All the oscillators using tuned LC circuits operate well at high frequencies. At low frequencies, as the inductors and capacitors required for the time circuit would be very bulky and RC oscillators are found to be more suitable. Two important RC oscillators are

- (i) RC phase-shift oscillator
- (ii) Wien-bridge oscillator
- (i). RC Phase-Shift Oscillator using BJT with Cascade connection of High-Pass Filter (Phase-lead RC Network)

BJT based RC phase-shift oscillator using phaselead RC network is shown in Figure 2.

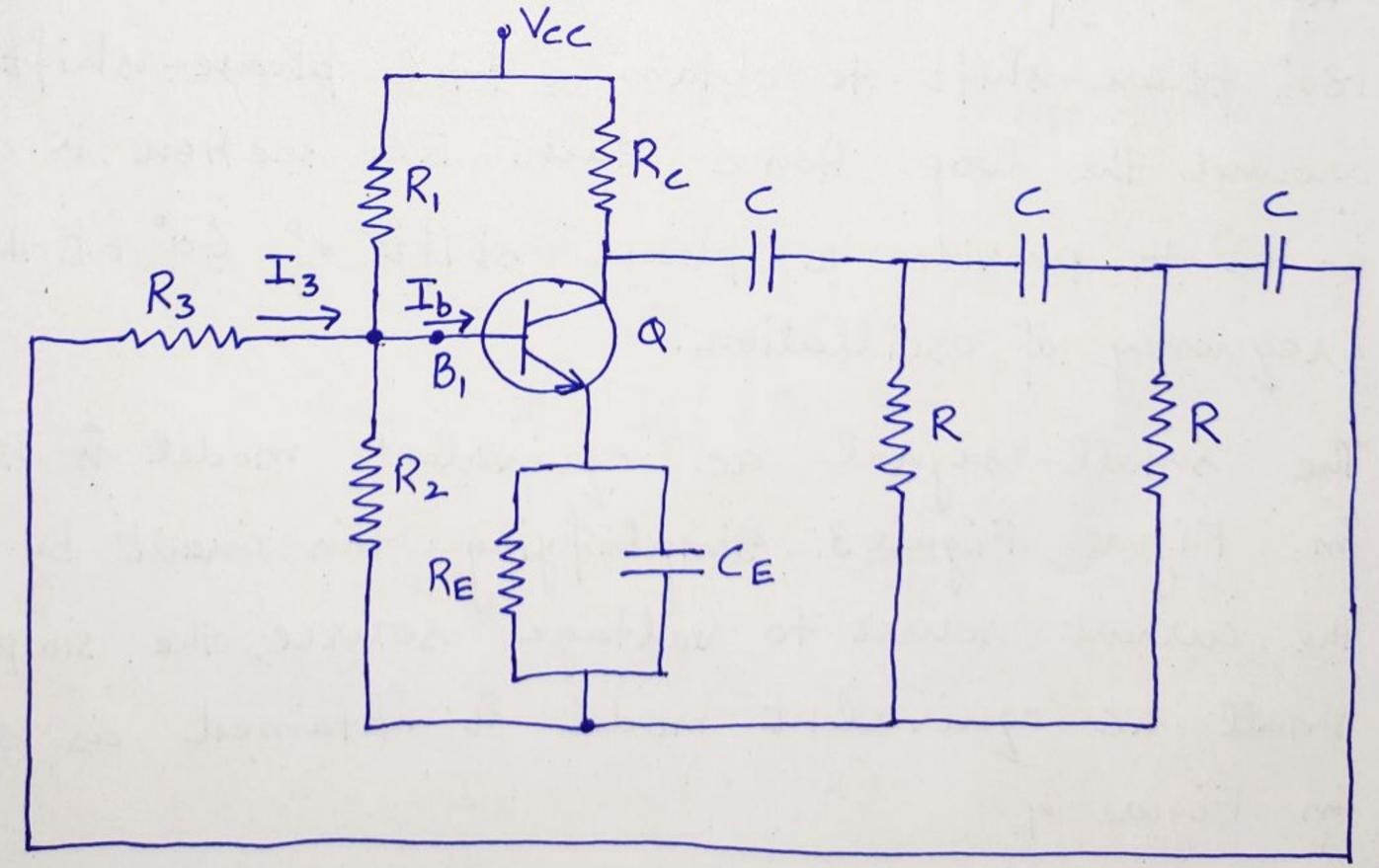


Figure 2. BJT-based Rc Phase-Shift Osciellator.

Here, the output of the feedback network is loaded appreciably by the relatively low resistance of the transistor. Thus, the resistance R of the feedback network is in parallel with the low input resistance this of the transistor, which reduces the effective value of R in the last section of the feedback network.

The feedback signal is coupled through the feedback resistor  $R_3$  in series with the amplifier stage input resistor. In order to make the three sections identical,  $R_3$  is chosen as  $R_3 = R - R_1$  where  $R_1$  is the input impedance of the circuit.

The BJT amplifier provides a phase-shift of 180° and the feedback RC network provides the remaining 180° phase-shift to obtain a total phase-shift of 360° around the loop. Hence, each RC section is designed so as to provide a phase-shift of 60° at the desired frequency of oscillation.

The small-signal ac equivalent model is shown in Figure Figure 3. Simplifying this circuit by replacing the current source to voltage source, the simplified small ac equivalent model is obtained as shown in Figure 4.

Applying KVL, we get

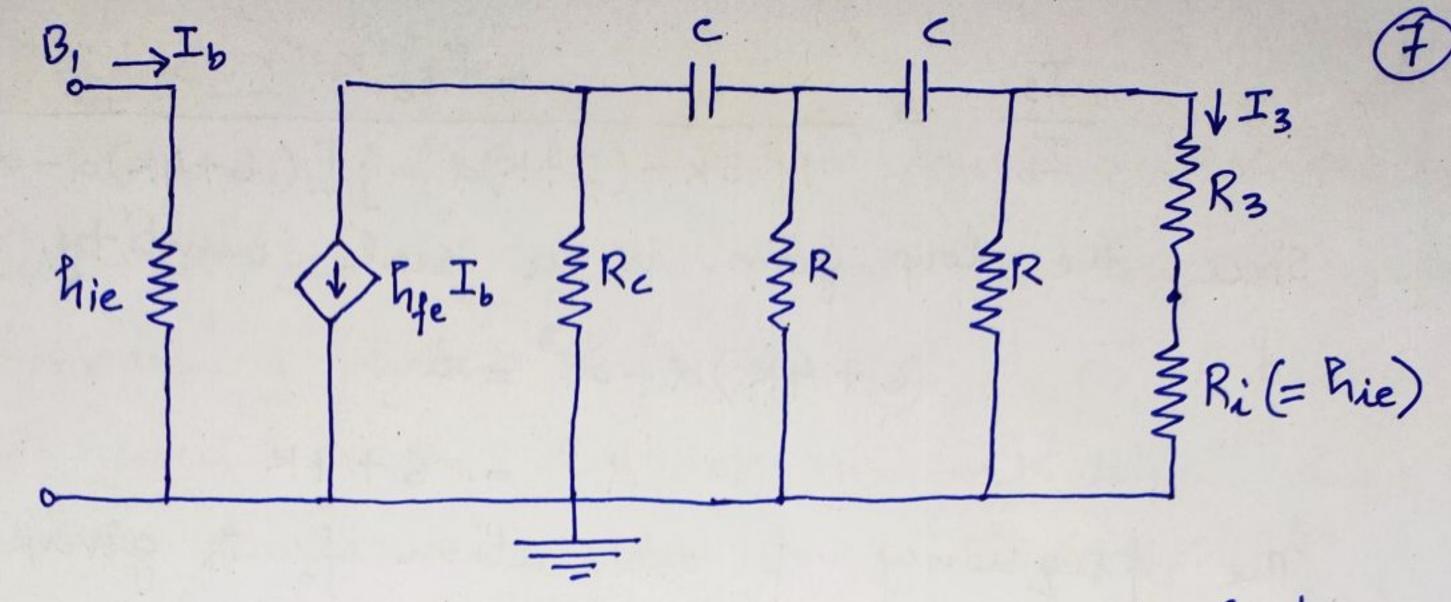


Figure 3. 5 mall-signal ac équivalent

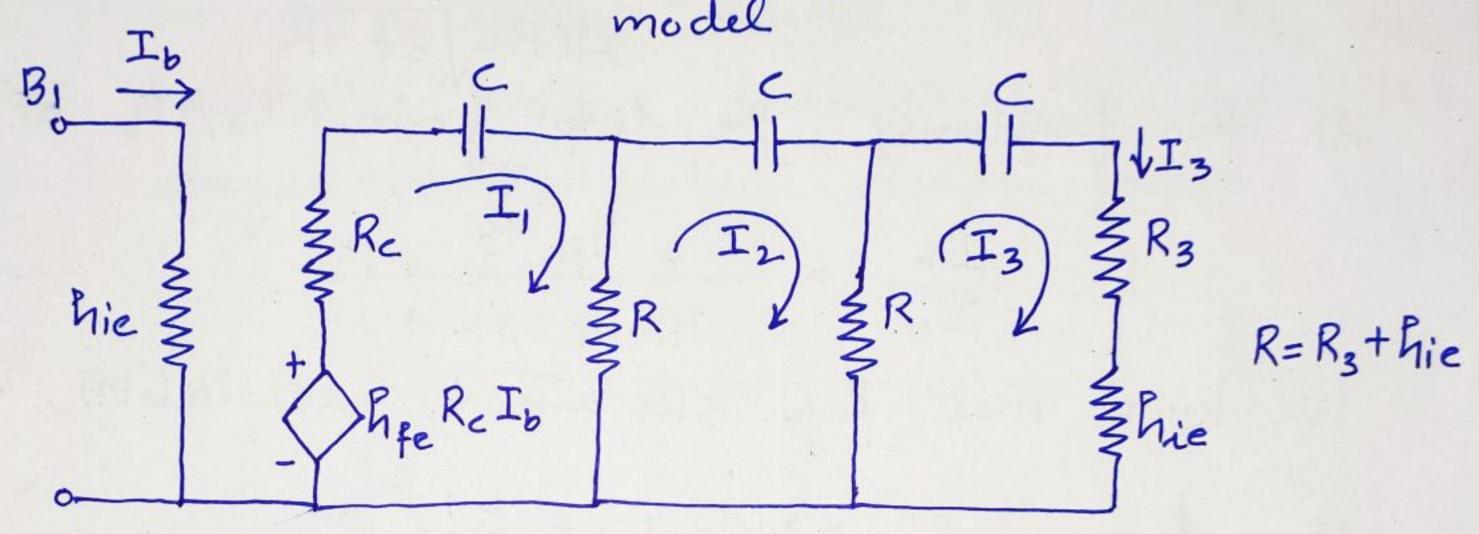


Figure 4. Simplified small-signer ac equivalent model.

$$I_{1}\left(R_{c}+R+\frac{1}{jwc}\right)-I_{2}R=-h_{fe}R_{c}I_{b}$$

$$-I_{1}R+I_{2}\left(2R+\frac{1}{jwc}\right)-I_{3}R=0$$

$$-I_{2}R+I_{3}\left(2R+\frac{1}{jwc}\right)=0$$
Let  $d=\frac{1}{wRc}$  and  $K=\frac{Rc}{R}$ 

Upon solving the above equations, we get  $I_2 = I_3 (2-j\alpha)$ 

and 
$$I_1 = I_3(3-a^2-j4\alpha)$$

Substituting the above I, and Iz equations in the first KVL equation, we get loop gain I3/Ib as

$$\frac{I_3}{I_b} = \frac{-h_{fe} K}{1+3k-(5+K)\alpha^2-j\left[(6+4K)\alpha-\alpha^3\right]}$$
Since the loop gain is a real quantity, we have
$$(6+4K)\alpha-\alpha^3=0$$

The frequency of oscillation for is given by

 $f_o = \frac{1}{2 \text{TT RC} / 6 + 4 \text{K}}$  At this frequency, the loop gain  $I_3/I_5$  becomes,

I3 = he K Tb = 4K2+23K+29

We know that for sustained oscillation, I3/Ib>1.

he >4K+23+ 29/K There fore

 $\frac{dh_{fe}}{dK} = 4 - \frac{29}{K^2} = 0$ Thus,

 $K = \left(\frac{29}{4}\right)^{1/2} = 2.7$ 

Therefore,

 $(h_{fe})_{min} = 4(2.7) + 23 + \frac{29}{2.7} = 44.5$ 

Hence, the value of life for a transistor must be at least 45 for the circuit to oscillate.

Figure 1 shows the circuit of a Wien-bridge oscillator. The circuit consists of a two-stage RC coupled amplifier which provides a phase-shift of 360° or 0°. A balanced bridge is used as the feedback network which tras no need to provide any additional phase-shift. The feedback network consists of a lead-lag network (R-C, end R2-C2) and a voltage divider (R3-R4). The lead-lag network provides a positive feedback to the input of the first stage and the voltage divider provides a negative

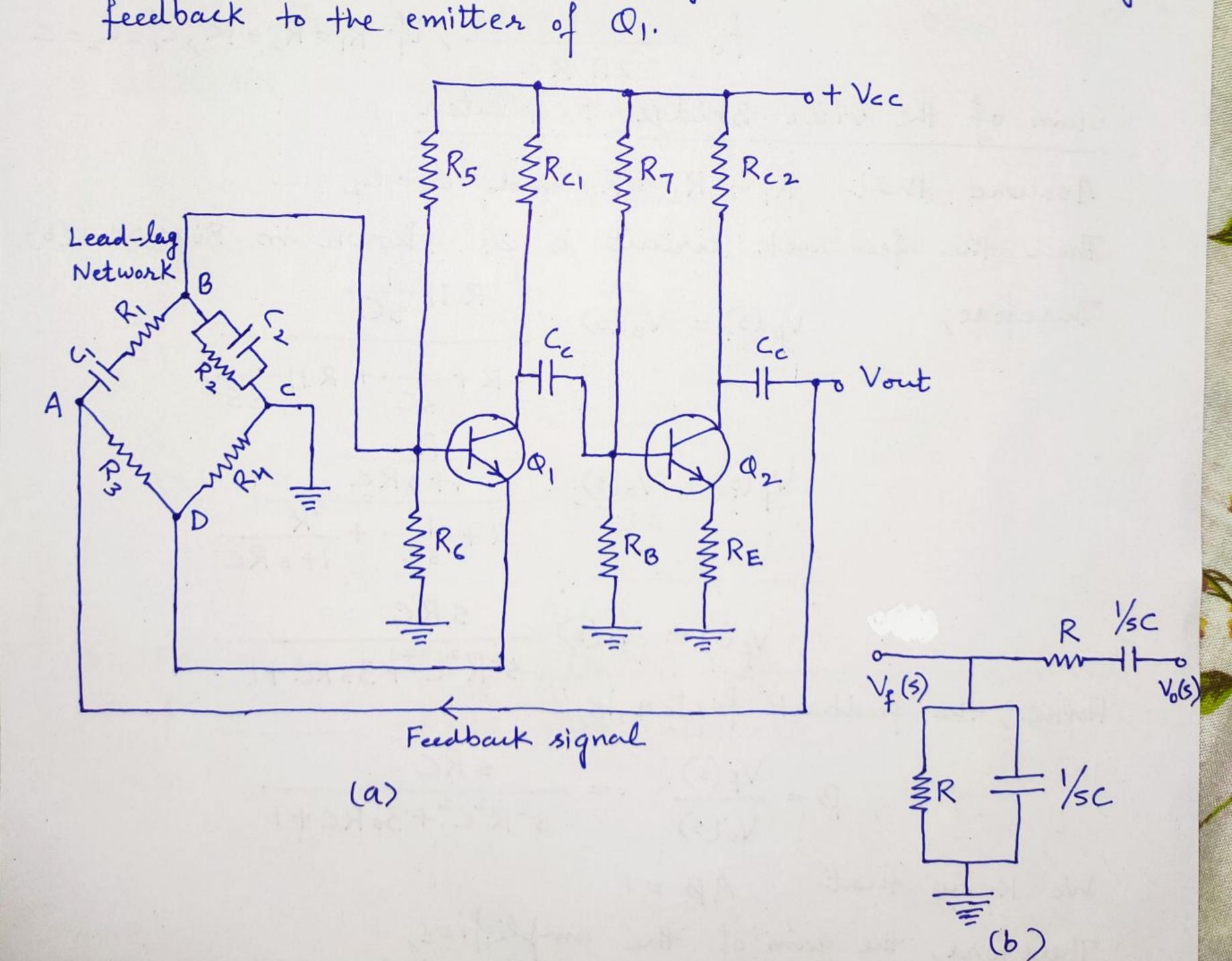


Figure 1.(4) Wien-bridge oscillator (b) Feedback circuit

$$\frac{R_3}{R_4} = \frac{R_1 - j \times c_1}{\left[\frac{R_2 \left(-j \times c_2\right)}{R_2 - j \times c_2}\right]}$$

where Xc, and Xc2 are the reactories of the capacitors. Simplifying the above equation and equating the real and imaginary parts on both sides, we get the frequency of oscillation as,

$$f_{o} = \frac{1}{2 \pi \sqrt{R_{1} R_{2} C_{1} C_{2}}}$$

 $f_0 = \frac{1}{2\pi Rc}$ , if  $R_1 = R_2 = R$ ,  $C_1 = C_2 = C$ 

Grain of the Wien-Bridge Oscillator

Assume that R1 = R2 = R and C1 = C2 = C

Then the feedback circuit is as shown in Figure 1(b).

$$V_{f}(s) = V_{o}(s)$$

$$\frac{R 11 \frac{1}{sC}}{R + \frac{1}{sC} + R 11 \frac{1}{cS}}$$

$$V_{f}(s) = V_{o}(s) \frac{R}{1+sRC}$$

$$R + \frac{1}{sC} + \frac{R}{1+sRC}$$

$$V_{f}(s) = V_{o}(s) - \frac{sRC}{s^{2}R^{2}c^{2} + 3sRC + 1}$$

Hence, the feedback factor is,

$$\beta = \frac{V_f(s)}{V_o(s)} = \frac{sRC}{s^2R^2C^2 + 3sRC + 1}$$

We Know that AB =

Therefore, the gain of the amplifier,  $A = \frac{1}{B} = \frac{5^2 R^2 C^2 + 3 s R C + 1}{s R C}$ 

Substituting s=jwo, where the frequency of oscillation 3

 $f_o = \frac{1}{2\pi RC}$  i.e  $w_o = \frac{1}{RC}$ 

in the equation of gain of the amplifier and simplifying, we get A=3. Hence, the gain of the Wien-bridge oscillator using a BJT amplifier is at least equal to 3 for oscillations to occur.

Q1. In a Wien-bridge oscillator, if the value of R is 100 K-2, and frequency of oscillation is 10 KHZ, find the value of the capacitor C.

Solution: The operating frequency of a Wien-bridge oscillator is given by,

 $f_0 = \frac{1}{2\pi RC}$ 

There fore,

 $C = \frac{1}{2\pi R_{f_0}^2}$ 

 $C = \frac{1}{2 \prod X |00 \times 10^3 \times 10 \times 10^3}$ 

C = 159 pF.

MCA
Q1. RC phase slift oscillator contain a minimum
of phase shift network
(a).1 (b) 2 (c) 3 (d) 0
Q2. One phase shift network of an RC phase shift
oscillator contain capacitor.
(a) 1 (b) 2 (c) 3 (d) 0
Q3. One phase shift network of an RC phase shift
oscillator Contains inductor.
(a) 1 (b) 2 (c) 3 (d) 0
Q4. One phase shift network of an RC phase shift
Q4. One phase shift network of an RC phase shift oscillator contain resistor.
(a) 1 (b) 2 (c) 3 (d) o
Q5. Phase shift provided by one phase shift network in RC phase shift oscillator in 3 stage is
in RC phase shift oscillator in 3 stage is
(9) 180° (b) 60° (c) 120° (d) 90°