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Homework 2 - Serial-Link Manipulator Kinematics

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In order to derive the Forward Kinematics, one should inspect the constants and variables on the constituent parts of the robot. There are 3 links, which have fixed lengths a_1 , a_2 and a_3 . We can easily see them as constant translations that have to be included to the Transformation operation. Also, there are 3 **revolute** joints, which can rotate, hence manipulate their own orientations. These rotations are directly controlled with θ_1 , θ_2 and θ_3 angles. In order to map points in frame E to frame O , we should just calculate the all rotations and translations, starting from the frame O up until frame E . For the math, see below:

$$f(\theta_1, \theta_2, \theta_3) = R(\theta_1) * T_x(a_1) * R(\theta_2) * T_x(a_2) * R(\theta_3) * T_x(a_3)$$

I want to clarify some possible confussions in here. Since this is a planar robot, there is only one rotational dimension. Hence, rotation operation R refers to it. Moreover, even though the link lengths seem as somewhat combination of $x - y$ dimensions, all rotational operations just before the translational operations T_x , align new x frame to the link direction exactly. Therefore, all T_x operations remain valid.

Writing all as homogeneous transformation matrices in a row and applying matrix multiplication from right-to-left:

$$\begin{bmatrix} \cos(\theta_3) & -\sin(\theta_3) & 0 \\ \sin(\theta_3) & \cos(\theta_3) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & a_3 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos(\theta_2) & -\sin(\theta_2) & 0 \\ \sin(\theta_2) & \cos(\theta_2) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & a_2 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos(\theta_1) & -\sin(\theta_1) & 0 \\ \sin(\theta_1) & \cos(\theta_1) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & a_1 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} = {}^O T_E$$

Writing the result directly:

$${}^O T_E = \begin{bmatrix} \cos(\theta_3 + \theta_2 + \theta_1) & -\sin(\theta_3 + \theta_2 + \theta_1) & a_3 \cos(\theta_3 + \theta_2 + \theta_1) + a_2 \cos(\theta_2 + \theta_1) + a_1 \cos(\theta_1) \\ \sin(\theta_3 + \theta_2 + \theta_1) & \cos(\theta_3 + \theta_2 + \theta_1) & a_3 \sin(\theta_3 + \theta_2 + \theta_1) + a_2 \sin(\theta_2 + \theta_1) + a_1 \sin(\theta_1) \\ 0 & 0 & 1 \end{bmatrix}$$

Consequently, these chains of rotations and translations produce a homogeneous transformation matrix, which maps points from E to O . Because, while the function above

pushes the operations from left-to-right, the frame E pops the operations from right-to-left and applies in that order. It is now clear that this is an exact homogeneous transformation from E to O , which can be denoted as ${}^O T_E$.

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For simplicity, assume ${}^O T_E^* = [x_d, y_d, \theta_d]$, which is the desired pose in SE(2). From the previous problem, we know that ${}^O T_E^* = f(\theta_1^*, \theta_2^*, \theta_3^*)$. This directly brings us the relation $(\theta_1^*, \theta_2^*, \theta_3^*) = f^{-1}({}^O T_E^*)$. Since $\theta_1^*, \theta_2^*, \theta_3^* \in S^1$, the function f^{-1} is properly set as $SE(2) \rightarrow S^1 \times S^1 \times S^1$. Now the problem reduces to derivation of inverse kinematic equations. In the previous question, the equations:

$$\begin{aligned} x_d &= a_3 \cdot \cos(\theta_3 + \theta_2 + \theta_1) + a_2 \cdot \cos(\theta_2 + \theta_1) + a_1 \cdot \cos(\theta_1) \\ y_d &= a_3 \cdot \sin(\theta_3 + \theta_2 + \theta_1) + a_2 \cdot \sin(\theta_2 + \theta_1) + a_1 \cdot \sin(\theta_1) \\ \theta_d &= \theta_1 + \theta_2 + \theta_3, \end{aligned}$$

were derived. Finding $(\theta_1, \theta_2, \theta_3)$ is a rigorous process through the equations above and might not have an analytical solution at all.

Let's call the last joint as $w(wrist)$. Since we both know θ_d and a_3 , applying inverse transformations to x_d, y_d will produce x_w, y_w for further usage, and wrist position will be very useful on the IK calculation. Below is the computation procedure:

$$\begin{bmatrix} 1 & 0 & a_3 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos\theta_d & -\sin\theta_d & 0 \\ \sin\theta_d & \cos\theta_d & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & x_w \\ 0 & 1 & y_w \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \cos\theta_d & -\sin\theta_d & x_d \\ \sin\theta_d & \cos\theta_d & y_d \\ 0 & 0 & 1 \end{bmatrix}$$

The relations at the end are:

$$x_d = \cos\theta_d x_w - \sin\theta_d y_w + a_3,$$

$$y_d = \sin\theta_d x_w + \cos\theta_d y_w$$

x_w and y_w can be straightforwardly computed from above equations. They can be also written in terms of a_1, a_2, θ_1 and θ_2 . Below are those equations (further applying necessary Trigonometric Identities):

$$x_w = a_1 \cos\theta_1 + a_2 (\cos\theta_1 \cos\theta_2 - \sin\theta_1 \sin\theta_2)$$

$$y_w = a_1 \sin\theta_1 + a_2 (\cos\theta_1 \sin\theta_2 + \sin\theta_1 \cos\theta_2)$$

Taking squares and isolating $\cos\theta_2$:

$\frac{x_w^2 + y_w^2 - a_1^2 - a_2^2}{2a_1a_2} = k = \cos\theta_2$, Observe that right hand side of the equation will not produce an expression that involves variable. All terms at lhs are known in advance. Hence $\theta_2 = \arccos(k)$.

In order to compute θ_1 , some more relations are necessary to be added. Those are:

$$x_w = k_1 \cdot \cos\theta_1 - k_2 \sin\theta_1$$

$$y_w = k_1 \cdot \sin\theta_1 + k_2 \cos\theta_1, \text{ where}$$

$$k_1 = a_1 + a_2 \cos\theta_2, \quad k_2 = a_2 \sin\theta_2.$$

Note that $\gamma + \theta_1$ is the ccw angle between Frame $\{0\}$ and Frame $\{W\}$. It is straightforward to compute this combined angle from x_w and y_w magnitudes. $\rightarrow \gamma + \theta_1 = \arctan(y_w, x_w)$. Adding two more relations will be enough to solve for θ_1 . Those are:

$$k_1 = r \cos\gamma$$

$$k_2 = r \sin\gamma, \text{ where } r \text{ is simply the length between wrist and origin. } \mathbf{Final equations:}$$

$$\theta_1 = \arctan(y_w, x_w) - \arctan(k_2, k_1)$$

$$\theta_2 = \arccos(k)$$

$$\theta_3 = \theta_d - \theta_1 - \theta_2.$$

3

Following the hint, I will start with the derivation of $c'(\gamma)$. Since $c(\gamma)$ is a column vector in 2D, derivation must be applied to both units in x and y dimensions. Below is the derivative:

$$c'(\gamma) = \begin{bmatrix} -10\pi \sin(2\pi\gamma) + 2\pi \cos(14\pi\gamma) + 10\pi \cos(12\pi\gamma) \cos(2\pi\gamma) \\ 10\pi \cos(2\pi\gamma) + 2\pi \sin(14\pi\gamma) + 10\pi \cos(12\pi\gamma) \sin(2\pi\gamma) \end{bmatrix}$$

Now, let's inspect this expression. $c'(\gamma)$ is the vector equation of the tangent to the curve for any given γ . Aligning this with \hat{E}_y simplifies the question further. Since the end effector is $\in SE(2)$, the \hat{E}_x must be orthogonal to \hat{E}_y . We already know that, two orthogonal vectors have 0 dot-product. Moreover, since this is a right-handed coordinate system, \hat{E}_x will have an orientation according to angle:

$$\arctan(c'(\gamma)(2), c'(\gamma)(1)) - \pi/2, \text{ where } c'(\gamma)(x) \text{ refers to MATLAB type indexing.}$$

Having computed the orientations of end-effector coordinate frames for any given γ , let's get back to the beginning of the problem. Assuming the orientation of the end-effector is not important, we can easily conclude that:

$${}^oT_E(\gamma) = \begin{bmatrix} I_{2 \times 2} & c(\gamma) \\ 0 & 1 \end{bmatrix}$$

Actually, translational part will remain as is. Only addition will be done through replacement of $I_{2 \times 2}$ with a $R(\theta)$ that assures the orthogonality of end-effector to the curve. In fact, the computation of θ is already done above:

$$\theta = \arctan(c'(\gamma)(2), c'(\gamma)(1)) - \pi/2$$

The final form of ${}^oT_E(\gamma)$ is below. Since, θ and $c(\gamma)$ is already known, I'm writing the compact form.

$${}^oT_E(\gamma) = \begin{bmatrix} R(\theta)_{2 \times 2} & c(\gamma)_{2 \times 1} \\ 0_{1 \times 2} & 1 \end{bmatrix}, \text{ where } R(\theta) = \begin{bmatrix} \cos(\theta) & -\sin(\theta) \\ \sin(\theta) & \cos(\theta) \end{bmatrix}$$

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In order to find minimum a_1 , the maximum distance on the curve from the origin should be calculated. Since the parametric formula is in our hands, computing $\frac{\frac{dy}{d\gamma}}{\frac{dx}{d\gamma}} = 0$ for γ will approximately solve the problem. Of course, γ will have many values from the equation above. Carefully picking one that corresponds to a maximum value is enough. Hence, I'm picking $\gamma = 0.31831(0.673542 + \pi)$ from Wolfram website. The rest is straightforward. Replacing γ with above magnitude in $c(\gamma)$ produces the maximum of the curvature:

$\begin{bmatrix} 0.2651 \\ 1.1650 \end{bmatrix}$, basically a point on the curve, which has the maximum distance from the origin.

Let's compute the magnitude of this length, which is $\sqrt{(0.2651)^2 + (1.1650)^2} = 1.1948$. So, minimum $a_1 = 1.1948 - 0.5 - 0.2 = 0.4948$.