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CONTROL SYSTEMS

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CONTROL SYSTEMS

Stability of Control Systems

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- **Time domain methods**
 - **Routh-Hurwitz Criterion**
 - **Root Locus Technique**
- **Frequency domain methods**
 - **Bode Analysis**
 - **Nyquist Stability Criterion**

FREQUENCY DOMAIN METHODS

Stability of Control Systems: Bode Plot

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Advantages

- Frequency response tests are generally simple and can be determined accurately by use of sinusoidal signal generators and precise measurement equipment.
- Transfer function of complicated systems can be determined experimentally by frequency response tests
- System may be designed so that effects of undesirable noise are negligible and such analysis and design can be extended to non linear systems

Advantages

- Modeling transfer functions from physical data.
- Designing compensators to meet steady state error and transient response requirements.
- Finding stability of systems

FREQUENCY RESPONSE

Sinusoidal Transfer Function



$$Y(s) = G_1(s) R(s)$$

$r(t) = A \sin \omega t \rightarrow$ Reference input

$$R(s) = \frac{A \omega}{s^2 + \omega^2}$$

$$Y(s) = G_1(s) R(s) = G_1(s) \frac{A \omega}{s^2 + \omega^2} \leftarrow G_1(s) \frac{A \omega}{(s+j\omega)(s-j\omega)} = \frac{A_1}{s+j\omega} + \frac{A_2}{s-j\omega}$$

$$A_1 = \frac{G_1(s) A \omega (s+j\omega)}{(s+j\omega)(s-j\omega)} \Bigg|_{s=-j\omega} = \frac{G_1(-j\omega) A \omega}{-2j\omega} = \frac{A G_1(-j\omega)}{-2j}$$

FREQUENCY RESPONSE

Sinusoidal Transfer Function

$$A_2 = \frac{G_1(s) A \omega (s/j\omega)}{(s+j\omega)(s-j\omega)} \Big|_{s=j\omega} = \frac{G_1(j\omega) A \cancel{\omega}}{2j\cancel{\omega}} = \frac{A G_1(j\omega)}{2j}$$

$$Y(s) = \frac{1}{2j} \left[-\frac{A G_1(-j\omega)}{s+j\omega} + \frac{A G_1(j\omega)}{s-j\omega} \right]$$

$$G_1(j\omega) = |G_1(j\omega)| e^{j\phi}, \quad \phi = \underline{|G_1(j\omega)|}$$

$$G_1(-j\omega) = |G_1(j\omega)| e^{-j\phi}$$

$$Y(s) = \frac{A |G_1(j\omega)|}{2j} \left[-e^{-j\phi} \frac{1}{s+j\omega} + e^{+j\phi} \frac{1}{s-j\omega} \right]$$

$$\text{ILT, } y(t) = \frac{A |G_1(j\omega)|}{2j} \left[-e^{-j\phi} \cdot e^{-j\omega t} + e^{+j\phi} \cdot e^{+j\omega t} \right] = \frac{A |G_1(j\omega)|}{2j} \left[-e^{-j(\phi+\omega t)} + e^{j(\phi+\omega t)} \right]$$

FREQUENCY RESPONSE

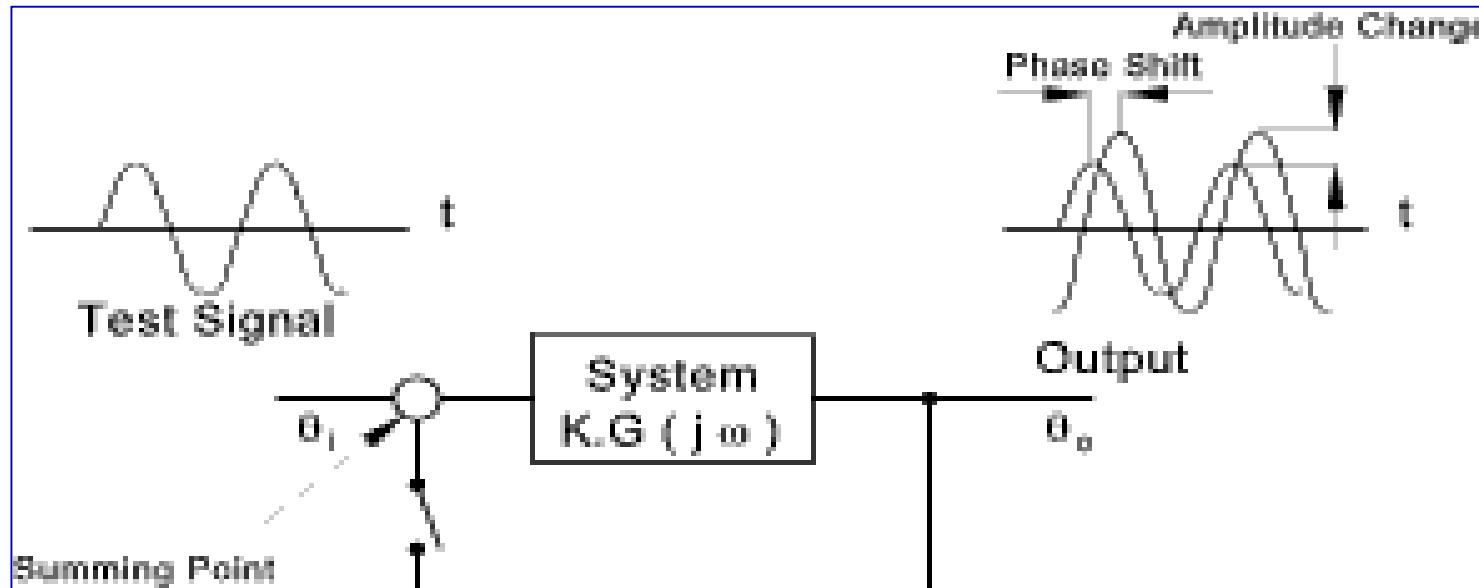
Sinusoidal Transfer Function

$$y(t) = A |G(j\omega)| \sin(\phi + \omega t)$$

FREQUENCY RESPONSE

Sinusoidal Transfer Function

- **Sinusoidal transfer function:** Transfer function as a function of $j\omega$
- For a linear system sinusoidal input results in sinusoidal output
- The steady state output will have same frequency as the input
- Amplitude and phase of output will vary with frequency



$$r(t) = A \sin \omega t$$
$$y(t) = A|G(j\omega)| \sin(\phi + \omega t)$$

FREQUENCY RESPONSE

Sinusoidal Transfer Function

- In the steady state, sinusoidal inputs to a linear system generate sinusoidal responses of the same frequency, but Output differs in amplitudes and phase angle from the input
- Differences are function of frequency.
- Frequency response: Steady state response (output) of a system to sinusoidal inputs of varying frequency.
- It is plot of magnitude and phase as a function of frequency (as only magnitude and phase change with change in frequency).

FREQUENCY RESPONSE

Sinusoidal Transfer Function

Ex: For the sinusoidal transfer function $G(s)=1/(s+1)$, find the magnitude and phase of $G(s)$

Procedure:

1. Put $s= j\omega$

2. $G(j\omega)=1/(j\omega+1)$

$$|G(j\omega)| = \frac{1}{\sqrt{\omega^2 + 1}}$$

$$M = 20 \log_{10}(1/\sqrt{1+\omega^2}) \text{ dB}$$

$$M = -20 \log_{10}\sqrt{1+\omega^2} \text{ dB}$$

$$\phi = \arg(G(j\omega)) = 0 - \tan^{-1}\frac{\omega}{1}$$

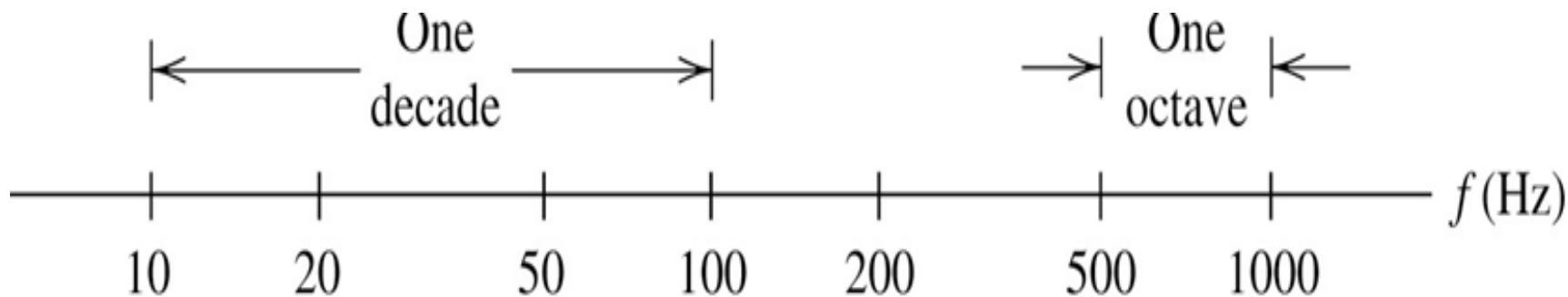
⇒ Magnitude in dB

$$20 \log |G(j\omega)| = 20 \log \frac{1}{\sqrt{\omega^2 + 1}}$$
$$M = -20 \log \frac{\sqrt{\omega^2 + 1}}{10}$$
$$M = -20 \log \sqrt{\omega^2 + 1}$$
$$\phi = \arg(G(j\omega)) = 0 - \tan^{-1}\frac{\omega}{1}$$

FREQUENCY RESPONSE

Sinusoidal Transfer Function

- On a logarithmic scale, the variable is multiplied by a given factor for equal increments of length along the axis.
- Decade Change – \log_{10}
- Octave change – \log_2



CONTROL SYSTEMS

Stability of Control Systems: Bode Plot

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FREQUENCY RESPONSE

Bode Plot

- Bode Plot:

Magnitude plot - magnitude vs frequency

Phase plot – phase vs frequency

Open loop transfer function

- Plotted in log scale(to cover large range)

Magnitude in decibels(dB)

Frequency in rad/sec (on log scale)

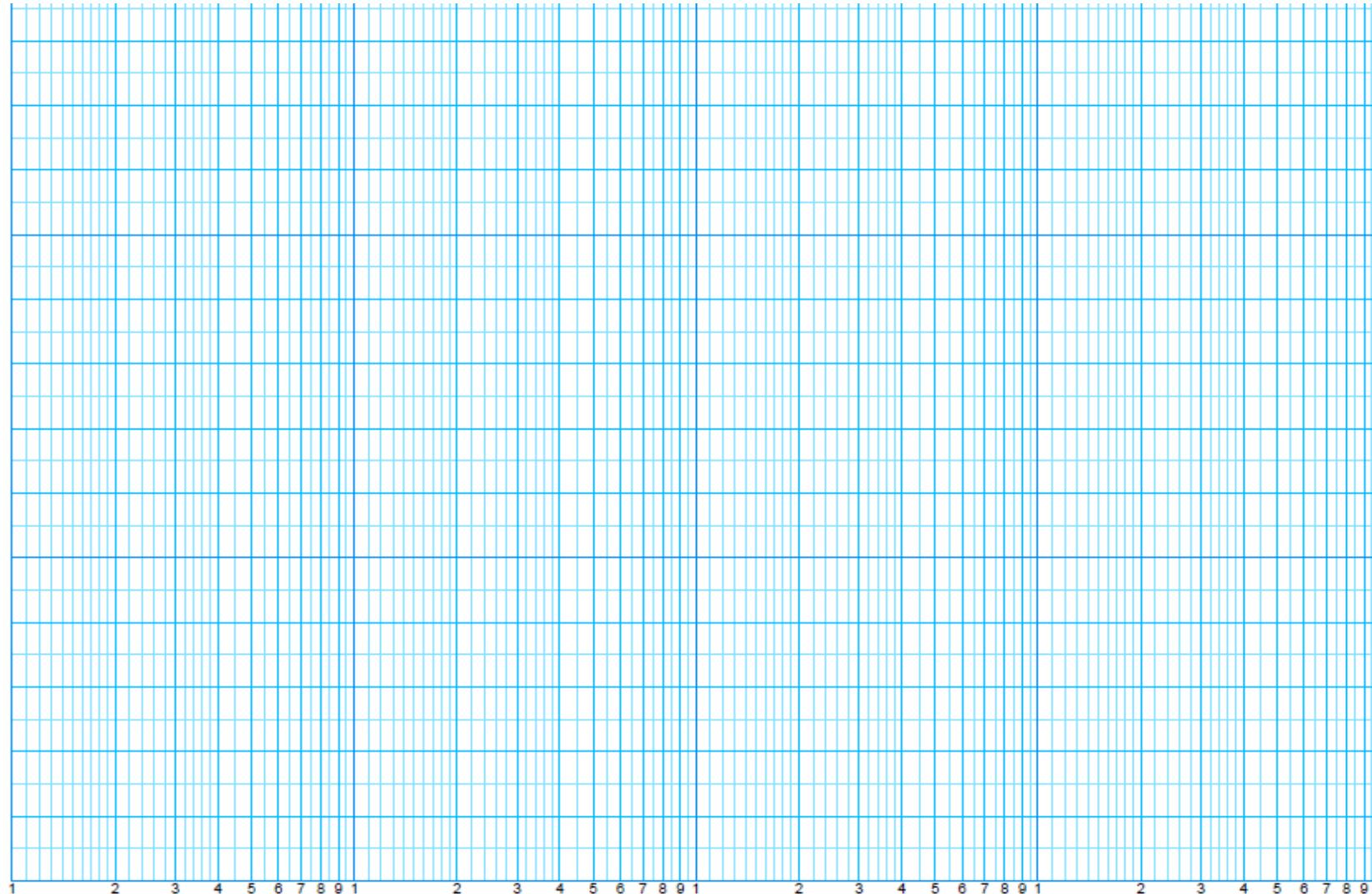
- Consider an open loop transfer function

$$G(s)H(s) = \frac{k(s + z_1)(s + z_2) \dots (s + z_m)}{(s + p_1)(s + p_2) \dots (s + p_n)}$$

- Poles and Zeros are the **singularities** of this function
- Find the expressions of magnitude($M(\omega)$ in dB) and phase($\varphi(\omega)$) in degrees of $G(j\omega)H(j\omega)$
- M and φ are plotted against $\log \omega$ to give the magnitude and phase plots:
Bode plot
- Plotted on a Semilog graph sheet
Frequency axis is logarithmic and magnitude axis is linear

FREQUENCY RESPONSE

Semi Log Sheet



- Since it is a logarithmic plot, the product of terms are converted to additions
- Complicated functions can be visualized in terms of individual standard plots
- Since log scale is used, it is helpful in covering a large range of magnitude and phase

$$G(s)H(s) = \frac{k(s + z_1)(s + z_2) \dots (s + z_m)}{(s + p_1)(s + p_2) \dots (s + p_n)}$$

FREQUENCY RESPONSE

Bode Plot



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$$G(j\omega) = \frac{1}{K} \prod_{i=1}^m (1 + T_{Z_i} j\omega)$$

$$\frac{1}{K} \prod_{j=1}^n (1 + T_{P_j} j\omega)$$

$$|G(j\omega)| = K \prod_{i=1}^m \sqrt{1 + T_{Z_i}^2 \omega^2}$$

$$\prod_{j=1}^n \sqrt{1 + T_{P_j}^2 \omega^2}$$

$$\sum_{j=1}^m \log_{10} \sqrt{1 + \tau_{z_j}^2 w_j^2} - \sum_{j=1}^n \log_{10} \sqrt{1 + \tau_{f_j}^2 w_j^2}$$

$$[G(j\omega)] = \sum_{i=1}^m \tan^{-1} \omega T_i - \sum_{j=1}^n \tan^{-1} \omega T_j$$

$$G(s) = K \frac{\prod_{i=1}^m (s + z_i)}{\prod_{j=1}^n (s + p_j)}$$

→ Pole - Zero form

$$= K' \frac{\prod_{i=1}^m (1 + T_{z_i} s)}{\prod_{j=1}^n (1 + T_{p_j} s)}$$

→ Time constant form

- Magnitude in dB:

$$20\log|G(j\omega)H(j\omega)| = 20\log k + 20\log \sqrt{1+\omega^2T_1^2} + 20\log \sqrt{1+\omega^2T_2^2} - \dots - 20\log \sqrt{1+\omega^2T_m^2}$$
$$- 20\log \sqrt{1+\omega^2T_a^2} + 20\log \sqrt{1+\omega^2T_b^2} - \dots - 20\log \sqrt{1+\omega^2T_n^2}$$

- Phase:

$$\varphi(j\omega) = \tan^{-1}(\omega T_1) + \tan^{-1}(\omega T_2) + \dots + \tan^{-1}(\omega T_m)$$
$$- \tan^{-1}(\omega T_a) - \tan^{-1}(\omega T_b) - \dots - \tan^{-1}(\omega T_n)$$

BODE PLOT

Bode Magnitude Plots

$$G(s) = \frac{K(1+zs)}{(sL + 1 + zs)}$$

Simple function :

$$K, s^n, \frac{1}{s^N}, (1+zs), \frac{1}{1+zs}$$

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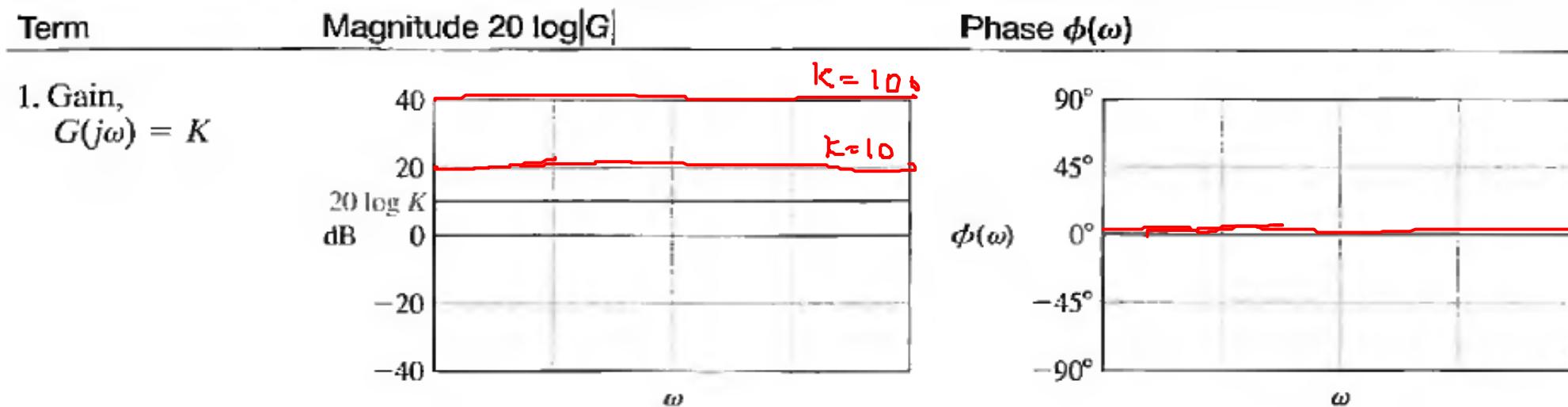
FREQUENCY RESPONSE

Bode Plot for Individual Singularities

- Constant k : Magnitude plot is a constant with magnitude $20 \log k$ dB

$$|k| = 20 \log_{10} |k| , \angle k = 0^\circ$$

$$k = 10, M_{dB} = 20 dB, K = 100, M_{dB} = 40 dB$$



FREQUENCY RESPONSE

Bode Plot for Individual Singularities

- Simple zero at origin: $G(s) = s$

$$G(j\omega) = j\omega \Rightarrow |G(j\omega)| = \omega$$

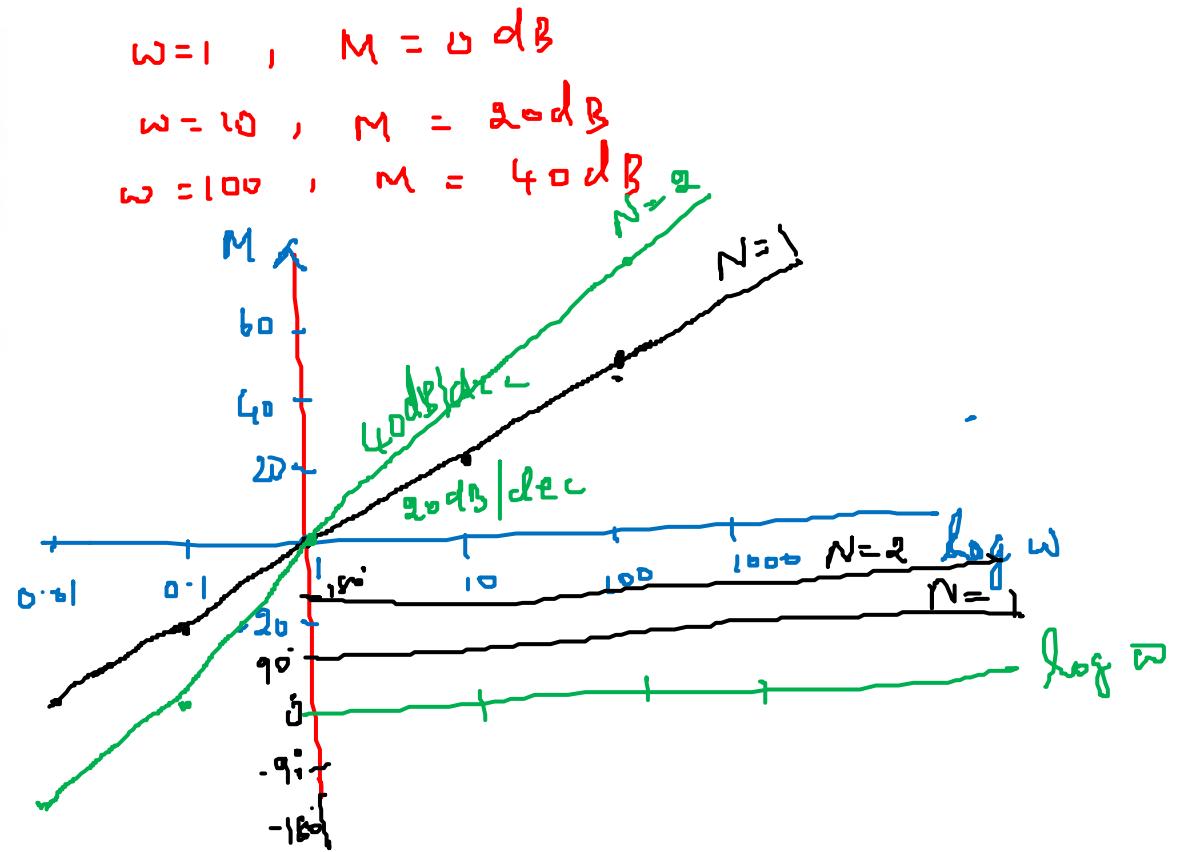
$$20 \log_{10} |G(j\omega)| = 20 \log_{10} \omega$$

- Straight line with slope 20 dB/dec passing through 0dB line at $\omega = 1$

$$20 \log|j\omega| = +20 \log \omega,$$

where the slope is +20 dB/decade and the phase angle is

$$\phi(\omega) = +90^\circ.$$



FREQUENCY RESPONSE

Bode Plot for Individual Singularities

- Multiple zeros at origin (N zeros): $G(s) = s^N$, $G(j\omega) = (j\omega)^N$
 $|G(j\omega)| = \omega^N$, $M = 20N \log_{10} \omega$
- Straight line with slope $20N$ dB/dec passing through 0dB line at $\omega = 1$ $= 40 \log_{10} \omega$

	$M [dB]$	ϕ
$N=2$, $\omega = 0.01$	- 20	π
0.1	- 40	π
1	0	$\frac{\pi}{2}$
10	40	$\frac{\pi}{4}$

$$G(j\omega) = N \pi / 2$$

FREQUENCY RESPONSE

Bode Plot for Individual Singularities



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- Simple pole at origin:

$$G(s) = \frac{1}{s}, \quad G(j\omega) = \frac{1}{j\omega}, \quad |G(j\omega)| = \frac{1}{\omega}$$

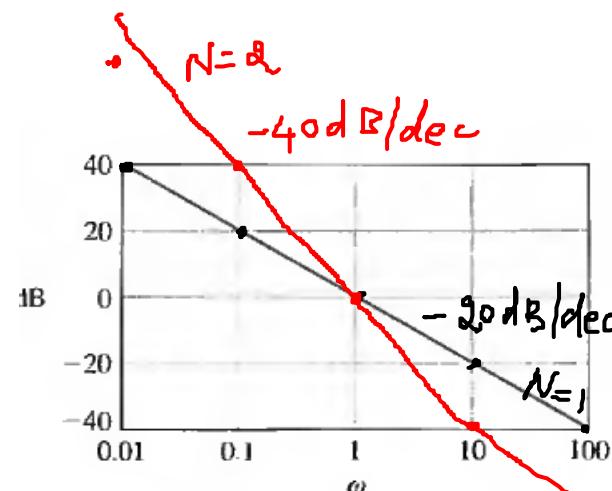
$$M = -20 \log_{10} \omega$$

- Straight line with slope -20 dB/dec passing through 0dB line at $\omega = 1$

$$\phi = 0 - \tan^{-1}\left(\frac{\omega}{\omega_0}\right) = -\bar{\gamma}/2$$

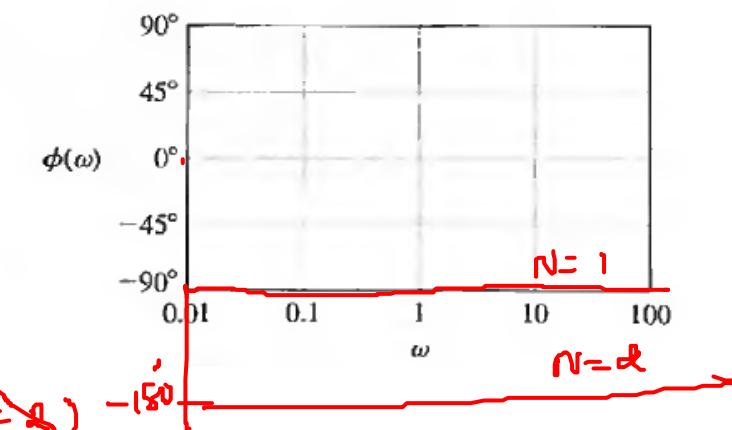
$$20 \log \left| \frac{1}{j\omega} \right| = -20 \log \omega \text{ dB}$$

$$\phi(\omega) = -90^\circ.$$



$$G(s) = \frac{1}{s^N} \Rightarrow M = -20N \log_{10} \omega \Rightarrow -40 \log_{10} \omega \quad (N=1)$$

$$\phi = -N\bar{\gamma}_2$$



FREQUENCY RESPONSE

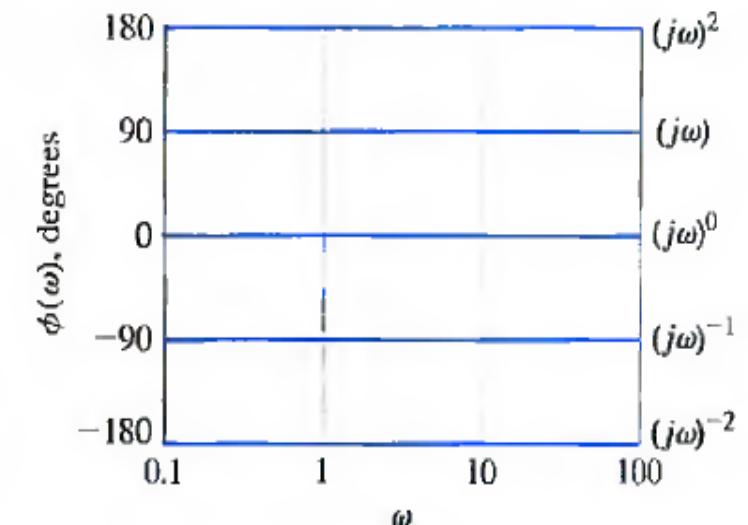
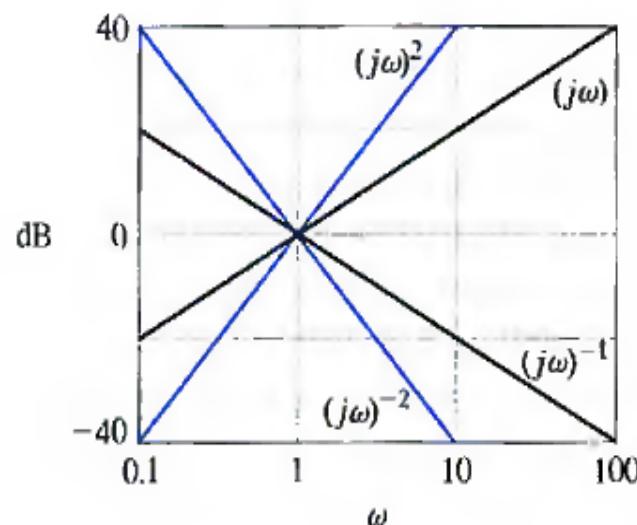
Bode Plot for Individual Singularities

- Multiple poles at origin (N Poles):

- Straight line with slope $-20N$ dB/dec passing through 0dB line at $\omega = 1$

$$20 \log \left| \frac{1}{(j\omega)^N} \right| = -20N \log \omega,$$

$$\phi(\omega) = -90^\circ N.$$



$$(s+1) (s+3)$$

- Simple/multiple zero (zero on real axis)
 - Corner Frequency: Value of ω where the slope changes from 0 dB to 20dB/dec
 - Magnitude is 0 dB till corner/critical/break frequency and straight line with slope of 20 dB/dec or $20N$ dB/dec beyond corner frequency
 - Hence approximate (asymptotic) plot has 2 lines (0dB and 20dB/dec line) meeting at corner frequency $\omega=1/T$
 - Determine the true/actual plot

FREQUENCY RESPONSE

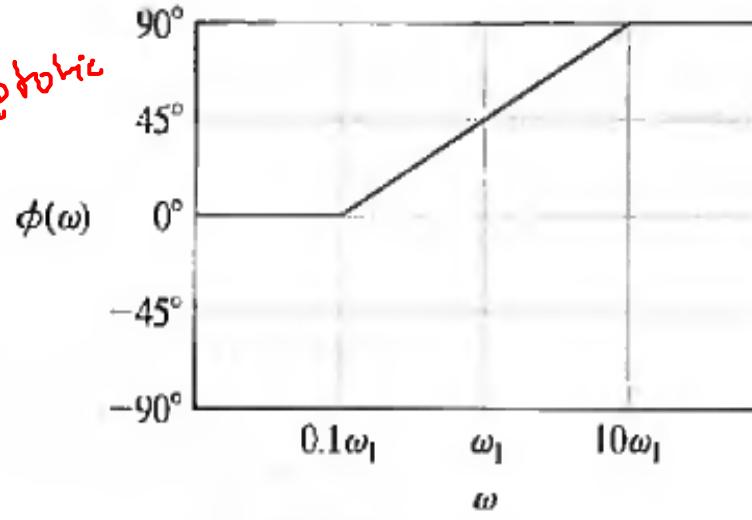
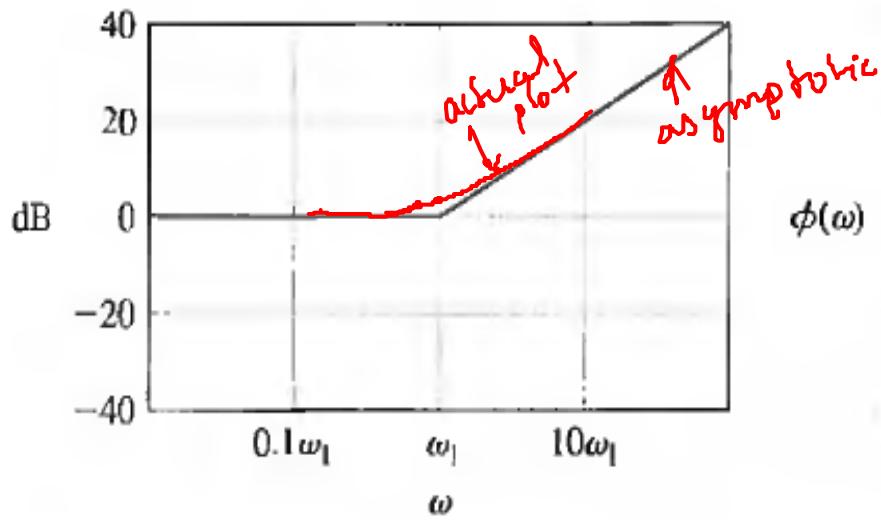
Bode Plot for Individual Singularities

Zero on the real axis: $(1 + \tau s)$

$$G(j\omega) = 1 + j\omega\tau$$

$$|G_1(j\omega)| = \sqrt{1 + \omega^2\tau^2}, \quad \angle G_1(j\omega) = \tan^{-1} \omega\tau$$

$$\text{at } \omega = 0 \log |G_1(j\omega)| = 0, \log_{10}(1 + \omega^2\tau^2) = \begin{cases} 0 \text{ dB}, & \omega\tau \ll 1 \\ 3 \text{ dB}, & \omega\tau = 1 \\ 20 \log \omega\tau, & \omega\tau \gg 1 \end{cases}$$



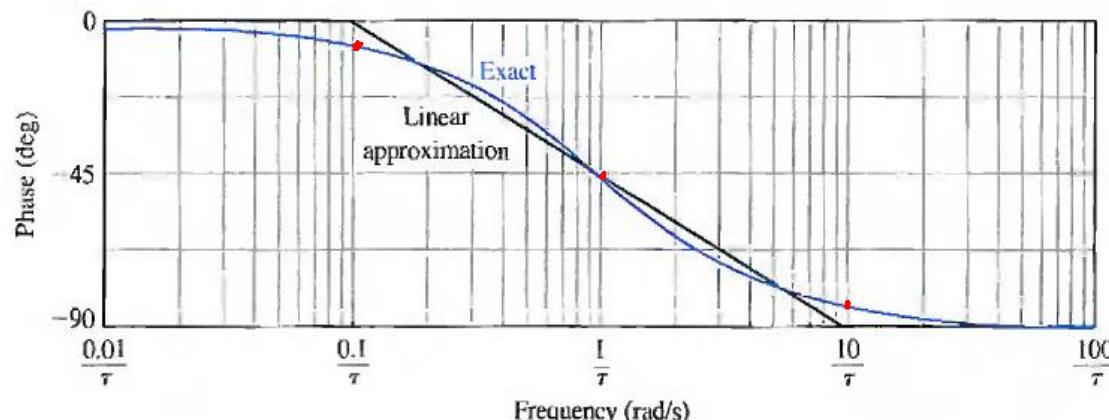
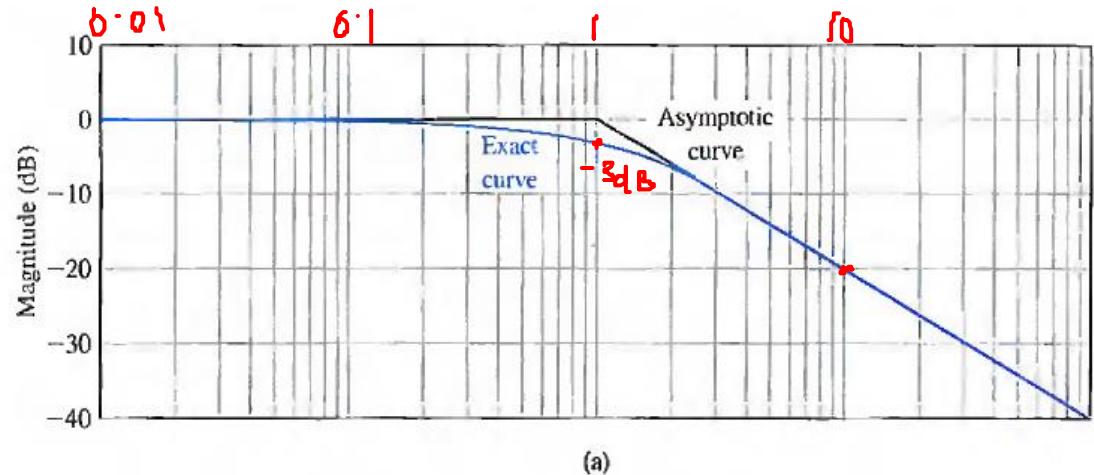
$$(S + Z_i) = Z_i \left(\frac{1}{Z_i} + 1 \right)$$

$\frac{1}{Z_i} \approx \frac{1}{Z} \Rightarrow \text{higher freq.}$

FREQUENCY RESPONSE

Bode Plot for Individual Singularities

Pole on the real axis: $\frac{1}{(1+\tau s)}$



$$G(j\omega) = \frac{1}{1 + j\omega\tau}$$

$$\{|G(j\omega)|\} = \frac{1}{\sqrt{1 + \omega^2\tau^2}}$$

$$\{|G(j\omega)|\}_{dB} = -10 \log_{10} (1 + \omega^2\tau^2)$$

$$= \begin{cases} 0 \text{ dB} & \omega\tau \ll 1 \\ -3 \text{ dB} & \omega\tau = 1 \\ -20 \log_{10} \omega\tau & \omega\tau \gg 1 \end{cases}$$

$$\angle G(j\omega) = -\tan^{-1} \omega\tau$$

$$= \begin{cases} 0^\circ & \omega\tau \ll 1 \\ -5^\circ & \omega\tau = 0.1 \\ -45^\circ & \omega\tau = 1 \\ -85^\circ & \omega\tau = 10 \\ -90^\circ & \omega\tau \gg 1 \end{cases}$$

FREQUENCY RESPONSE

Bode Plot for Individual Singularities

Complex conjugate poles or zeros: $\frac{1}{(s^2 + 2\zeta\omega_n s + \omega_n^2)} \Rightarrow G(j\omega) = \frac{1}{-\omega^2 + 2\zeta\omega_n j\omega + \omega_n^2}$

Normalized form: $G(j\omega) = \frac{1}{(1-u^2) + j2\zeta u}$, where $u = \frac{\omega}{\omega_n}$

$|G(j\omega)| = \sqrt{(1-u^2)^2 + 4\zeta^2 u^2} \rightarrow \text{normalized form}$

$$20 \log|G(j\omega)| = -10 \log((1-u^2)^2 + 4\zeta^2 u^2),$$

$$\phi(\omega) = -\tan^{-1} \frac{2\zeta u}{1-u^2}$$

$$= \frac{1}{\omega_n^2 \left(-\frac{\omega^2}{\omega_n^2} + 2j\zeta \frac{\omega}{\omega_n} + 1 \right)}$$

$$= \frac{1}{\omega_n^2 \left(-\omega^2 + 2j\zeta \omega_n + 1 \right)}$$

$$= \frac{1}{(1-u^2) + j2\zeta u}$$

When $u \ll 1$, the magnitude is

$$20 \log|G(j\omega)| = -10 \log 1 = 0 \text{ dB},$$

When $u \gg 1$,

$$20 \log|G(j\omega)| = -10 \log u^4 = -40 \log u,$$

FREQUENCY RESPONSE

Bode Plot for Individual Singularities

Complex conjugate poles or zeros: $\frac{1}{(s^2 + 2\zeta\omega_n s + \omega_n^2)}$

Normalized form: $G(j\omega) = \frac{1}{(1-u^2)+j2\zeta u}$, where $u = \frac{\omega}{\omega_n}$

$$20 \log|G(j\omega)| = -10 \log((1 - u^2)^2 + 4\zeta^2 u^2),$$

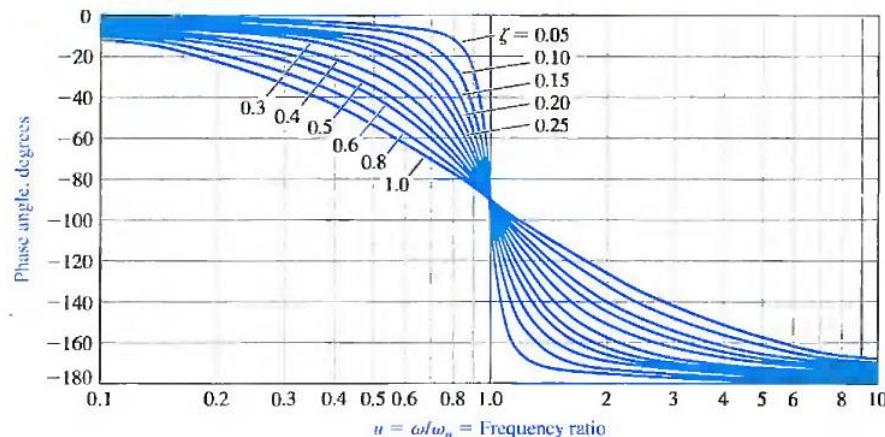
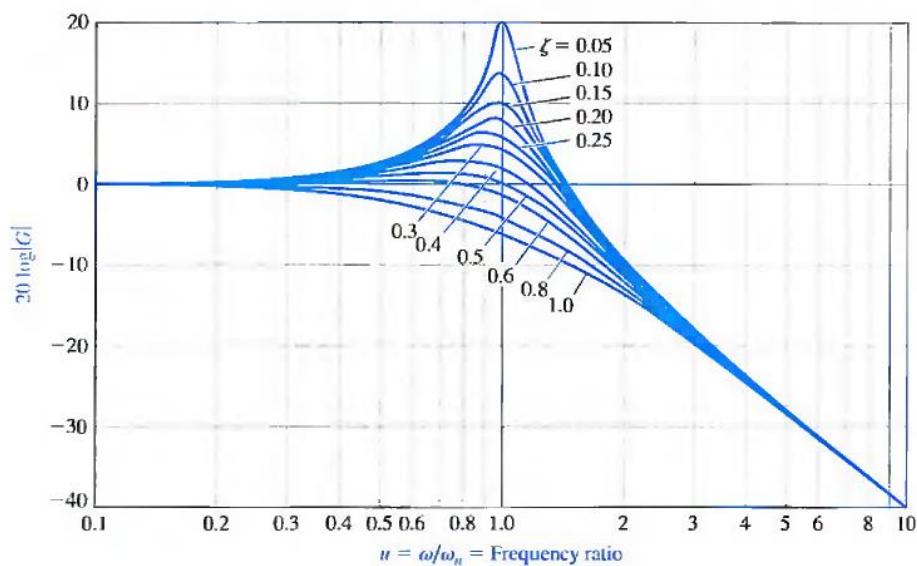
$$\phi(\omega) = -\tan^{-1} \frac{2\zeta u}{1 - u^2}.$$

When $u \ll 1$, the magnitude is

$$20 \log|G(j\omega)| = -10 \log 1 = 0 \text{ dB},$$

When $u \gg 1$,

$$20 \log|G(j\omega)| = -10 \log u^4 = -40 \log u,$$



FREQUENCY RESPONSE

Bode Plot for Individual Singularities

➤ We know that $GH = -1$; Gain = 0 dB, Phase = -180°

$$\begin{aligned} C.E \Rightarrow 1 + GH &= 0 \\ GH &= -1 \\ |GH| &= 1 \rightarrow \\ 20 \log \frac{|GH|}{|G|H|} &= 0 \text{ dB} \end{aligned}$$

• Gain Crossover Frequency (GCF)

- There must be some frequency at which the Magnitude of $G(jw)H(jw) = 1$
- Frequency at which gain is 0dB or the magnitude plot crosses 0dB line

• Phase crossover frequency (PCF)

$$\text{Phase} = -180^\circ$$

- There must be some frequency at which the phase of $G(jw)H(jw) = -180^\circ$
- Frequency where angle is -180° or the phase plot crosses -180° line.

FREQUENCY RESPONSE

Bode Plot for Individual Singularities

- **Gain Margin:** Gain measured w.r.t 0 dB axis at PCF
 - Difference between zero and gain at PCF
- **Phase Margin:** Phase measured w.r.t -180° at GCF
 - Difference between phase and -180° at GCF
- **Stability:** GM and PM should be positive ($GCF < PCF$)
- **Marginal stability:** both GM and PM are zero or $GM = PM$ ($GCF = PCF$)
- **Unstable:** GM and PM are negative ($GCF > PCF$)

$$GM = \theta - (-)$$

$$PM = -180^\circ +$$

FREQUENCY RESPONSE

Gain Margin and Phase Margin

- **GM:**

is +ve: if the intersection of line extended from PCF intersects the Magnitude plot below 0dB line

is -ve: if the line intersects above the 0dB line

- **PM:**

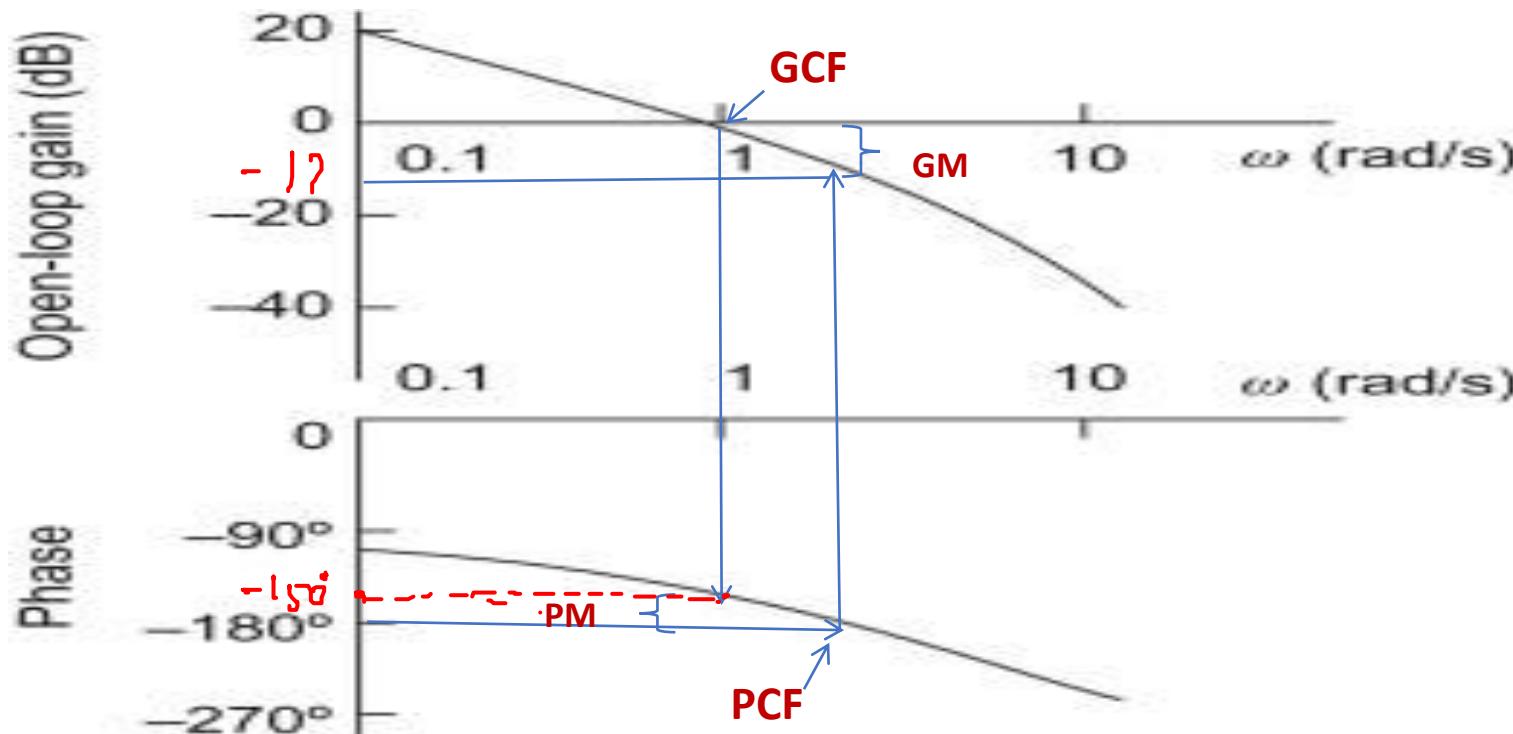
is +ve: if the intersection of line extended from GCF intersects the phase plot above -180° line

is -ve: if the line intersects, above the -180° line

FREQUENCY RESPONSE

Gain Margin and Phase Margin

- Example
- For the Bode plot shown in Figure, determine
- (a) whether the system is stable, (b) Justify the answer



$$GM = D - (Gain/\text{PCF})$$

$$\begin{aligned} GM &= 0 - (-17) \\ &= 17 \text{ dB} \end{aligned}$$

ϕ/PCF

$$\begin{aligned} PM &= 180^\circ + (\phi) \\ PM &\in \frac{180^\circ - 150^\circ}{180^\circ} \\ &= \cancel{+} 30^\circ \end{aligned}$$

Since $GM > PM$
+ve, S/m is stable

FREQUENCY RESPONSE

Gain Margin and Phase Margin

$$G(s) = \frac{200(s+10)}{s(s+5)(s+20)}$$

$$= \frac{200 \times \frac{1}{s} (\frac{1}{10}s + 1)}{s \times \frac{1}{s} (\frac{1}{5}s + 1) \times \frac{1}{20} (s + 1)} = \frac{200 (0.1s + 1)}{s (0.2s + 1) (0.05s + 1)}$$

Factor	Corner frequency	Slope contributed by each factor	Net Slope	Freq. range
$20/s$	NIL	-20dB/dec	-20dB	Start ω to $\omega=5$ rad/sec
$1/(1+0.2s)$	$W_c = 1/T = 5$	0dB till the corner frequency and -20dB/dec after corner frequency	-40 dB	$\omega=5$ rad/sec to $\omega=10$ rad/sec
$(1+0.1s)$	$W_c = 1/T = 10$	0dB till the corner frequency and +20dB/dec after corner frequency	-20 dB	$\omega=10$ rad/sec to $\omega=20$ rad/sec
$1/(1+0.05s)$	$W_c = 1/T = 20$	0dB till the corner frequency and -20dB/dec after corner frequency	-40 dB	$\omega=20$ rad/sec onwards

$$G(j\omega) = \frac{20 [0.1(j\omega + 1)]}{j\omega [0.2(j\omega + 1)] [0.05(j\omega + 1)]}$$

$$\begin{aligned} G(j\omega) &= \tan^{-1} 0.1\omega - 90^\circ \\ &\quad - \tan^{-1} 0.2\omega \\ &\quad - \tan^{-1} 0.05\omega \end{aligned}$$

FREQUENCY RESPONSE

Gain Margin and Phase Margin

$$G(s) = \frac{200(s+10)}{s(s+5)(s+20)}$$

$$A = 20 \log |20/j\omega| = 20 \log \frac{20}{\omega} = 20 \log 20 - 20 \log \omega . = 26 - 20 \log \omega .$$

$$\omega=0.1 \quad A = 26 + 20 = 46 .$$

$$\therefore \omega=1 \quad A = 26 + 0 = 26 . \quad [\text{Start from } \omega=1 \text{ with } 26 \text{ dB}] .$$

$$\underline{\underline{G(j\omega)}} = -90^\circ - \tan^{-1}(0.2\omega_1) + \tan^{-1}(0.1\omega_1) - \tan^{-1}(0.05\omega_1)$$

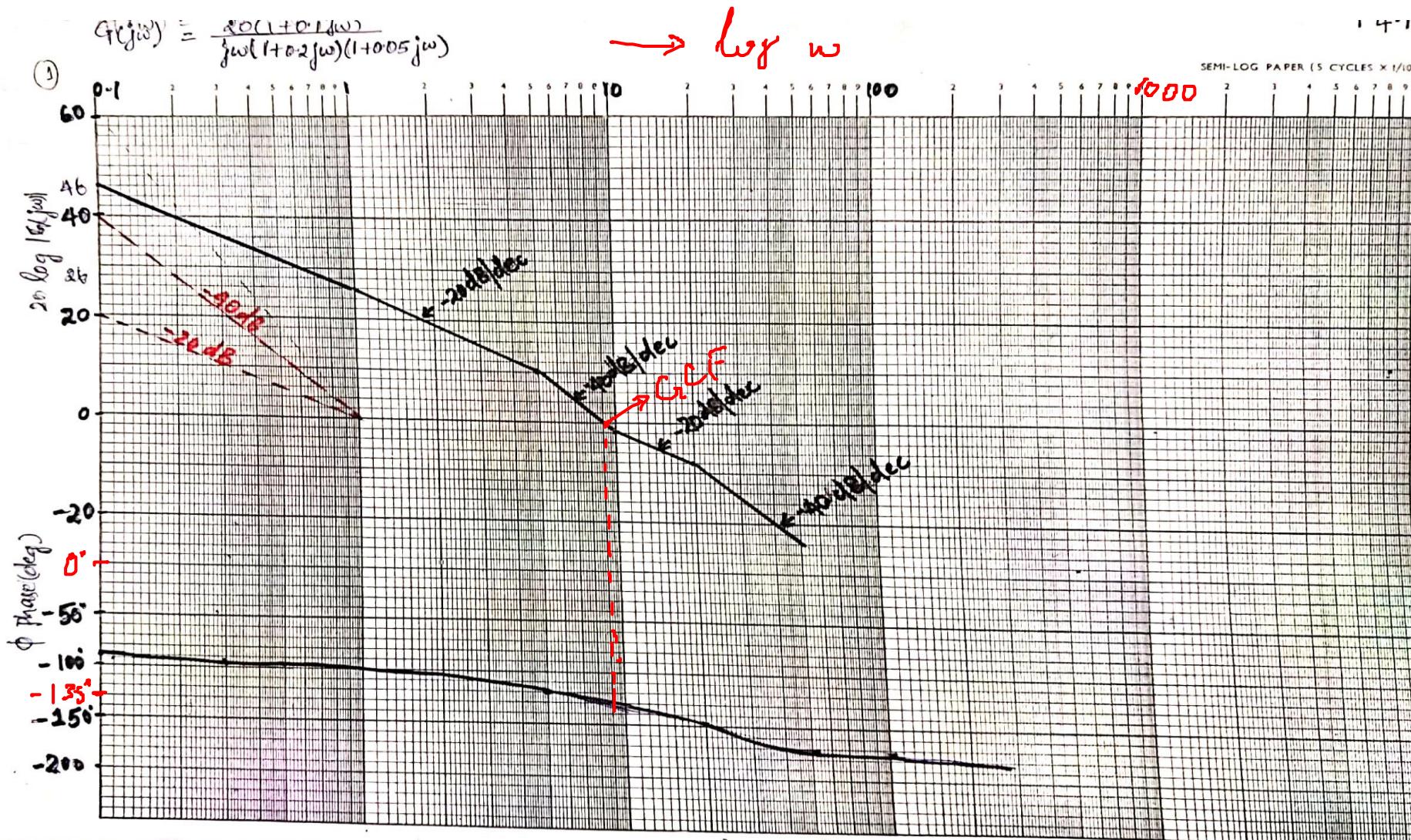
ω	0	0.1	0.2	0.4	0.8	1	5	10	20	50	100	ω
$\underline{\underline{G(j\omega)}}$	-90°	-90.86°	-91.71°	-93.43°	-96.8°	-98.4°	-122°	-135°	-147.5°	-163.79°	-171°	-180°
							-94.28	-106.2°				

FREQUENCY RESPONSE

Gain Margin and Phase Margin



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$$GCF = 9 \text{ rad/sec}$$

$$\begin{aligned} PM &= 180 + (-135) \\ &= 45^\circ \end{aligned}$$

No -180° crossing

$$GM = \infty$$

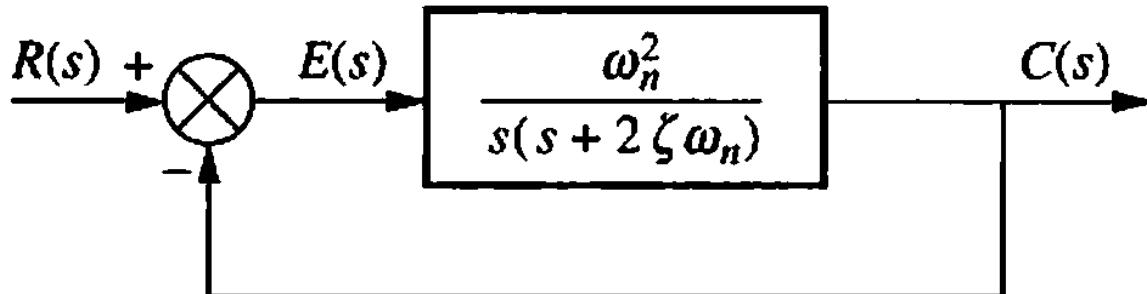
PM & GM are +ve

\therefore system is stable

FREQUENCY RESPONSE

Second order closed loop system

Consider second order closed loop system:



Closed loop transfer function

$$\frac{C(s)}{R(s)} = T(s) = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

Magnitude $\zeta_{\text{ub}} \xi = j\omega$, $|T(j\omega)| =$

$$M = |T(j\omega)| = \frac{\omega_n^2}{\sqrt{(\omega_n^2 - \omega^2)^2 + 4\xi^2\omega_n^2\omega^2}}$$

FREQUENCY RESPONSE

Second order closed loop system

Magnitude:

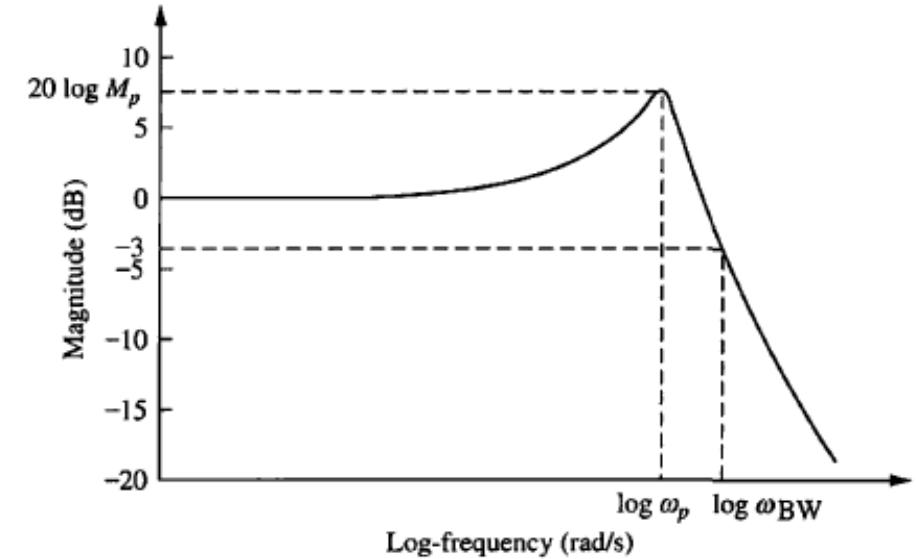
$$M = |T(j\omega)| = \frac{\omega_n^2}{\sqrt{(\omega_n^2 - \omega^2)^2 + 4\xi^2\omega_n^2\omega^2}}$$

Diff. M w.r.to ω^2 and equating to zero yields maximum value M_p

$$M_p = \frac{1}{2\xi\sqrt{1-\xi^2}}$$

Where the frequency is

$$\omega_p = \omega_n\sqrt{1-2\xi^2}$$



FREQUENCY RESPONSE

Second order closed loop system

Cutoff frequency:

The frequency at which the magnitude of the closed loop frequency response is -3dB below its zero frequency is called cutoff frequency

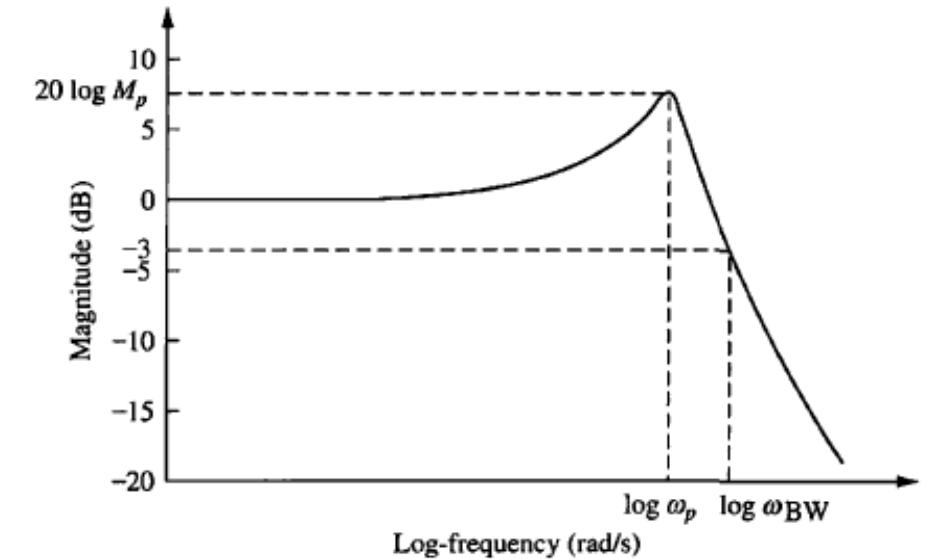
Bandwidth:

Bandwidth is the frequency at which the frequency has declined 3dB from its low frequency value.

$$M = \frac{1}{\sqrt{2}}$$
$$|G(j\omega)| = \left| \frac{1}{(1 - u^2) + j2\zeta u} \right| = \frac{1}{\sqrt{2}}$$

Solving for u

$$u = \frac{\omega_B}{\omega_n} \Rightarrow \omega_B = \omega_n \sqrt{[(1 - 2\zeta^2) + \sqrt{4\zeta^4 - 4\zeta^2 + 2}]}$$

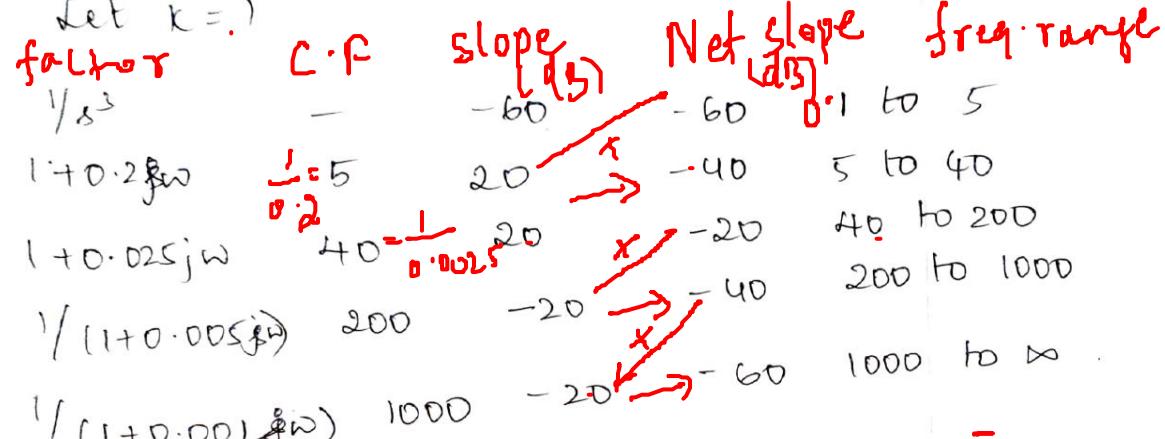


FREQUENCY RESPONSE

Example 2

$$G(s) = \frac{k(1+0.2s)(1+0.025s)}{s^3(1+0.001s)(1+0.005s)}$$

Let $k = 1$



$$\phi = -270 + \tan^{-1} 0.2\omega + \tan^{-1} 0.025\omega - \tan^{-1} 0.005\omega - \tan^{-1} 0.001\omega$$

ω	0.1	0.2	1	3	10	15	30	60	100	300	400	1000
$G(j\omega)$	-268	-260	-257	-236	-198	-183	-163	-148	-147	-172	-182	-211

$$20 \log k = 60$$

$$20 \log k = 104$$

$$1122 < k < 167880$$

Stability

$$G(j\omega) = \frac{k(1+0.2j\omega)(1+0.025j\omega)}{(j\omega)^3(1+0.001j\omega)(1+0.005j\omega)}$$

$$\frac{1}{0.2} = 5 \quad \frac{1}{0.025} = 40$$

$$\frac{1}{0.001} = 1000 \quad \frac{1}{0.005} = 200$$

$$A = 20 \log \left| \frac{1}{j\omega^3} \right| = 20 \log \frac{1}{\omega^3}$$

$$= 20 \log_{10} 1 - 3 \times 20 \log \omega$$

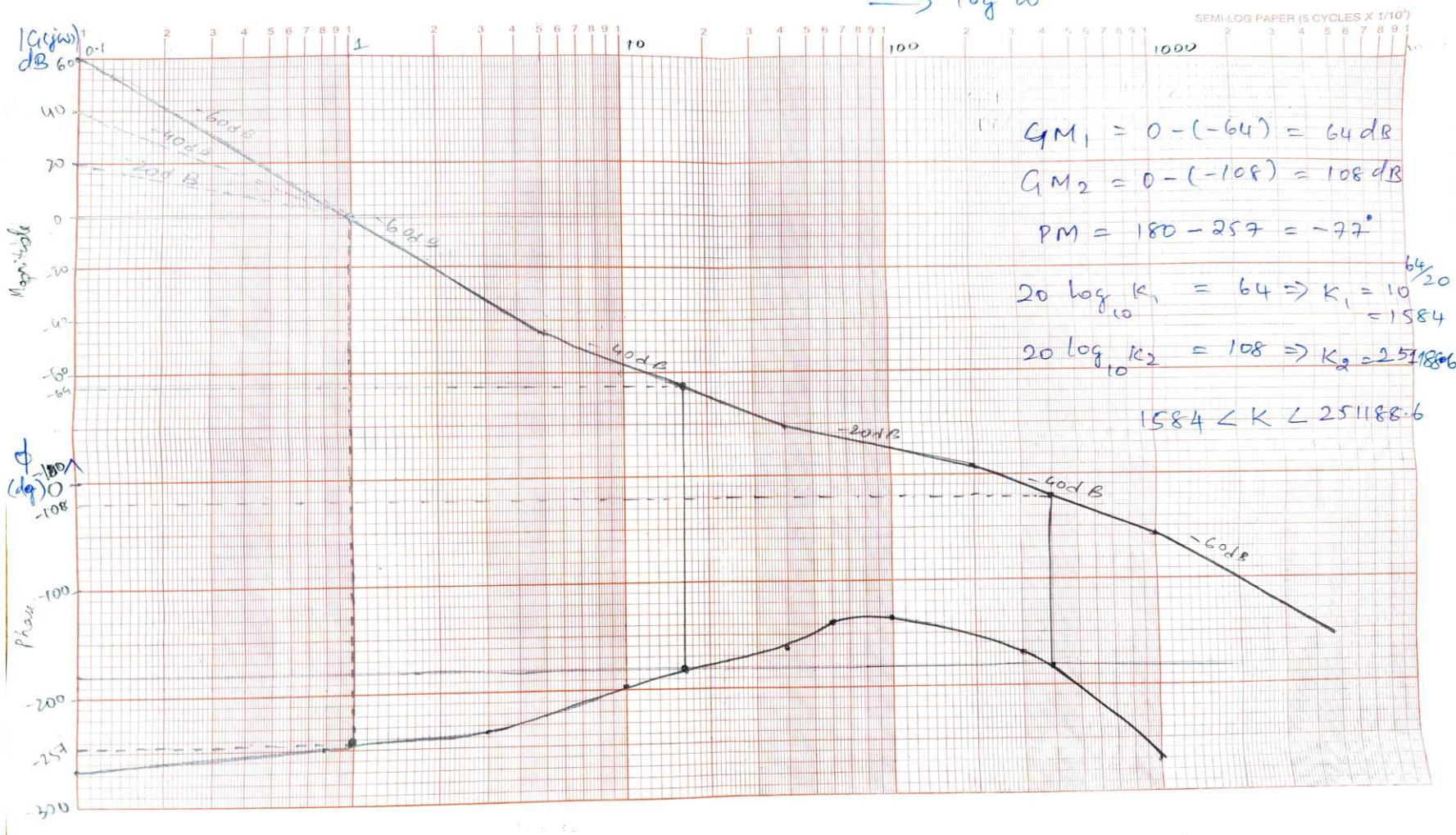
$$= -60 \log_{10} \omega$$

$$\omega = 0.1$$

$$A = -60 \text{ dB}$$

FREQUENCY RESPONSE

Example 2



FREQUENCY RESPONSE

Example 3



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$$G(s) = \frac{1}{(s+3)^3}$$

$$G(s) = \frac{1}{27(s+3)^3} = \frac{0.037}{(0.33s+1)^3}$$

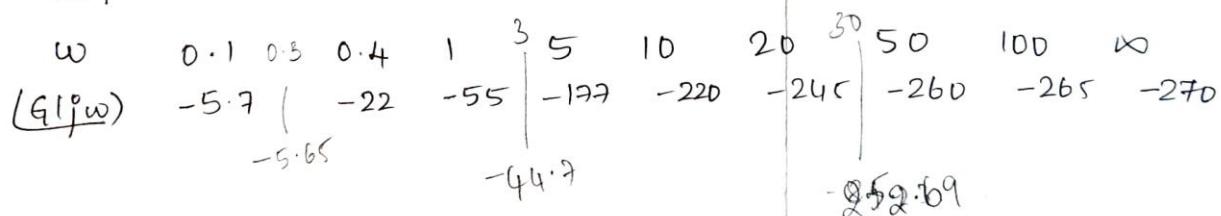
$$G(j\omega) = G(s) \Big|_{s=j\omega} = \frac{0.037}{(1+0.33j\omega)^3}$$

$$20 \log (0.037) = -28.63$$

Factor	corner freq	Contributed slope	Net slope	Freq range
0.037	none	0	0	0.1 to 3

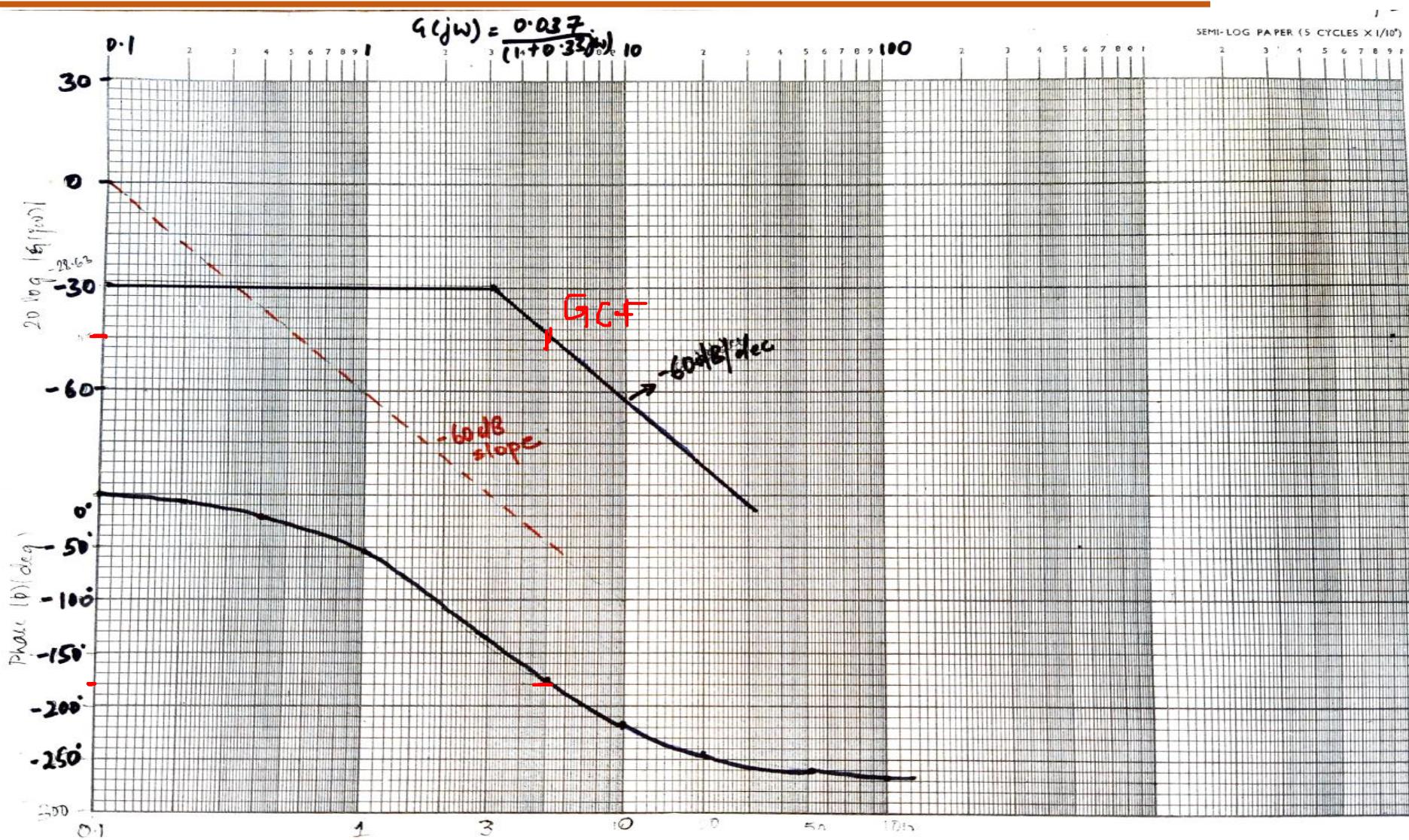
$$\frac{1}{(0.33j\omega+1)^3} \quad \frac{1}{0.33} = 3 \quad -20 \times 3 = -60 \quad -60 \quad 3 \text{ to } \infty$$

$$\underline{G(j\omega)} = -3 \tan^{-1}(0.33\omega)$$



FREQUENCY RESPONSE

Example 3



$$GM = 0 - (-45) \\ = 45$$

$$PM = \infty$$

\therefore System is stable

FREQUENCY RESPONSE

Example 4



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$$G(j\omega) = \frac{5(1+j0.1\omega)}{j\omega(1+j0.5\omega)(1+j0.6(\omega/\omega_0) + (\omega/\omega_0)^2)}$$

$$A = 20 \log \left| \frac{5}{\omega} \right| = 20 \log 5 - 20 \log \omega = 14 - 20 \log \omega.$$

Factor	corner freq	Slope contributed by each factor	Net slope	Freq range
$5/j\omega$	none	-20 dB/dec	-20	0.1 to 2
$1+j0.5j\omega$	2	-20 dB/dec	-40	2 to 10
$1+j0.1\omega$	10	20 dB/dec	-20	10 to 50
$\frac{1}{(1+j0.6(\omega/\omega_0) + (\omega/\omega_0)^2)}$	50	-40 dB/dec	-60	50 to ∞

ω	0.1	0.4	0.8	1	2	5	10	20	50	100	∞
$\angle G(j\omega)$	-92	-99	-108	-112	-125	-135	-131	-126	-109		

$$\angle G(j\omega) = -90 + \tan^{-1}(0.1\omega) - \tan^{-1}(0.5\omega) - \tan^{-1} \left(\frac{\frac{0.6\omega}{50}}{1 - \omega^2/50^2} \right)$$

$$\begin{aligned} & \tan^{-1} \left(\frac{2yu}{1-u^2} \right) \\ & - \left(\pi - \tan^{-1} \left(\frac{0.6\omega/50}{\omega^2/50^2 - 1} \right) \right) + w > 50^2 \end{aligned}$$

$$G(s) = \frac{5(1+0.1s)}{s(1+0.5s)(1+\frac{0.6s}{50} + \frac{s^2}{50^2})}$$

$\frac{1}{D_1} = 10$

$\frac{1}{0.5} = 2$

$\omega_n = 50$

$$A = 20 \log \left| \frac{5}{\omega} \right| = 20 \log \frac{5}{\omega}$$

$$\begin{aligned} \text{At } \omega = 0.1, \quad A &= 14 - 20 \log_{10} 0.1 \\ &= 34 \text{ dB} \end{aligned}$$

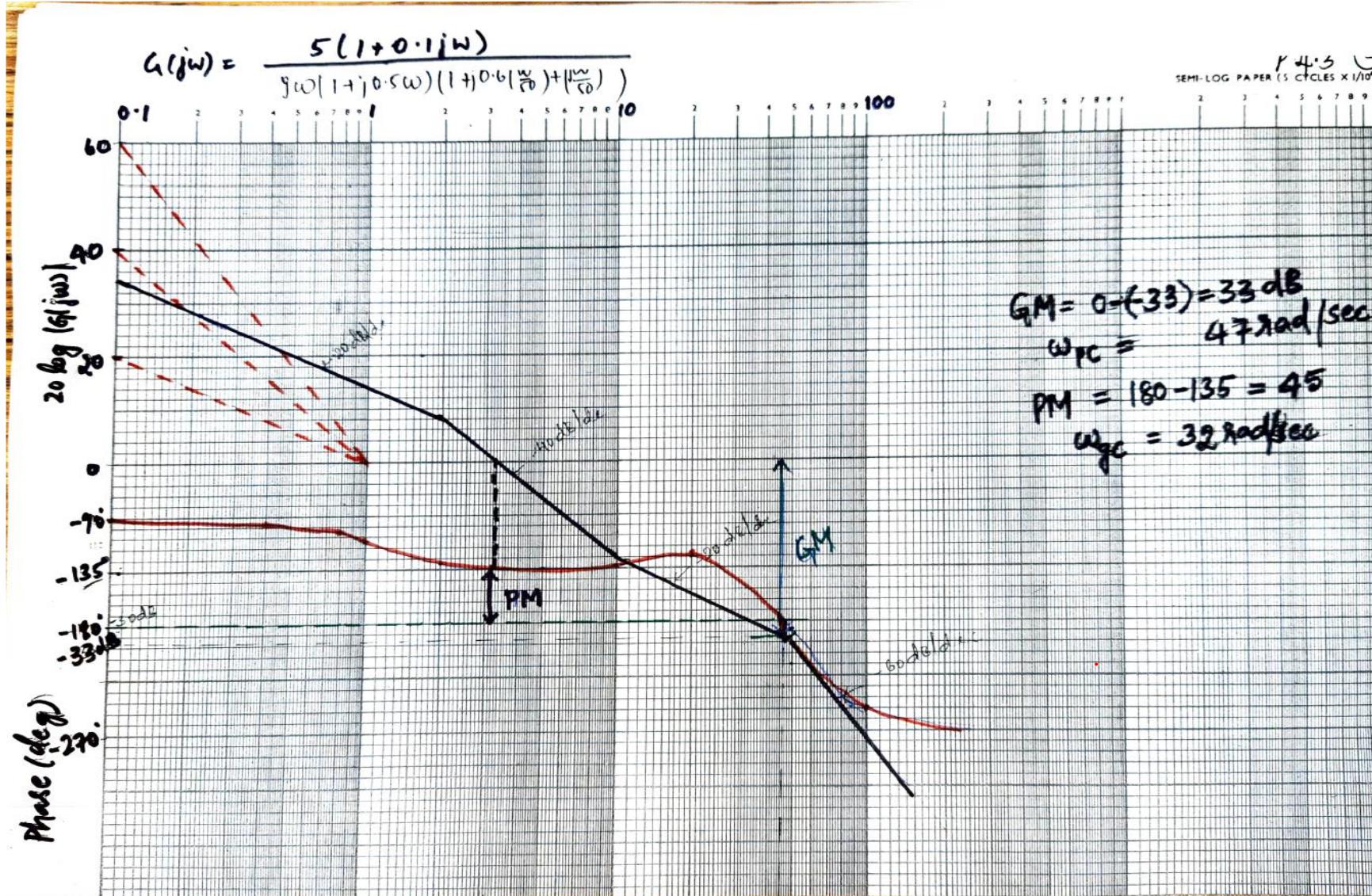
$$\begin{aligned} \text{error} &= -10 \log(4\%) \\ &= -10 \log(4 \times 0.3^2) \\ &= 4.4 \text{ dB} \end{aligned}$$

FREQUENCY RESPONSE

Example 4



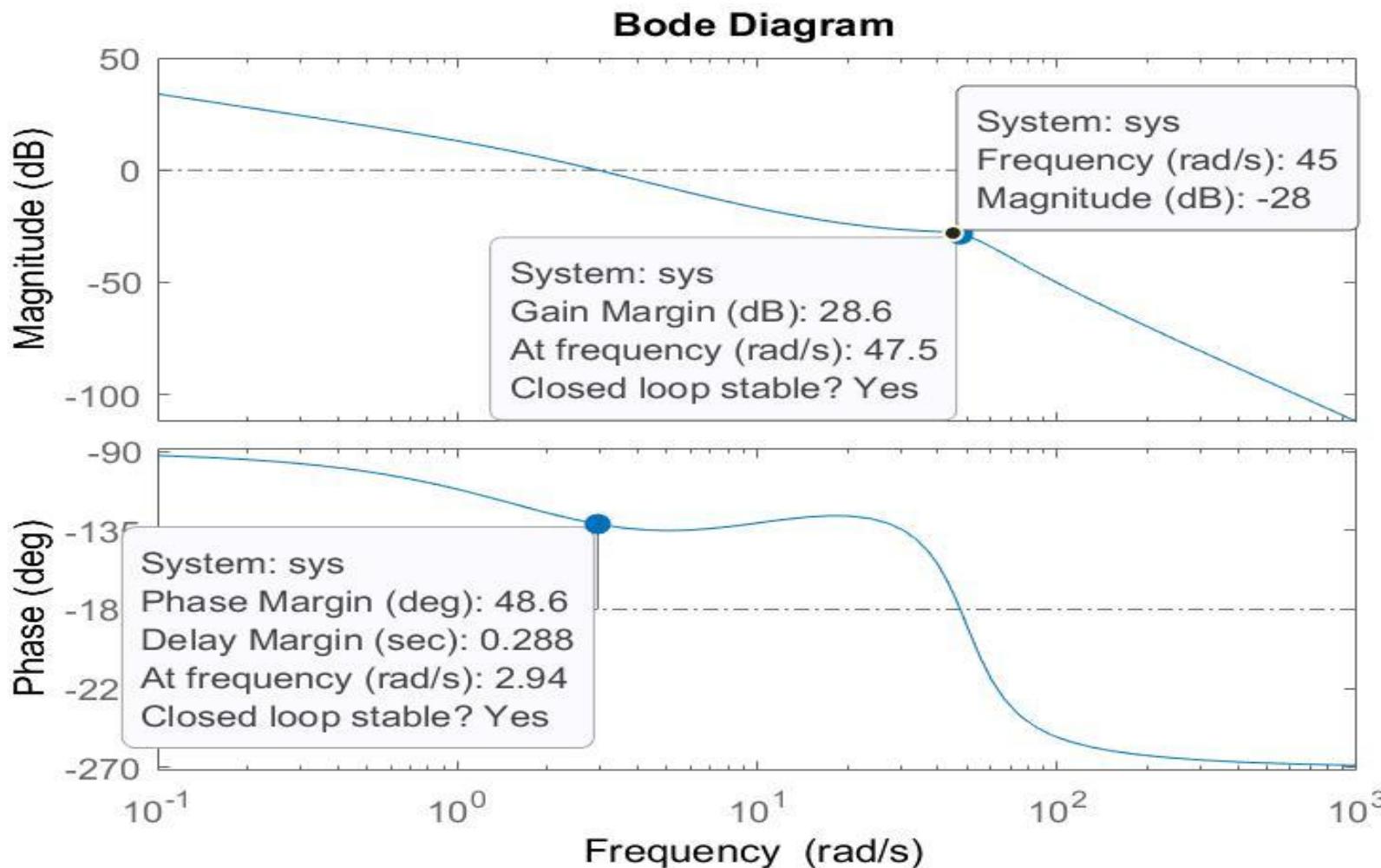
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$$\begin{aligned}
 GM &= 33 \text{ dB} \\
 &\quad \text{per rev} \\
 &= 33 - 4 \\
 &= 28.6 \text{ dB}
 \end{aligned}$$

FREQUENCY RESPONSE

Example 4



FREQUENCY RESPONSE

Example 5

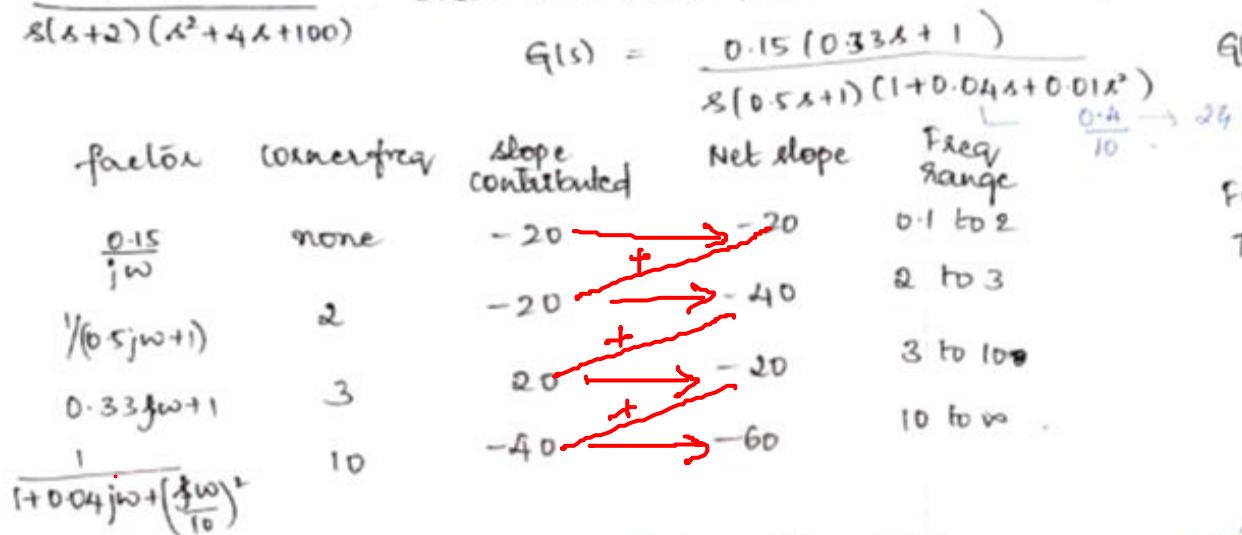
$$\omega_n^2 = 100 \Rightarrow \omega_n = 10$$

$$2\zeta\omega_n = 4 \Rightarrow \zeta = \frac{2}{10}$$



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The open loop transfer function of an unity feedback system is given by $G(s) = \frac{10(s+3)}{s(s+2)(s^2+4s+100)}$. Draw the Bode plot and hence find the gain margin & phase margin.



ω	0.1	1	5	10	20	100
$(G(j\omega))$	-91.2	-100	-114	-126	-258	-270

$$(G(j\omega)) = -90 - \tan^{-1}(0.5\omega) + \tan^{-1}(0.33\omega) - \tan^{-1}\left(\frac{0.04\omega}{0.01\omega^2 + 1}\right)$$

$$A = 20 \log\left(\frac{0.15}{\omega}\right) = 20 \log 0.15 - 20 \log 0.1 = 3.52$$

$$20 \log 0.15 - 20 \log 1 = -16.478$$

$$A = 20 \log \left| \frac{0.15}{\omega} \right|$$

$$\begin{aligned} -0.01\omega^2 + 1 &< 0 \\ 0.01\omega^2 &> 1 \\ \omega^2 &> 1/0.01 \\ \omega &> 10 \end{aligned}$$

at $\omega = 0.1$, $A = 3.52 \text{ dB}$

$$= 20 \log 0.15$$

$$= -20 \log \frac{10}{\omega}$$

$$= 3.52 \text{ dB}$$

$$\begin{aligned} \text{For quadratic factor} \\ \text{Total error at corner freq} \\ -10 \log (4\zeta^2) &= -10 \log (4 \cdot 0.2^2) \\ &= -7.95 = 8 \\ \therefore GM &= 40 - 8 = 32 \text{ dB} \end{aligned}$$

$$G(j\omega) = \frac{0.15(0.33j\omega + 1)}{j\omega(0.5j\omega + 1)(1 + 0.04j\omega + 0.01\omega^2)}$$

$$(1 - 0.01\omega^2) + 0.04\omega j$$

$$G(s) = 10(s+3)$$

$$\frac{s(s+2)}{(s^2 + 4s + 100)}$$

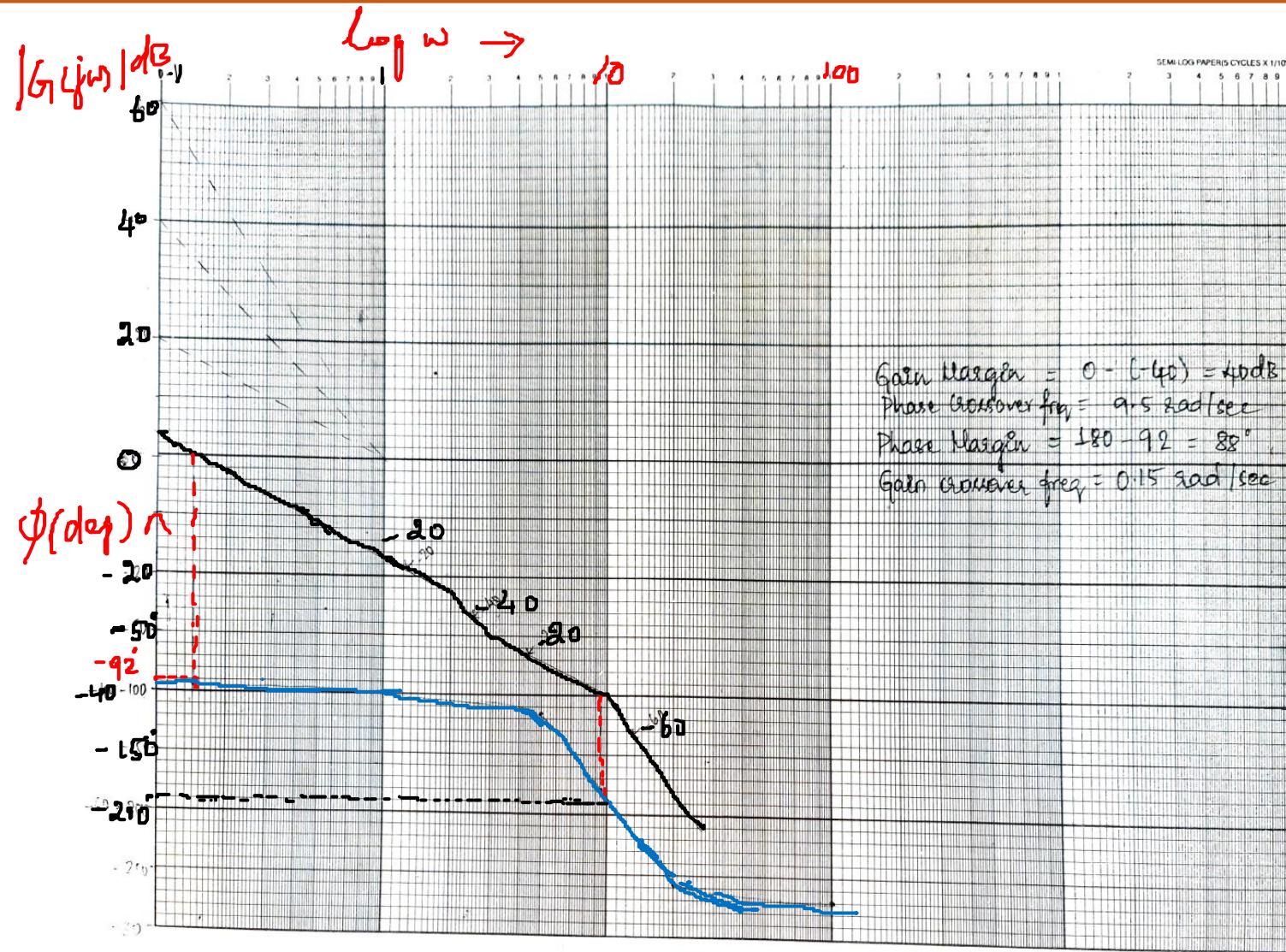
$$\frac{10 \times 3 \left(\frac{1}{3}s + 1 \right)}{s^2 + 4s + 100}$$

$$+ \frac{4}{100}s + 1$$

$$\frac{3/20(0.33s+1)}{s(0.5s+1)(0.01s^2 + 0.04s + 1)}$$

FREQUENCY RESPONSE

Example 5



$$G_{LF} = 0.1 \text{ rad/sec}$$

$$P_{CF} = 9 \text{ rad/sec}$$

$$GM = 0 - (-40) = 40 \text{ dB}$$

$$\text{Error} = 8 \text{ dB}$$

$$GM = 40 - 8 = 32 \text{ dB}$$

$$PM = 180 - 92 = 88^\circ$$

FREQUENCY RESPONSE

Example 6 – H.W

Draw the bode plot for the system $G(s) = \frac{10(s+1)}{(s+2)(s+5)}$

FREQUENCY RESPONSE

Example 7 – Manual calculations

Find the PCF and GM for the system with $G(s) = \frac{10}{s(1+0.5s)(1+0.1s)}$

Sol. To find PCF, (ω_{PC})

$$\boxed{G(j\omega)} = -180^\circ \quad |_{\omega=\omega_{PC}}$$

$$-90^\circ - \tan^{-1} 0.5\omega - \tan^{-1} 0.1\omega = -180^\circ$$

$$-\tan^{-1} 0.5\omega_{PC} - \tan^{-1} 0.1\omega_{PC} = -90^\circ$$

$$\tan^{-1} 0.5\omega_{PC} + \tan^{-1} 0.1\omega_{PC} = 90^\circ$$

$$\tan^{-1} \frac{0.5\omega_{PC} + 0.1\omega_{PL}}{1 - (0.5\omega_{PC} \cdot 0.1\omega_{PL})} = 90^\circ$$

$$G(j\omega) = \frac{10}{j\omega (1+0.5j\omega) (1+0.1j\omega)}$$

$$\frac{0.5\omega_{PC}}{1 - 0.05\omega_{PC}^2} = \infty = \frac{1}{0}$$

$$1 - 0.05\omega_{PC}^2 = 0$$

$$\omega_{PC} = 2\sqrt{5} = 4.47 \text{ rad/sec}$$

$$GM = \frac{1}{|G(j\omega)H(j\omega)|} \Big|_{\omega=\omega_{PC}}$$

GM in dB

$$M = -20 \log_{10} |G(j\omega)H(j\omega)| \Big|_{\omega=\omega_{PL}}$$

FREQUENCY RESPONSE

Example 7 – Manual calculations

$$G_M \text{ dB} = -20 \log_{10} \left(\frac{10}{\omega \sqrt{1 + 0.5 \omega^2} \sqrt{1 + (0.1 \omega)^2}} \right) \quad | \omega = \omega_p C$$
$$= 1.57 \text{ dB}$$

FREQUENCY RESPONSE

Example 8

Find the GCF, PCF, PM and GM for the system with $G(s) = \frac{10}{(s+20)}$

Sol: $G(s) = \frac{10/z_0}{1 + s/z_0} = \frac{0.5}{1 + s/20}$ $G \cdot M = \frac{1}{M} \Big|_{\omega = \omega_{PC}}$, $PM = 180^\circ + \phi_{\omega=\omega_{GC}}$

$$G(j\omega) = \frac{0.5}{1 + j\omega/20}$$

To find ω_{GC} ,

$$\sqrt{\frac{0.5}{1 + \frac{\omega^2}{400}}} \Bigg|_{\omega=\omega_{GC}} = 1$$

$$\Rightarrow 0.5 = \sqrt{1 + \frac{\omega_{GC}^2}{400}}$$

$\omega_{GC} = 17.32j \Rightarrow \therefore$ it is imaginary
GCF does not exist

To find ω_{PC} , $\phi = -\tan^{-1} \omega/20$ $\left. \begin{array}{l} \omega = \omega_{PC} = -180^\circ \\ \omega_{PC} = 0 \end{array} \right| \quad \left. \begin{array}{l} \therefore PM \text{ is } \infty \\ G_M = \frac{1}{M} \Big|_{\omega = \omega_{PL}} = \frac{1}{0.5} = 2 \end{array} \right| \quad \left. \begin{array}{l} 4M_{dB} = -20 \log 2 \\ = 6 dB \end{array} \right.$

BODE PLOT

Reverse Bode Analysis

Karpagavalli S.

Department of Electronics and Communication Engineering

- Finding the transfer function for the given Bode plot
- Steps:
 1. Initial slope of magnitude plot represents poles or zeros at the origin, if slope is
 - $-20\text{dB} \Rightarrow 1$ pole at origin
 - $-40\text{dB} \Rightarrow 2$ poles at origin
 - $0\text{dB} \Rightarrow$ No pole
 - $20\text{dB} \Rightarrow 1$ zero at origin
 - $40\text{ dB} \Rightarrow 2$ zeros at origin

Step 2: Observe the shift in the magnitude plot at corner frequency which represents $20\log K$, from which K can be determined

$$20 \log_{10} |G(j\omega)|_{at \omega=\omega_1} = 20 \log_{10}(X)$$

Where X can be K or $\frac{K}{\omega}$ or $K\omega$ or $\frac{K}{\omega^2}$ or $K\omega^2$ and so on, depends on the initial slope

Step 3: Identify the corner frequencies

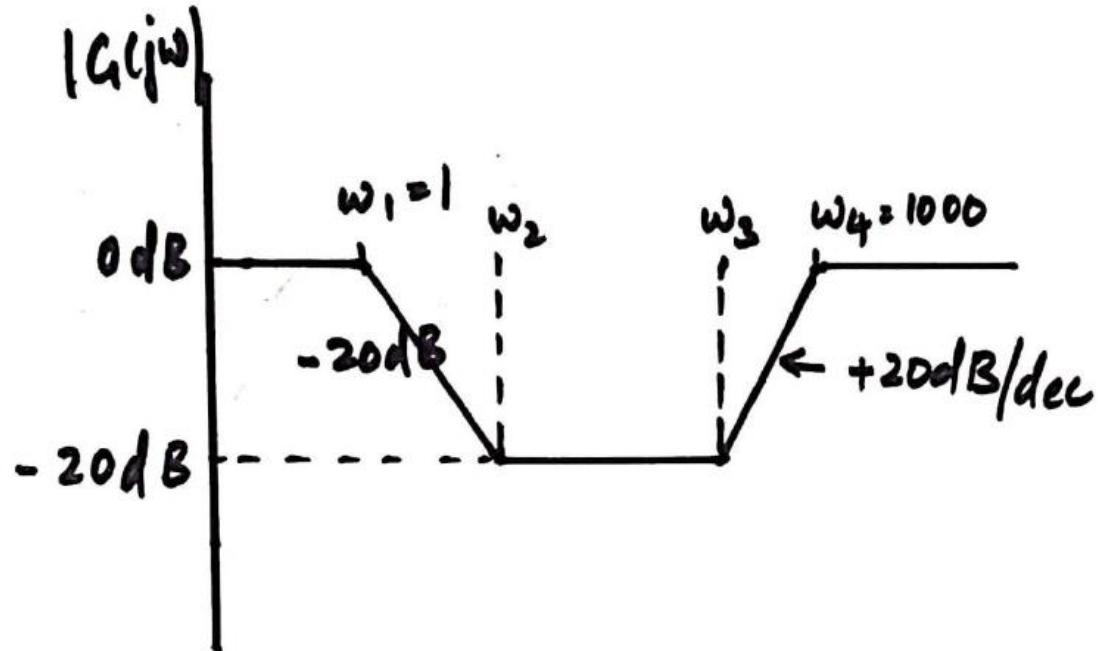
Step 4: If changes in slope is -20dB/decade, then the factor is a simple pole $1/(1+\tau s)$

Step 5: If changes in slope is 20dB/decade, then the factor is a simple zero $(1+\tau s)$, where $\tau = 1/\omega$

FREQUENCY RESPONSE

Reverse Bode Analysis – Example 1

Determine the transfer function for the given bode plot



$$Slope = \frac{y_2 - y_1}{\log(\omega_2) - \log(\omega_1)}$$

FREQUENCY RESPONSE

Reverse Bode Analysis – Example 1

- $20 \log_{10} |G(j\omega)| = 20 \log_{10} K - 20 \log_{10} \omega$

- $0dB = 20 \log_{10} K \Rightarrow K = 1$

- Guess the factors , $G(s) = K \frac{(1+s/\omega_2)(1+s/\omega_3)}{(1+s/\omega_1)(1+s/\omega_4)}$

- Where ω_1 and ω_4 are known but ω_2 and ω_3 are unknown

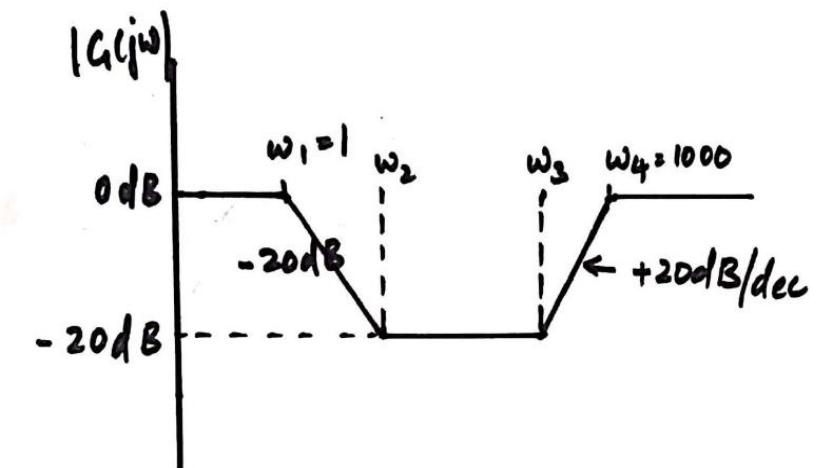
- So we need to determine ω_2 and ω_3

- Slope = $\frac{y_2 - y_1}{\log(\omega_2) - \log(\omega_1)} \Rightarrow -20 = \frac{-20 - 0}{\log_{10} \omega_2 - \log_{10} 1}$

- $\omega_2 = 10$, similarly, $\omega_3 = 100$

$$\log_{10} \frac{\omega_3}{\omega_2} = \frac{20}{20} = 1 \Rightarrow \omega_3 = 10^1 = 10$$

$$\begin{aligned} -20dB &\rightarrow \frac{1}{1 + j\omega/\omega_1} \\ +20dB &\rightarrow 1 + j\omega/\omega_2 \\ 20dB &\rightarrow 1 + j\omega/\omega_3 \\ -20dB &\rightarrow \frac{1}{1 + j\omega/\omega_4} \end{aligned}$$



FREQUENCY RESPONSE

Reverse Bode Analysis – Example 1

- $G(s) = K \frac{(1+s/10)(1+s/100)}{(1+s/1)(1+s/1000)}$

- $G(s) = \frac{(1+0.1s)(1+0.01s)}{(1+s)(1+0.001s)}$

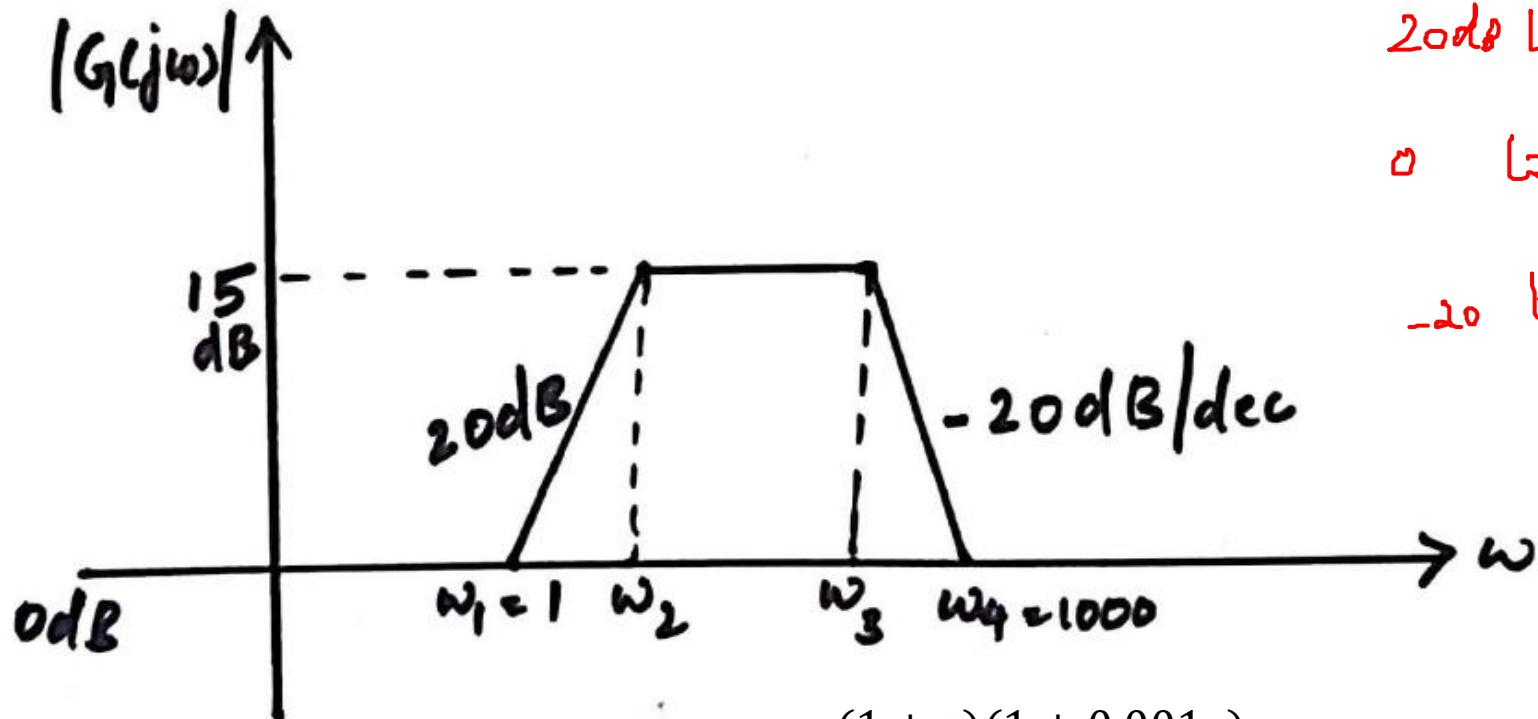
FREQUENCY RESPONSE

Reverse Bode Analysis – Example 2



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Determine the transfer function for the given bode plot



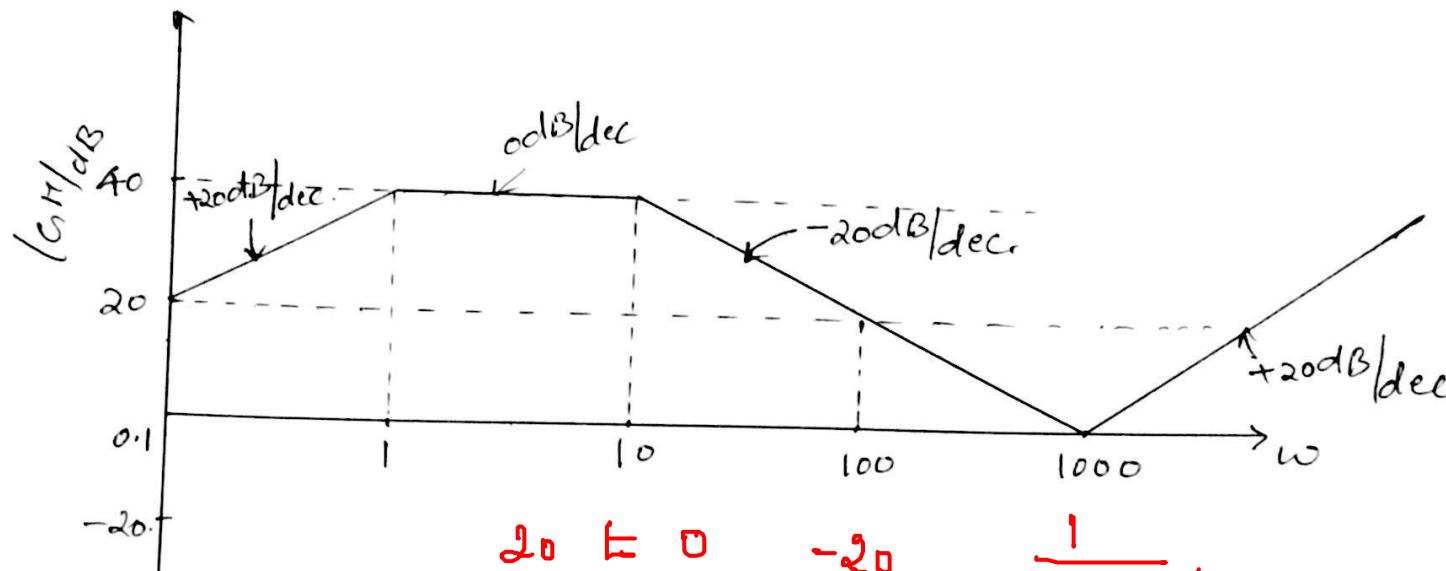
$$G(s) = \frac{(1+s)(1+0.001s)}{(1+0.177s)(1+0.0056s)}$$

$$\begin{aligned} & 0 \leftarrow 20 \text{ dB} & 20 \text{ dB} & 1 + j\omega/\omega_1 \\ & 20 \text{ dB} \leftarrow 0 \text{ dB} & -20 \text{ dB} & \frac{1}{1 + j\omega/\omega_2} \\ & 0 \leftarrow -20 \text{ dB} & -20 \text{ dB} & \underline{\underline{1}} \\ & -20 \leftarrow 0 & 20 \text{ dB} & 1 + j\omega/\omega_3 \\ & & 1 + j\omega/\omega_4 & \frac{1}{1 + j\omega/\omega_4} \\ & 20 = \frac{15 - 0}{\log \omega_2 - \log \omega_1} & \log_{10} \omega_2 = \frac{15}{20} \\ & \log_{10} \omega_2 = \frac{15}{20} & \omega_2 = 10^{15/20} \end{aligned}$$

FREQUENCY RESPONSE

Reverse Bode Analysis – Example 3

Determine the transfer function of the system whose approximate plot is shown in figure below.



$$\begin{array}{lll} 20 \leftarrow 0 & -20 & \frac{1}{1+j\omega/\omega_1} \\ 0 \leftarrow -20 & -20 & \frac{1}{1+j\omega/\omega_2} \\ -20 \leftarrow 20 & 40 & \frac{1}{(1+j\omega/\omega_3)^2} \end{array}$$

initial slope $+20 \text{ dB}$
 $\Rightarrow 2 \text{ zero at origin}$

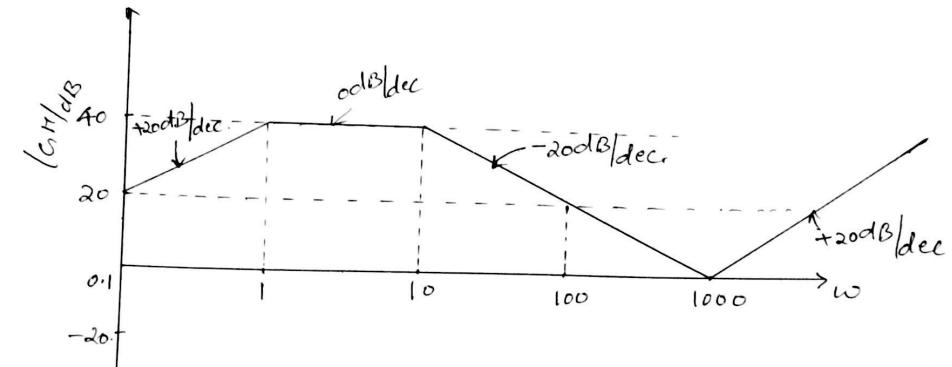
$$\begin{aligned} 40 \text{ dB} &= 20 \log_{10} \frac{k \omega_1}{\omega_1} \\ &= 20 \log_{10} k + 20 \log_{10} \frac{\omega_1}{\omega_1} \\ \log_{10} k &= 2 \\ k &= 10^2 = 100 \end{aligned}$$

$$G(s) = \frac{100 s (1 + \frac{s}{1000})^2}{(1 + \frac{s}{\omega_1})(1 + \frac{s}{\omega_2})}$$

FREQUENCY RESPONSE

Reverse Bode Analysis – Example 3

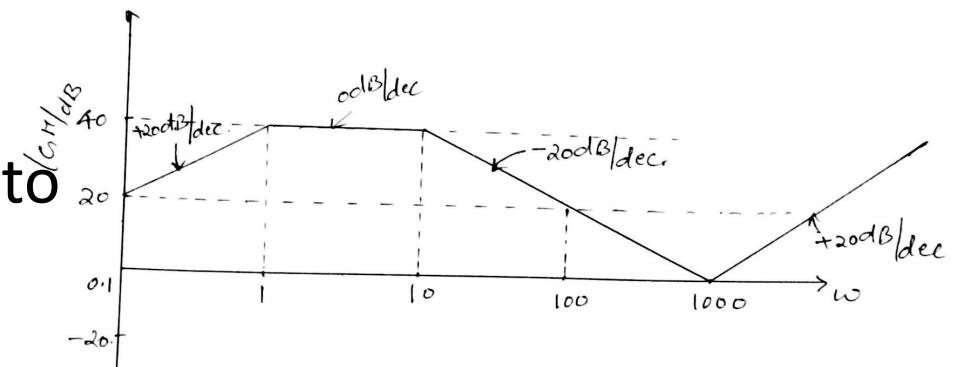
- Initial slope is +20dB/dec indicating a simple zero at origin
- This line should have crossed zero dB line at $\omega=1$ but at $\omega=1$ gain is 40dB
- This indicates a shift of 40dB due to constant
- $20 \log_{10}|G(j\omega)| = 20 \log_{10}(X)$
- \Rightarrow magnitude at $\omega_1 = 20 \log_{10} K \omega_1$
- $\Rightarrow 40 = 20 \log_{10} k + 20 \log_{10} \omega_1$
 $\Rightarrow 20 \log k = 40$ or $k=100$
- Corner frequencies: 1,10,1000



FREQUENCY RESPONSE

Reverse Bode Analysis – Example 3

- Corner frequencies: 1,10,1000
- At $\omega=1$, slope changes from 20dB/dec to 0dB/dec indicating that there is a pole with -20dB/dec line from corner frequency at $\omega=1$ hence canceling the previous slope
- At $\omega=10$, slope changes from 0dB/dec to -20dB/dec to indicating that there is a pole with -20dB/dec line from corner frequency at $\omega=10$
- At $\omega=1000$, slope changes from -20dB/dec to +20dB/dec indicating that there are two zeros with +20dB/dec line from this corner frequency(resulting in +40 dB/dec line) which gives a slope of +20 dB/dec

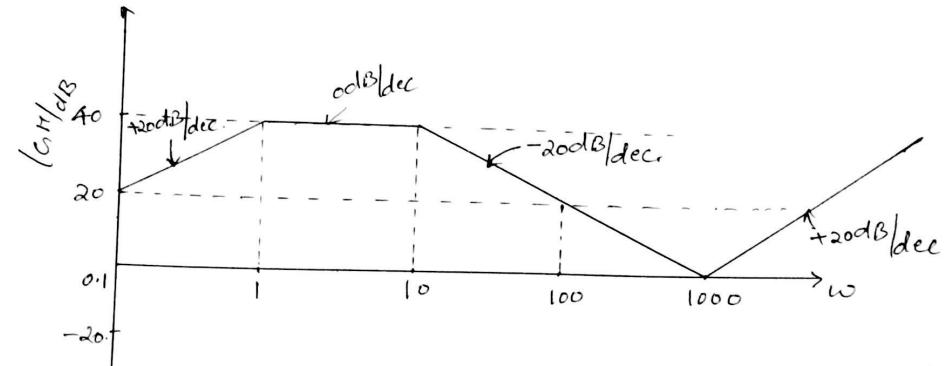


FREQUENCY RESPONSE

Reverse Bode Analysis – Example 3

- Hence the open loop transfer function would be

$$G(s)H(s) = \frac{100s(1 + 0.001s)^2}{(1 + s)(1 + 0.1s)}$$





THANK YOU

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