1 ZMP LQR Riccati Equation

Using z(t) as the 2D position of the ZMP, we formulate:

This can be rewritten as a cost on state, in coordinates relative to the final conditions, $\bar{x} = x - \begin{bmatrix} z_d^T(t_f) & 0 & 0 \end{bmatrix}^T$, $\bar{z}_d(t) = z_d(t) - z_d(t_f)$:

Note that this implies that $\bar{x}(\infty) = 0$ in order for the cost to be finite. The resulting cost-to-go is given by

$$J = \bar{x}^T S_1(t) \bar{x} + \bar{x}^T S_2(t) + S_3(t),$$

with the corresponding Riccati differential equation given by

$$\dot{S}_1 = -\left(Q_1 - (N + S_1 B) R_1^{-1} (B^T S_1 + N^T) + S_1 A + A^T S_1\right)
\dot{s}_2 = -\left(q_2(t) - 2(N + S_1 B) R^{-1} r_s(t) + A^T s_2\right), \quad r_s(t) = \frac{1}{2} (r_2(t) + B^T s_2(t))
\dot{s}_3 = -\left(q_3(t) - r_s(t)^T R^{-1} r_s(t)\right)$$

Note that S_1 has no time-dependent terms, and therefore $S_1(t)$ is a constant, given by the steady-state solution of the algebraic Riccati equation (e.g. from time-invariant LQR). Similarly, the feedback controller is given by

$$u(t) = K_1(t)\bar{x} + k_2(t),$$

and again the feedback $K_1(t)$ is a constant (derived from the infinite horizon LQR with Q, R, and N set as above).

1.1 Solving for $s_2(t)$

Given this, the affine terms in the Riccati differential equation are given by the linear differential equations:

$$\dot{s}_2(t) = A_2 s_2(t) + B_2 \bar{z}_d(t), \quad s_2(t_f) = 0$$

with

$$A_2 = (N + S_1 B)R^{-1}B^T - A^T, \quad B_2 = \begin{bmatrix} 2I_{2 \times 2} \\ 0_{2 \times 2} \end{bmatrix} + 2\frac{h}{g}(N + S_1 B)R^{-1}$$

Assuming $\bar{z}_d(t)$ is described by a *continuous* piecewise polynomial of degree k with n+1 breaks at t_i (with $t_0=0$ and $t_n=t_f$):

$$\bar{z}_d(t) = \sum_{i=0}^k c_{j,i}(t-t_j)^i$$
, for $j = 0, ..., n-1$, and $\forall t \in [t_j, t_{j+1})$,

this system has a closed-form solution given by:

$$s_2(t) = e^{A_2(t-t_j)}\alpha_j + \sum_{i=0}^k \beta_{j,i}(t-t_j)^i, \quad \forall t \in [t_j, t_{j+1}),$$

with α_j and $\beta_{j,i}$ vector parameters to be solved for. Taking

$$\dot{s}_{2}(t) = A_{2}e^{A_{2}(t-t_{j})}\alpha_{j} + \sum_{i=0}^{k} A_{2}\beta_{j,i}(t-t_{j})^{i} + \sum_{i=0}^{k} B_{2}c_{j,i}(t-t_{j})^{i}$$

$$= A_{2}e^{A_{2}(t-t_{j})}\alpha_{j} + \sum_{i=1}^{k} i\beta_{j,i}(t-t_{j})^{i-1}$$

forces that

$$A_2\beta_{j,i} + B_2c_{j,i} = (i+1)\beta_{j,i+1}, \quad \text{for } i = 0, ..., k-1$$

 $A_2\beta_{j,k} + B_2c_{j,k} = 0.$

Note: need to prove that A_2 is full rank (it appears to be in practice). Solve backwards (i = k, k - 1, ..., 0) for $\beta_{j,i}$. Finally, the continuity and the terminal boundary condition $s(t_f) = 0$ gives

$$e^{A(t_{j+1}-t_j)}\alpha_j + \sum_{i=0}^k \beta_{j,i}(t_{j+1}-t_j)^{i+1} = s(t_{j+1}).$$

1.2 Reading out $k_2(t)$

The remaining term for the controller is a simple read-out given the solution to $s_2(t)$:

$$k_2(t) = -\frac{h}{a}R^{-1}\bar{z}_d(t) - \frac{1}{2}R^{-1}B^Ts_2(t)$$

which can be written as

$$k_2(t) = \alpha_L e^{A_2(t-t_j)} \alpha_{j,R} + \sum_{i=0}^k \gamma_{j,i} (t-t_j)^i$$

with

$$\alpha_L = -\frac{1}{2}R^{-1}B^T$$

$$\alpha_R = \alpha_{j,R} = \alpha_j$$

$$\gamma_{j,i} = -\frac{h}{g}R^{-1}c_{j,i} - \frac{1}{2}R^{-1}B^T\beta_{j,i}$$

1.3 Solving for $x_{com}(t)$

The resulting system is

$$\dot{x} = Ax + B(K_1x + k_2(t)) = (A + BK_1)x + Bk_2(t),$$

where $x = [x_{com}, y_{com}, \dot{x}_{com}, \dot{y}_{com}]^T$. Since the solution $k_2(t)$ is the result of another linear system (cascaded in front of this one), it is easiest for me to solve jointly, using $y = \begin{bmatrix} x \\ s_2 \end{bmatrix}$:

$$\dot{y} = A_y y + B_y \bar{z}_d$$

$$A_y = \begin{bmatrix} A + BK_1 & -\frac{1}{2}BR^{-1}B^T \\ 0 & A_2 \end{bmatrix}, \quad B_y = \begin{bmatrix} -\frac{h}{g}BR^{-1} \\ B_2 \end{bmatrix}$$

$$y(t) = e^{A_y(t-t_j)}a_j + \sum_{i=0}^k b_{j,i}(t-t_j)^i$$

i can solve for b using the same technique as above (and re-using the β sol), and then solve for the top half of a_j forward in time.

1.4 Solving for $s_3(t)$

Having solved for $s_2(t)$, the dynamics of $s_3(t)$ in segment j can be written as

$$\dot{s}_3(t) = \bar{z}_d^T(t) \left(\frac{h^2}{g^2} R^{-1} - I \right) \bar{z}_d(t) + \frac{1}{4} s_2^T(t) B R^{-1} B^T s_2(t) + \frac{h}{g} \bar{z}_d^T(t) R^{-1} B^T s_2(t)$$

Let us rewrite our vector polynomials as, for instance, $\bar{z}_d(t) = \vec{c}_j m_k (t - t_j)$, with

$$\mathbf{c}_j = \begin{bmatrix} c_{j,0} & c_{j,1} & \dots & c_{j,k} \end{bmatrix}$$

and

$$m_k(t) = \begin{bmatrix} 1 \\ t \\ t^1 \\ \dots \\ t^k \end{bmatrix}.$$

We will also use the fact that

$$(e^{At})^T e^{At} = e^{(A^T + A)t}$$

Then we have (dropping the j's for notational convenience and leaving $t_j = 0$):

$$\dot{s}_{3}(t) = m_{k}^{T}(t) \left[\mathbf{c}^{T} \left(\frac{h^{2}}{g^{2}} R^{-1} - I \right) \mathbf{c} + \frac{1}{4} \beta^{T} \beta \right] m_{k}(t) + \frac{1}{4} \alpha^{T} e^{A_{2}^{T} t} B^{T} R^{-1} B e^{A_{2} t} \alpha \dots \right.$$
$$+ m_{k}^{T}(t) \left[\frac{1}{2} \beta^{T} B + \frac{h}{g} \mathbf{c}^{T} \right] R^{-1} B^{T} e^{A_{2} t} \alpha$$

The integral of this is ugly, and the requirement for accuracy here is less strict. For parsimony, we will approximate $s_3(t)$ with a Hermite cubic spline with the values and derivatives set (analytically) at the breakpoints of the desired ZMP trajectory. This means that we can cut a few computational corners in order to evaluate the value of $s_3(t)$ at the breakpoints, instead of maintaining the entire closed-form solution. Note that $s_3(t)$ is continuous - the left and right derivates are equal.

We'll make use of the following steps to complete the integral:

$$\frac{d}{dt}m_{k}(t) = \begin{bmatrix} 0\\1\\2t\\ \vdots\\kt^{k-1} \end{bmatrix} = \begin{bmatrix} 0_{1\times k}\\ \mathrm{diag}(1,2,\cdots,k) \end{bmatrix} m_{k-1}(t) \equiv D_{k}m_{k-1}(t)$$

$$\int m_{k}(t)dt = \begin{bmatrix} t\\ \frac{1}{2}t^{2}\\ \vdots\\ \frac{1}{k+1}t^{k+1} \end{bmatrix} = \begin{bmatrix} 0_{k+1\times 1} & \mathrm{diag}(1,\frac{1}{2},\cdots,\frac{1}{k+1}) \end{bmatrix} m_{k+1}(t) \equiv D_{k+1}^{\sharp}m_{k+1}(t)$$

$$\int_{0}^{a} m_{k}(t)dt = D_{k+1}^{\sharp}m_{k+1}(a)$$
Note $:D_{k} \text{ is } k+1\times k, D_{k}^{\sharp} \text{ is pinv}(D_{k})$

$$\int e^{At}dt = A^{-1}e^{At}$$

$$\int_{0}^{a} m_{k}^{T}(t)Pm_{k}(t)dt = \int_{0}^{a} \mathrm{Tr}(Pm_{k}(t)m_{k}^{T}(t))dt = \int_{0}^{a} \mathrm{vec}(P^{T})^{T}\mathrm{vec}(m_{k}(t)m_{k}^{T}(t))dt$$