Sun's position for navigation with DM15L Manual

Michael Josefsson

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Overview

The handheld calculator DM15 (a HP-15c look-a-like with more memory) can be used for determining the sun's position with precision enough for celestial navigation purposes. The accompanying program, listed in the Appendix, constitutes a handy tool for either finding the Nautical Almanac's entries GHA (Greenwich Hour Angle) and Declination, or — with AP (Assumed Position) — directly calculate the sun's Altitude Hc and Azimuth Az for this position.

The algorithm relies on pure Keplerian motion of the sun. No planetary perturbations are taken into account. Resulting angular accuracy is about 1 minute of arc, which is adequate for general navigation at sea.

1. Usage

Before use, notice that:

- All times entered are UT ("GMT") even if observer's longitude is not the prime meridian. Of course, local hour angles take longitude into consideration, but all times are still UT. Time format is *hh.mmss*, where *mm* and *ss* must be two-digit numbers.
- The program makes use of the calculator's internal decimal to degrees, minutes and seconds routines both for **entry** and **displayed result**. In navigation a more common format of degrees, minutes and tenths of a minute is used. That conversion, if needed, is readily done by dividing the arc-seconds number or multiplying the minute's decimal by 6.

Example

Convert angle in ddd.mmss to $ddd.mm \cdot t$

```
98° 26′ 12″, entered as 98.2612, is 98° 26·2′ where 12''/6=2 98° 26′ 43″, entered as 98.2643, is 98° 26·7′ where 43''/6\approx 7
```

Example

Convert angle in $ddd.mm \cdot t$ to ddd.mmss

```
14^{\circ} 7.3' is 14^{\circ} 7' 18'' where 3 \cdot 6 = 18
277° 4.5' is 277° 4.30' where 5 \cdot 6 = 30
```

1.1. User-defined buttons

The programs user-defined functions are accessed via the buttons below

1. Usage

Button	Function
Α	Date for Aries angle at UT=0h
В	Time for Sun Altitude and Azimuth
C	SHA and declination for own object
D	Time for own object's Altitude and Azimuth
Ε	Time for GHA Aries and LHA Aries
.5	After B for GHA and declination
	(as a Nautical Almanac entry)

1.2. Assumed Position

An AP ($Assumed\ Position$) is entered in registers 8 and .8 before any calculations can be performed.

Example

Entering AP.

A location of Lat N58 $^{\circ}$ 34', Long E14 $^{\circ}$ 34' 12" is entered into registers 8 and .8:

Data	Format	Key	Display shows	Meaning
58.3400	$\pm dd.mmss$	$\mathrm{g}{ ightarrow}\mathrm{H}$ STO 8	58.5667	Decimal degrees
14.3412	$\pm dd.mmss$	$\mathrm{g}{ ightarrow}\mathrm{H}\;\mathtt{STO}$.8	14.5700	Decimal degrees

East and North are positive, West and South are negative.

The position is permanently stored until manually changed and need only be set once.

1.3. Daily entry

Every day has its own parameters that require the A-routine to be run once for each day.

Example

Entering the date.

Enter June 12th 2022, i.e. year 2022, month 6 and day 12.

Data	Format	Key	Display shows	Meaning
2022	YYYY	ENTER	2022.0000	
6	mm	ENTER	6.0000	
12	dd	f A	260.1816	260° 18′ 16″, GHA Aries at 0h
				(Nautical Almanac 2022: 260° 18'·1)

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1.4. Sun's Altitude and Azimuth

Next the sun's position for time of date UT/GMT can be calculated.

Example

Find sun's Hc and Az for UT 09h 54m 48s. Date as above.

Enter time in format *hh.mmss* then use routine B.

Data	Format	Key	Display shows	Meaning
9.5448	hh.mmss	f B	52.3845	$Hc = 52^{\circ} 38' 45''$
		х<>у	154.1140	$Az = 154^{\circ} 11' 40''$

Result: $Hc = 52^{\circ} 38.7'$, $Az = 154^{\circ}$

A new time can be entered directly. For example, also find sun's Hc and Az a few minutes later at UT 10h 02m 30s.

Data	Format	Key	Display shows	Meaning
10.0230	hh.mmss	f B	53.0338	$Hc = 53^{\circ} 03' 38''$
		х<>у	157.0236	$Az = 157^{\circ} 2' 36''$

Result: $Hc = 53^{\circ} 03.6'$, $Az = 157^{\circ}$

1.5. GHA and declination

The program can also produce values for GHA and declination imitating the *Nautical Almanac*.

Example

Find GHA and decl for 10h on June 12th 2023

After calculating Hc and Az as above, use GSB .5 to get GHA and declination δ :

Data	Format	Key	Display shows	Meaning
10.0000	hh.mmss	fВ		$Hc = 52^{\circ} 55' 08''$
		GSB .5	330.0248	$GHA = 330^{\circ} 2' 48''$
		x<>y	23.0901	$\delta = 23^{\circ} 09' 01''$

Result: GHA = 330° 2·8′, Decl = 23° 09·0′ (Nautical Almanac gives 330° 2·8′ and 23° 8·8′). GHA and Decl can of course be calculated for any other time during the day in the same manner.

5

1. Usage

Specify and calculate position for an object with known SHA and declination

The coordinates of a celestial object, for example a star, are given as SHA ($Sidereal\ Hour\ Angle$) and declination.¹

Example

Enter coordinates of Vega (SHA $80^{\circ} 34.3'$, declination $38^{\circ} 48.2'$).

Data	Format	Key	Display shows	Meaning
80.3418	ddd.mmss	ENTER	80.3418	SHA
38.4812	ddd.mmss	f C	279.4283	RA in decimal degrees

Now find Vega's calculated position for $UT = 23h\ 02m\ 10s$ on June 12th 2023 already entered above.

Data	Format	Key	Display shows	Meaning
23.0210	hh.mmss	f D	67.0015	$Hc = 67^{\circ} 00' 15''$
		х<>у	141.1224	$Az = 141^{\circ} 12' 24''$

Result: Vega can be expected at $Hc = 67^{\circ} \, 0.2'$ and $Zn = 141^{\circ}$. Set the sextant for 67° and search for it in south-east.

GHA Aries and LHA Aries

Find GHA Aries on 4 October 2022 at 7h 57m 20s. Also find LHA Aries longitude in .8 $(14^{\circ} 34' 12'' \text{ E as before})$.

	Data	Format	Key	Display shows	Meaning
-	2022	YYYY	ENTER	2022.0000	Year
	10	mm	ENTER	10.0000	Month
	4	dd	f A	12.4006	12° 40′ 6″, GHA Aries at 0h
	7.5720	hh.mmss	f E	132.1942	GHA Aries = $132^{\circ} 19' 42''$
			$x \leftrightarrow y$	146.5354	LHA Aries = $146^{\circ} 53' 54''$

¹Right Ascension can be entered as $\alpha = 360 - SHA$ if needed.

Use as Sight Reduction Table

The program can also solve the navigational triangle and be used as a $Sight\ Reduction\ Table$ replacement (Ho-214/Ho-229 etc). To solve the triangle 1) AP latitude, 2) object's declination and 3) hour angle need to be entered.

AP latitude is entered in register 8 as before, declination is set via $\boldsymbol{\mathsf{C}}$ and hour angle is entered into register .2. The hour angle is positive if westward.

Example

Find Hc and Az as in Ho-214

Assume latitude N58°, Declination $8^{\circ} 30'$ and an hour angle of 54° (object to the west of observer).

Data	Format	Key	Display shows	Meaning
58	dd.mmss	STO 8	58.0000	Decimal latitude
8.3000	dd.mmss	С	8.5000	Decimal declination
54	dd.mmss	$g \rightarrow H$	54.0000	Decimal Hour angle
		STO .2	54.0000	
		GSB 7	25.4102	$Hc = 25^{\circ} 41' 02''$
		$x \leftrightarrow y$	242.3616	$Az = 242^{\circ} 36' 16'' = 242.6^{\circ}$

Ho-214 gives Alt. = $25^{\circ} 41.0'$ and Az. = 117.4° . Where true azimuth is $360 - 117.4 = 242.6^{\circ}$.

A. Program and information

Register usage

The lower registers r0..r7 are used by the calculator's statistics functions and are not permanently used by this program. They are used however for intermediate results via the normal operating sequences A-B or A-C-D or A-E.

In short: Use r0..r7 as you wish but they will be altered by **A**.

Program installation

For a fresh install of the program perform steps 1–6 below.

- 1. Make space on the DM15 for program and registers:
 - Enter 21 f DIM (i)
 - Double check: g MEM should read 21.209
- 2. In HP-15C/Preferences/DM15 menu: Select 229 as Number of registers.
- 3. File/Open Program: file.15c
- 4. Write program to DM15.
 - On device enable serial communication (hold C while pressing ON-button)
 - File/Write DM15
- 5. Before use enter the following constants constants into the respective registers:

Register	Constant	Meaning
.3	279.4055638	Longitude at epoch JD=2459944.5
.4	283.3328093	Longitude of perigee for epoch
.5	1.016860112	$\sqrt{\frac{1+e}{1-e}}$
.6	23.44188400	Ecliptic obliquity
.7	0.002737909	$\frac{1}{365.2422}$

6. That's it. Now the samples in this document give expected results.

Program listing

Note: In the listing below some minor self explanatory key appearances have changed. SIN^{-1} is replaced with ASIN etc, $x \leftrightarrow y$ is x <> y and $R \downarrow$ is Rv.

A. Program and information

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g RAD
ENTER
000 {
                                           059 {
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                                                          43
                      }
}
001
       42 21 48
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002
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003
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004
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                                                                    f FIX 9
                    0
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                         g RTN
f LBL
005
                   32
                      }
                                                      42 10
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                                                                  } f SOLVE 8
               43
                                           064
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     {
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                      }
                           LBL 4
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                                                                  } RCL .5
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                      }
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010
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                      } x<>y
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                   24
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                      } f LBL 2
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016
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f LBL 7
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057
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                    3 }
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058 {
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118 {
               43 23 } g ASIN 36 } ENTER
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                                           177 {
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119 {
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                                            178 {
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                   1 } STO .1
                                                               36 } ENTER
     {
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                                           180 {
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122
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                    8 } RCL 8
                                            181
                                                               36 } ENTER
123
               32
                   4 } GSB 4
                                            182 {
                                                       45 48
                                                               8 } RCL .8
                                                               40 } +
124
     {
{
{
}

                   16 } CHS
                                            183 {
125
           45 48
                   0
                       } RCL .0
                                            184
                                                           32
                                                                2
                                                                  } GSB 2
                   23 } SIN
126
                                                                5 } STO 5
                                            185
                                                           44
     {
                                            186 {
127
                   40 } +
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                      } x<>y
} RCL 8
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128
                                            187
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                         RCL 8
129
               45
                    8
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                                                               34
                                                                   } x<>y
                                            189 {
190 {
                      GSB 5
130
     {
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                                                                9 } f LBL 9
               32
                  5
131
                   10 } /
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                   24 } g ACOS
2 } f x<> .2
                                           191 {
192 {
193 {
132
               43
                                                               34 } x<>y
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{
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133
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                       } SIN
                                                           43 32 } g RTN
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134
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{
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                       } g TEST x<0
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195 {
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135
                    2
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136
               22
                    6 } ĞTO 6
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                    8 } GSB .8
2 } RCL .2
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137
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138
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199 {
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139
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141
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202 {
203 {
204 {
                    1 } RCL .1
2 } RCL .2
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}
142
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143
           45 48
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144 {
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                    8 } f LBL 8
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146
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209 {
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212 {
213 {
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152
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154
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215 {
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                   16 } CHS
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40 } +
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                  9 } RCL 9
157
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158
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                   30 } -
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159
                   32 } g RTN
                                            218 {
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                                                                3 } STO 3
     {
               43
                    3 } f LBL C
2 } g ->H
0 } STO .0
                                           219 {
220 {
221 {
160
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161
                    2
                                                           44
               43
                                                           43 32 } g RTN
21 11 } f LBL
44 4 } STO 4
162
           44
              48
                                            222 {
223 {
                                                       42 21
163
                   33 } Rv
                    2 } g ->H
8 } GSB .8
               43
164
                                                               33 } Rv
           32 48
                                            224
165
                                            225 {
226 {
                       } x<>y
166
                   34
                                                               5 } STO 5
                                                               33 } Rv
167
                   30 } -
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168
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               44
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169
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                  32
                      } g RTN
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                       } f LBL E
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230 {
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170
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171
               43
                   2
                      } g ->H
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                    4 } ŠTO 4
172 {
                                                           32
               44
                                            231 {
                                                                1 } GSB 1
                       } RCL .7 } 1
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233 {
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30 } -
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173
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174
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235 {
175 {
176 {
                   40 }
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```

A. Program and information

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3 } RCL 3
40 } +
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                                                                       }
}
}
236 {
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237
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238
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                     2
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                        } STO 1
239
                44
                     1
                                              276
                                                               43 44 } g INT
16 } CHS
240
                42
                     2 } f ->H.MS
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                43 32 } g RTN
21 1 } f LBL 1
241 {
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                                              297
                                                               45
                                                                    9
                                                                         RCL 9
                43 44
                                                                   30
261
                             INT
                                              298
                           g
262
                    40
                        }
                                              299
                                                                   40
                                                                       }
                                                               32
                                                                      } GSB 2
263
                    34
                        } x <> y
                                              300
                                                                    2
                        } ENTER
} f x<> 1
                                                           45 48
                                                                    0 } RCL .0
264
     {
                    36
                                              301
                                                    {
265
            42
                                              302
                                                               22
                                                                    9
                                                                       }
                                                                         GTO 9
                        }
                                                                    0 } f LBL .0
266
                     9
                          9
                                              303 {
                                                      42 21
                                                               48
                       } +
} 1
} 2
} /
                                                                   7 } RCL .7
8 } GSB .8
267
                    40
                                              304
                                                    {
                                                           45
                                                              48
                                              305 {
306 {
307 {
268
                                                           32 48
                     1
                                                               20 } *
43 32 } g RTN
                     2
269
270
                    10
                       }
}
271
                43
                   44
                             INT
                           g
272 {
```

Program Resources

Labels

Name	Description
Α	
В	
С	
D	
Е	
0	
1	

Name	Description
2	
3	
4	
5	
6	
7	Lat -> r8, LHA -> r12, decl -> r10 ==>> Hc, Zn
8	

Name	Description
9	
11	
12	
15	After B: GHA and Declination
16	
18	

Storage Registers

Name	Description				
0	JD of start of year				
1	LHA 0h				
3	3 GMST yearly constant				
4	UT entered 024, decimal				
5	LHA Aries				
6	JD of date				

	Name	Description
	8	Observer's latitude, degrees (N/S=+/-)
	9	Objects Right Ascension, degrees
	10	Object's declination, degrees (N/S=+/-)
-	11	Hc, calculated altitude, degrees
	12	LHA of object -> Zn, calculated azimuth
	13	Constant, L of epoch 279.4055638 for JD=2459944.5

Name	Description
14	Constant, Long of perigee, 283.3328090 fo JD above
15	1.016860112 [sqrt((1+e)/(1-e)]
16	Constant, Obliquity, 23.4382144
17	1/365.2422
18	Observer's longitude (E/W=+/-)

Program

Line	Display	Key Sequence
000		
001	42,21, .8	f LBL .
002	3	3
003	6	6
004	0	0
005	43 32	g RTN
006	42,21, 4	f LBL 4
007	23	SIN
008	34	x↔y
009	23	SIN

Line	Display	Key Sequence
113	45 .0	RCL .
114	32 5	GSB 5
115	20	×
116	45 .0	RCL .
117	45 8	RCL 8
118	32 4	GSB 4
119	40	+
120	43 23	g SIN-1
121	36	ENTER
122	36	ENTER

Line	Display	Key Sequence
226	20	×
227	2	2
228	4	4
229	0	0
230	0	0
231	48	
232	0	0
233	5	5
234	1	1
235	2	2

026	010	22 .6	GTO . 6	123	44 .1	STO .	236	6	6
013	011	42,21, 5	f LBL 5	124	45 8	RCL 8	237	2	2
014	012	24	cos	125	32 4	GSB 4	238	40	+
014	013	34	x↔y	126	16	CHS	239	20	×
015	014	24	cos	127	45 .0	$\overline{}$	240	6	6
017 32 .8 8 130 34	015	22 .6		128	23	SIN	241	48	
017 32 .8 8 130 34	016	42,21, 2	f LBL 2	129	40	+	242	6	6
019	017	32 .8		130	34	x↔y	243	4	4
020	018	10	÷	131	45 8	RCL 8	244	6	6
020	019	42 44	f FRAC	132	32 5	GSB 5	245	0	0
022	020	43,30, 1		133	10	÷	246	6	6
022	021	22 3	GTO 3	134	43 24	g COS-1	247	5	5
024 42,21, 3 f LBL 3 137 43,30, 2 g TEST x<0	022	1	1	135			248	6	6
025 32 .8	023	40	+	136	23		249	40	+
025 32 .8 8 138 22 6 G10 6 251 32 2 GSB 2 026 42,21, f LBL . 139 32 .8 8 RCL . 252 44 3 STO 3 027 20 x 140 45 .2 2 2 253 45 6 RCL 6 028 43 32 g RTN 141 30 - 254 44 0 STO 0 029 42,21, f LBL . 142 44 .2 2 2 2 255 43 32 g RTN 030 1 1 1 143 42,21, 6 f LBL 6 256 42,21,11 f LBL A 031 5 5 144 45 .1 RCL . 257 44 4 STO 4 032 22 .6 GTO . 145 45 .2 RCL . 258 33 R↓ 033 42,21,12 f LBL B 146 22 9 GTO 9 259 44 5 STO 5 034 32 15 GSB E 147 42,21, 8 f LBL 8 260 33 R↓ 035 45 6 RCL 6 148 23 SIN 261 32 0 GSB C	024	42,21, 3	f LBL 3	137	43,30, 2	$\overline{}$	250	32 .2	
026 .6 6 139 32 .8 8 252 44 3 \$10 3 027 20 x 140 45 .2 2 253 45 6 RCL 6 6 028 43 32 gRTN 141 30 — 254 44 0 \$TO 0 0 029 42,21, f LBL . 142 44 .2 \$STO . 255 43 32 \$gRTN 030 1 1 143 42,21, 6 f LBL 6 256 42,21,11 f LBL A 031 5 5 144 45 .1 RCL . 257 44 4 \$STO 4 032 22 .6 GTO . 145 45 .2 RCL . 258 33 R↓ 033 42,21,12 f LBL B 146 22 9 GTO 9 259 44 5 \$TO 5 034 32 15 GSB E 147 42,21, 8 f LBL B 260 33 R↓ 035 45 6 RCL 6 148 23 SIN 261 32 0 GSB C	025	32 .8		138	22 6	GTO 6	251	32 2	GSB 2
027 26 x 140 45 . 2 2 253 45 6 RCL 6 6 028 43 32 g RTN 141 30 — 254 44 0 STO 0 2 029 42,21, f LBL 142 44 .2 STO 255 43 32 g RTN 030 1 1 143 42,21, 6 f LBL 6 256 42,21,11 f LBL A 031 5 5 144 45 . 1 RCL 257 44 4 STO 4 032 22 . 6 6 6 145 45 . 2 RCL 258 33 R↓ 033 42,21,12 f LBL B 146 22 9 GTO 9 259 44 5 STO 5 034 32 15 GSB E 147 42,21, 8 f LBL B 260 33 R↓ 035 45 6 RCL 6 148 23 SIN 261 32 0 GSB 0	026			139	32 .8		252	44 3	STO 3
029 42,21, f LBL	027	20	×	140	45 .2		253	45 6	RCL 6
029 .2 2 030 1 1 143 42,21, 6 f LBL 6 256 42,21,11 f LBL A 257 44 4 STO 4 144 45 .1 1 145 45 .2 RCL . 258 33 R↓ 033 42,21,12 f LBL B 146 22 9 GTO 9 259 44 5 STO 5 034 32 15 GSB E 147 42,21, 8 f LBL 8 260 33 R↓ 035 45 6 RCL 6 148 23 SIN 261 32 0 GSB C	028	43 32	g RTN	141	30	_	254	44 0	STO 0
031 5 5 144 45 .1 RCL . 1 257 44 4 STO 4 032 22 .6 GTO . 6 145 45 .2 RCL . 258 33 R↓ 033 42,21,12 f LBL B 146 22 9 GTO 9 259 44 5 STO 5 034 32 15 GSB E 147 42,21, 8 f LBL 8 260 33 R↓ 035 45 6 RCL 6 148 23 SIN 261 32 0 GSB C	029		$\overline{}$	142	44 .2		255	43 32	g RTN
031 5 5 144 45 .1 1 032 22 .6 6 145 45 .2 2 258 33 R↓ 033 42,21,12 f LBL B 146 22 9 GTO 9 259 44 5 STO 5 034 32 15 GSB E 147 42,21, 8 f LBL 8 260 33 R↓ 035 45 6 RCL 6 148 23 SIN 261 32 0 GSB 0	030	1	1	143	42,21, 6	f LBL 6	256	42,21,11	f LBL A
032 22 . 6 6 033 42,21,12 f LBL B 034 32 15 GSB E 145 45 . 2 146 22 9 GTO 9 147 42,21, 8 f LBL 8 259 44 5 STO 5 260 33 R↓ 33 R↓ 34 32 0 GSB C	031	5	5	144	45 .1		257	44 4	STO 4
034 32 15 GSB E 147 42,21, 8 f LBL 8 260 33 R↓ 035 45 6 RCL 6 148 23 SIN 261 32 0 GSB C	032	22 .6		145	45 .2		258	33	R↓
035 45 6 RCL 6 148 23 SIN 261 32 0 GSB C	033	42,21,12	f LBL B	146	22 9	GTO 9	259	44 5	STO 5
	034	32 15	GSB E	147	42,21, 8	f LBL 8	260	33	R₽
036 2 2 149 48 . 262 45 1 RCL 1	035	45 6	RCL 6	148	23	SIN	261	32 0	GSB 0
				149			-		
	-								
	-						-		
	-								
040 9 9 153 7 7 266 45 0 RCL 0	040	9	9	153	7	7	266	45 0	RCL 0

042	041	4	4	154	1	1	267	30	_
044 5 5 5 5 5 157 16 CHS 270 20 x 20 x	042	4	4	155	8	8	268	45 .7	
045	043	48		156	20	×	269	32 .8	
046	044	5	5	157	16	CHS	270	20	×
047	045	30	_	158	40	+	271	20	×
048	046	45 4	RCL 4	159	45 9	RCL 9	272	45 3	RCL 3
049	047	2	2	160	30	_	273	40	+
050	048	4	4	161	43 32	9	274	32 2	GSB 2
051	049	10	÷	162	42,21,13	f LBL C	275	44 1	STO 1
051	050	40	+	163	43 2	$g \rightarrow H$	276	42 2	f →H.MS
052	051	45 .7	7	164	44 .0		277	43 32	gRTN
054	052	32 .8	$\overline{}$	165	33	R↓	278	42,21, 1	f LBL 1
054	053	20	×	166	43 2	$g \rightarrow H$	279	1	1
055	054	20	×	167	32 .8		280	7	7
057	055	45 .3		168	34	$x \leftrightarrow y$	281	2	2
057	056	40	+	169	30	_	282	1	1
059 42 3 f → RAD 172 42,21,15 f LBL E 285 3 3 060 44 9 STO 9 173 43 2 g → H 286 48 . 061 43 8 g RAD 174 44 4 STO 4 287 5 5 062 36 ENTER 175 45 . 7 7 288 40 + 063 1 1 176 1 1 289 34 x → y 064 0 0 177 40 + 290 44 1 STO 1 065 42, 7, 9 9 178 20 x 291 2 2 066 42, 10, 8 8 179 32 . 2 GSB . 292 7 7 067 42, 7, 4 f FIX 180 45 1 RCL 1 293 5 5 068 2 2 181 40 + 294 20 x 069 10 ÷ 182 36 ENTER 29	057	45 .4		170	44 9	STO 9	283	0	0
060	058	30	_	171	43 32	g RTN	284	1	1
061 43 8	059	42 3	$\boxed{f} \longrightarrow RAD$	172	42,21,15	f LBL E	285	3	3
062 36 ENTER 175 45 .7 7 288 40	060	44 9	STO 9	173	43 2	$g \rightarrow H$	286	48	
062	061	43 8	g RAD	174	44 4	STO 4	287	5	5
064 0 0 177 40 + 290 44 1 STO 1 065 42, 7, 9 f FIX 178 20 x 291 2 2 066 42, 10, 8 f SOLVE 179 32 . 2 GSB . 292 7 7 067 42, 7, 4 f FIX 180 45 1 RCL 1 293 5 5 068 2 2 181 40 + 294 20 x 069 10 ÷ 182 36 ENTER 295 9 9 070 25 TAN 183 36 ENTER 296 10 ÷ 071 45 . 5 S 184 45 . 8 RCL . 297 43 44 G INT	062	36	ENTER	175	45 .7	RCL . 7	288	40	+
065 42, 7, 9 f FIX 9 178 20 x 291 2 2 066 42, 10, 8 f SOLVE 8 179 32 . 2 GSB . 292 7 7 067 42, 7, 4 f FIX 4 180 45 1 RCL 1 293 5 5 068 2 2 181 40 + 294 20 x 069 10 ÷ 182 36 ENTER 295 9 9 070 25 TAN 183 36 ENTER 296 10 ÷ 071 45 . 5 5 184 45 . 8 RCL . 297 43 44 GINT	063	1	1	176	1	1	289	34	x↔y
065 42, 7, 9 9 066 42,10, 8 f SOLVE 179 32 .2 2 20 x 292 7 7 7 067 42, 7, 4 180 45 1 RCL 1 293 5 5 068 2 2 181 40 + 294 20 x 069 10 ÷ 182 36 ENTER 295 9 9 070 25 TAN 183 36 ENTER 296 10 ÷ 071 45 .5 5 184 45 .8 RCL . 297 43 44 G INT	064	0	0	177	40	+	290	44 1	STO 1
066 42,10,8 8 067 42,7,4 f FIX 180 45 1 RCL 1 293 5 5 5 068 2 2 181 40 + 294 20 × 295 9 9 9 070 25 TAN 183 36 ENTER 296 10 297 43 44 G 184 45 .8 8	065	42, 7, 9	\sim	178	20	×	291	2	2
067 42, 7, 4 4 068 2 2 069 10 ÷ 070 25 TAN 183 36 ENTER 296 10 297 43 44 45 184 45 8	066	42,10, 8		179	32 .2		292	7	7
069 10 ÷ 182 36 ENTER 295 9 9 070 25 TAN 183 36 ENTER 296 10 ÷ 071 45 .5 RCL . 184 45 .8 RCL . 297 43 44 G INT	067	42, 7, 4		180	45 1	RCL 1	293	5	5
070 25 TAN 183 36 ENTER 296 10 ÷ 071 45 .5 RCL . 184 45 .8 RCL . 297 43 44 G INT	068	2	2	181	40	+	294	20	×
071 45 .5 RCL . 184 45 .8 RCL . 297 43 44 g int	069	10	÷	182	36	ENTER	295	9	9
0/1 45 .5 5 184 45 .8 8 29/ 43 44 g ini	070	25	TAN	183	36	ENTER	296	10	÷
072 20 x 185 40 + 298 40 +	071	45 .5	\sim	184	45 .8		297	43 44	gINT
	072	20	x	185	40	+	298	40	+

073	43 25	g TAN-1	186	32 2	GSB 2	299	34	x↔y
074	2	2	187	44 5	STO 5	300	36	ENTER
075	20	×	188	34	x↔y	301	42, 4, 1	f X ↔
076	43 3	g →DEG	189	32 2	GSB 2	302	9	9
077	43 7	g DEG	190	34	x ↔ y	303	40	+
078	45 .4	RCL .	191	42,21, 9	f LBL 9	304	1	1
079	40	+	192	42 2	f →H.MS	305	2	2
080	44 .0	STO	193	34	$x \leftrightarrow y$	306	10	÷
081	45 .0	RCL .	194	42 2	f →H.MS	307	43 44	gINT
082	23	SIN	195	43 32	g RTN	308	40	+
083	45 .6	RCL .	196	42,21, 0	f LBL 0	309	7	7
084	24	cos	197	1	1	310	20	×
085	20	×	198	36	ENTER	311	4	4
086	45 .0	RCL .	199	0	0	312	10	÷
087	24	cos	200	32 1	GSB 1	313	43 44	gINT
088	43 1	g →P	201	2	2	314	16	CHS
089	33	R↓	202	4	4	315	40	+
090	44 9	STO 9	203	1	1	316	45 1	RCL 1
091	45 .0	RCL .	204	5	5	317	3	3
092	23	SIN	205	0	0	318	6	6
093	45 .6	RCL .	206	2	2	319	7	7
094	23	SIN	207	0	0	320	20	×
095	20	×	208	30	_	321	40	+
096	43 23	g SIN ⁻¹	209	3	3	322	44 6	STO 6
097	44 .0	STO .	210	6	6	323		g RTN
098	45 9	RCL 9	211	5	5	324	42,21,14	f LBL D
099	42,21, .1	f LBL .	212	2	2	325	32 15	
100	45 5	RCL 5	213	5	5	326	32 .1	GSB .
101	32 .8	GSB .	214	10	÷	327		gRTN
102	45 9	RCL 9	215	36	ENTER	328	42,21, .5	f LBL .
103	30	_	216	36	ENTER	329	45 5	RCL 5

104	40	+	217	48		330	45 .8 RCL .
105	32 2	GSB 2	218	0	0	331	30 _
106	44 .2	STO . 2	219	0	0	332	32 .8 GSB .
107	32 7	GSB 7	220	0	0	333	45 9 RCL 9
108	43 32	g RTN	221	0	0	334	30 _
109	42,21, 7	f LBL 7	222	2	2	335	40 +
110	45 .2	RCL .	223	5	5	336	32 2 GSB 2
111	24	cos	224	8	8	337	45 .0 RCL .
112	45 8	RCL 8	225	1	1	338	22 9 GTO 9