

D07 (HW 2009, 9.3)

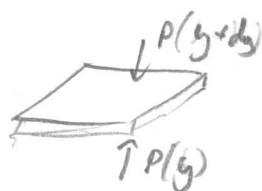


$$f_0(\vec{p}, x, y, z) = \frac{n(y)}{(2\pi m k_B T(y))^{3/2}} e^{-\frac{p^2}{2m k_B T(y)}}$$

- a)  $T(y)$  non uniform  $\rightarrow$  flow of heat & particles  
 $\rightarrow \mu$  not uniform

Mechanical equilibrium:  $P = n k_B T = \text{const}$

$$\rightarrow n(y) \cdot T(y) = \text{const}$$



$$\text{i.e. } P(y+dy) = P(y)$$

- b) for  $n(y) \sim \frac{1}{T(y)}$  we have  $f_0 \sim T(y)^{-5/2} e^{-\frac{p^2}{2m k_B T(y)}}$

$$\text{but } \left( \frac{\partial}{\partial t} + v_y \frac{\partial}{\partial y} \right) f_0 = \frac{p_y}{m} \left( -\frac{5}{2} \frac{1}{T(y)} + \frac{p^2}{2m k_B T^2(y)} \right) \frac{\partial T}{\partial y} \cdot f_0(p, y) \neq 0$$

$$\text{whereas } e^{-\frac{\beta m}{2}(v_1^2 + v_2^2)} = e^{-\frac{\beta m}{2}(v_1'^2 + v_2'^2)} \rightarrow \delta f_2 - \delta f_2' = 0 \rightarrow \left( \frac{\partial f}{\partial t} \right)_{\text{coll}} = 0$$

$$\text{Using the relaxation time approximation } \left( \frac{\partial f}{\partial t} \right)_{\text{coll}} = -\frac{(f_1 - f_0)}{\tau}$$

$$\text{we have } f_1 = f_0 \left( 1 + \frac{\tau p_y}{m} \left( \frac{5}{2} \frac{1}{T(y)} - \frac{p^2}{2m k_B T^2(y)} \right) \frac{\partial T}{\partial y} \right)$$

- c)  $Q = n \frac{\langle p_y p^2 \rangle}{2m^2}$ , why?

$$Q = \text{Heat flow} = \text{Energy} \times \text{particle flux}$$

$$= \frac{p^2}{2m} \cdot n v_y = \frac{p^2}{2m} \cdot n \frac{p_y}{m}$$

$$\langle Q \rangle = \frac{n}{2m^2} \langle p^2 p_y \rangle \quad \leftarrow \text{this average with the actual distribution, but } f_1 \text{ approximates it}$$

$$\langle p_y p^2 \rangle_0 = 0 \quad \leftarrow \text{since } f_0 \text{ can't contribute to the flow.}$$

$$\langle Q \rangle = \frac{n}{2m^2} \frac{\tau}{m} \left\langle p_y^2 p^2 \cdot \frac{5}{2} \frac{1}{T(y)} - p_y^2 p^4 \cdot \frac{1}{2m k_B T^2(y)} \right\rangle_0 \frac{\partial T}{\partial y}$$

$$= \frac{n}{2m^2} \cdot \frac{\tau}{m} \left[ \frac{25m^2 k_B^3 T^2}{2} - \frac{35}{2m} k_B^3 T^2 \right] = \frac{-5}{2} \frac{n \tau}{m} k_B^2 T \frac{\partial T}{\partial y}$$

$$Q = -\kappa \frac{\partial T}{\partial y} \rightarrow \underbrace{\kappa = \frac{5}{2m} k_B^2 n T}_{\text{doesn't depend on } y!} = \text{const}$$

d) Steady state  $\rightarrow$  no flow (of heat or anything else)

$$\rightarrow Q = \text{const}$$

$$\rightarrow n(y) \cdot T(y) \cdot \frac{\partial T}{\partial y} = \text{const}$$

$$\text{but } n(y) T(y) = \text{const} \rightarrow \frac{\partial T}{\partial y} = \text{const}$$

$$\boxed{T = T_0 + \frac{y}{W} (T_2 - T_1)} \leftarrow \text{with boundary conditions}$$

e) We are looking for  $\frac{\kappa}{\sigma} \propto T$

$$\sigma = \frac{J_y}{\frac{1}{2} \mu} = \frac{n v_y}{\frac{1}{2} \mu}$$

$$\text{but } \mu(y) = \mu_0 + \phi(y) \rightarrow \frac{\partial \mu}{\partial y} = \frac{\partial \phi}{\partial y} = -E$$

Since

$$j = \sigma E = -\sigma \frac{\partial \mu}{\partial y}$$

what we need is to replace the  $\Delta T$  between the plates with electric field  $E$  and solve for Boltzmann's eq. see q. D03.