

Ultra-High Flux project: X-ray/THz Source based on Asymmetric Dual Axis Energy Recovery Configuration

I.V. Konoplev, A. Seryi

JAI, Oxford, UK

G. Burt

Cockcroft Institute, Lancaster, UK

R. Ainsworth

FNAL, USA

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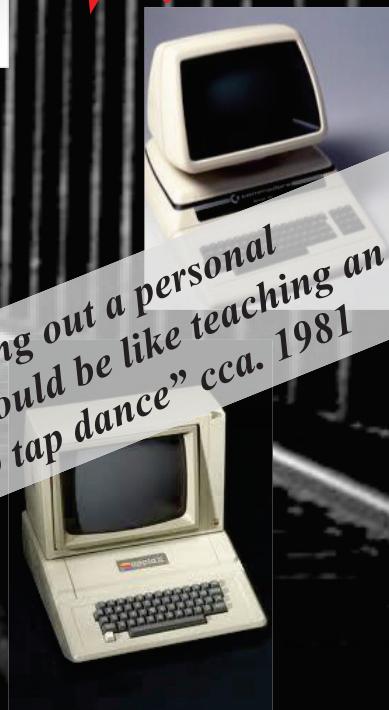
c/ X-ray source of radiation

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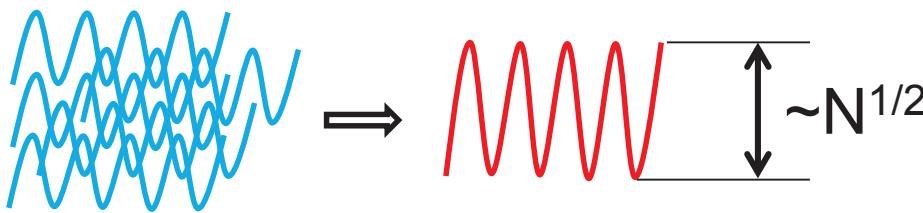
Evolution of computers and light sources



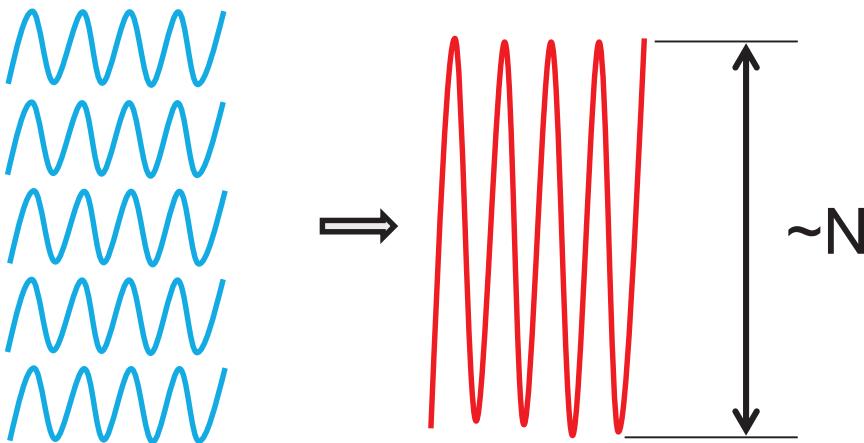
"IBM bringing out a personal computer would be like teaching an elephant to tap dance" cca. 1981



3rd generation => 4th generation



3rd generation SR sources:
the electrons emit photons with
random phases



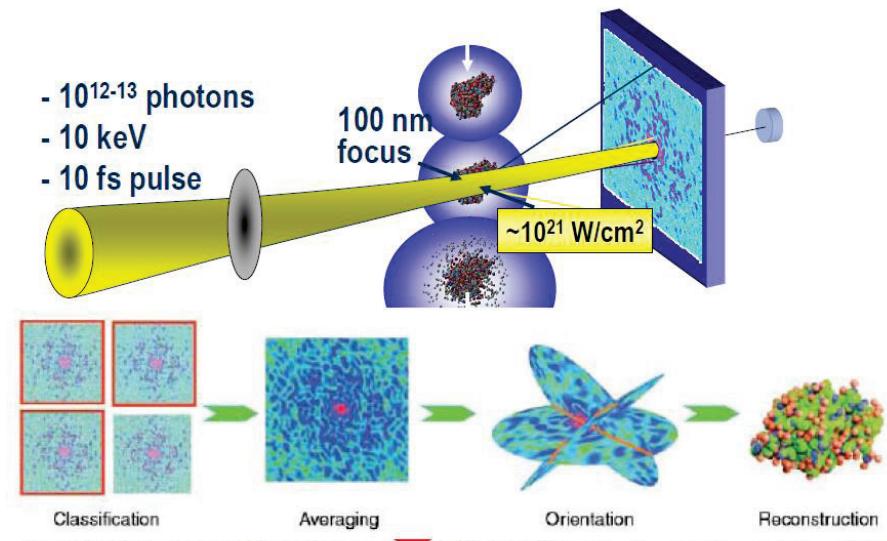
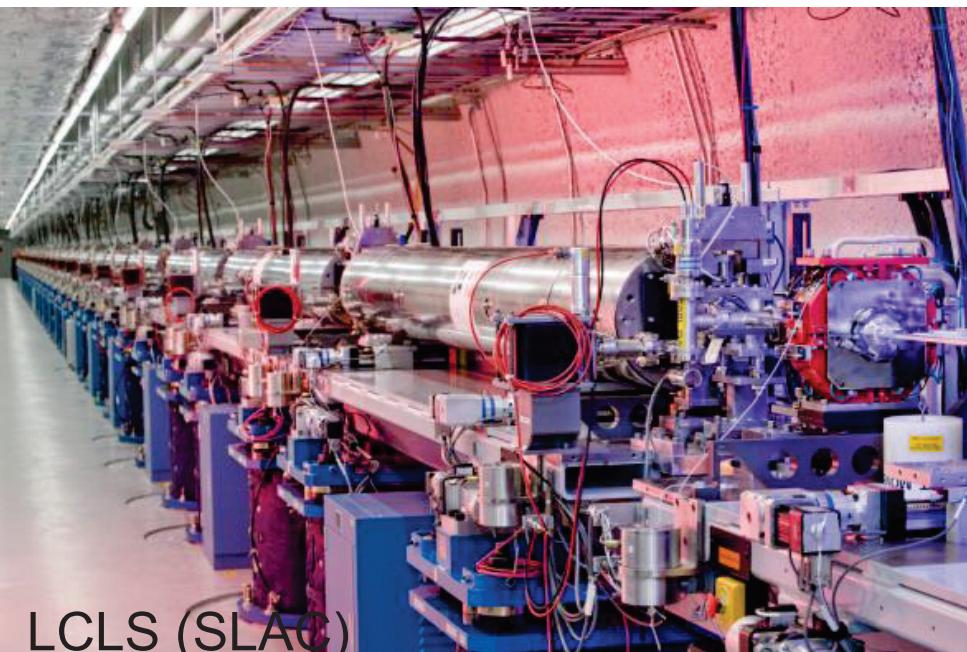
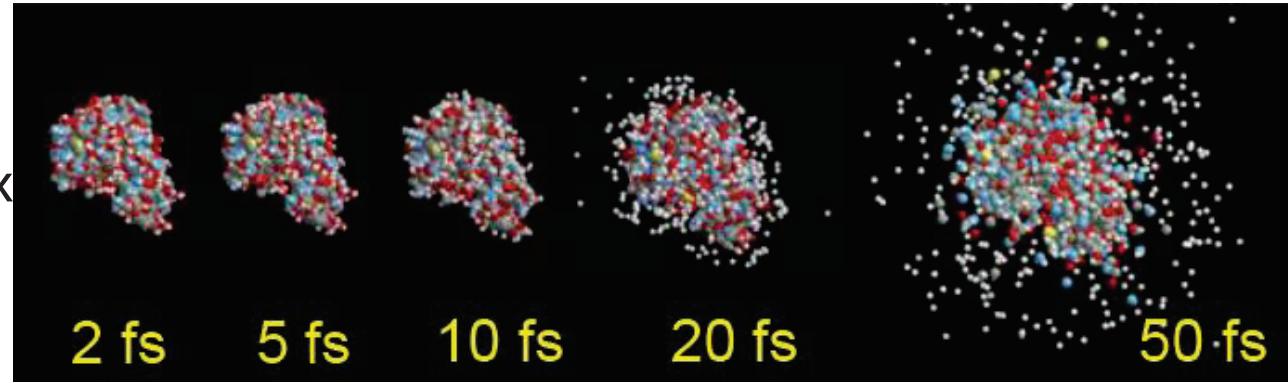
4th generation SR sources:
the electrons emit photons
all as one

4th generation sources – Free Electron Lasers (FELs)

FEL brightness is 10 orders of magnitude higher than brightness of 3rd generation sources

4th generation - FEL at Stanford

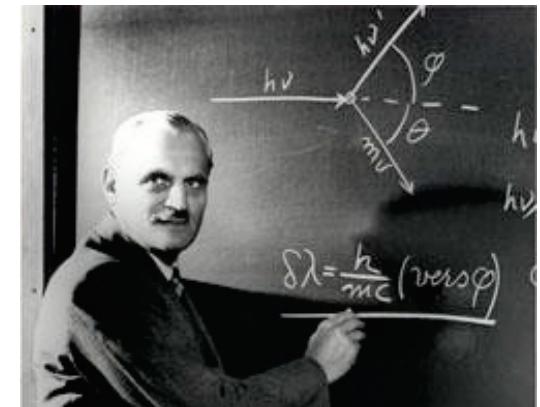
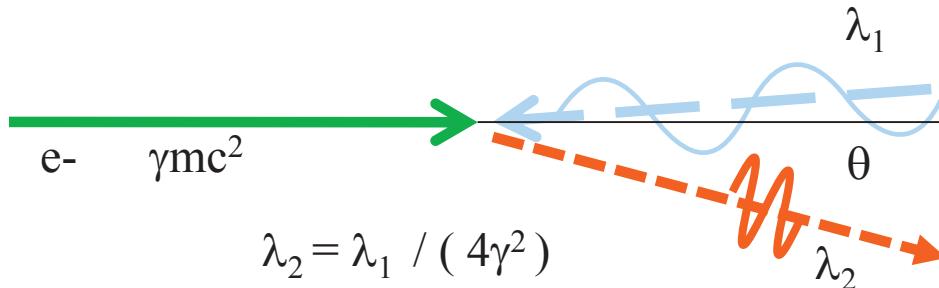
Immense brightness -
analysis of very complex
molecules (proteins)



Calculations. in vacuum Neutze et al., Nature 2000 Chapman, Gaffney Science 2007

Compton light sources

Based on the reflection of photons from accelerated electrons with an energy transfer to photons



Arthur Compton

Compact X-ray light source

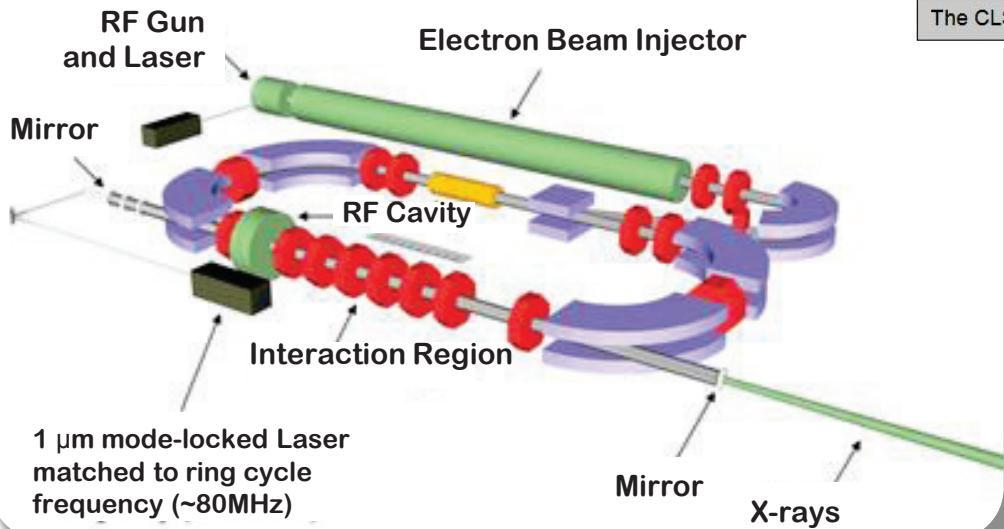
- 25 MeV accelerator
- X-ray tuneable from a few keV up to 35 keV

Commercially available, e.g.:
Lyncean Technologies, Inc.

Compact X-ray light source

25 MeV accelerator
X-ray tuneable from a few keV up to
35 keV

Fits in a 10x25 ft room

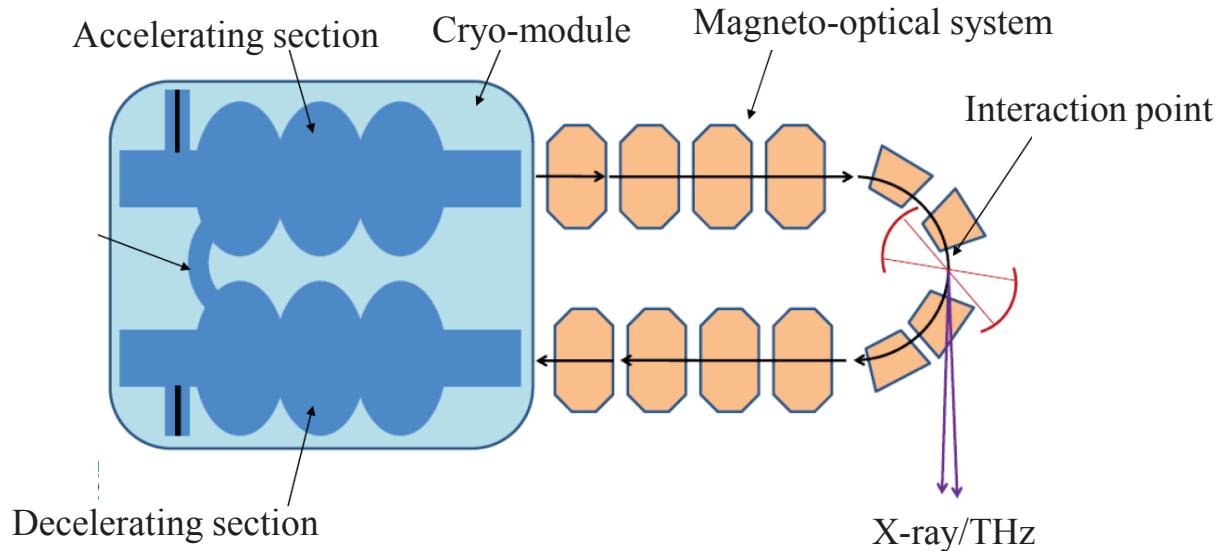


The CLS assembled at the headquarters of Lyncean Technologies, Inc. in Palo Alto, CA

RF power source outside (not on the photo)

<http://www.lynceantech.com/index.html>

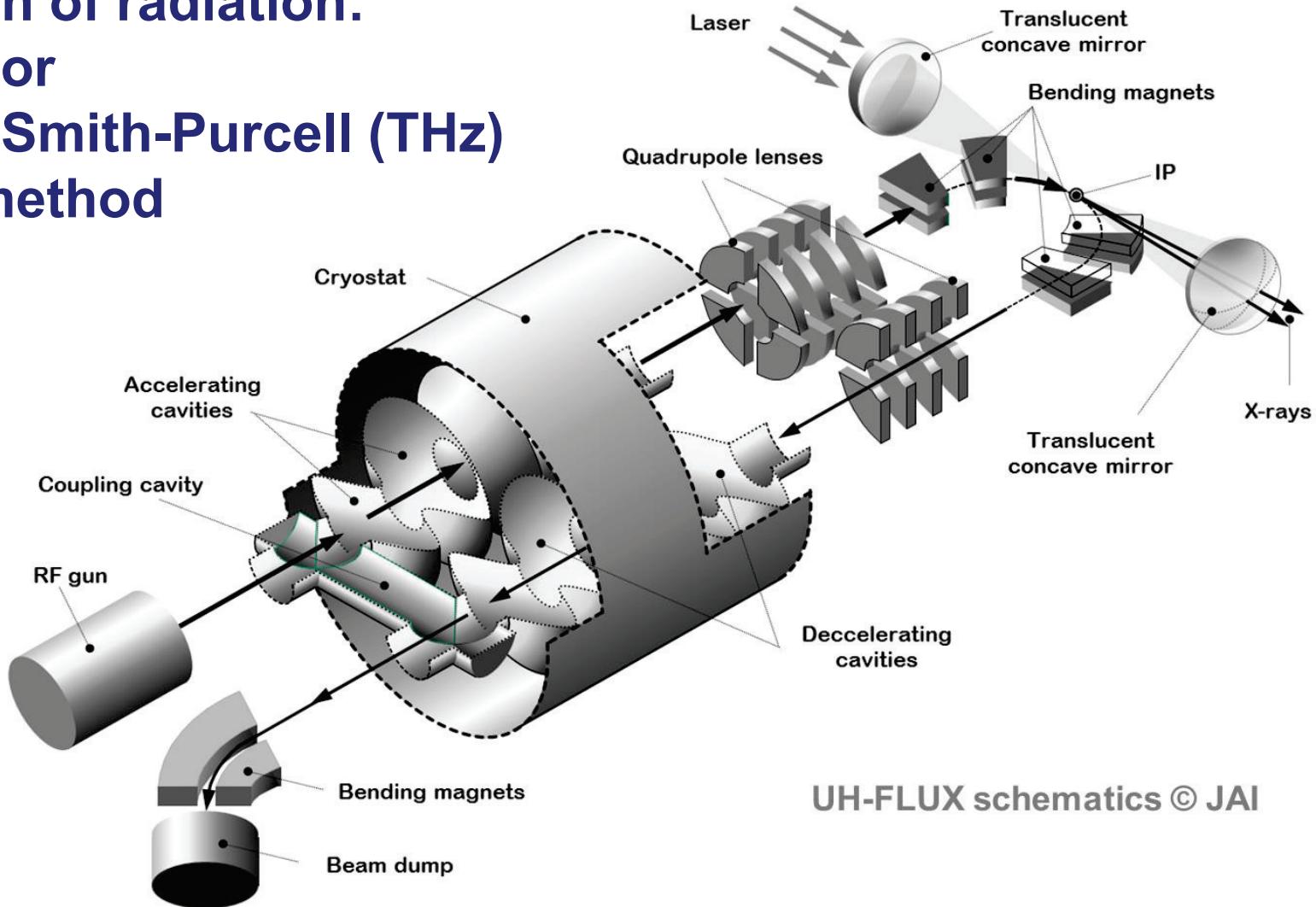
Next steps in Compton/THz sources – UH-FLUX project



- **Collaboration of UK centers JAI, CI, STFC and UK industry is developing an advanced Compton/THz source**
- [1] International (PCT) Patent Application No. PCT/GB2012/052632 (WO2013/061051) filed on the 26th October 2012
- [2] Oxford University Isis Project No. 11330 – “Asymmetric superconducting RF structure” (UK Priority patent application 1420936.5 titled ‘Asymmetric superconducting RF structure’ filed on the 25th November 2014

UH-FLUX – conceptual layout

Generation of radiation:
Compton or
Coherent Smith-Purcell (THz)
or other method

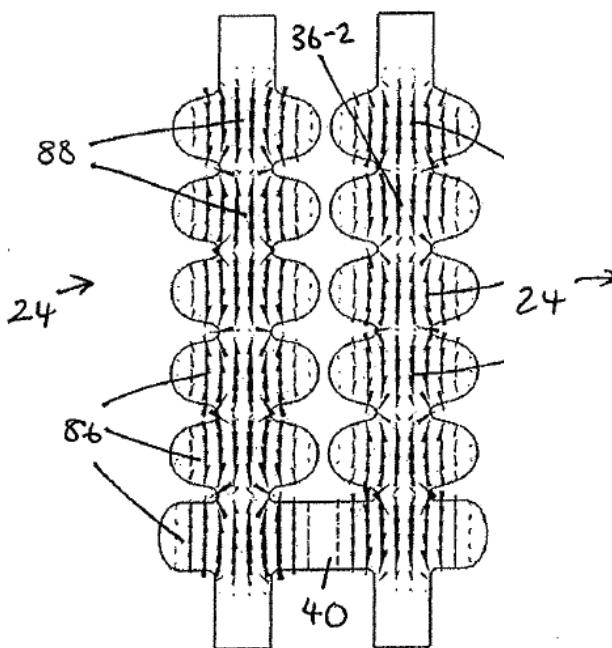


UH-FLUX schematics © JAI

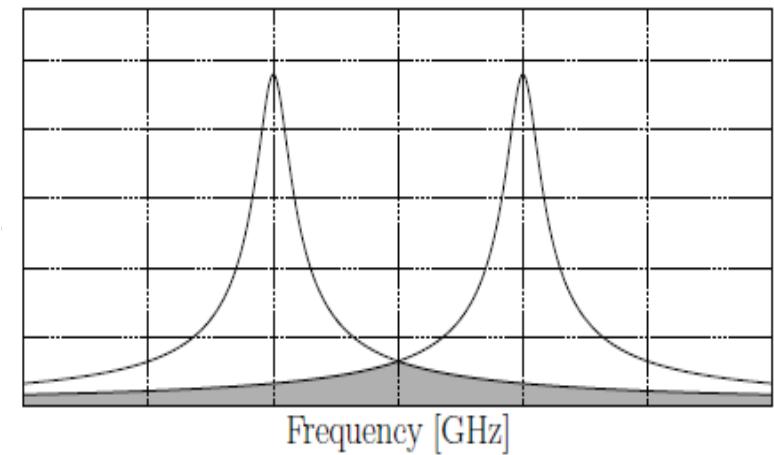
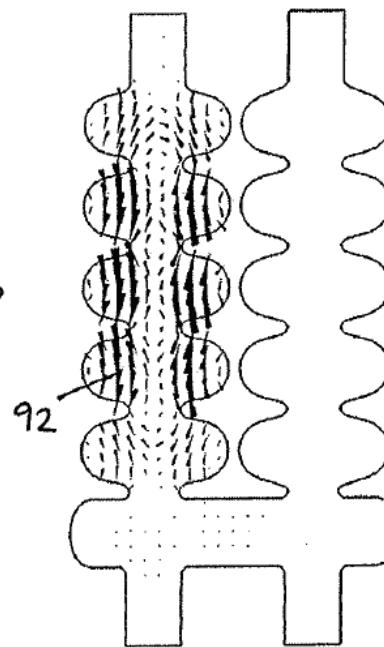
UH-FLUX: Asymmetric ERL

Decoupling all modes except the accelerating mode to maximize the beam current

Acc. mode



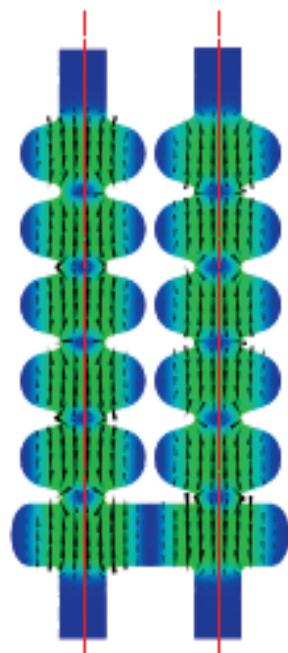
One of transverse modes



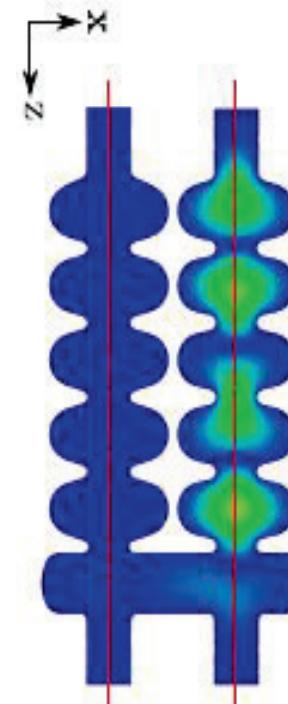
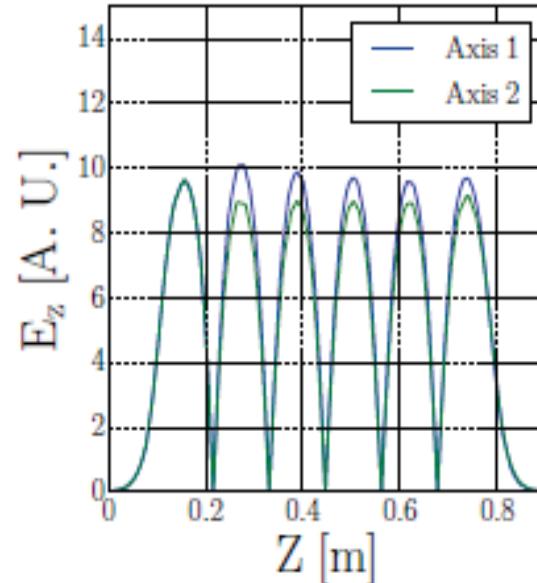
UH-FLUX: Asymmetric ERL

Electric field contour plot of operating eigenmode at 1.3GHz

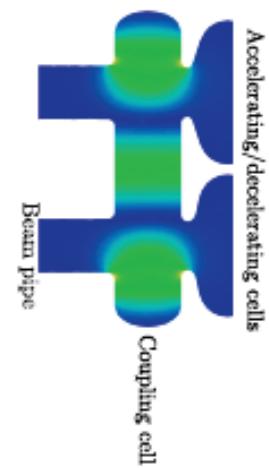
Axis 1 Axis 2



Operating field flatness @1.3GHz



Electric field contour plot of resonant coupler eigenmode at 1.48GHz



Electric field contour plot of dipole eigenmode at 1.73GHz

UH-FLUX: Asymmetric ERL

$$\Delta r \cong -\frac{2c}{\omega} \nabla_{\perp} V(r, \varphi) \frac{L}{W} \mathbf{R}_{12} \quad \text{Electron bunch deviation from designed trajectory due to HOM}$$

$$\Delta\tau \cong \frac{1}{2} \left(\frac{\mathbf{R}_{12}\theta}{S_0} \right)^2 T_g = \frac{\Delta r}{2S_0} \frac{\Delta r}{c} \quad \text{Time detuning of the electron bunch due to HOM}$$

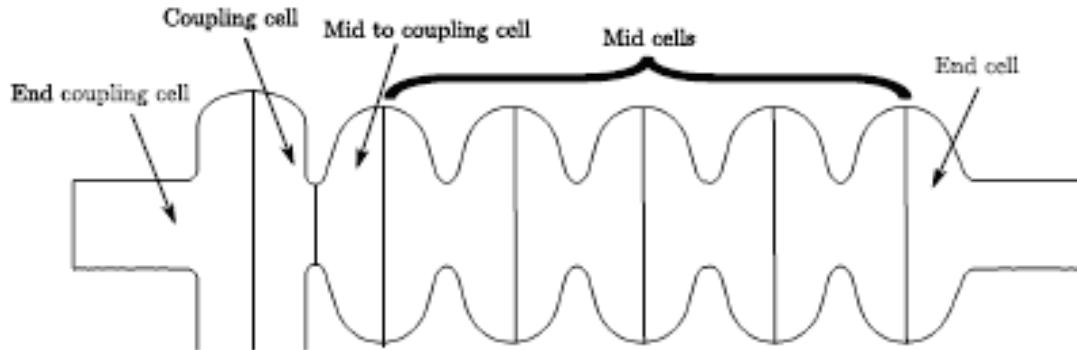
$$\Delta\phi \cong \frac{(\mathbf{R}_{12}\theta)\Delta r}{S_0\lambda_0}\pi \quad \text{Phase detuning of the electron bunch due to HOM}$$

$$I_{max} = (D_2 W \omega) / (2r K_m F^{\infty}) \quad \text{Maximum electron beam current above which beam transportation will be interrupted due to HOM}$$

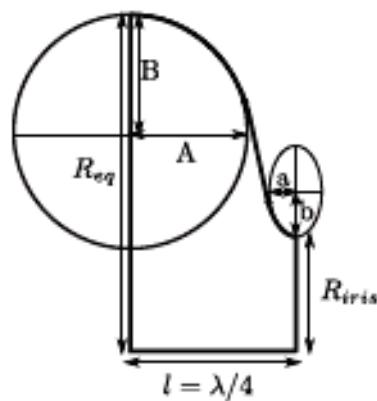
$$F^{\infty} = \frac{\sin(\delta\omega_n T_{rep})}{2 \cosh(T_{rep}/T_{dec}) - \cos(\delta\omega_n T_{rep})}$$

$$|V_2| = \left| V_1 e^{-T_{rep}/T_{dec}} \right| \quad K_m = c/4[R/Q]_j^m$$

Technical drawing



Midcell



Coupling cell

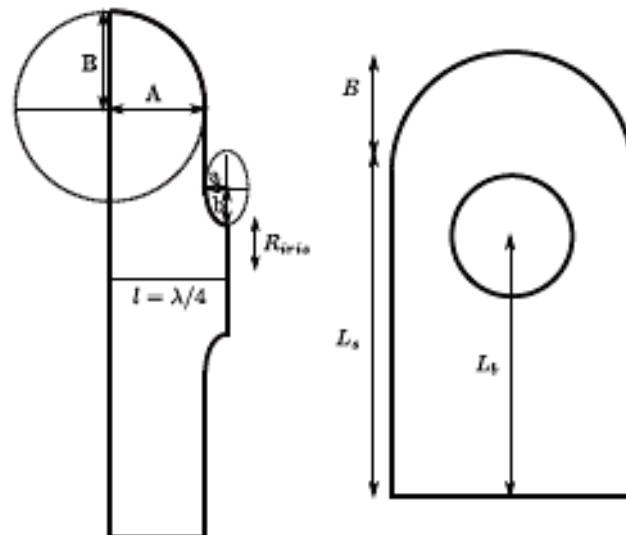
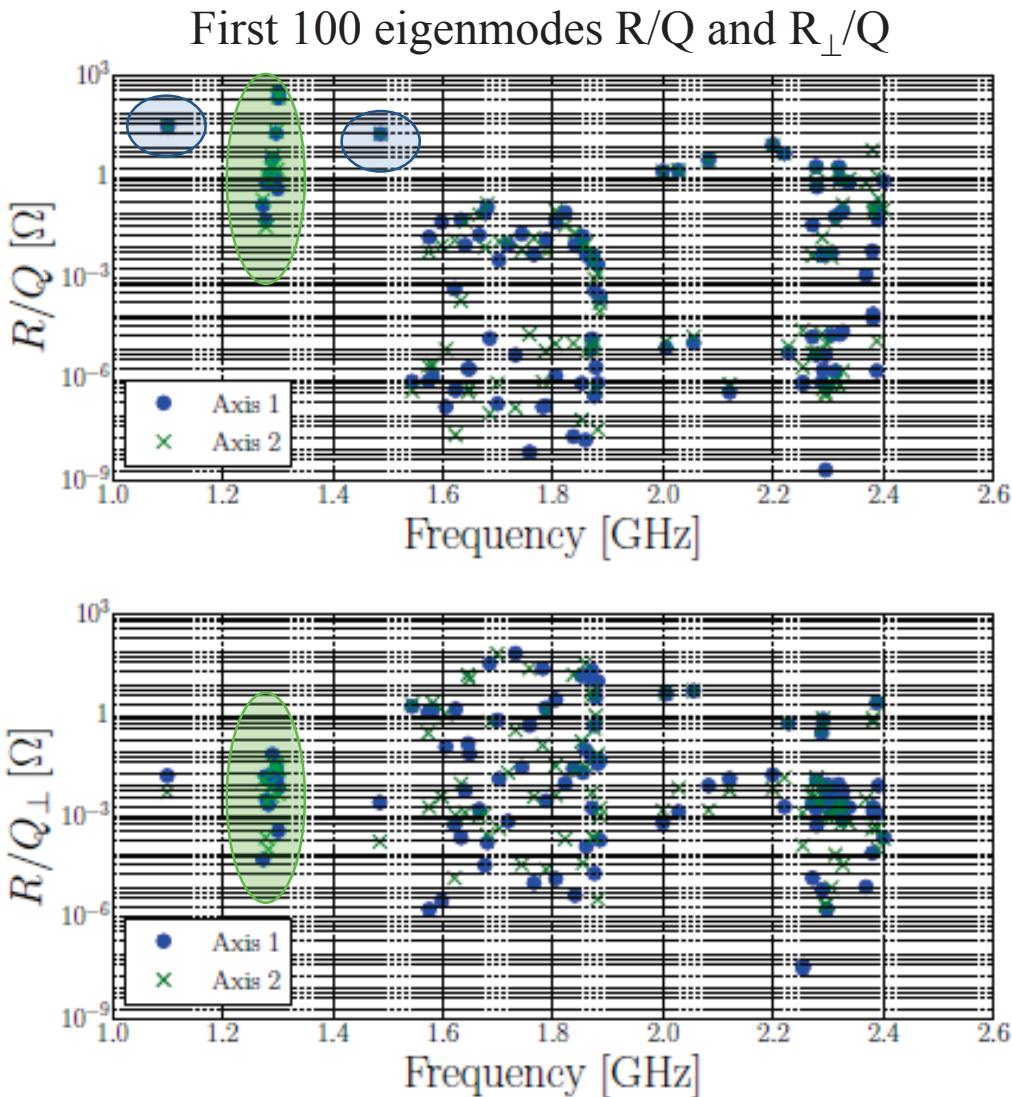


Table of numerical model parameters

Parameter	Axis 1 cell [mm]	Axis 2 cell [mm]
Mid cells		
R_{eq}	103.3	103.3
A	42	42
B	42	43.1
R_{iris}	35.75	37
a	12.75	11.75
b	18	20
l	57.7	57.7
End cells		
R_{eq}	103.3	104.3
A	42	42
B	42	43
R_{iris}	39	39
a	12.75	11.75
b	18	20
l	58.54	60.96
Mid to coupling cells		
R_{eq}	103.3	104.3
A	42	42
B	43.4	43.5
R_{iris}	35	35
a	12.75	9.69
b	18	20
l	57.7	57.7
Coupling cells		
A	48.052	48.052
B	29	29
R_{iris}	35	35
a	9.6	9.6
b	10.152	10.152
l	57.652	57.652
L_s	150	150
L_b	111	111
End coupling cells		
A	47.5	47.5
B	29.76	29.76
R_{iris}	39	39
a	9.945	9.945
b	9.945	9.945
l	57.652	57.652
L_s	150	150
L_b	111	111



Frequency GHz	Axis 1 R/Q Ω	Axis 2 R/Q Ω	Axis 1 $R/Q_{\perp,x}$ Ω	Axis 2 $R/Q_{\perp,x}$ Ω	Axis 1 $R/Q_{\perp,y}$ Ω	Axis 2 $R/Q_{\perp,y}$ Ω
Highest R/Q						
1.3	348.71	301.51	0.0675	0.0365	0.0074	0.0
1.29943	231.71	247.59	0.0014	0.0059	0.0003	0.0048
1.09966	32.622	32.367	9.5769	9.0660	0.0166	0.0055
1.29532	21.075	23.878	0.0014	0.0267	0.0281	0.0333
1.48554	20.337	20.429	12.094	12.360	0.0026	0.0001
Highest $R/Q_{\perp,x}$						
1.70216	0.0035	0.0127	65.207	0.8680	0.0134	0.0004
1.74343	0.0211	0.0069	61.997	0.4792	0.0294	3.8679
1.87193	0.0050	0.0029	35.500	0.0810	0.0555	0.0002
1.85436	0.0181	0.0091	17.329	0.3260	0.0208	4.2119
1.48554	20.337	20.429	12.094	12.360	0.0026	0.0001
Highest $R/Q_{\perp,y}$						
1.73192	5.4419	1.4736	0.0005	0.0001	72.089	0.3764
1.68526	1.6890	9.9178	0.0024	1.8274	36.312	0.6537
1.78142	1.5499	8.7076	0.0039	0.0070	25.636	0.1329
1.87103	1.6368	7.9211	4.8525	0.0037	22.491	4.0005
1.8523	7.7902	6.4131	0.0033	0.0001	15.388	0.1740

$$R/Q_n = \frac{|V_{\parallel,n}(0)|^2}{\omega_n U_n} \quad R/Q_{\perp,n} = \frac{|V_{\perp,n}(x)|^2}{\omega_n U_n}$$

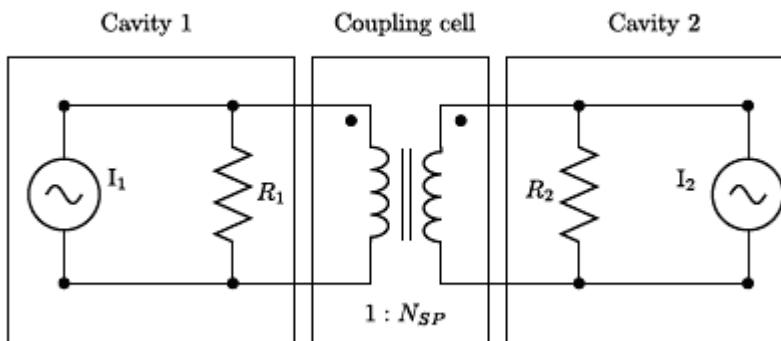
$$V_{\parallel,n}(x) = \int_{-\infty}^{\infty} E_{z,n}(x, z) e^{i\omega_n z/c} dz$$

$$V_{\perp,n} = i \frac{c}{\omega_n x} [V_{\parallel,n}(x) - V_{\parallel,n}(0)]$$

The R_{\perp}/Q calculated @ 1mm from the axis

Maximize the BBU start current allowing to transport up to 2A beam without break-up

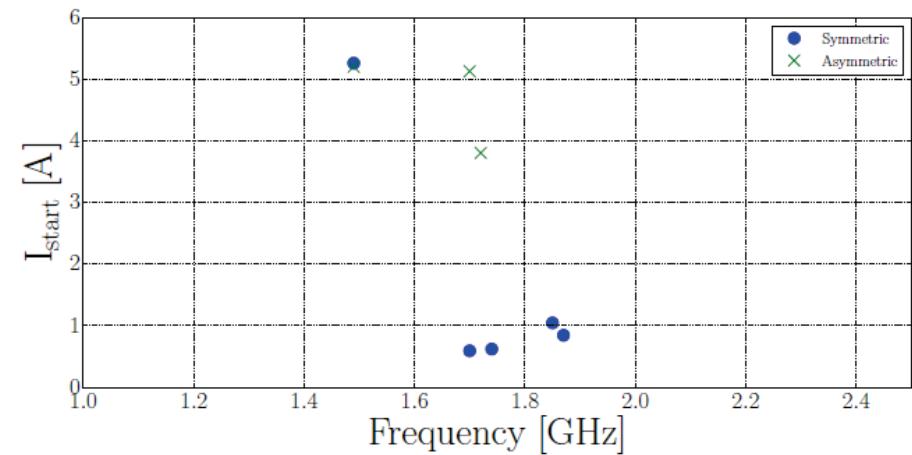
Schematic of RLC diagram of dual axis structure



$$I_{asymmetric} > \frac{(1 + N_{SP}^2) I_{symmetric}}{2N_{SP}}$$

N_{SP} is the voltage transformer ratio

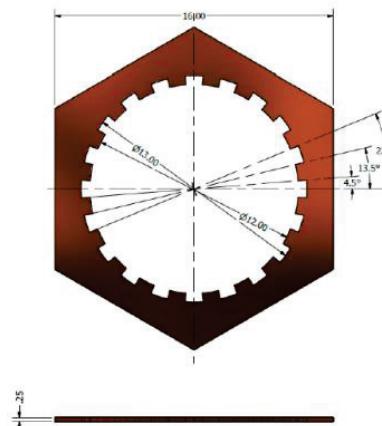
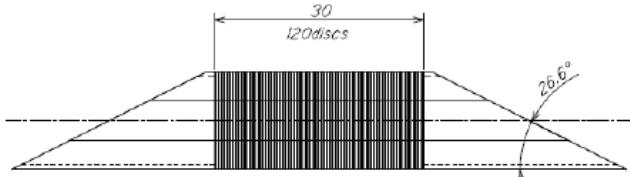
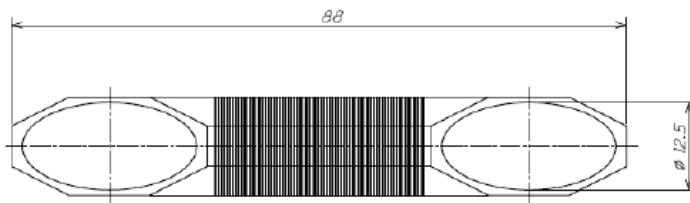
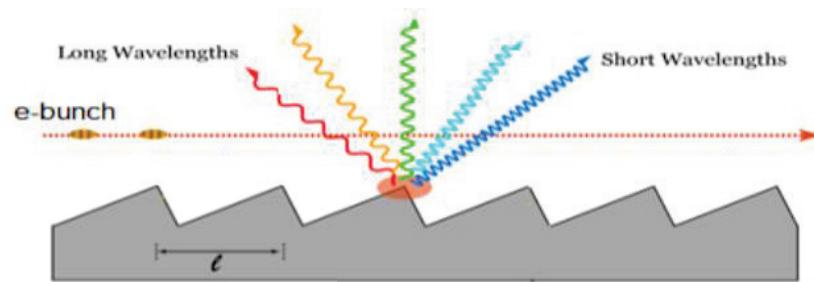
HOMs start currents



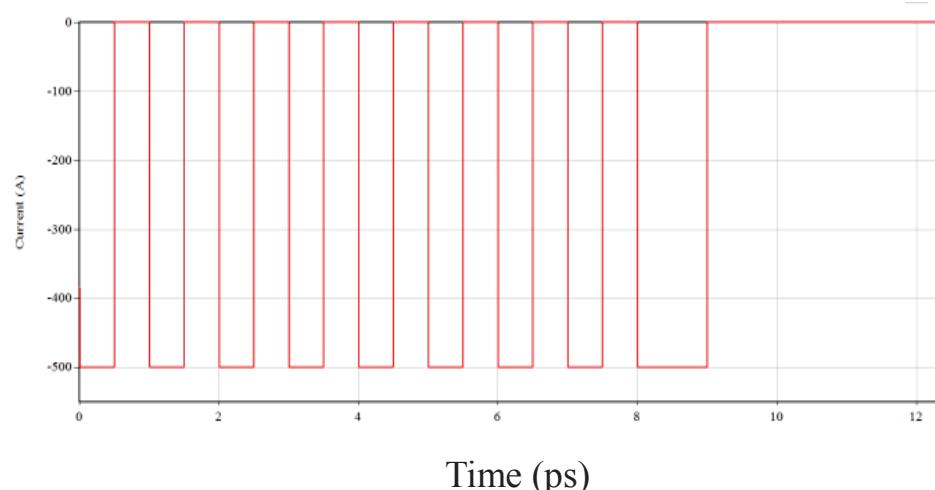
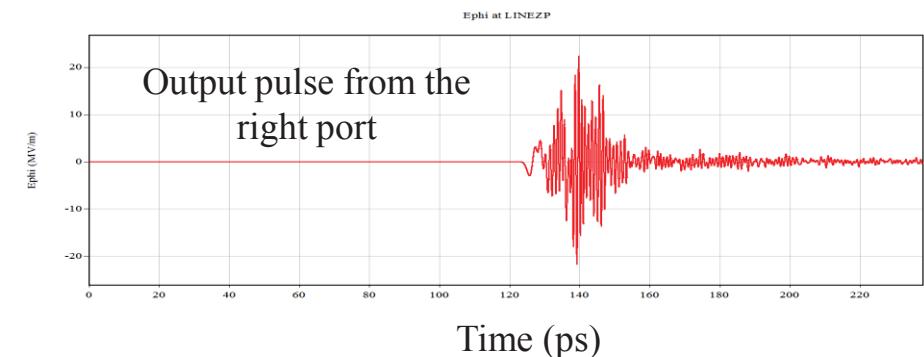
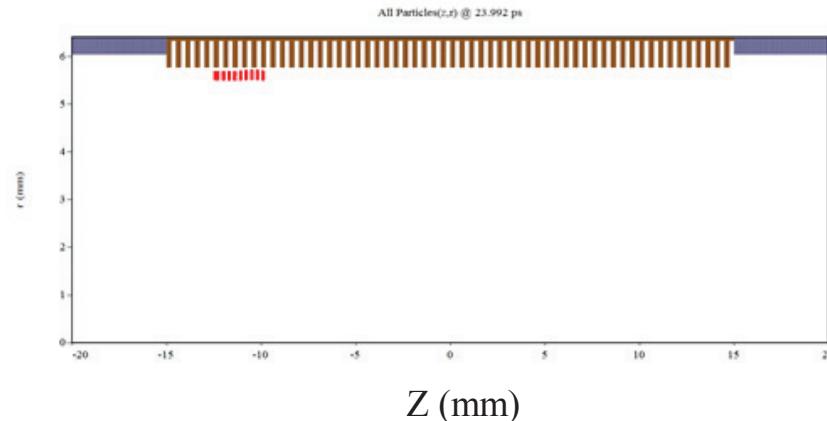
The smallest current is above 3.8A for the AERL configuration

UH-FLUX –THz

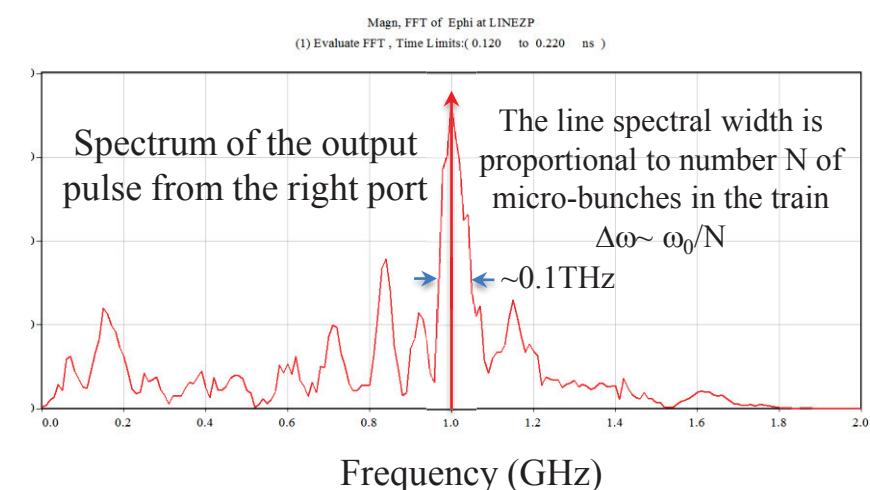
Coherent Smith-Purcell



UH-FLUX –THz Coherent Smith-Purcell

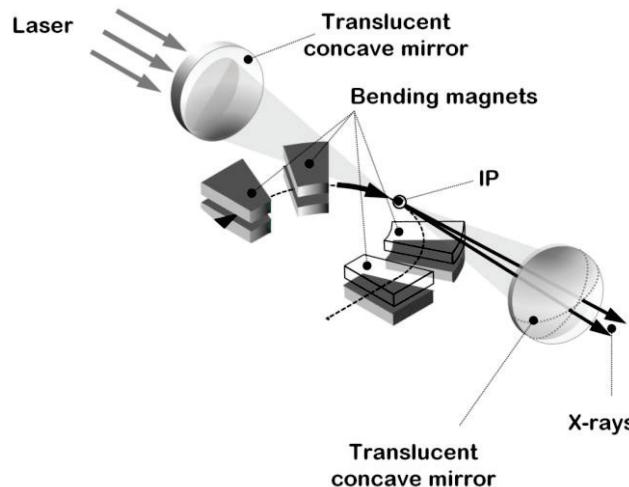


9 Micro-bunches were generated



UH-FLUX – X-ray

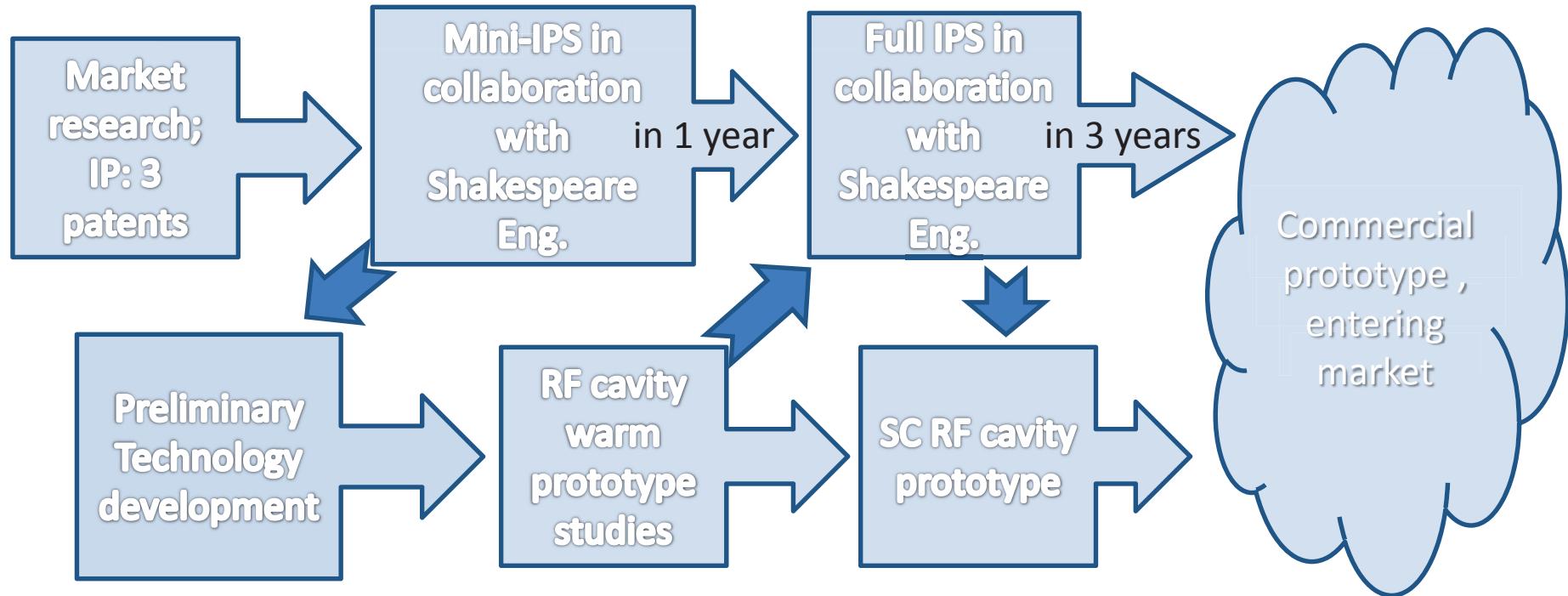
Compton source



- 1/ The peak brightness $\sim 10^{23} - 10^{24}$ photons /($\text{mm}^2 \times \text{mrad}^2 \times \text{s} \times 0.1\%$ bandwidth)
- 2/ X-ray flux $\sim 9 \times 10^{12} - 3 \times 10^{13}$ photons/second inside a 0.1% bandwidth
- 3/ Average brightness $\sim 10^{14}$ photons/($\text{mm}^2 \times \text{mrad}^2 \times \text{s} \times 0.1\%$ bandwidth)
at 15keV photons for 20MeV beam

We are studying the range of possible applications of UH-FLUX technology, including medical direction

UH-FLUX: Asymmetric Energy Recovery Linac – Next steps



1/ PCT international patent application PCT/GB2012/052632 titled 'X-ray Generation' filed on the 24th October 2012.

2/ PCT/GB2013/053101 titled 'Distributed electron beam collector" filed on the 25th November 2013.

3/UK Priority patent application 1420936.5 titled 'Asymmetric superconducting RF structure' filed on the 25th November 2014.

Summary

UH Flux: X-ray/THz compact SCRF AERL Light Source

- Based on novel dual axis asymmetric cavity energy-recovery system
- Energy-recovery SCRF system = increased efficiency
- Asymmetric structure = high current (>1A)
- High current = high flux of THz or X-ray photons
- New distributed electron beam collector – to reduce impact of high current electron beam

Thank you