

1. Convince yourself that:

$$\frac{1}{T} \frac{dT}{dt} = - \frac{\nabla}{H_p}, \text{ where } \nabla = \frac{P}{T} \frac{dT}{dp} \text{ and } H_p \text{ is the pressure scale height.}$$

Use the chain rule and divide & multiply by P :

$$\frac{P}{P} \frac{1}{T} \frac{dT}{dp} \frac{dp}{dr} = \nabla \frac{1}{P} \frac{dp}{dt}$$

Note that the differential

$$d\ln p = \frac{1}{P} dp, \text{ and } \frac{d\ln p}{dt} = \frac{1}{P} \frac{dp}{dt}$$

Pressure scale height:

$$\frac{d\ln p}{dr} = -\frac{1}{H_p} \Rightarrow \int_{P_0}^P d\ln p = - \int_0^r \frac{dr}{H_p}$$

$$\ln \frac{P}{P_0} = -\frac{r}{H_p} \quad || \exp$$

$$\frac{P}{P_0} = \exp \left\{ -\frac{r}{H_p} \right\} \Rightarrow P = P_0 \exp \left\{ -\frac{r}{H_p} \right\}$$

Therefore from above:

$$\frac{1}{T} \frac{dT}{dt} = \nabla \frac{1}{P} \frac{dp}{dt} = - \frac{\nabla}{H_p}$$

2. Show that:

$$\left. \frac{dT}{dt} \right|_a = -\frac{g}{c_p}.$$

Start again with the chain rule:

$$\left. \frac{dT}{dt} \right|_a = \left. \frac{dT}{dp} \right|_a \frac{dp}{dr} = -\left. \frac{dT}{dp} \right|_a sg$$

$$\frac{dp}{dr} = -sg$$

On the other hand:

$$\frac{dT}{dp} \Big|_a = \left(\frac{\partial T}{\partial p} \right)_{dp} \Big|_a \overset{\text{def}}{=} \nabla_a, \text{ and } p = R_{\text{spec}} ST = (c_p - c_v) ST \Leftrightarrow \frac{T}{p} = \frac{1}{(c_p - c_v) S}$$

$$\Rightarrow \frac{dT}{dp} \Big|_a =$$

Substitute above:

$$\frac{dT}{dp} \Big|_a \frac{dp}{dt} = - \frac{dT}{dp} \Big|_a S g = - \frac{\nabla_a}{(c_p - c_v) S} S g.$$

Recall that $\nabla_a = \frac{\gamma - 1}{p}$ and $p = \frac{c_v}{c_p}$:

$$\frac{dT}{dt} \Big|_a = - \frac{\gamma - 1}{p} \frac{1}{(c_p - c_v)} g = - \frac{\gamma - 1}{\frac{c_v}{c_p}} \frac{1}{c_v (\gamma - 1)} g = - \frac{g}{\frac{c_v}{c_p}}.$$

3. Use the 2nd law of thermodynamics

$$ds = \frac{dQ}{T}$$

to show that an adiabatic process is isentropic.

Recall that:

$$dQ = du + p dV = c_v dT - p \frac{dg}{S^2}.$$

Now we have:

$$ds = c_v \frac{dT}{T} - \frac{p}{\gamma} \frac{dg}{S^2}. \quad \text{On the other hand:} \quad \frac{1}{c_p} \frac{dp}{p} = \frac{dg}{S} + \frac{dT}{T} \Rightarrow \frac{dT}{T} = \frac{dp}{p} - \frac{dg}{S}$$

$$\frac{ds}{c_p} = \frac{1}{\gamma} \left(\frac{dp}{p} - \frac{dg}{S} \right) - \frac{p}{c_p T} \frac{dg}{S^2}. \quad ; \quad p = (c_p - c_v) S T \Leftrightarrow \frac{p}{T} = (c_p - c_v) S$$

$$\begin{aligned} \frac{ds}{c_p} &= \frac{1}{\gamma} \left(\frac{dp}{p} - \frac{dg}{S} \right) - \frac{(c_p - c_v) S}{c_p} \frac{dg}{S^2} \\ &= \frac{1}{\gamma} \left(\frac{dp}{p} - \frac{dg}{S} \right) - \left(1 - \frac{1}{\gamma} \right) \frac{dg}{S} \end{aligned}$$

$$= \frac{1}{\gamma} \left(\frac{dp}{p} - \frac{dg}{S} \right) - \left(1 - \frac{1}{\gamma} \right) \frac{dg}{S} = \frac{1}{\gamma} \frac{dp}{p} - \frac{dg}{S}$$

Continued...

$$\frac{ds}{cp} = \frac{1}{p} \frac{dp}{p} - \frac{dg}{g} = \frac{1}{g} (d\ln p - g d\ln g)$$

For an adiabatic process we know that:

$$\frac{g}{p} \frac{dp}{dg} = \frac{d\ln p}{d\ln g} = g \Leftrightarrow d\ln p = g d\ln g.$$

which leads to:

$$\frac{ds}{cp} = 0$$

Show that super-adiabatic T-gradient is related to the specific s-gradient:

$$-\frac{1}{cp} \frac{ds}{dr} = \frac{1}{H_p} (\nabla - \nabla_{ad})$$

Start from:

$$ds = c_v \frac{dT}{T} - \frac{p}{T} \frac{dg}{g^2},$$

and use:

$$\frac{p}{Tg} = c_p - c_v, \text{ and } \frac{dg}{g} = \frac{dp}{p} - \frac{dT}{T},$$

to get

$$ds = c_v \cancel{\frac{dT}{T}} - (c_p - c_v) \left(\frac{dp}{p} - \cancel{\frac{dT}{T}} \right) = c_p \frac{dT}{T} - (c_p - c_v) \frac{dp}{p}$$

Divide by c_p and differentiate w.r.f. r:

$$\begin{aligned} \frac{1}{cp} \frac{ds}{dt} &= \frac{1}{T} \frac{dT}{dt} - \underbrace{\frac{c_p - c_v}{c_v}}_{=1-\frac{1}{g}=\nabla_a} \frac{1}{p} \frac{dp}{dt} = -\frac{\nabla}{H_p} + \frac{\nabla_a}{H_p} \\ &= -\frac{\nabla}{H_p} = 1 - \frac{1}{g} = \nabla_a = -\frac{\nabla}{H_p} \end{aligned}$$

Therefore:

$$\underline{-\frac{1}{cp} \frac{ds}{dt} = \frac{1}{H_p} (\nabla - \nabla_a)}$$

9. Use the N-S equation and definition of F_{conv} to estim. convective velocity and T-fluctuations in the Sun.

$$g \frac{\partial \bar{u}}{\partial t} = - g \bar{u} \cdot \nabla \bar{u} - g \bar{q} + \nabla p + \bar{F}_{\text{visc}} \quad ; \quad F_{\text{conv}} = c_p g u T'$$

- Assume hydrostatic equilibrium on average:

$$\Rightarrow \frac{d\bar{p}}{dr} = \bar{g} g_r .$$

- Then the buoyancy force driving convection is: $\bar{g}' g_r$.

- Assume low internal friction $\Rightarrow \bar{F}_{\text{visc}} \approx 0$.

- Balance the remaining terms:

$$g \bar{u} \cdot \nabla \bar{u} \sim g' \bar{q} \xrightarrow{\text{dom}} \frac{\bar{g} u^2}{H} \sim g' q \Leftrightarrow \frac{u^2}{H} \sim g \frac{g'}{g} \sim g \frac{T'}{T}$$

- Assume convection to transport all of the energy: $F_{\text{conv}} = F_{\text{tot}} = \frac{L}{4\pi r^2}$.

$$T' = \frac{F_{\text{tot}}}{c_p g u}$$

- In combination:

$$\frac{u^2}{H} \sim \frac{g F_{\text{tot}}}{c_p T g u} \xrightarrow{\text{circled}} \Rightarrow u' = \frac{F_{\text{tot}}}{S} ; \text{ or } u = \underline{\underline{\left(\frac{F_{\text{tot}}}{S}\right)^{1/2}}} .$$

- Now the T-fluctuation is:

$$T' = \frac{F_{\text{tot}}}{c_p g u} = \frac{1}{c_p} \underline{\underline{\left(\frac{F_{\text{tot}}}{S}\right)^{1/2}}} .$$

$$F_{\text{tot}} \approx \frac{L_0}{4\pi r^2} \xrightarrow{r=0.85R_\odot} \approx 8 \cdot 10^7 \frac{\text{W}}{\text{m}^2} ; g(r=0.85R_\odot) \approx 55 \frac{\text{kg}}{\text{m}\cdot\text{s}^2} ; c_p \approx 2.07 \cdot 10^4 \frac{\text{J}}{\text{kg}\cdot\text{K}}$$

$$\Rightarrow u \approx 116 \frac{\text{m}}{\text{s}} ; T \approx 0.66 \text{ K} . \quad \text{Think if these make sense!}$$