



UE20EC303 EMF THEORY UNIT -3

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EMF THEORY

TEXT BOOK AND REFERENCES

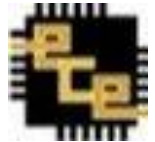


Textbook:

1. **“Principles of Electromagnetics”**, Matthew N. O. Sadiku, 4th / 6th Edition, Oxford University Press, 2007 / 2018.

Reference Books:

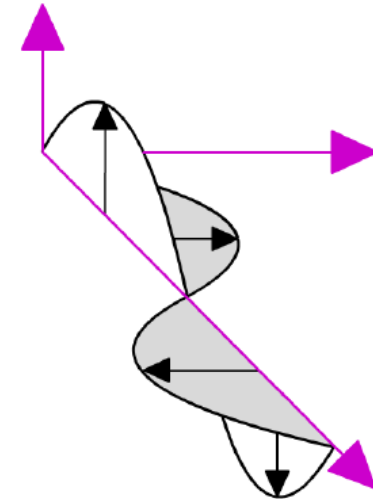
1. **“Electromagnetic Field Theory Fundamentals”**, Bagh Singh Guru, Huseyin R Hiziroglu, Cambridge University Press, 2nd Edition, 2002.
2. **“Engineering Electromagnetics”**, William H Hayt Jr, J.A. Buck, 7th Edition, Tata McGraw Hill, 2007.
3. **“Microwave Devices and Circuits”**, Samuel. Y. Liao, Third Edition, Pearson, 2006.
4. **“Engineering Electromagnetics Essentials”**, B. N. Basu, Universities Press (India), 2015.



UNIT - 3

Maxwell's Equations for Time – Varying Fields

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EMF Theory – Unit – 3 {Text Book Sec. 9.1 - 9.5, 9.7, 5.9, 8.7, 10.1 – 10.7}

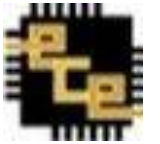
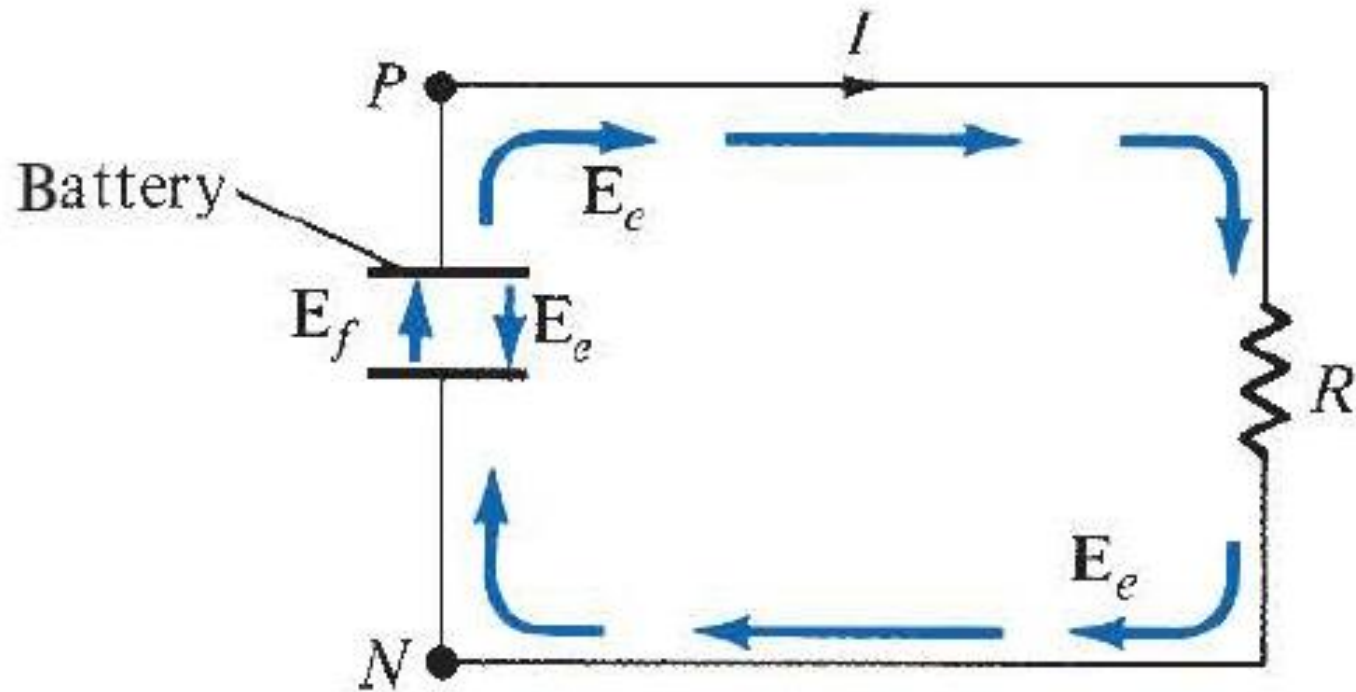
CONTENTS

- ❖ Faraday's Law.
- ❖ Transformer & Motional Electromotive Forces.
- ❖ Displacement Current.
- ❖ Maxwell's Equations in their final forms.
- ❖ Time Harmonic Fields.
- ❖ Electric & Magnetic Boundary conditions.
- ❖ Waves, propagation of waves in different media.
- ❖ Wave polarisation.



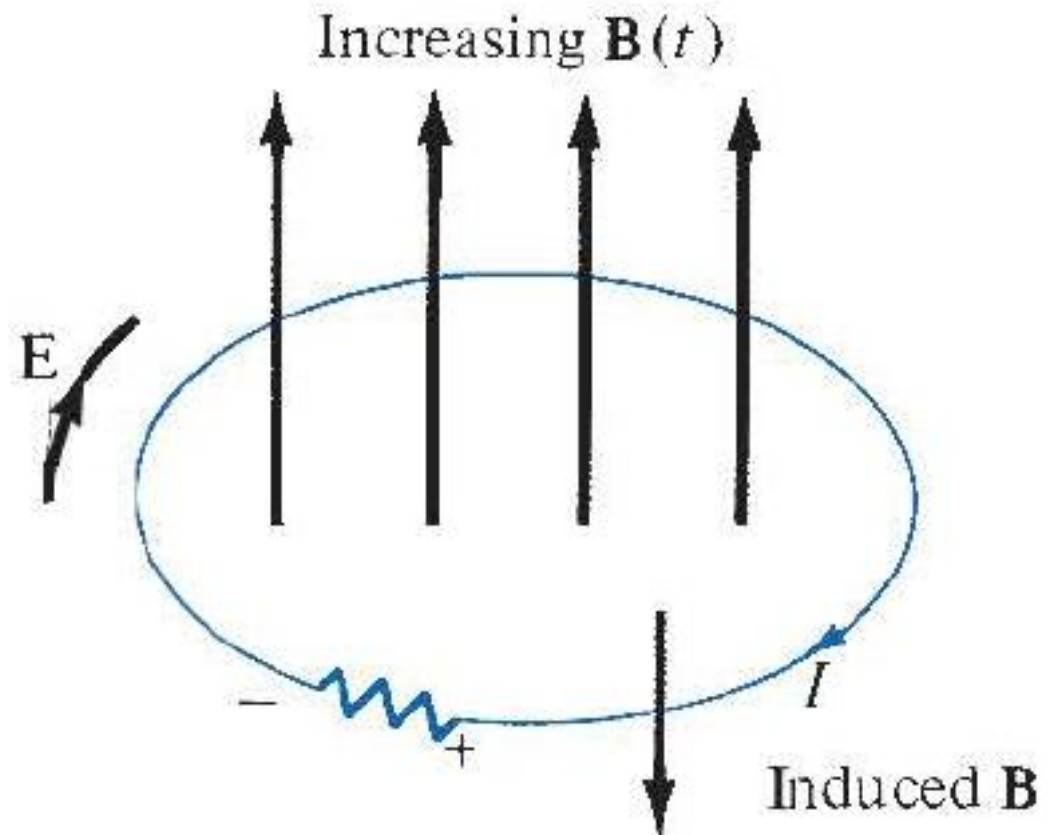
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FARADAY'S LAW



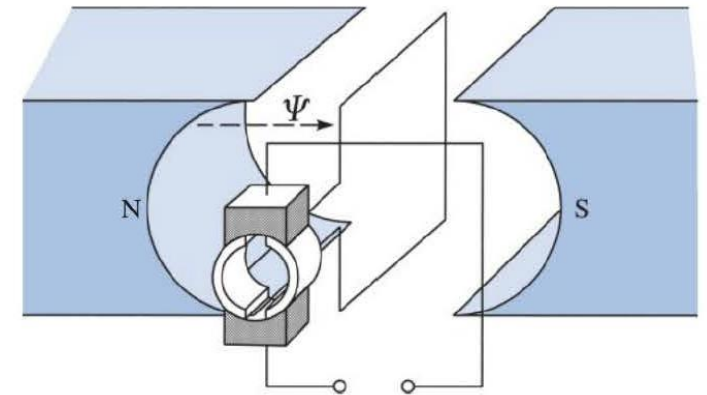
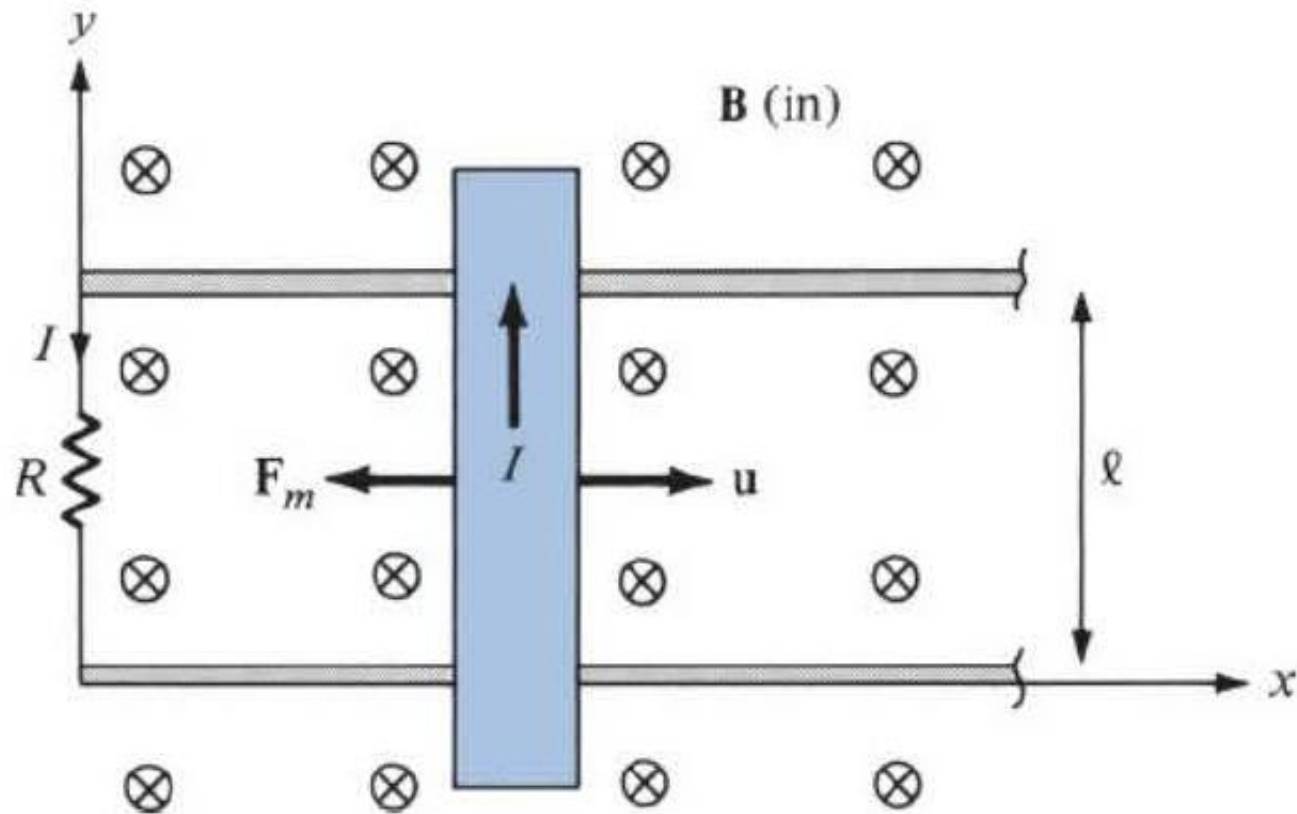
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TRANSFORMER EMF



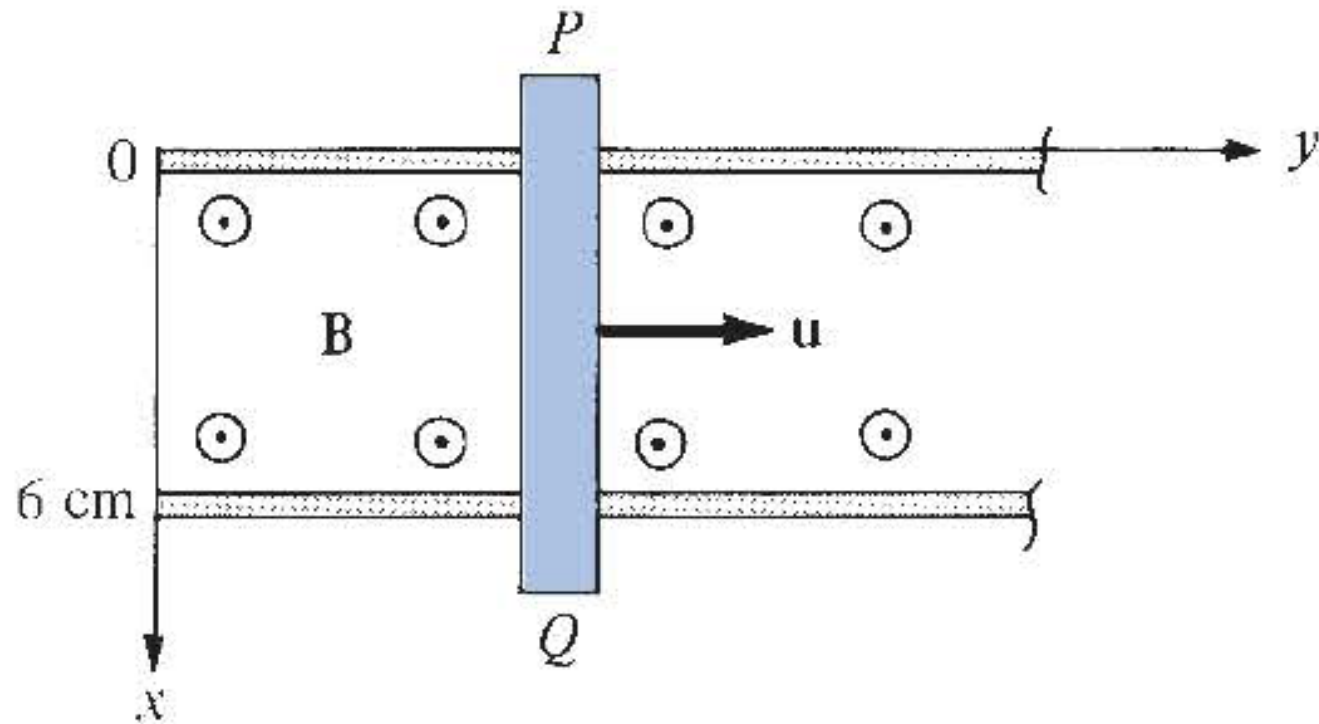
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MOTIONAL EMF



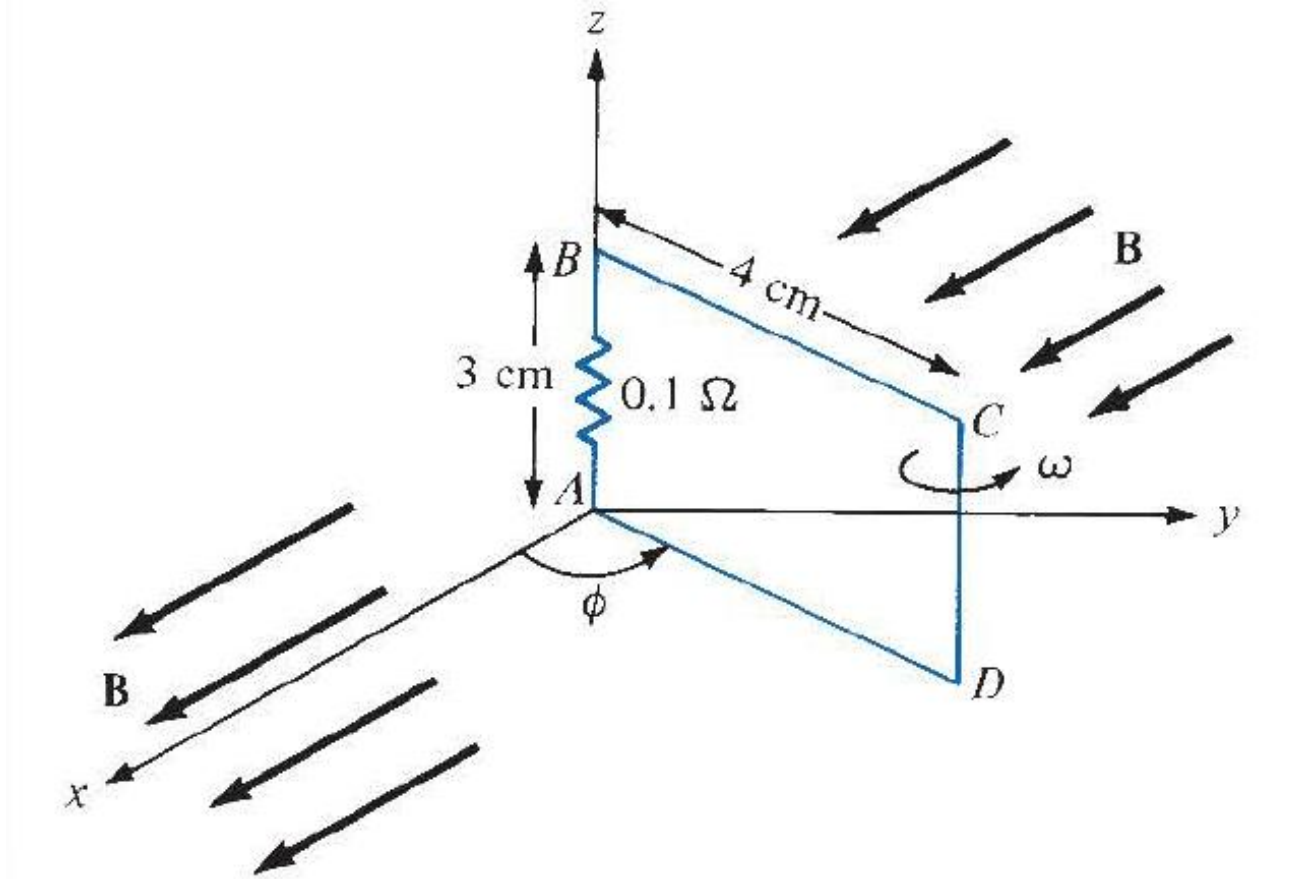
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NUMERICALS



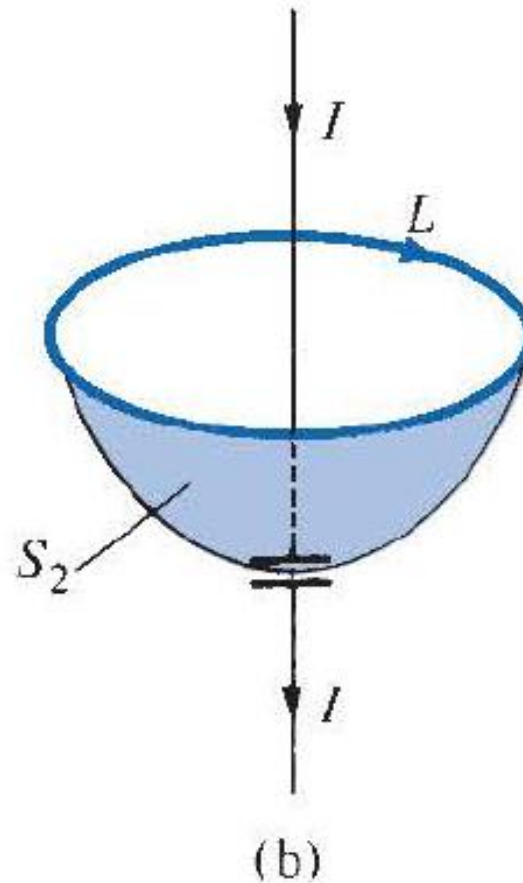
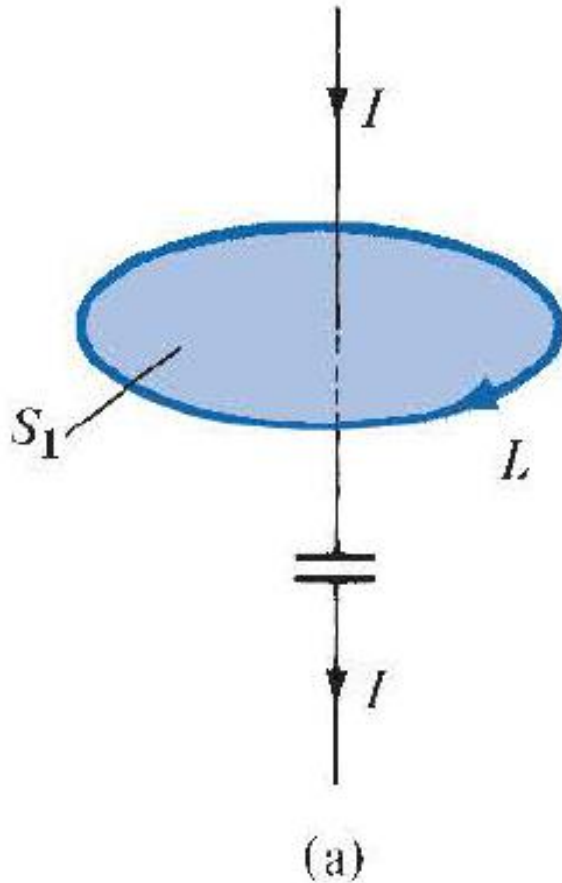
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NUMERICALS



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DISPLACEMENT CURRENT

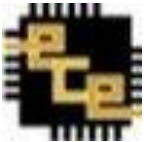


Self Study from Text Book

TABLE 9.1 Generalized Forms of Maxwell's Equations

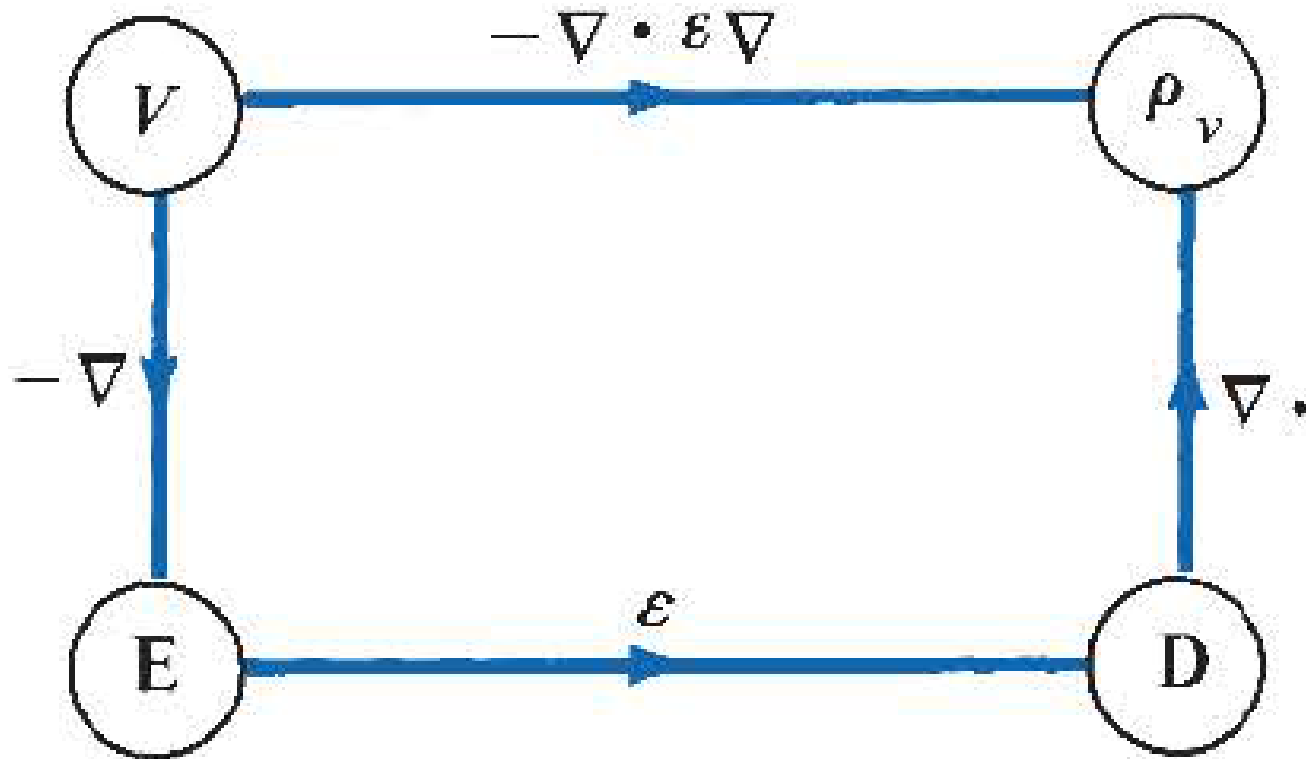
| Differential Form | Integral Form | Remarks |
|--|--|---|
| $\nabla \cdot \mathbf{D} = \rho_v$ | $\oint_S \mathbf{D} \cdot d\mathbf{S} = \int_v \rho_v dv$ | Gauss's law |
| $\nabla \cdot \mathbf{B} = 0$ | $\oint_S \mathbf{B} \cdot d\mathbf{S} = 0$ | Nonexistence of isolated magnetic charge* |
| $\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$ | $\oint_L \mathbf{E} \cdot d\mathbf{l} = -\frac{\partial}{\partial t} \int_S \mathbf{B} \cdot d\mathbf{S}$ | Faraday's law |
| $\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}$ | $\oint_L \mathbf{H} \cdot d\mathbf{l} = \int_S \left(\mathbf{J} + \frac{\partial \mathbf{D}}{\partial t} \right) \cdot d\mathbf{S}$ | Ampère's circuit law |

*This is also referred to as Gauss's law for magnetic fields.



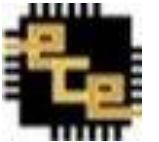
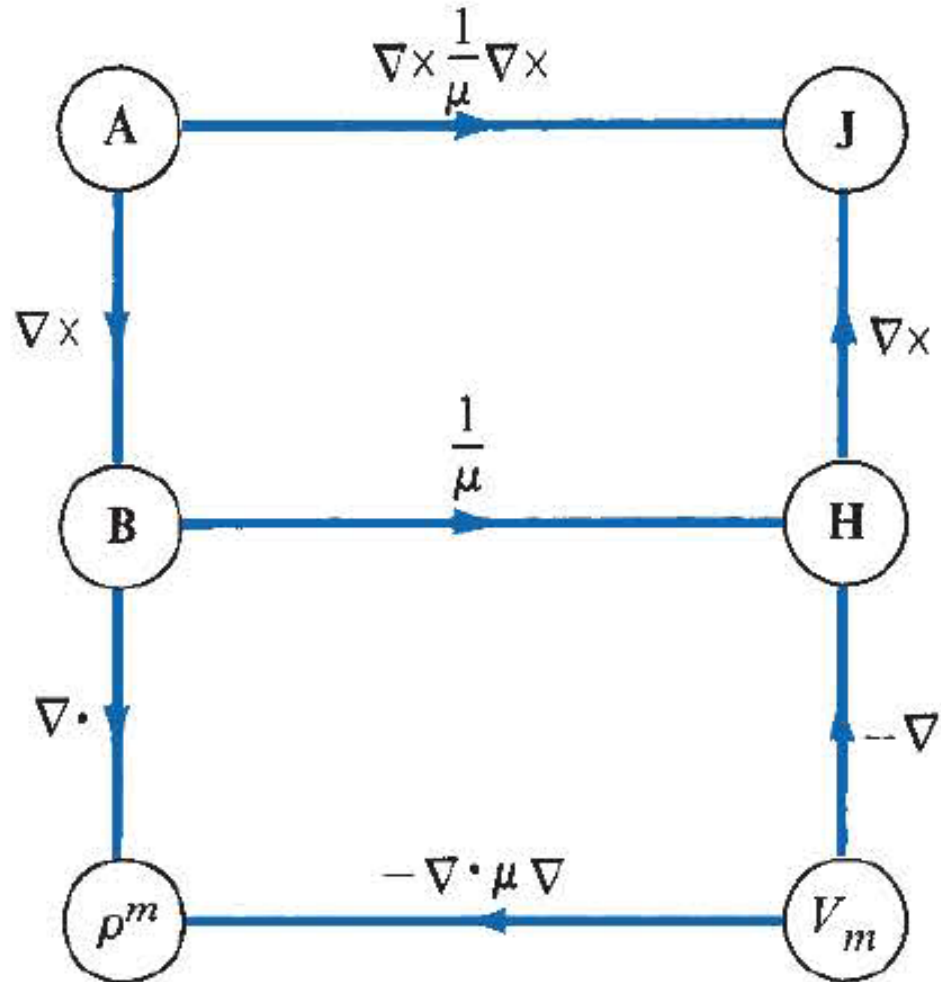
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FLOW DIAGRAM – ELECTROSTATIC SYSTEM



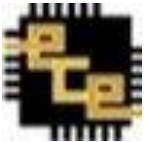
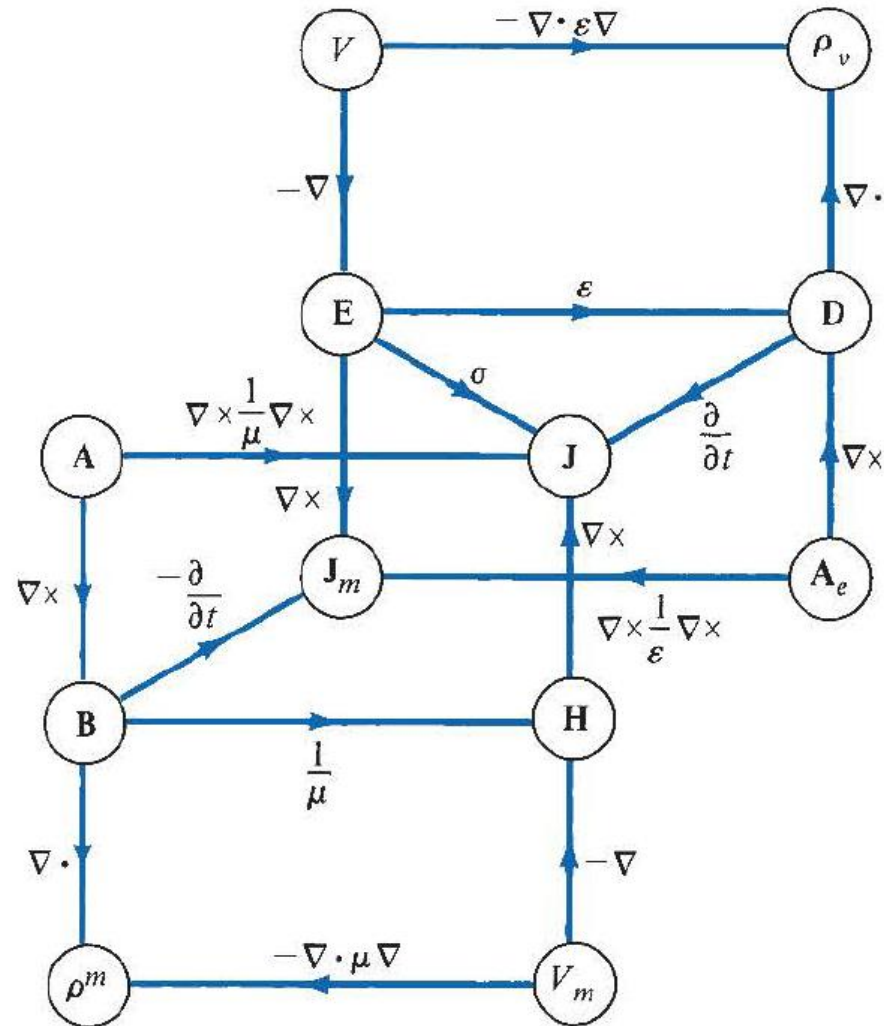
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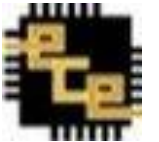
FLOW DIAGRAM – MAGNETOSTATIC SYSTEM



EMF Theory – Unit -3

FLOW DIAGRAM – ELECTROMAGNETIC SYSTEM





Point Form

Integral Form

$$\nabla \cdot \mathbf{D}_s = \rho_{vs}$$

$$\oint \mathbf{D}_s \cdot d\mathbf{S} = \int \rho_{vs} dv$$

$$\nabla \cdot \mathbf{B}_s = 0$$

$$\oint \mathbf{B}_s \cdot d\mathbf{S} = 0$$

$$\nabla \times \mathbf{E}_s = -j\omega \mathbf{B}_s$$

$$\oint \mathbf{E}_s \cdot d\mathbf{l} = -j\omega \int \mathbf{B}_s \cdot d\mathbf{S}$$

$$\nabla \times \mathbf{H}_s = \mathbf{J}_s + j\omega \mathbf{D}_s$$

$$\oint \mathbf{H}_s \cdot d\mathbf{l} = \int (\mathbf{J}_s + j\omega \mathbf{D}_s) \cdot d\mathbf{S}$$



Boundary Conditions.

- Till now, the discussion considered the existence of electric field in a homogeneous medium.
- If the field exists in a region consisting of two different media, the conditions that the field must satisfy at the interface separating the media are called Boundary Conditions.
- These conditions are helpful in determining the field on one side of the boundary if the field on the other side is known.
- Subsequent discussions would be for the following interfaces separating:
 - (a) Dielectric (ϵ_{r1}) & Dielectric (ϵ_{r2})
 - (b) Conductor & dielectric
 - (c) Conductor & free space.



→ To determine the boundary conditions, we use the following Maxwell's equations:

$$\oint_S \vec{D} \cdot d\vec{S} = Q_{enc} \quad \text{— first eqn.}$$

$$\oint_L \vec{E} \cdot d\vec{l} = 0 \quad \text{— second eqn.}$$

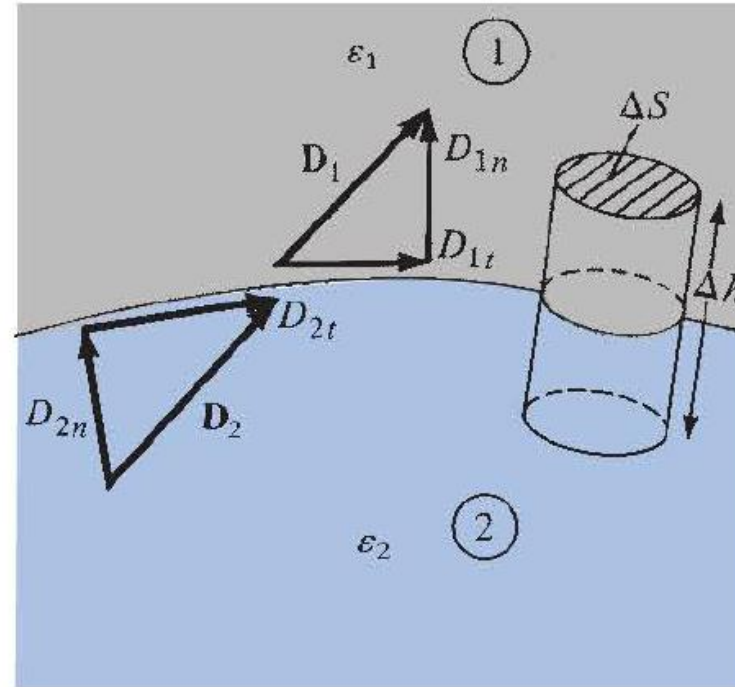
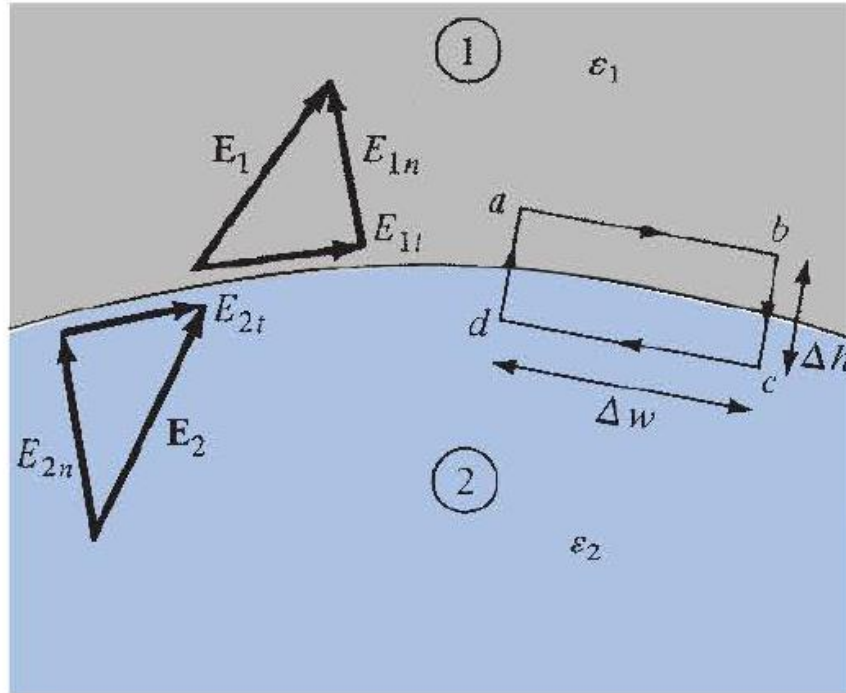
→ The electric field intensity \vec{E} is decomposed into two orthogonal components:

$$\vec{E} = \vec{E}_t + \vec{E}_n \quad ; \quad \begin{array}{l} \vec{E}_t - \text{Tangential component} \\ \vec{E}_n - \text{Normal component} \end{array}$$

→ A similar decomposition can be done for the electric flux density \vec{D} .

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ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



Dielectric – Dielectric Boundary Conditions



Dielectric - Dielectric Boundary Conditions.

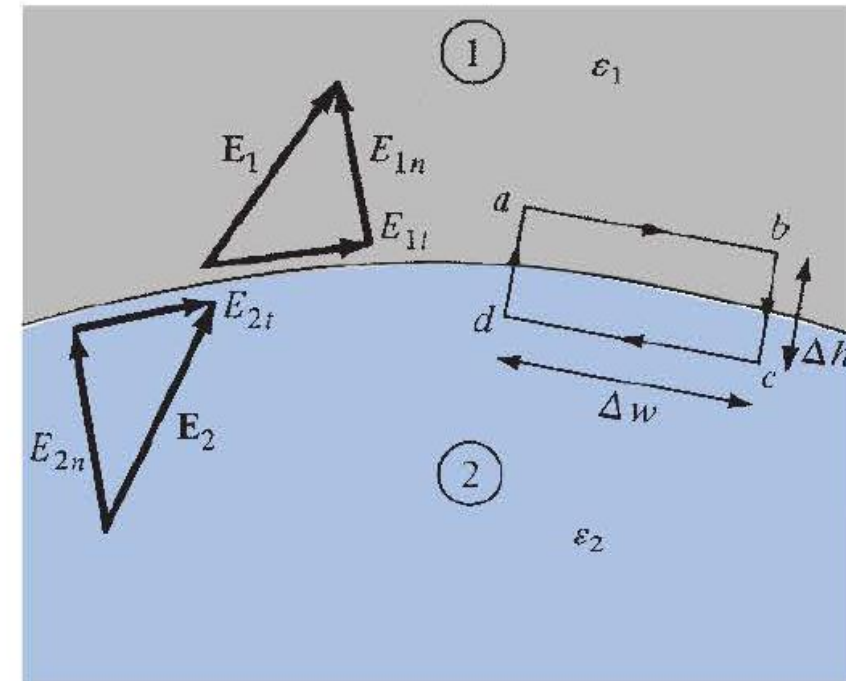
→ Consider the \vec{E} field existing in a region that consists of 2 different dielectric characterised by $\underline{\underline{E_1 = E_0 \epsilon_1}}$ & $\underline{\underline{E_2 = E_0 \epsilon_2}}$.

→ The fields \vec{E}_1 & \vec{E}_2 in media 1 & 2, respectively can be decomposed into.

$$\vec{E}_1 = \vec{E}_{1t} + \vec{E}_{1n} \quad \& \quad \vec{E}_2 = \vec{E}_{2t} + \vec{E}_{2n}$$

→ While applying the eqn. $\oint \vec{E} \cdot d\vec{l} = 0$ to the closed path abceda as shown, assuming that the ~~path~~ path is very small w.r.t spatial variations, we have

$$0 = \underbrace{E_{1t} \Delta w}_{ab} - E_{1n} \frac{\Delta h}{2} - \underbrace{E_{2n} \frac{\Delta h}{2}}_{cd} - E_{2t} \Delta w + \underbrace{E_{2n} \frac{\Delta h}{2} + E_{1n} \frac{\Delta h}{2}}_{da}$$



(a)

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ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



✗ The signs are obtained referring the direction of travel along abcd to the direction of the component vectors.

→ Also $E_t = |\vec{E}_t|$ & $E_n = |\vec{E}_n|$. The $\frac{\Delta h}{2}$ terms cancel resulting in

$$0 = E_{1t} \Delta w + E_{2t} \Delta w = (E_{1t} - E_{2t}) \Delta w$$

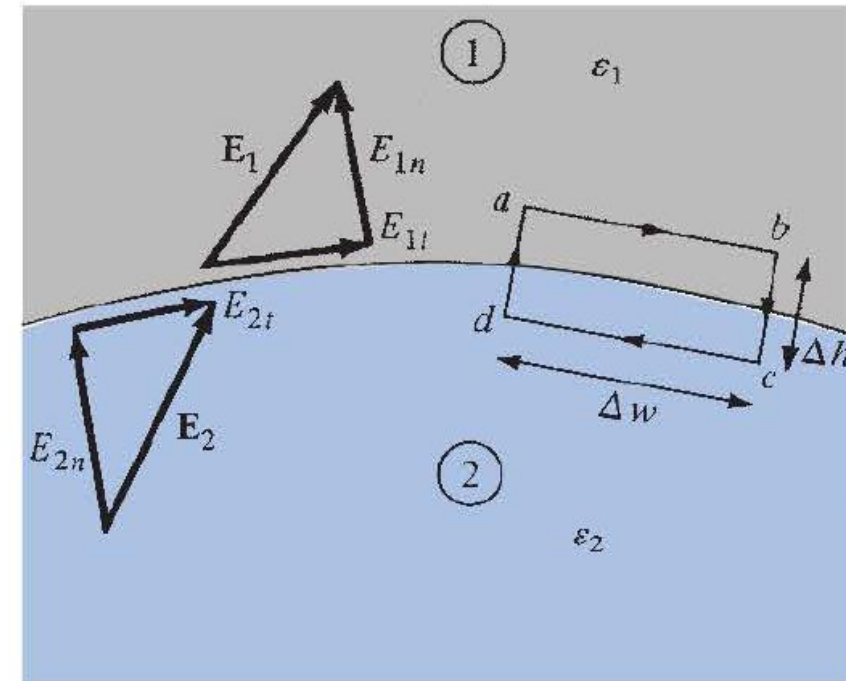
or

$$\boxed{E_{1t} = E_{2t}}$$

✗ Thus the tangential components of \vec{E} are same on the two sides of the boundary.

→ In other words, \vec{E}_t undergoes no change on the

✗ boundary & it is said to be continuous across the boundary.



(a)

EMF Theory – Unit -3

ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



→ Since $\vec{D} = \epsilon \vec{E} = \vec{D}_t + \vec{D}_n$, the equation $\vec{E}_{1t} = \vec{E}_{2t}$ can be expressed as

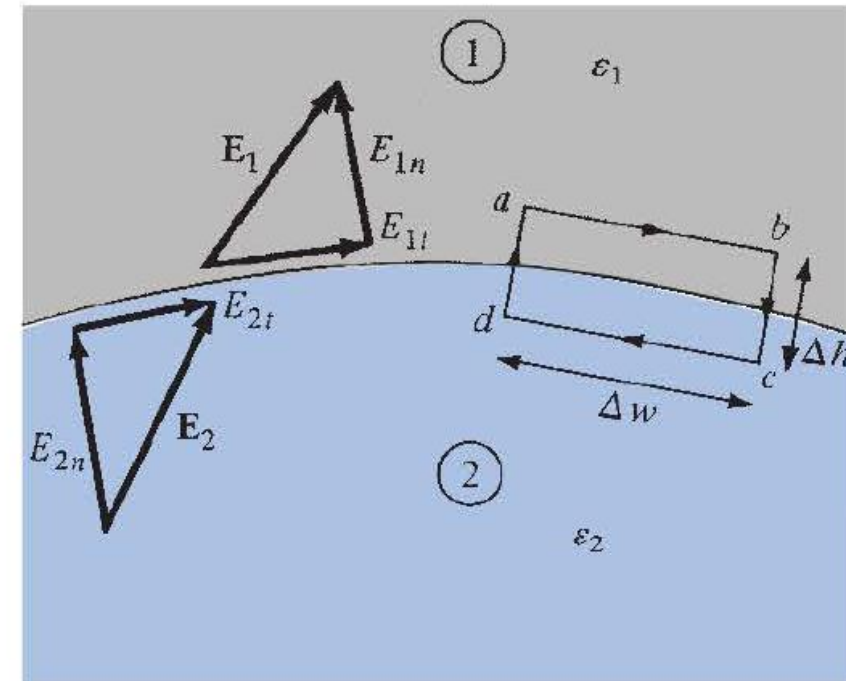
$$\frac{D_{1t}}{\epsilon_1} = E_{1t} = E_{2t} = \frac{D_{2t}}{\epsilon_2}$$

or

$$\boxed{\frac{D_{1t}}{\epsilon_1} = \frac{D_{2t}}{\epsilon_2}}$$

→ \vec{D}_t undergoes some change across the interface. Hence \vec{D}_t is said to be "discontinuous" across the interface.

(19)



(a)

EMF Theory – Unit -3

ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



→ Similarly, when apply the Equation $\oint \vec{D} \cdot d\vec{S} = Q_{enc}$ to the cylindrical Gaussian surface in the other figure,
→ The contribution due to the sides vanishes. Allowing $\Delta h \rightarrow 0$ gives

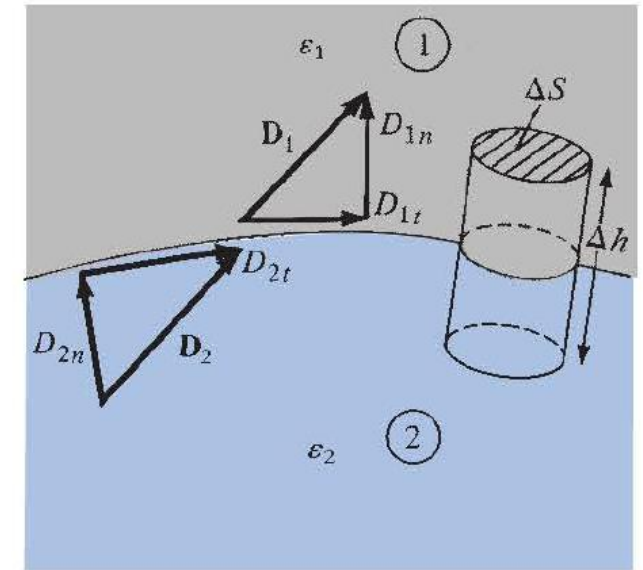
$$\Delta Q = \rho_s \Delta S = D_{1n} \Delta S - D_{2n} \Delta S$$

[-ve sign due to opposite direction at the bottom]

$$\text{or } \boxed{D_{1n} - D_{2n} = \rho_s}$$

where ρ_s is the free charge density placed deliberately at the boundary.

→ It is to be noted that the eqn. $D_{1n} - D_{2n} = \rho_s$ is based on the assumption that \vec{D} is directed from Region 2 to Region 1 & it should be applied accordingly.



(b)

EMF Theory – Unit -3

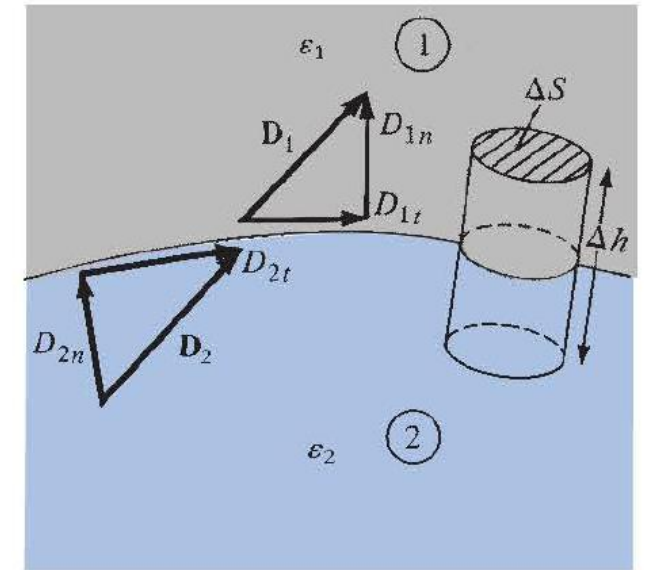
ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



→ If no free charges exist at the interface (i.e. charges are not deliberately placed), $\rho_s = 0$, then

$$\boxed{D_{1n} = D_{2n}} \text{ with } \rho_s = 0$$

→ Thus the normal component of \vec{D} is continuous across the interface (or) D_n undergoes no change at the boundary.



(b)

EMF Theory – Unit -3

ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS

Since $\vec{D} = \epsilon \vec{E}$, we have

(20)

$$\epsilon_1 E_{1n} = \epsilon_2 E_{2n}$$

meaning the normal component of E is discontinuous at the boundary.

→ Summarising the Boundary conditions that need to be satisfied by an electrostatic field at the boundary separating two different dielectrics,

$$E_{1t} = E_{2t}$$

;

$$\frac{D_{1t}}{\epsilon_1} = \frac{D_{2t}}{\epsilon_2}$$

$$\epsilon_1 E_{1n} = \epsilon_2 E_{2n}$$

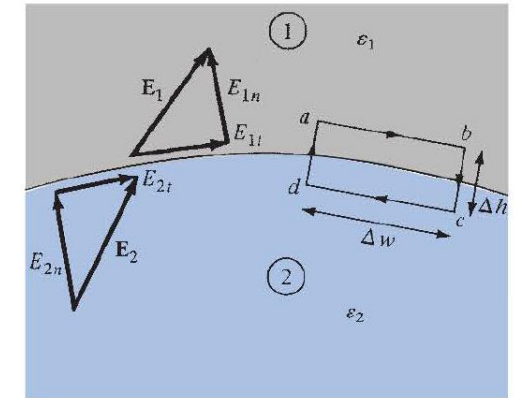
;

$$D_{1n} = D_{2n}$$

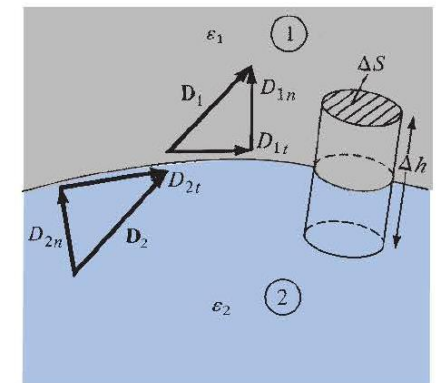
with $\rho_s = 0$



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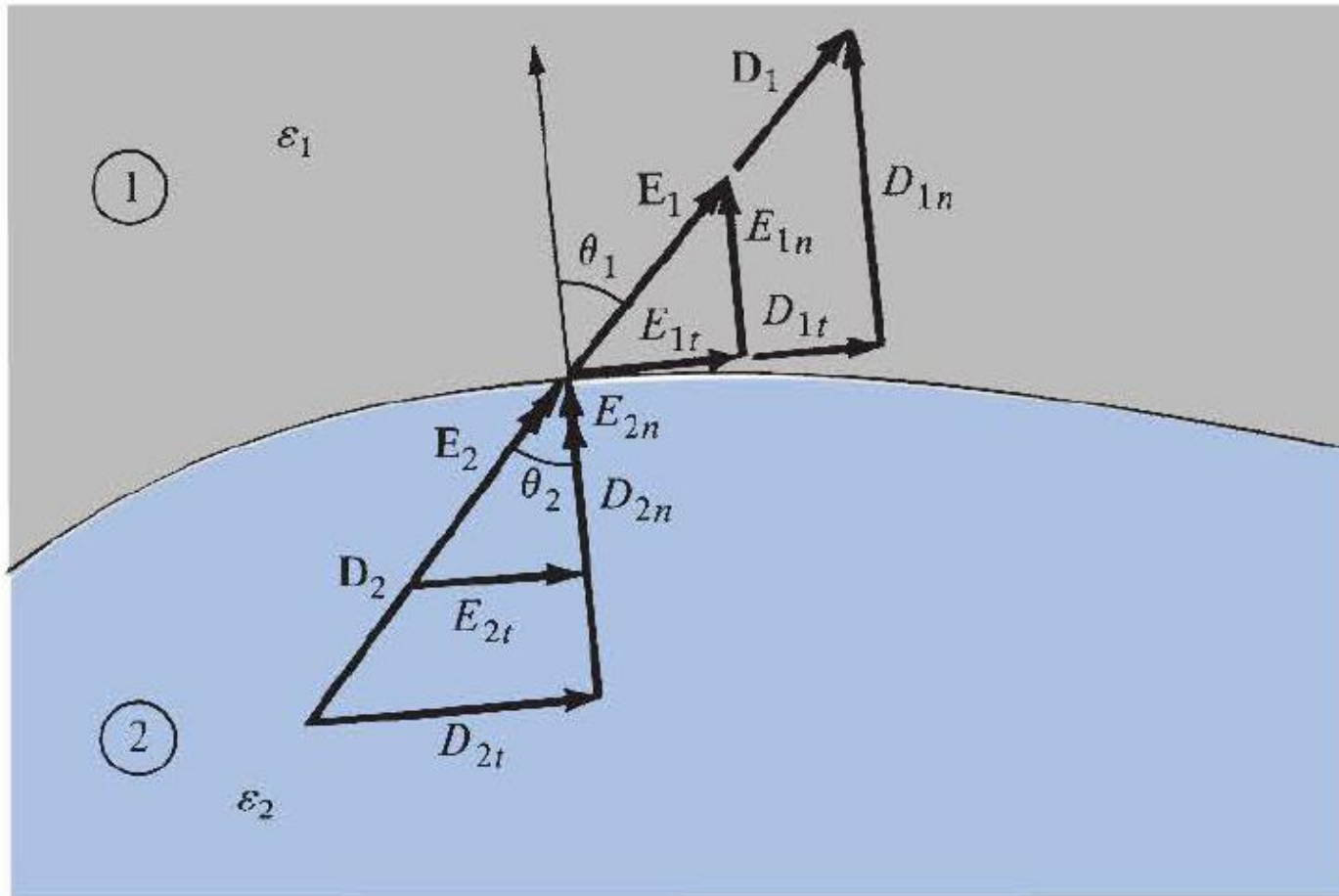
(a)



(b)

EMF Theory – Unit -3

ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



Refraction in Dielectric – Dielectric Boundary

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ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS

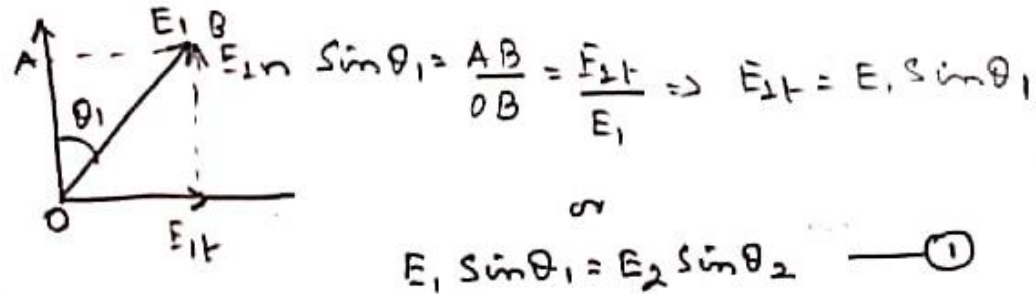


Refraction of Electric field using Boundary Conditions.

→ Refer the figure. Consider \vec{D}_1 or \vec{E}_1 & \vec{D}_2 or \vec{E}_2 making angles θ_1 & θ_2 with the normal to the interface as shown.

→ Using the Eqn. $E_{1t} = E_{2t}$, we have.

$$E_1 \sin \theta_1 = E_{1t} = E_{2t} = E_2 \sin \theta_2 \quad (\text{in magnitude form})$$

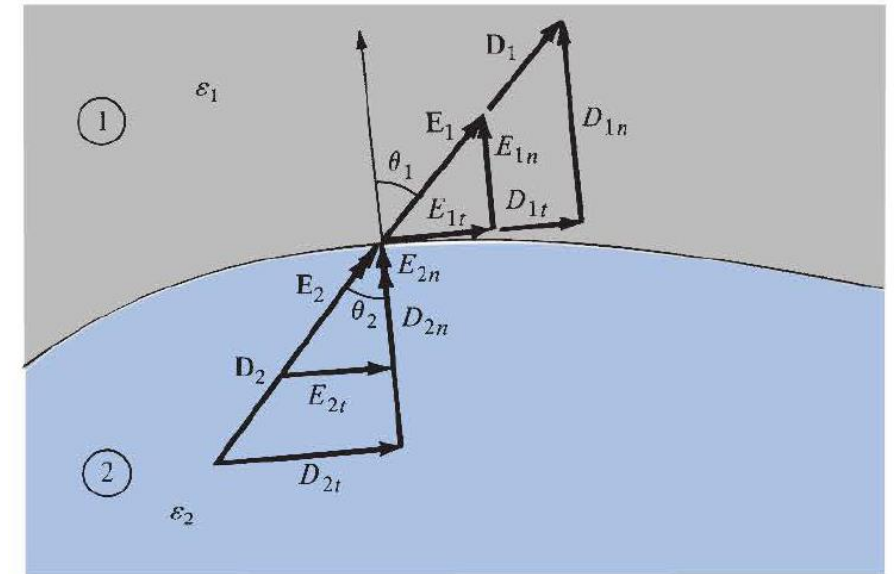


→ Similarly, by applying

$$\epsilon_1 E_1 \cos \theta_1 = D_{1n} = D_{2n} = E_2 \epsilon_2 \cos \theta_2$$

(or)

$$\epsilon_1 E_1 \cos \theta_1 = \epsilon_2 E_2 \cos \theta_2 \quad \text{--- (2)}$$



EMF Theory – Unit -3

ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



Using ① + ② we have

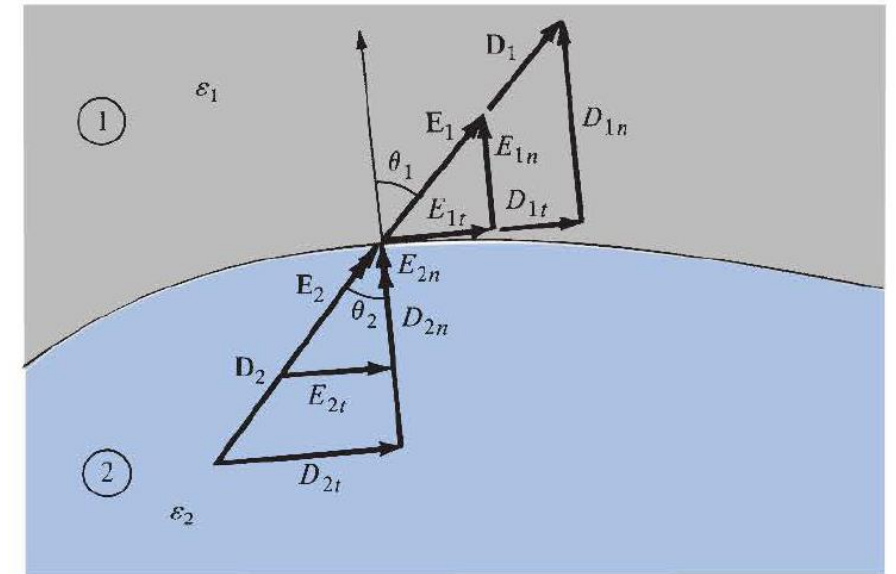
$$\frac{\tan \theta_1}{\epsilon_1} = \frac{\tan \theta_2}{\epsilon_2}$$

→ Since $E_1 = E_0 E_{r1}$ & $E_2 = E_0 E_{r2}$, we have

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{E_{r1}}{E_{r2}}$$

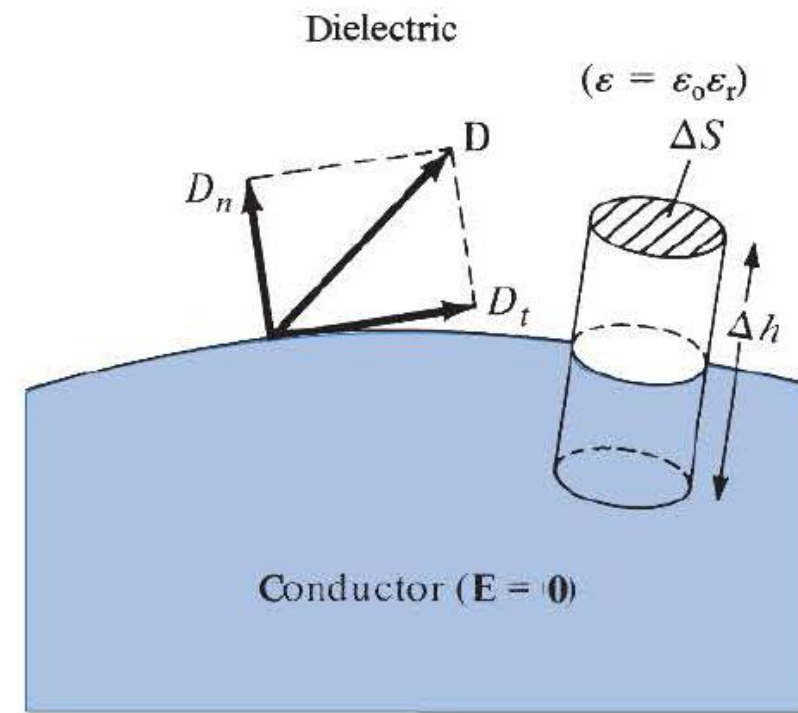
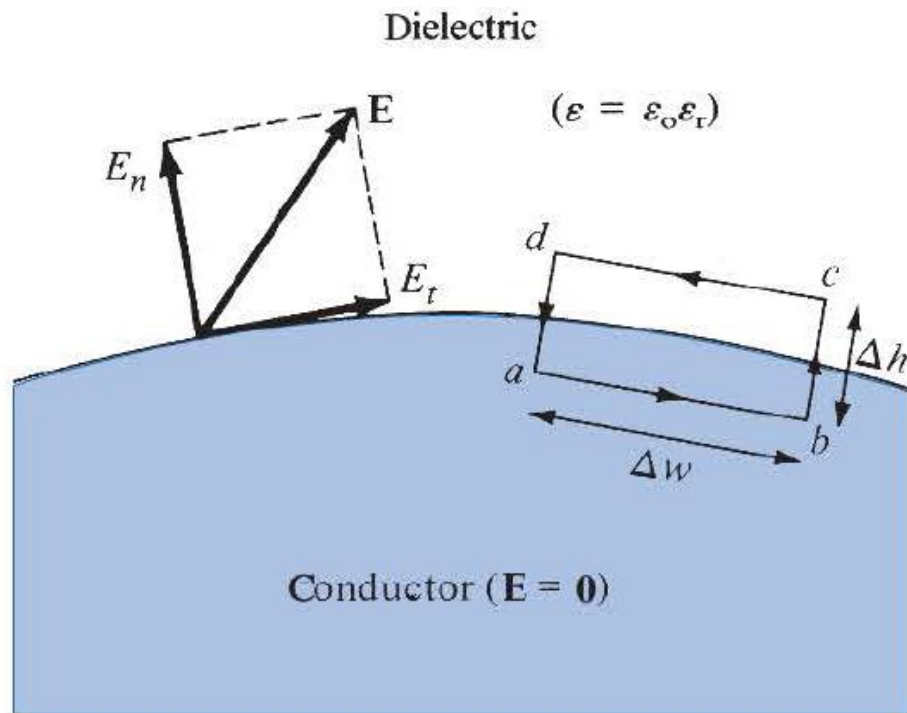
→ This is "law of refraction" of electric field at the boundary, free of charge ($\rho_s = 0$ assumed)

→ In general, an interface between 2 dielectrics produce a bending of flux lines.



EMF Theory – Unit -3

ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



Conductor – Dielectric Boundary Conditions

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ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



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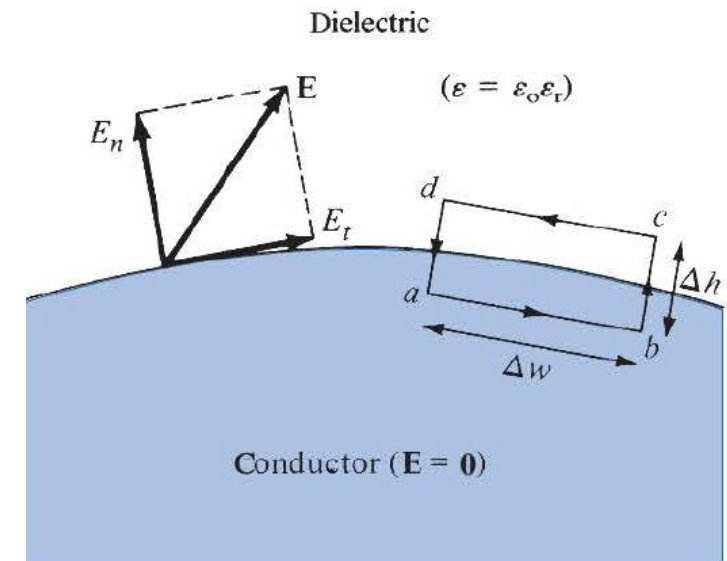
Conductor-Dielectric Boundary conditions.

- The conductor is assumed to be perfect ($\sigma \rightarrow \infty$).
- To determine the boundary conditions, we follow the same procedure, except that $\vec{E} = 0$ inside the conductor.

→ Using the equation $\oint \vec{E} \cdot d\vec{l} = 0$ to the closed path 'abcd a' as in the figure, gives

$$0 = \cancel{0 \cdot \Delta w} + \cancel{0 \cdot \frac{\Delta h}{2}} + E_n \frac{\Delta h}{2} - E_t \cdot \Delta w - \cancel{E_n \cdot \frac{\Delta h}{2}} + \cancel{0 \cdot \frac{\Delta h}{2}}$$

→ As $\Delta h \rightarrow 0$ $E_t = 0$



(a)

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ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



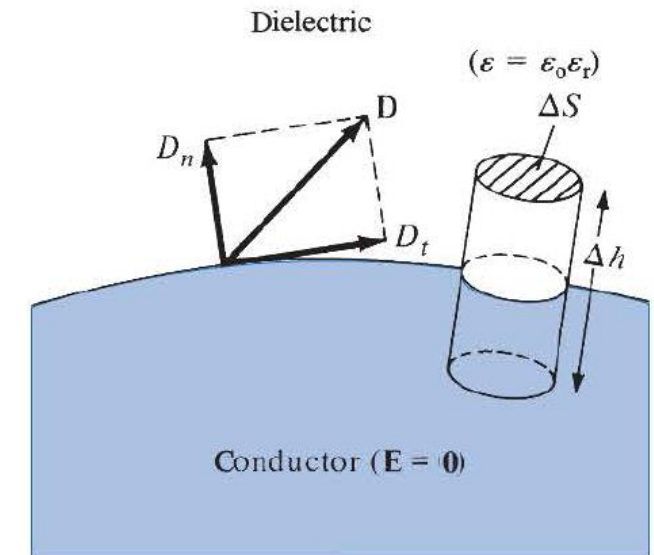
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→ Similarly, using $\oint_S \vec{D} \cdot d\vec{S} = Q_{enc.}$ w the cylindrical Gaussian surface & letting $\Delta h \rightarrow 0$, we have

$$\Delta Q = D_n \Delta S - \cancel{0 \cdot \Delta S} = P_s \Delta S$$

→ Since $\vec{D} = \epsilon \vec{E} = 0$ inside the conductor, we have

$$\boxed{D_n = P_s}$$



(b)

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ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



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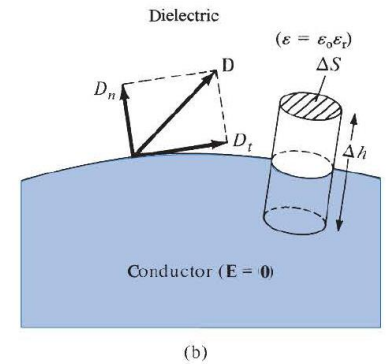
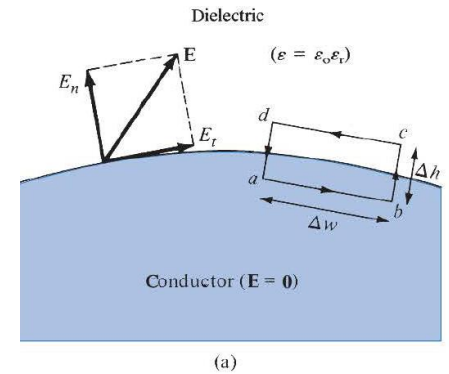
Conclusions! Under static conditions, following⁽²²⁾ can be inferred/concluded for a perfect conductor:

→ NO electric field may exist within the conductor.
 $\rho_v = 0$; $\vec{E} = 0$

→ Since $\vec{E} = \nabla V = 0$, there can be no potential difference between any 2 points in the conductor i.e. a conductor is an equipotential body.

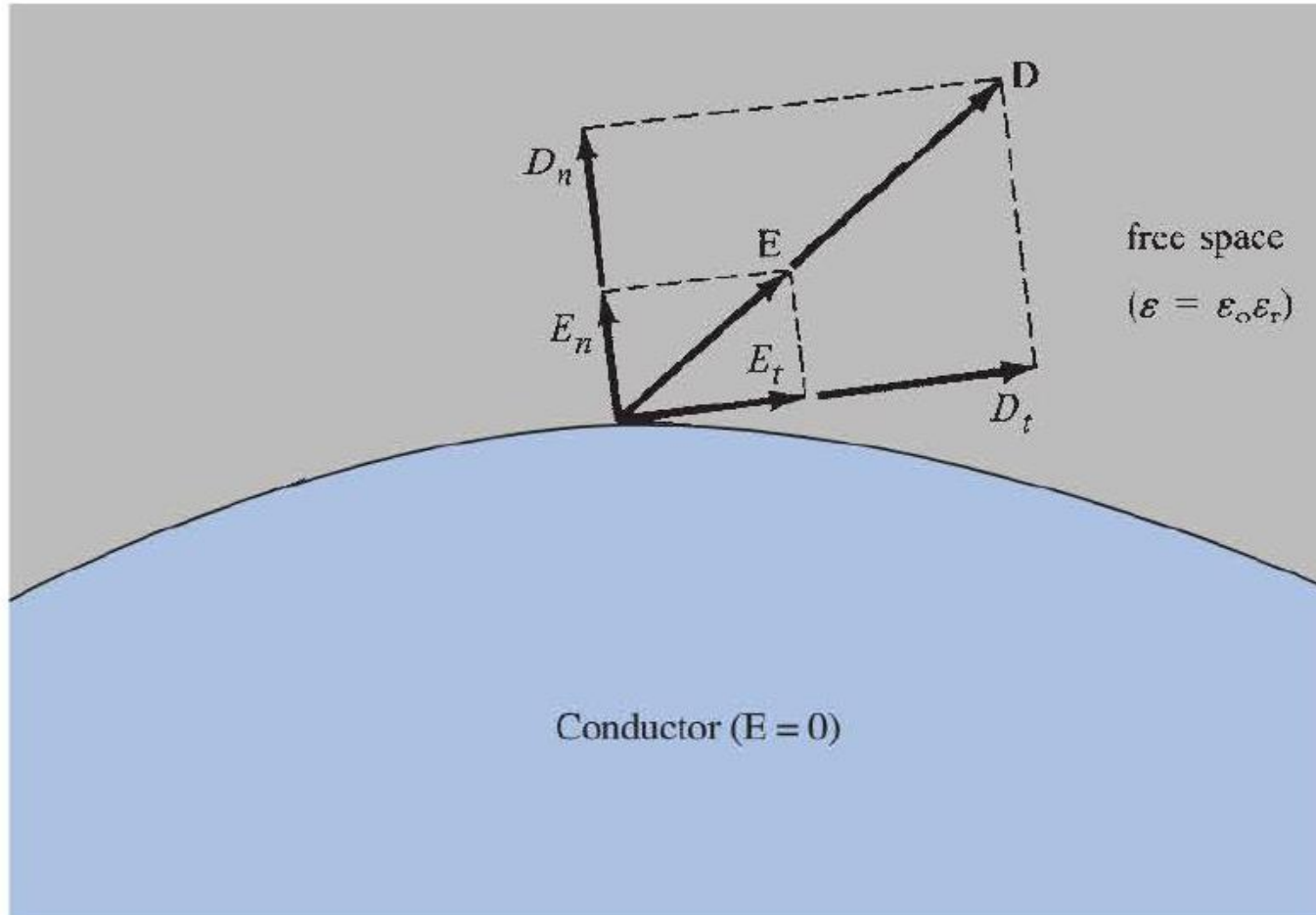
→ An electric field \vec{E} must be external to the conductor & must be normal to its surface.

$$D_t = \epsilon_0 \epsilon_r E_t = 0 \text{ \& } D_n = \epsilon_0 \epsilon_r E_n = \rho_s$$



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ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



Conductor – Free Space Boundary Conditions

EMF Theory – Unit -3

ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



Conductor - Free Space Boundary Conditions.

→ Refer the figure.

→ Boundary conditions can be obtained from

$$D_t = \epsilon_0 E_t = 0 \quad \& \quad D_n = \epsilon_0 E_n = \rho_s$$

by replacing ϵ_r by 1 (\because free space may be regarded as a special dielectric for which $\epsilon_r = 1$).

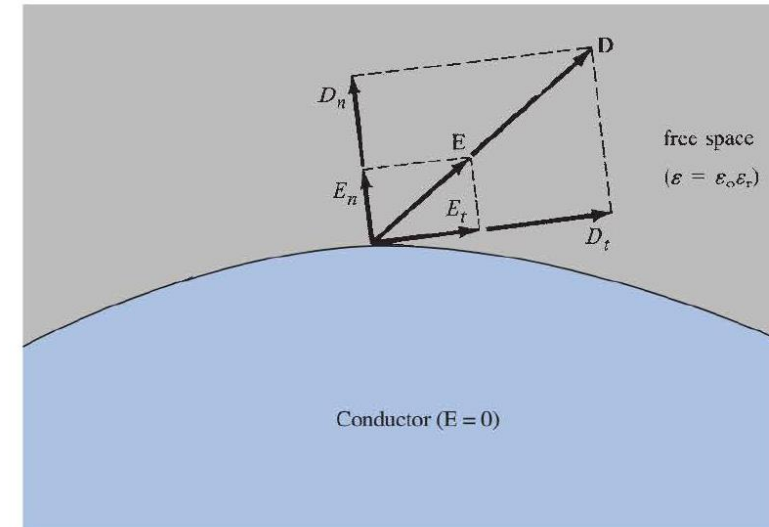
→ The electric field E must be external to the conductor & normal to its surface.

→ Then

$$D_t = \epsilon_0 E_t = 0 \quad \& \quad D_n = \epsilon_0 E_n = \rho_s$$

→ The above relation implies that the E field must approach the conducting surface normally.

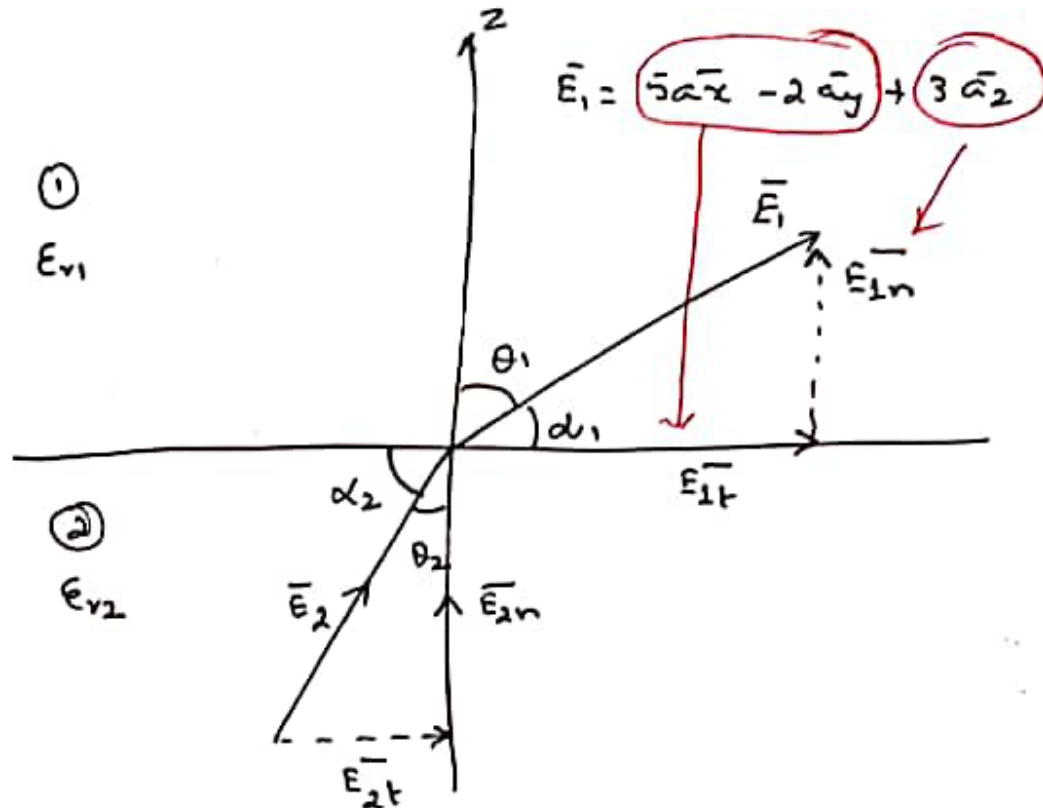
→ $\boxed{E \times \hat{n} = 0}$



EMF Theory – Unit -3

ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS

Two extensive homogeneous, isotropic dielectrics (23) meet on plane $z=0$. For $z>0$; $\epsilon_{r1}=4$, & for $z<0$ $\epsilon_{r2}=3$. A uniform electric field $\vec{E}_1 = 5\vec{a}_x - 2\vec{a}_y + 3\vec{a}_z$ kV/m exists for $z \geq 0$.



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ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



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(a) Find \vec{E}_2 for $z \leq 0$

Since \vec{a}_2 (unit vector in z-direction) is normal to the boundary plane, we can obtain the normal component as

$$E_{1n} = \vec{E}_1 \cdot \vec{a}_n = (5\vec{a}_x - 2\vec{a}_y + 3\vec{a}_z) \cdot (\vec{a}_z) = 3.$$

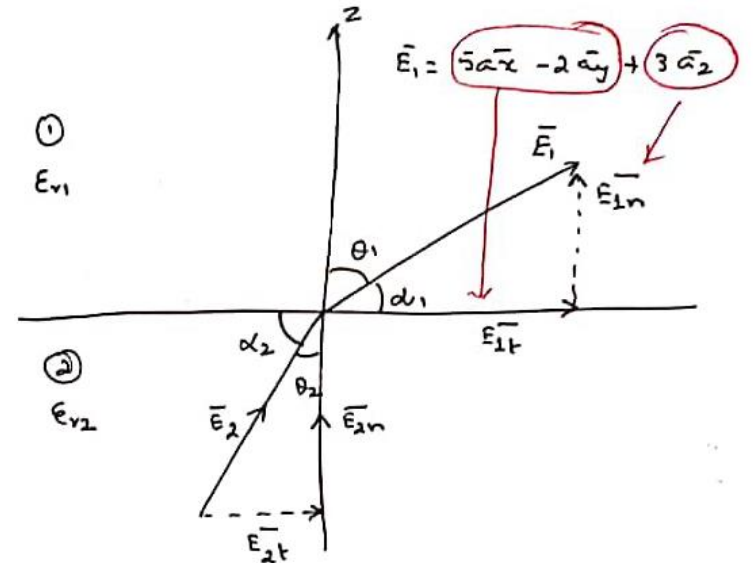
$$\therefore \vec{E}_{1n} = 3\vec{a}_z \text{ (in the +ve z direction)}$$

Similarly $\boxed{\vec{E}_{2n} = (E_2 \cdot \vec{a}_z) \vec{a}_z}$

$$\text{Now } \vec{E} = \vec{E}_t + \vec{E}_n \Rightarrow \vec{E}_{1t} = \vec{E}_1 - \vec{E}_{1n} = 5\vec{a}_x - 2\vec{a}_y + 3\vec{a}_z - 3\vec{a}_z$$
$$\underline{\underline{5\vec{a}_x - 2\vec{a}_y}}$$

Now using the boundary conditions of D-D, we have

$$\vec{E}_{1t} = \vec{E}_{2t} \text{ Hence } \underline{\underline{\vec{E}_{1t} = \vec{E}_{2t} = 5\vec{a}_x - 2\vec{a}_y}}$$



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ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS

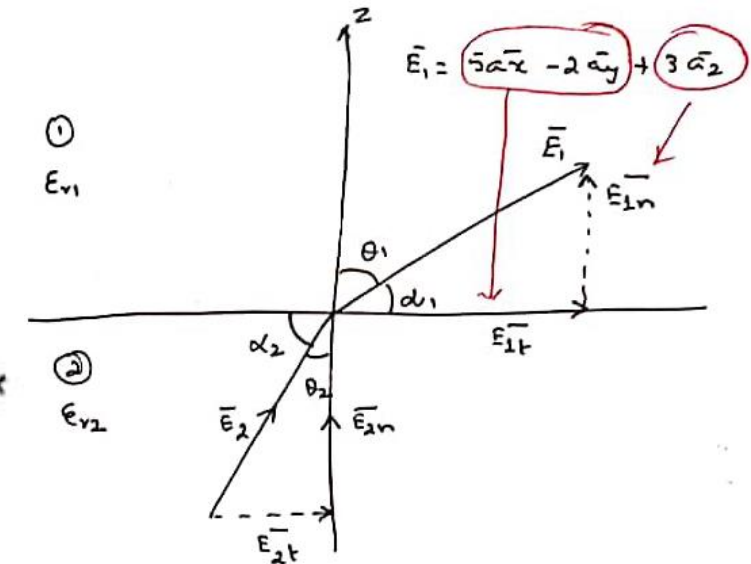
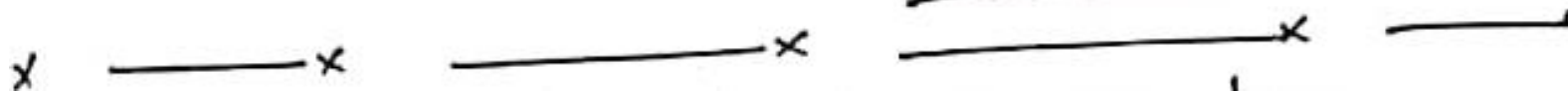


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Similarly $\underline{\underline{D_{1n} = D_{2n}}}$ or $\underline{\underline{E_{v1} \bar{E}_{1n} = E_{v2} \bar{E}_{2n}}}$ (24)

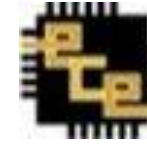
or $\bar{E}_{2n} = \frac{E_{v1}}{E_{v2}} \bar{E}_{1n} = \frac{4}{3} (3 \bar{a}_2) = \underline{\underline{4 \bar{a}_2}}$

Thus $\bar{E}_2 = \bar{E}_{2t} + \bar{E}_{2n} = \underline{\underline{5 \bar{a}_x - 2 \bar{a}_y + 4 \bar{a}_z}}$ kV/m



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(b) The angles \vec{E}_1 & \vec{E}_2 make with the interface.
from the diagram $\alpha_1 = 90^\circ - \theta_1$ & $\alpha_2 = 90^\circ - \theta_2$

method-1 Now $|\vec{E}_{1n}| \propto E_{1n} = 3$; $|\vec{E}_{1t}| = E_{1t} = \sqrt{5^2 + (-2)^2}$
 $= \underline{\underline{\sqrt{29}}}$

Hence $\tan \theta_1 = \frac{|\vec{E}_{1t}|}{|\vec{E}_{1n}|} = \frac{E_{1t}}{E_{1n}} = \frac{\sqrt{29}}{3}$

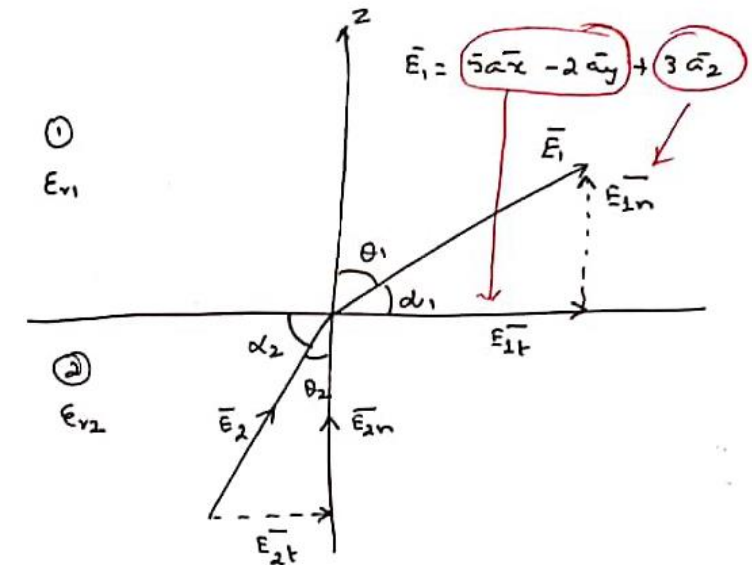
or $\theta_1 = \tan^{-1}\left(\frac{\sqrt{29}}{3}\right) = \underline{\underline{60.8784^\circ}}$

$\therefore \alpha_1 = 90^\circ - 60.8784 = \underline{\underline{29.1216^\circ}}$

method-2 $\vec{E}_1 \cdot \vec{a}_n = |\vec{E}_1| \cdot |\vec{a}_n| \cos \theta_1$

or $\cos \theta_1 = \frac{\vec{E}_1 \cdot \vec{a}_n}{|\vec{E}_1| (1)} \quad \text{since } \vec{a}_n = \vec{a}_2 = \frac{3}{\sqrt{5^2 + (-2)^2 + 3^2}}$

$\cos \theta_1 = \frac{3}{\sqrt{38}} = \underline{\underline{60.8784^\circ}} \Rightarrow \alpha_1 = 90^\circ - 60.8784 = \underline{\underline{29.1216^\circ}}$



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ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



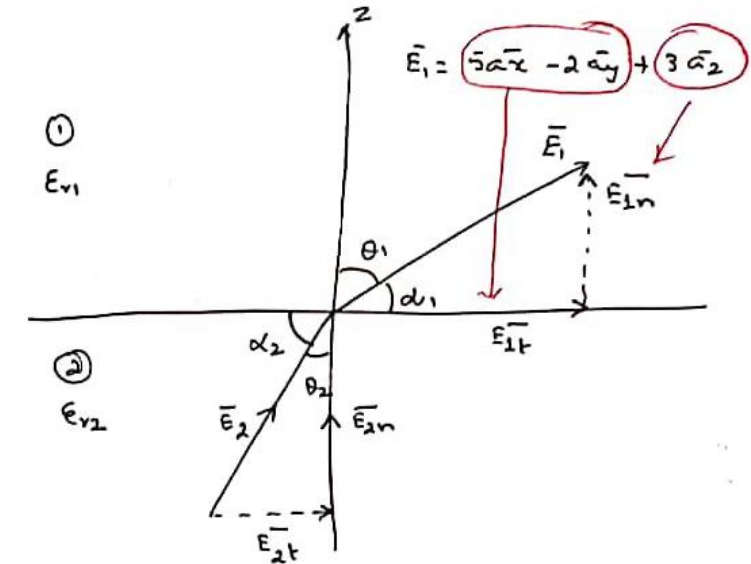
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Similarly $|\vec{E}_{2n}| = |4\vec{a}_2| = 4$; $E_{2t} = E_{1t} = \sqrt{29}$

$$\therefore \tan \theta_2 = \frac{E_{2t}}{E_{2n}} = \frac{\sqrt{29}}{4} = 1.346 \Rightarrow \theta_2 = \tan^{-1}(1.346) \\ = \underline{\underline{53.3957^\circ}}$$

Hence $\alpha_2 = 90^\circ - \theta_2 = \underline{\underline{36.6043^\circ}}$

Check $\frac{\tan \theta_1}{\tan \theta_2} = \frac{E_{v1}}{E_{v2}} \Rightarrow \underline{\underline{1.333}}$



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ELECTRIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



(c) The energy densities in both dielectrics. (25)

Recall $w_E = \frac{1}{2} \mathbf{D} \cdot \mathbf{\bar{E}} = \frac{1}{2} \epsilon \bar{E}^2$ $\epsilon = |\bar{\epsilon}|$: $\epsilon = \epsilon_0 \epsilon_r$

$$\begin{aligned} \text{Then } w_{E1} &= \frac{1}{2} \epsilon_1 |\bar{E}_1|^2 = \frac{1}{2} \times \frac{4 \times 10^{-9}}{36\pi} \times (25+4+9) \times 10^6 \\ &= \underline{\underline{672 \mu\text{J}/\text{m}^3}} \end{aligned}$$

$\underbrace{\quad}_{\epsilon_1 = \epsilon_0 \epsilon_{r1}} \quad \underbrace{\quad}_{|\bar{E}_1|^2}$

Similarly

$$\begin{aligned} w_{E2} &= \frac{1}{2} \epsilon_2 |\bar{E}_2|^2 = \frac{1}{2} \times \frac{3 \times 10^{-9}}{36\pi} \times (25+4+16) \times 10^6 \\ &= \underline{\underline{597 \mu\text{J}/\text{m}^3}} \end{aligned}$$

————— x —————

(d) The energy within a cube of side 2m centred at (3,4,-5).

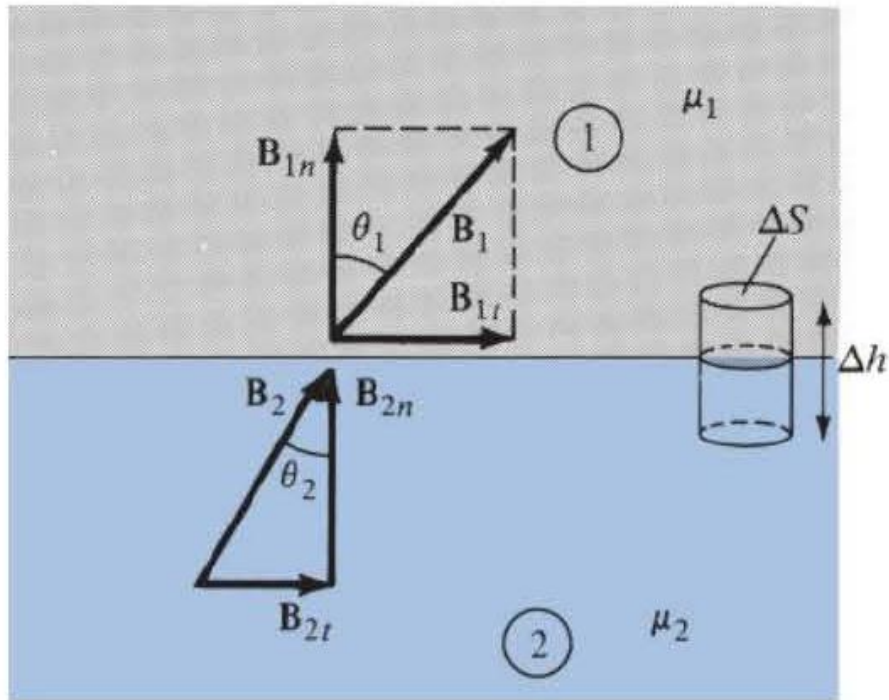
At the centre (3,4,-5), of the cube of side 2m, $z = -5 < 0$
i.e. the cube is in Region ② with $2 \leq x \leq 4$, $3 \leq y \leq 5$
4 $-6 \leq z \leq -4$. Therefore

$$W_E = \int W_{E2} dv = \int_{x=2}^4 \int_{y=3}^5 \int_{z=-6}^{-4} w_{E2} dz dy dx.$$
$$= w_{E2} (2)(2)(2) = 597 \times 8 = \underline{\underline{4.776 \text{ mJ}}}$$

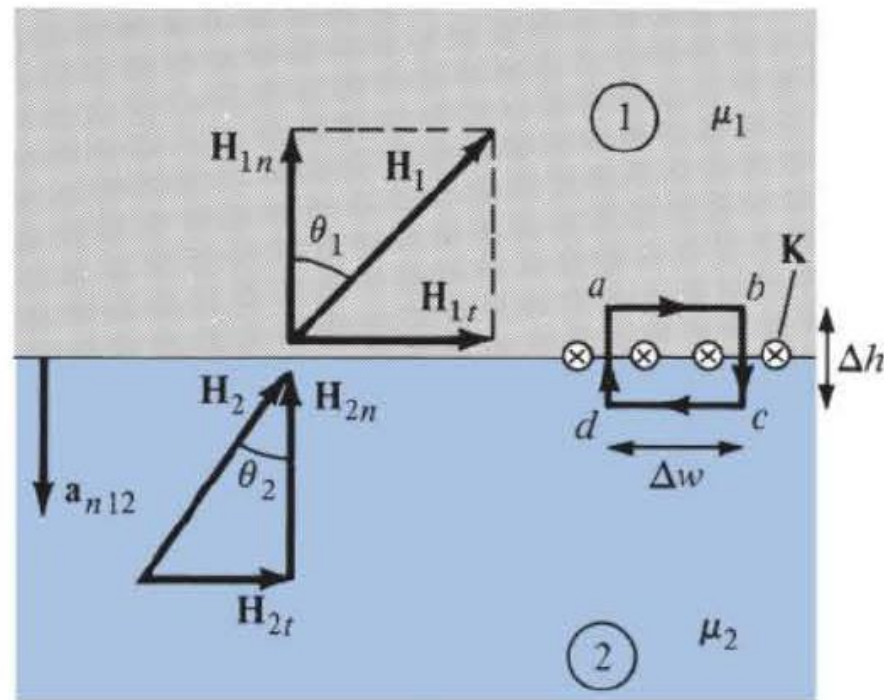


EMF Theory – Unit -3

MAGNETIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



(a)



(b)



Summary:

$$B_{1n} = B_{2n} \quad \text{or} \quad \mu_1 H_{1n} = \mu_2 H_{2n}$$

$$(H_{1n} - H_{2n}) \times a_{n12} = K$$

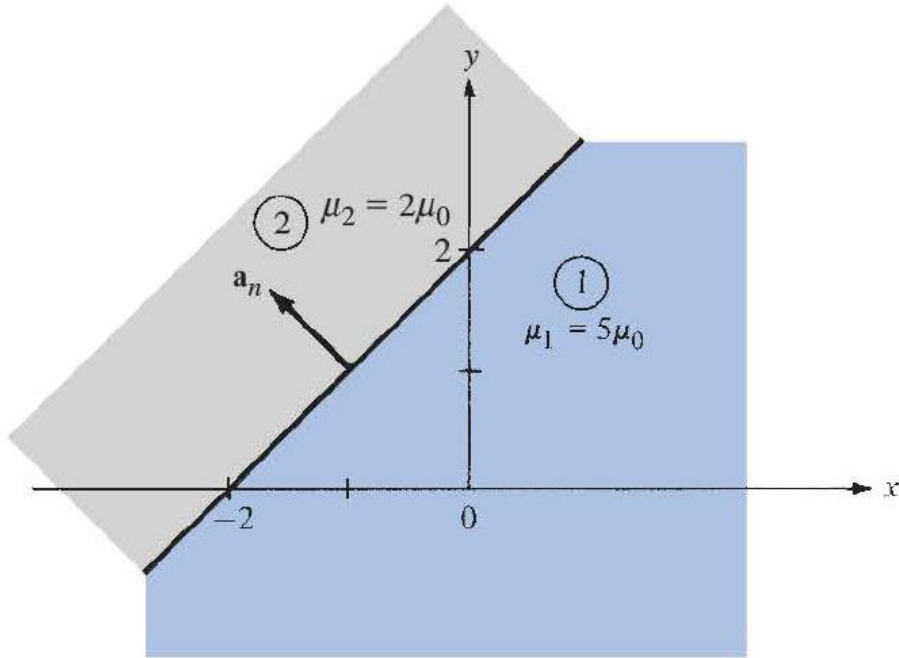
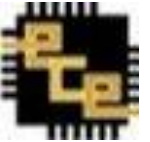
$$H_{1t} = H_{2t} \quad \text{or} \quad \frac{B_{1t}}{\mu_1} = \frac{B_{2t}}{\mu_2} \quad \text{with the boundary free of current.}$$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\mu_1}{\mu_2}$$



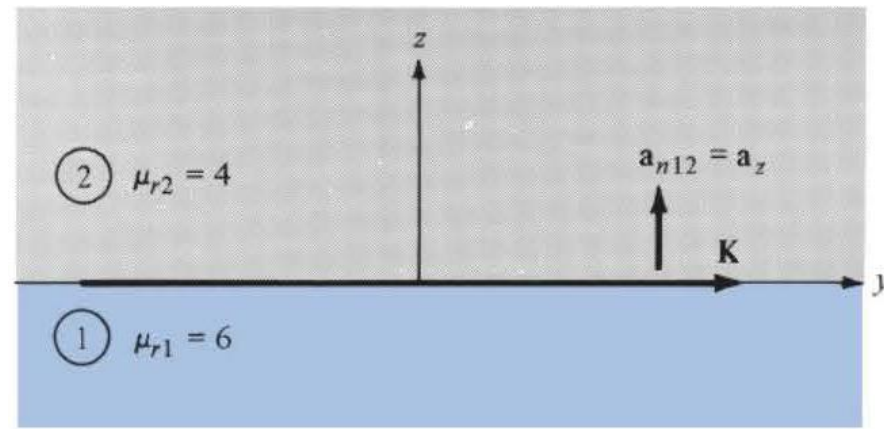
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MAGNETIC FIELDS IN MATERIAL SPACE – BOUNDARY CONDITIONS



Ex. 1

Ex. 2





THANK YOU

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