

# Fluid Mechanics

## Fluid Properties

### Density and Specific Weight

Density:

$$\rho = \frac{m}{V}$$

Specific Weight:

$$\gamma = \rho g$$

Specific Gravity:

$$SG = \frac{\rho}{\rho_{H_2O}} = \frac{\gamma}{\gamma_{H_2O}}$$

### Viscosity

Dynamic (Absolute) Viscosity:

$$\tau = \mu \frac{du}{dy}$$

Kinematic Viscosity:

$$\nu = \frac{\mu}{\rho}$$

**Newton's Law of Viscosity:** Fluids where  $\tau \propto du/dy$  are Newtonian

**Typical Values:** - Water at 20°C:  $\mu = 1.0 \times 10^{-3} \text{ Pa} \cdot \text{s}$ ,  $\nu = 1.0 \times 10^{-6} \text{ m}^2/\text{s}$  - Air at 20°C:  $\mu = 1.8 \times 10^{-5} \text{ Pa} \cdot \text{s}$ ,  $\nu = 1.5 \times 10^{-5} \text{ m}^2/\text{s}$

### Surface Tension

$$\Delta P = \sigma \left( \frac{1}{R_1} + \frac{1}{R_2} \right)$$

For spherical droplet:

$$\Delta P = \frac{2\sigma}{R}$$

For cylindrical jet:

$$\Delta P = \frac{\sigma}{R}$$

Capillary Rise:

$$h = \frac{2\sigma \cos \theta}{\rho g r}$$

where  $\theta$  is contact angle

## Bulk Modulus

**Compressibility:**

$$E_v = -V \frac{dP}{dV} = \rho \frac{dP}{d\rho}$$

**Speed of Sound:**

$$c = \sqrt{\frac{E_v}{\rho}}$$

For ideal gas:  $c = \sqrt{kRT}$

## Fluid Statics

### Pressure Variation

**Hydrostatic Equation:**

$$\frac{dP}{dz} = -\rho g$$

For incompressible fluid:

$$P_2 - P_1 = -\rho g(z_2 - z_1) = \rho gh$$

**Absolute vs Gage Pressure:**

$$P_{abs} = P_{gage} + P_{atm}$$

## Manometry

**U-Tube Manometer:**

$$P_A - P_B = \rho_{fluid}gh$$

**Differential Manometer:**

$$P_A - P_B = (\rho_2 - \rho_1)gh$$

## Forces on Submerged Surfaces

**Horizontal Flat Surface:**

$$F_R = P_c A = \rho gh_c A$$

where  $h_c$  is depth to centroid

**Location of Center of Pressure:**

$$y_{cp} = y_c + \frac{I_{xc}}{y_c A}$$

where  $I_{xc}$  is second moment of area about centroidal axis

**Inclined Flat Surface:**

Same formulas with  $y$  measured along inclined surface

**Curved Surface:**

Horizontal component:  $F_H = \rho g h_c A_{projected}$

Vertical component:  $F_V = \rho g V_{fluid}$

**Buoyancy****Buoyant Force (Archimedes):**

$$F_B = \rho_{fluid} g V_{displaced}$$

Acts upward through centroid of displaced volume (center of buoyancy)

**Floating Body:**

$$W = F_B$$

$$\rho_{body} V_{body} g = \rho_{fluid} V_{submerged} g$$

**Stability:**

Stable if metacenter is above center of gravity

**Kinematics****Velocity Field****Eulerian Description:**

$$\mathbf{V} = u(x, y, z, t)\mathbf{i} + v(x, y, z, t)\mathbf{j} + w(x, y, z, t)\mathbf{k}$$

**Lagrangian Description:**

Follow individual particles

**Acceleration****Material (Substantial) Derivative:**

$$\frac{D\mathbf{V}}{Dt} = \frac{\partial \mathbf{V}}{\partial t} + (\mathbf{V} \cdot \nabla) \mathbf{V}$$

$$a_x = \frac{Du}{Dt} = \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z}$$

Local acceleration + Convective acceleration

## Flow Classification

**Steady:**  $\partial/\partial t = 0$

**Uniform:**  $\partial/\partial s = 0$  along streamline

**Incompressible:**  $\rho = \text{constant}$

## Streamlines, Pathlines, Streaklines

**Streamline:** Tangent to velocity at instant

For 2D:  $\frac{dy}{dx} = \frac{v}{u}$

**Pathline:** Trajectory of fluid particle

**Streakline:** Locus of particles passing through a point

For steady flow: all three coincide

## Vorticity and Circulation

**Vorticity:**

$$\boldsymbol{\omega} = \nabla \times \mathbf{V}$$

In 2D:

$$\omega_z = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}$$

**Circulation:**

$$\Gamma = \oint_C \mathbf{V} \cdot d\mathbf{s}$$

**Irrotational Flow:**  $\nabla \times \mathbf{V} = 0$

## Conservation Laws

### Conservation of Mass (Continuity)

**Differential Form:**

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{V}) = 0$$

**Incompressible:**

$$\nabla \cdot \mathbf{V} = 0$$

In Cartesian:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

**Integral Form (Control Volume):**

$$\frac{\partial}{\partial t} \int_{CV} \rho dV + \int_{CS} \rho \mathbf{V} \cdot \mathbf{n} dA = 0$$

**Steady Flow:**

$$\sum \dot{m}_{in} = \sum \dot{m}_{out}$$

$$\rho_1 A_1 V_1 = \rho_2 A_2 V_2$$

For incompressible:

$$Q = AV = \text{constant}$$

**Momentum Equation**

**Differential Form (Navier-Stokes):**

For incompressible, Newtonian fluid:

$$\rho \frac{D\mathbf{V}}{Dt} = -\nabla P + \mu \nabla^2 \mathbf{V} + \rho \mathbf{g}$$

x-component:

$$\rho \left( \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) = -\frac{\partial P}{\partial x} + \mu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) + \rho g_x$$

**Euler's Equation (Inviscid):**

$$\rho \frac{D\mathbf{V}}{Dt} = -\nabla P + \rho \mathbf{g}$$

**Integral Form (Control Volume):**

$$\sum \mathbf{F} = \frac{\partial}{\partial t} \int_{CV} \rho \mathbf{V} dV + \int_{CS} \rho \mathbf{V} (\mathbf{V} \cdot \mathbf{n}) dA$$

**Steady Flow:**

$$\sum \mathbf{F} = \sum \dot{m}_{out} \mathbf{V}_{out} - \sum \dot{m}_{in} \mathbf{V}_{in}$$

## Energy Equation

**First Law (Control Volume):**

$$\dot{Q} - \dot{W}_s = \frac{\partial}{\partial t} \int_{CV} \rho e dV + \int_{CS} \rho \left( e + \frac{P}{\rho} \right) (\mathbf{V} \cdot \mathbf{n}) dA$$

where  $e = u + V^2/2 + gz$  and  $\dot{W}_s$  is shaft work

## Bernoulli Equation

**Along a Streamline:**

$$\frac{P}{\rho} + \frac{V^2}{2} + gz = \text{constant}$$

or

$$\frac{P}{\gamma} + \frac{V^2}{2g} + z = \text{constant}$$

**Assumptions:** - Steady flow - Incompressible - Inviscid (frictionless) - Along a streamline

**Extended Bernoulli (with losses):**

$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_L$$

**With pump/turbine:**

$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 + h_p = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_t + h_L$$

**Pitot Tube:**

$$V = \sqrt{\frac{2(P_0 - P)}{\rho}} = \sqrt{2gh}$$

where  $P_0$  is stagnation pressure

## Dimensional Analysis

### Buckingham Pi Theorem

If physical phenomenon involves  $n$  variables and  $m$  fundamental dimensions:

Number of dimensionless groups =  $n - m$

## Important Dimensionless Numbers

**Reynolds Number:**

$$Re = \frac{\rho V L}{\mu} = \frac{V L}{\nu} = \frac{\text{inertial forces}}{\text{viscous forces}}$$

**Froude Number:**

$$Fr = \frac{V}{\sqrt{gL}} = \frac{\text{inertial forces}}{\text{gravity forces}}$$

**Euler Number:**

$$Eu = \frac{P}{\rho V^2} = \frac{\text{pressure forces}}{\text{inertial forces}}$$

**Mach Number:**

$$Ma = \frac{V}{c} = \frac{\text{flow velocity}}{\text{sound velocity}}$$

**Weber Number:**

$$We = \frac{\rho V^2 L}{\sigma} = \frac{\text{inertial forces}}{\text{surface tension forces}}$$

**Drag Coefficient:**

$$C_D = \frac{F_D}{\frac{1}{2}\rho V^2 A}$$

**Lift Coefficient:**

$$C_L = \frac{F_L}{\frac{1}{2}\rho V^2 A}$$

## Viscous Flow in Pipes

### Flow Regimes

**Laminar:**  $Re < 2300$

**Transitional:**  $2300 < Re < 4000$

**Turbulent:**  $Re > 4000$

### Fully Developed Laminar Flow

**Velocity Profile (Poiseuille Flow):**

$$u(r) = u_{max} \left[ 1 - \left( \frac{r}{R} \right)^2 \right]$$

where  $u_{max} = \frac{R^2}{4\mu} \left( -\frac{dP}{dx} \right)$

**Average Velocity:**

$$V = \frac{u_{max}}{2} = \frac{R^2}{8\mu} \left( -\frac{dP}{dx} \right) = \frac{D^2}{32\mu} \left( -\frac{dP}{dx} \right)$$

**Hagen-Poiseuille Equation:**

$$\Delta P = \frac{32\mu LV}{D^2} = \frac{128\mu LQ}{\pi D^4}$$

**Friction Factor:**

$$f = \frac{64}{Re}$$

**Turbulent Flow**

**Friction Factor:**

Smooth pipes (Blasius):

$$f = \frac{0.316}{Re^{1/4}} \quad (Re < 10^5)$$

Colebrook equation (implicit):

$$\frac{1}{\sqrt{f}} = -2.0 \log \left( \frac{\epsilon/D}{3.7} + \frac{2.51}{Re\sqrt{f}} \right)$$

where  $\epsilon$  is roughness height

**Moody Chart:** Graphical representation of  $f$  vs  $Re$  for various  $\epsilon/D$

**Power Law Velocity Profile:**

$$u(r) = u_{max} \left[ 1 - \frac{r}{R} \right]^{1/n}$$

where  $n \approx 7$  for turbulent flow

**Head Loss**

**Major Loss (Darcy-Weisbach):**

$$h_L = f \frac{L}{D} \frac{V^2}{2g}$$

**Minor Losses:**

$$h_L = K_L \frac{V^2}{2g}$$

where  $K_L$  is loss coefficient (from tables)

Common values: - Pipe entrance (sharp):  $K_L = 0.5$  - Pipe exit:  $K_L = 1.0$  - 90° elbow:  $K_L \approx 0.9$  - Gate valve (open):  $K_L \approx 0.2$

**Total Head Loss:**

$$h_L = f \frac{L}{D} \frac{V^2}{2g} + \sum K_L \frac{V^2}{2g}$$



## Pipe Systems

### Pipes in Series:

$$Q = Q_1 = Q_2 = Q_3$$

$$h_L = h_{L1} + h_{L2} + h_{L3}$$

### Pipes in Parallel:

$$Q = Q_1 + Q_2 + Q_3$$

$$h_L = h_{L1} = h_{L2} = h_{L3}$$

### Three-Reservoir Problem:

Use continuity and energy equations at junction

## External Flow

### Boundary Layer

#### Boundary Layer Thickness ( $\delta$ ):

Height where  $u = 0.99U_\infty$

#### Displacement Thickness:

$$\delta^* = \int_0^\infty \left(1 - \frac{u}{U}\right) dy$$

#### Momentum Thickness:

$$\theta = \int_0^\infty \frac{u}{U} \left(1 - \frac{u}{U}\right) dy$$

### Flat Plate

#### Laminar ( $Re_x < 5 \times 10^5$ ):

Boundary layer thickness:

$$\delta = \frac{5x}{\sqrt{Re_x}}$$

Local skin friction coefficient:

$$C_{f,x} = \frac{0.664}{\sqrt{Re_x}}$$

Average skin friction coefficient:

$$\bar{C}_f = \frac{1.328}{\sqrt{Re_L}}$$

#### Turbulent ( $Re_x > 5 \times 10^5$ ):

Boundary layer thickness:

$$\delta = \frac{0.37x}{Re_x^{1/5}}$$

Local skin friction coefficient:

$$C_{f,x} = \frac{0.059}{Re_x^{1/5}}$$

Average (with turbulent from leading edge):

$$\overline{C}_f = \frac{0.074}{Re_L^{1/5}}$$

**Drag Force:**

$$F_D = \overline{C}_f \left( \frac{1}{2} \rho V^2 \right) A_s$$

where  $A_s$  is surface area

## Flow Over Cylinder and Sphere

**Drag:**

$$F_D = C_D \left( \frac{1}{2} \rho V^2 \right) A_f$$

where  $A_f$  is frontal area

**Typical  $C_D$  Values:**

Sphere: -  $Re < 1$ :  $C_D = 24/Re$  (Stokes flow) -  $10^3 < Re < 2 \times 10^5$ :  $C_D \approx 0.4$  -  $Re > 3 \times 10^5$ :  $C_D \approx 0.1$  (turbulent, drag crisis)

Cylinder: -  $Re < 1$ :  $C_D \approx 10/Re$  -  $10^3 < Re < 2 \times 10^5$ :  $C_D \approx 1.2$

**Terminal Velocity:**

When  $F_D = W - F_B$ :

$$V_t = \sqrt{\frac{2(W - F_B)}{\rho C_D A_f}}$$

## Potential Flow

### Velocity Potential

For irrotational flow:

$$\mathbf{V} = \nabla \phi$$

$$u = \frac{\partial \phi}{\partial x}, \quad v = \frac{\partial \phi}{\partial y}$$

**Laplace Equation:**

$$\nabla^2 \phi = 0$$

**Stream Function**

For 2D incompressible flow:

$$u = \frac{\partial \psi}{\partial y}, \quad v = -\frac{\partial \psi}{\partial x}$$

Lines of constant  $\psi$  are streamlines

**Volume Flow Rate:**

Between two streamlines:

$$Q = \psi_2 - \psi_1$$

**Elementary Flows****Uniform Flow:**

$$\phi = Ux, \quad \psi = Uy$$

**Source/Sink:**

$$\phi = \frac{m}{2\pi} \ln r, \quad \psi = \frac{m}{2\pi} \theta$$

where  $m$  is strength (positive for source)

**Vortex:**

$$\phi = \frac{\Gamma}{2\pi} \theta, \quad \psi = -\frac{\Gamma}{2\pi} \ln r$$

where  $\Gamma$  is circulation

**Doublet:**

$$\phi = -\frac{\Lambda \cos \theta}{r}, \quad \psi = \frac{\Lambda \sin \theta}{r}$$

**Superposition:**

Complex potential flows can be created by superposition of elementary flows

**Compressible Flow****Speed of Sound**

$$c = \sqrt{\left. \frac{\partial P}{\partial \rho} \right|_s}$$

For ideal gas:

$$c = \sqrt{kRT}$$

## Mach Number Relations

**Subsonic:**  $Ma < 1$

**Sonic:**  $Ma = 1$

**Supersonic:**  $Ma > 1$

**Hypersonic:**  $Ma > 5$

## Isentropic Relations

**Stagnation Properties:**

$$\frac{T_0}{T} = 1 + \frac{k-1}{2} Ma^2$$

$$\frac{P_0}{P} = \left(1 + \frac{k-1}{2} Ma^2\right)^{k/(k-1)}$$

$$\frac{\rho_0}{\rho} = \left(1 + \frac{k-1}{2} Ma^2\right)^{1/(k-1)}$$

**Critical Conditions ( $Ma = 1$ ):**

$$\frac{T^*}{T_0} = \frac{2}{k+1}$$

$$\frac{P^*}{P_0} = \left(\frac{2}{k+1}\right)^{k/(k-1)}$$

## Normal Shock

**Across shock:**

$$\frac{P_2}{P_1} = 1 + \frac{2k}{k+1} (Ma_1^2 - 1)$$

$$\frac{\rho_2}{\rho_1} = \frac{(k+1)Ma_1^2}{(k-1)Ma_1^2 + 2}$$

$$Ma_2^2 = \frac{(k-1)Ma_1^2 + 2}{2kMa_1^2 - (k-1)}$$

Shock always:  $Ma_1 > 1$ ,  $Ma_2 < 1$

# Open Channel Flow

## Froude Number

$$Fr = \frac{V}{\sqrt{gy}}$$

where  $y$  is flow depth

**Subcritical:**  $Fr < 1$  (tranquil)

**Critical:**  $Fr = 1$

**Supercritical:**  $Fr > 1$  (rapid)

## Manning Equation

$$V = \frac{1}{n} R_h^{2/3} S^{1/2}$$

where: -  $n$  = Manning roughness coefficient -  $R_h = A/P$  = hydraulic radius -  $S$  = channel slope

**Flow Rate:**

$$Q = \frac{1}{n} A R_h^{2/3} S^{1/2}$$

## Specific Energy

$$E = y + \frac{V^2}{2g}$$

**Critical Depth:**

For rectangular channel:

$$y_c = \left( \frac{q^2}{g} \right)^{1/3}$$

where  $q = Q/b$  is discharge per unit width

## Quick Reference

**Common Fluid Properties (at 20°C, 1 atm):**

Water: -  $\rho = 998 \text{ kg/m}^3$  -  $\mu = 1.0 \times 10^{-3} \text{ Pa} \cdot \text{s}$  -  $\nu = 1.0 \times 10^{-6} \text{ m}^2/\text{s}$

Air: -  $\rho = 1.20 \text{ kg/m}^3$  -  $\mu = 1.8 \times 10^{-5} \text{ Pa} \cdot \text{s}$  -  $\nu = 1.5 \times 10^{-5} \text{ m}^2/\text{s}$

**Standard Atmosphere:** -  $P = 101.325 \text{ kPa} = 1 \text{ atm}$  -  $T = 15^\circ\text{C} = 288 \text{ K}$  -  $\rho = 1.225 \text{ kg/m}^3$