

CONTROL SYSTEMS

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UNIT 5: STABILITY IN THE FREQUENCY DOMAIN

Introduction

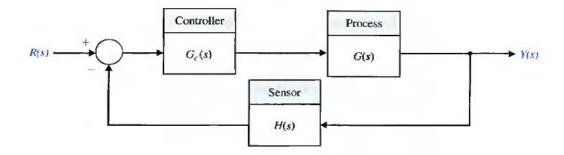
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Introduction



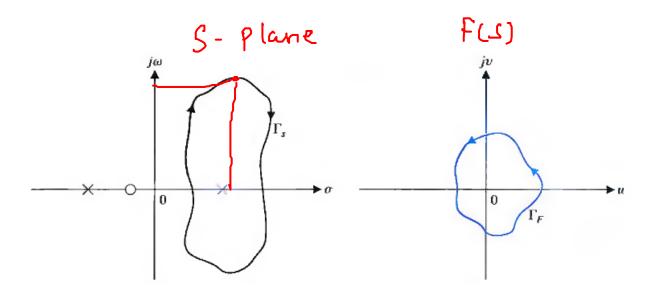
- The major advantage of Polar Plot lies in stability study of systems
- Harry Nyquist related the stability of a dynamical system to these plots (1932 at Bell Labs)
- His work on Polar plots (applied to stability of systems) are called as Nyquist
 Plots



Introduction



- Given open loop frequency response , Nyquist Plots determines closed loop system stability
- For a given continuous closed path in the s-plane that does not go through the singular points, there corresponds a closed curve in the F(s) plane.



Introduction



- Number and direction of encirclements plays an important role in the stability of the system.
- For each point in the s-plane , there corresponds a point in the F(s) plane. i.e., for $s = \sigma + j\omega$, there would be F(s) = u + jv in F(s) plane. This is called mapping.



UNIT 5: STABILITY IN THE FREQUENCY DOMAIN

Mapping of Contours in s - plane

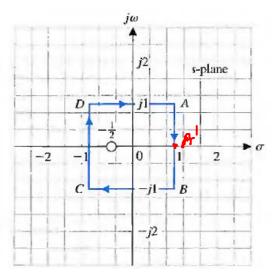
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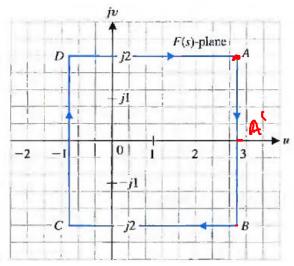
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Mapping of Contours in s - plane

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- A contour map is a contour or trajectory in one plane mapped or translated into another plane by a relation F(s).
- For example, F(s) = 2s + 1 $S = 6 + j \omega, \quad F(s) = a(6 + j \omega) + l$ $= 26 + j + j 2 \omega$
- This type of mapping, which retains the angles of the s-plane contour on the F(s)plane is called conformal mapping.





$$G = \{1, \frac{1}{2} = 1\}$$
 $A = \{1 + \frac{1}{2}\}$
 $F(S) = 3 + 2\frac{1}{2}$
 $F(S) = 3 + 2\frac{1}{2}$
 $F(S) = 3$
 $F(S) = 3 - 2\frac{1}{2}$
 $F(S) = -1 - 2\frac{1}{2}$
 $F(S) = -1 + 2\frac{1}{2}$

Mapping of Contours in s - plane

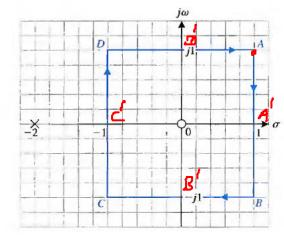


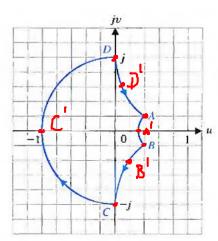
For example,
$$F(s) = \frac{s}{s+2}$$

$$F(s) = (\sigma + j w) (\sigma + 2 - j w)$$

$$(\sigma + 2)^{2} + w^{2}$$

$$= \frac{(^{2}+w^{2}+1)^{2}+w^{2}}{(^{2}+2)^{2}+w^{2}} + \frac{1}{(^{2}+2)^{2}+w^{2}}$$





Mapping of Contours in s - plane



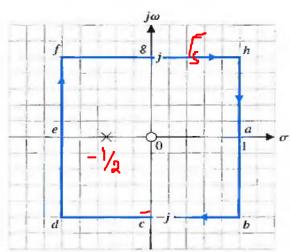
Cauchy's Theorem(Principle of Argument)

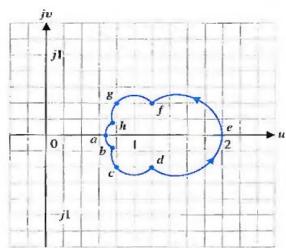
If a contour Γ_S in the s- plane encircles z zeros and p poles of F(s) and does not pass through any pole or zero of F(s) and the traversal is in the clockwise direction along the contour, the corresponding contour Γ_F in the F(s) plane encircles the origin of the F(s) – plane N = Z – P times in the clockwise direction

$$F(s) = \frac{s}{s + 1/2}$$

$$P = 1$$

$$N = 1 - 1 = 0$$

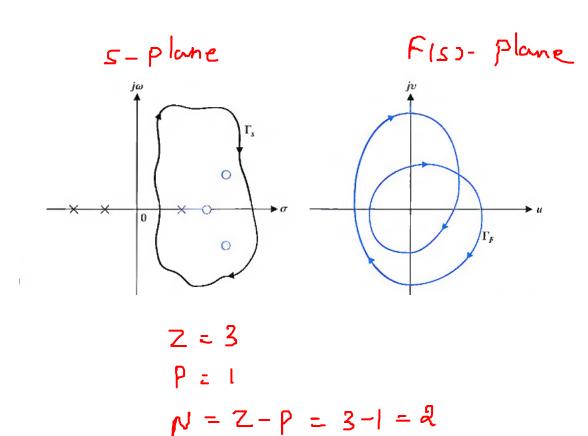




Mapping of Contours in s - plane



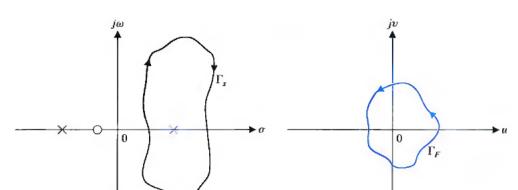
$$2 = 3$$
 $P = 1$
 $N = 2 - p$
 $= 3 - 1$



Mapping of Contours in s - plane



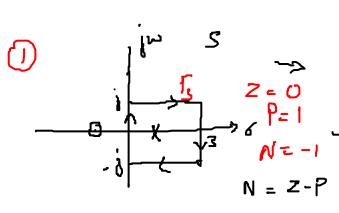
Different closed contours in s – plane gives rise to different closed curves in F(s) – plane.

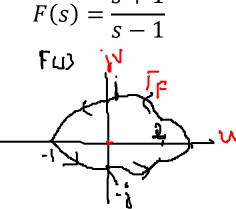


Mapping of Contours in s - plane

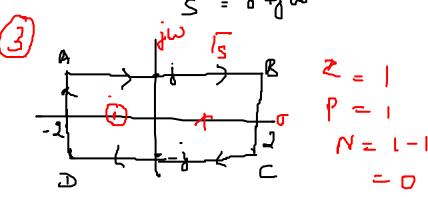


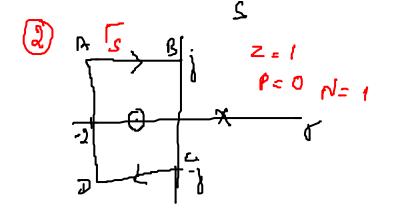
Different closed contours in s – plane gives rise to different closed curves in F(s) – plane.

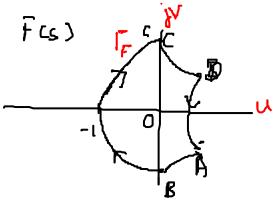


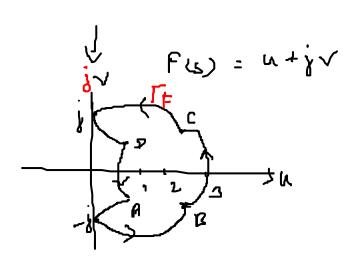














UNIT 4: STABILITY IN THE FREQUENCY DOMAIN

Nyquist Stability Criterion

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Nyquist Stability Criterion

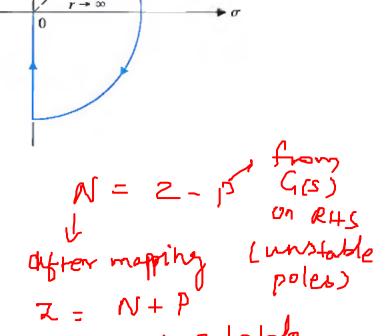
The Nyquist path encloses the entire RHS plane and encloses all the zeros and poles of 1 + G(s)H(s) that have positive real parts.

In general,
$$G_1(S)H(S) = K(S+Z_1)(S+Z_2)---(S+Z_m)$$
 _ () $(S+P_1)(S+P_2)---(S+P_n)$

C.E,
$$F(s) = |+ (\eta(s) H(s) = 0)$$

= $|+ (s+z_1)(s+z_2) \cdot - \cdot (s+z_m)| = 0$
 $(s+R)(s+P_2) \cdot - \cdot (s+P_n)$
 $(s+P_1)(s+P_2) \cdot - \cdot (s+z_m)| = 0$ (2)
 $(s+P_1)(s+P_2) \cdot - \cdot (s+z_m)| = 0$





Nyquist contour

Nyquist Stability Criterion

$$G(s) H(s) = \frac{S+1}{(S+2)(S-1)}$$

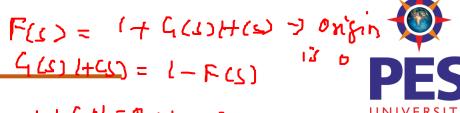


Comparing equations 1 & 2,

- we observe that the poles of F(s) and poles of G(s)H(s) are same.
- The zeros of F(s) are the roots of characteristic equation.
- For the system to be stable, the roots of the characteristic equation must lie in the LHS plane. i.e., zeros of F(s) must lie in the LHS plane.
- The number of RH plane zeros of F(s) is equal to the number of poles 1+G(s)H(s) in the RH plus the number of encirclements of the origin of the F(s) plane. N=2-P

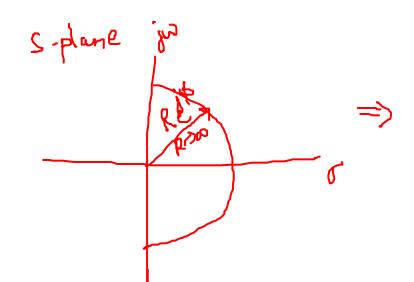
N=2-P
NO-OF
Z=N+P_>^poles of GLOPHUS) which lie in RHS of s-plane
Tunstable poles

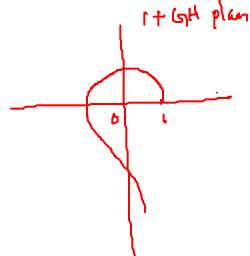
Nyquist Stability Criterion



$$F(s)=1+L(s) => L(s) = F(s) - 1 = F'(s)$$

GH. Plane







always mapping is between s-plane to GH plane instead of F=1+67H plane



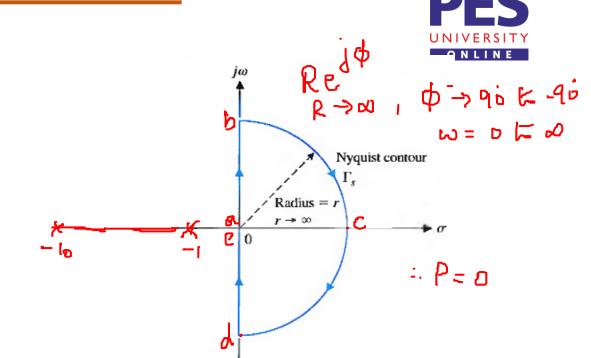
- A feedback system is stable if and only if the contour Γ_L in the L(s) plane does not encircle the (-1, 0) point when the number of poles of L(s) in the right hand s-plane is zero(P = 0)
- A feedback control system is stable if and only if, for the contour Γ_L , the number of encirclement of the (-1,0) point is equal to the number of poles of L(s) with positive real parts.
- The basis for the 2 statements lies in the following expression
- Z = N + P

Example,
$$L(s) = \frac{K}{(s+1)(0.1s+1)}$$

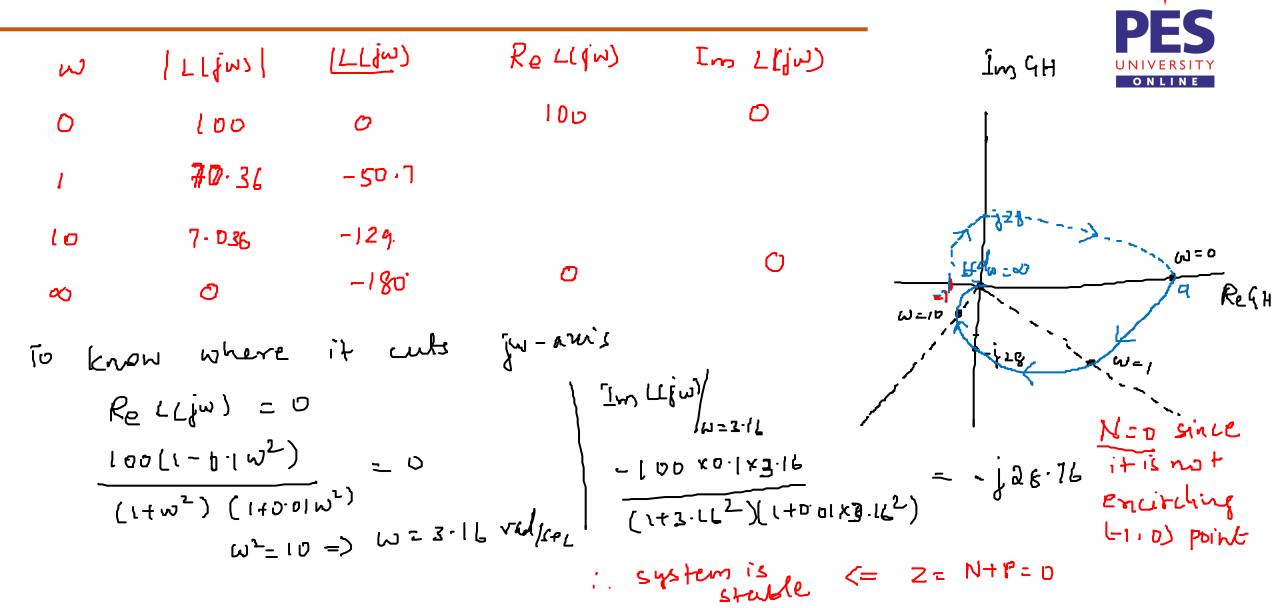
$$L(j\omega) = \frac{k}{(j\omega+1)(0-1j\omega+1)}$$
Let $K=100$

$$|L[[\omega]] = \frac{100}{[\omega^2 + 1] (\omega \cdot (\omega)^2 + 1)}$$

$$L(Jw) = \frac{100 (1-jw)(1-0.1 \sqrt{w})}{(w^2+1)((0.1 \sqrt{w})+1)}$$



$$= \frac{100(1-0.1 M^2) - i(100 \times 1.1 M)}{(M^2 + 1)(0.01 M^2 + 1)}$$





$$L(s) = \lim_{R \to \infty} \frac{100}{(1 + Re^{i\phi})(0 - 1Re^{i\phi} + 1)} = \lim_{R \to \infty} \frac{100}{Re^{i\phi} \times 0 - 1Re^{i\phi}} = \lim_{R \to \infty} \frac{100}{0 - 1Re^{i\phi}}$$

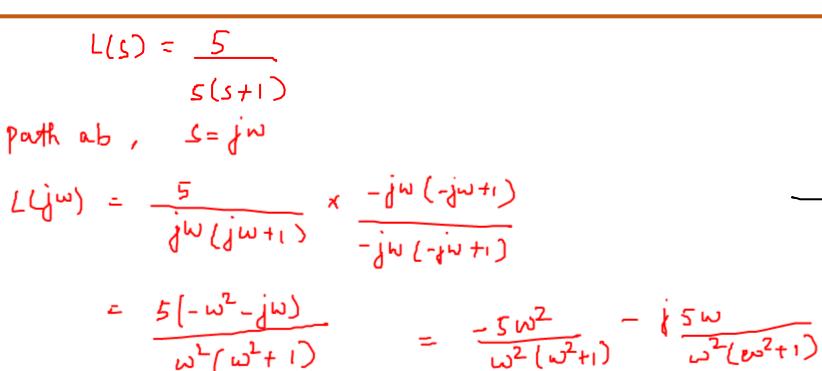
$$= 0, e^{-i2\phi}$$

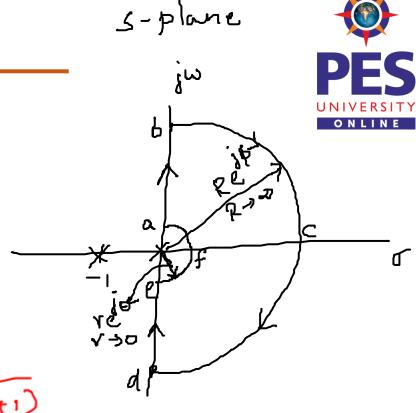
path de,
$$S = -j\omega$$
, $\omega = -00$ 50
mirror image of path ab

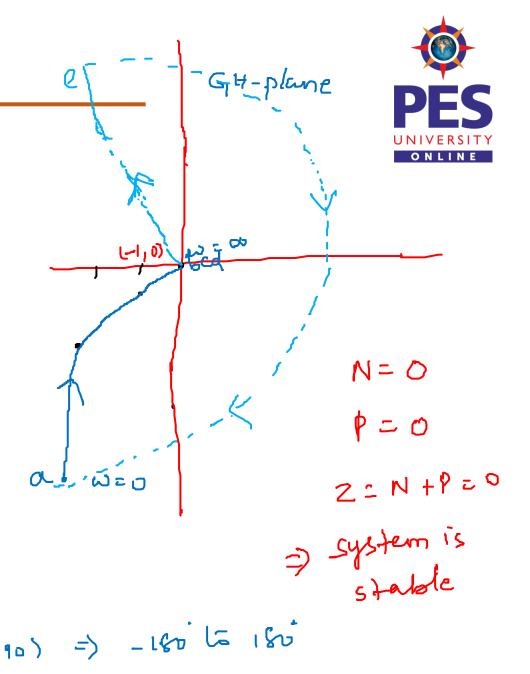


$$C_{21}$$
 $S = Re^{i\theta}$, $R \to \infty$

Nyquist Stability Criterion – Example 2

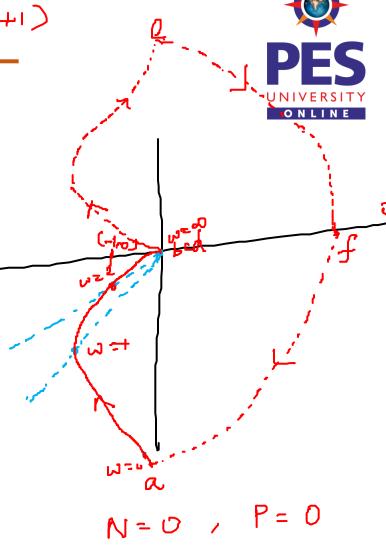






Nyquist Stability Criterion

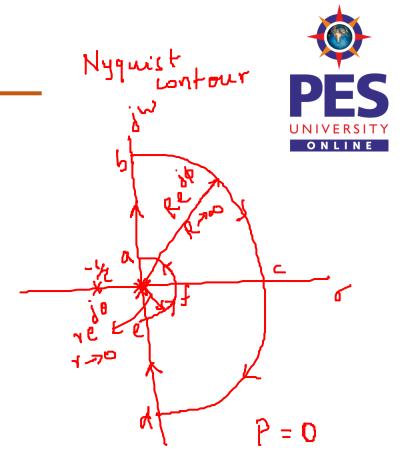
for path ab



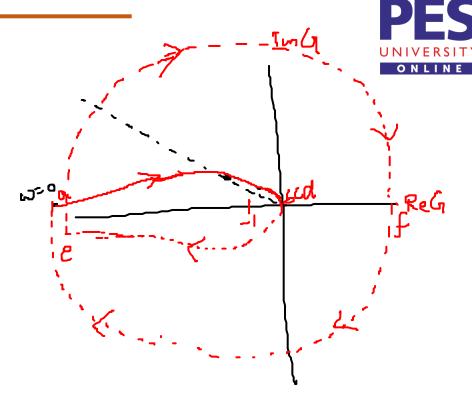
Nyquist Stability Criterion – Example 3

fx3, G(s) =
$$\frac{K}{s^2(zs+1)}$$

sol: path ab, $s = jw$, $K = 1$, $\ell = 1$
 $|G(jw)| = \frac{1}{w^2 \sqrt{w^2 + 1}}$
 $|G(jw)| = \frac{1}{-w^2(jw+1)} \times \frac{1-jw}{(1-jw)}$
 $= \frac{1}{-1+jw}$



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1	4-707	- 225°		
2	0.11	-243		
ø	٥	– २ २ ७°		•
puth	6cd, <u>c</u> =	Response	φ ⇒ 90° -	6 1º
GLS) = lin [Reit) (Reit+1)				
	= livs RTO	R3 e355	β = D € , - 2	176 - 0 - 27

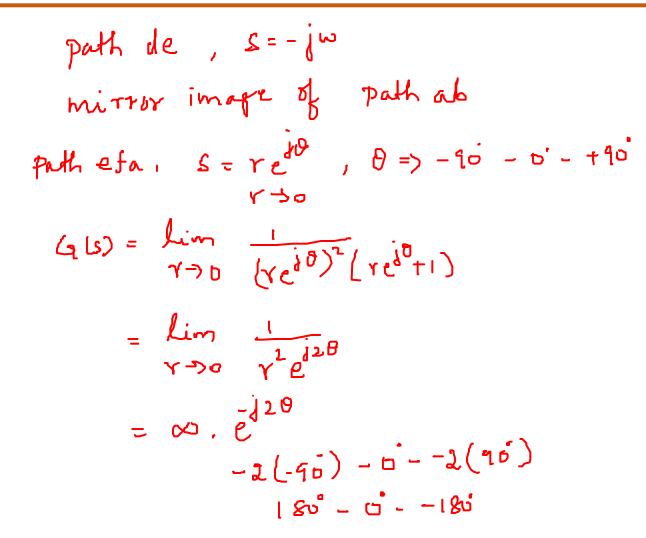


$$N = 2$$

$$P = 0$$

$$Z = 2+0 = 2$$

$$\Rightarrow \therefore \text{ system is unstable}$$





Polar plot for different type of systems



$$G_1(s) = \frac{k}{Z_{s+1}}$$

$$G(S) = \frac{k}{Z_{S+1}}$$

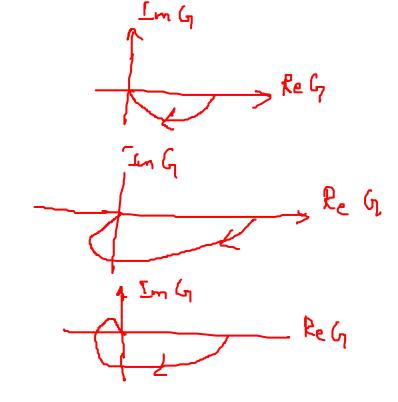
$$M = k$$

$$M = D$$

$$D = -90$$

$$G(\zeta) = \frac{1}{(\zeta_1 S_{71})(\zeta_2 S_{71})} \qquad M = K$$

$$\phi = 0$$



Polar plot for different type of systems

$$\omega_{=0}$$
 $\omega = \infty$

Order



$$M = \infty$$

 $M = \omega \qquad M = 0$ $\emptyset = -90^{\circ} \qquad \emptyset = -70^{\circ}$

$$M = \infty$$

(3)
$$K = \infty \qquad M = 0$$

$$S(Z_1S+1)(Z_2S+1) \qquad \not p = -90 \qquad \not p = -270$$

Polar Plat

$$(4)$$
 (73571) (73571) (73571) (73571) (73571)

Nyquist Stability Criterion



Example,
$$G_7(S) = \frac{k_1}{s(s-1)}$$

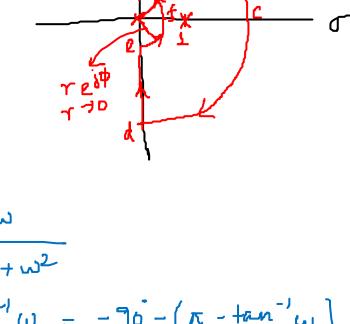
$$G_{7}(jw) = \frac{k_{1}}{jw(jw-1)} \times \frac{-w^{2}+jw}{-w^{2}+jw}$$

$$= \frac{-K_1\omega^2 + \frac{1}{6}K_1\omega}{\omega^4 + \omega^2} - \frac{-K_1\omega^2}{\omega^4 + \omega^2} + \frac{1}{6}\frac{K_1\omega}{\omega^4 + \omega^2}$$

$$|G(j\omega)| = \frac{K_1}{\omega \sqrt{\omega^2 + 1}}, \quad |G(j\omega)| = -90 - t\omega n^2 \omega = -90 - (\kappa - t\omega n^2 \omega)$$

$$= -90 - (\kappa - t\omega n^2 \omega)$$

$$= -30 - (\kappa - t\omega n^2 \omega)$$



Nyquist



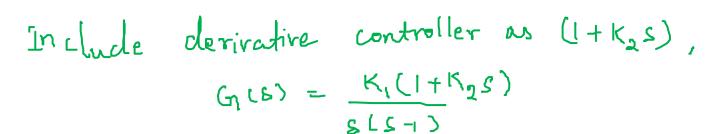
(a) path bold,
$$S = Re^{j\theta}$$
 $O \Rightarrow 9iboi = -9i$
 $R \Rightarrow \infty$

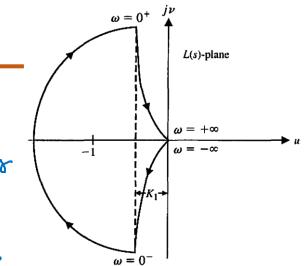
$$G(S) = \lim_{R \to \infty} \frac{K_1}{R \Rightarrow \infty} = \lim_{R \to \infty} \frac{K_1}{R^2 e^{j2} e^{j2}}$$
 $= 0 e^{j\theta} (Re^{j\theta} - 1) \xrightarrow{R \Rightarrow \infty} \frac{K_2}{R^2 e^{j2} e^{j2}}$
 $= 0 e^{j\theta} - 0$
 $= 0$, $-2(9i)$ $= 0$

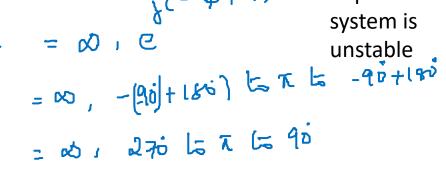
Nyquist Stability Criterion

- (3) path de, $S=-j\omega$ mirror image of polar plot obtained for path ab
- ④ path efa, S= re^{ff} / Ø=> -90 to 6 to 90

$$G(S) = \lim_{r \to 0} \frac{k_1}{re^{i\phi}} = \lim_{r \to 0} \frac{k_1}{re^{i\phi} \cdot e^{i\phi}}$$







check whether system is stable



N=1, P=1,
Z=1+1=2,
2 CL poles
on RHS
implies that
system is
unstable
-qr+lsv



UNIT 5: STABILITY IN THE FREQUENCY DOMAIN

Relative stability and Nyquist Criterion

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Relative stability & Nyquist Stability Criterion

Gain Margin: GM is the reciprocal of the magnitude $|G(j\omega)|$ at the frequency at which phase angle is -180.

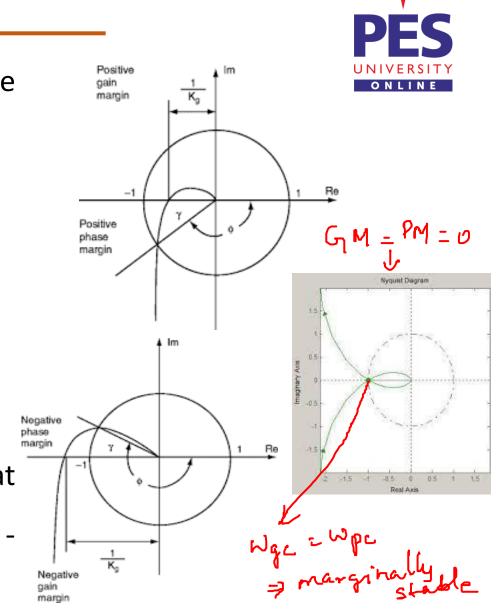
GM in dB =
$$20 \log \frac{1}{|G(j\omega)|} = -20 \log_{10} |G(j\omega)|$$

Where $K_g = |G(j\omega)|$

The GM in dB is +ve if $K_g > 1$

The GM in dB is -ve if $K_g < 1$

Phase cross over frequency(PCF), ω_{pc} : frequency at which phase angle of open loop transfer function equals - 180.



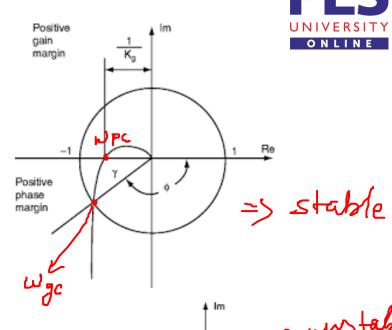
Relative stability & Nyquist Stability Criterion

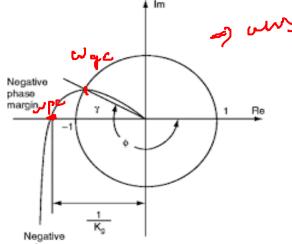
Phase Margin: PM is the amount of additional phase lag at the gain cross over frequency required to bring the system to the verge of instability.

$$PM = 180 + \phi$$

Where
$$\phi = angle\{G(j\omega)\}|_{\omega = \omega_{gc}}$$

Gain cross over frequency(GCF), ω_{gc} : frequency at which magnitude of open loop transfer function equals unity.





Relative Stability and Nyquist Stability Criterion



For example,
$$G(s) = \frac{1}{s(s+1)(s+0.5)}$$
 Find a) wgc , b) wpc c) $G(s) = \frac{1}{s(s+1)(s+0.5)}$

$$G(j_0) = \frac{1}{j_0(j_0 + 1)(j_0 + 1/2)}$$

$$G(i\omega) = -\frac{\omega^2}{2} - \omega^2 + j(\omega^3 - \omega_2)$$

$$(\omega^{4} + \omega^{2}) (\omega^{2} + \frac{1}{4})$$

$$|G(i\omega)| = \frac{1}{\omega \sqrt{\omega^{2} + 1}} \sqrt{\omega^{2} + 1/4}$$

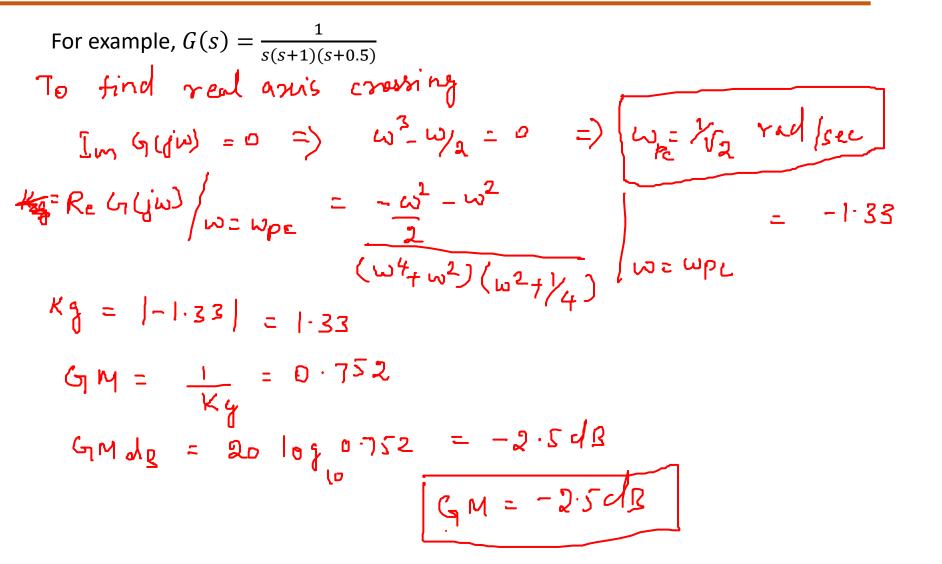
For example,
$$G(s) = \frac{1}{s(s+1)(s+0.5)}$$

path de, $S = -jw$

mirror image of path ab

Path efa, $S = re^{j\Theta}$, $\theta = -je^{j\Theta} - 0 - 0 - 90$
 $G(s) = \lim_{r \to 0} \frac{1}{re^{j\Theta}(re^{j\Theta}+1)} (re^{j\Theta}+0.5)$
 $\lim_{r \to 0} \frac{1}{re^{j\Theta}(re^{j\Theta}+1)} (re^{j\Theta}+0.5)$
 $\lim_{r \to 0} \frac{1}{re^{j\Theta}(re^{j\Theta}+1)} (re^{j\Theta}+0.5)$
 $\lim_{r \to 0} \frac{1}{re^{j\Theta}(re^{j\Theta}+1)} (re^{j\Theta}+0.5)$









For example,
$$G(s) = \frac{1}{s(s+1)(s+0.5)}$$

To find wasc

$$|G(yw)|_{W=w_{ac}} = |G(yw)|_{W=c} = |G(yw)|_{W=c}$$

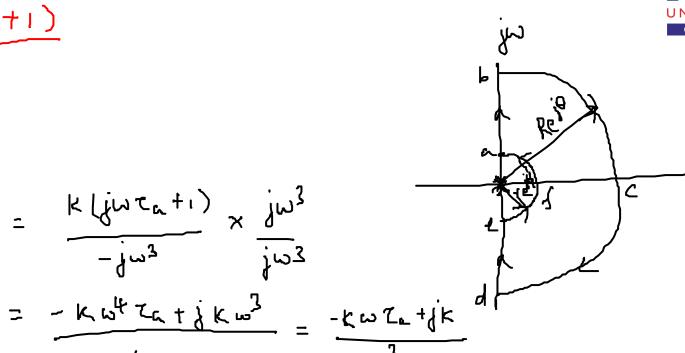
Relative Stability and Nyquist Stability Criterion



$$E_X$$
, $G_1H(S) = K(S_{a}+1)$

1 path ab, s-jw

$$\frac{(jw)^{2}}{(jw)^{2}} = \frac{k(jwz_{\alpha}+1)}{-jw^{2}} \times \frac{jw^{2}}{j\omega^{2}}$$



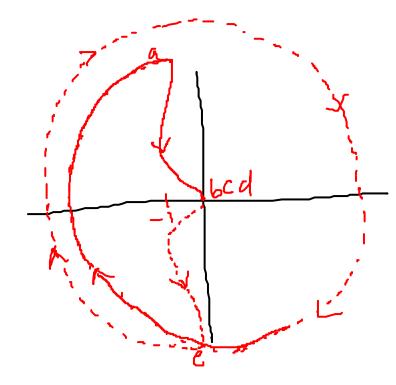
Relative Stability and Nyquist Stability Criterion



$$\infty$$

$$\alpha$$

凶





path esa,
$$S = re^{i\phi}$$
, $\phi \Rightarrow -9i \Rightarrow 0 \Rightarrow 9i$
 $G(S) = \frac{K(re^{i\phi}ta + 1)}{r^3} = \frac{K}{r^3} \cdot e^{i3i\phi}$
 $= \infty$, $\frac{-3(-9i)}{270i} \Rightarrow 0 \Rightarrow -3(9i)$
 $= 270i \Rightarrow (65i \Rightarrow 90i \Rightarrow 0) \Rightarrow -180i \Rightarrow -270i$

Relative Stability and Nyquist Stability Criterion

Example,
$$G_{1}(S) = \frac{K(S+4)}{(S-1)(S-2)}$$
 Find the range of $(S-1)(S-2)$ k for which the system is stable. Sol: path ab , $S = jw$

$$G_{1}(jw) = \frac{K(jw+4)}{(jw-1)(jw-2)}$$

$$= K(jw+4)(-jw-1)(-jw-2)$$

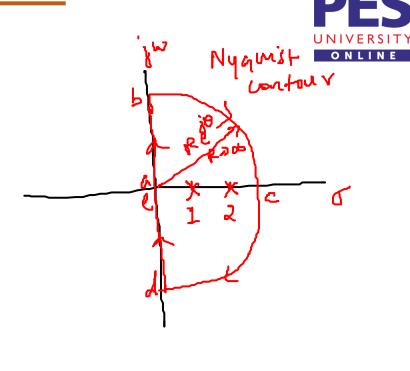
$$= K(jw+4)(-w^{2}+4)$$

$$= K(4+jw)(-w^{2}+3jw+2)$$

$$= K(4+jw)(-w^{2}+4)$$

$$= K(4+jw)(-w^{2}+4)$$

system is stuble.

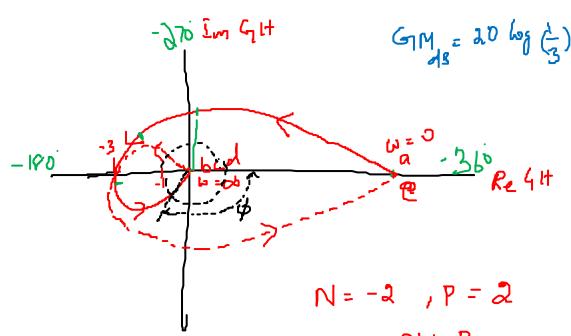


$$= \frac{K(\kappa + j | 2w - 4w^{2} + 2jw - 3w^{2} - jw^{3})}{(w^{2} + 1)(w^{2} + 4)}$$

$$= \frac{K(\kappa - 7w^{2})}{(w^{2} + 1)(w^{2} + 4)} + \frac{j}{j} \frac{K(14w - w^{3})}{(w^{2} + 1)(w^{2} + 4)}$$



$$|G(i\omega)| = \frac{K\sqrt{\omega^2+16}}{4} \int_{0.00}^{0.00} |G(i\omega)| = +\omega n^{-1}\omega - (180 - +\omega n^{-1}\omega) - (180 - +\omega n^{-1}\omega)$$



(a) Path bed
$$S = Re^{i\theta}$$
, $R \to \infty$, $B \to 90 \to 00 \to -90$
 $(965) = \frac{k(Re^{i\theta} + 4)}{(Re^{i\theta} - 2)} = \frac{K}{R}e^{i\theta} = 0$, $(-90 \to 00) \to 90$

$$z = N + P$$

$$= -\lambda + 2$$

$$= 0$$

$$= 0$$

$$= 0$$

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$$\frac{(W^{2}+1)(W^{2}+4)}{(W^{2}+4)} = 0 \Rightarrow 14W-W^{2} = 0$$

$$W^{2} = 14 = 0 \Rightarrow W = \sqrt{14} = W^{2}C$$

=)
$$K > \frac{1}{0.33}$$

 $K > 3.003$

To find
$$W_{gc}$$
, $|G_{G_{gi}}| = 1$

$$K \left[\frac{\omega_{jc}^2 + 1b}{\omega_{gc}^2 + 1} \right] = 1$$

$$|G_{gi}| = 1$$

let $k = 8$, $W_{gc} = 1$

Sub. W_{gc} in $|G_{gi}| = 4$

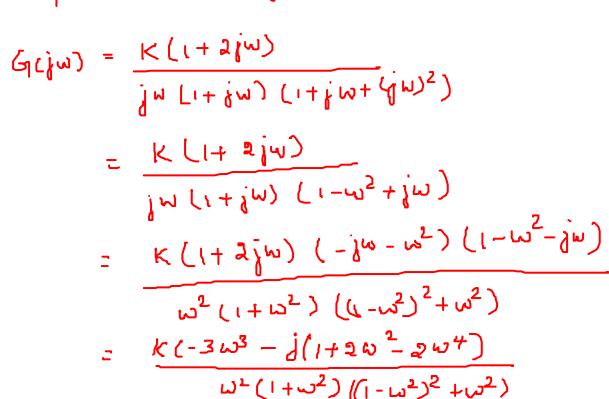
$$|G_{gi}| = 4$$

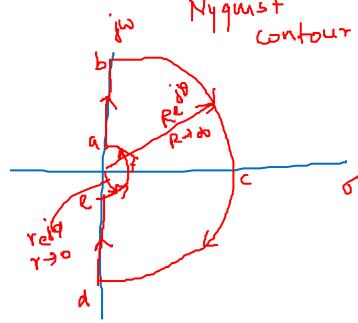
$$|G_{gi}| = 4$$





Example,
$$(\eta(s)) = \frac{K(1+2s)}{S(1+s+s^2)}$$
 Find the $S(1+s)(1+s+s^2)$ for which $S=0$, $S=0$



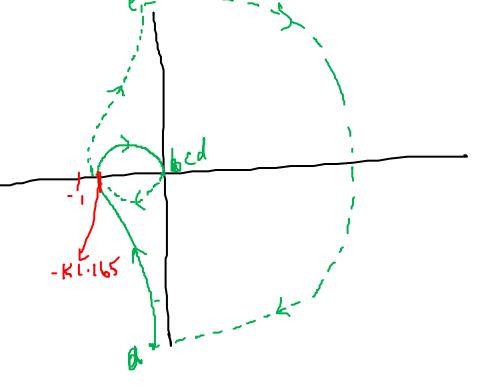


Relative Stability and Nyquist Stability Criterion



$$|G(j\omega)| = \frac{K\sqrt{1+4\omega^2}}{\omega\sqrt{1+\omega^2}\sqrt{1+\omega^4-\omega^2}}$$

1



$$N=0$$
, $P=0=$) $z=0$
=) system stable to $\times \times 0.86$



where it cuts the real and is
$$\lim_{n \to \infty} (\omega_{n}) = 0$$

$$Re((\eta L | w)) \Big|_{w = 1.168} = -k \cdot 3 w^{3}$$

$$\omega(1 + w^{2}) ((1 - w^{2})^{2} + w^{2}) \Big|_{w = 1.168} = -k \cdot 1.165$$

For the system to be stable,
$$N=0$$
 : $P=0$, ... -1<1.165 >-1

 $K \subset \frac{1}{1.165}$
 $0 \le K \le 0$



THANK YOU

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