Tutorial: Active Inference Controller for Dynamic Systems

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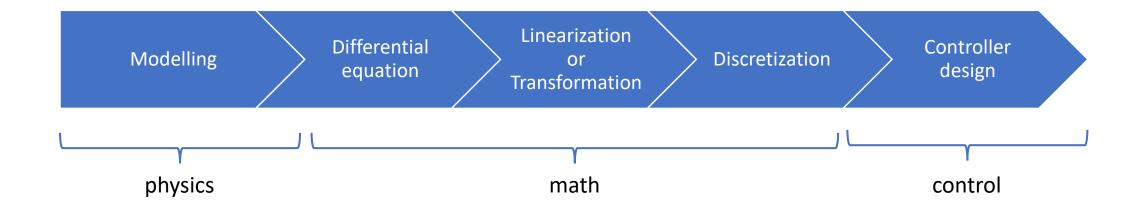




Active inference for robots

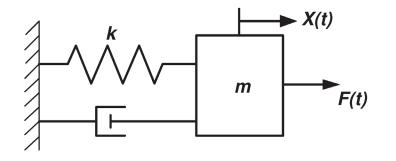
Methodology

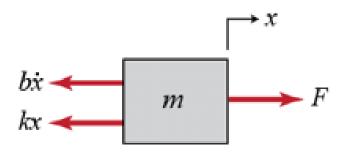




Modelling the dynamic system

Step 1: Derive the equations of motion of the dynamic system





Free body diagram

$$F - b\dot{x} - kx = 0$$

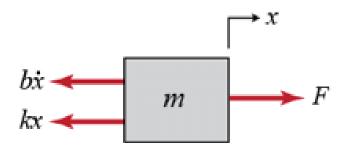
static system

$$F - b\dot{x} - kx = m\ddot{x}$$

dynamic system

Equations of motion to differential equations

Step 2: convert the dynamic model to a differential equation



$$F - b\dot{x} - kx = m\ddot{x}$$

$$m\frac{d^2x}{dt^2} + b\frac{dx}{dt} + kx = F$$

$$\frac{d^2x}{dt^2} + \frac{b}{m}\frac{dx}{dt} + \frac{k}{m}x = \frac{F}{m}$$

Governing equation of motion ——— Differential equations of motion

Linear time invariant (LTI) state space systems

Step 3a: convert the differential equation to an LTI system

$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$y(t) = Cx(t) + Du(t)$$

A, B, C, D are independent of time

$$\frac{d^2x}{dt^2} + \frac{b}{m}\frac{dx}{dt} + \frac{k}{m}x = \frac{F}{m}$$

$$\dot{X} = AX + Bu$$

$$x_1 = x x_2 = \dot{x}$$

$$X = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$\dot{X} = \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} x_2 \\ \ddot{x} \end{bmatrix}$$
$$\ddot{x} = -\frac{b}{m}\dot{x} - \frac{k}{m}x + \frac{F}{m}$$

$$\dot{X} = \begin{bmatrix} x_2 \\ -\frac{b}{m}\dot{x} - \frac{k}{m}x + \frac{F}{m} \end{bmatrix}$$

Linear time invariant state space systems

$$x_{1} = x x_{2} = \dot{x}$$

$$X = \begin{bmatrix} x_{1} \\ x_{2} \end{bmatrix}$$

$$\dot{X} = \begin{bmatrix} \dot{x}_{1} \\ \dot{x}_{2} \end{bmatrix} = \begin{bmatrix} x_{2} \\ \ddot{x} \end{bmatrix}$$

$$\ddot{x} = -\frac{b}{x}\dot{x} - \frac{k}{x}x + \frac{F}{x}$$

$$\dot{X} = \left[-\frac{b}{m} \dot{x} - \frac{k}{m} x + \frac{F}{m} \right]$$

$$\dot{X} = \begin{bmatrix} x_2 \\ -\frac{b}{m}\dot{x} - \frac{k}{m}x + \frac{F}{m} \end{bmatrix} = \begin{bmatrix} x_2 \\ -\frac{b}{m}x_2 - \frac{k}{m}x_1 + \frac{F}{m} \end{bmatrix}$$
$$= \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{b}{m} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1/m \end{bmatrix} F$$

$$\dot{X} = AX + Bu$$

$$\dot{X} = \begin{bmatrix} x_2 \\ -\frac{b}{m}\dot{x} - \frac{k}{m}x + \frac{F}{m} \end{bmatrix} \qquad A = \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{b}{m} \end{bmatrix}, \qquad B = \begin{bmatrix} 0 \\ 1/m \end{bmatrix}, \qquad u = F, \qquad X = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

Linear time invariant state space systems

$$\dot{x} = Ax + Bu$$
$$y = Cx + Du$$

$$\dot{X} = AX + Bu$$

$$A = \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{b}{m} \end{bmatrix}, \qquad B = \begin{bmatrix} 0 \\ 1/m \end{bmatrix}, \qquad u = F, \qquad X = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$y = CX$$
 $y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x \\ \dot{x} \end{bmatrix}$

Observation model

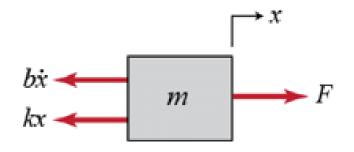
Differential equations

LTI system

LTI systems through linearization

Step 3b: linearize the differential equation to form an LTI system

$$\dot{X} = \begin{bmatrix} x_2 \\ -\frac{b}{m}x_2 - \frac{k}{m}x_1 + \frac{F}{m} \end{bmatrix} = \begin{bmatrix} f_1(X, u) \\ f_2(X, u) \end{bmatrix} \qquad y = x_1 = g(X, u)$$



$$\dot{X} = f(X, u)$$
 $\ddot{X} = f(X, u) = AX + Bu$
 $y = g(X, u)$ $y = g(X, u) = CX + Du$

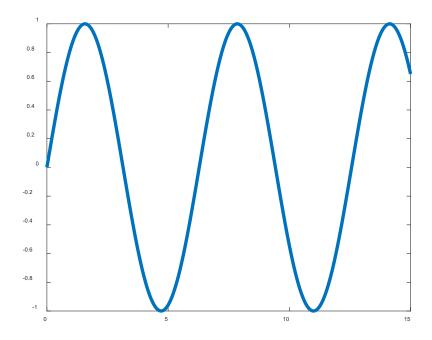
$$A = \frac{\partial f}{\partial X_{\{X = X^e, u = u^e\}}}, \qquad B = \frac{\partial f}{\partial u_{\{X = X^e, u = u^e\}}}, \qquad C = \frac{\partial g}{\partial X_{\{X = X^e, u = u^e\}}}, \qquad D = \frac{\partial g}{\partial u_{\{X = X^e, u = u^e\}}}$$

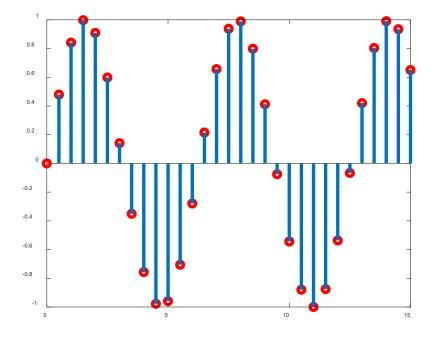
$$A = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} \\ \frac{\partial f_2}{\partial x} & \frac{\partial f_2}{\partial x} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{b}{m} \end{bmatrix}, \qquad B = \begin{bmatrix} \frac{\partial f_1}{\partial u} \\ \frac{\partial f_2}{\partial x} \end{bmatrix} = \begin{bmatrix} 0 \\ 1/m \end{bmatrix}, \qquad C = \begin{bmatrix} \frac{\partial g}{\partial x_1} & \frac{\partial g}{\partial x_2} \end{bmatrix} = \begin{bmatrix} 1 & 0 \end{bmatrix}, \qquad D = \frac{\partial g}{\partial u} = 0$$

Discretization

Step 4: discretize the continuous time model to discrete time model

Why? Because the robot world is discrete!!





Discretization

$$\dot{X} = A_c X + B_c u$$

$$x[t+1] = A_d x[t] + B_d u[t]$$
$$y[t] = C_d x[t] + D_d u[t]$$

$$A_d = e^{A_c \Delta t}$$

$$B_d = A_c^{-1} (A_d - I) B_c$$

$$C_d = C_c, \quad D_d = D_c$$

 $e^{A_c\Delta t}$ is a matrix exponential expm(.) and not exp(.)

$$e^X = \sum_{k=0}^\infty rac{1}{k!} X^k$$

Stability of an LTI system

Step 5: check the stability of the system

The system is stable if the output is finite for all possible finite inputs

$$\dot{X} = A_c X + B_c u$$

The system is asymptotically stable if and only if all the eigen values of A_c are in the left-hand plane

$$\dot{X} = A_d X + B_d u$$

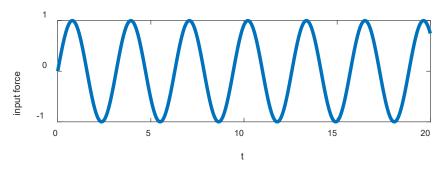
The system is asymptotically stable if and only if all the eigen values of A_d are inside the unit circle

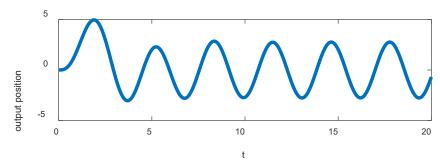
Stability of an SMD system

$$A_c = \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{b}{m} \end{bmatrix}$$

$$m = 0.1kg,$$
 $k = 0.1\frac{N}{m},$ $b = 0.1\frac{Ns}{m},$

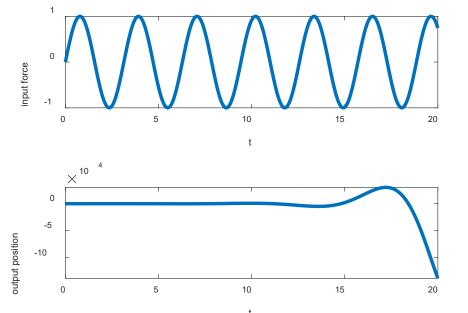
$$eig(A_c) = \{-0.5 + 0.866i, -0.5 - 0.866i\}$$





$$m = 0.1kg,$$
 $k = 0.1\frac{N}{m},$ $b = -0.1\frac{Ns}{m},$

$$eig(A_c) = \{0.5 + 0.866i, 0.5 - 0.866i\}$$



Active Inference controller

Step 6: derive the control law

Take control actions that follow the gradient of free energy

$$\frac{du}{dt} = -\gamma \frac{\partial F}{\partial u}$$

F – free energy γ – learning rate u – control action

$$F = \frac{1}{2}(\tau - \tau^g)^T P^{\tau^g}(\tau - \tau^g) + \frac{1}{2}(u - \eta^u)^T P^u(u - \eta^u) \qquad P^{\tau^g} - \text{goal precision (inverse covariance matrix) of } \tau^g$$

au – task variable au^g - goal for task variable au^{σ^g} - goal precision (inverse covariance matrix) of au^g η^u - prior on control action P^u - prior control precision

Active Inference controller

$$\frac{du}{dt} = -\gamma \frac{\partial F}{\partial u}$$

$$F = \frac{1}{2} (\tau - \tau^g)^T P^{\tau^g} (\tau - \tau^g) + \frac{1}{2} (u - \eta^u)^T P^u (u - \eta^u)$$

 $\eta^u = 0$ with high P^u forces the controller to minimize the control action $\eta^u = 0$ with low P^u allows the controller to explore

$$\frac{du}{dt} = -\gamma \frac{\partial F}{\partial \tau} \frac{\partial \tau}{\partial u} + \frac{\partial F}{\partial u} \qquad \qquad \frac{\partial F}{\partial \tau} = (\tau - \tau^g)^T P^{\tau^g} \qquad \qquad \frac{\partial F}{\partial u} = (u - \eta^u)^T P^u$$

$$\frac{\partial F}{\partial \tau} = (\tau - \tau^g)^T P^{\tau^g}$$

$$\frac{\partial F}{\partial u} = (u - \eta^u)^T P^u$$

System dynamics

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

Active inference control for position control

$$\frac{du}{dt} = -\gamma \frac{\partial F}{\partial \tau} \frac{\partial \tau}{\partial u} \qquad \tau = x \qquad \frac{du}{dt} = -\gamma \frac{\partial F}{\partial x} \frac{\partial x}{\partial u} + \frac{\partial F}{\partial u}$$
$$F = \frac{1}{2} (x - x^g)^T P^{x^g} (x - x^g) + \frac{1}{2} (u - \eta^u)^T P^u (u - \eta^u)$$

$$\dot{x} = Ax + Bu$$

$$\frac{\partial \dot{x}}{\partial u} = A \frac{\partial x}{\partial u} + B, \qquad \frac{\partial \dot{x}}{\partial u} = 0 \Rightarrow \frac{\partial x}{\partial u} = -A^{-1}B$$

$$\frac{du}{dt} = -\gamma \left(\frac{\partial F}{\partial x} \frac{\partial x}{\partial u} + \frac{\partial F}{\partial u} \right) = -\gamma \left((x - x^g)^T P^{x^g} A^{-1} B + u^T P^u \right)$$

Active inference control for velocity control

$$\frac{du}{dt} = -\gamma \frac{\partial F}{\partial \tau} \frac{\partial \tau}{\partial u} \qquad \tau = \dot{x} \qquad \frac{du}{dt} = -\gamma \frac{\partial F}{\partial x} \frac{\partial \dot{x}}{\partial u} + \frac{\partial F}{\partial u}$$
$$F = \frac{1}{2} (\dot{x} - \dot{x}^g)^T P^{\dot{x}^g} (\dot{x} - \dot{x}^g) + \frac{1}{2} (u - \eta^u)^T P^u (u - \eta^u)$$

$$\dot{x} = Ax + Bu$$

$$\frac{\partial \dot{x}}{\partial u} = A \frac{\partial x}{\partial u} + B, \qquad \frac{\partial x}{\partial u} = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \Rightarrow \frac{\partial \dot{x}}{\partial u} = A \begin{bmatrix} 1 \\ 1 \end{bmatrix} + B$$

$$\frac{du}{dt} = -\gamma \left(\frac{\partial F}{\partial x} \frac{\partial \dot{x}}{\partial u} + \frac{\partial F}{\partial u} \right) = -\gamma \left((\dot{x} - \dot{x}^g)^T P^{\dot{x}^g} \left(A \begin{bmatrix} 1 \\ 1 \end{bmatrix} + B \right) + u^T P^u \right)$$

Discretization of the controller

 $u(t + \Delta t) = u(t) - \gamma \frac{\partial F}{\partial u} \Delta t$

Step 7: discretize the control law for discrete time update rule

Euler method

$$u(t + \Delta t) = u(t) + \left(e^{\left(-k\frac{\partial^2 F}{\partial u^2}\Delta t\right)} - I\right)\left(\frac{\partial^2 F}{\partial u^2}\right)^{-1} \frac{\partial F}{\partial u}$$

Unknowns: $\frac{\partial F}{\partial u}$, $\frac{\partial^2 F}{\partial u^2}$

Position control:

$$F = \frac{1}{2}(x - x^g)^T P^{x^g}(x - x^g) + \frac{1}{2}(u - \eta^u)^T P^u(u - \eta^u)$$

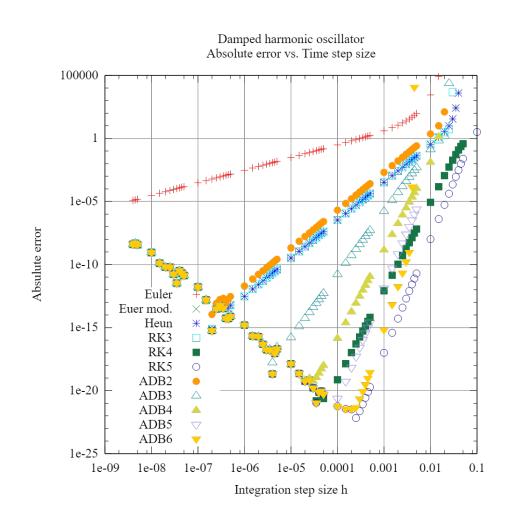
$$\frac{\partial F}{\partial u} = (x - x^g)^T P^{xg} A^{-1} B + u^T P^u$$
$$\frac{\partial^2 F}{\partial u^2} = (A^{-1} B)^T P^{xg} A^{-1} B + P^u$$

Velocity control:

$$F = \frac{1}{2}(\dot{x} - \dot{x}^g)^T P^{\dot{x}^g}(\dot{x} - \dot{x}^g) + \frac{1}{2}(u - \eta^u)^T P^u(u - \eta^u)$$

$$\frac{\partial F}{\partial u} = (\dot{x} - \dot{x}^g)^T P^{\dot{x}^g} \left(A \begin{bmatrix} 1 \\ 1 \end{bmatrix} + B \right) + u^T P^u$$
$$\frac{\partial^2 F}{\partial u^2} = \left(A \begin{bmatrix} 1 \\ 1 \end{bmatrix} + B \right)^T P^{\dot{x}^g} \left(A \begin{bmatrix} 1 \\ 1 \end{bmatrix} + B \right) + P^u$$

Pitfalls of discretization



Active inference controller for dynamic systems

- Step 1: model the motion of the system
- Step 2: convert the dynamic model to a differential equation
- Step 3a: convert the differential equation to an LTI system
- Step 3b: linearize the differential equation to form an LTI system
- Step 4: discretize the continuous time model to discrete time model
- Step 5: check the stability of the system
- Step 6: derive the control law
- Step 7: discretize the control law for discrete time update rule

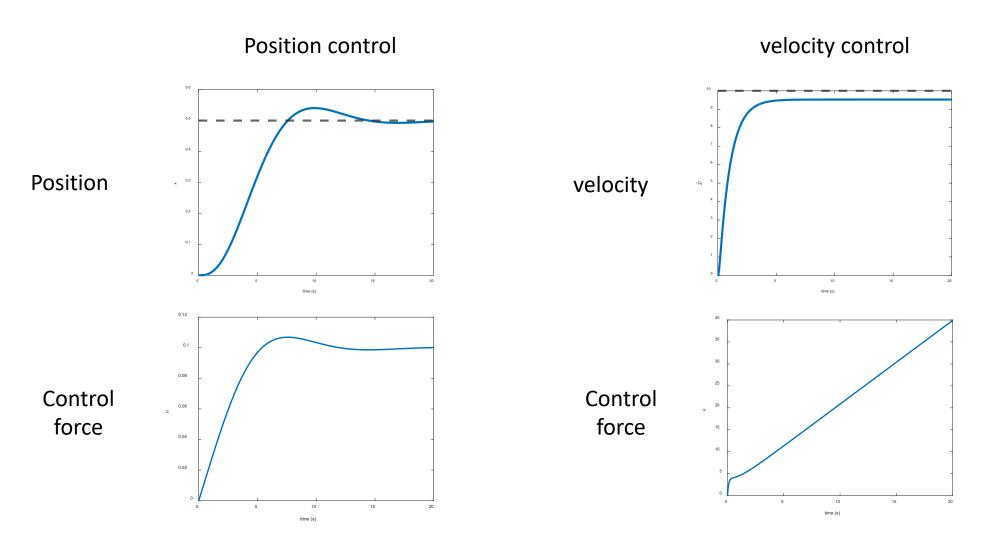
MATLAB implementation

```
% Define the model
model.A = [0 1; -k/m -b/m];
                                 model.B = [0; 1/m]; model.C = [1 0];
% define all the required variables
Pa = .00001*eye(nu); Pi g = diag([.01 .01]); goal x = [.5; 0]; k h = 1; dt = .01; nt = 2000;
% discretize the system
sys d = c2d(ss(model.A, model.B, model.C, []), dt, 'zoh');
for i = 1:nt
        dFda = (brain.x - goal x).'*Pi g*(-pinv(model.A)*model.B) + Pa*a(:,i-1);
        dFdaa = (-pinv(model.A) *model.B).'*Pi g*(-pinv(model.A) *model.B) + Pa;
        a(:,i) = a(:,i-1) + (expm(-k*dFdaa*dt)-eye(ny))*pinv(dFdaa)*dFda;
        % Generative process - take action in the world
        model.x(:,i+1) = sys d.A*model.x(:,i) + sys d.B*a(:,i);
end
```

Running code: https://github.com/ajitham123/mTAIC_IWAI2023

Ajith Anil Meera and Pablo Lanillos, "Towards metacognitive robot decision making for tool selection" IWAI 2023.

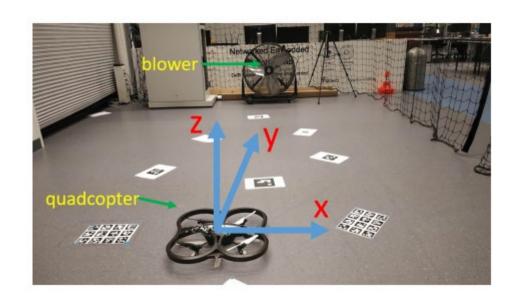
Active inference to control an SMD



Ajith Anil Meera and Pablo Lanillos, "Towards metacognitive robot decision making for tool selection" IWAI 2023.

Active inference for robots

Modelling: Quadrotors as LTI system



$$\dot{\mathbf{x}} = A\mathbf{x} + B\mathbf{v} + \mathbf{w}$$
$$\mathbf{y} = C\mathbf{x} + \mathbf{z}.$$

$$\begin{bmatrix} \dot{\phi} \\ \ddot{\phi} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \phi \\ \dot{\phi} \end{bmatrix} + \begin{bmatrix} 0 & 0 & 0 & 0 \\ \frac{c_{B\phi}}{I_{xx}} & -\frac{c_{B\phi}}{I_{xx}} & -\frac{c_{B\phi}}{I_{xx}} & \frac{c_{B\phi}}{I_{xx}} \end{bmatrix} \begin{bmatrix} pwm_1 \\ pwm_2 \\ pwm_3 \\ pwm_4 \end{bmatrix}$$

$$y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \phi \\ \dot{\phi} \end{bmatrix}$$

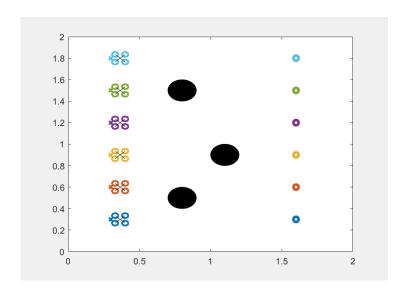
 ϕ and $\dot{\phi}$ are roll angle and roll velocity Pwm are the input signals to the rotors

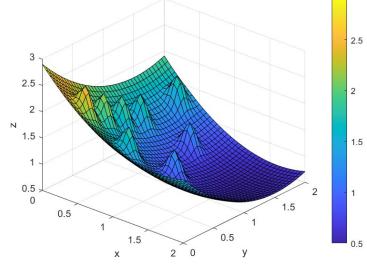
Active inference for robot navigation

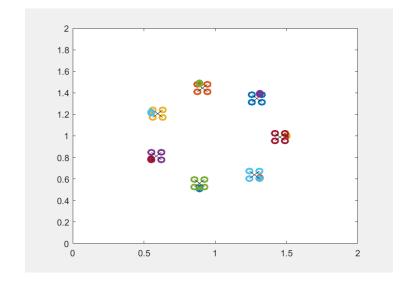
$$F^{g} = \frac{1}{2}(x - x^{g})^{T} P^{x^{g}}(x - x^{g}) + \frac{1}{2}(y - y^{g})^{T} P^{y^{g}}(y - y^{g})$$

$$F = F^g + F^{os} + F^{od}$$

$$\frac{\partial u^{x}}{\partial t} = -\gamma \frac{\partial F}{\partial x} \frac{\partial x}{\partial u^{x}} = -\gamma \frac{\partial F}{\partial x}$$







Static obstacles

Free energy

Dynamic obstacles

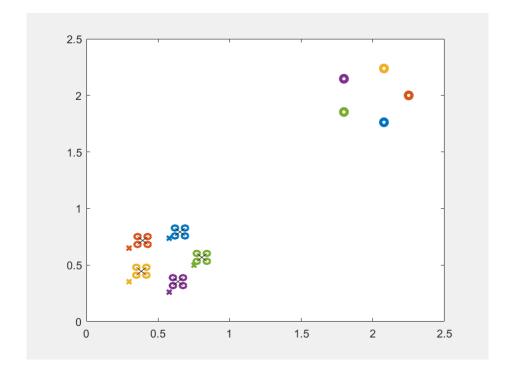
[&]quot;Free Energy Principle Based Precision Modulation for Robot Attention: towards brain inspired robot intelligence", PhD thesis, Department of Cognitive Robotics, TU Delft, 2023

Multi robot navigation in formation

- Expects to reach the goal
- Expects to avoid obstacles
- Expects to keep the formation

$$F = F^g + F^{os} + F^{od} + F^f$$

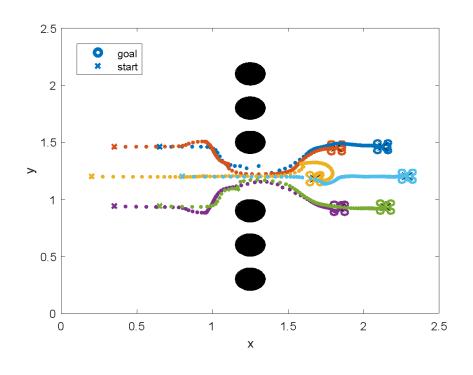
$$F^{f} = \frac{1}{2} \Pi^{f} \sum_{i=1}^{n} \sum_{j=i+1}^{n} \left(||p^{j} - p^{i}|| - ||pf^{j} - pf^{i}|| \right)^{2}$$

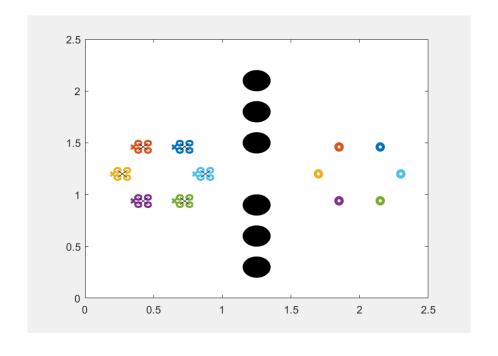


 p^i and p^j are position vector of drone i and j p^{fi} and p^{fj} are the initial position vector of drone i and j

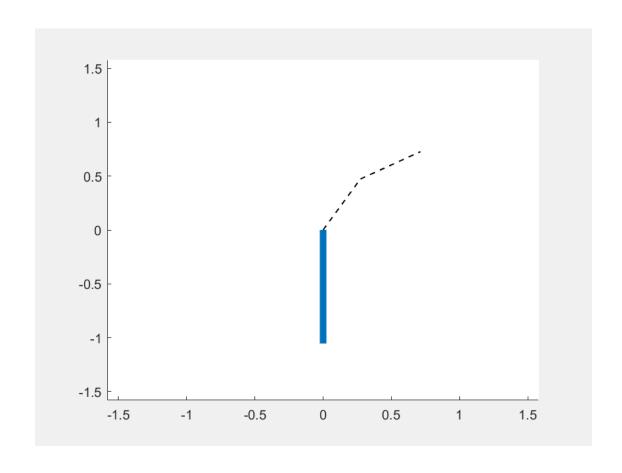
[&]quot;Free Energy Principle Based Precision Modulation for Robot Attention: towards brain inspired robot intelligence", PhD thesis, Department of Cognitive Robotics, TU Delft, 2023

Escape manoeuvre for tight spaces





Active Inference on a 2DOF robot arm



Thank you



Martijn Wisse, TU Delft



Pablo Lanillos, Radboud University