

The 60th ICFA Advanced Beam Dynamics Workshop Future Light Source 2018
Mar. 8 2018, Shanghai Institute of Applied Physics

Ultra-short Period High Field Undulators for Compact Light Sources



The 60th ICFA Advanced Beam Dynamics Workshop



FLS2018 - Potential of Bulk Superconductor -

Mar. 5-9, 2018
Shanghai Institute of Applied Physics

Toshiteru KII

Institute of Advanced Energy, Kyoto University

Contents

1. Introduction

~ Limitation of Present Undulators ~

2. Bulk HTS

~ Potential of bulk HTS, How to make periodic field ~

3. Bulk HTS SAU

~ Principle of Operation, Experimental results, Numerical model ~

4. Conclusion

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1. Introduction

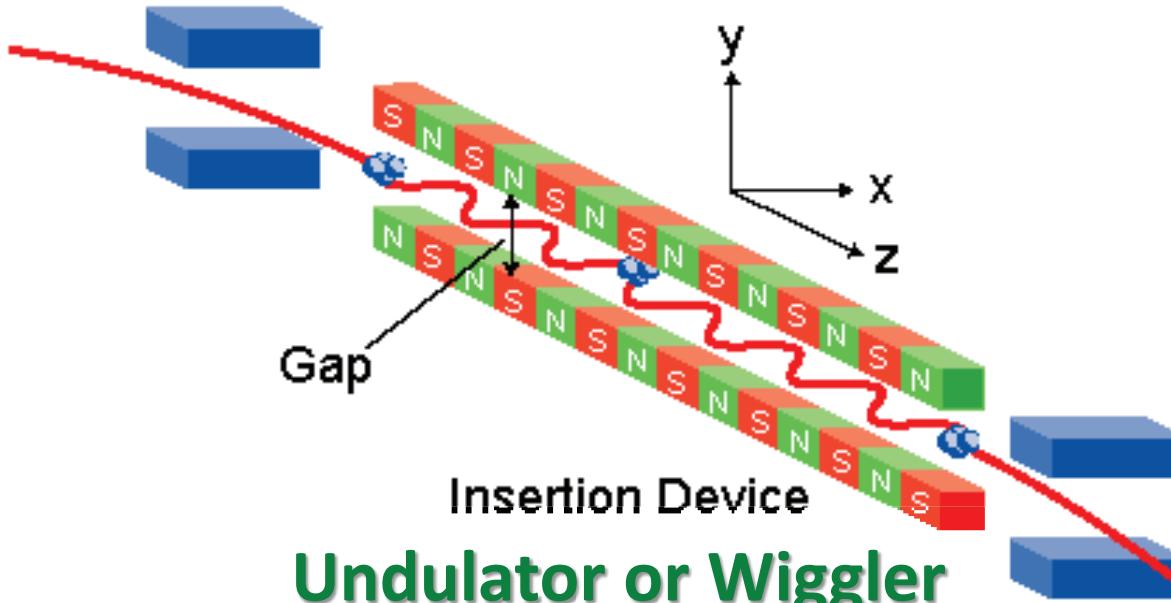
Ultra-short:

**Shorter than the established technology of
permanent magnet and SC wire.**

If we develop undulator using static material,
spin or transport current limit
the performance of the undulator.

limiting condition

Bending Magnet



Undulator or Wiggler

Radiation

$$\lambda_R [\text{\AA}] = \frac{\lambda_u}{2\gamma^2} \left(1 + \frac{K^2}{2} \right) \approx 13.056 \frac{\lambda_u [\text{cm}]}{(E[\text{GeV}])^2} \left(1 + \frac{K^2}{2} \right)$$

$$K = \frac{e \cdot B_0 \cdot \lambda_u}{2\pi \cdot m_0 c} \approx 93.36 B_0 [\text{T}] \cdot \lambda_u [\text{m}]$$

Requirement

1. Strong field in Short period

2. Field amplitude error < 1%

3. Field phase error < 3.6 degree (1%)

For Hard X-ray > 10 keV

20 GeV $\lambda_u = 36 \text{ mm}$, $B_{\text{und}} = 1.25 \text{ T}$, $K = 4.2$

14 GeV $\lambda_u = 30 \text{ mm}$, $B_{\text{und}} = 1.1 \text{ T}$, $K = 3$

8 GeV $\lambda_u = 18 \text{ mm}$, $B_{\text{und}} = 1.3 \text{ T}$, $K = 2.2$

— Technical gap —

3 GeV $\lambda_u = 5 \text{ mm}$, $B_{\text{und}} = 2.5 \text{ T}$, $K = 1.17$

3 GeV $\lambda_u = 6 \text{ mm}$, $B_{\text{und}} = 1.6 \text{ T}$, $K = 0.9$

$$\lambda_R[\text{\AA}] = \frac{\lambda_u}{2\gamma^2} \left(1 + \frac{K^2}{2} \right) \approx 13.056 \cdot \frac{\lambda_u[\text{cm}]}{(E[\text{GeV}])^2} \left(1 + \frac{K^2}{2} \right)$$

$$K = \frac{e \cdot B_0 \cdot \lambda_u}{2\pi \cdot m_0 c} \approx 93.36 B_0[\text{T}] \cdot \lambda_u[\text{m}]$$

Recent trend of SR facility

Lower cost!



Higher performance!



Compact 3rd generation SR facility

with high quality electron beam

Max IV, NSLS-II, etc. : 3 GeV $\varepsilon < 1 \text{ nmrad}$



6~8 GeV → 3 GeV → more compact!

Undulator period should be reduced
to get hard X-ray (10 keV).

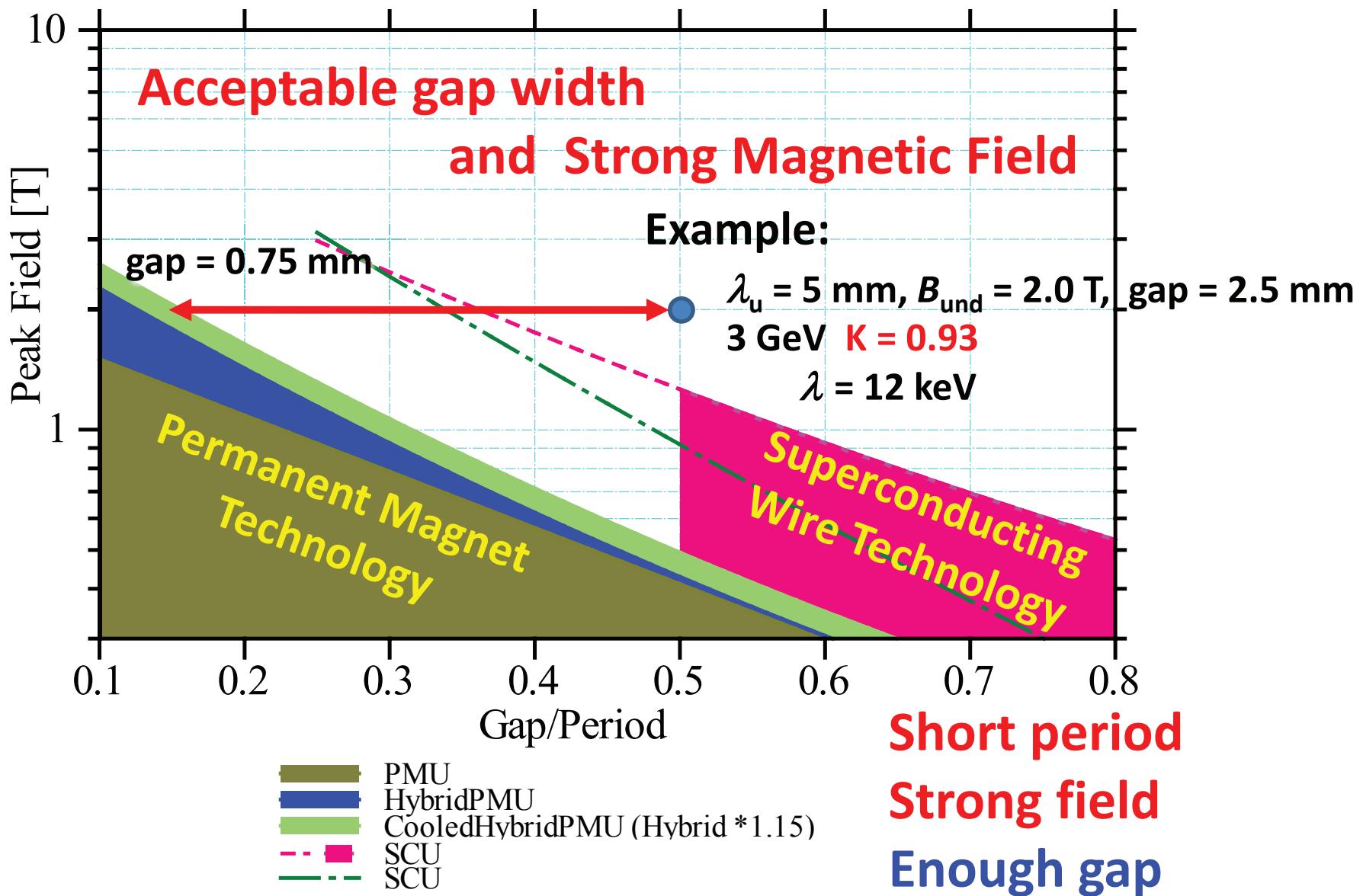
$$\lambda_R [\text{\AA}] = \frac{\lambda_u [\text{\AA}]}{2\gamma^2} \left(1 + \frac{K^2}{2} \right) \approx 13.056 \frac{\lambda_u [\text{cm}]}{(E[\text{GeV}])^2} \left(1 + \frac{K^2}{2} \right)$$

Required magnet: (Example)

$E_e = 3 \text{ GeV}, 12 \text{ KeV}$ require $\lambda_u = 5 \text{ mm}$, $B_{\text{und}} = 2 \text{ T}$

Such Ultra High-performance Undulator was not established!

Design flexibility of Compact LS using Ideal Undulators



Toward inaccessible region

permanent magnet

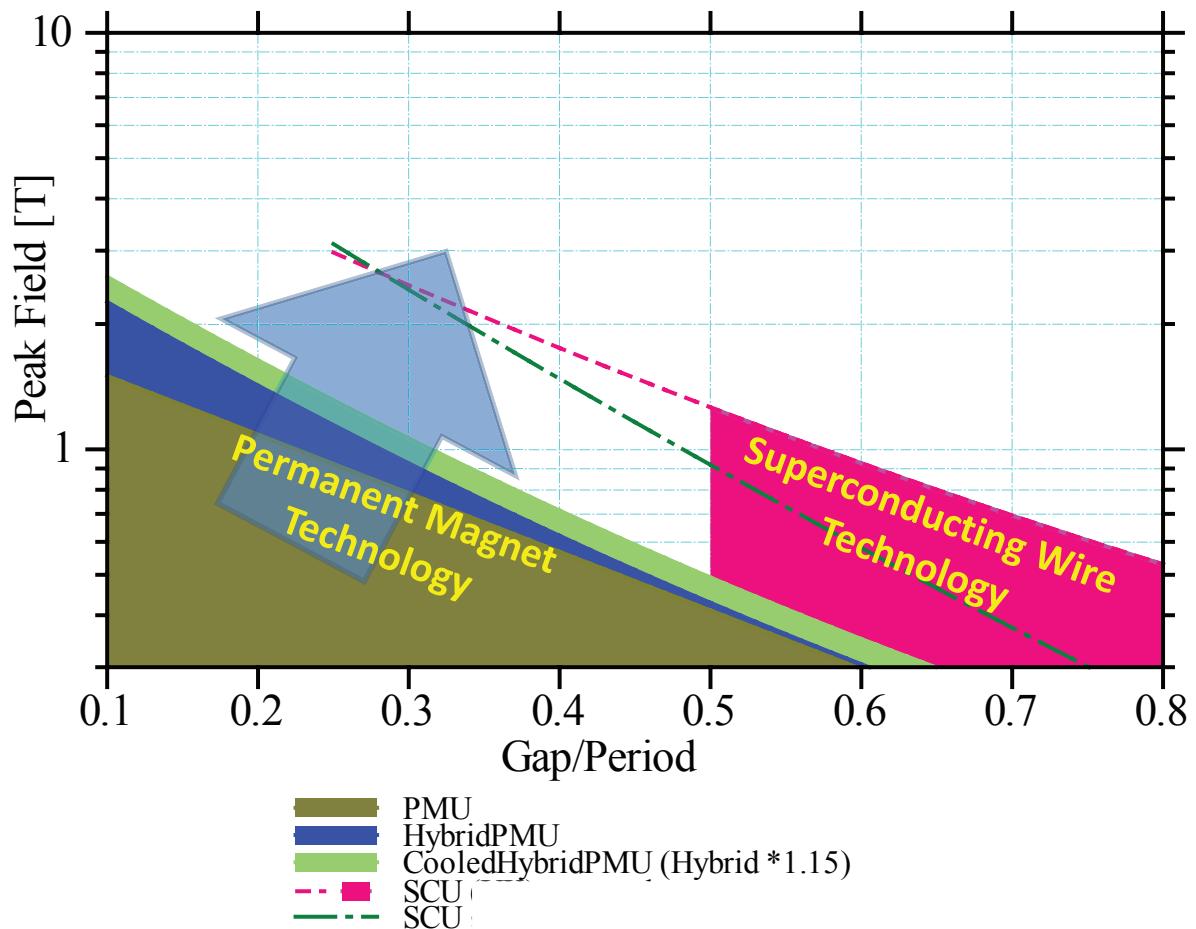
- BH(max) is approaching to the theoretical limit.

- New material?
- New structure?

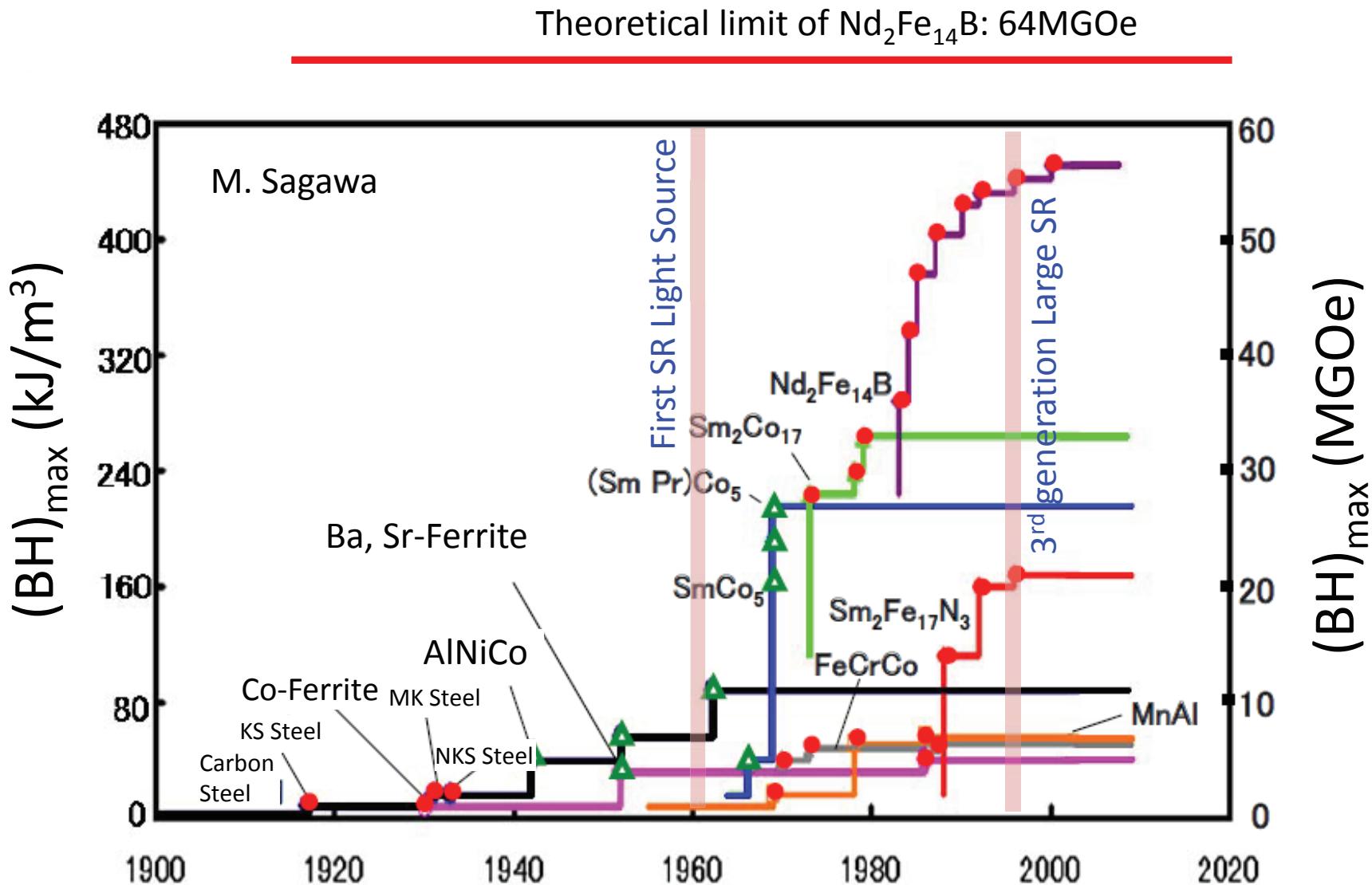
Anisotropic Nanocomposite

Superlattice Ordering

These new material/structure are not established yet.



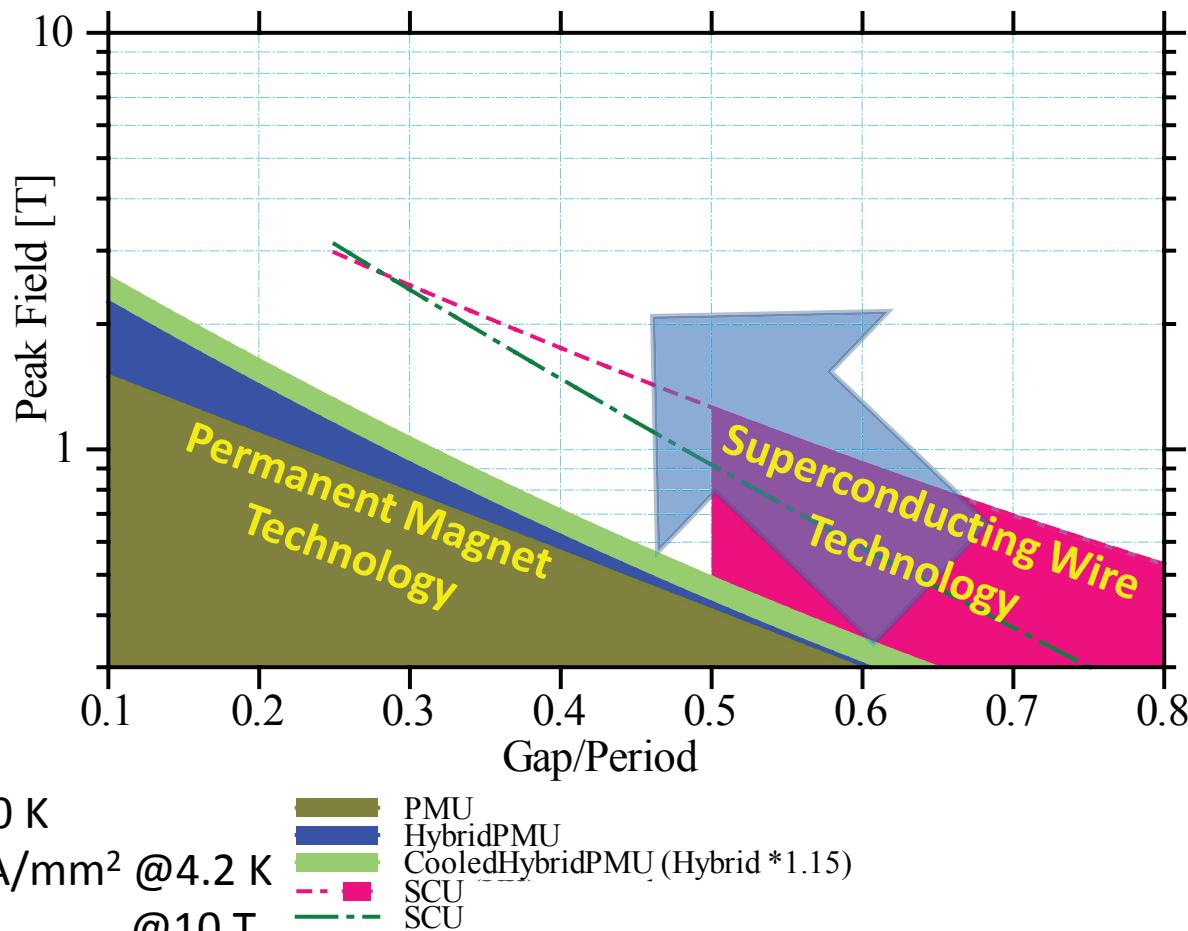
History of Permanent Magnet



Toward inaccessible region

Superconducting wire

- Engineering Critical Current Density of SC wires are still increasing!
- Nb₃Sn, NbTi, and REBCO CC are promising.
1 kA/mm² @ 4.2K or 2K
- New material
MgB₂ (2001)/ FeSC (2008)?
FeSC has high potential.



LaFeAsO_{1-x}F_x 1111

ReFePnO family 1111

Good Jc-B property is obtained for small bulk or single crystal.

T_c: > 50 K

J_c: 1 kA/mm² @ 4.2 K
@ 10 T

PMU
HybridPMU

CooledHybridPMU (Hybrid *1.15)

SCU

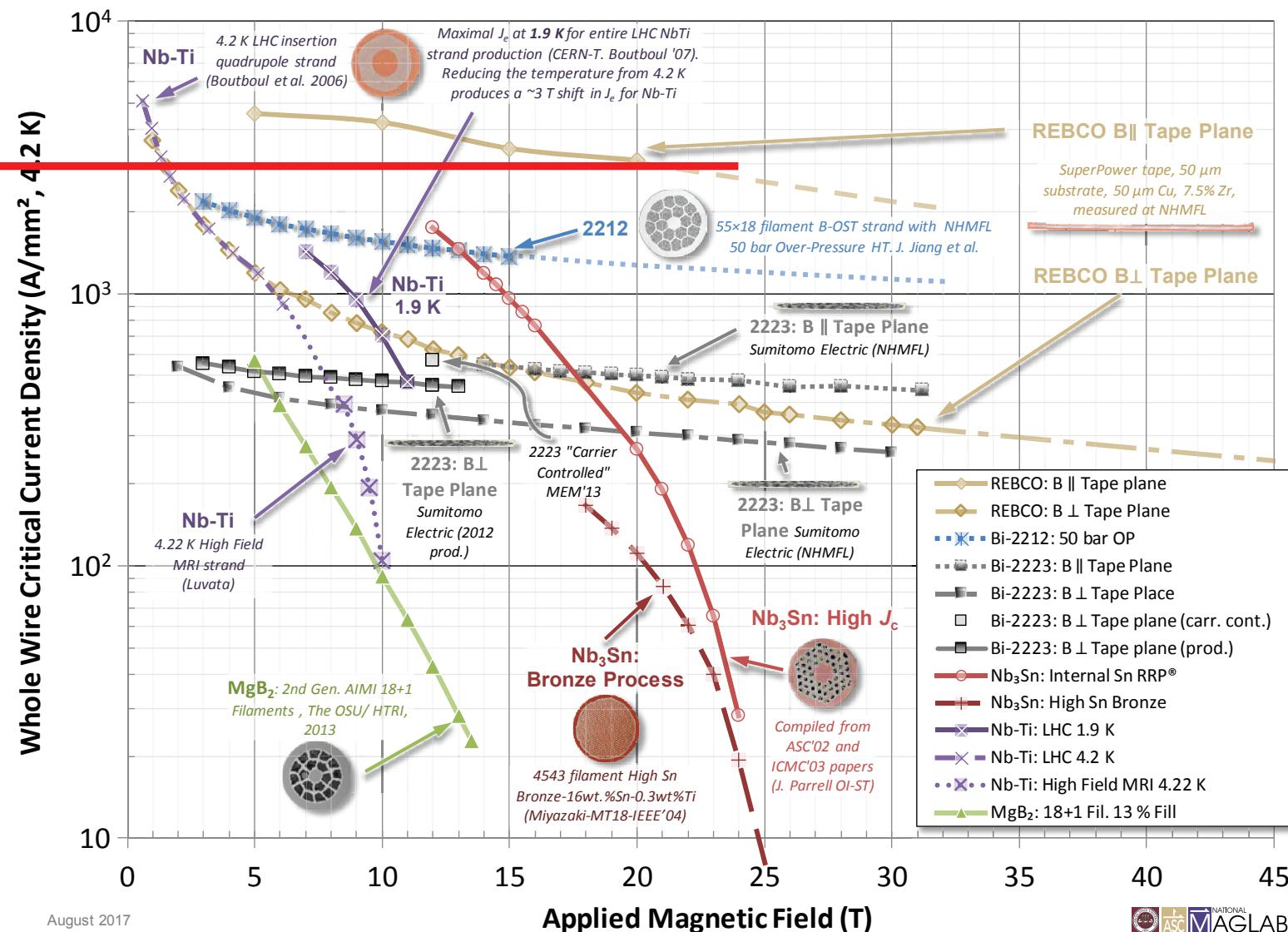
SCU

Engineering Critical Current Density vs. Applied Field

3 kA/mm²

Nb₃Sn wire is most promising.

3 kA/mm²
@4.2 K, 10 T



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2 Potential of bulk HTS

~How to make periodic field~

Permanent magnet: New material is not available.

Superconducting Wire: Practical level is 1 kA/mm^2 .

Bulk HTS ?

Short-period Undulator and Design flexibility of Compact LS

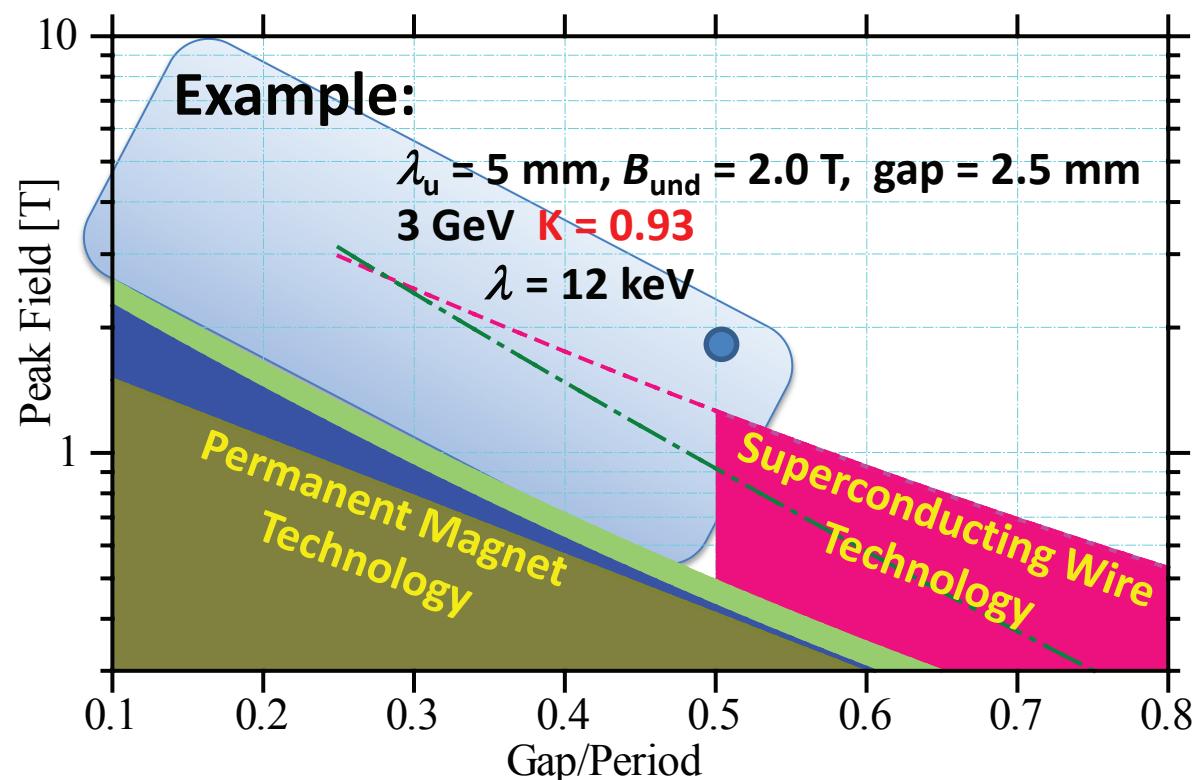
Short period **5 – 10 mm**

High field **> 1 T**

Enough gap **> 2 mm**

$$\lambda_R^\circ [A] = \frac{\lambda_u}{2\gamma^2} \left(1 + \frac{K^2}{2}\right) \approx 13.056 \frac{\lambda_u [\text{cm}]}{(E[\text{GeV}])^2} \left(1 + \frac{K^2}{2}\right)$$

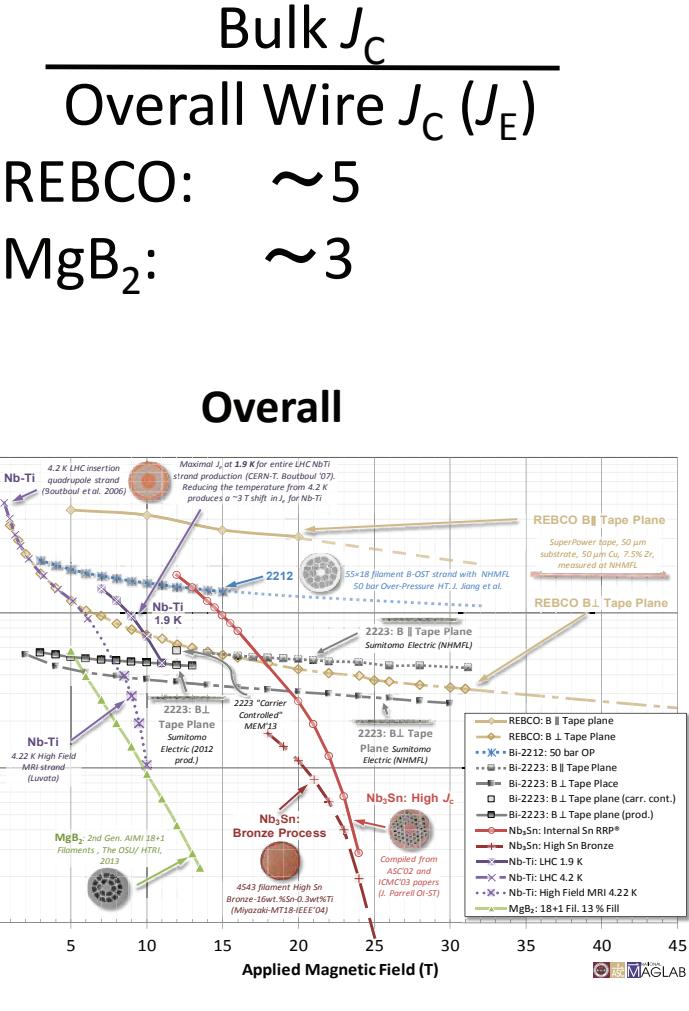
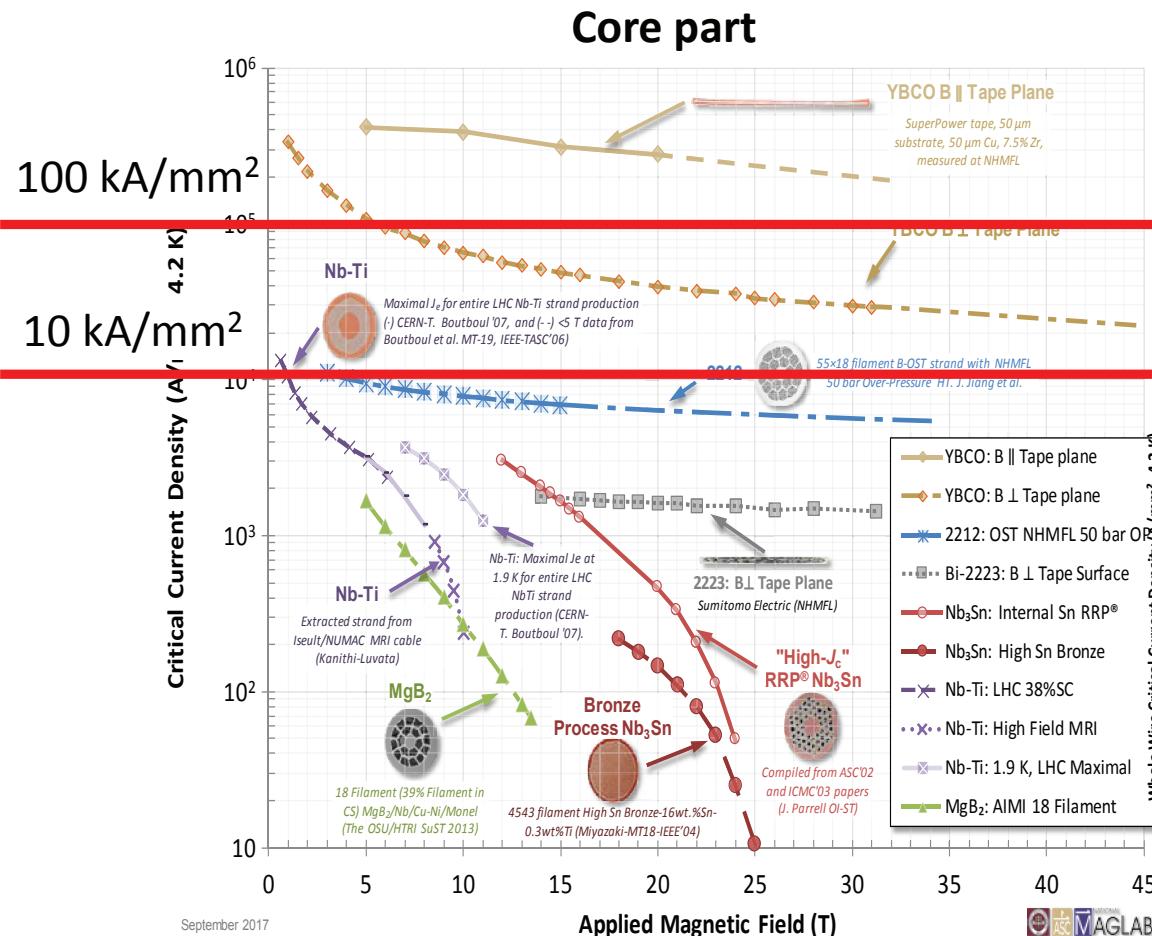
Can we get to the “fresh ground” ?



Toward inaccessible region

3. Superconducting bulk

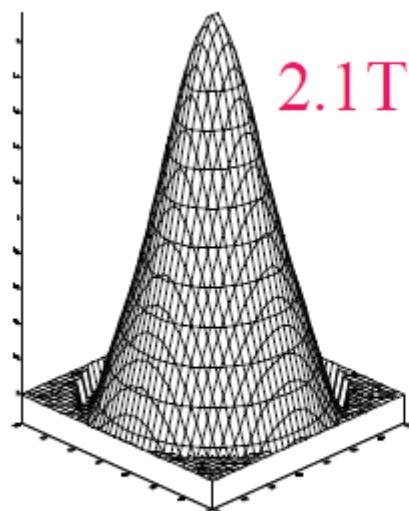
- Core part of superconducting wires have higher current density.



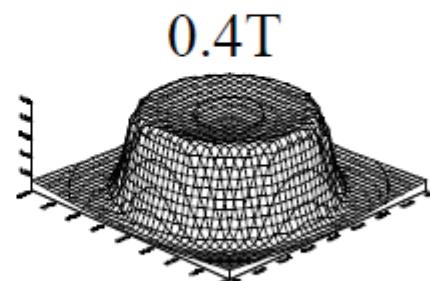
Potential of bulk Superconductor

Bulk superconductor can be used as

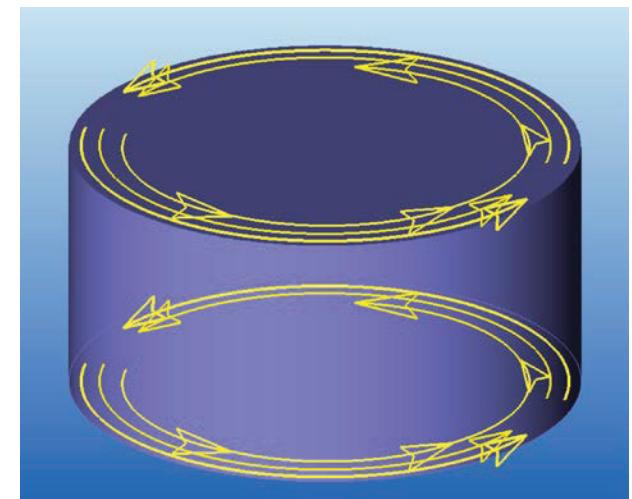
Very Strong Permanent Magnet



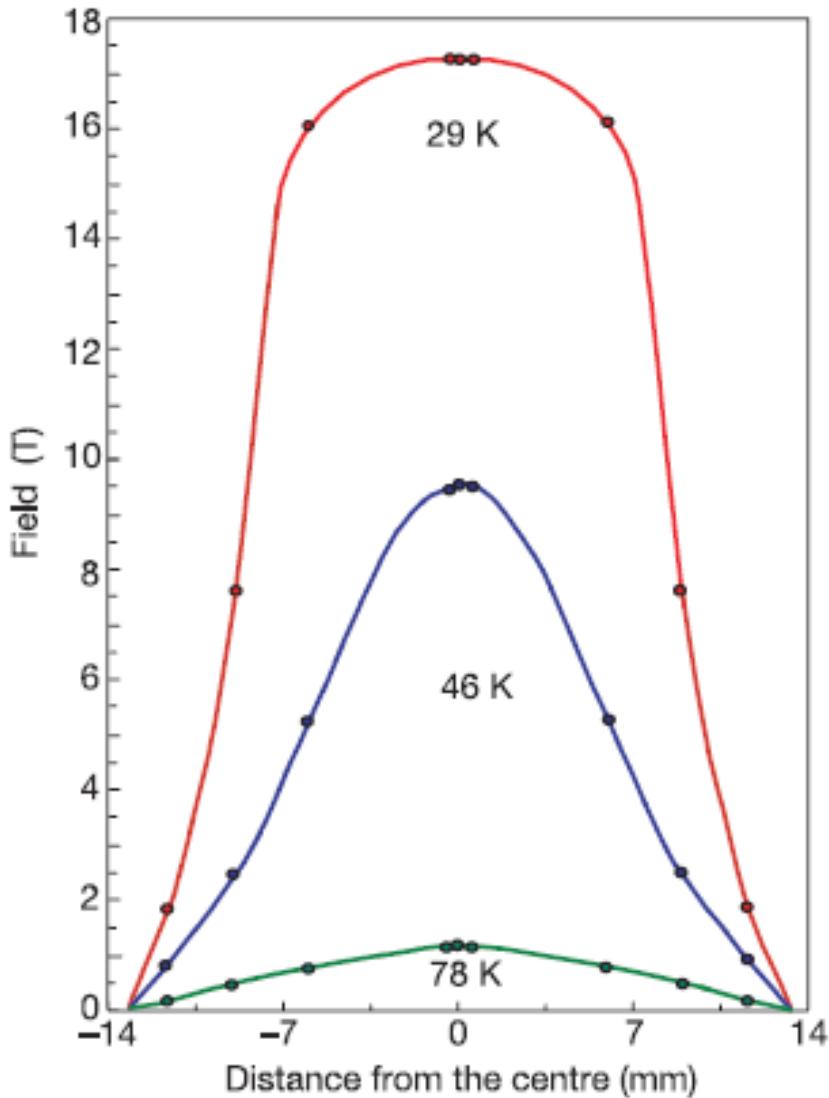
Bulk SC Magnet
Diameter : 60 mm
Temperature : 77 K



Permanent Magnet
NeFeB



Performance of bulk HTS at low temp.



Y-Ba-Cu-O

Thickness :15 mm

Diameter: 26.5 mm

~17 T @ 29K

M. Tomita, M. Murakami,
NATURE Vol. 421, 30 January 2003

17.4 T

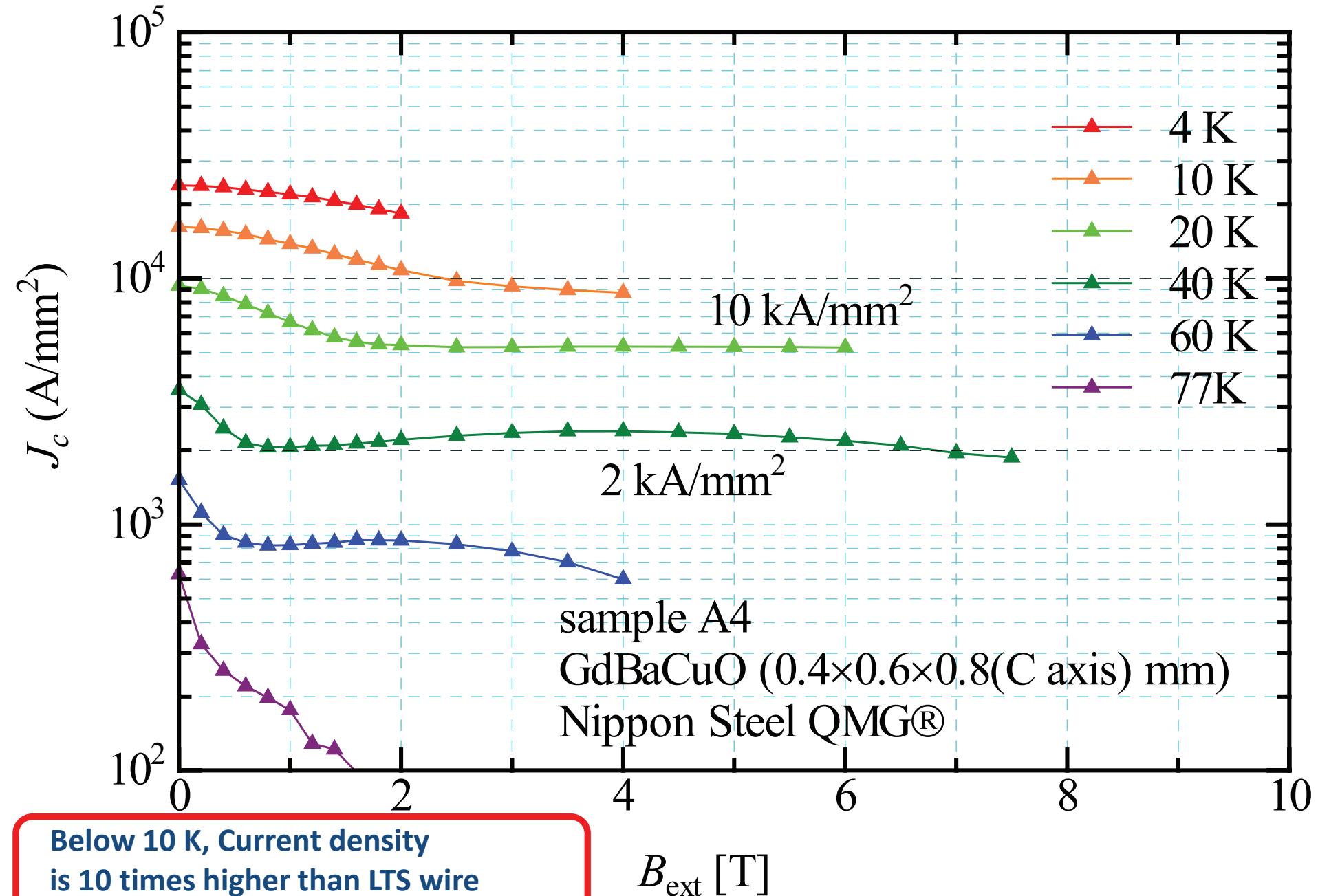
J. H. Durrell et al.,
Supercond. Sci. Technol. 27 0820001 2014

17.6 T

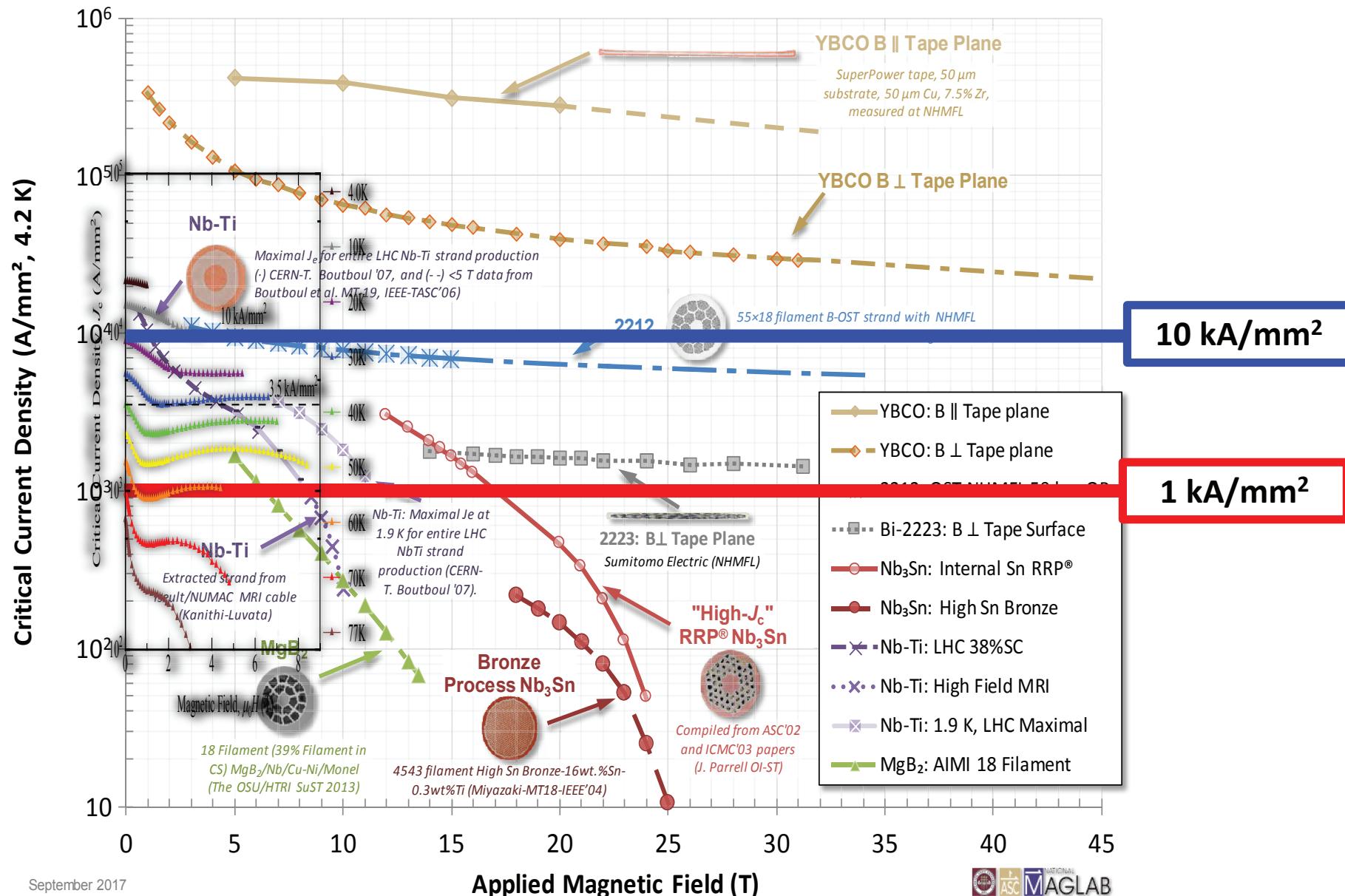
M. Tomita, M. Murakami,

Performance of Bulk HTS material (GdBaCuO)

19

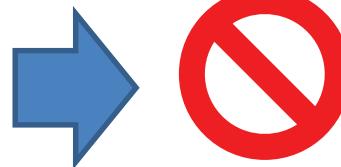


Material J_c = Core part of wires, Bulk HTS itself(overlay)



How to make Periodic field using Bulk SC

Magnetize bulk HTS in SC Magnet
then
Move bulk HTS and Assemble Array



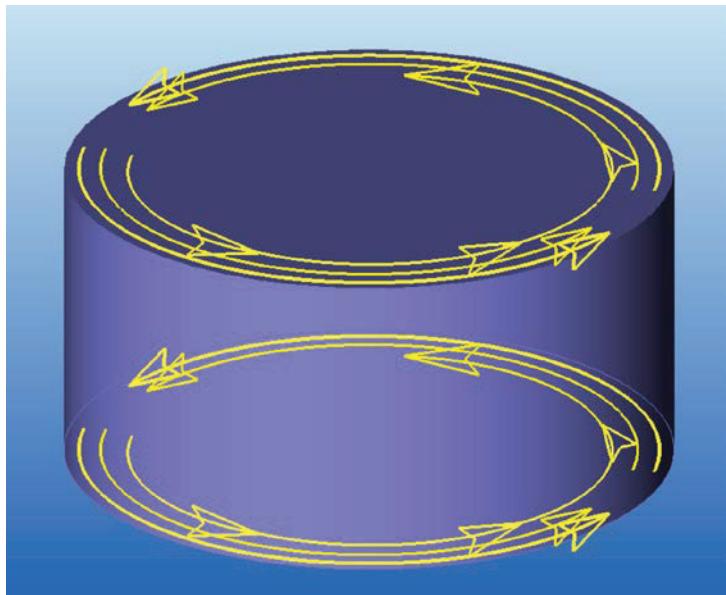
NOT
Realistic!

Magnetize bulk **HTS Array** in SC Magnet



Possible?

How to excite induction current in single bulk SC



External B-field is changed.
→ Induction currents appear to
keep B-field in the bulk SC.

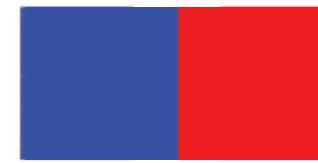
“External B-field is
trapped by bulk SC.”

Side View



Partially magnetized

Side View

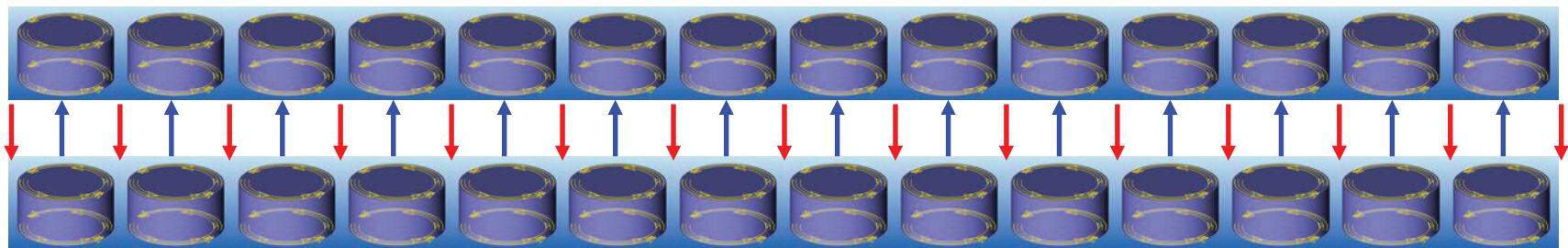


Fully magnetized

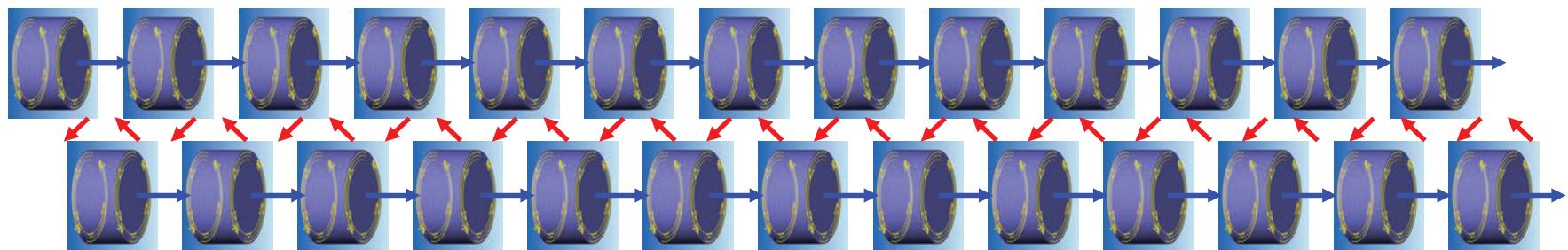
If HTS Array is placed in SC Magnet...

Two configurations of HTS array

1. SPring-8 T. Tanaka *et al.* (2005)



2. Kyoto-U T. Kii *et al.* (2006)



Periodic magnetic field is generated.

1. SCPMU (SPring-8)

Pure-type superconducting permanent-magnet undulator

2005

Journal of
Synchrotron
Radiation
ISSN 0909-0495

Takashi Tanaka,* Rieko Tsuru and Hideo Kitamura

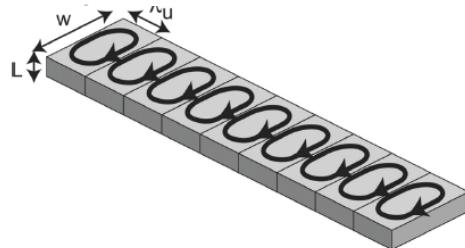


Figure 1
An array of magnetized superconducting blocks that work as PMs.

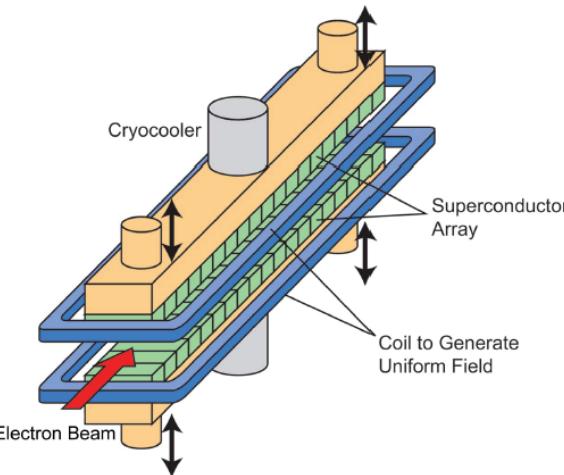


Figure 2
Schematic illustration of the SCPMU.

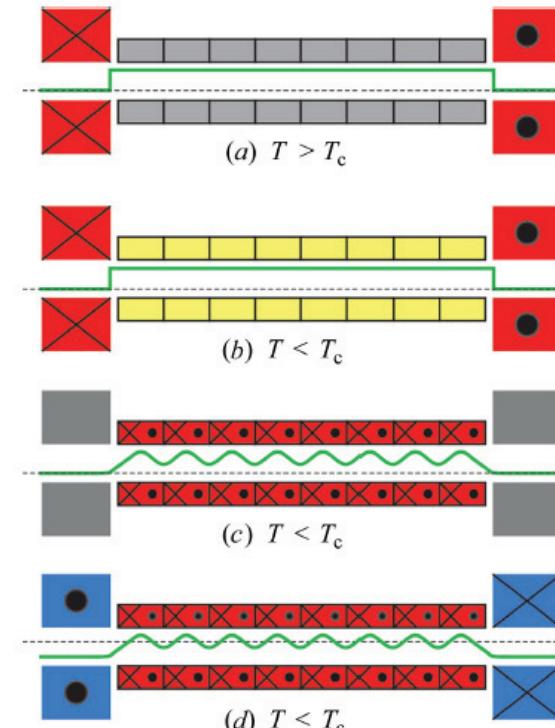


Figure 3
Method for magnetizing the HTSCs and eliminating the field offset in type A.

Bulks have to be fully magnetized.

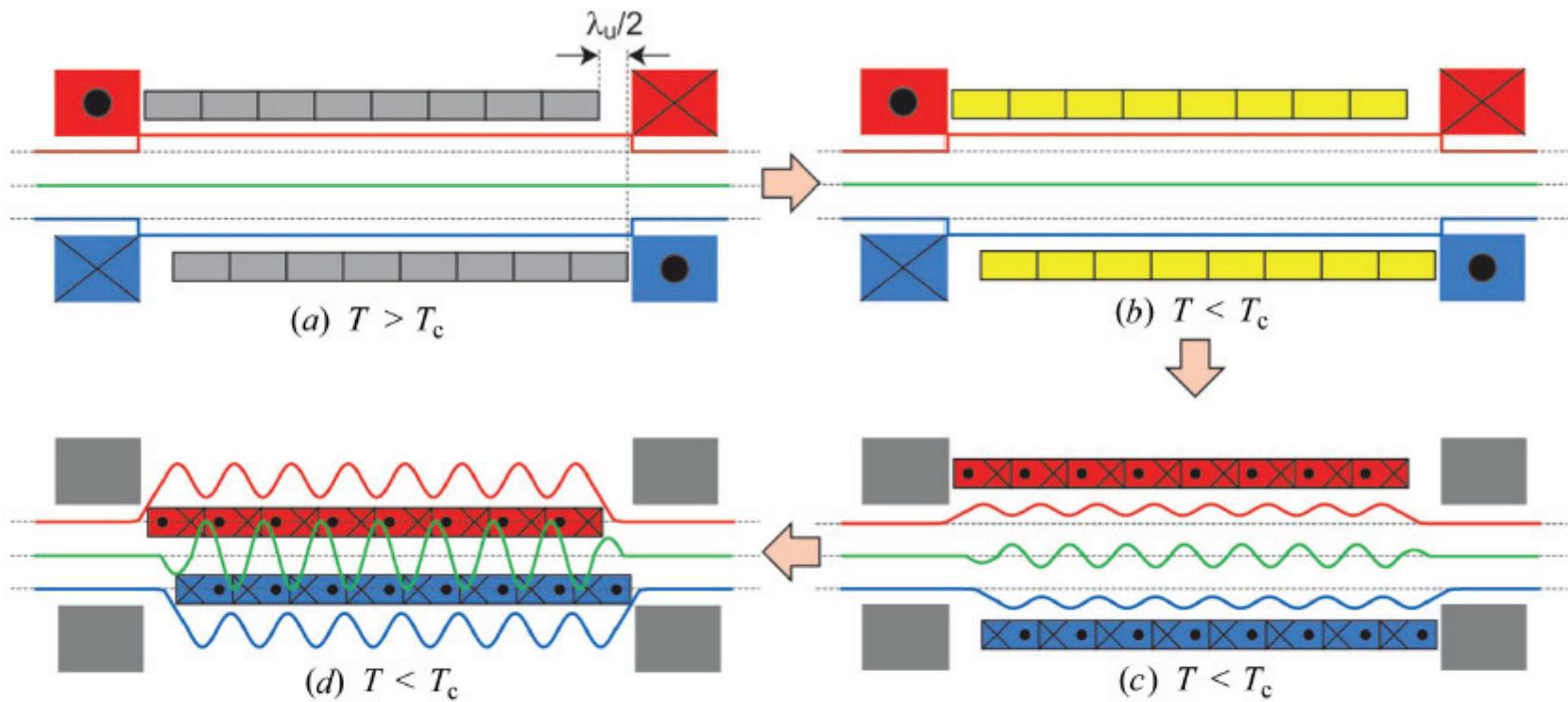
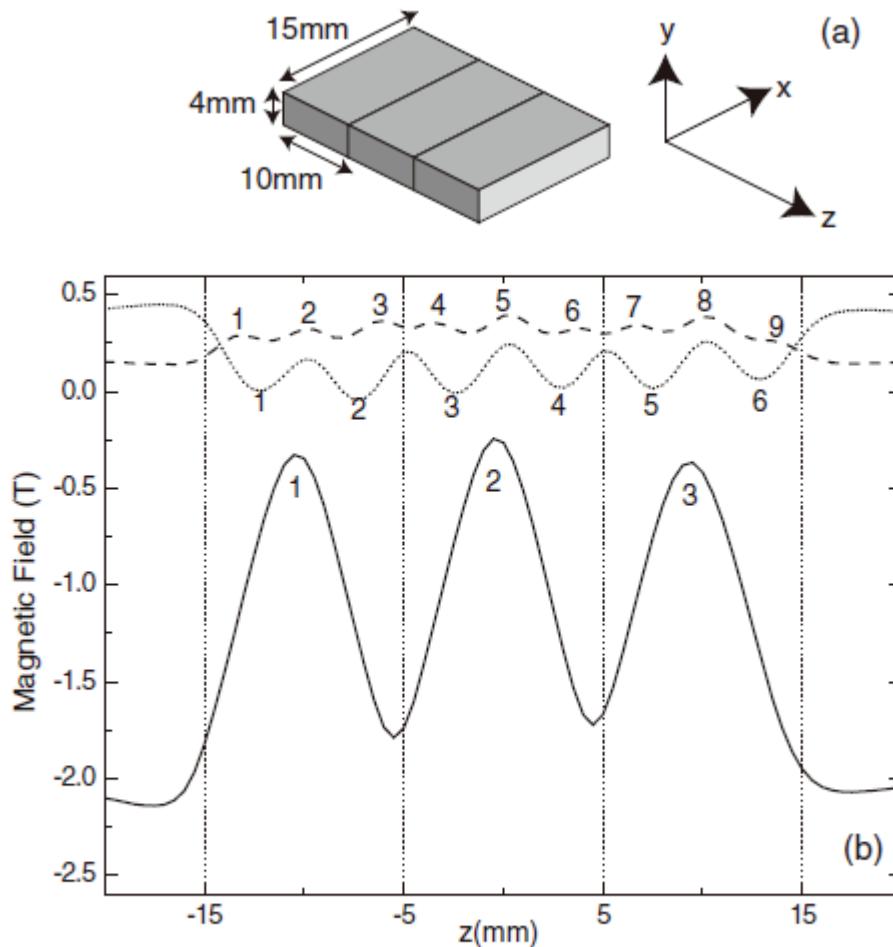


Figure 4

Method for magnetizing the HTSCs and eliminating the field offset in type B.



**Period length of 10 mm
Gap is not defined
(half array)**

Figure 8. Measured magnetic distribution for the three pieces of HTS bulk magnets.

Better performance will be obtained at lower temp.

**Expected
 B_{und}**

$$B_p = \frac{2\mu_0 I}{\lambda_u} \frac{1 - \exp(-k_u b)}{k_u b} \frac{\sin(k_u a/2)}{k_u a/2} \exp(-k_u g/2). \quad (6)$$

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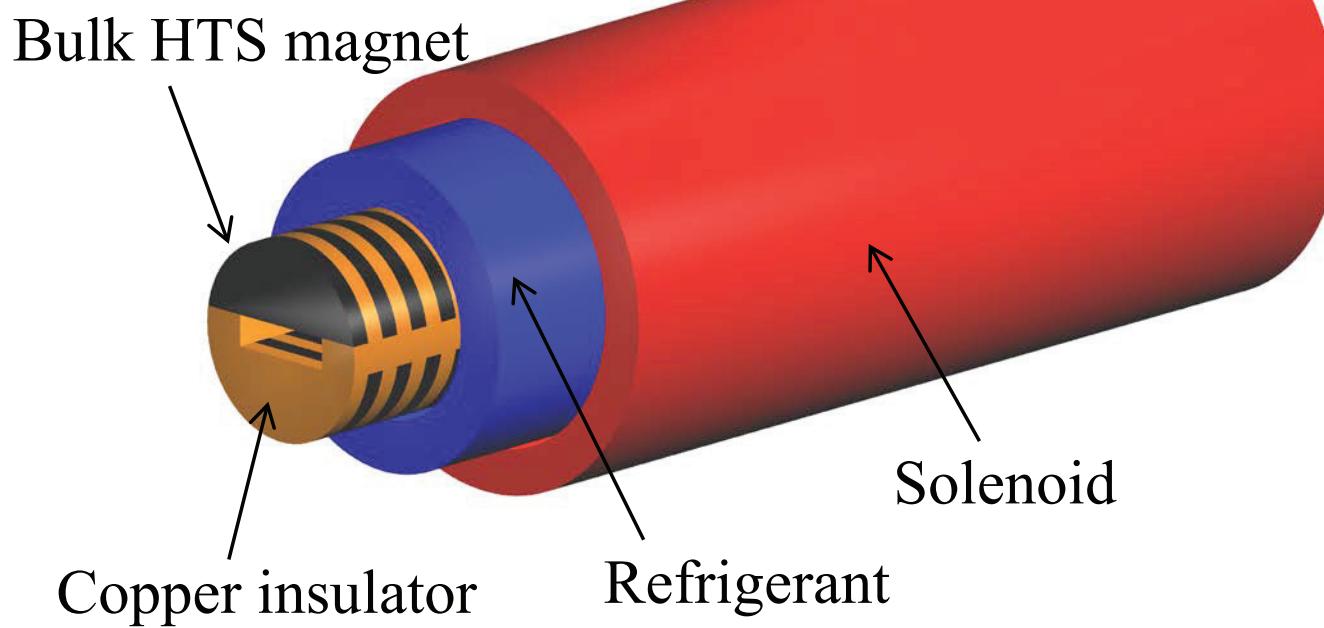
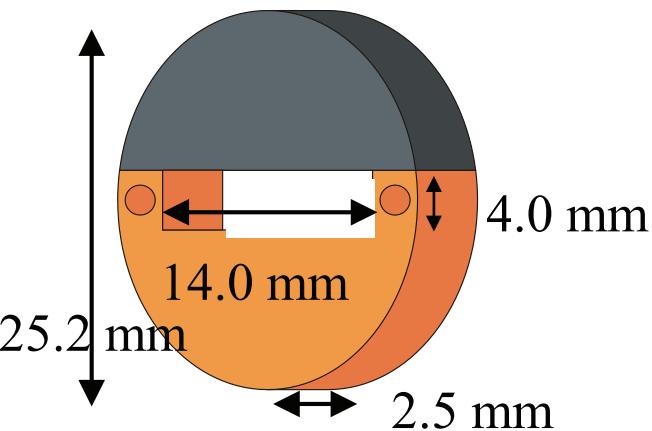
~ Principle of Operation, Experimental results, Numerical model ~

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Bulk HTS Undulator (Kyoto-U)

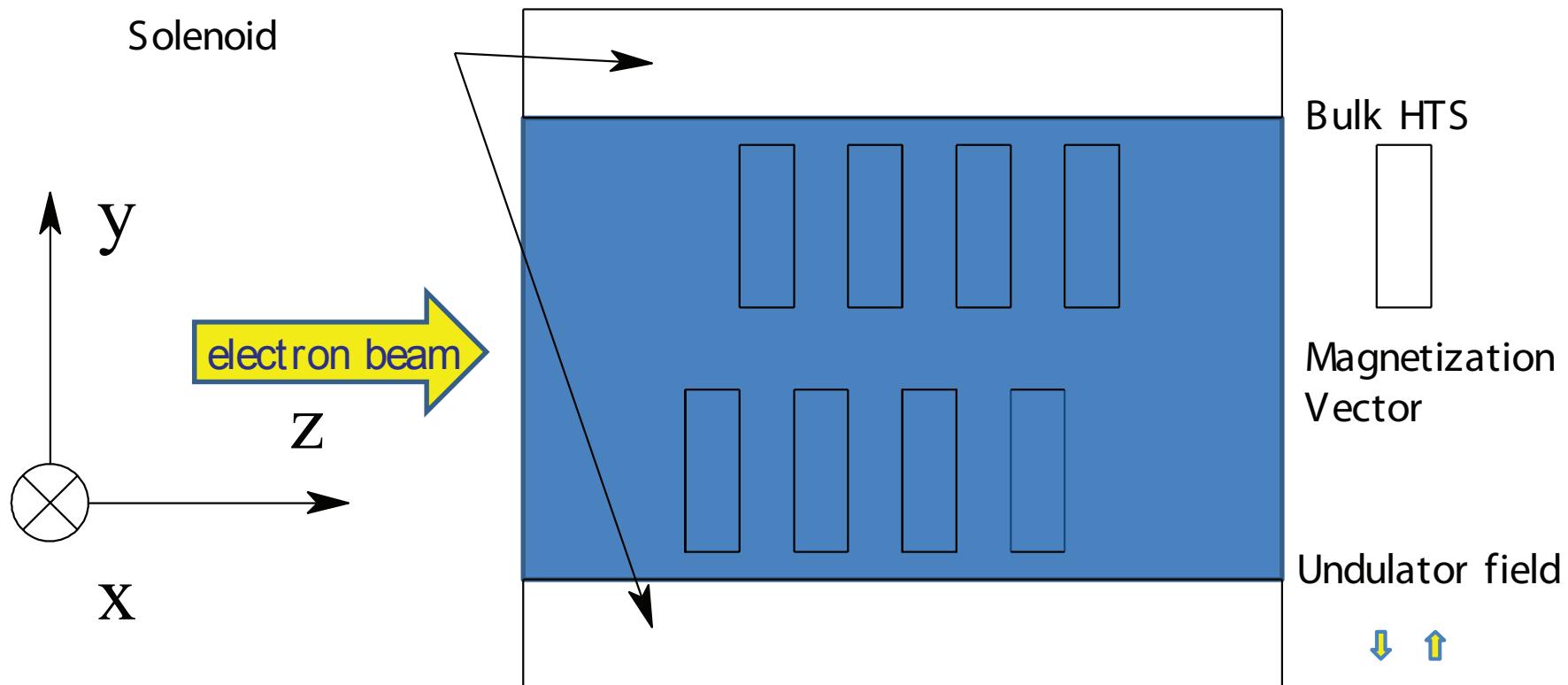
We proposed
new structure using bulk HTS

Bulk HTS SAU =
Stacked HTS array + Solenoid



Principle of Operation bulk HTS SAU (1)

Side view of “Bulk HTSC SAU”

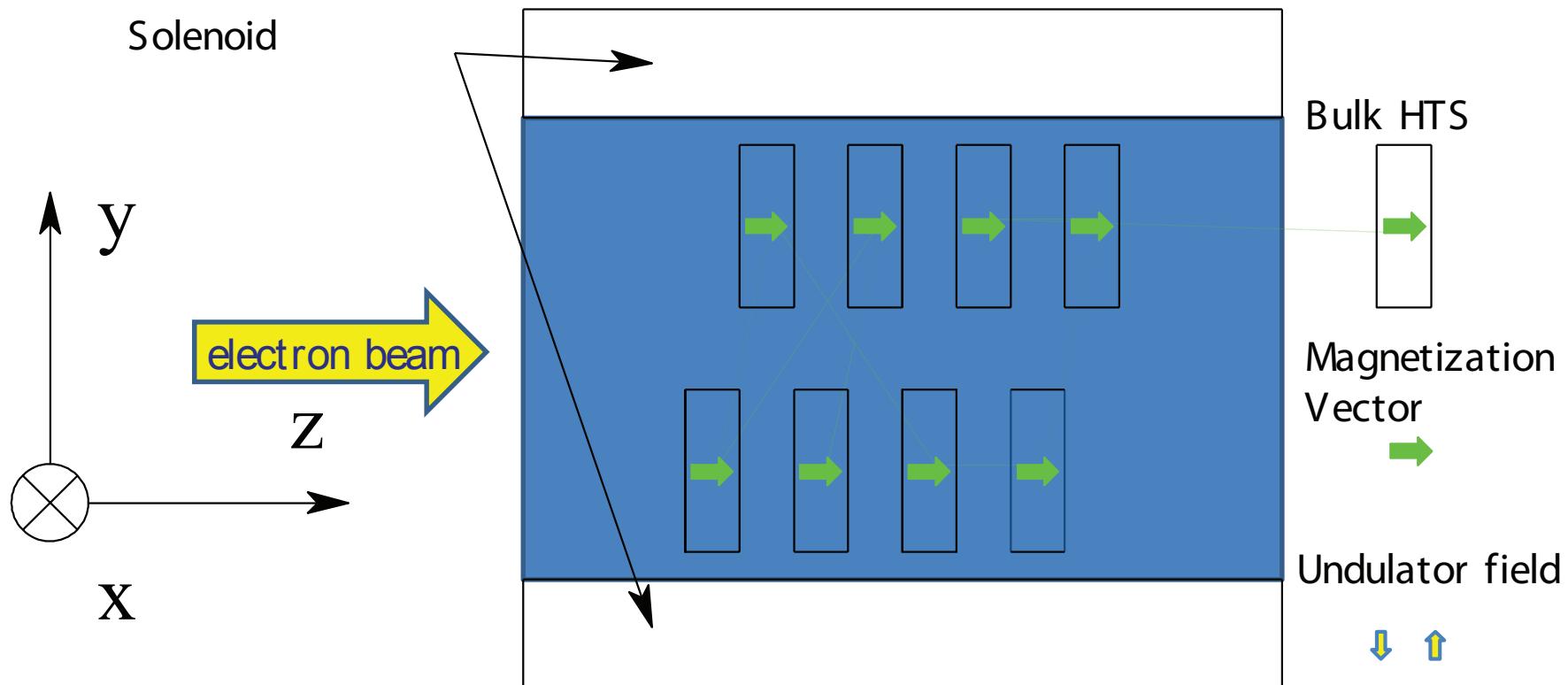


Magnetic field is changed. : $B_{\text{start}} \rightarrow B_{\text{end}}$

Undulator field is generated by superposition of magnetic field

Principle of Operation bulk HTS SAU (1)

Side view of “Bulk HTSC SAU”

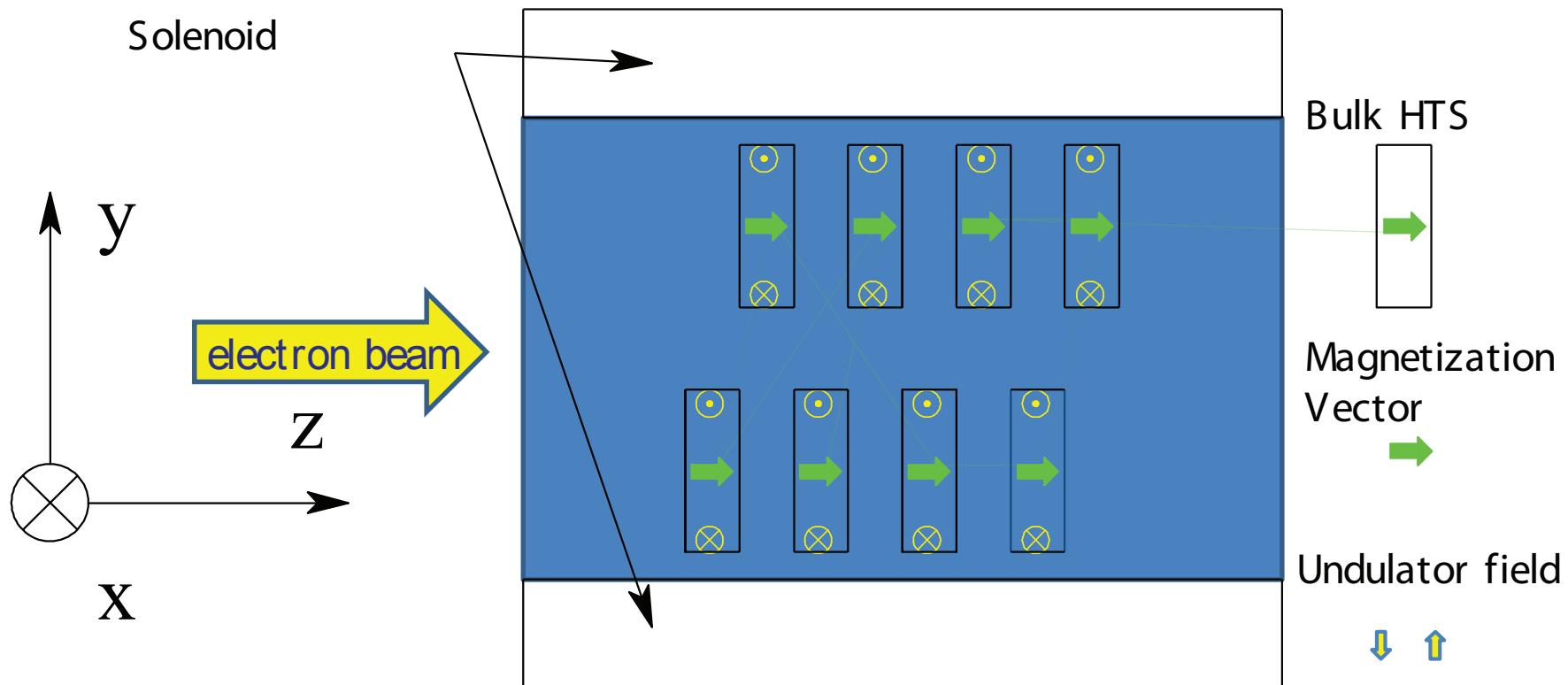


Magnetic field is changed. : $B_{\text{start}} \rightarrow B_{\text{end}}$

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Principle of Operation bulk HTS SAU (1)

Side view of “Bulk HTSC SAU”

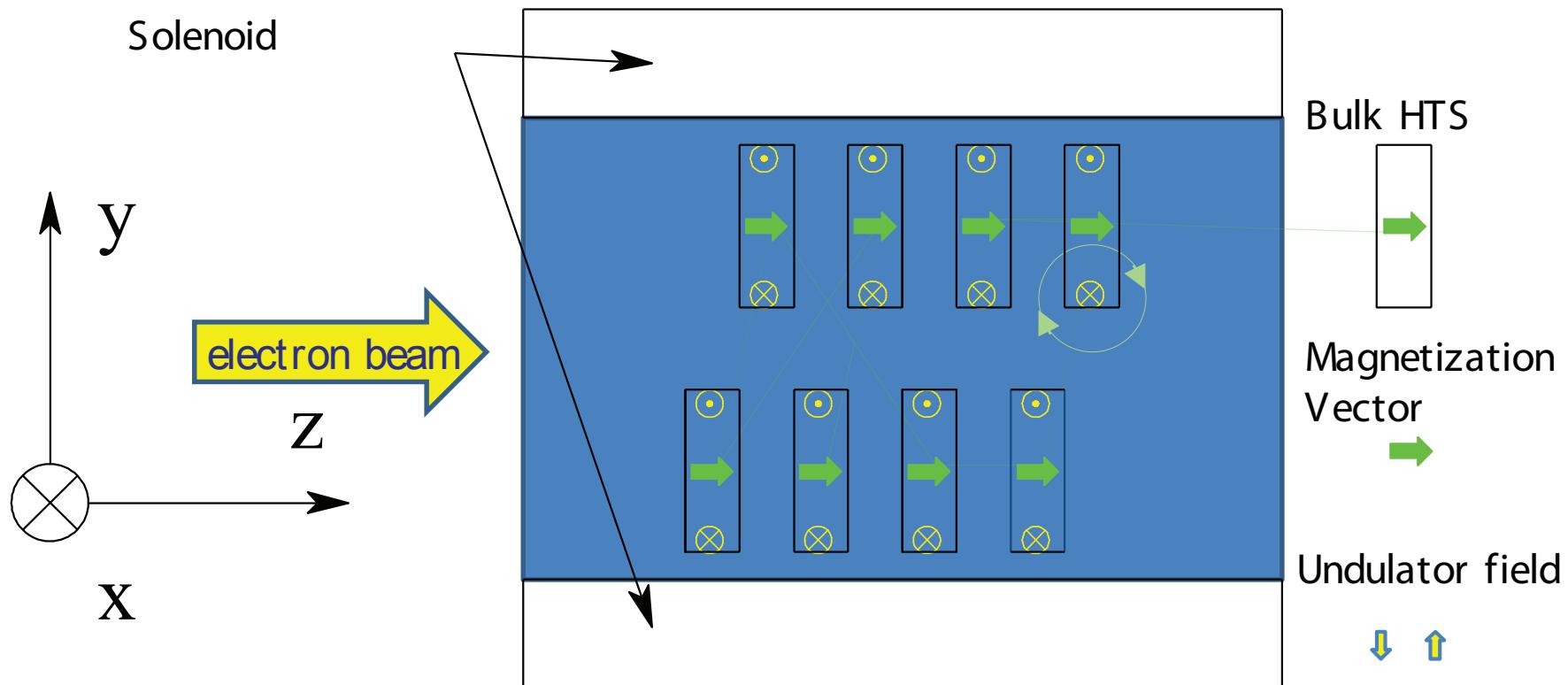


Magnetic field is changed. : $B_{\text{start}} \rightarrow B_{\text{end}}$

Undulator field is generated by superposition of magnetic field

Principle of Operation bulk HTS SAU (1)

Side view of “Bulk HTSC SAU”

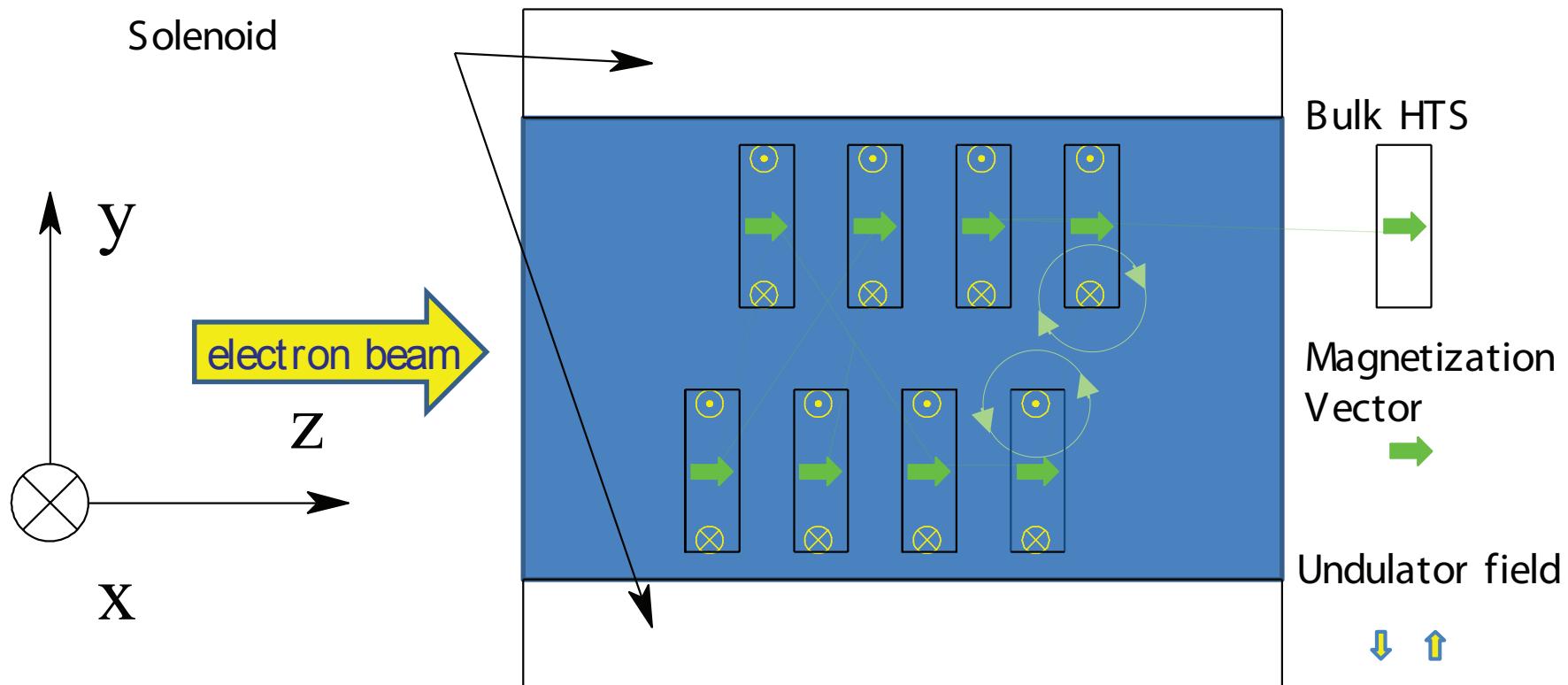


Magnetic field is changed. : $B_{\text{start}} \rightarrow B_{\text{end}}$

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Principle of Operation bulk HTS SAU (1)

Side view of “Bulk HTSC SAU”

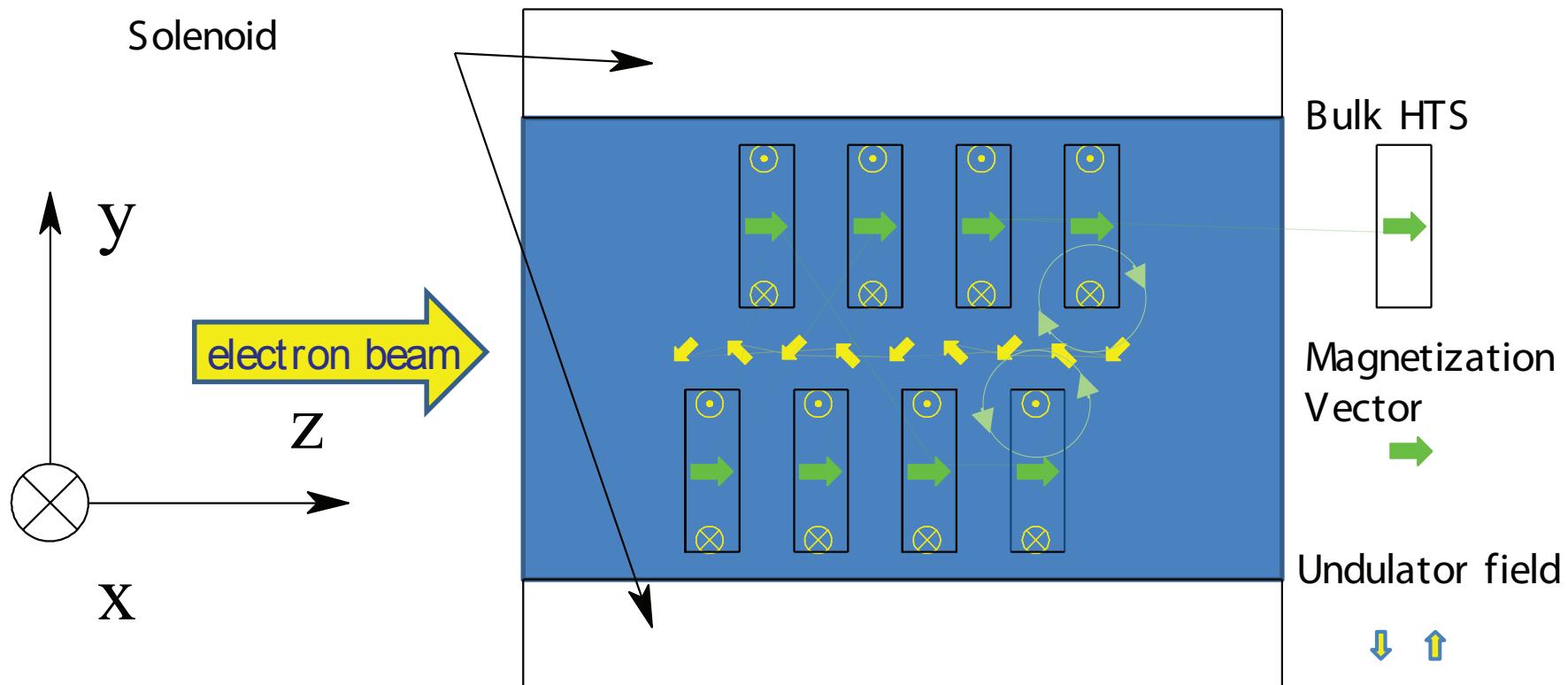


Magnetic field is changed. : $B_{\text{start}} \rightarrow B_{\text{end}}$

Undulator field is generated by superposition of magnetic field

Principle of Operation bulk HTS SAU (1)

Side view of “Bulk HTSC SAU”



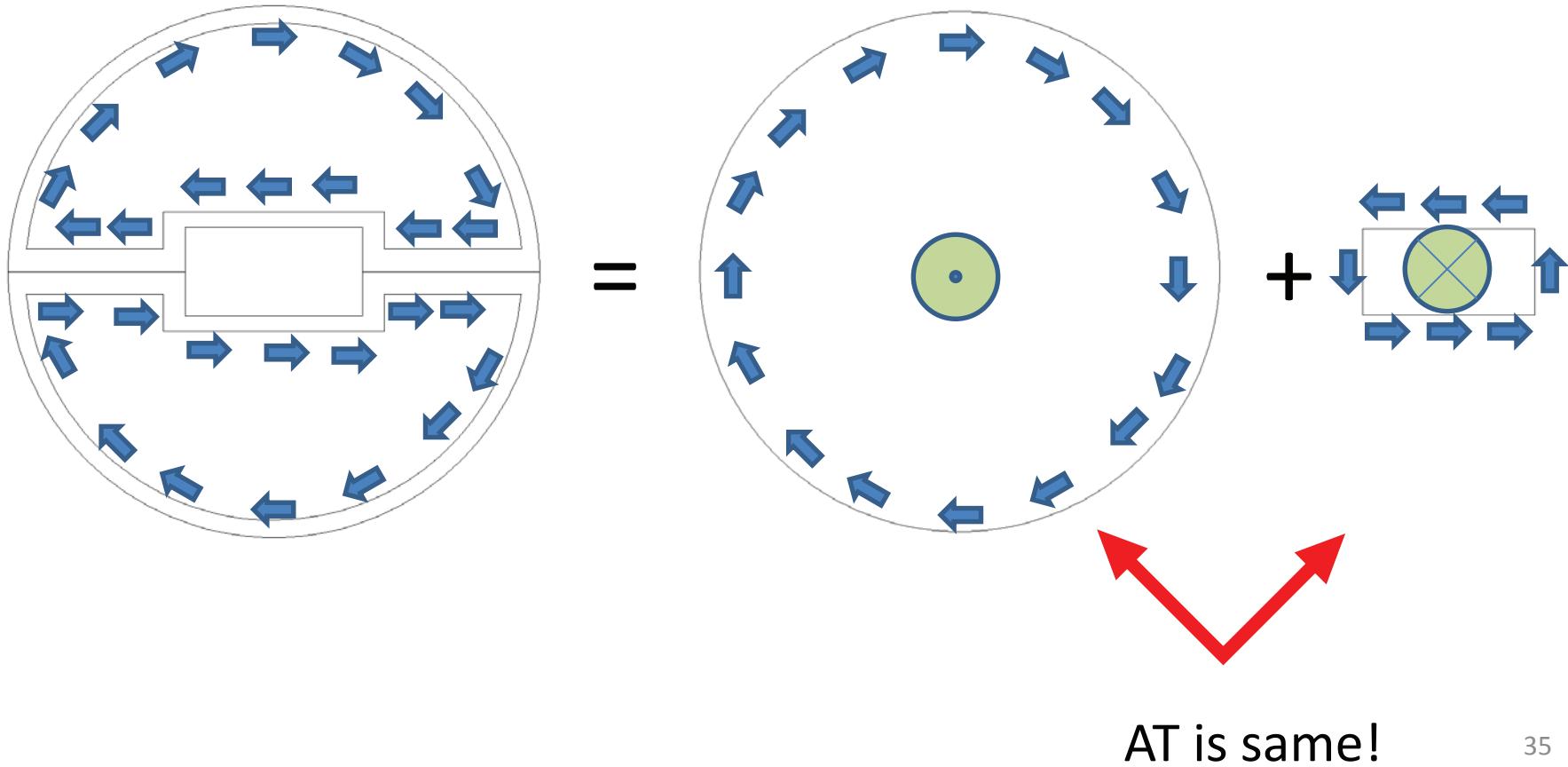
Magnetic field is changed. : $B_{\text{start}} \rightarrow B_{\text{end}}$

Undulator field is generated by superposition of magnetic field

Principle of Operation bulk HTS SAU (2)

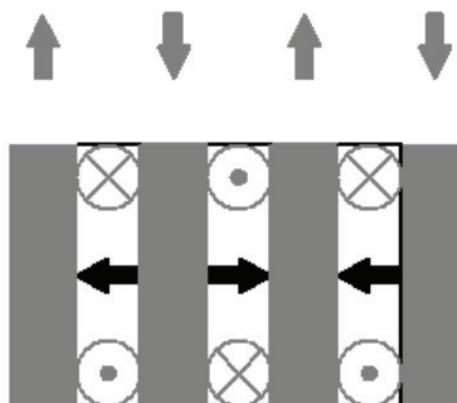
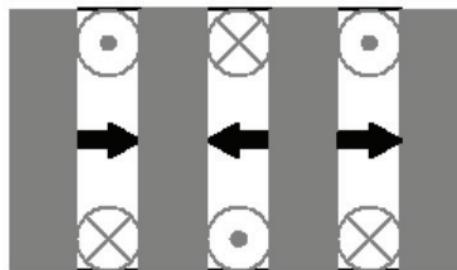
Axial field component: $B_z \approx 0$

If undulator total length is long enough.

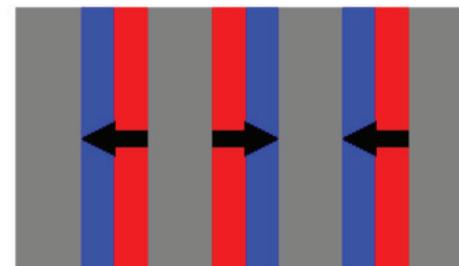
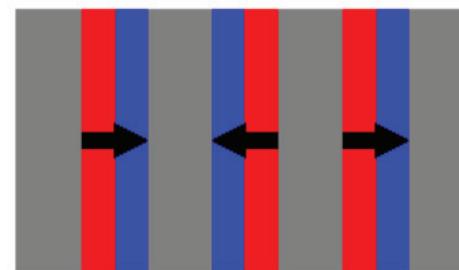


Analog to

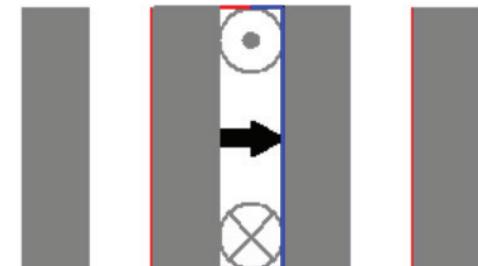
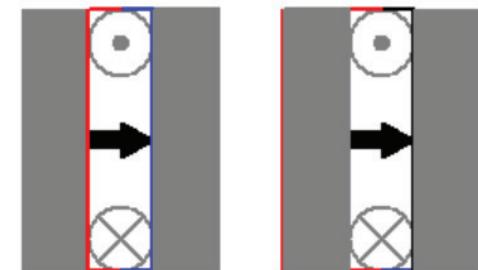
Wire SC
Hybrid Und.



Hybrid Und.



Bulk SC SAU



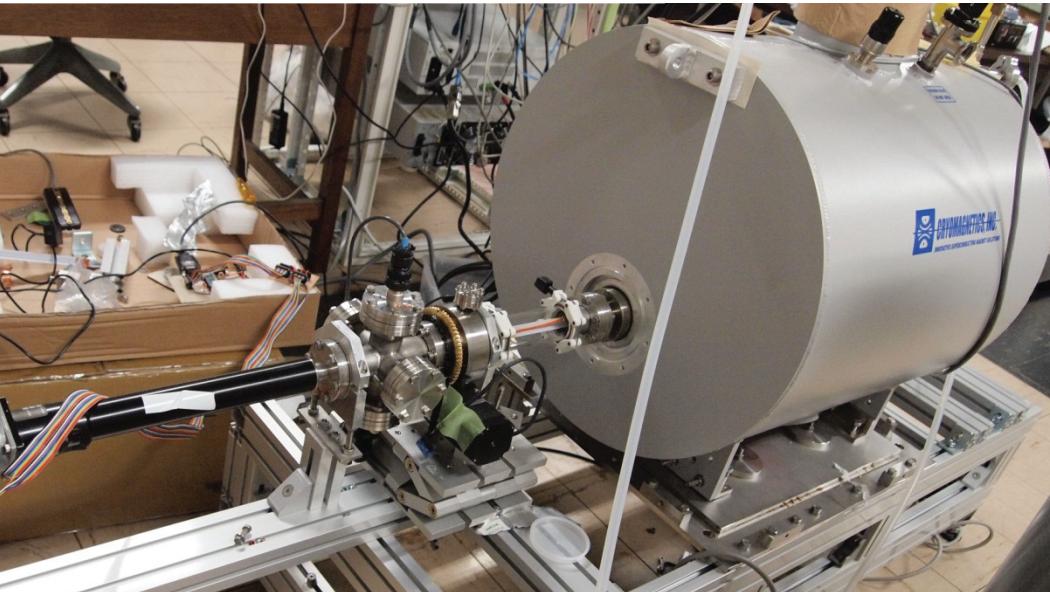
Advantage of the Bulk HTS SAU

- (1) Bulk HTS can be magnetized **using single solenoid**.
- (2) 10 K operation is enough. : **Easy cooling**.
- (3) No mechanical component.
- (4) Cold mass is very small.
 - (All the cooled component is placed in $\phi = 75$ mm RT bore)
- (5) Bulk HTS can be effectively **cooled by copper insulator**.
- (6) **Magnet sorting technique** can be applicable.
- (7) Radiation irradiation improve J_c performance. (Benefit > Damage)
- (8) Fluctuation of the critical current density for each HTS is
automatically suppressed.
- (9) Local magnetic field property can be controlled
by using **machined bulk HTS / ferromagnetic plate**.

Challenging issue of the Bulk HTS SAU

- (1) End field termination is not easy.

Prototype



He Cryostat
2 T SC solenoid

Period : 10 mm

Gap : 4 mm

Number of Period

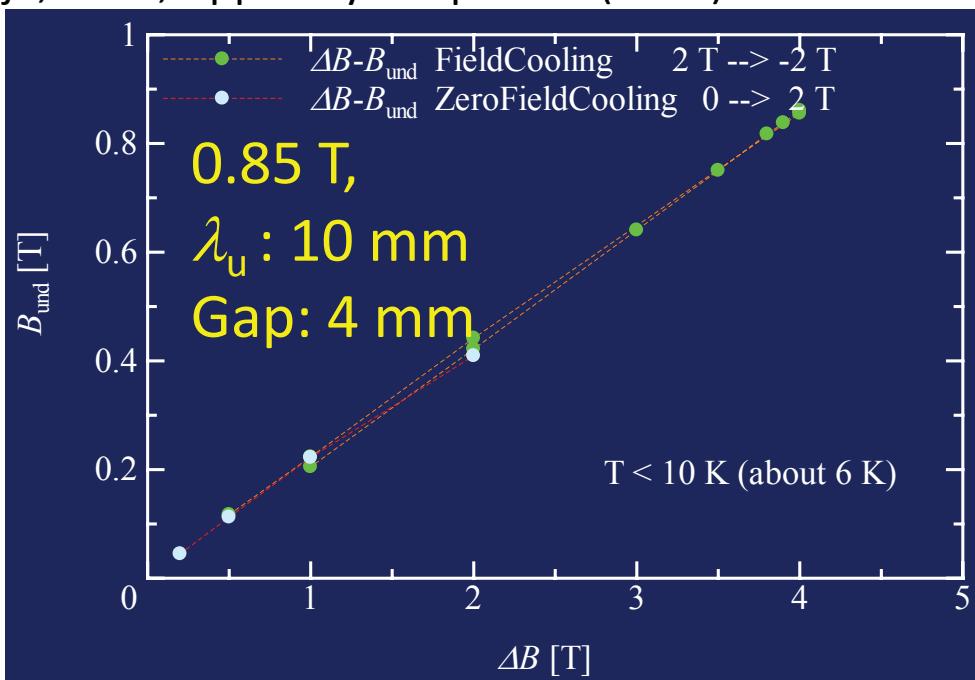
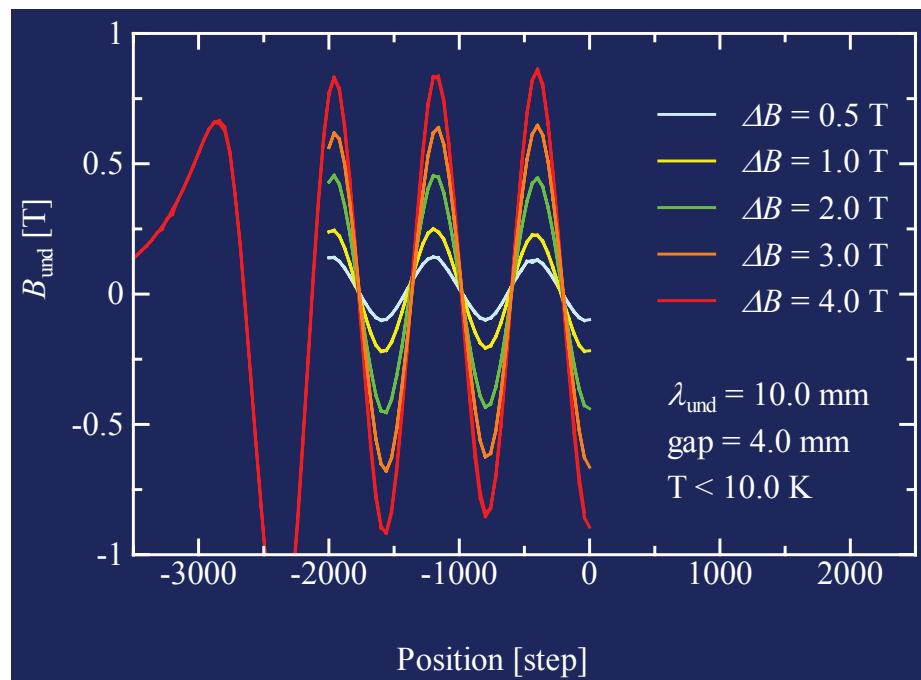
: 6

GdBaCuO Tc 91 K

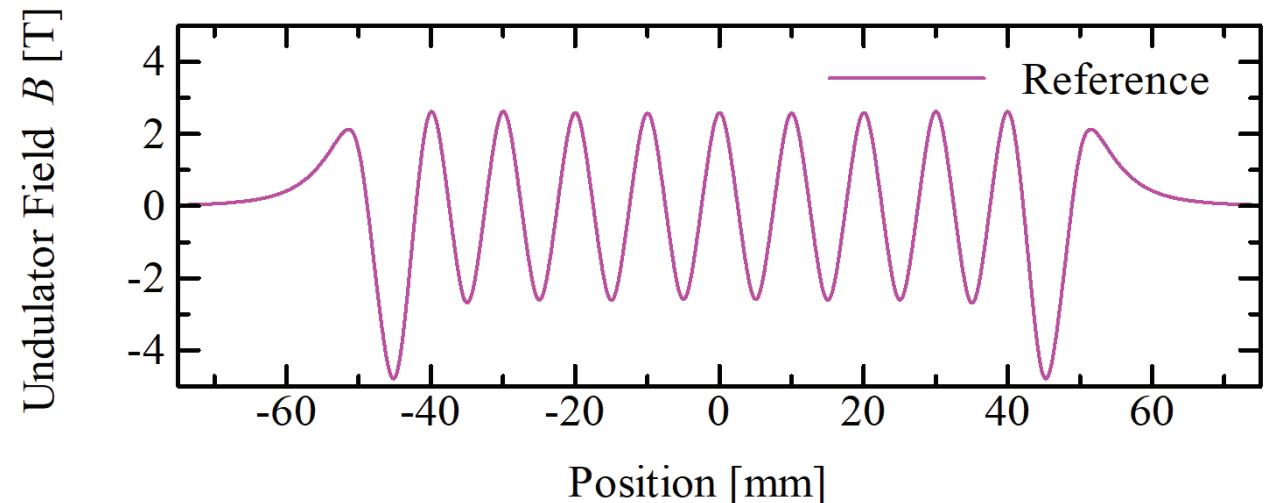


Experimental demonstration

R. Kinjo, et al., Appl. Phys. Express 6 (2013) 042701



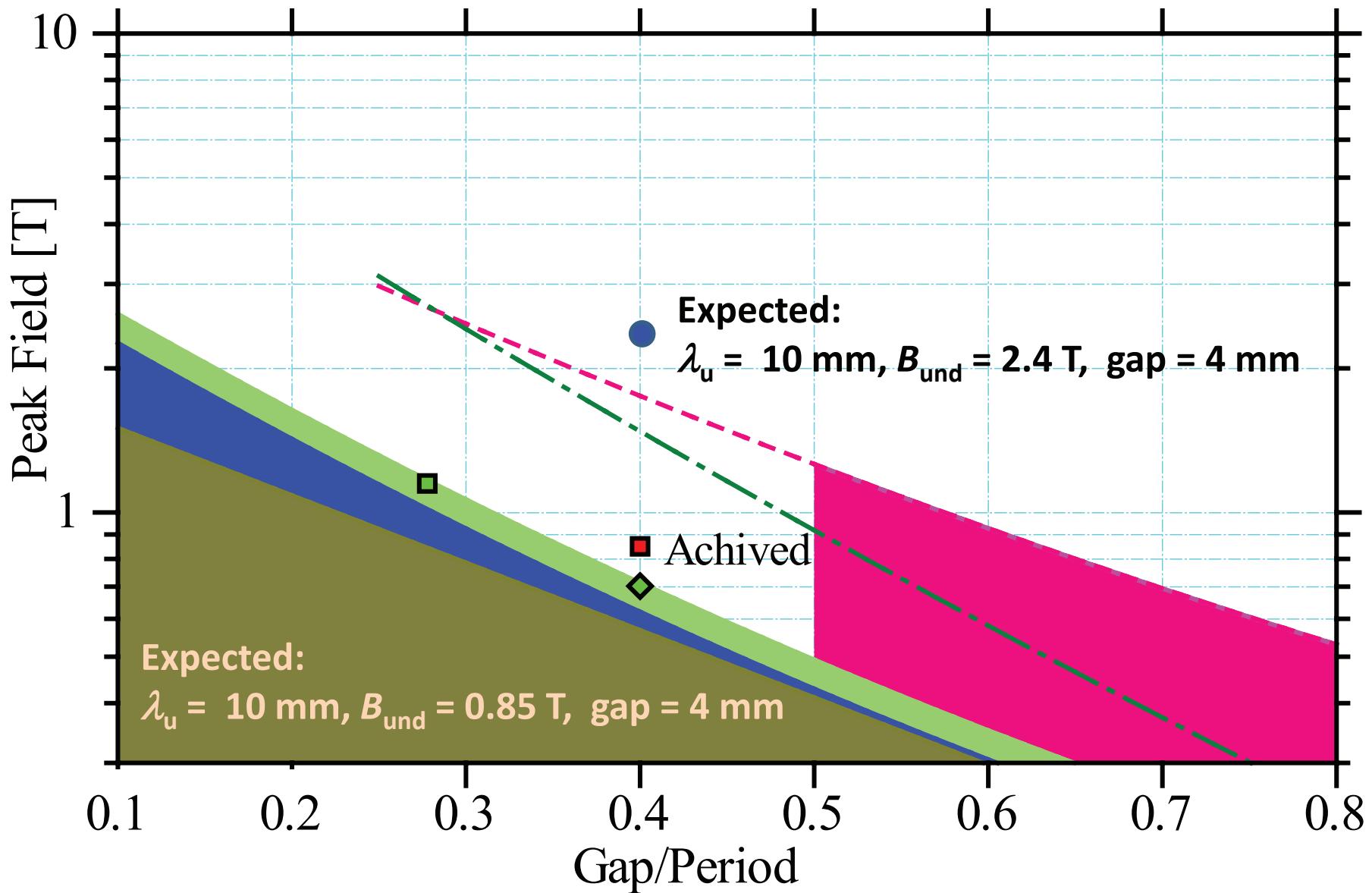
Numerical expectation



Parameters for the numerical expectation:

- $J_c = 18 \text{ kA/mm}^2$
- $\Delta B = 15 \text{ T}$
- $B_{\text{und}} = 2.4 \text{ T}$
- Period $\lambda_{\text{und}} = 10 \text{ mm}$
- Gap $g = 4.0 \text{ mm}$

Demonstrated and expected parameters

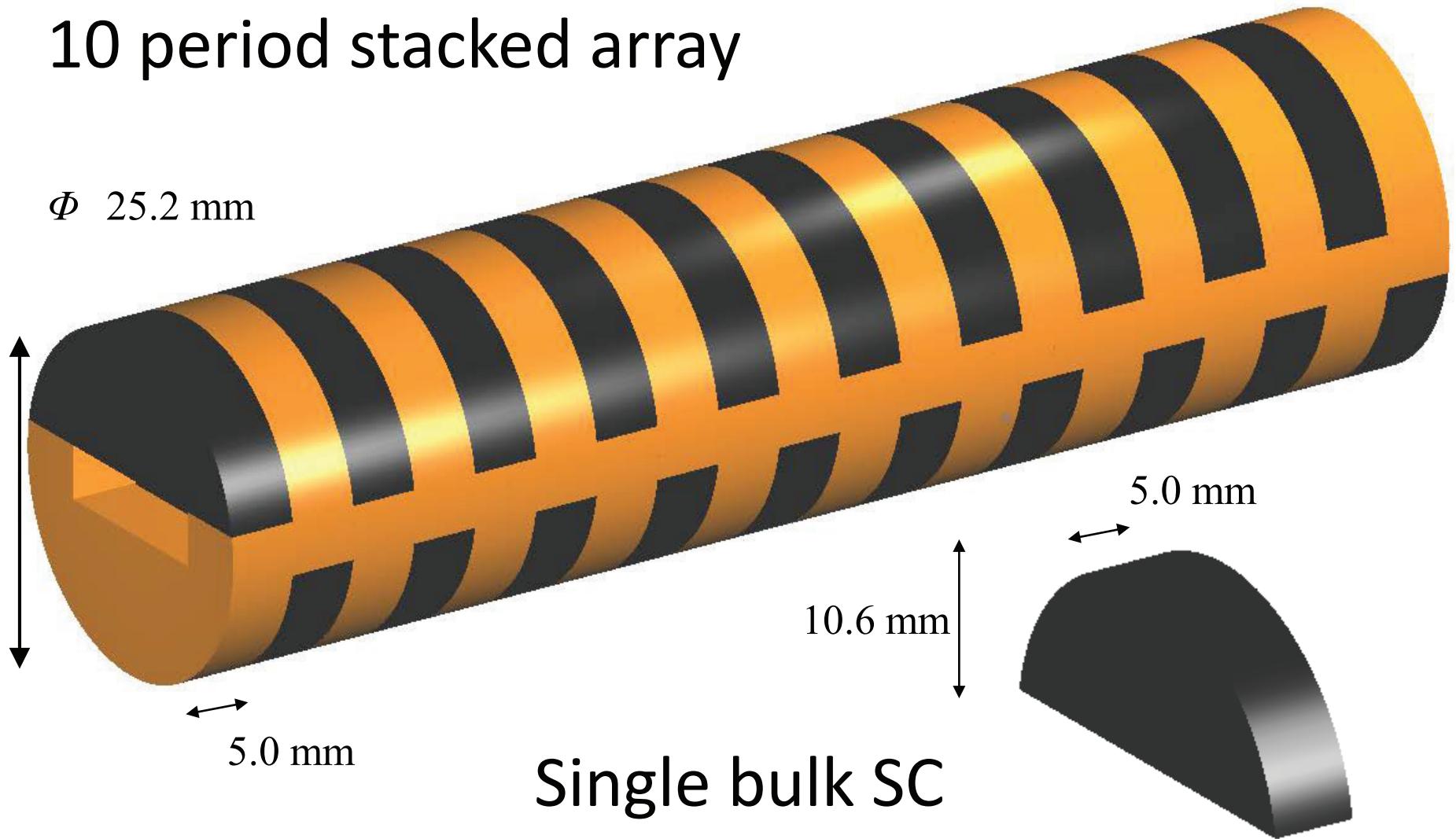


Status of development

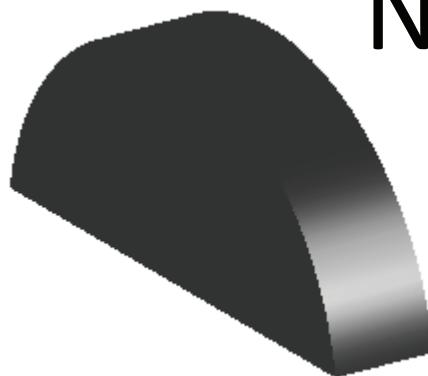
1. Method to reduce field error.
 2. Numerical model for Fast simulation.
 3. Method for End Field Termination.
 4. Next prototype.
-
1. Bulk sorting + Precise machining + Shim film
 2. Loop current modeling
 3. Additional bulks to the end part
 4. 6 T solenoid + HTS array

Numerical Model (1)

10 period stacked array

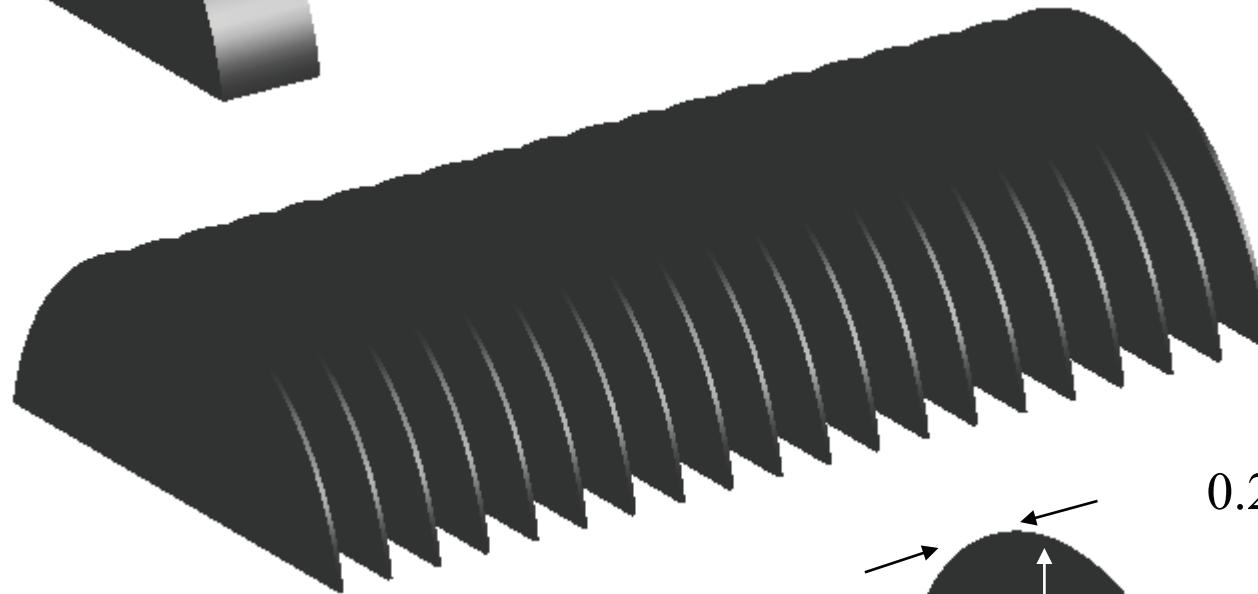


5.0 mm

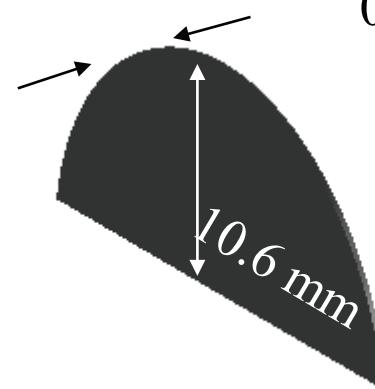


Numerical Model (2)

Single bulk SC



0.25 mm



Sliced into 20 layer

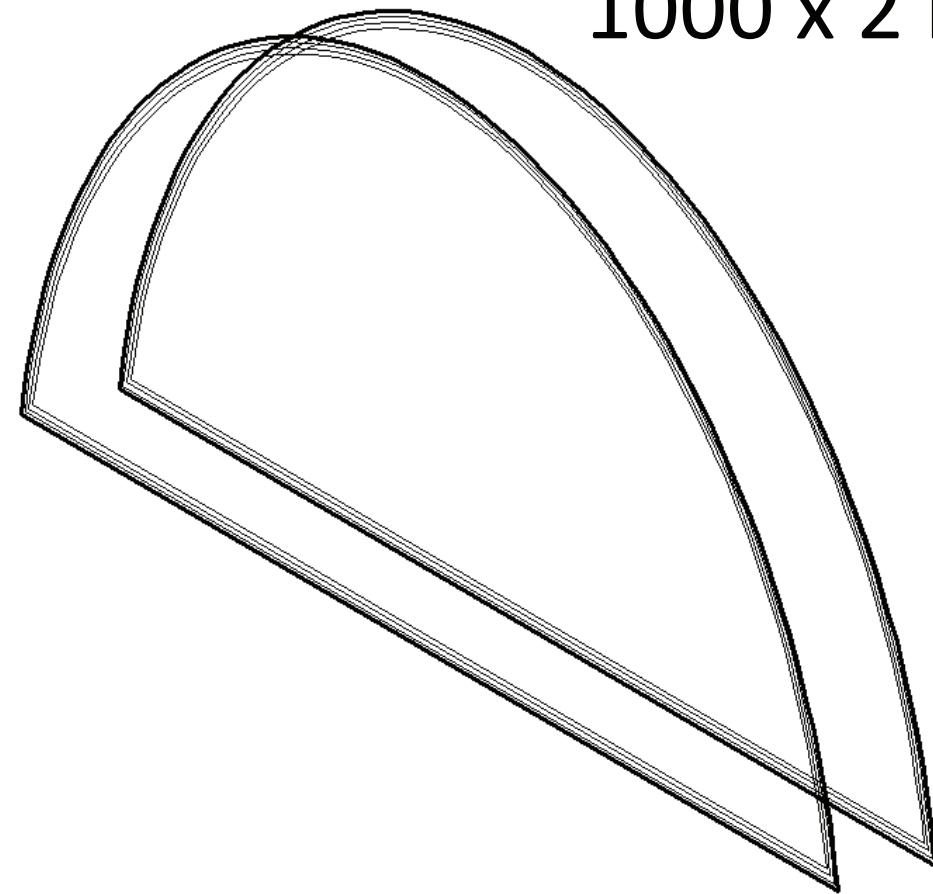
0.6 mm

Numerical Model (3)

Single layer

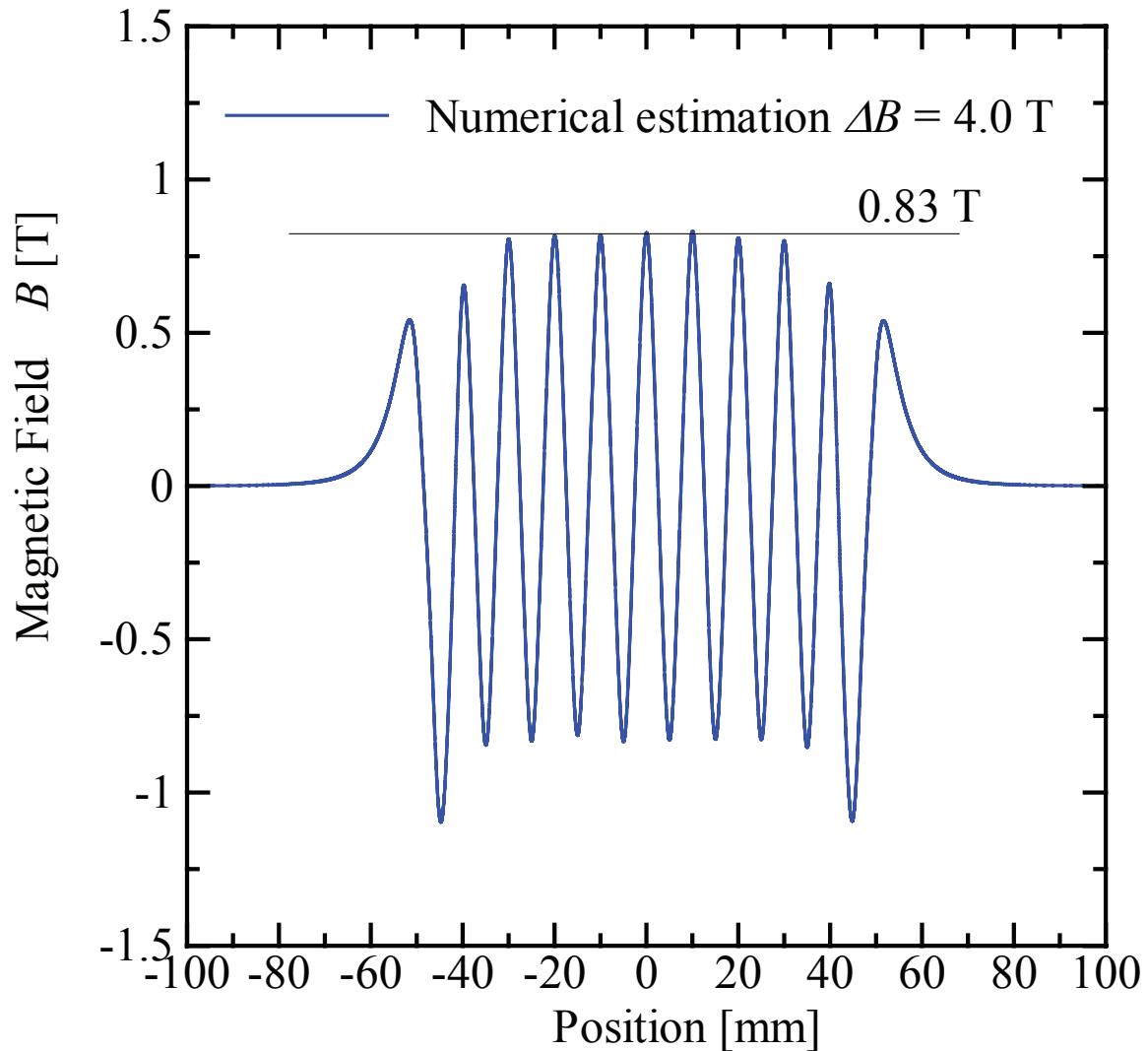


1000 x 2 loops



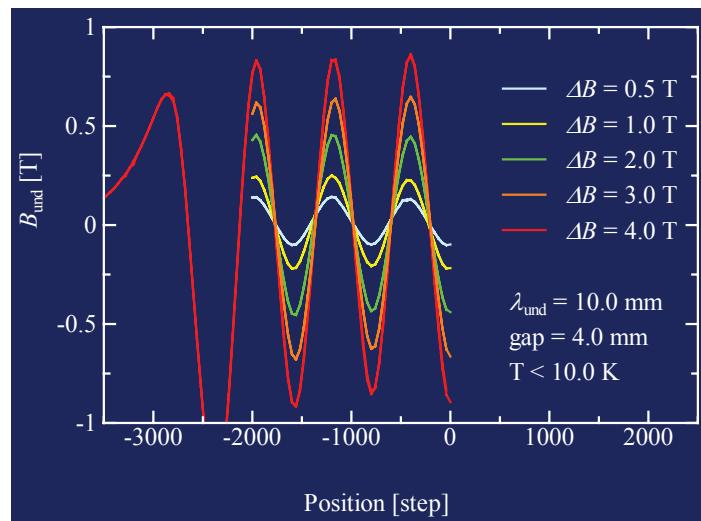
$1000 \times 2 \times 20 \times 20 = 800,000$ loops

Numerical Results (1)



Undulator field amplitude
is well reproduced.

EXP. 0.85 T
Calc. 0.83 T

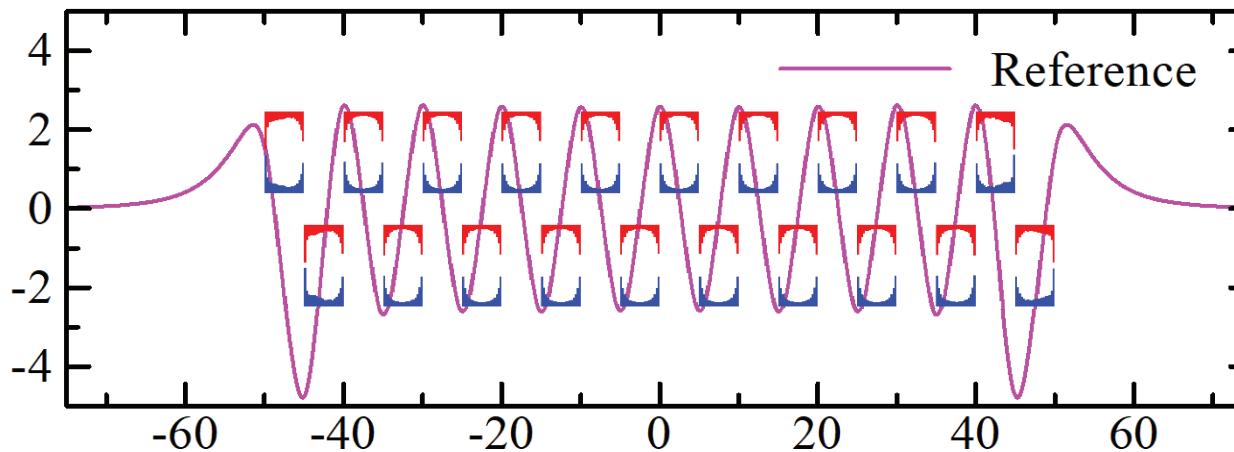


Numerical Results (2)

$$J_c = 18 \text{ kA/mm}^2$$

$$\Delta B = 15 \text{ T}$$

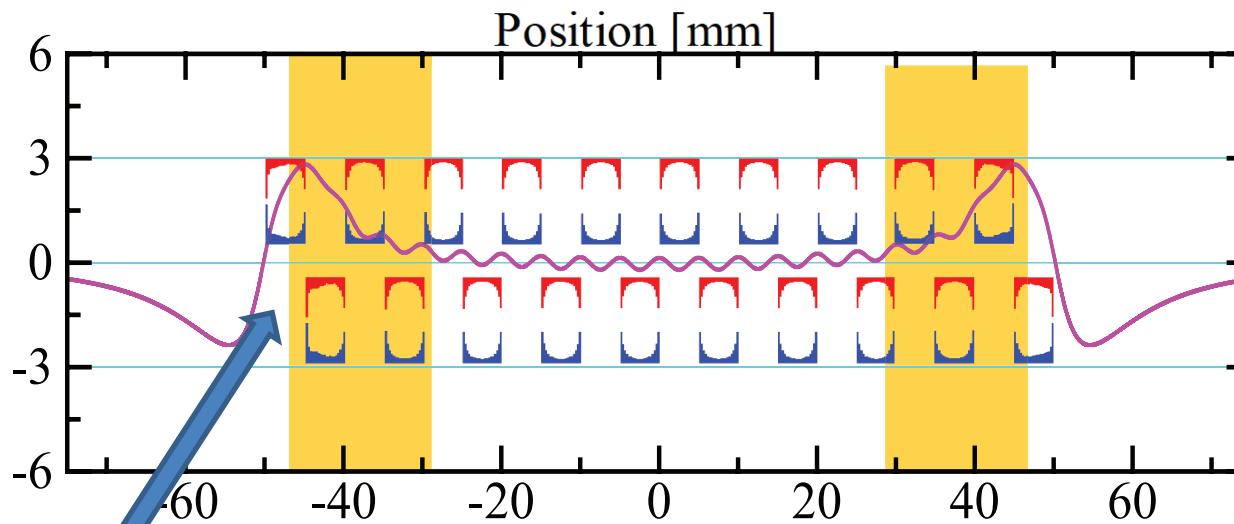
Undulator Field B [T]



$$B_{\text{und}}$$

$$= 2.4 \text{ T}$$

Axial Field B [T]



$$\lambda_{\text{und}}$$

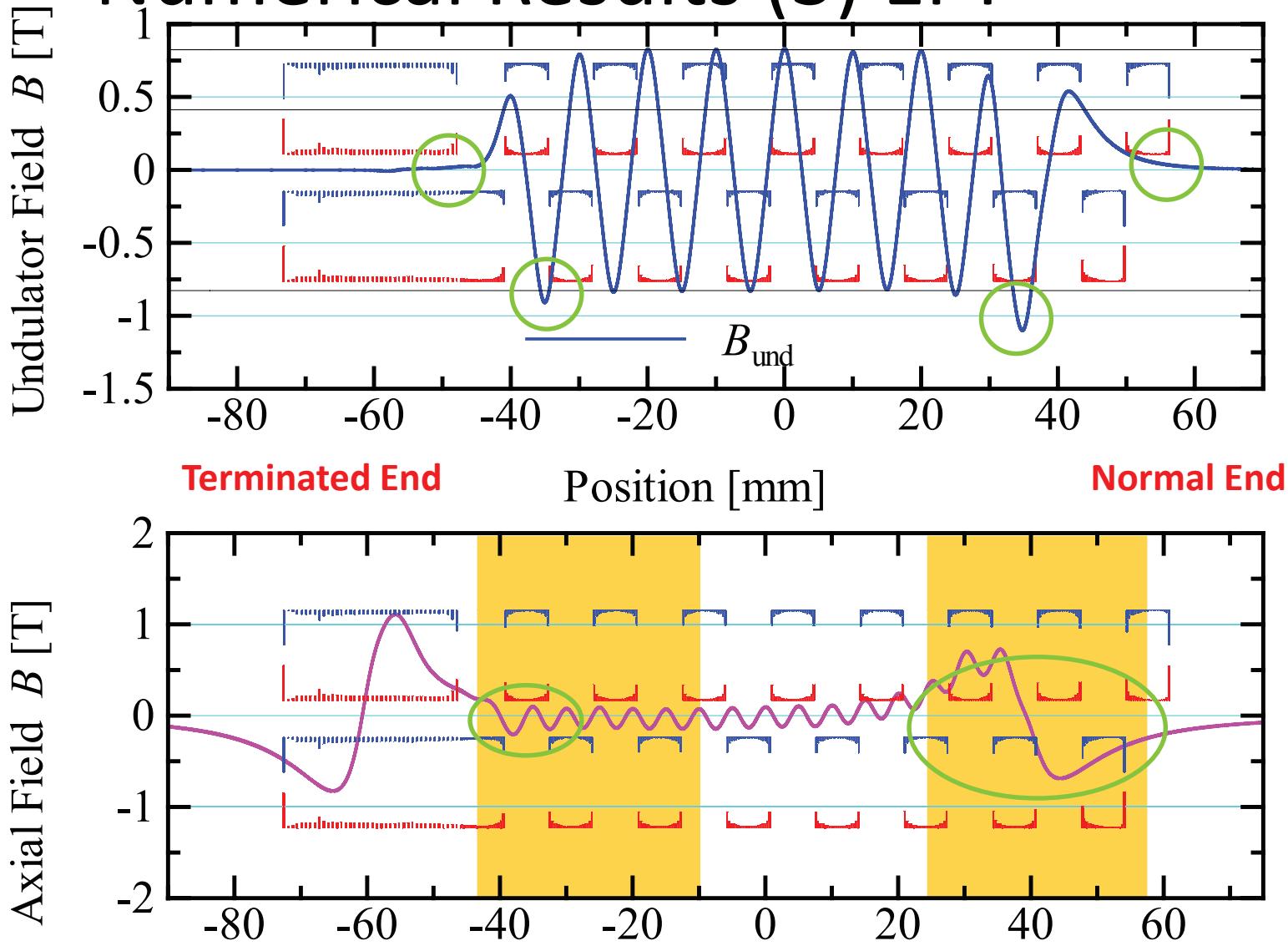
$$= 10 \text{ mm}$$

$$\text{Gap } g = 4.0 \text{ mm}$$



B_z remains at the end part.

Numerical Results (3) EFT



End part is well terminated.
 B_z is reduced at the end part.

Contents

1. Introduction

~ Limitation of Present Undulators ~

2. Bulk HTS

~ Potential of bulk HTS, How to make periodic field ~

3. Bulk HTS SAU

~ Principle of Operation, Experimental results, Numerical model ~

4. Conclusion

Conclusion

Potential of Bulk HTS:

Higher J_c 10 kA/mm² is possible at 10 K.

Bulk SC Array can be used as undulator.

Bulk SC SAU is under development.

Conclusion

Potential of Bulk HTS:

Higher J_c 10 kA/mm² is possible at 10 K.

Bulk SC Array can be used as undulator.

Bulk SC SAU is under development.

Possible configuration: $\lambda_u = 10$ mm gap = 4 mm

400 MeV $B_{und} = 1.23$ T $K = 1.14$ $\lambda = 13.5$ nm

1 GeV $B_{und} = 2.00$ T $K = 1.86$ $E_x = 0.34$ keV

3 GeV $B_{und} = 1.00$ T $K = 0.93$ $E_x = 5.95$ keV

3 GeV $B_{und} = 1.23$ T $K = 1.14$ $E_x = 5.15$ keV

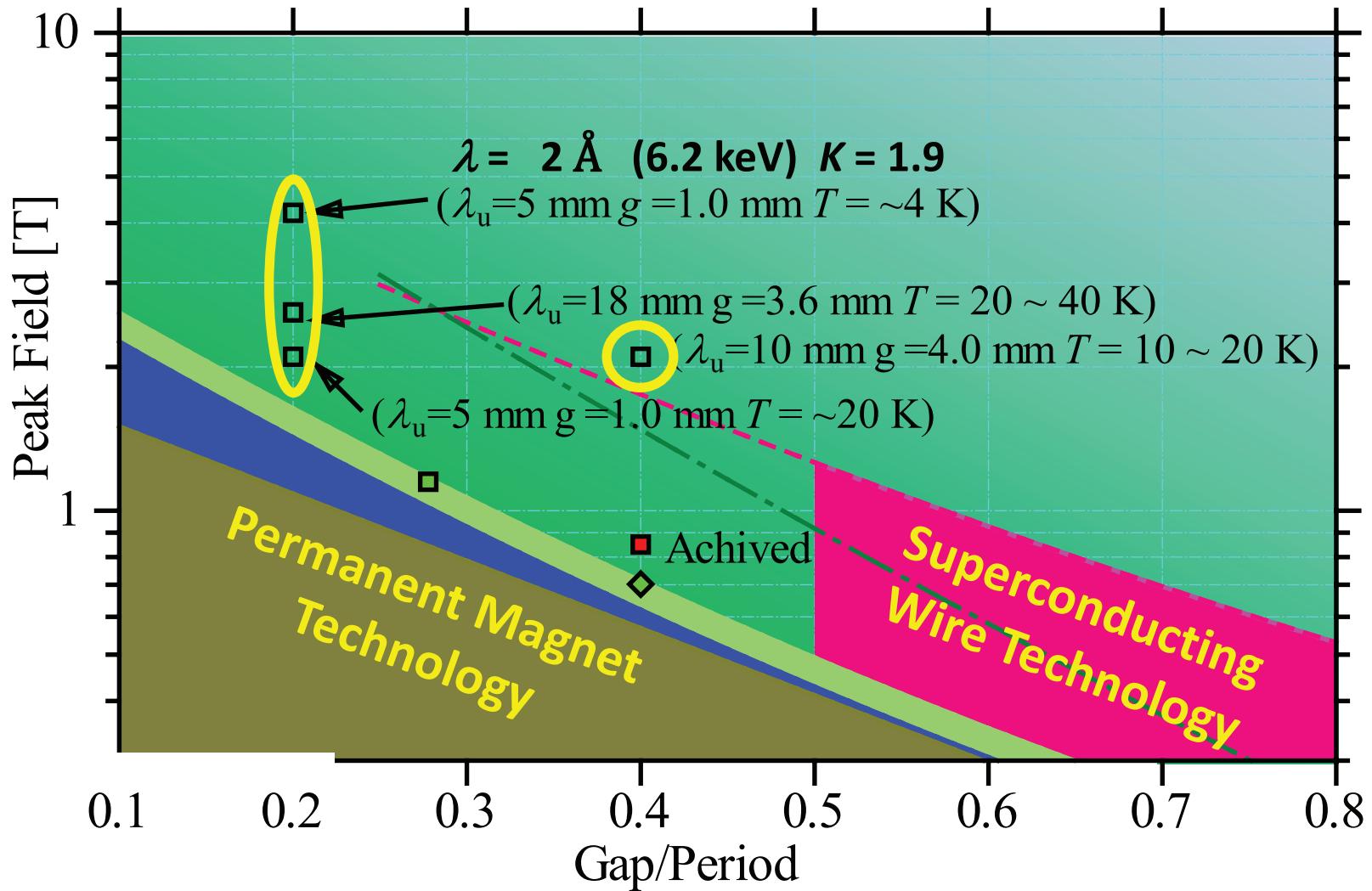
3 GeV $B_{und} = 2.40$ T $K = 2.24$ $E_x = 2.44$ keV

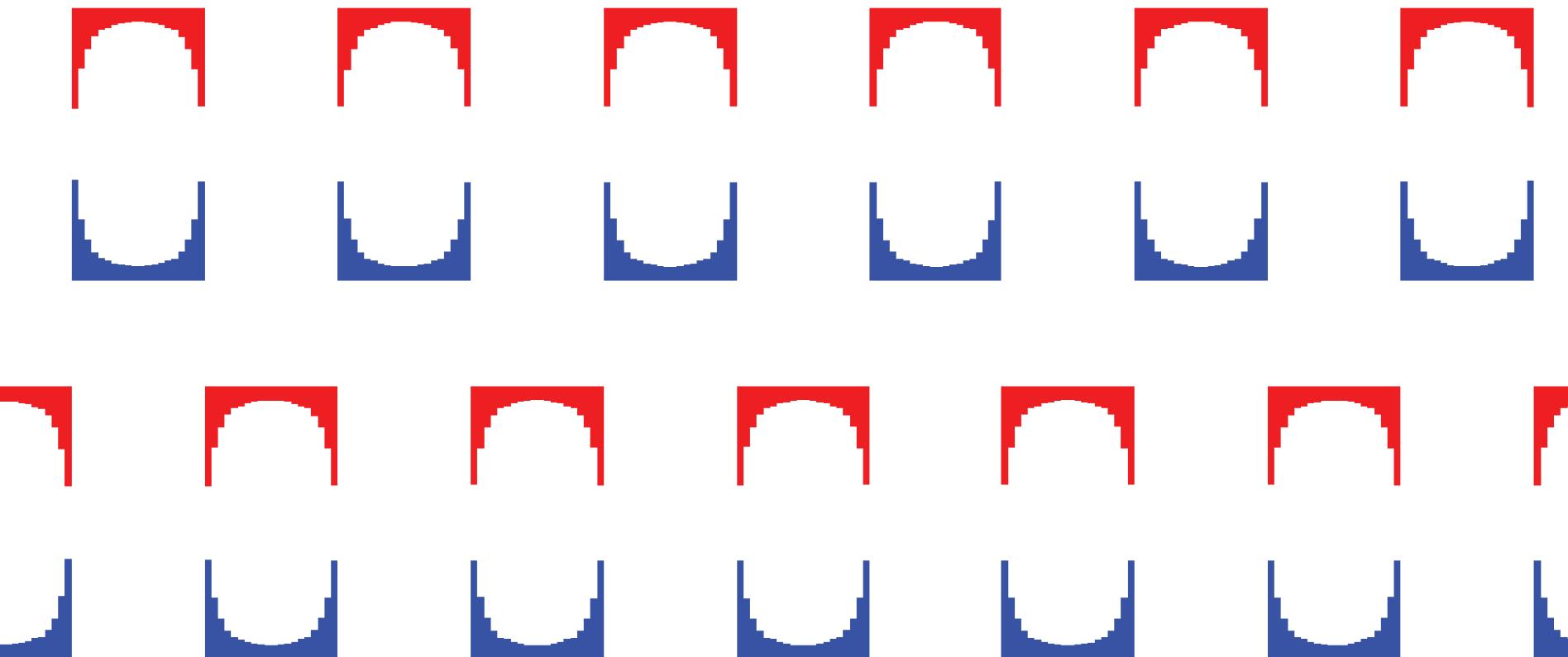
250 GeV $B_{und} = 1.00$ T $K = 0.93$ $E\gamma = 41.3$ MeV

250 GeV $B_{und} = 1.23$ T $K = 1.14$ $E\gamma = 25.8$ MeV

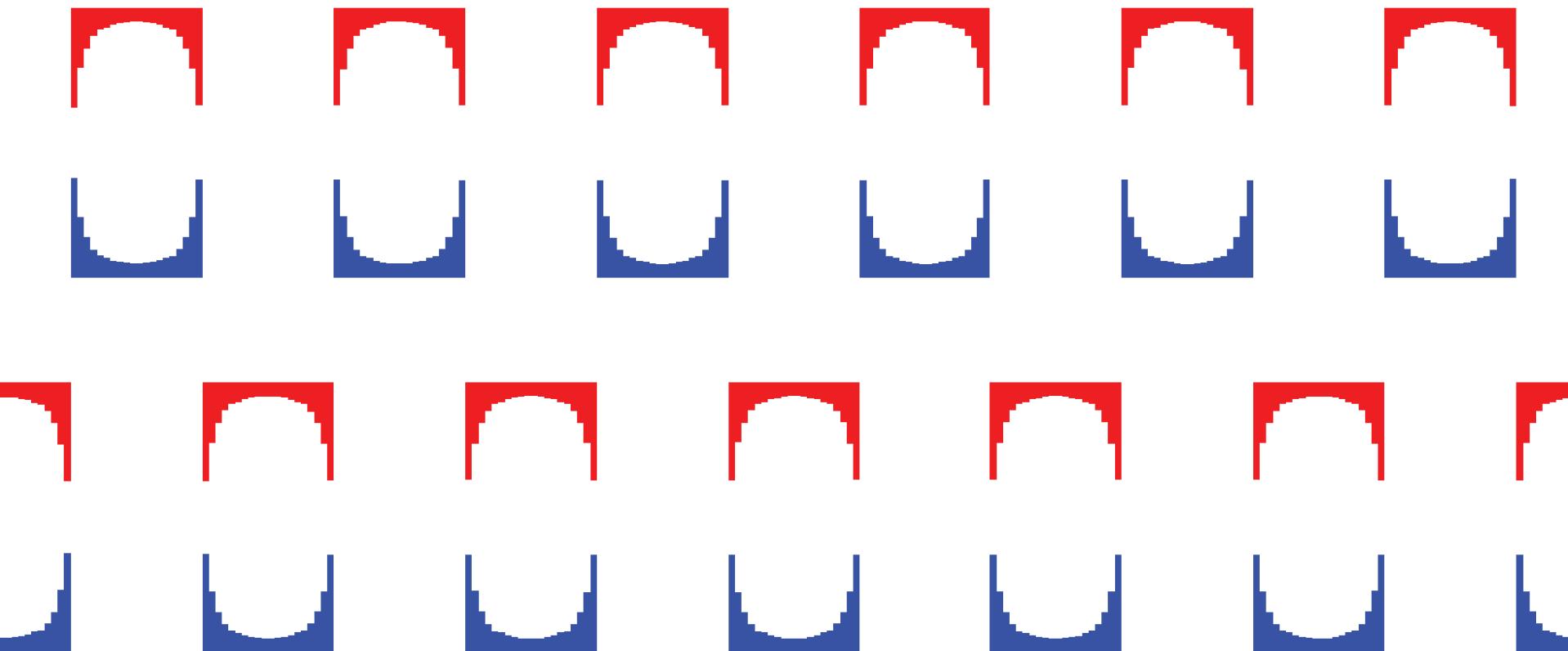
250 GeV $B_{und} = 2.40$ T $K = 2.24$ $E\gamma = 16.9$ MeV

Bulk SC may lead us to “fresh ground”

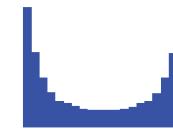
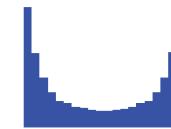




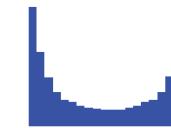
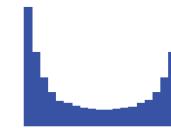
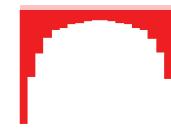
This work was supported by KAKENHI 17H01127



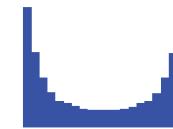
This work was supported by KAKENHI 17H01127



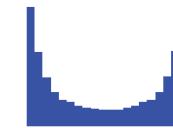
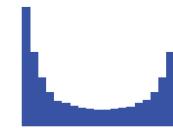
Thank you for your attention



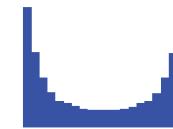
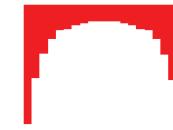
This work was supported by KAKENHI 17H01127



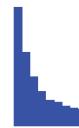
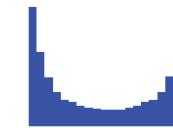
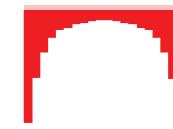
Thank you for your attention



This work was supported by KAKENHI 17H01127



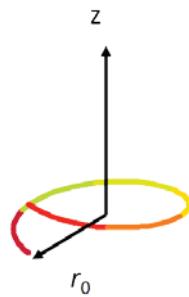
Thank you for your attention



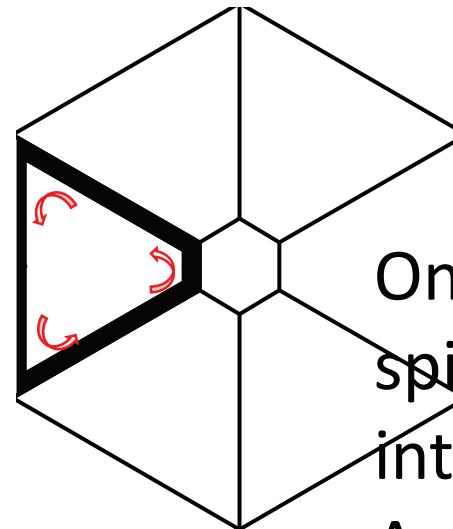
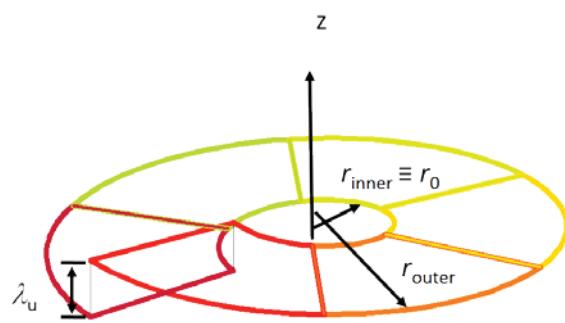
This work was supported by KAKENHI 17H01127

Design example for Helical SAU

a)

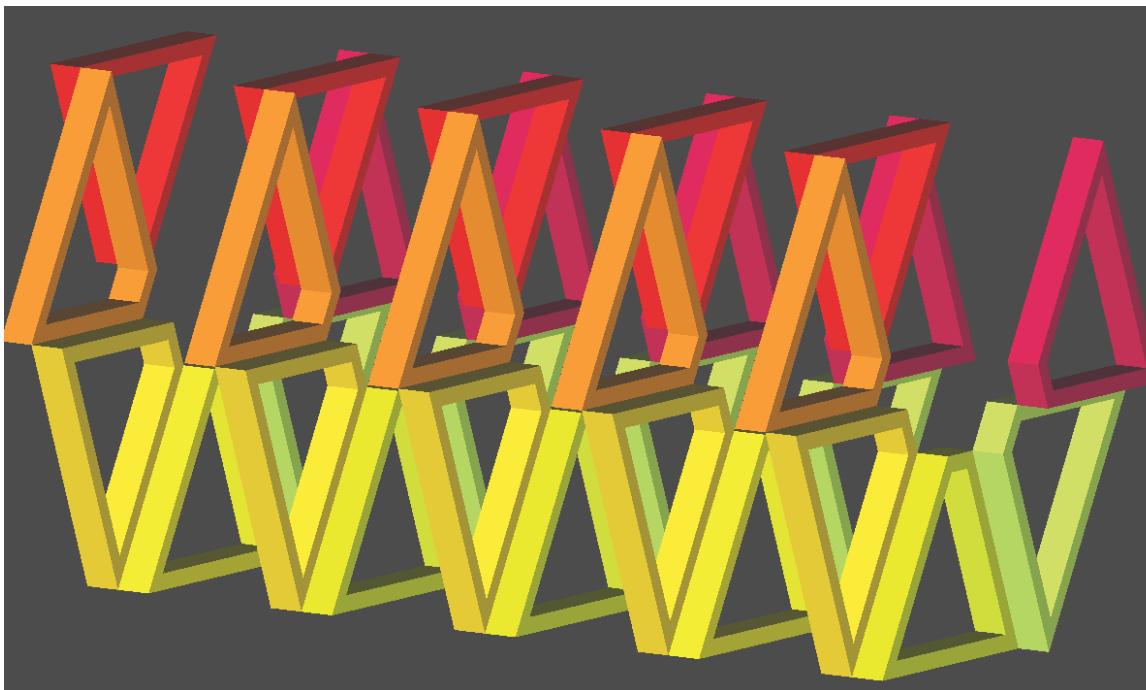


b)



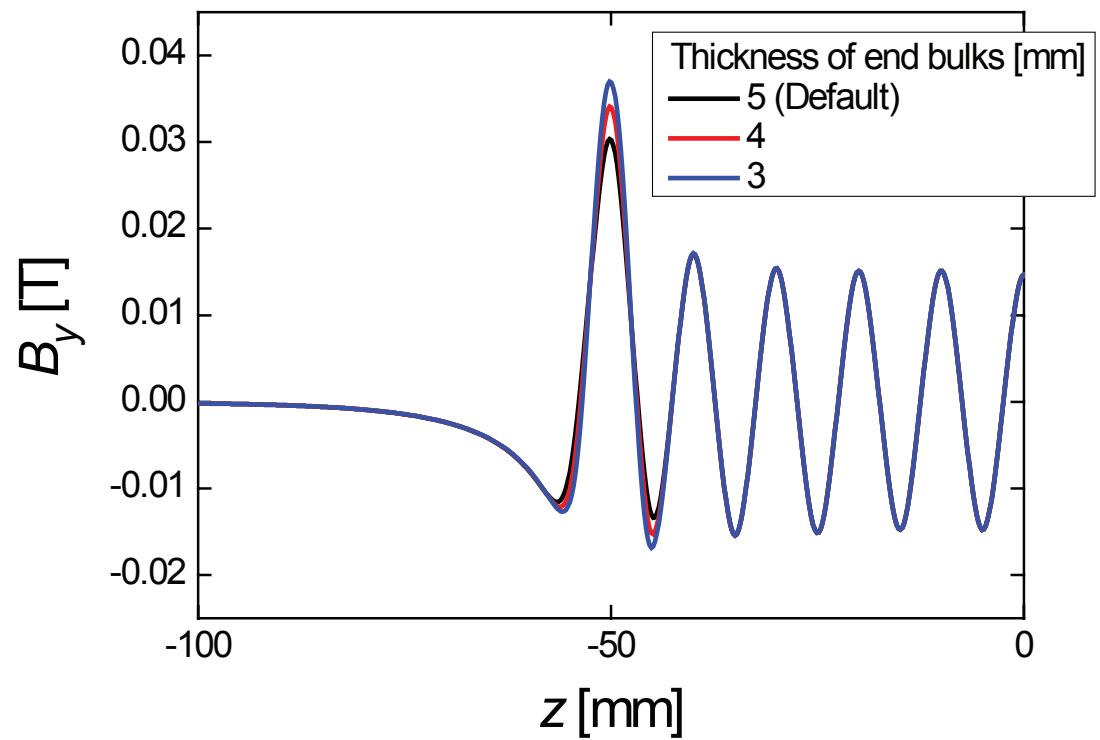
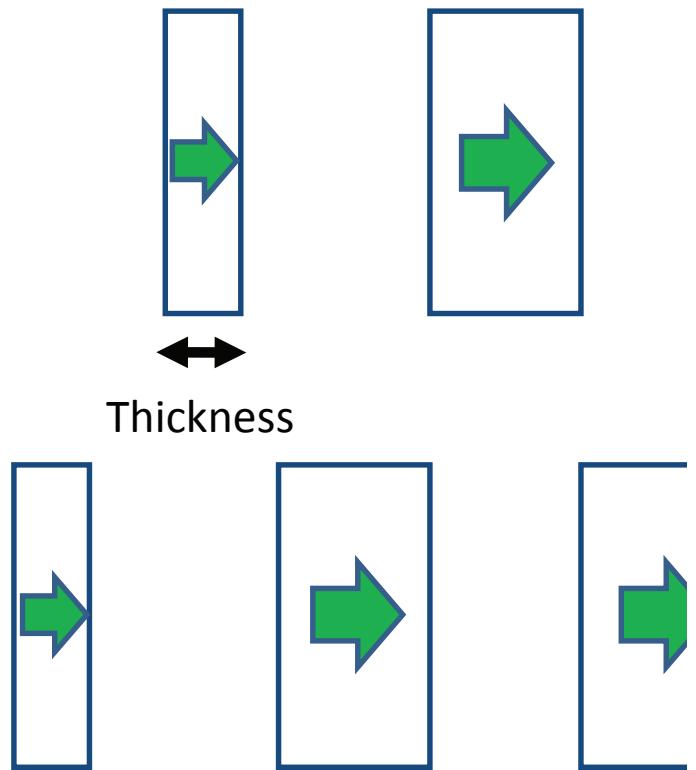
One period of spiral is divided into 6 bulk HTSs.

Arc lines are modified to straight lines.
Colored area represents supercurrent in each HTS



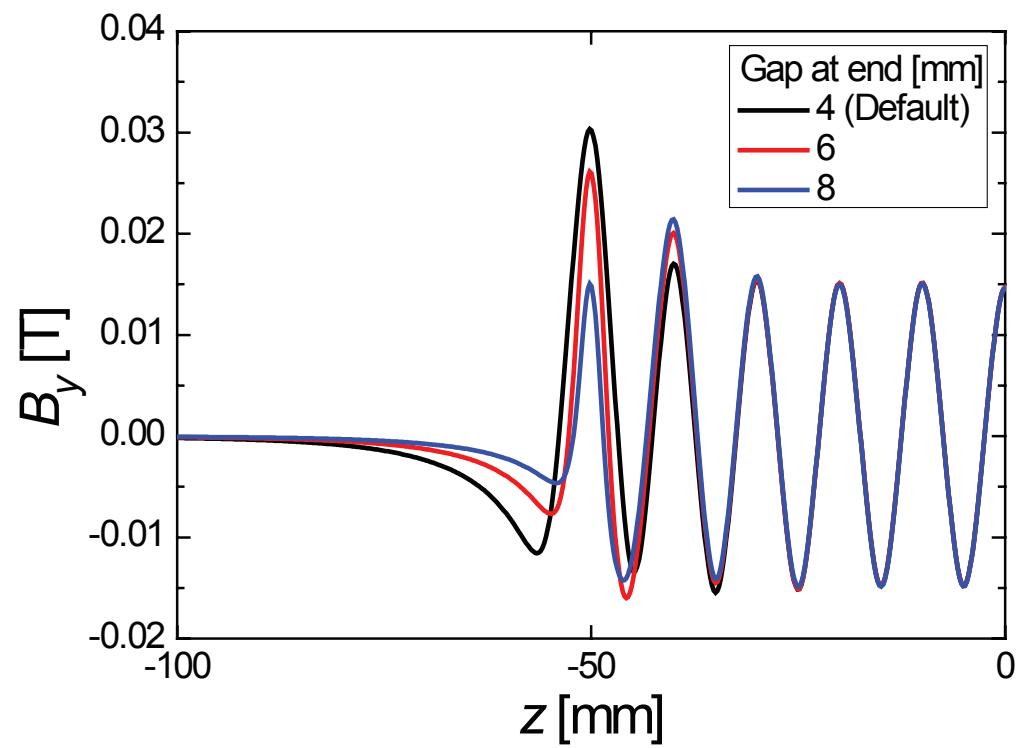
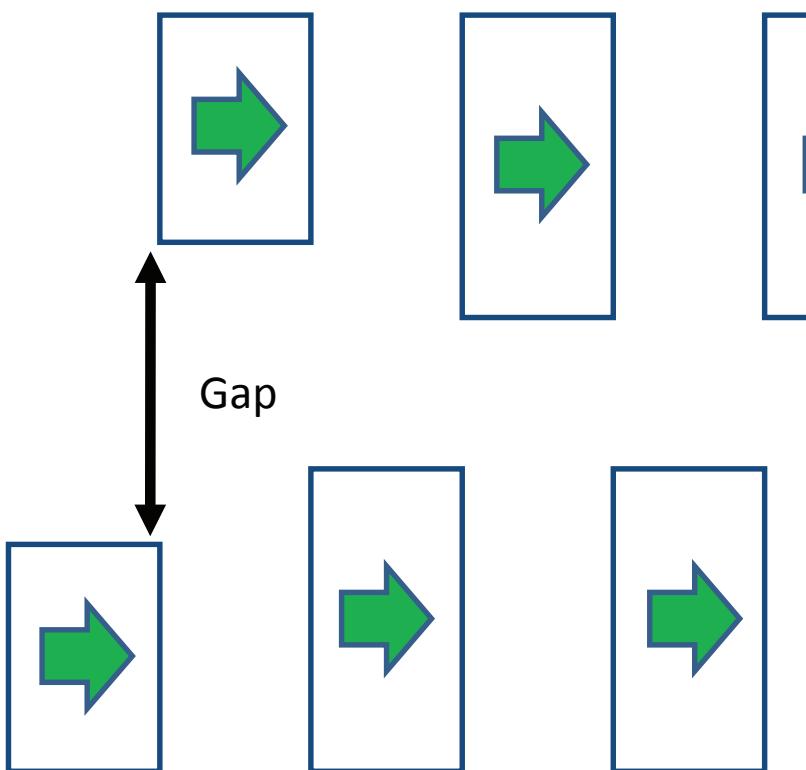
End field termination 1

Thin bulks are used at the end



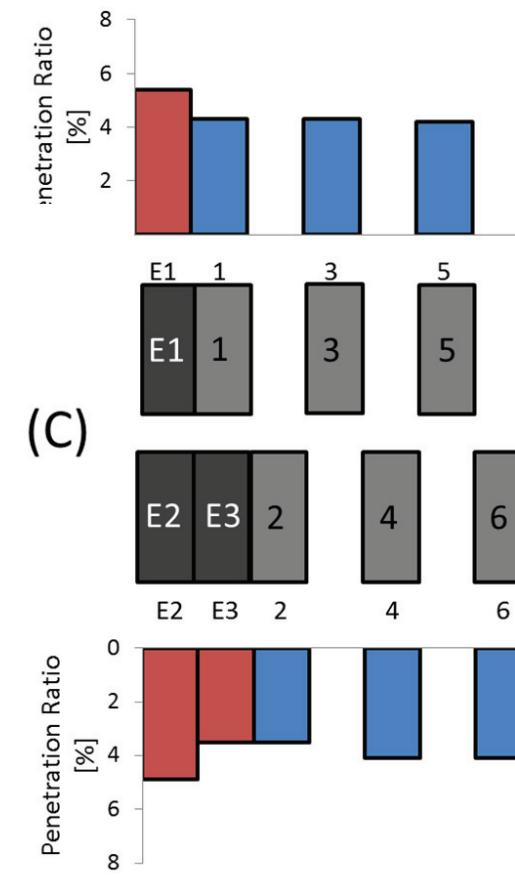
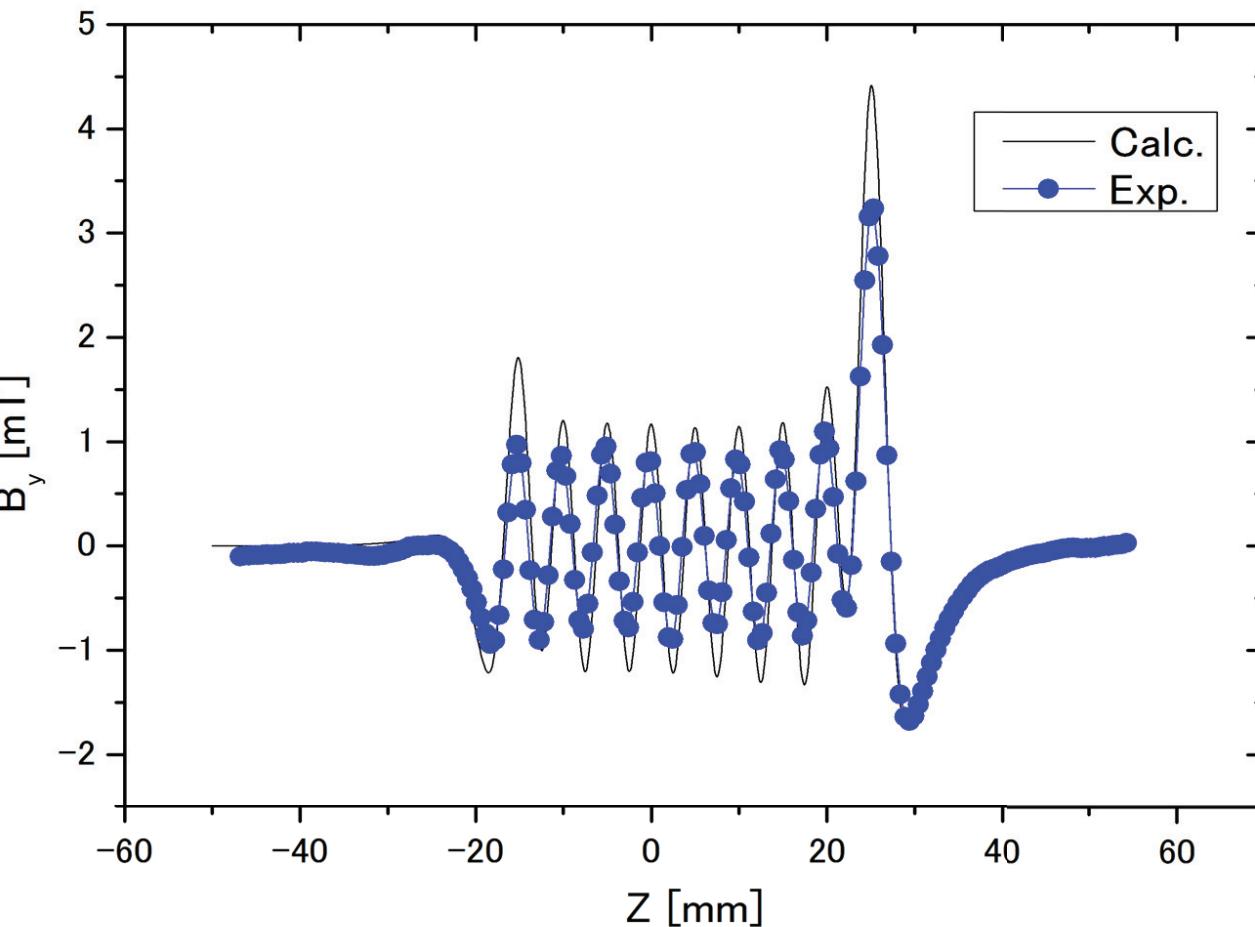
End field termination 2

Gap is extended at the end (Low height bulks)



End field termination 3

Additional bulks are attached at the end



Influence of J_c difference (numerical simulation)

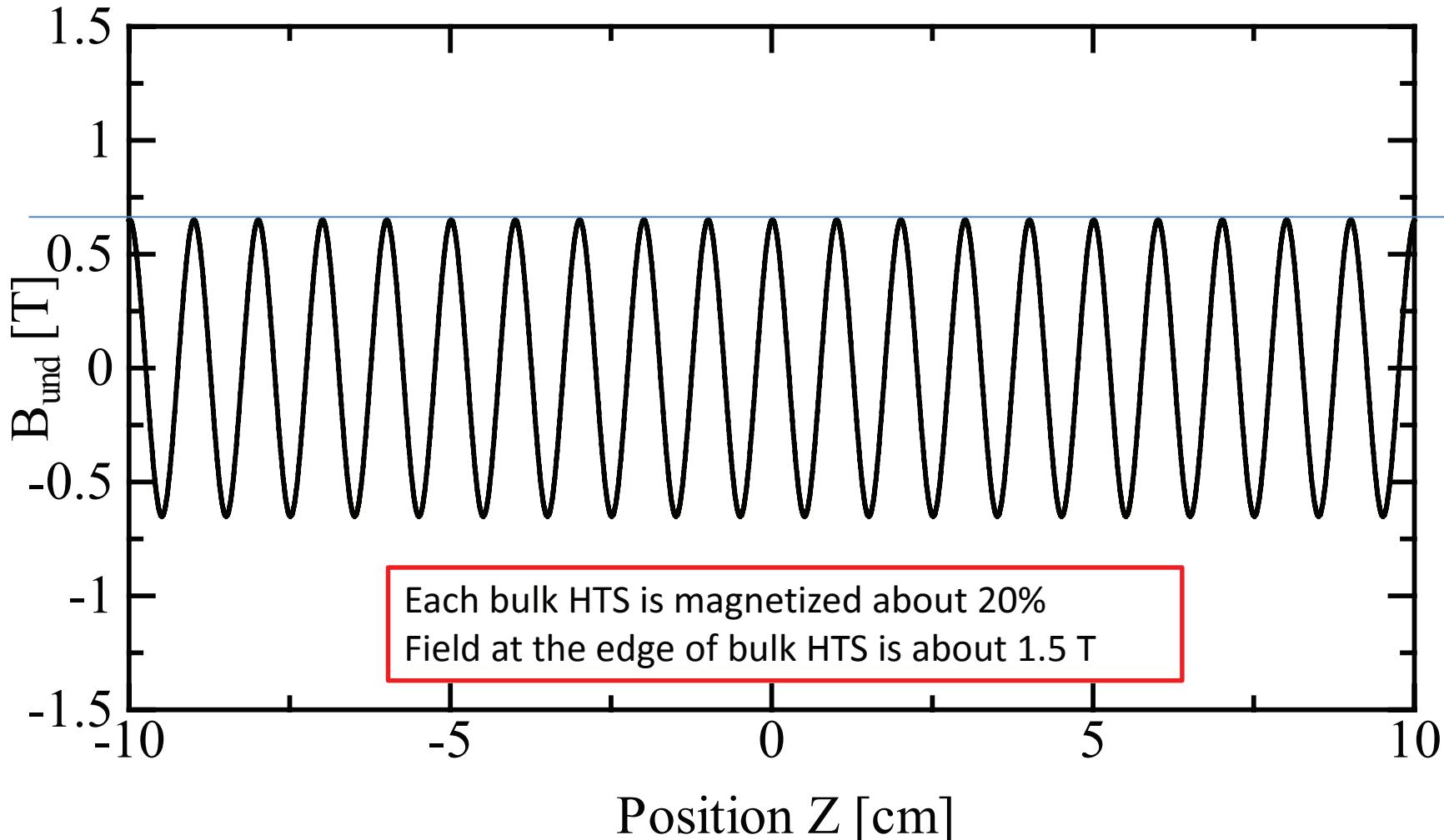
Assumed condition

J_c 5 kA/mm²

$J_c \sigma$ 0%

$B_{\text{und}} \sigma$ 0%

Target peak field uniformity < 1% will be obtained for J_c uniformity of 5%



Influence of J_c difference (numerical simulation)

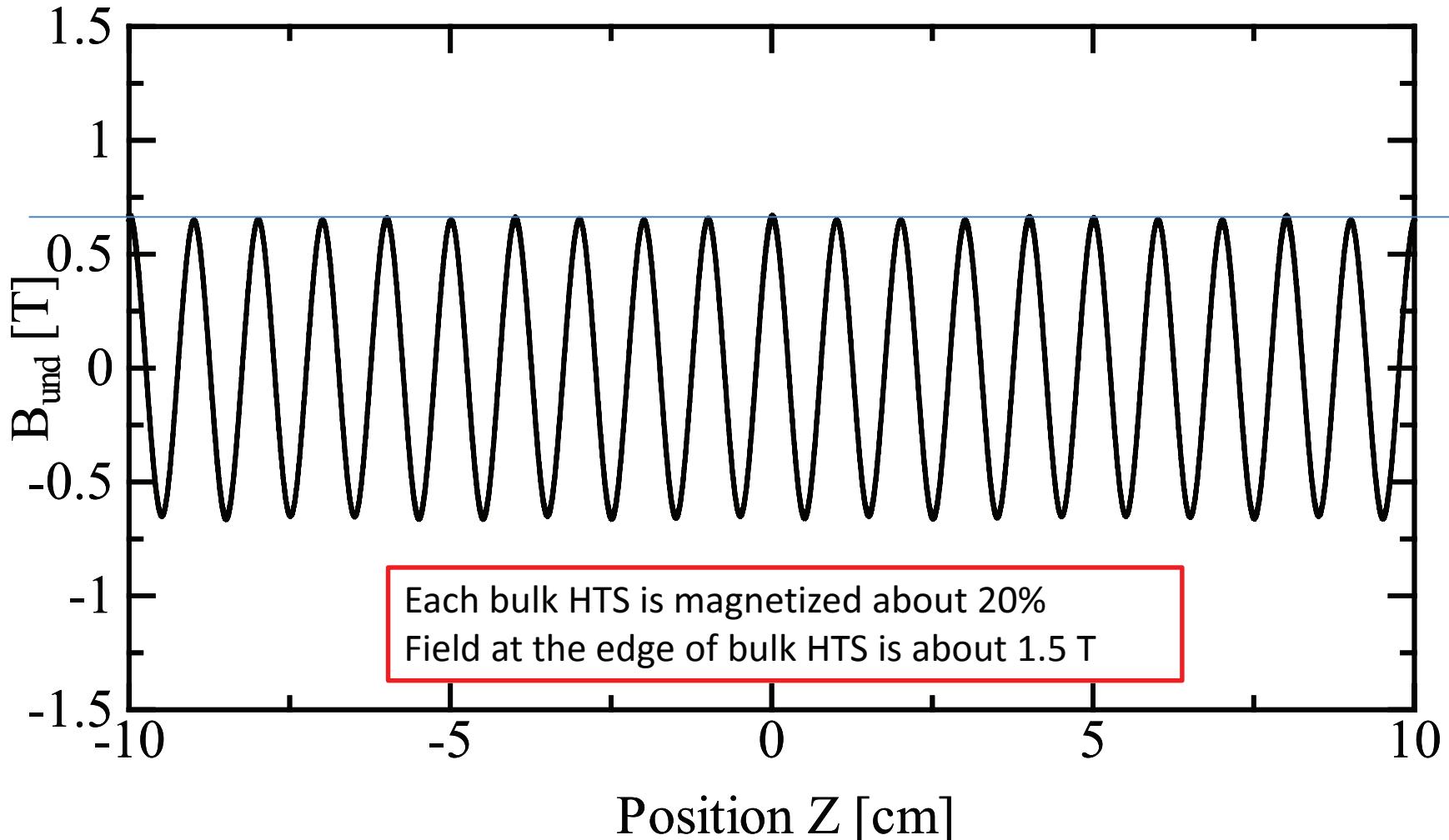
Assumed condition

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Influence of J_c difference (numerical simulation)

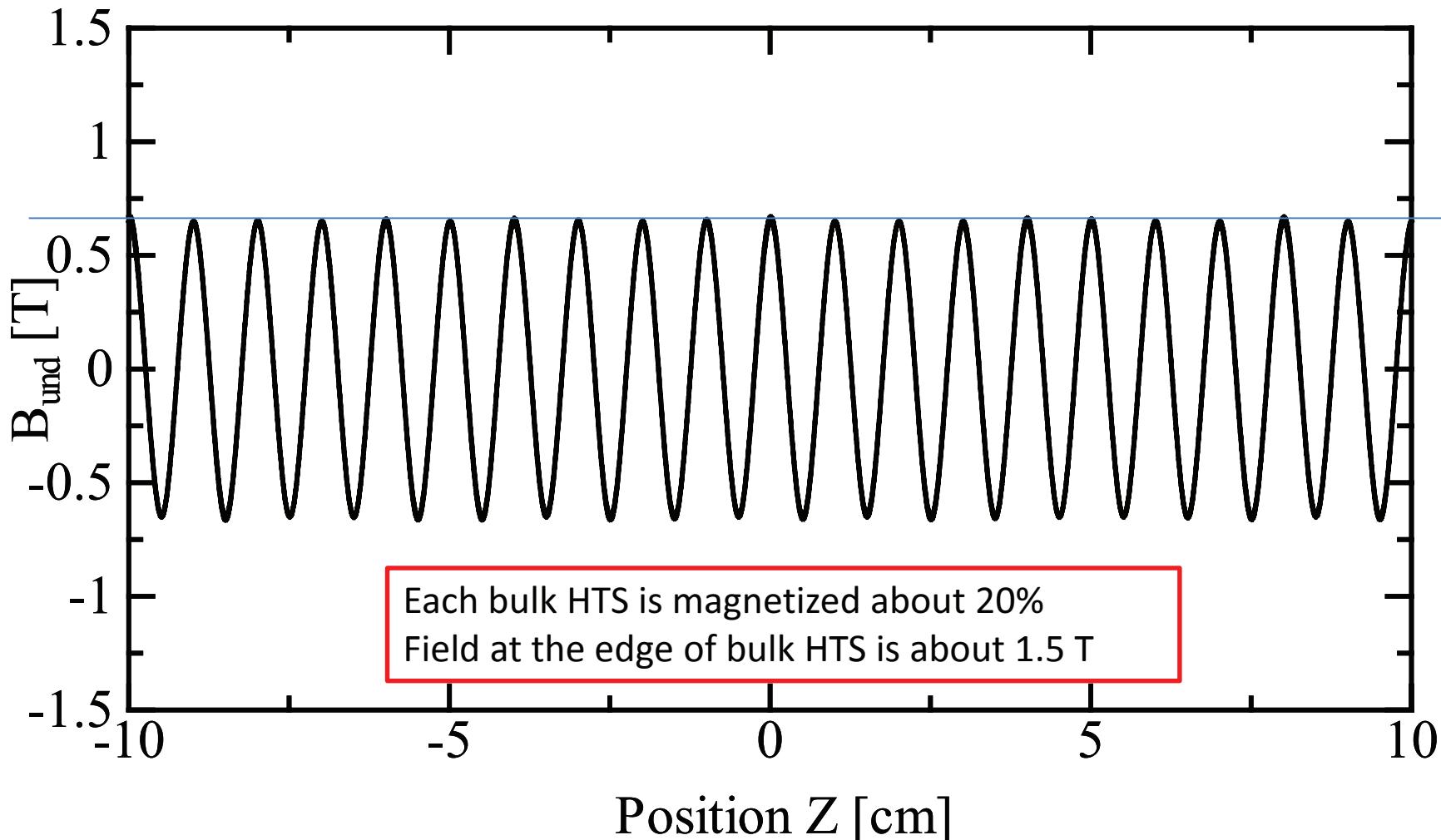
Assumed condition

J_c 5 kA/mm²

$J_c \sigma$ 0%

B_{und} \varnothing 000%

Target peak field uniformity < 1% will be obtained for J_c uniformity of 5%



Influence of J_c difference (numerical simulation)

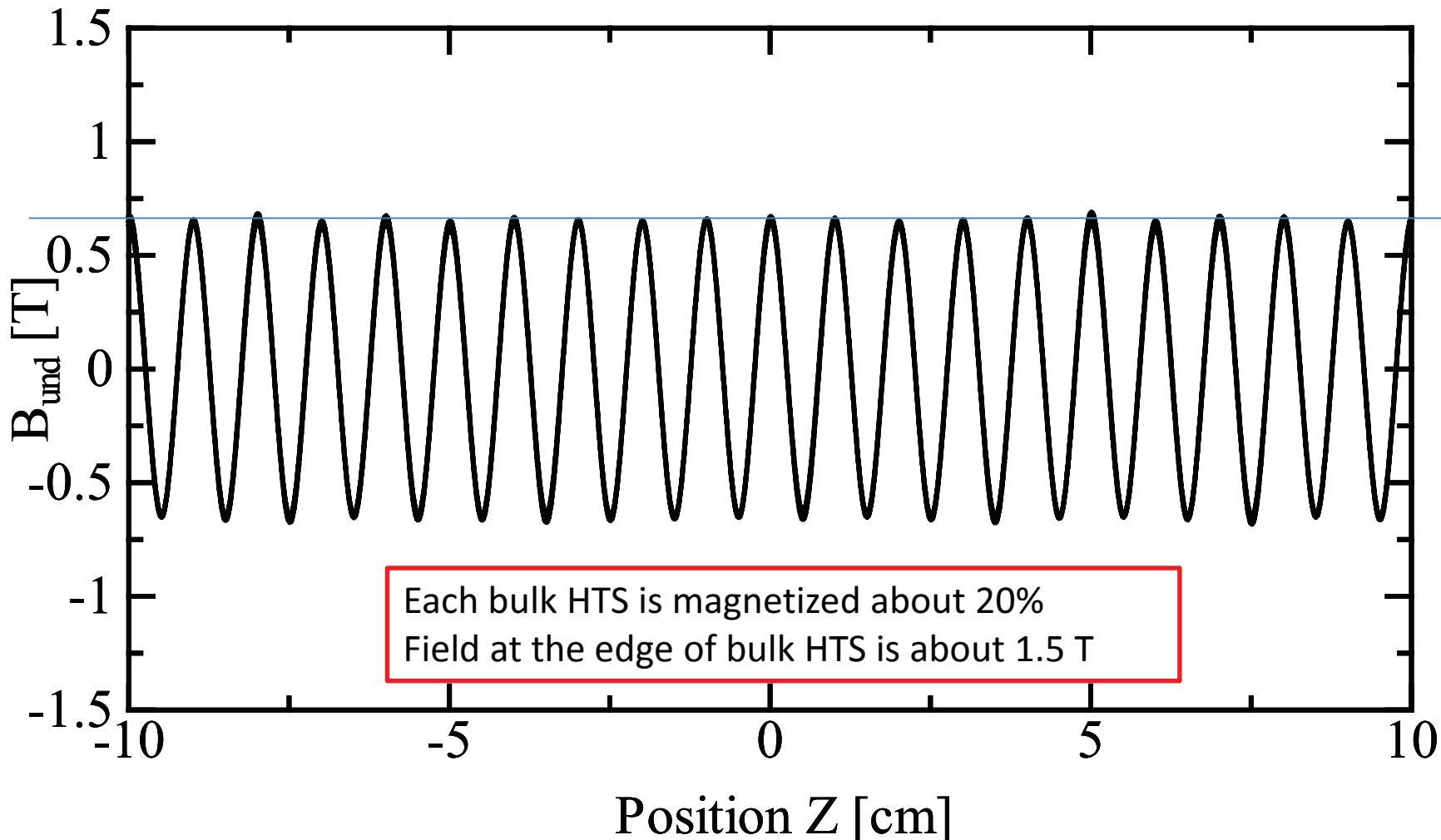
Assumed condition

J_c 5 kA/mm²

$J_c \sigma$ 0%

B_{und} \varnothing 008%

Target peak field uniformity < 1% will be obtained for J_c uniformity of 5%



Influence of J_c difference (numerical simulation)

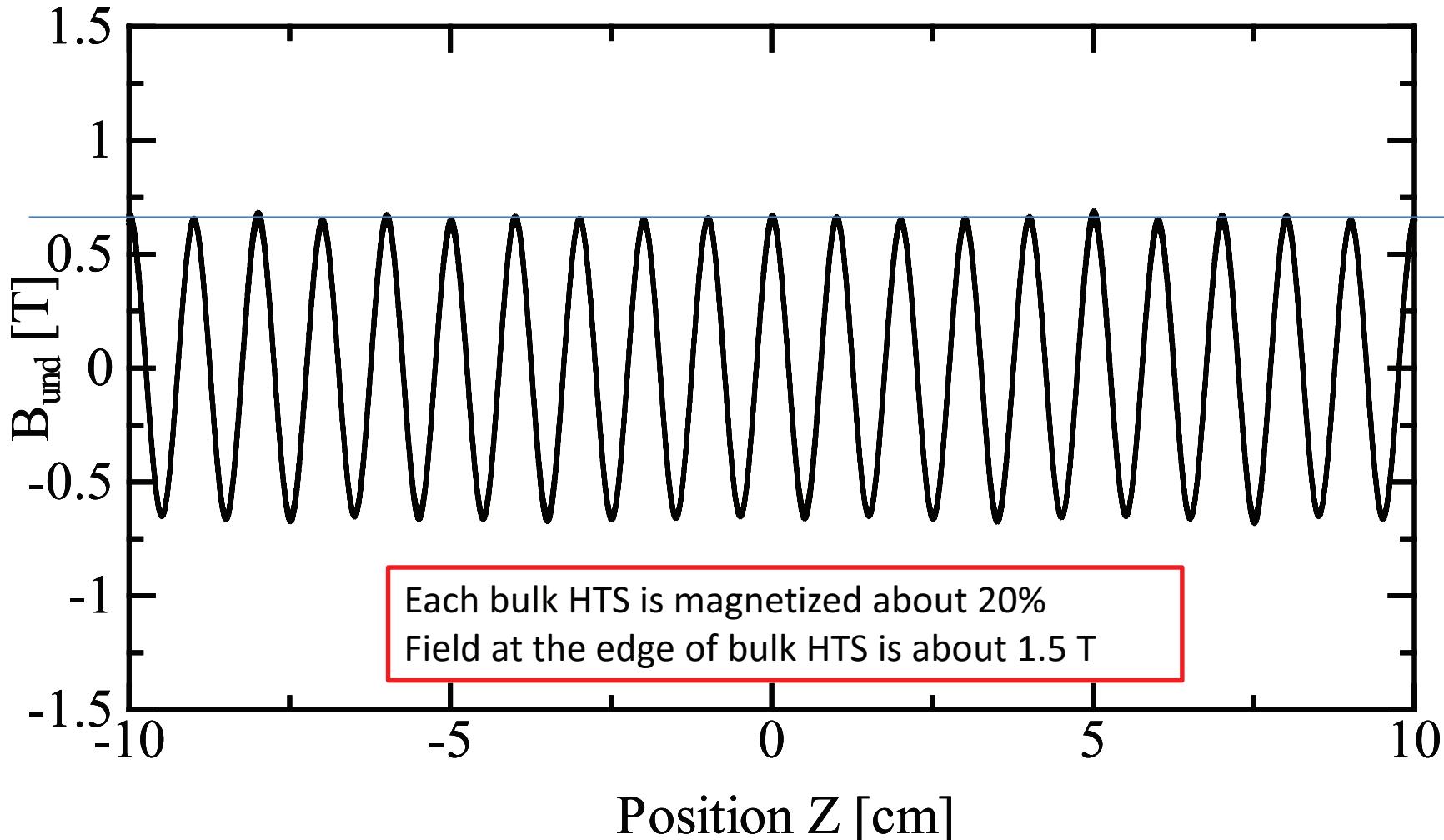
Assumed condition

$$J_c \text{ } 5 \text{ kA/mm}^2$$

$$J_c \sigma \text{ } 0\%$$

$$B_{\text{und}} \varphi \text{ } 0.05\%$$

Target peak field uniformity < 1% will be obtained for J_c uniformity of 5%



Influence of J_c difference (numerical simulation)

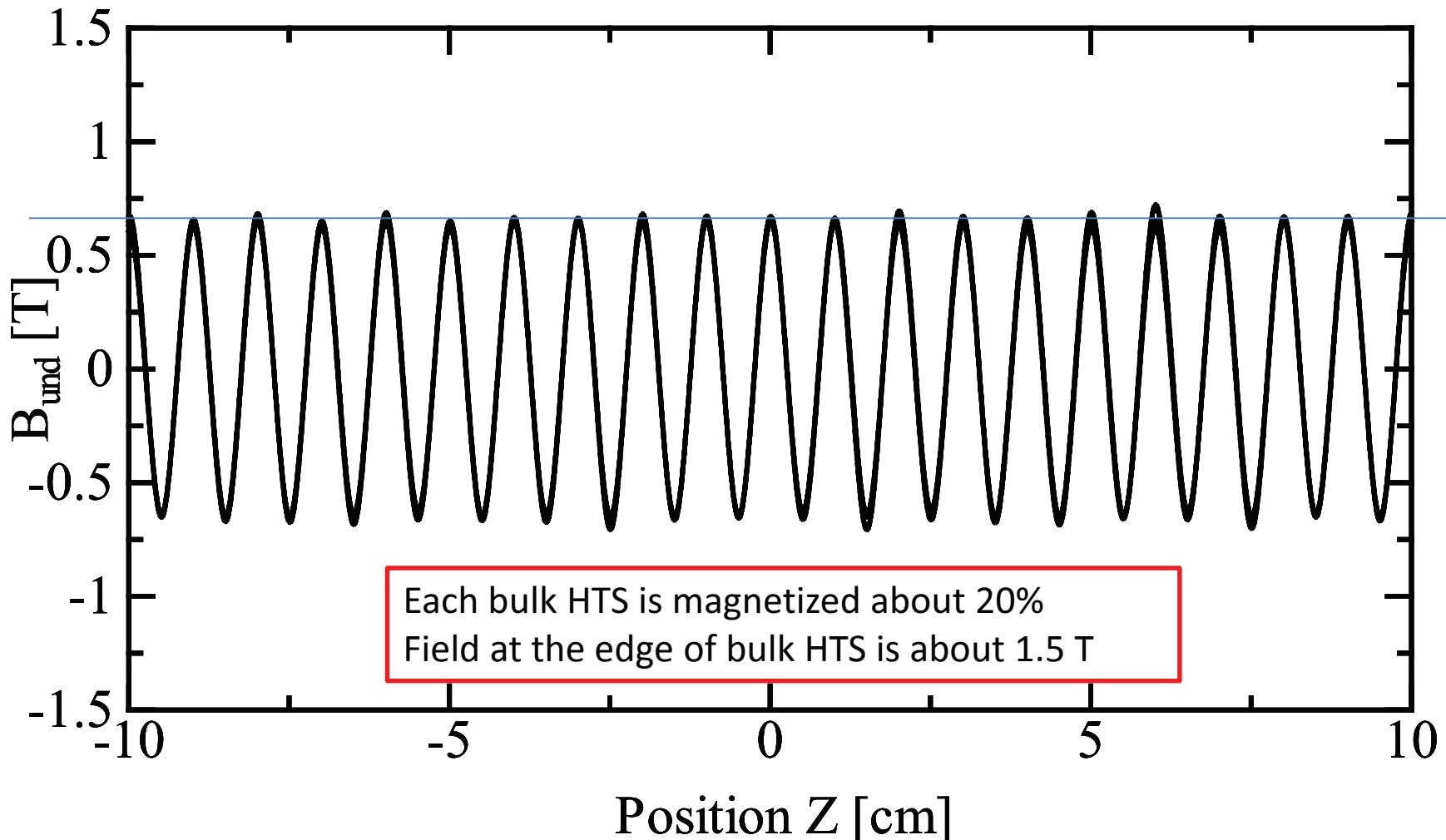
Assumed condition

$$J_c \text{ } 5 \text{ kA/mm}^2$$

$$J_c \sigma \text{ } 0\%$$

$$B_{\text{und}} \varphi \text{ } 0.05\%$$

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Influence of J_c difference (numerical simulation)

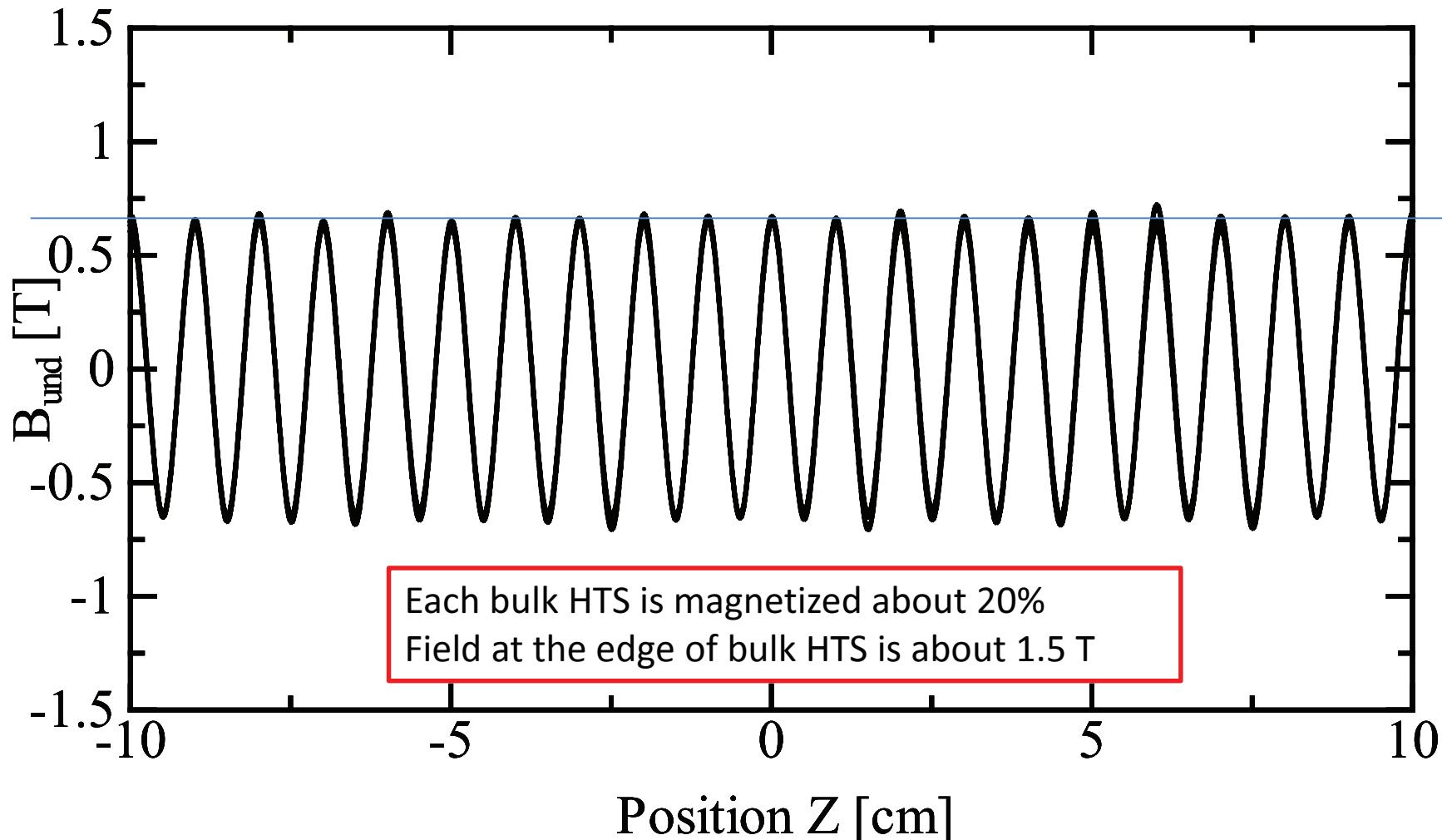
Assumed condition

$$J_c \text{ } 5 \text{ kA/mm}^2$$

$$J_c \sigma \text{ } 10\%$$

$$B_{\text{und}} \sigma \text{ } 0.05\%$$

Target peak field uniformity < 1% will be obtained for J_c uniformity of 5%



Influence of J_c difference (numerical simulation)

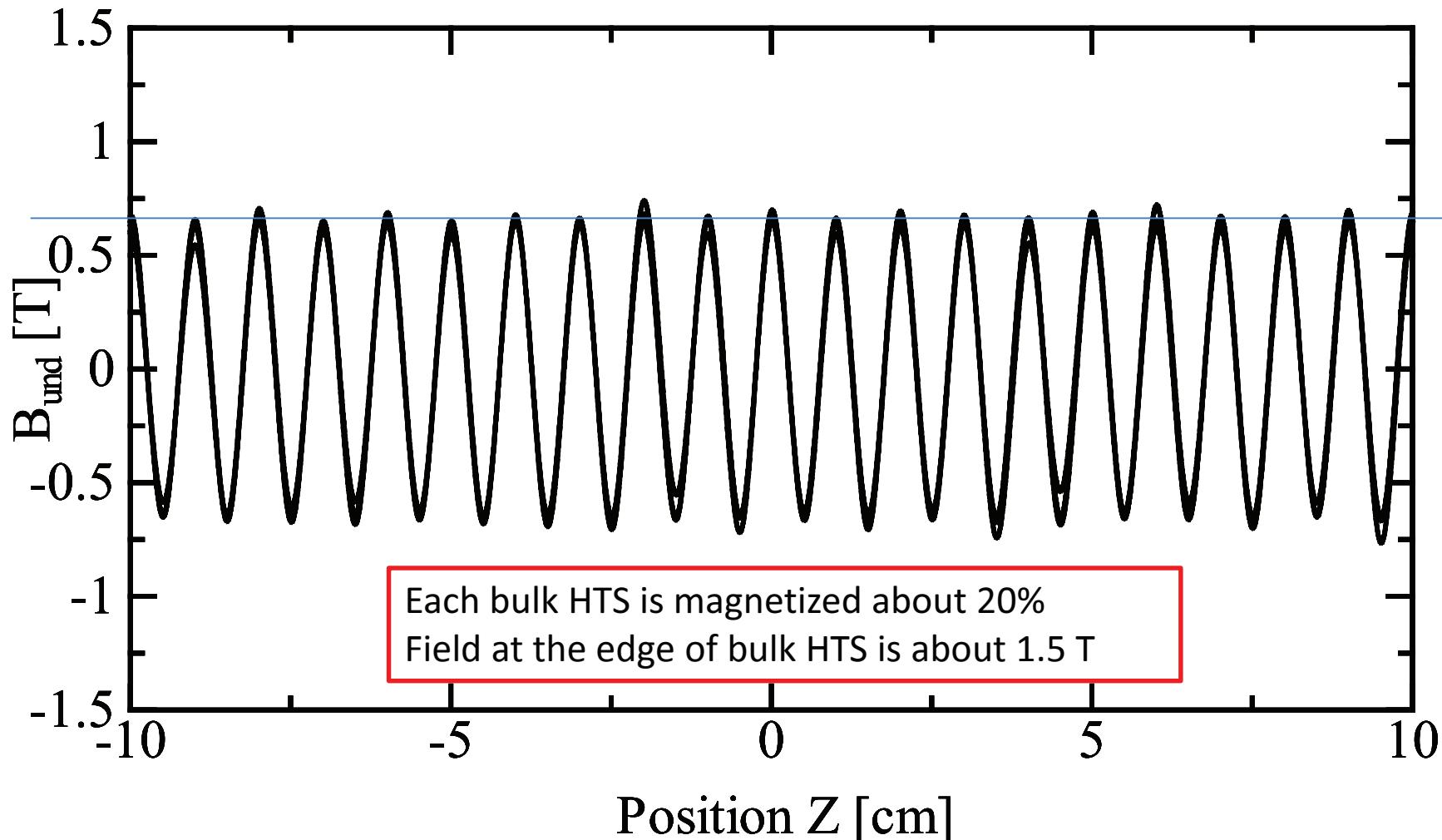
Assumed condition

J_c 5 kA/mm²

$J_c \sigma 10\%$

$B_{und} \varnothing 0.05\%$

Target peak field uniformity < 1% will be obtained for J_c uniformity of 5%



Influence of J_c difference (numerical simulation)

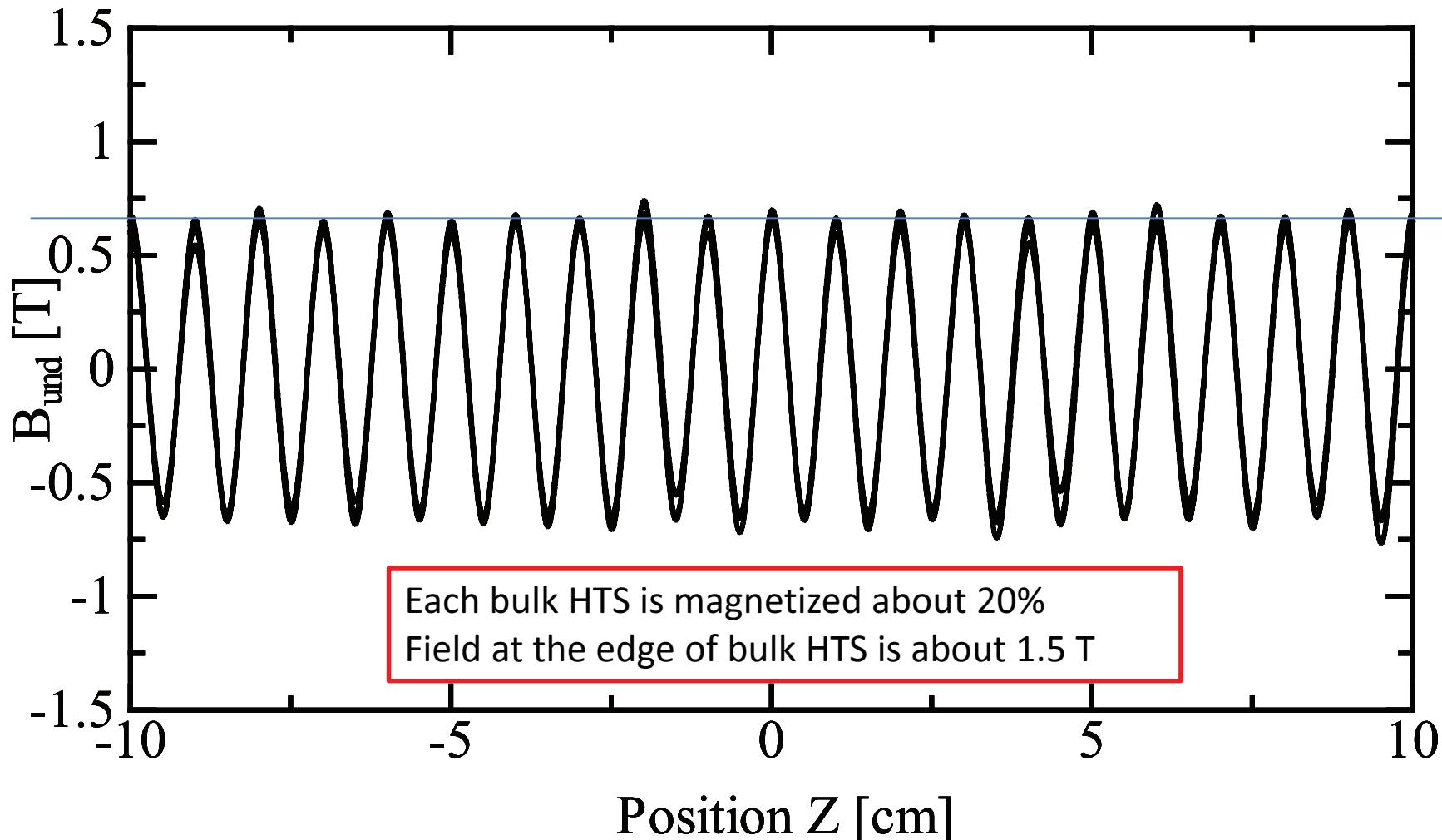
Assumed condition

J_c 5 kA/mm²

$J_c \sigma$ 20%

B_{und} ~~σ~~ 0.5%

Target peak field uniformity < 1% will be obtained for J_c uniformity of 5%



Influence of J_c difference (numerical simulation)

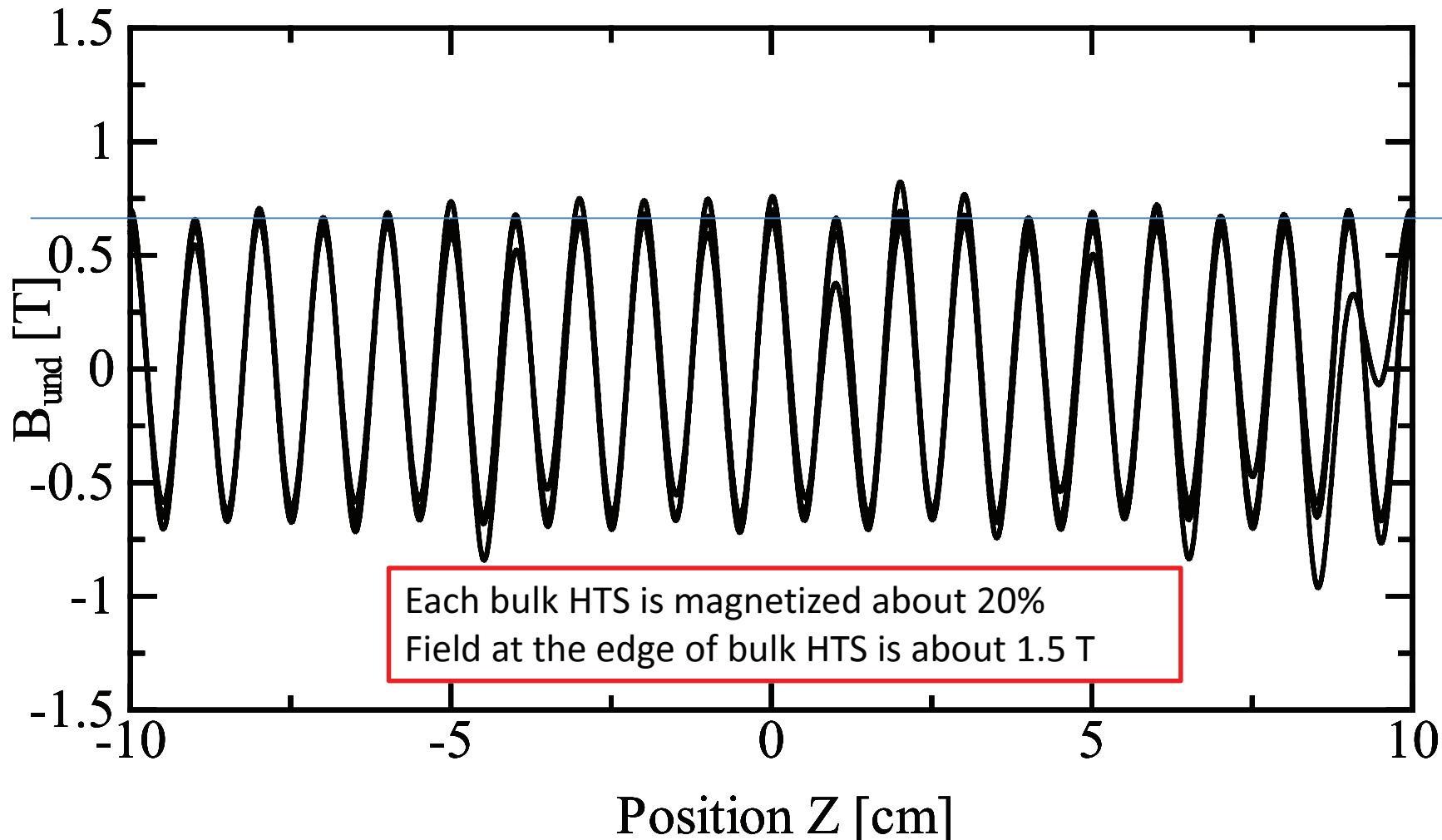
Assumed condition

J_c 5 kA/mm²

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B_{und} ~~σ~~ 0.5%

Target peak field uniformity < 1% will be obtained for J_c uniformity of 5%



Influence of J_c difference (numerical simulation)

Assumed condition

$$J_c \text{ } 5 \text{ kA/mm}^2$$

$$J_c \sigma \text{ } 20\%$$

$$B_{\text{und}} \sigma \text{ } 0.05\%$$

Target peak field uniformity < 1% will be obtained for J_c uniformity of 5%

