Introduction to Communication Engineering SSY121, Lecture # 6

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Outline

- A Short Summary of Last Lecture
 - 1D and 2D Passband Transmission
 - Spectrum of a Train of Pulses
 - Constellations
- 2 MFR for 1D and 2D Modulations
 - 1D Modulations
 - 2D Modulations
- 3 Diagnostic Plots
 - Eye Diagram
 - Constellation Plots

Part I

A Short Summary of Last Lecture

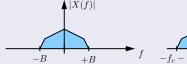
1D Passband Transmission

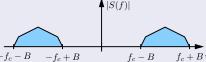
• The baseband signal x(t) is multiplied by a sinusoid of frequency f_c :

$$s(t) = x(t)\cos(2\pi f_c t)$$

• In frequency domain:

$$\begin{split} S(f) &= \mathcal{F}\{x(t)\cos{(2\pi f_c t)}\} = \mathcal{F}\{x(t)\} * \mathcal{F}\{\cos{(2\pi f_c t)}\} \\ &= X(f) * \frac{1}{2} \bigg[\delta(f - f_c) + \delta(f + f_c) \bigg] = \frac{1}{2} \bigg[X(f - f_c) + X(f + f_c) \bigg] \end{split}$$





The spectrum of a train of pulses

Consider the signal

$$s(t) = \sum_{k=0}^{\infty} a_k v(t - kT_s).$$

The linear modulation spectrum theorem (Theo. 2.3-1 in [p. 31, Anderson]) simply states that the spectrum of s(t) has the same form of the spectrum of the pulse v(t).

Consequences

The passband signal

$$s(t) = \sum_{k=0}^{\infty} a_k v(t - kT_s) \cos(w_c t)$$

- has a spectrum that is simply the spectrum of V(f) at $\pm f_c$,
- ullet has a BW that depends on the symbol period (See "Symbol rate BW tradeoff" in L_2)

The spectrum of BPSK with sinc and RRC pulses (from [Anderson])

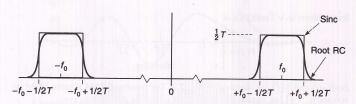


Figure 3.3 Idealized power spectral densities for BPSK for sine and root RC pulses; T = symbol time.

2D Passband Transmission

The transmitted signal will be of the form

$$s(t) = \sum_{k=0}^{\infty} a_k \phi_1(t - kT_s) + b_k \phi_2(t - kT_s),$$

$$\phi_1(t) = \sqrt{2}v(t)\cos(w_c t),$$

$$\phi_2(t) = \sqrt{2}v(t)\sin(w_c t),$$

where v(t) is a unit-energy baseband pulse

- Orthonormal basis: $||\phi_1(t)|| = ||\phi_2(t)|| = 1$ and $\langle \phi_1(t), \phi_2(t) \rangle = 0$
- ullet ISI-free transmission if v(t) is $T_{
 m s}$ -orthogonal:

$$\int_{-\infty}^{\infty} \phi_1(t)\phi_1(t-nT_s)dt = \int_{-\infty}^{\infty} \phi_2(t)\phi_2(t-nT_s)dt = 0,$$

$$\int_{-\infty}^{\infty} \phi_1(t)\phi_2(t-nT_s)dt = \int_{-\infty}^{\infty} \phi_2(t)\phi_1(t-nT_s)dt = 0,$$

for $n = \pm 1, \pm 2, ...$

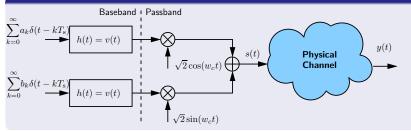
Passband signal for 2D modulations

• The passband signal for the 2D constellations can be written as

$$s(t) = \sqrt{2} \sum_{k=0}^{\infty} a_k v(t - kT_s) \cos(w_c t) + b_k v(t - kT_s) \sin(w_c t)$$

- Every point $(a_k,b_k)\in\mathbb{R}^2$ can be represented using an amplitude $A_k=\sqrt{a_k^2+b_k^2}$ and an angle $\psi_k=\arctan(b_k/a_k)$
- The 1D signals can be obtained by using $b_k = 0$.

2D Tx



Quaternary phase shift keying (QPSK)

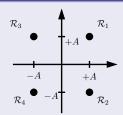
$$s_1(t) = +A\phi_1(t) + A\phi_2(t), \quad s_1 = [+A, +A]$$

$$s_2(t) = +A\phi_1(t) - A\phi_2(t), \quad s_2 = [+A, -A]$$

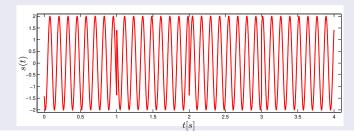
$$s_3(t) = -A\phi_1(t) + A\phi_2(t), \quad s_3 = [-A, +A]$$

$$s_4(t) = -A\phi_1(t) - A\phi_2(t), \quad s_4 = [-A, -A]$$

Constellation



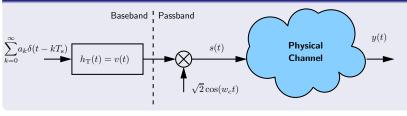
QPSK signal using square pulses



Part II

MFR for 1D and 2D Modulations





The transmitted signal

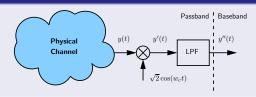
The passband signal for the 1D modulations can be written as

$$s(t) = \sqrt{2} \sum_{k=0}^{\infty} a_k v(t - kT_s) \cos(w_c t).$$

And the 1D Rx?

How do we design the 1D MFRx?

1D Rx



Why?

If the channel is good, we can assume $y(t) \approx s(t)$, and thus

$$y'(t) = \sqrt{2}y(t)\cos(w_{c}t) \approx \sqrt{2}s(t)\cos(w_{c}t)$$

$$= 2\sum_{k=0}^{\infty} a_{k}v(t - kT_{s})\cos^{2}(w_{c}t)$$

$$= \sum_{k=0}^{\infty} a_{k}v(t - kT_{s})\left[1 + \cos(2w_{c}t)\right]$$

$$= \sum_{k=0}^{\infty} a_{k}v(t - kT_{s}) + \sum_{k=0}^{\infty} a_{k}v(t - kT_{s})\cos(2w_{c}t)$$

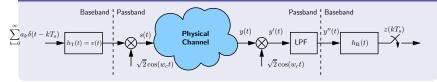
After the LPF

After the LPF, we obtain

$$y''(t) = \sum_{k=0}^{\infty} a_k v(t - kT_s),$$

which is an expression we have seen before, haven't we?

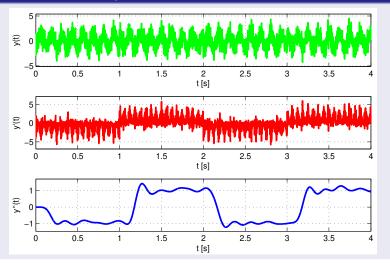
1D Tx and Rx



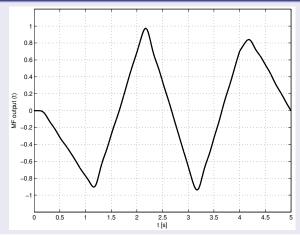
The selection of $h_{\rm R}(t)$?

How do we choose the impulse response of the Rx filter?

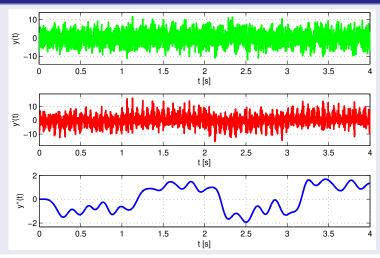
BPSK Receiver and a good channel



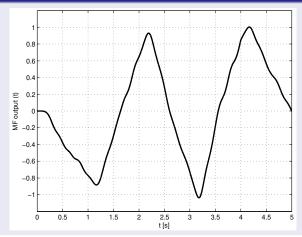
Matched filter's output



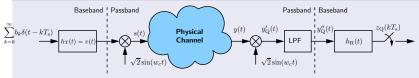
BPSK Receiver and a bad channel



Matched filter's output



Quadrature component in 2D Rx



If the channel is good, we can assume $y(t) \approx s(t)$, and thus

$$y_{\mathbf{Q}}'(t) \approx \left[\sqrt{2} \sum_{k=0}^{\infty} a_k v(t - kT_{\mathbf{s}}) \cos(w_c t) + b_k v(t - kT_{\mathbf{s}}) \sin(w_c t) \right] \sqrt{2} \sin(w_c t)$$

$$= 2 \sum_{k=0}^{\infty} a_k v(t - kT_{\mathbf{s}}) \cos(w_c t) \sin(w_c t) + 2 \sum_{k=0}^{\infty} b_k v(t - kT_{\mathbf{s}}) \sin^2(w_c t)$$

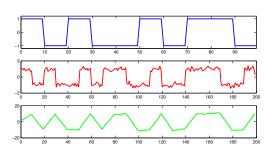
$$= \sum_{k=0}^{\infty} a_k v(t - kT_{\mathbf{s}}) \sin(2w_c t) + \sum_{k=0}^{\infty} b_k v(t - kT_{\mathbf{s}}) \left[1 - \sin(2w_c t)\right]$$

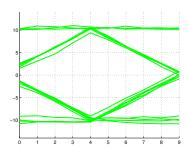
$$= \sum_{k=0}^{\infty} b_k v(t - kT_{\mathbf{s}}) + \sum_{k=0}^{\infty} (a_k - b_k) v(t - kT_{\mathbf{s}}) \sin(2w_c t)$$

HW: The inphase component for 2D Rx: $y_1'(t) = y(t)\sqrt{2}\cos(w_c t)$?

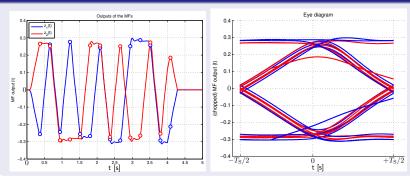
Eye Diagram

- Study the output of the MF (before sampling)
- Chop it in segments of length $T_{\rm s}$
- Overlay the segments





MF's output and Eye Diagram

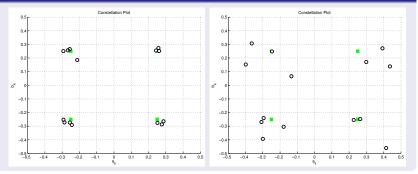


Why are eye diagrams important?

Because it illustrates

- The best sampling instant
- The ability to separate the signal alternatives
- The sensitivity to synchronization errors

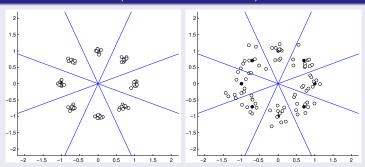
Constellation Plot QPSK (Good and Bad Channel)



Constellation Plots

- Study the samples of the MFs
- Let the sampled values at a given time be the coordinates of a point
- Plot those points for a large number of samples

Constellation Plot 8PSK (Good and Bad Channel)



Why are constellation plots important?

Because it illustrates

- The energy of the signal alternatives
- How reliable the outputs of the MFs are (distances between the constellation points)
- It shows how much the channel affects the decisions

Today's Summary

- 1D and 2D Passband Transmission
- Spectrum of Pulses
- 1D and 2D MFRx
- Eye Diagrams
- Constellation Plots
- Constant Envelope Modulations (FSK or CPFSK) and PA