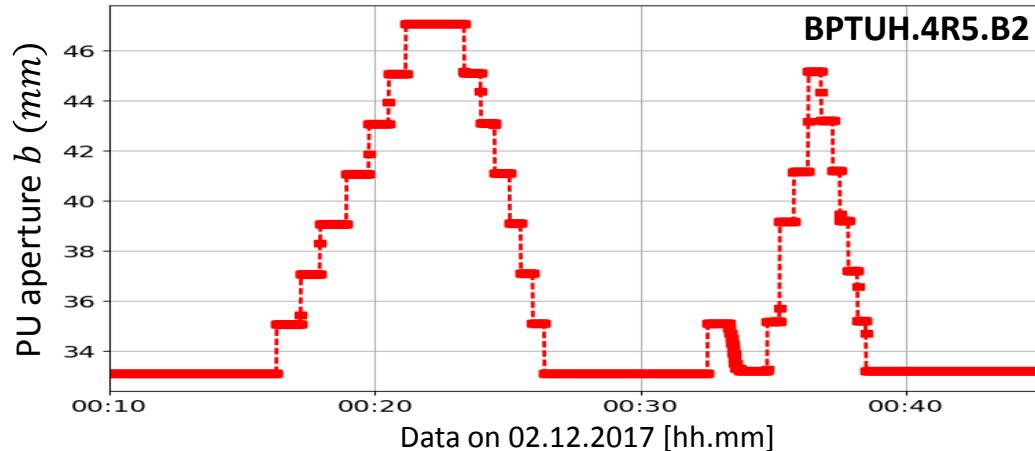


- More samples
- Cover wide aperture range
- Reconstruct uncertainties behaviour

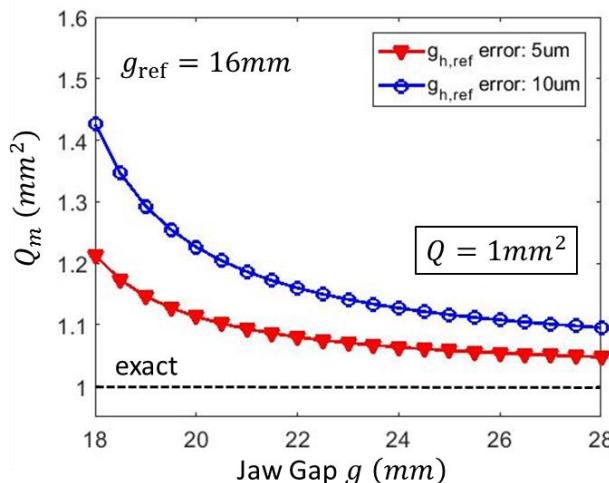
- Error of standard method dominated by linear asymmetry.
- Much smaller deviations using the d-Norm approach
- Further studies to understand the small discrepancies of d-Norm method



d-Norm Method: More Studies

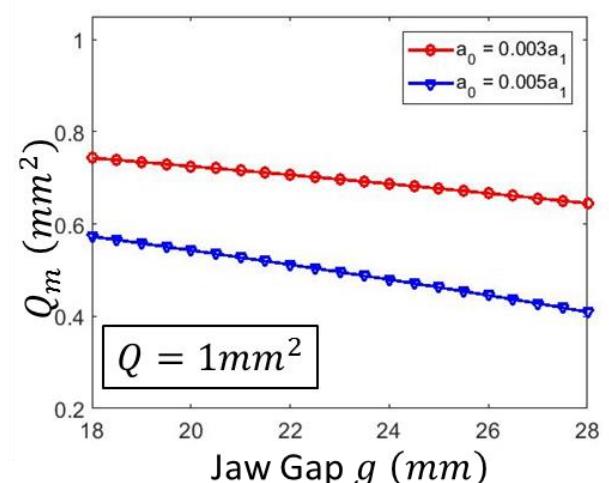


- More samples
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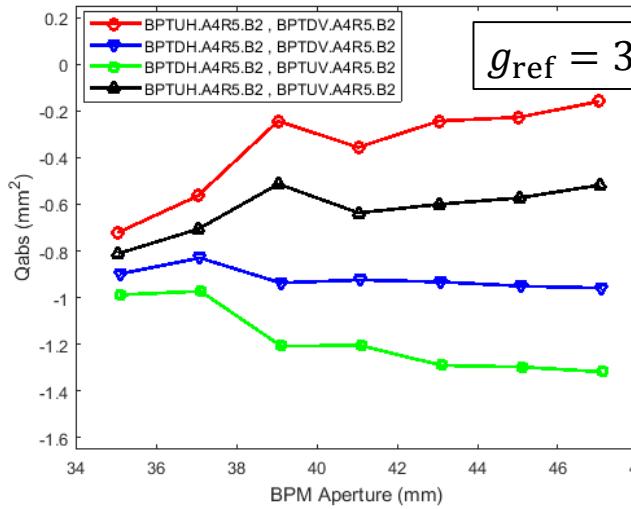


Error in differential aperture measurement

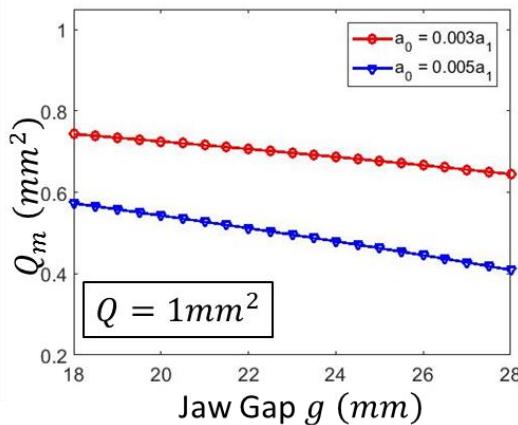
Error due to offset asymmetries



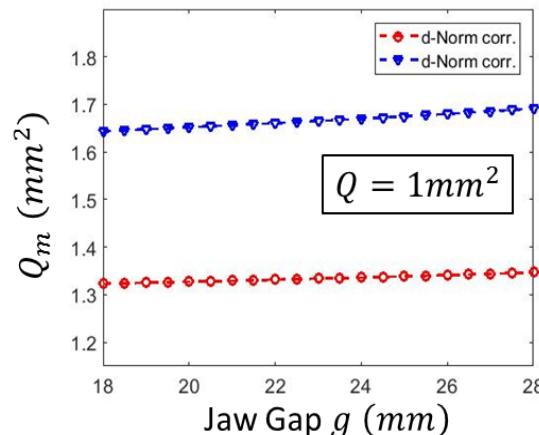
Identifying Uncertainty



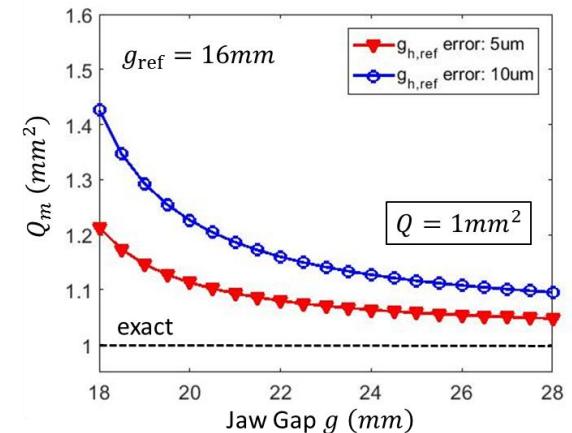
offset asymmetry



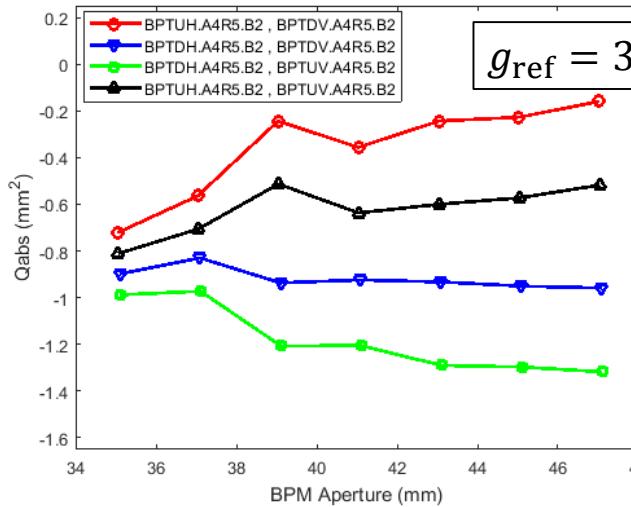
non-linear asymmetry



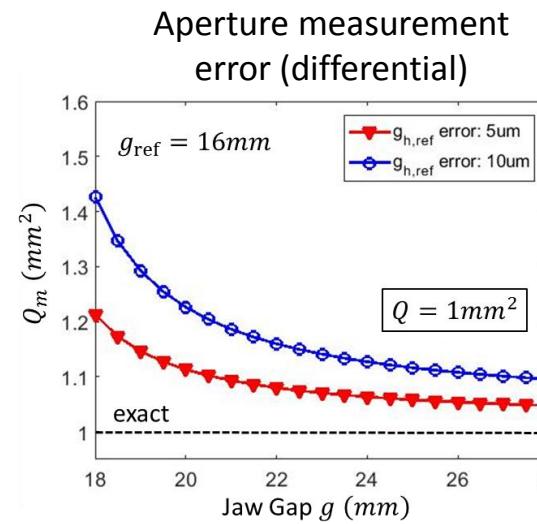
Aperture measurement error (differential)



Identifying Uncertainty



Different behaviour of aperture error - *should expect clear convergence as g increases*

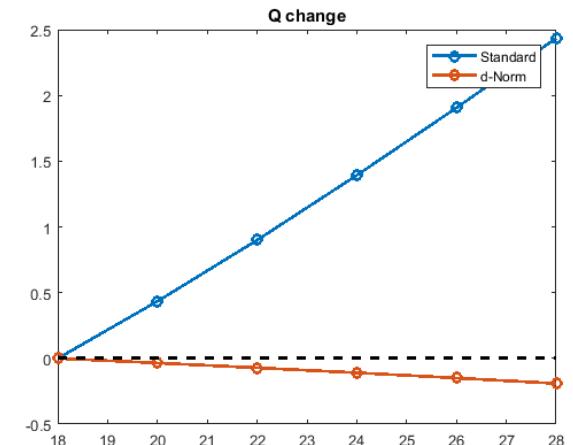
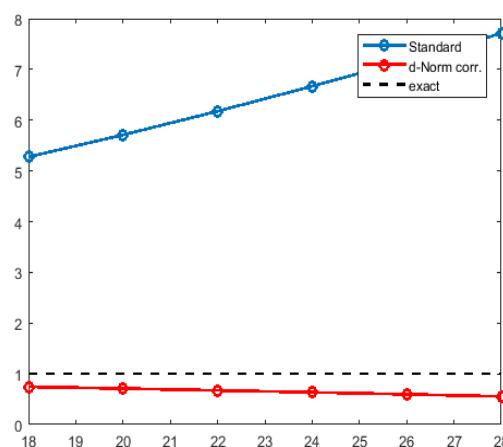


Identifying Uncertainty

Additional overview via the “standard method”

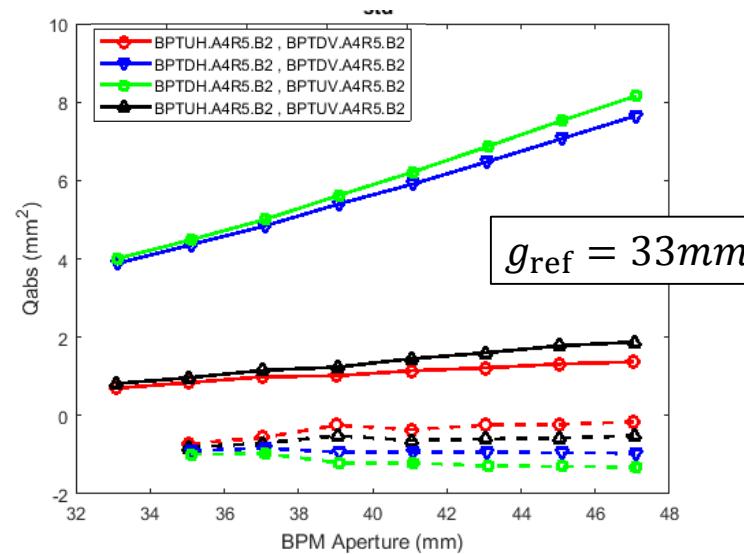
Estimation assuming asymmetries:

- $a_0 = 0.005$
- $a_1 = 0.02$
- $a_2 = 0.005$

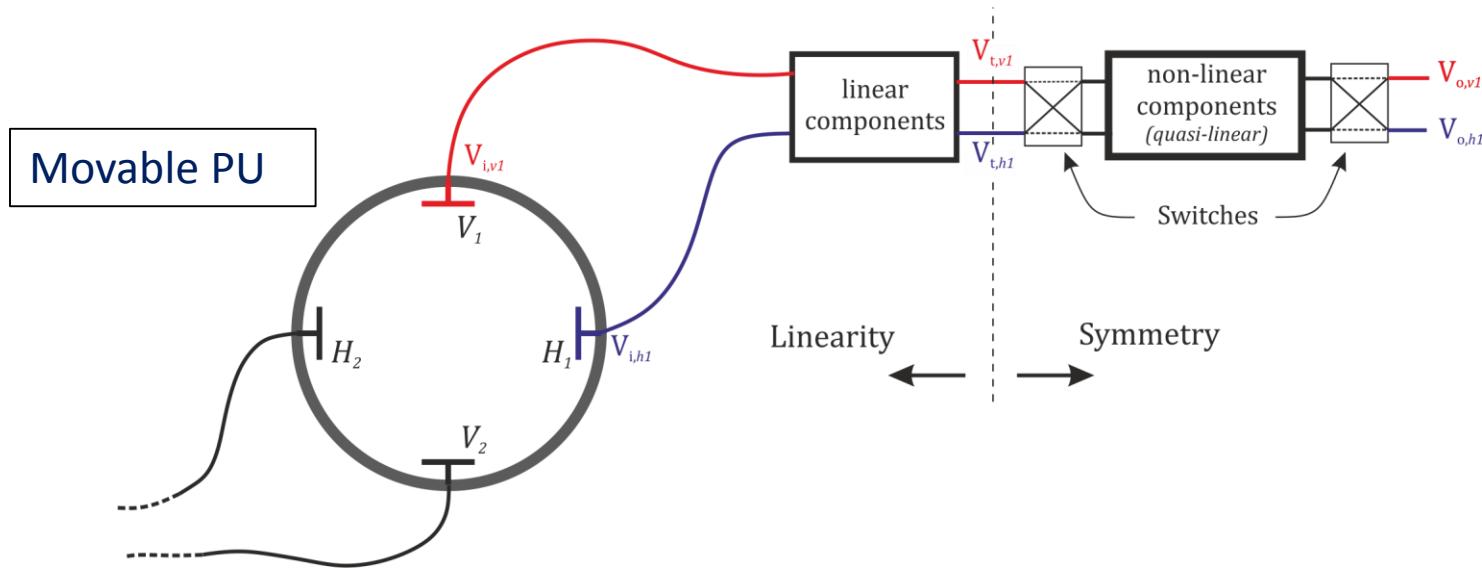


Error of standard method dominated by linear asymmetry.

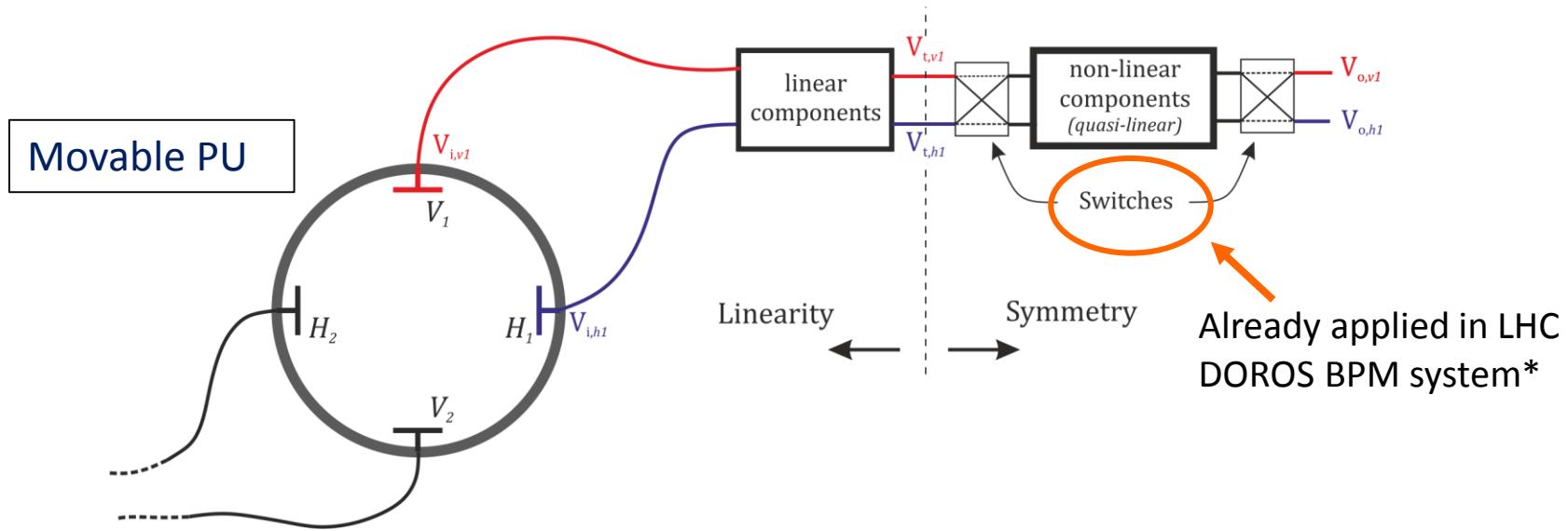
Much smaller deviations using d-Norm method



d-Norm Method – Modified

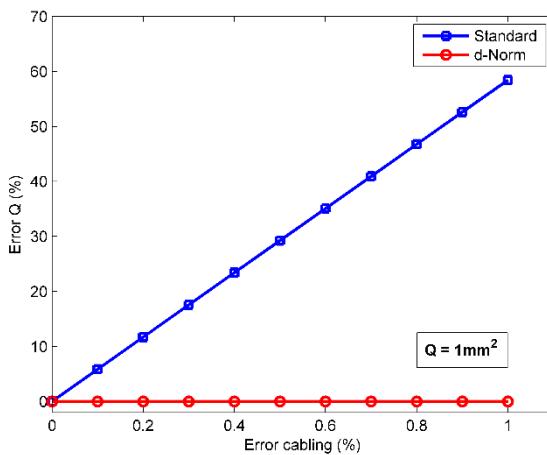
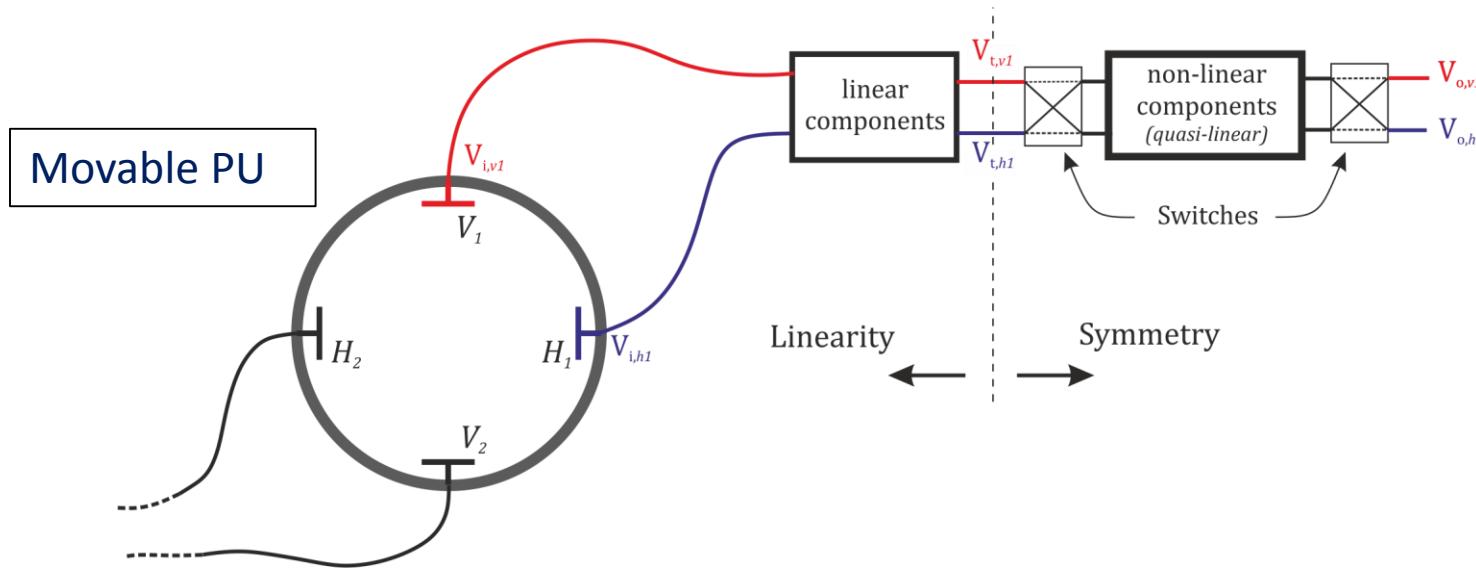


d-Norm Method – Modified



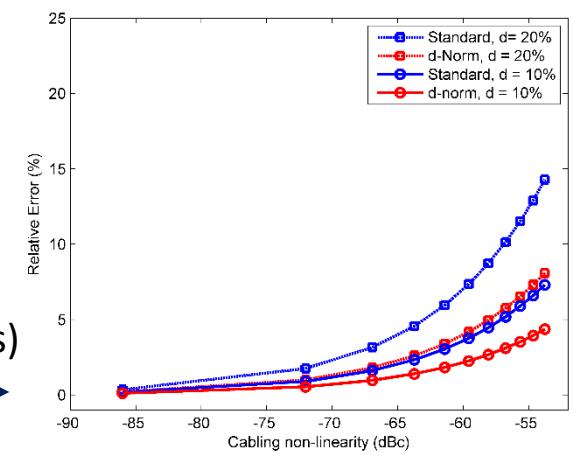
*M. Gasior, “Calibration of a non-linear beam position monitor electronics (...)”, Proceedings of IBIC 2013

d-Norm Method – Modified



Considering a cabling asymmetry

Considering a ‘non-linearity’ in the cabling part (including connectors/attenuators/switches)



Emittance Measurement

Consider two PUs at different, low dispersion, locations

$$Q^{(1)} = \beta_x^{(1)}\varepsilon_x - \beta_y^{(1)}\varepsilon_y$$

$$Q^{(2)} = \beta_x^{(2)}\varepsilon_x - \beta_y^{(2)}\varepsilon_y$$

The emittances can be derived by
solving the above linear system