

Q1. An amplifier has voltage gain with feedback of ① 100. If the gain without feedback changes by 20% and the gain with feedback should not vary more than 2%, determine the values of open-loop gain 'A' and feedback ratio β .

Solution: Given $A_f = 100$, $\frac{dA_f}{A_f} = 2\% = 0.02$

$$\text{and } \frac{dA}{A} = 20\% = 0.2$$

We know that

$$\frac{dA_f}{A_f} = \frac{dA}{A} \cdot \frac{1}{(1+A\beta)}$$

$$0.02 = 0.2 \times \frac{1}{(1+A\beta)}$$

$$\therefore 1+A\beta = \frac{0.2}{0.02} = 10$$

Also, we know that the gain with feedback is,

$$A_f = \frac{A}{1+A\beta}$$

$$\text{i.e. } 100 = \frac{A}{10}$$

$$\therefore A = 1000$$

$$\text{Now, } 1+A\beta = 10, \text{ i.e. } A\beta = 9$$

$$\therefore \beta = \frac{9}{A} = \frac{9}{1000} = 0.009$$

Q.2. An amplifier has a voltage gain of 400, $f_1 = 50 \text{ Hz}$, $f_2 = 200 \text{ KHz}$ and a distortion of 10% without feedback. Determine the amplifier voltage gain, f_{1f} , f_{2f} , and

D_f when a negative feedback is applied with feedback ratio of 0.01.

Solution: Given $A = 400$, $f_1 = 50 \text{ Hz}$, $f_2 = 200 \text{ KHz}$

Distortion, $D = 10\%$ and $\beta = 0.01$

We know that voltage gain with feedback

$$A_f = \frac{A}{1 + A\beta} = \frac{400}{1 + 400 \times 0.01} = 80$$

New lower 3 dB frequency,

$$f_{1f} = \frac{f_1}{1 + A\beta} = \frac{50}{1 + 400 \times 0.01} = 10 \text{ Hz}$$

New upper 3 dB frequency,

$$f_{2f} = (1 + A\beta) \times f_2 = (1 + 400 \times 0.01) \times 200 \times 10^3$$

$$f_{2f} = 1 \text{ MHz}$$

Distortion with feedback,

$$D_f = \frac{D}{1 + A\beta} = \frac{10}{5} = 2\%$$

Classification of Power Amplifiers

①

Based on the amount of transistor bias and amplitude of the input signal, amplifiers can be classified as Class A, Class B, Class AB and Class C.

Class A Amplifier

In a Class A amplifier, the transistor is biased such that the output current flows and the transistor is ON for the full cycle (360°) of the input ac signal as shown in Figure (a).

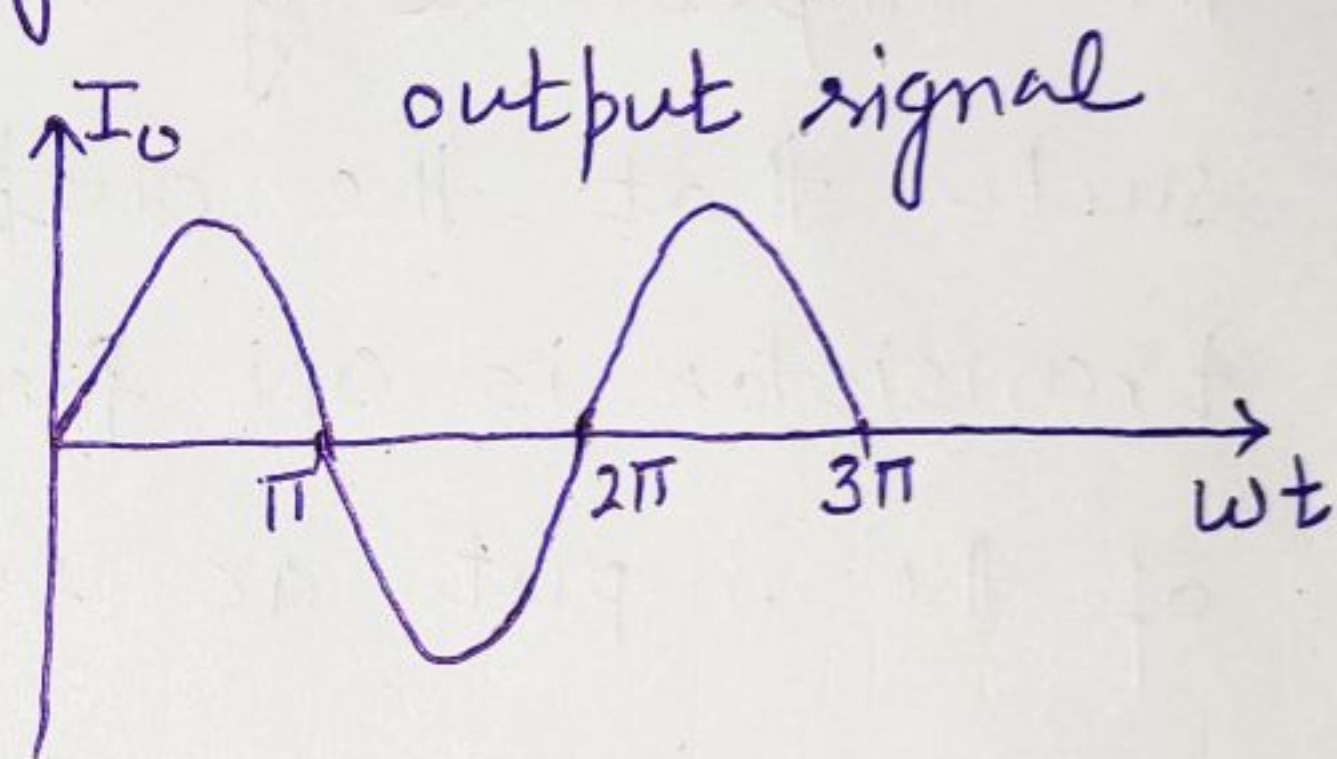
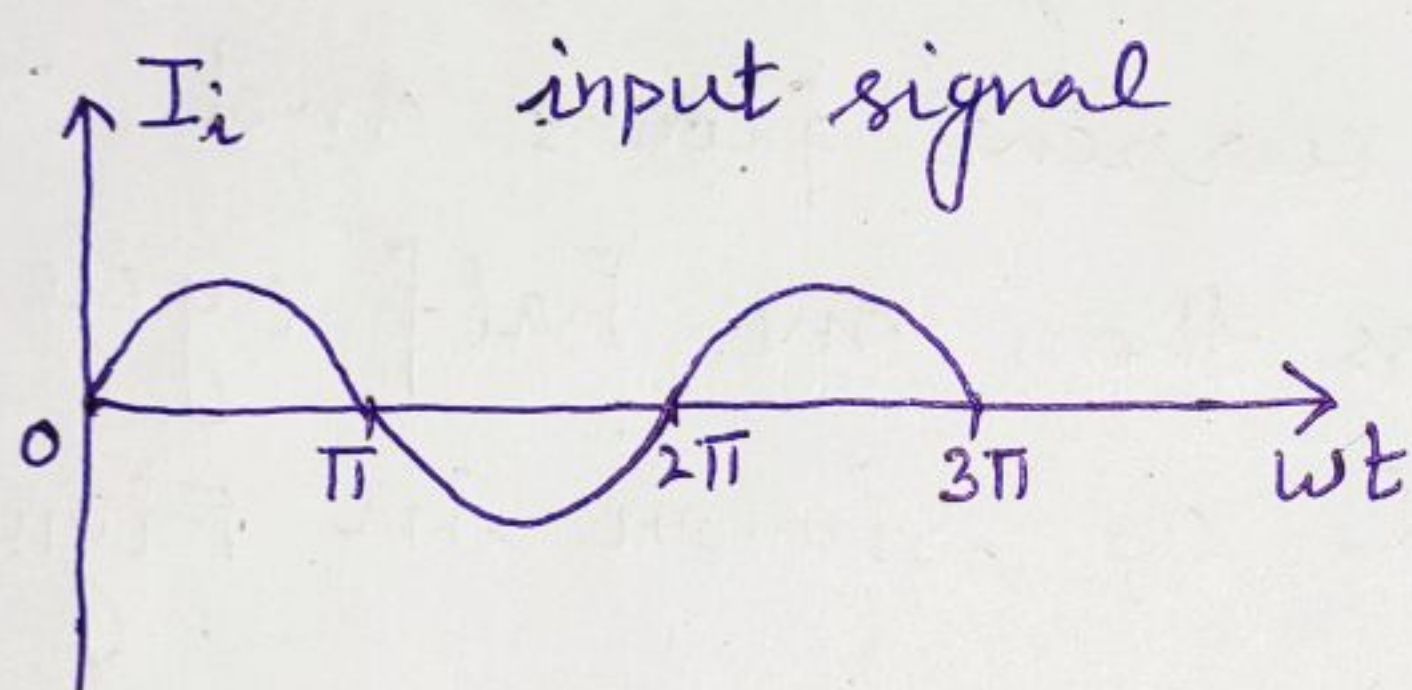


Fig. (a)

Class B Amplifier

In a Class B amplifier, the transistor bias and the amplitude of the input signal are selected such that the output current flows and the transistor is ON for only one half cycle (180°) of the input ac signal as shown in Figure (b).

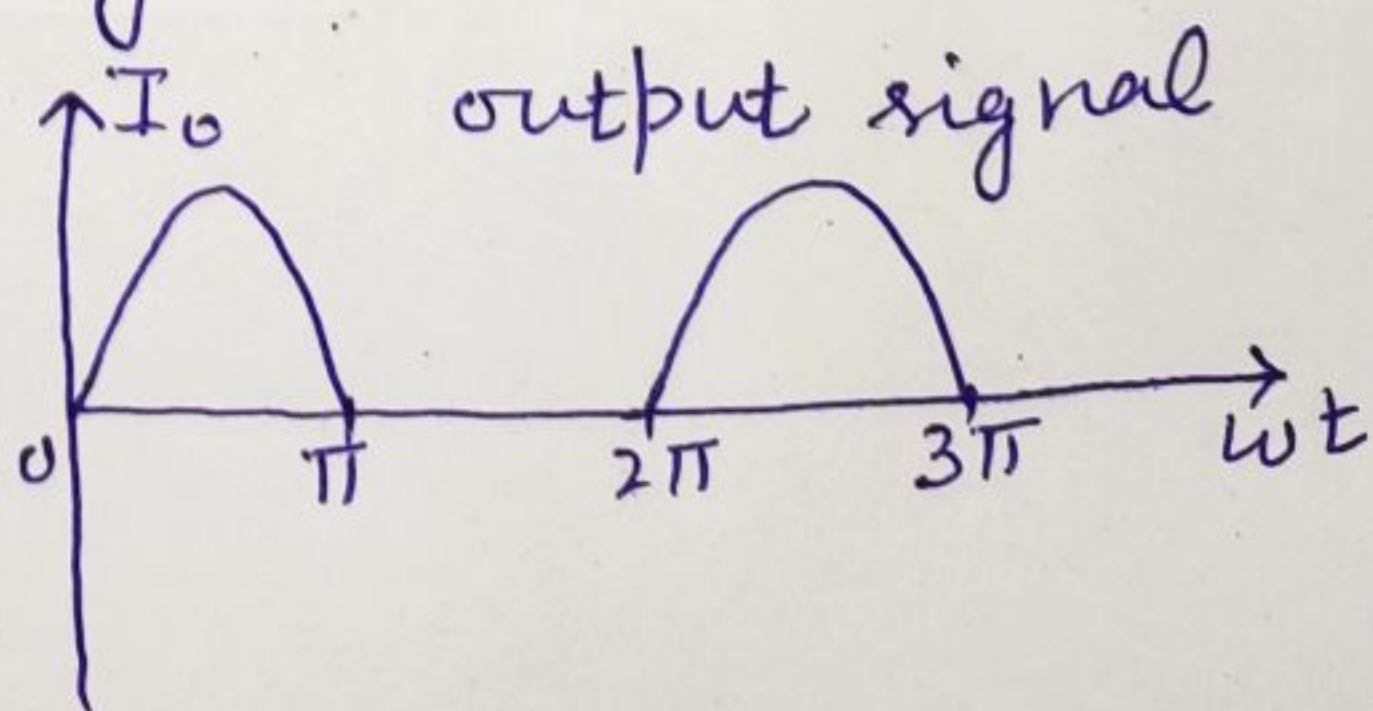
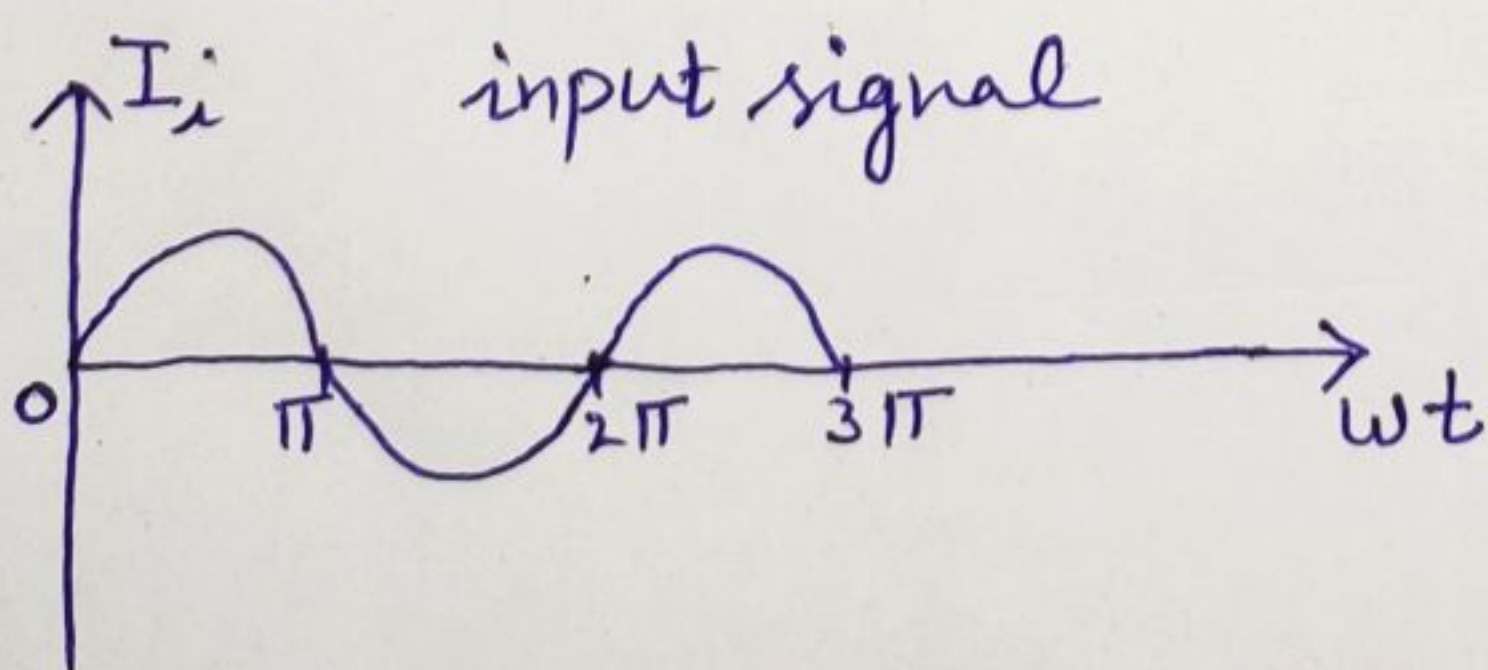


Fig (b)

Class AB Amplifiers

(2)

In a Class AB amplifier, the transistor operates between the two extremes defined for Class A and Class B amplifiers. Hence, the output signal exists for more than 180° but less than 360° of the input ac signal.

Class C Amplifier

In a Class C amplifier, the transistor bias and the amplitude of the input signal are selected such that the output current flows and the transistor is ON for less than one half cycle (180°) of the input ac signal as shown in Figure (c).

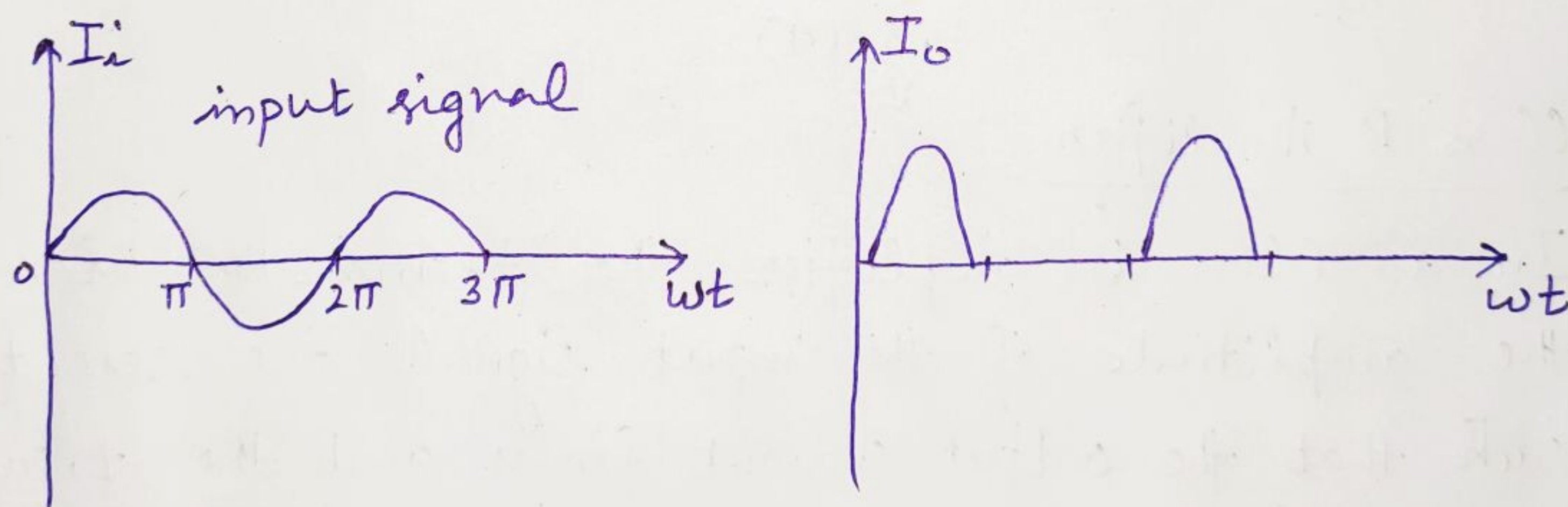


Fig. (c).

The main aim of a large-signal amplifier, otherwise called power amplifier, is to deliver a substantial amount of power to a load. ①

Class A Large Signal Amplifiers

A simple transistor amplifier that supplies power to a pure resistance load R_L is shown in Figure 1. Assuming that the static output characteristics are equidistant for equal increments of input base current i_B , if the input signal i_B is a sinusoidal, the output current and voltage are also sinusoidal as shown in Figure 2. i_c and v_c are instantaneous deviations from quiescent values I_c and V_c . The Power output is given by the equation $P = V_c \times I_c = I_c^2 \times R_L$, where V_c and I_c are the RMS values of the output voltage v_c and current i_c , respectively.

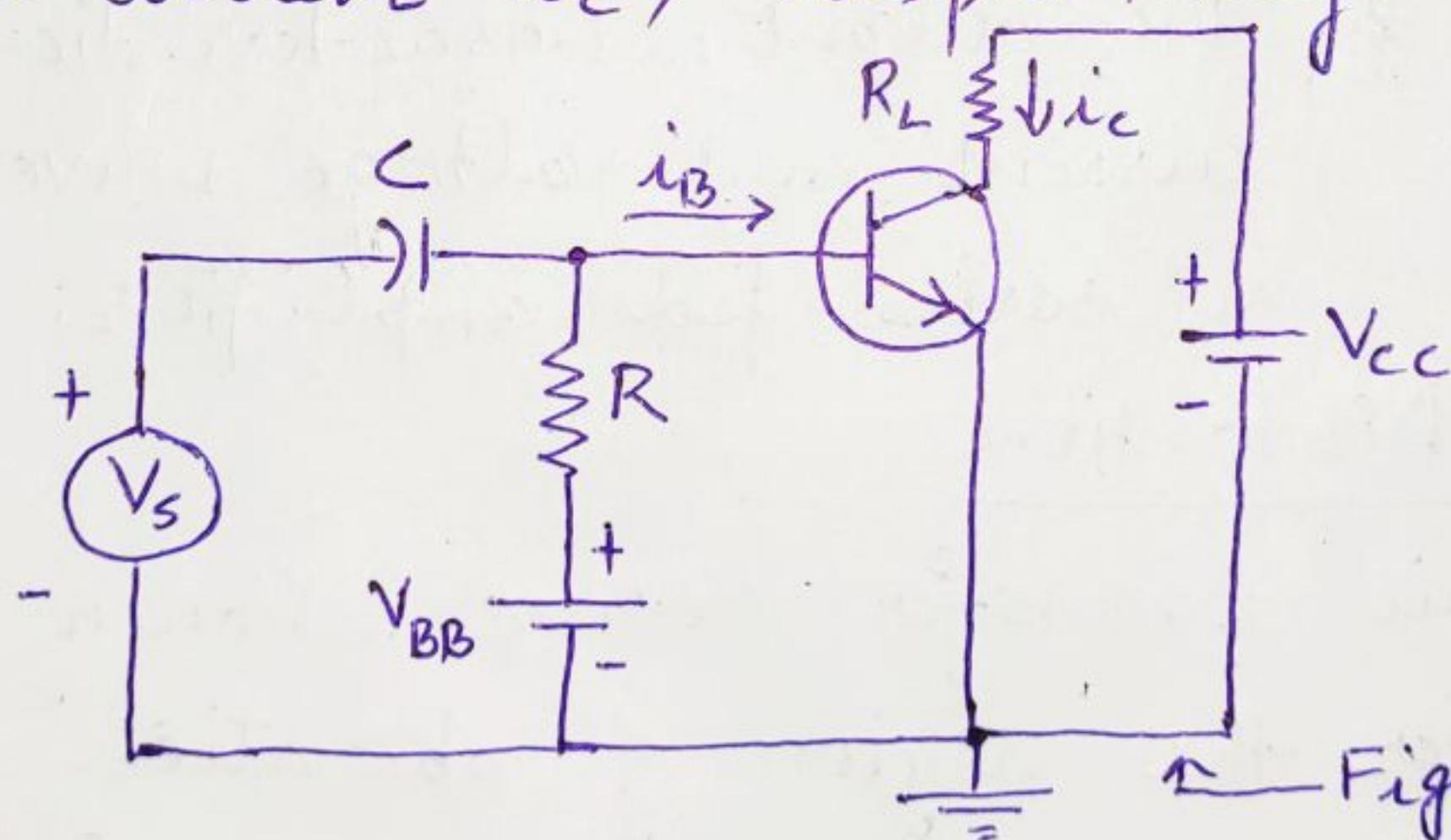


Figure 1. Simple series-fed amplifier

Now,
$$I_c = \frac{I_m}{\sqrt{2}} = \frac{I_{max} - I_{min}}{2\sqrt{2}}$$

and
$$V_c = \frac{V_m}{\sqrt{2}} = \frac{V_{max} - V_{min}}{2\sqrt{2}}$$

The Power output,
$$P = V_c I_c = \frac{(V_{max} - V_{min})(I_{max} - I_{min})}{8}$$

The power output can be expressed in terms of R_L as

$$P = V_c I_c = \frac{V_m I_m}{2} = \frac{I_m^2 R_L}{2} = \frac{V_m^2}{2 R_L}$$

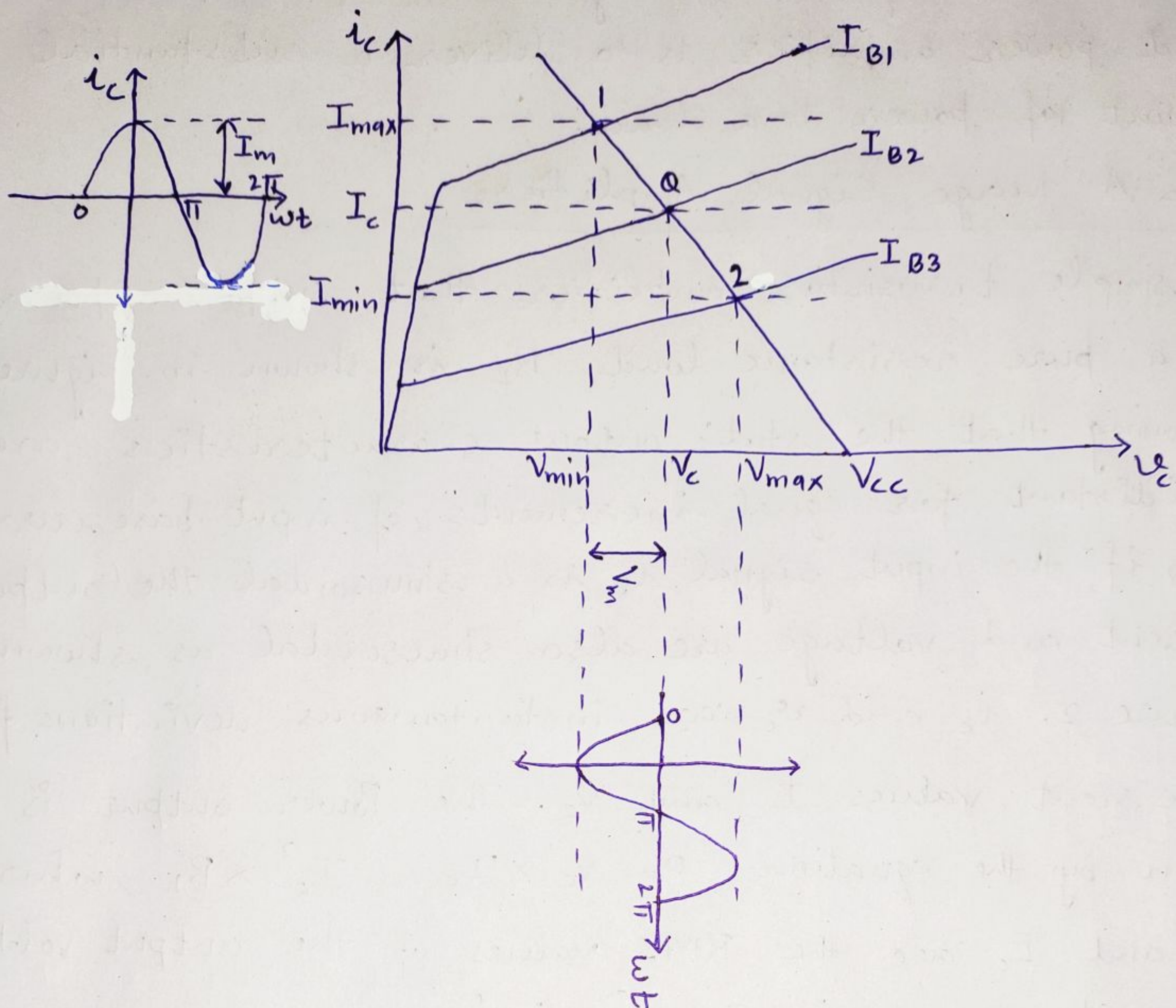


Figure 2. The output characteristics and the current and voltage waveforms for a series-fed amplifier.

Second - Harmonic Distortion

Since the dynamic transfer curve shown in Figure 3 is non-linear over the region of operation described by a parabolic equation, the output waveform differs from the input signal. Hence, this distortion is called non-linear or amplitude distortion. The output waveform now consists of fundamental and higher harmonics.

Harmonic distortion is caused by the non-linearity of the characteristic curve of an active device. The second-harmonic distortion is determined from the

dynamic transfer curve using the three-point method (3) for small signals. The relationship between alternating current i_c and the input excitation i_b is expressed by

$$i_c = K_1 i_b + K_2 i_b^2$$

where K_1 and K_2 are constants.

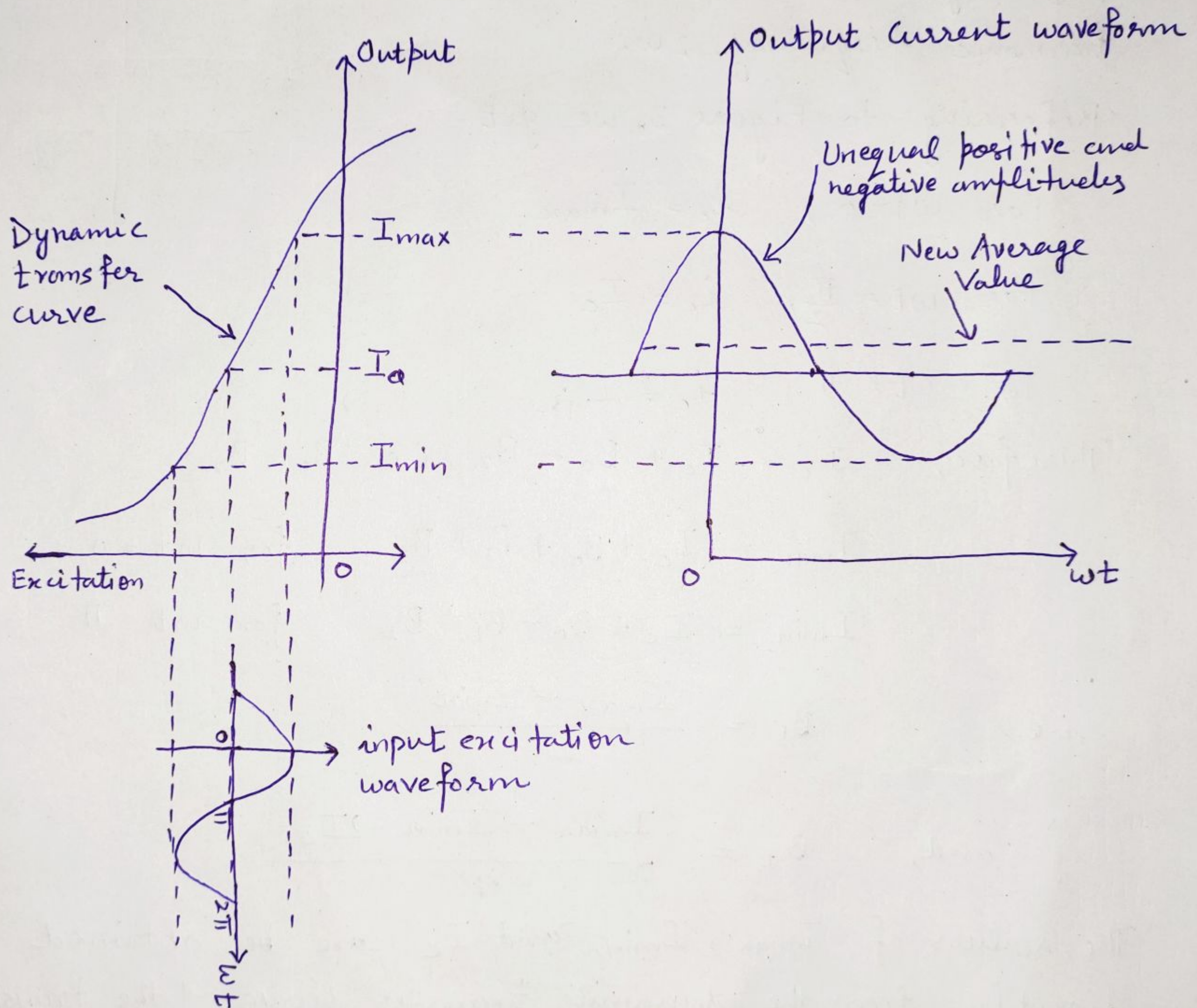


Figure 3. Dynamic transfer curve showing harmonic distortion.

Let the excitation be sinusoidal and expressed by

$$i_b = I_{bm} \cos \omega t. \text{ Therefore}$$

$$i_c = K_1 I_{bm} \cos \omega t + K_2 I_{bm}^2 \cos^2 \omega t$$

As $2 \cos^2 \omega t = 1 + \cos 2\omega t$, the instantaneous total current

i_c reduces to the form

$$i_c = I_c + B_0 + B_1 \cos \omega t + B_2 \cos 2\omega t$$

where I_c is the dc component of current, B_0 is the extra dc component due to rectification of the signal, B_1 is the amplitude of the desired signal at the fundamental frequency, ω , and B_2 is the amplitude of the second-harmonic frequency, 2ω .

Referring to Figure 3, we get

$$\text{For } \omega t = 0, \quad i_c = I_{\max}$$

$$\text{For } \omega t = \frac{\pi}{2}, \quad i_c = I_c$$

$$\text{For } \omega t = \pi, \quad i_c = I_{\min}$$

$$\text{Therefore, } I_c = I_c + B_0 - B_2, \text{ i.e. } B_0 = B_2$$

$$I_{\max} = I_c + B_0 + B_1 + B_2 \quad \text{for } \omega t = 0$$

$$I_{\min} = I_c + B_0 - B_1 + B_2 \quad \text{for } \omega t = \pi$$

$$\text{i.e. } B_1 = \frac{I_{\max} - I_{\min}}{2}$$

$$\text{and, } B_2 = \frac{I_{\max} + I_{\min} - 2I_c}{4}$$

The values of I_{\max} , I_{\min} , and I_c can be obtained directly from the dynamic transfer curve of the transistor and from the intersection of the load line drawn on the characteristic curves.

The second-harmonic distortion D_2 in percentage is defined as

$$D_2 = \frac{|B_2|}{|B_1|} \times 100\%$$

If $I_c = \frac{I_{\max} + I_{\min}}{2}$, then B_2 and B_0 are equal to zero. Hence there is no 2nd distortion.