

UESTC3001 Dynamics & Control
Lecture 6

Characteristics and Performance of Feedback Control Systems – II

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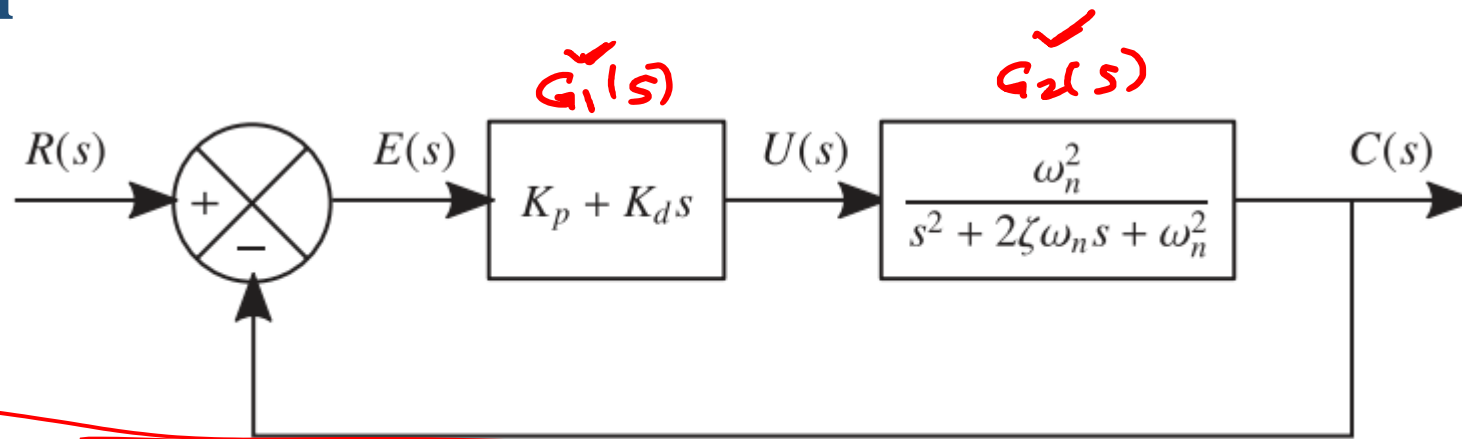
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Outline

- Proportional + Derivative Control of a Second-Order System and Effect on a Second-Order System
- Integral Control of a First-Order/Second-Order System and Effect on a First-Order/Second-Order System
- Proportional + Integral Control of a First-Order System and Effect on a First-Order System
- Proportional + Derivative + Integral Control of a First-Order /Second-Order System and Effect on a First-Order System

Proportional Plus Derivative (PD) Control of a Second-Order System



$$\frac{C(s)}{R(s)} = \frac{G_1(s)G_2(s)}{1 + G_1(s)G_2(s)}$$

$$R(s) = \frac{1}{s}$$

$$\frac{C(s)}{R(s)} = \frac{(K_p + K_d s) \omega_n^2}{s^2 + (2\zeta \omega_n + K_d \omega_n^2) s + (1 + K_p) \omega_n^2}$$

$$C_{ss} = \lim_{s \rightarrow 0} s C(s) = \lim_{s \rightarrow 0} s \times \frac{1}{s} \times \frac{(K_p + K_d s) \omega_n^2}{s^2 + (2\zeta \omega_n + K_d \omega_n^2) s + (1 + K_p) \omega_n^2}$$

$$= \frac{K_p \omega_n^2}{(1 + K_p) \omega_n^2} = \frac{K_p}{1 + K_p}$$

$$\frac{E(s)}{R(s)} = \frac{1}{1 + G_1(s)G_2(s)}$$

$$R(s) = \frac{1}{s}$$

$$\frac{E(s)}{R(s)} = \frac{s^2 + 2\xi\omega_n s + \omega_n^2}{s^2 + (2\xi\omega_n + K_d\omega_n^2)s + (1 + K_p)\omega_n^2}$$

$$e_{ss} = \lim_{s \rightarrow 0} s E(s) = \lim_{s \rightarrow 0} s \times \frac{1}{s} \times \frac{s^2 + 2\xi\omega_n s + \omega_n^2}{s^2 + (2\xi\omega_n + K_d\omega_n^2)s + (1 + K_p)\omega_n^2}$$

↓ 0

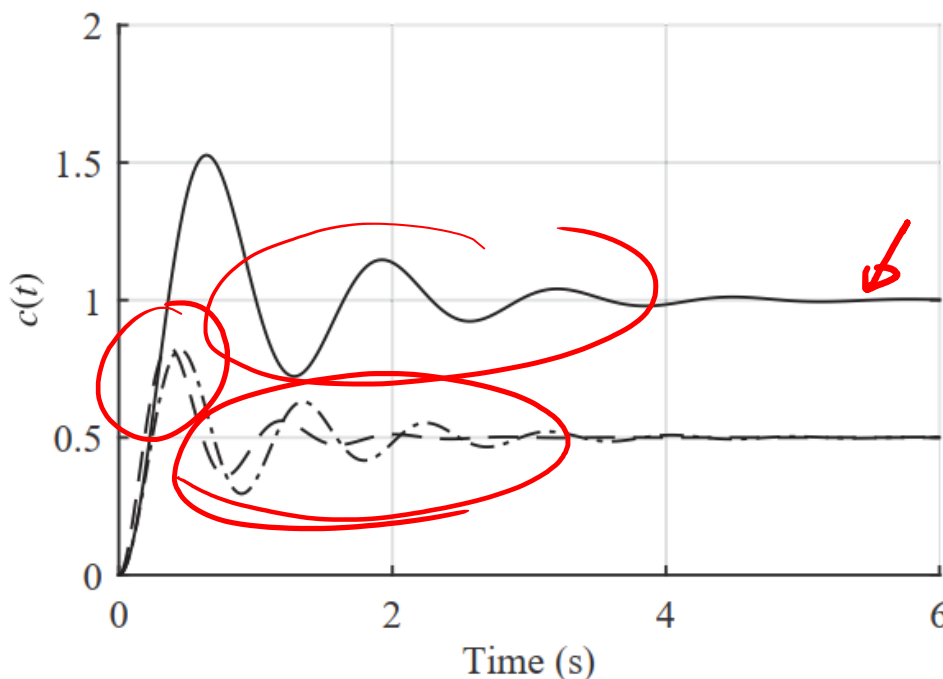
$$= \frac{\cancel{\omega_n^2}}{(1 + K_p)\cancel{\omega_n^2}}$$

$$= \left(\frac{1}{1 + K_p} \right) //$$

Effect of Proportional Plus Derivative (PD) Control on a Second-Order System

$$s^2 + 2\zeta_{cl}\omega_{n,cl}s + \omega_{n,cl}^2 = 0$$

$$c(t) = \frac{K_p}{K_p + 1} \left[1 - e^{-\zeta_{cl}\omega_{n,cl}t} \left(\cos \omega_{d,cl}t + \frac{K_p\zeta_{cl} - K_d\omega_{n,cl}}{K_p \sqrt{1 - \zeta_{cl}^2}} \sin \omega_{d,cl}t \right) \right]$$



— Open-loop - - - Prop. con. ($K_p = 1$)
 - - - PD control ($K_p = 1, K_d = 0.1$)

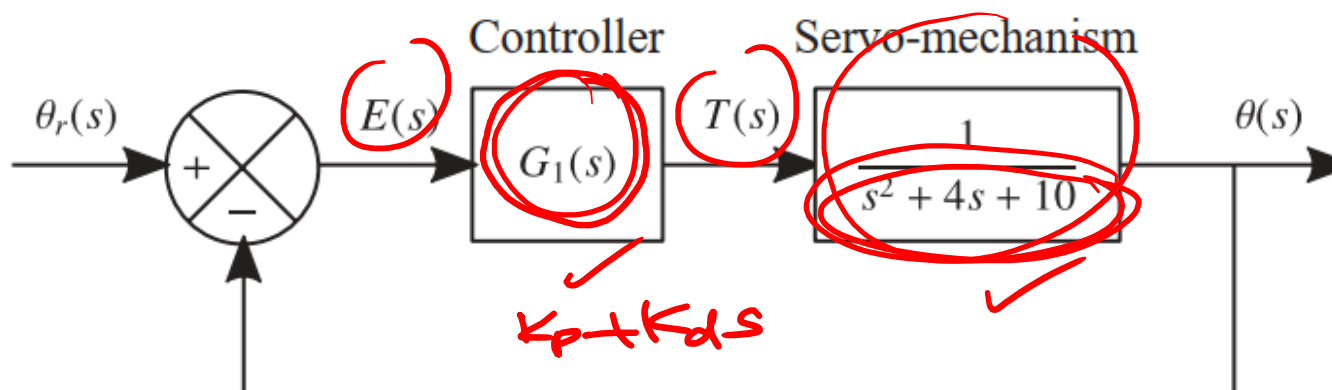
$$\omega_{n,cl} = \omega_n \sqrt{K_p + 1}$$

$$\zeta_{cl} = \frac{\zeta + \frac{1}{2}K_d\omega_n}{\sqrt{K_p + 1}}$$

Exercise 1

The angular output of a servo-mechanism θ is controlled as indicated in the figure below where θ_r is the required (reference) displacement. The controller transfer function is given by $G_1(s)$, the torque it applies to the servo-mechanism is denoted by $T(s)$ and the error signal $E(s)$.

- (a) Calculate the damping and natural frequency of the uncontrolled open-loop system. What is the maximum overshoot of the uncontrolled system in response to a unit step change in torque $T(s)$?
- (b) Proportional control with gain $K_p = 10$ is applied. Calculate the closed-loop natural frequency and damping. What is the steady state error in response to a unit step input in $\theta_r(s)$? Calculate the resulting maximum overshoot.
- (c) Derivative action with gain $K_d = 4$ is now added to the proportional action. Calculate the closed-loop natural frequency and damping. What is the steady state error in response to a unit step input in $\theta_r(s)$? Calculate the resulting maximum overshoot.



$$O/L \ T/f = G_1(s)G_2(s) = G_1(s) \cdot \frac{1}{s^2 + 4s + 10}$$

$$ch \ e \Rightarrow s^2 + \underline{4}s + \underline{10} = 0$$

$$s^2 + \underline{2\zeta\omega_n}s + \underline{\omega_n^2} = 0$$

$$\omega_n^2 = 10 \Rightarrow \omega_n = \underline{3.162} \text{ rad/s}$$

$$2\zeta\omega_n = 4 \Rightarrow \zeta = \frac{4}{2 \times 3.162} = \underline{0.6325}$$

$$M_p = \underline{100} e^{-\zeta\omega_n t_p} (\%)$$

$$\omega_d = \omega_n \sqrt{1 - \zeta^2}$$

$$M_p = \underline{e^{-\left(\frac{\pi\zeta}{\sqrt{1-\zeta^2}}\right)}}$$

$$t_p = \frac{\pi}{\omega_d}$$

$$\omega_d = \omega_n \sqrt{1 - \zeta^2}$$

$$t_s = \frac{3}{\zeta\omega_n} = \frac{3}{0.6325 \times 3.162} = \underline{1.5 \text{ s}}$$

$$\omega_d = 2.4492$$

$$M_p = \underline{e^{-\left(\frac{\pi \times 0.6325}{\sqrt{1 - 0.6325^2}}\right)}} = 7.6892\%$$

$$t_p = \frac{\pi}{\omega_d} = 1.2827 \text{ s}$$

b)

$$C/L \ T/f = \frac{G_1(s) G_2(s)}{1 + G_1(s) G_2(s)} = \frac{10 \times \left(\frac{1}{s^2 + 4s + 10} \right)}{1 + 10 \times \left(\frac{1}{s^2 + 4s + 10} \right)} = \frac{10}{s^2 + 4s + 20}$$

$$s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$$

$$s^2 + 4s + 20 = 0$$

$$\omega_n^2 = 20 \Rightarrow \omega_n = 4.472 \text{ rad/s}$$

$$2\zeta\omega_n = 4 \Rightarrow \zeta = \frac{4}{2 \times 4.472} = 0.4472$$

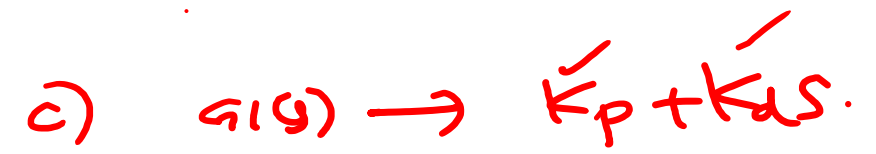
$$\frac{E(s)}{R(s)} = \frac{1}{1 + G_1(s) G_2(s)} = \left(\frac{s^2 + 4s + 10}{s^2 + 4s + 20} \right)$$

$$E(s) = \frac{1}{s} \times \left(\frac{s^2 + 4s + 10}{s^2 + 4s + 20} \right)$$

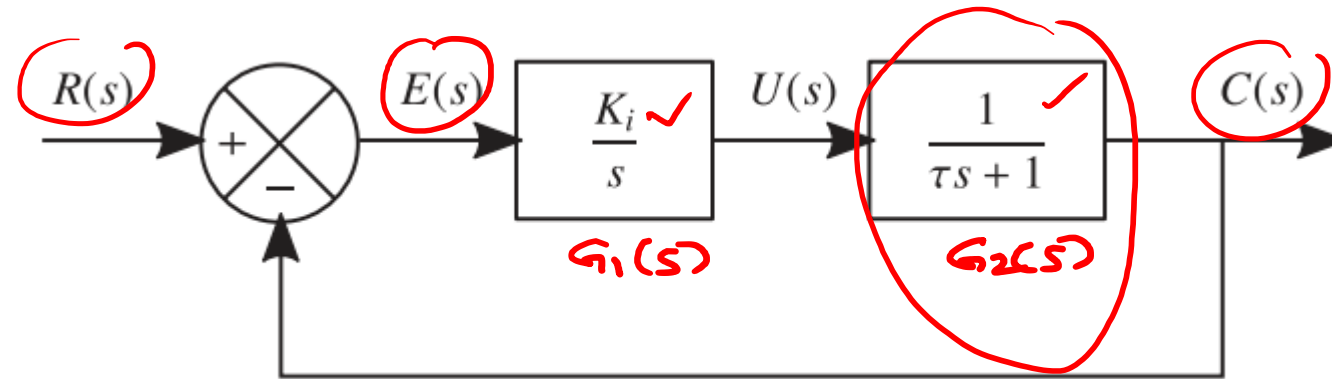
$$R_{ss} = \lim_{s \rightarrow 0} s E(s) = \lim_{s \rightarrow 0} s \times \frac{1}{s} \left(\frac{s^2 + 4s + 10}{s^2 + 4s + 20} \right) = \frac{10}{20}$$

$$= 0.5$$

$$M_p = 20.789 \%$$



Integral Control of a First-Order System



$$\frac{C(s)}{R(s)} = ?$$

$$\frac{E(s)}{R(s)} = ?$$

$$R(s) = 1/s$$

$$\downarrow$$

$$C_{ss} ? \quad E_{ss} ?$$

$$\frac{C(s)}{R(s)} = \frac{G_1 G_2}{1 + G_1 G_2} = \frac{K_i}{\tau s^2 + s + K_i}$$

$$R(s) = 1/s$$

$$C(s) = \frac{1}{s} \left(\frac{K_i}{\tau s^2 + s + K_i} \right)$$

$$C_{ss} = \lim_{s \rightarrow 0} s C(s) = \lim_{s \rightarrow 0} s \times \frac{1}{s} \times \left(\frac{K_i}{\tau s^2 + s + K_i} \right) = \frac{K_i}{K_i}$$

$$= 1$$

$$\frac{E(s)}{R(s)} = \frac{1}{1 + G_1 G_2} = \frac{s(\tau s + 1)}{\tau s^2 + s + K_i}$$

1/s

$$E(s) = \frac{1}{s} \frac{s(\tau s + 1)}{\tau s^2 + s + K_i}$$

$$e_{ss} = \lim_{s \rightarrow 0} s E(s) = \lim_{s \rightarrow 0} \cancel{s} \times \frac{1}{\cancel{s}} \times \frac{s(\tau s + 1)}{\tau s^2 + s + K_i} = \frac{0}{K_i}$$

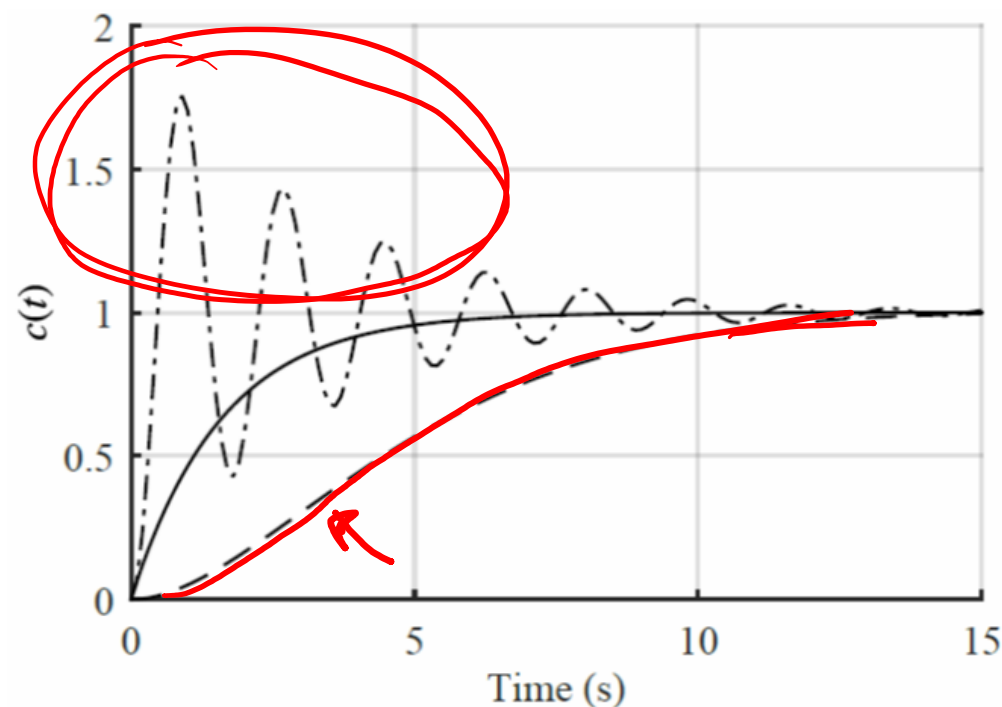
$$= 0$$

Effect of Integral Control on a First-Order System

$$s^2 + 2\zeta_{cl}\omega_{n,cl}s + \omega_{n,cl}^2 = 0$$

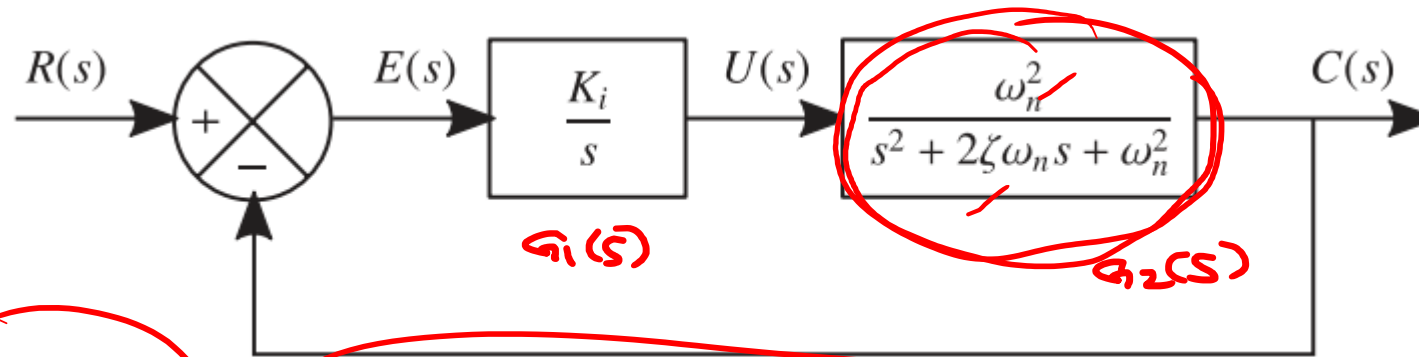
$$\omega_{n,cl} = \sqrt{\frac{K_i}{\tau}}$$

$$\zeta_{cl} = \frac{1}{2\sqrt{\tau K_i}}$$



— Open-loop - - - - Integral con. ($K_i = 20$)
 - . - - Integral con. ($K_i = 0.2$)

Integral Control of a Second-Order System



$$\frac{C(s)}{R(s)} = \frac{G_1 G_2}{1 + G_1 G_2} = \frac{K_i \omega_n^2}{s^3 + 2\zeta \omega_n s^2 + \omega_n^2 s + K_i \omega_n^2}$$

$$R(s) = \frac{1}{s} \Rightarrow C(s) = \frac{1}{s} \times \left(\frac{K_i \omega_n^2}{s^3 + 2\zeta \omega_n s^2 + \omega_n^2 s + K_i \omega_n^2} \right)$$

$$C_{ss} = \lim_{s \rightarrow 0} s C(s) = \lim_{s \rightarrow 0} s \times \frac{1}{s} \times \frac{K_i \omega_n^2}{s^3 + 2\zeta \omega_n s^2 + \omega_n^2 s + K_i \omega_n^2}$$

$$= \frac{K_i \omega_n^2}{K_i \omega_n^2} = 1$$

$$\frac{E(s)}{R(s)} = \frac{1}{1 + G_1 G_2} = \left(\frac{s(s^2 + 2\zeta\omega_n s + \omega_n^2)}{s^3 + 2\zeta\omega_n s^2 + \omega_n^2 s + K_i \omega_n^2} \right)$$

$$R(s) = \frac{1}{s} \Rightarrow E(s) = \frac{1}{s} \times ()$$

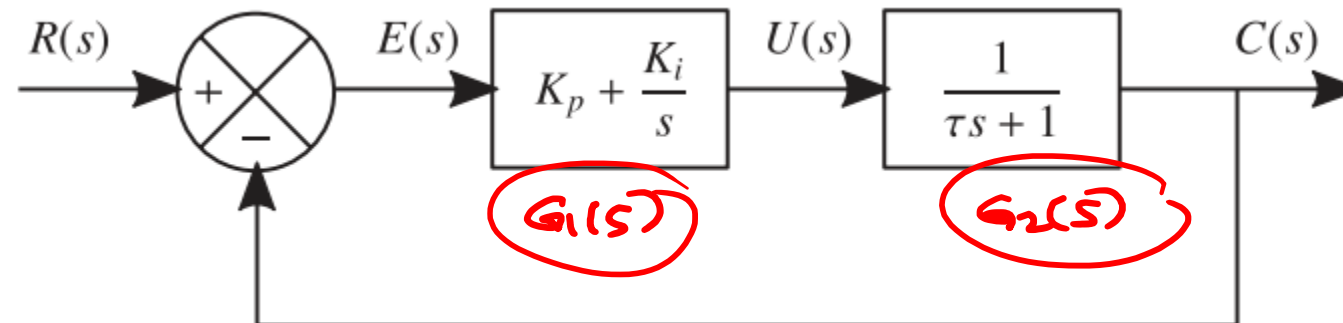
$$P_{ss} = \lim_{s \rightarrow 0} s E(s) = \lim_{s \rightarrow 0} s \times \frac{1}{s} \times \frac{s(s^2 + 2\zeta\omega_n s + \omega_n^2)}{s^3 + 2\zeta\omega_n s^2 + \omega_n^2 s + K_i \omega_n^2}$$

\downarrow
 0

$$= \frac{0}{K_i \omega_n^2}$$

$$= 0$$

PI Control of a First-Order System



$$\frac{C(s)}{R(s)} = \frac{G_1 G_2}{1 + G_1 G_2} = \frac{K_p s + K_i}{s^2 + (K_p + 1)s + K_i}$$

$$P(s) = \frac{1}{s}$$

$$C_{ss} = 1$$

$$\frac{E(s)}{R(s)} = \frac{1}{1 + G_1 G_2} = \frac{s(zs + 1)}{zs^2 + (K_p + 1)s + K_i}$$

$\frac{1}{s}$ ✓

$E(s)$ ✓

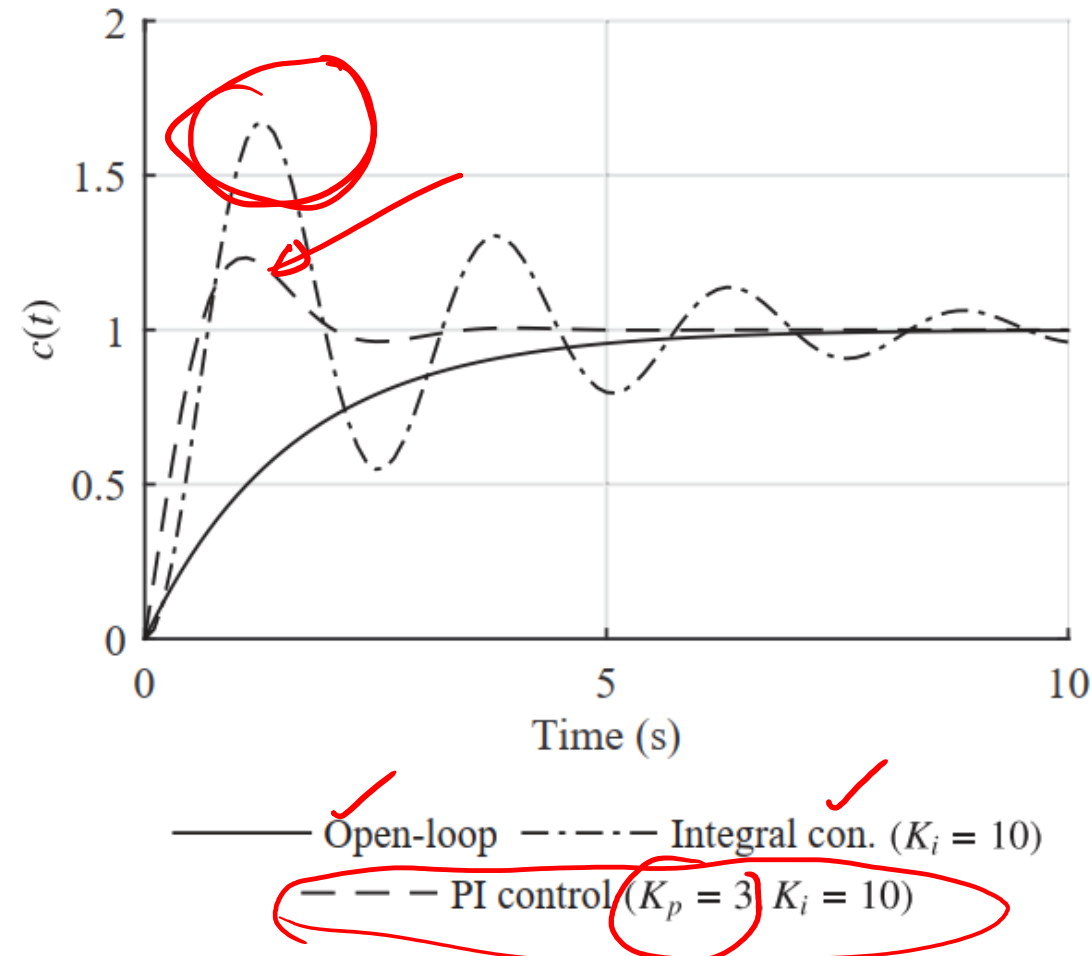
$R_{ss} = 0$

Effect of PI Control on a First-Order System

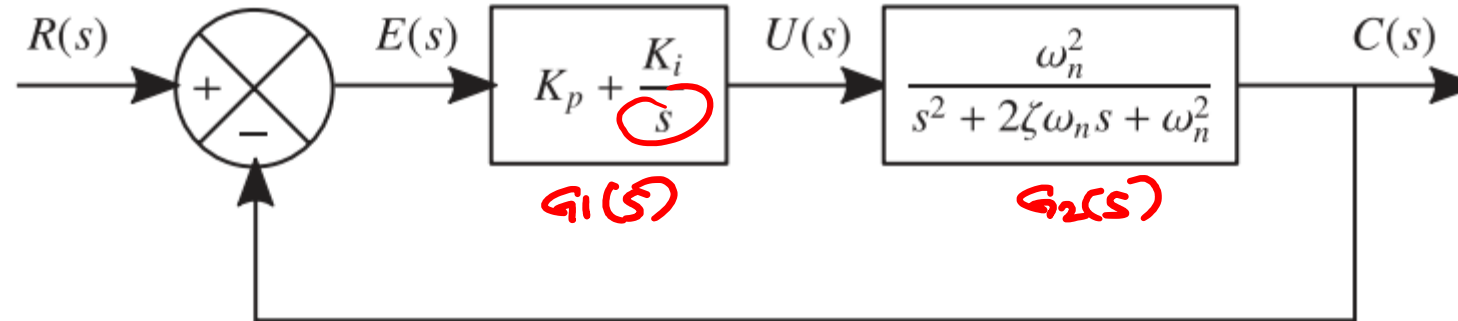
$$s^2 + 2\zeta_{cl}\omega_{n,cl}s + \omega_{n,cl}^2 = 0$$

$$\omega_{n,cl} = \sqrt{\frac{K_i}{\tau}}$$

$$\zeta_{cl} = \frac{K_p + 1}{2\sqrt{\tau K_i}}$$



PI Control of a Second-Order System



$$\frac{C(s)}{R(s)} = \frac{(K_i + K_p s) \omega_n^2}{s^3 + 2\zeta \omega_n s^2 + \omega_n^2 (K_p + 1) s + K_i \omega_n^2}$$

$$R(s) = 1/s$$

$$C_{ss} = 1$$

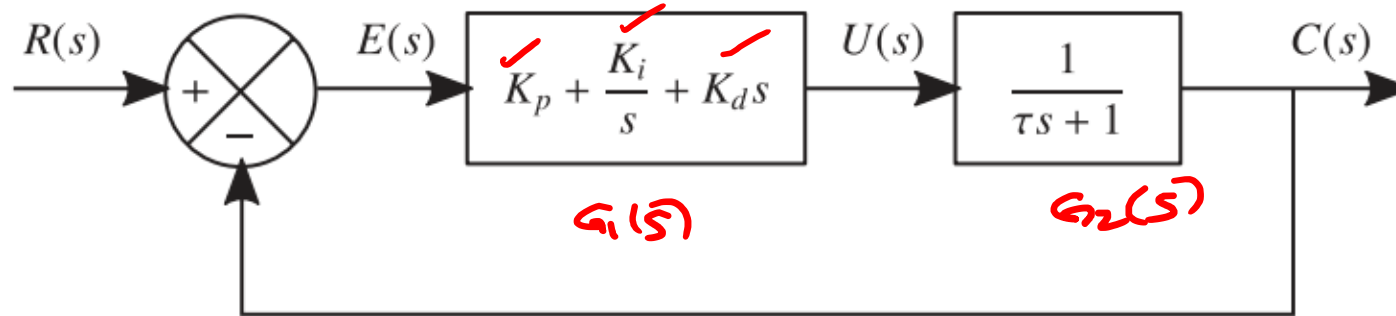
$$\frac{E(s)}{R(s)} = \frac{s(s^2 + 2\zeta\omega_n s + \omega_n^2)}{s^3 + 2\zeta\omega_n s^2 + \omega_n^2(K_p + 1)s + K_i\omega_n^2}$$

\swarrow
 $1/s$

$E(s)$ ✓

$p_{ss} = 0$

PID Control of a First-Order System



$$\frac{C(s)}{R(s)} = \frac{K_d s^2 + K_p s + K_i}{(z + 1)s^2 + (K_p + 1)s + K_i}$$

$\leftarrow \frac{1}{s}$

$$C_{ss} = 1$$

$$Y_S \leftarrow \frac{E(s)}{R(s)} = \frac{s(zs+1)}{(z+k_d)s^2 + (k_p+1)s + k_i}$$

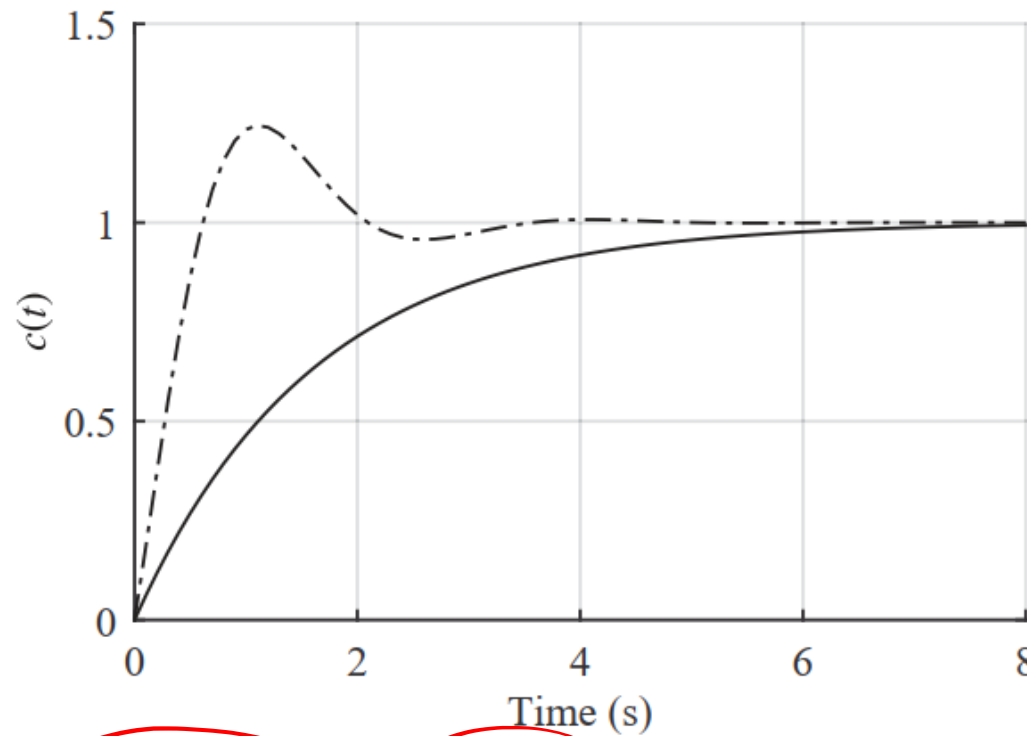
$e_{ss} = 0$

Effect of PID Control on a First-Order System

$$s^2 + 2\zeta_{cl}\omega_{n,cl}s + \omega_{n,cl}^2 = 0$$

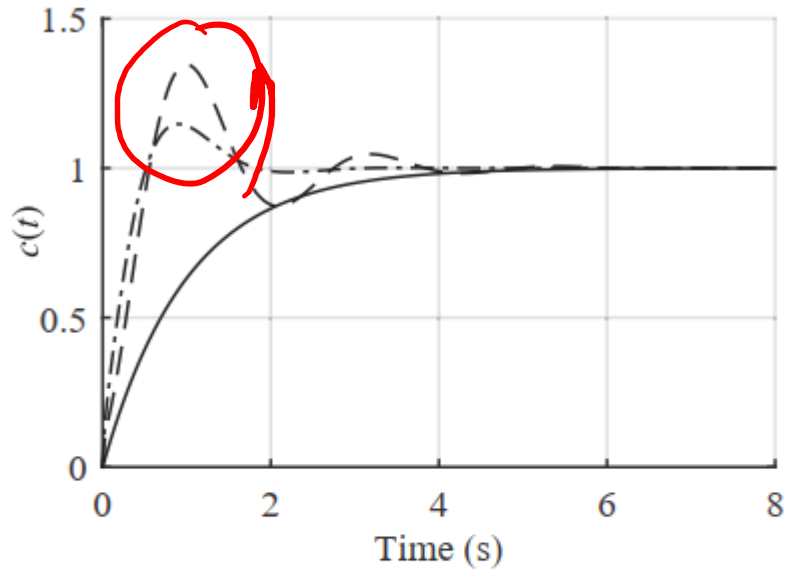
$$\omega_{n,cl} = \sqrt{\frac{K_i}{\tau + K_d}}$$

$$\zeta_{cl} = \frac{K_p + 1}{2\sqrt{K_i(\tau + K_d)}}$$



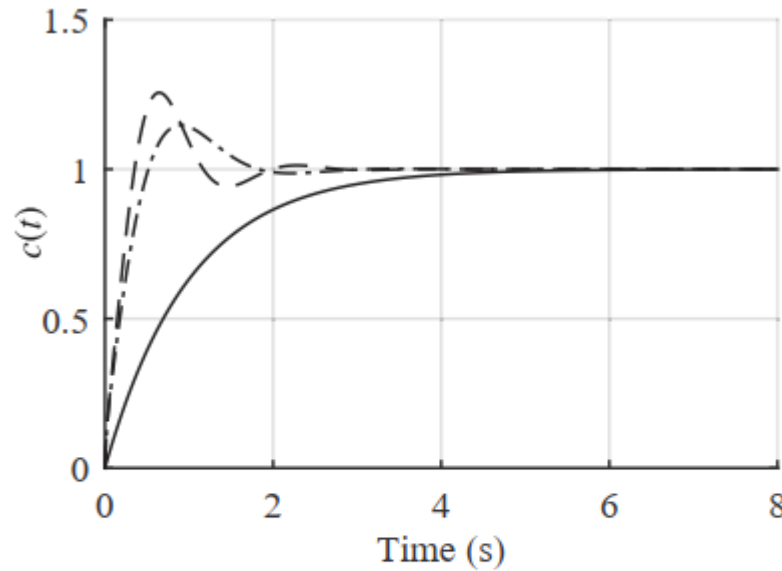
— Open-loop
- - - PID control ($K_p = 3, K_i = 10, K_d = 0.1$)

Effect of PID Control on a First-Order System cont.



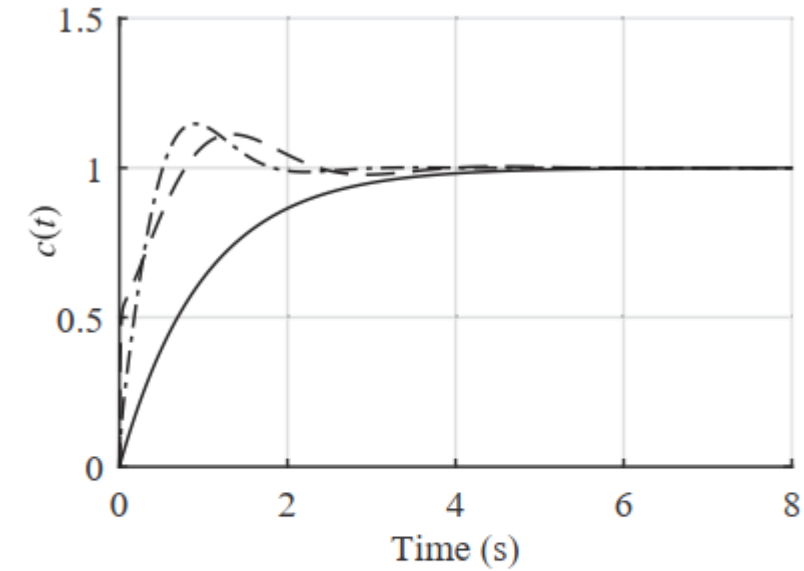
— Open-loop
 - - - PID control ($K_p = 3, K_i = 10, K_d = 0.1$)
 - . - PID control ($K_p = 1, K_i = 10, K_d = 0.1$)

(a) Proportional action.



— Open-loop
 - - - PID control ($K_p = 3, K_i = 10, K_d = 0.1$)
 - . - PID control ($K_p = 3, K_i = 20, K_d = 0.1$)

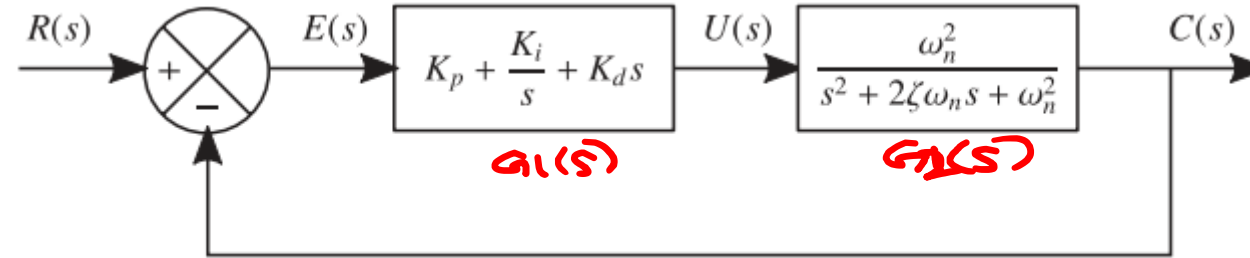
(b) Integral action.



— Open-loop
 - - - PID control ($K_p = 3, K_i = 10, K_d = 0.1$)
 - . - PID control ($K_p = 3, K_i = 10, K_d = 1$)

(c) Derivative action.

PID Control of a Second-Order System



$$\frac{C(s)}{R(s)} = \frac{(K_i + K_p s + K_d s^2) \omega_n^2}{s^3 + (2 \zeta \omega_n + K_d \omega_n^2) s^2 + \omega_n^2 (K_p + 1) s + K_i \omega_n^2}$$

$$C(s) = R$$

$$C_{ss} = 1$$

PID Control of a Second-Order System cont.

$$Y_s \leftarrow \frac{E(s)}{R(s)} = \frac{s(s^2 + 2\xi\omega_n s + \omega_n^2)}{s^3 + (2\xi\omega_n + K_d\omega_n^2)s^2 + \omega_n^2(K_p + 1)s + K_i\omega_n^2}$$

$E(s)$ ✓

$$\underline{\underline{e_{ss} = 0}}$$

Summary

- PD Control of a Second-Order System and Effect on a Second-Order System
- Integral Control of a First-Order/Second-Order System and Effect on a First-Order/Second-Order System
- PI Control of a First-Order System and Effect on a First-Order System
- PID Control of a First-Order /Second-Order System and Effect on a First-Order System

Reference:

-Control Systems Engineering, 7th Edition, N.S. Nise
-UESTC3001 2019/20 Notes, J. Le Kernec