

Fort Calhoun Station 9610 Power Lane Blair, NE 68008

> LIC-10-0008 February 10, 2010

U. S. Nuclear Regulatory Commission Attn: Document Control Desk Washington, DC 20555-0001

Reference: Docket No. 50-285

Subject:

Licensee Event Report 2009-005 Revision 0 for the Fort Calhoun

Station

Please find attached Licensee Event Report 2009-005, Revision 0, dated February 10, 2010. This report is being submitted pursuant to 10CFR50.73(a)(2)(i)(B). There are no commitments contained in this submittal. A revision to this LER will be submitted following completion and approval of the root cause analysis.

If you should have any questions, please contact me.

Sincerel

Jeffrey A. Reinhart Site Vice President

JAR / epm

Attachment

C: E. E. Collins, NRC Regional Administrator, Region IV

L. E. Wilkins, NRC Senior Project Manager

J. C. Kirkland, NRC Senior Resident Inspector

INPO Records Center

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NRC FORM 366 (9-2007)			U.S. NUCLEAR REGULATORYCOMMISSION						APPROVED BY OMB: NO. 3150-0104						EXPIRES: 08/31/201		
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Fort Calhoun Station										050002	285			1	1 C)F 4	
4. TITLE			Inoper	able Auxili	ary Fe	edwat	er Train	Due	e to	an Inope	rable	Injecti	on Va	alve	·		
5. EVENT DATE			6. LER NUMBER			7. REPORT DATE		DATE						FACILITIES INVOLVED			
MONTH	DAY	YEAR	YEAR	SEQUENTI AL NUMBER	REV NO	MONTH	I DAY	YEA	·R	FACILITY NA					,	05000	NUMBER
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YES (If yes, complete 15. EXPECTED SUBMISSION DATE) □ NO
ABSTRACT (Limit to 1400 spaces, i.e., approximately 15 single-spaced typewritten lines)

14. SUPPLEMENTAL REPORT EXPECTED

COMPONENT

MANU-

FACTURER

On November 1, 2009, Fort Calhoun Station began a refueling outage. The station entered mode 5 (less than 210 degrees F, refueling) on November 2, 2009. On November 6, 2009, during performance of air operated valve diagnostic testing of HCV-1107A (Steam Generator 'A' auxiliary feedwater (AFW) inlet valve), the air regulator setting was found to be 23.6 pounds per square inch gauge (psig). The regulator pressure setting of 23.6 psig is contrary to the required nominal setting of 35 psig credited in calculation FC06904, "Category 1 Air-Operated Valve (AOV) Operator Margin Analysis." (HCV-1107A is an air-to-close valve.)

CAUSE

SYSTEM

COMPONENT

15. EXPECTED

SUBMISSION

DATE

A root cause analysis (RCA) was initiated to determine the cause of the apparent failure of the valve HCV-1107A. By December 12, 2009, the causal analysis had progressed to the point where it was concluded that the valve's regulator had been inadvertently set to the wrong pressure setting during the 2006 refueling outage. As part of the detailed work instructions, the air regulator for HCV-1107A has been reset from 23.6 psig to 35 psig.

The RCA is not complete. A supplement to this LER will be made with the results of the RCA.

REPORTABLE TO EPIX

CAUSE

SYSTEM

MANU-

FACTURER

MONTH

4

REPORTABLE

TO EPIX

YEAR

2010

DAY

30

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LICENSEE EVENT REPORT (LER) CONTINUATION SHEET

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NARRATIVE

BACKGROUND

Fort Calhoun Station (FCS) is a two-loop Combustion Engineering (CE) design reactor coolant system (RCS). Each loop has one steam generator (SG) and two reactor coolant pumps (RCPs). Each SG has one main feedwater (MFW) nozzle and one auxiliary feedwater (AFW) nozzle. The MFW nozzle is the normal path for feeding the SGs.

The AFW system is provided for storage, pumping and delivery of makeup water to the SGs in order to remove decay heat if the MFW system is not available. The AFW system consists of one emergency feedwater storage tank; one safety-related motor-driven (FW-6), one safety-related turbine-driven (FW-10) AFW pump; one non-safety-related, diesel-driven AFW pump (FW-54); one non-safety-related diesel fuel oil transfer pump with a day tank; non-safety-related fuel oil piping and valves; remotely operated flow control valves; interconnecting piping to the MFW system and piping to the AFW nozzles on the SGs.

The AFW line to each SG has an isolation valve on the inside of containment (the 'A' valves) and one on the outside of containment (the 'B' valves). The HCV-1107A/B valves are the isolation valves for the 'A' SG. The HCV-1108A/B valves are the isolation valves for the 'B' SG. The AFW isolation valves are 3-inch, pneumatically operated globe valves. These valves are air to close and spring to open.

FW-54 is the startup AFW pump. FW-54 takes its suction from the condensate storage tank and discharges to the normal feedwater header. FW-54 and its associated equipment are not safety-related.

The AFW system provides a redundant means of supplying one or both SGs with feedwater. Operation of the safety-related portion of the AFW system is automatically initiated on a low SG water level or manually initiated as follows:

- Automatic initiation via an auxiliary feedwater actuation signal (AFAS).
- Automatic start signals to the safety-related pumps (FW-6 and FW-10).
- Manual initiation from the control room.
- Manual initiation from alternate shutdown panel for FW-10 and the AFW injection valves and locally for FW-6.

The system is designed to add feedwater to either or both SGs under any condition, including the loss of all electrical power along with the loss of the MFW system and the loss of the main steam piping downstream of the main steam isolation valves. The AFW system fulfills both safety-related and non-safety-related functions.

Technical Specification (TS) 2.5, "Steam and Feedwater Systems," states, in part:

- (1) Two AFW trains shall be OPERABLE when Toold is above 300 (degrees) F.
 - A. With one steam supply to the turbine driven AFW pump inoperable, restore the steam supply to OPERABLE status within 7 days and within 8 days from discovery of failure to meet the LCO.
 - B. With one AFW train inoperable for reasons other than condition A, restore the AFW train to OPERABLE status within 24 hours.
 - C. If the required action and associated completion times of condition A or B are not met, then the unit shall be placed in MODE 2 in 6 hours, in MODE 3 in the next 6 hours, and less than 300 (degrees) F without reliance on the steam generators for decay heat removal within the next 18 hours.

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NARRATIVE

EVENT DESCRIPTION

On November 1, 2009, FCS began a refueling outage. The station entered mode 5 (less than 210 degrees F, refueling) on November 2, 2009. On November 6, 2009, during performance of air operated valve diagnostic testing of HCV-1107A, the air regulator setting was found to be 23.6 pounds per square inch gauge (psig). The regulator pressure setting of 23.6 psig is contrary to the required nominal setting of 35 psig credited in calculation FC06904, "Category 1 Air-Operated Valve (AOV) Operator Margin Analysis." (HCV-1107A is an air-to-close valve.) A root cause analysis was initiated to determine the cause of the apparent failure of the valve. By December 12, 2009, the causal analysis had progressed to the point where it was concluded that the valve's regulator had been inadvertently set to the wrong pressure setting during a previous refueling outage.

HCV-1107A has a safety-related function to shut to isolate AFW flow to a SG as well as to open to allow AFW flow to a SG. With the valve regulator set to 23.6 psig, HCV-1107A was unable to perform its design safety function for longer than the TS allowed outage time.

Based on the root cause analysis, the date of discovery for this report was determined to be December 12, 2009, instead of the date of the test on November 6, 2009. This event is being reported pursuant to 10 CFR 50.73(a)(2)(i)(B).

CONCLUSION

In the fall of 2006 FCS conducted a SG replacement refueling outage. On September 11, 2006, work order (WO) 218003/01 paperwork was issued out to remove and install the valve operator for HCV-1107A per the applicable portions of procedure PE-RR-VX-0414S, "Inspection and Repair of Safety Related Fisher 'HSC' Valves." An "As Found" flowscan of HCV-1107A was performed on September 11, 2006. This identified that the input pressure was adjusted slightly greater than 35 psig. The stem coupling and regulator from HCV-1107A were removed on September 12, 2006, for storage. An as found diagnostic test (Flowscan) was performed on HCV-1107A and its actuator. (Flowscan is a diagnostic device and methodology used to perform baseline or diagnostic testing on AOV and their actuators.) When HCV-1107A was reinstalled, the "As Left" Flowscan dated October 27, 2006, identified that the input pressure to the flow scanner was adjusted to slightly greater than 23 psig.

In the period of time between the flowscan of September 11, 2006, and the flowscan of October 27, 2006, the air regulator for HCV-1107A setting was reset to 23.6 psig instead of 35 psig as specified. There is no record of any activity during those dates that would have changed the regulator setting from the required 35 psig to 23.6 psig. The plant records do not show any maintenance on the regulator for IA-HCV-1107A prior to September 11, 2006, or after November 2, 2006.

The as-left setting of the air regulator for HCV-1107A at 23.6 psig went undetected by station personnel until the performance of AOV diagnostic testing of HCV-1107A on November 6, 2009. The regulator pressure setting of 23.6 psig is contrary to the required nominal setting of 35 psig credited in calculation FC06904, "Category 1 Airoperated Valve (AOV) Operator Margin Analysis." This LER will be updated upon completion of the root cause analysis (RCA).

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NARRATIVE

CORRECTIVE ACTIONS

The RCA is not complete. A supplement to this LER will be made based on the results of the RCA.

As part of the WO's detailed work instructions, the air regulator for HCV-1107A has been reset from 23.6 psig to 35 psig. Additional corrective actions will be controlled by the corrective action system.

SAFETY SIGNIFICANCE

The safety significance of this event will be assessed in detail on completion of the root cause analysis.

SAFETY SYSTEM FUNCTIONAL FAILURE

This event does not result in a safety system functional failure in accordance with NEI-99-02.

PREVIOUS SIMILAR EVENTS

None