

Manufacturing

Metal Casting

Solidification and Cooling

Chvorinov's Rule:

$$t = C \left(\frac{V}{A} \right)^n$$

where: - t = total solidification time - V = volume of casting - A = surface area of casting - C = mold constant (depends on material and mold properties) - n = exponent (typically $n = 2$)

Modulus of Casting:

$$M = \frac{V}{A}$$

Larger modulus \rightarrow slower cooling \rightarrow larger grain size

Riser Design:

For riser to solidify last:

$$\left(\frac{V}{A} \right)_{\text{riser}} > \left(\frac{V}{A} \right)_{\text{casting}}$$

Fluidity and Filling

Fluidity: Ability of molten metal to flow and fill mold cavities

Factors affecting fluidity: - Temperature (higher \rightarrow better fluidity) - Composition (lower melting point \rightarrow better fluidity) - Surface tension - Oxide formation

Pouring Basin and Sprue:

Flow rate through sprue:

$$Q = A_2 v_2 = A_2 \sqrt{2gh}$$

where h is height of molten metal above sprue base

Shrinkage

Total Shrinkage = Liquid shrinkage + Solidification shrinkage + Solid shrinkage

Typical total shrinkage: 3-8% depending on material

Must account for shrinkage in pattern making

Metal Forming

True Stress and True Strain

True Strain:

$$\epsilon_T = \ln\left(\frac{L}{L_0}\right) = \ln(1 + \epsilon_E)$$

where ϵ_E is engineering strain

True Stress:

$$\sigma_T = \sigma_E(1 + \epsilon_E)$$

For plastic deformation (constant volume):

$$\sigma_T = \frac{F}{A} = \frac{FL}{A_0 L_0}$$

Flow Stress

Flow Curve (Power Law):

$$\bar{\sigma} = K\epsilon^n$$

where: - $\bar{\sigma}$ = flow stress (true stress) - K = strength coefficient - ϵ = true strain - n = strain hardening exponent

Average Flow Stress:

$$\bar{Y}_f = \frac{K\epsilon^n}{1+n}$$

Used to calculate forces in forming operations

Rolling

Draft:

$$d = t_0 - t_f$$

where t_0 is initial thickness, t_f is final thickness

Reduction:

$$r = \frac{d}{t_0} = \frac{t_0 - t_f}{t_0}$$

True Strain:

$$\epsilon = \ln\left(\frac{t_0}{t_f}\right)$$

Roll Force (approximate):

$$F = \bar{Y}_f w L$$

where: - \bar{Y}_f = average flow stress - w = width of strip - L = contact length $\approx \sqrt{R \cdot d}$ - R = roll radius

Roll Torque:

$$T = 0.5FL$$

Roll Power:

$$P = 2\pi NT$$

where N is rotational speed (rev/time)

Forging

Forging Force (open die, no friction):

$$F = \bar{Y}_f A_f$$

where A_f is final area

With Friction (disk approximation):

$$F = \bar{Y}_f A_f \left(1 + \frac{2\mu r}{3h} \right)$$

where: - μ = coefficient of friction - r = radius of workpiece - h = height of workpiece

Extrusion

Extrusion Ratio:

$$r_x = \frac{A_0}{A_f}$$

where A_0 is initial billet area, A_f is final extrudate area

True Strain:

$$\epsilon = \ln(r_x)$$

Extrusion Force (Johnson Formula):

$$F = A_0 \bar{Y}_f [a + b \ln(r_x)]$$

where: - $a = 0.8$ (typical) - $b = 1.2$ to 1.5 (depends on friction and die angle)

Ram Pressure:

$$p = \frac{F}{A_0}$$

Maximum Extrusion Ratio:

Limited by: - Material strength - Press capacity - Buckling of billet

Wire and Tube Drawing

Drawing Stress (ideal, no friction):

$$\sigma_d = \bar{Y}_f \ln \left(\frac{A_0}{A_f} \right)$$

With Friction:

$$\sigma_d = \bar{Y}_f \left[1 + \frac{\mu}{\tan \alpha} \right] \ln \left(\frac{A_0}{A_f} \right)$$

where α is die semi-angle

Drawing Force:

$$F = \sigma_d A_f$$

Drawing Power:

$$P = Fv$$

where v is drawing velocity

Maximum Reduction per Pass:

Limited by tensile strength of material:

$$\sigma_d \leq \sigma_{UTS}$$

Sheet Metal Working

Bend Allowance:

$$L_b = \alpha(R + kt)$$

where: - α = bend angle (radians) - R = bend radius - t = sheet thickness - k = factor (0.33 for $R < 2t$, 0.5 for $R > 2t$)

Minimum Bend Radius:

$$R_{min} = \frac{t}{2} \left(\frac{100}{\%RA} - 1 \right)$$

where $\%RA$ is percent reduction in area at fracture

Bending Force:

$$F = \frac{K_{bf} TS_{ut} w^2}{D}$$

where: - K_{bf} = bending factor (depends on die geometry) - TS = tensile strength - w = width - D = die opening width

Deep Drawing:

Drawing ratio:

$$DR = \frac{D_0}{D_p}$$

where D_0 is blank diameter, D_p is punch diameter

Maximum $DR \approx 2.0$ for single draw

Limiting Drawing Ratio (LDR):

$$LDR = \frac{D_{0,max}}{D_p}$$

Drawing Force:

$$F = \pi D_p t \bar{Y}_f (DR - 0.7)$$

Machining

Cutting Speed, Feed, and Depth of Cut

Cutting Speed:

$$v = \frac{\pi D n}{1000}$$

where: - v = cutting speed (m/min) - D = workpiece diameter (mm) - n = rotational speed (rpm)

Feed:

$$f = n \cdot f_r$$

where f_r is feed per revolution (mm/rev)

Material Removal Rate (MRR):

$$MRR = v \cdot f \cdot d$$

where d is depth of cut

For turning:

$$MRR = \frac{\pi D n f_r d}{1000}$$

Cutting Forces and Power

Cutting Force:

$$F_c = K_s \cdot A_c$$

where: - K_s = specific cutting energy (material property) - A_c = cross-sectional area of cut = $f \times d$

Power:

$$P_c = F_c \cdot v$$

Specific Cutting Energy:

Varies with material: - Aluminum: 0.4-1.1 GPa - Steel: 2.7-9.3 GPa - Titanium: 3.0-4.1 GPa

Tool Life

Taylor Tool Life Equation:

$$vT^n = C$$

or

$$T = \frac{C}{v^{1/n}}$$

where: - T = tool life (min) - v = cutting speed (m/min) - n = exponent (typically 0.1-0.5, 0.125 for HSS, 0.25-0.4 for carbide) - C = constant (depends on material, tool, conditions)

Extended Tool Life Equation:

$$vT^n f^m d^p = C$$

Cost per Part:

Optimal cutting speed minimizes:

$$C_{part} = C_{machine} t_m + \frac{C_{tool} + C_{change}}{n_{parts}}$$

where t_m is machining time

Turning

Machining Time:

$$t_m = \frac{L}{f_r n} = \frac{L}{f_r} \cdot \frac{1000}{\pi D n}$$

where L is length of cut

For facing operation:

$$t_m = \frac{r}{f_r n}$$

where r is radius

Milling

Cutting Speed:

$$v = \frac{\pi D n}{1000}$$

where D is cutter diameter

Feed per Tooth:

$$f_t = \frac{f}{n \cdot N_t}$$

where: - f = table feed rate (mm/min) - N_t = number of teeth on cutter

Material Removal Rate:

$$MRR = w \cdot d \cdot f$$

where w is width of cut

Machining Time:

$$t_m = \frac{L + L_a}{f}$$

where L_a is approach distance

Drilling

Feed:

$$f = n f_r$$

where f_r is feed per revolution

Material Removal Rate:

$$MRR = \frac{\pi D^2}{4} \cdot f$$

Drilling Time:

$$t = \frac{L + A}{f_r n}$$

where A is approach allowance (typically $A = D/(2 \tan \theta)$ for drill point angle 2θ)

Torque:

$$T = \frac{1}{2} F_c \cdot \frac{D}{2}$$

Power:

$$P = \frac{2\pi n T}{60}$$

Surface Finish and Metrology

Surface Roughness

Average Roughness (R_a):

$$R_a = \frac{1}{L} \int_0^L |y(x)| dx$$

Arithmetic average of absolute deviations from mean line

Root Mean Square Roughness (R_q):

$$R_q = \sqrt{\frac{1}{L} \int_0^L y^2(x) dx}$$

Maximum Peak-to-Valley Height (R_t):

Distance between highest peak and lowest valley

Theoretical Surface Roughness (turning, shaping):

$$R_t = \frac{f^2}{8R_n}$$

where: - f = feed - R_n = tool nose radius

Geometric Dimensioning and Tolerancing (GD&T)

Fundamental Tolerance Equation:

$$\text{Tolerance} = \text{Upper Limit} - \text{Lower Limit}$$

Bilateral Tolerance:

$$50.0 \pm 0.1 \text{ mm}$$

Unilateral Tolerance:

$$50.0_0^{+0.2} \text{ mm}$$

Fits:

- Clearance fit: Minimum hole size > Maximum shaft size
- Interference fit: Maximum hole size < Minimum shaft size
- Transition fit: Can be either clearance or interference

Standard Tolerance Grades (IT):

IT01 to IT18, where lower numbers indicate tighter tolerances

Non-Traditional Machining

Electrical Discharge Machining (EDM)

Material Removal Rate:

$$MRR = K_m \cdot I \cdot V$$

where: - I = discharge current - V = gap voltage - K_m = material removal constant

Advantages: Can machine hard materials, complex shapes

Electrochemical Machining (ECM)

Material Removal Rate (Faraday's Law):

$$MRR = \frac{CIA}{nF\rho}$$

where: - C = current efficiency - I = current - A = atomic weight - n = valence - F = Faraday's constant (96,485 C/mol) - ρ = density

Laser Beam Machining (LBM)

Energy Density:

$$E_d = \frac{P}{A}$$

where P is laser power and A is spot area

High energy density → vaporization of material

Additive Manufacturing (3D Printing)

Build Time Estimation

Layer-by-Layer Build:

$$t = \frac{h}{v_b}$$

where: - h = total build height - v_b = build rate (height/time)

Material Usage:

$$m = V \cdot \rho$$

where V is part volume and ρ is material density

Common AM Processes

- Fused Deposition Modeling (FDM) - Stereolithography (SLA) - Selective Laser Sintering (SLS) - Electron Beam Melting (EBM) - Binder Jetting

Heat Treatment

Time-Temperature Transformation

Cooling Rate:

$$CR = \frac{\Delta T}{\Delta t}$$

Different cooling rates produce different microstructures: - Slow cool: Pearlite - Medium cool: Bainite - Fast cool (quench): Martensite

Hardness After Heat Treatment

Jominy End-Quench Test:

Measures hardenability by cooling rate

Distance from quenched end correlates with cooling rate

Tempering:

Reduces hardness and increases toughness

Temperature and time determine final properties

TRIBOLOGY

Friction

Coulomb (Dry) Friction

Friction Force:

$$F_f = \mu N$$

where: - μ = coefficient of friction - N = normal force

Static Friction:

$$F_s \leq \mu_s N$$

Kinetic Friction:

$$F_k = \mu_k N$$

Typically $\mu_k < \mu_s$

Friction Laws

Amontons' Laws: 1. Friction force proportional to normal load 2. Friction force independent of apparent contact area 3. Kinetic friction independent of sliding velocity (approximately)

Friction Mechanisms

Adhesion: Bonding at contact points, must be sheared

Plowing: Harder asperities plow through softer material

Total Friction:

$$\mu = \mu_{adhesion} + \mu_{plowing}$$

Rolling Friction

Rolling Resistance Coefficient:

$$\mu_r = \frac{F_r}{N}$$

Generally $\mu_r \ll \mu_k$

Rolling Resistance Force:

$$F_r = \frac{C_r N}{r}$$

where: - C_r = rolling resistance coefficient (length) - r = wheel radius

Wear

Archard Wear Equation

Wear Volume:

$$V = K \frac{NL}{H}$$

where: - K = dimensionless wear coefficient - N = normal load - L = sliding distance - H = hardness of softer material

Wear Rate:

$$\frac{dV}{dt} = K \frac{Nv}{H}$$

where v is sliding velocity

Wear Coefficient:

Ranges from 10^{-8} (mild wear) to 10^{-2} (severe wear)

Types of Wear

Adhesive Wear: Material transfer between surfaces

Abrasive Wear: Hard particles or asperities scratch surface

- Two-body: Hard surface against soft - Three-body: Hard particles between surfaces

Fatigue Wear: Repeated loading causes surface cracks, spalling

Corrosive Wear: Chemical reaction forms oxide, then removed

Fretting Wear: Small amplitude oscillatory motion

Specific Wear Rate

$$k = \frac{V}{NL}$$

Units: $\text{mm}^3/(\text{N} \cdot \text{m})$

Lower k indicates better wear resistance

Lubrication

Viscosity

Dynamic Viscosity (μ):

$$\tau = \mu \frac{du}{dy}$$

Units: $\text{Pa} \cdot \text{s}$ or $\text{N} \cdot \text{s}/\text{m}^2$ or poise (1 poise = $0.1 \text{ Pa} \cdot \text{s}$)

Kinematic Viscosity (ν):

$$\nu = \frac{\mu}{\rho}$$

Units: m^2/s or stoke (1 stoke = $10^{-4} \text{ m}^2/\text{s}$)

Temperature Dependence:

Viscosity decreases with increasing temperature

Lubrication Regimes

Stribeck Curve: Friction vs. $\frac{\mu v}{P}$

Boundary Lubrication: - High load, low speed, thin film - Metal-to-metal contact - High friction ($\mu \approx 0.1$ to 0.15)

Mixed Lubrication: - Partial fluid film, partial contact - Transition regime

Hydrodynamic (Fluid Film) Lubrication: - Surfaces completely separated by fluid film - Low friction ($\mu \approx 0.001$ to 0.01) - Load supported by pressure in fluid

Elastohydrodynamic (EHL) Lubrication: - High pressure deforms surfaces - Common in gears, rolling bearings

Reynolds Equation

1D Simplified:

$$\frac{d}{dx} \left(h^3 \frac{dp}{dx} \right) = 6\mu U \frac{dh}{dx}$$

where: - h = film thickness - p = pressure - U = velocity

Describes pressure distribution in fluid film

Minimum Film Thickness

For journal bearing:

$$h_{min} = c(1 - \epsilon)$$

where: - c = radial clearance - ϵ = eccentricity ratio

For safe operation: $h_{min} > 3\sigma$ (where σ is composite surface roughness)

Lubricant Selection

Viscosity Index (VI):

Measure of viscosity change with temperature

Higher VI → less change with temperature

Pour Point: Lowest temperature at which oil flows

Flash Point: Temperature at which vapor ignites

Surface Characterization

Surface Topography

Peak Count: Number of peaks per unit length

Bearing Ratio: Fraction of surface above a certain depth

Wavelength: Distance between repeating features

Contact Mechanics

Hertzian Contact (elastic):

For cylinder on cylinder:

$$p_{max} = \frac{2P}{\pi bL}$$

where: - P = normal load - b = contact width - L = contact length

Real Contact Area:

$$A_r = \frac{N}{H}$$

where H is hardness

Real area \ll Apparent area

Solid Lubricants

Common solid lubricants: - Graphite (requires moisture or gases) - MoS₂ (works in vacuum) - PTFE (Teflon) - Soft metals (lead, indium)

Used when liquid lubricants fail (high temp, vacuum, contamination concerns)

Quick Reference Values

Typical Friction Coefficients:

Interface	μ
Steel on steel (dry)	0.6-0.8
Steel on steel (lubricated)	0.05-0.1
Steel on bronze (dry)	0.2
Brake materials	0.3-0.5
Rubber on pavement	0.6-0.9
Teflon on steel	0.04-0.1