

Problem 1

a) At time $t=0$, $\epsilon(0) = \epsilon_0$. At the instantaneous application of stress, the visco-elastic body has no instantaneous viscous response.

Under this assumption, we may neglect the viscosity term by taking $\eta \rightarrow \infty$ in the constitutive equation, therefore reducing it to $\dot{\epsilon} = \frac{\dot{\sigma}}{K}$.

Integrating, we find that $\epsilon_0 = \frac{\sigma_0}{K}$, or that the initial stress on the body is $\sigma(t=0) = K \epsilon_0$.

b) Now, consider when $t > 0$. We may perform a variable separation to solve the constitutive equation for $\sigma(t)$:

$$\dot{\epsilon} = \frac{\dot{\sigma}}{K} + \frac{\sigma}{\eta}$$

Since $\epsilon(t)$ is constant, $\dot{\epsilon} = 0$, and therefore

$$0 = \frac{\dot{\sigma}}{K} + \frac{\sigma}{\eta} \Rightarrow \frac{d\sigma}{dt} = -\frac{K}{\eta} \sigma$$

$$\frac{d\sigma}{\sigma} = -\frac{K}{\eta} dt \Rightarrow \int_{\sigma_0}^{\sigma(t)} \frac{d\sigma'}{\sigma'} = -\frac{K}{\eta} \int_0^t dt'$$

Hence

$$\log |\sigma| \Big|_{\sigma_0}^{\sigma(t)} = -\frac{K}{n} t$$

$$\log |\sigma(t)| - \log |\sigma_0| = -\frac{K}{n} t.$$

$$\Rightarrow \sigma(t) = \sigma_0 e^{-\frac{K}{n} t}$$

or

$$\sigma(t) = e_0 K e^{-\frac{K}{n} t}$$

Problem 2

- a) The restoring force on the mantle may be determined by comparing the forces in the two columns, such as by taking the difference $\Delta F = F_2 - F_1$.

On column 1 (centre column),

$$\begin{aligned} F_1 &= F_{\text{mantle}} + F_{\text{water}} \\ &= (D-d) g \rho_m SA + d g \rho_w SA \end{aligned}$$

And on column 2,

$$F_2 = D g \rho_m SA. \quad (\text{Just mantle force}).$$

$$\text{Therefore } \Delta F = \cancel{D g \rho_m SA} - \cancel{D g \rho_m SA} + d g \rho_m SA - d g \rho_w SA$$

$$F_{\text{res}} = d g SA (\rho_m - \rho_w)$$

which is the restoring force on the mantle. Note that

$d = b(t)$, hence

$$F_{\text{res}} = b(t) g SA (\rho_m - \rho_w)$$

The net stress is then $\sigma(t) = \frac{F_{\text{res}}(t)}{SA}$, or

$$\sigma(t) = b(t) g (\rho_m - \rho_w)$$

where $\sigma(0) = d g (\rho_m - \rho_w)$.

b) To determine $b(t)$, we may apply the constitutive equation:

$$\dot{\epsilon} = \frac{\dot{\sigma}}{K} + \frac{\sigma}{\eta}.$$

Since the strain rate $\dot{\epsilon}$ is equivalent to the column lengthening rate, $-\frac{\dot{b}}{D}$, hence

$$-\frac{\dot{b}}{D} = \frac{\dot{b} g(P_m - P_w)}{K} + \frac{b g(P_m - P_w)}{\eta}.$$

Variable separation yields

$$-\dot{b} \left(\frac{1}{D} + \frac{g(P_m - P_w)}{K} \right) = b \frac{g(P_m - P_w)}{\eta}$$

$$\dot{b} = - \frac{g(P_m - P_w)}{\eta} \cdot \left(\frac{1}{D} + \frac{g(P_m - P_w)}{K} \right)^{-1} b$$

Which therefore yields

$$b(t) = b(t=0) \cdot \exp \left\{ - \frac{g}{\eta} (P_m - P_w) \cdot \left(\frac{1}{D} + \frac{g(P_m - P_w)}{K} \right)^{-1} t \right\}.$$

Simplification of the term in the argument of the exponential, with noting that $b(t=0) = d$, we obtain the expression for $b(t)$:

$$b(t) = d \exp \left\{ \frac{-g(P_m - P_w)D}{\eta(K + gD(P_m - P_w))} t \right\}$$

c) To determine t_{exp} , we wish to solve when

$$\exp \left\{ \frac{-g(P_m - P_w) D}{\eta(K + gD(P_m - P_w))} t \right\} = \exp \{-1\}$$

Hence

$$t_{exp} \cdot \frac{g(P_m - P_w) D}{\eta(K + gD(P_m - P_w))} = 1,$$

which yields the exponential decay constant time

$$t_{exp} = \frac{\eta(K + gD(P_m - P_w))}{g(P_m - P_w) D}$$

$$\boxed{t_{exp} = \frac{\eta K}{g(P_m - P_w) D} + \eta}$$

d) Upon rearranging the exponential decay term previously found, we find that

$$\eta = \frac{t_{exp} \cdot D K g(P_m - P_w)}{K + gD(P_m - P_w)},$$

With $t_{exp} \approx 3'000 \text{ yr} = 9,4608 \times 10^{10} \text{ s}$,

$P_m = 3'300 \frac{\text{kg}}{\text{m}^3}$, $P_w = 1'000 \frac{\text{kg}}{\text{m}^3}$, $g = 10 \frac{\text{m}}{\text{s}^2}$,

$D = 2'400'000 \text{ m}$, and $K = 8 \times 10^{10} \text{ Pa}$, we find

$$\eta = \frac{(9.4608 \times 10^{-10} \text{ s})(2.9 \times 10^{-6} \text{ m})(8 \times 10^9 \text{ Pa})(10 \frac{\text{m}}{\text{s}^2})(2300 \frac{\text{kg}}{\text{m}^3})}{(8 \times 10^9 \text{ Pa}) + (2.9 \times 10^{-6} \text{ m})(10 \frac{\text{m}}{\text{s}^2})(2300 \frac{\text{kg}}{\text{m}^3})}$$

$$\boxed{\eta = 3.44 \times 10^{21} \text{ Pa-s}}$$

c) The current rate of change is given by differentiation of $b(t)$,

$$\frac{db}{dt} = - \left(\frac{DKg(Am - Pw)}{\eta(K + Dg(Am - Pw))} \right) b(t) \Big|_{b(t)=30 \text{ m}}$$

$$\left| \frac{db}{dt} \right| = 30 \text{ m} \cdot \left(\frac{(2.9 \times 10^{-6} \text{ m})(8 \times 10^9 \text{ Pa})(10 \frac{\text{m}}{\text{s}^2})(2300 \frac{\text{kg}}{\text{m}^3})}{(3.44 \times 10^{21} \text{ Pa-s}) [8 \times 10^9 \text{ Pa} + (2.9 \times 10^{-6} \text{ m})(10 \frac{\text{m}}{\text{s}^2})(2300 \frac{\text{kg}}{\text{m}^3})]} \right)$$

$$= 3.17211 \times 10^{-10} \frac{\text{m}}{\text{s}}$$

Which, by converting to mm/yr, yields

$$\boxed{\dot{b} = 9.98 \text{ mm/yr}}$$

Compared with the Lecture literature value of 9 mm/yr,

this value of lake-depth change is approximately equivalent.

This is as expected.

Problem 3

- 2) If only radiogenic heat is being produced, the amount of heat produced in an infinitesimal time dt is

$$dQ = H dm dt.$$

Integrated over the whole mass yields the total heat production,

$$Q = HM dt.$$

The heat flux Φ is given by heat/unit area · unit time,

which implies that

$$\Phi = \frac{Q}{A dt} \Rightarrow \boxed{\Phi = \frac{HM}{A}}$$

- b) This total heat flux may be represented by the relation

$$\Phi_{tot} = \frac{K(T-T_s)}{d} \cdot \left(\frac{Ra}{Ra_c} \right)^{1/3}$$

where K : thermal conductivity, d : mantle depth, T : internal temperature, T_s : surface temperature, Ra : Rayleigh number, and Ra_c : critical Rayleigh number for convection.

Noting that $Ra \equiv \frac{g \alpha d^3}{K \nu} \Delta T$, we find that

$$\frac{HM}{A} = \frac{K(T-T_s)}{d} \left(\frac{g \alpha d^3}{K \nu Ra_c} \right)^{1/3} (T-T_s)^{1/3}$$

with $\Delta T = T - T_s$.

Simple rearranging yields

$$(T - T_s)^{4/3} = \frac{MH}{AK} \left(\frac{g \propto}{K v R_{ac}} \right)^{1/3}$$

c) With $H(t) = H_0 e^{-\lambda t}$, $v = v_0 e^{A_0/T}$, differentiation with respect to time yields

$$\dot{H} = -\lambda H, \quad \dot{v} = -\frac{v A_0}{T^2} \frac{dT}{dt}$$

Then, by chain/product rule,

$$\frac{d}{dt} (T - T_s)^{4/3} = \frac{4}{3} (T - T_s)^{1/3} \frac{dT}{dt} \quad \text{and}$$

$$\left(\text{Let } C_0 \equiv \frac{MH}{AK} \left(\frac{g \propto}{K R_{ac}} \right)^{1/3} \right)$$

$$\begin{aligned} \frac{d}{dt} [C_0 H v^{1/3}] &= C_0 \frac{dH}{dt} v^{1/3} + C_0 H \frac{1}{3} v^{-2/3} \frac{dv}{dt} \\ &= -\lambda C_0 H v^{1/3} + C_0 H \frac{1}{3} v^{-2/3} \left(-\frac{v A_0}{T^2} \right) \frac{dT}{dt} \\ &= C_0 H v^{1/3} \left[-\lambda - \frac{1}{3} \frac{A_0}{T^2} \frac{dT}{dt} \right] \end{aligned}$$

Setting LHS = RHS, and noting that $C_0 H v^{1/3} = (T - T_s)^{4/3}$,

$$\frac{4}{3} \Delta T^{1/3} \dot{T} = -\Delta T^{4/3} \left(\lambda + \frac{A_0}{3T^2} \dot{T} \right)$$

$$\Rightarrow \dot{T} \left(1 + \frac{A_0}{4T^2} \Delta T \right) = -\frac{3\lambda}{4} \Delta T$$

$$\Rightarrow \boxed{\frac{dT}{dt} = -\frac{3\lambda}{4} (T - T_s) \left[1 + \frac{A_0}{4T^2} (T - T_s) \right]^{-1}}$$

which is as required.

- d) First, note that if $T_s = 300 \text{ K}$ and $T = 2300 \text{ K}$, then $T - T_s = 2000 \text{ K}$ which is still in the order of magnitude of $\sim 2000 \text{ K}$. Therefore it is OK to neglect the $(T - T_s)$ term. This follows since $T - T_s \ll A_0 = 80'000 \text{ K}$.

The equation simplifies accordingly to

$$\begin{aligned}\frac{dT}{dt} &= -\frac{3\lambda}{4} (T - T_s) \left[\frac{A_0}{4T^2} (T - T_s) \right]^{-1} \\ &= -\frac{3\lambda T^2}{A_0},\end{aligned}$$

Hence $\boxed{\dot{T} = -\frac{3\lambda T^2}{A_0}}$

- e) The cooling rate, given that $T = \sim 2300 \text{ K}$,

$\lambda = 1.42 \times 10^{-17} \text{ s}^{-1}$, and $A_0 = 8 \times 10^4 \text{ K}$, is

therefore just

$$\begin{aligned}\dot{T} \Big|_{T=2300 \text{ K}} &= -\frac{3 \cdot (1.42 \times 10^{-17} \text{ s}^{-1})}{8 \times 10^4 \text{ K}} (2300 \text{ K})^2 \\ &= -5.634 \times 10^{-15} \frac{\text{K}}{\text{s}}\end{aligned}$$

or $\boxed{\dot{T} = 1.777 \times 10^{-7} \frac{\text{K}}{\text{yr}}}$ is the cooling rate.

f) We have the ODE $\frac{dT}{dt} = -\frac{3\lambda}{A_0} T^2$,

which, by variable separation, is

$$\int \frac{dT}{T^2} = -\frac{3\lambda}{A_0} \int dt$$

$$-\frac{1}{T} = -\frac{3\lambda}{A_0} t + T_0$$

$$\Rightarrow \boxed{T(t) = \frac{A_0}{3\lambda t} + T_0'}$$

where T_0' is an initial condition.

To find T_0' , we may invoke the condition that at

$t = 4.54$ byr (current time), if $A_0 = 8 \times 10^4$ K,

$\lambda = 1.42 \times 10^{-17} \text{ s}^{-1}$, the current average mantle temperature

is 2300 K.

$$2300 \text{ K} = \frac{A_0}{3\lambda (4.54 \text{ byr})} + T_0'$$

$$\Rightarrow T_0' = 2300 \text{ K} - \frac{A_0}{3\lambda \cdot 4.54 \text{ byr}}$$

$4.54 \text{ byr} \approx 1.4327 \times 10^{17} \text{ s}$, hence

$$T_0' = 2300 \text{ K} - \frac{80000}{3(1.42 \times 10^{-17} \text{ s}^{-1})(1.4327 \times 10^{17} \text{ s})}$$

$$\approx -10'807,5211 \text{ K}.$$

When $t \rightarrow 0$ (earth formation), $T \rightarrow \infty$, which is not

possible. This is why this may not be a good estimate

for earth's initial mantle temperature.