

Advanced Analysis Methods and Simulation tools for Noise in VCOs and PLLs

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Outline

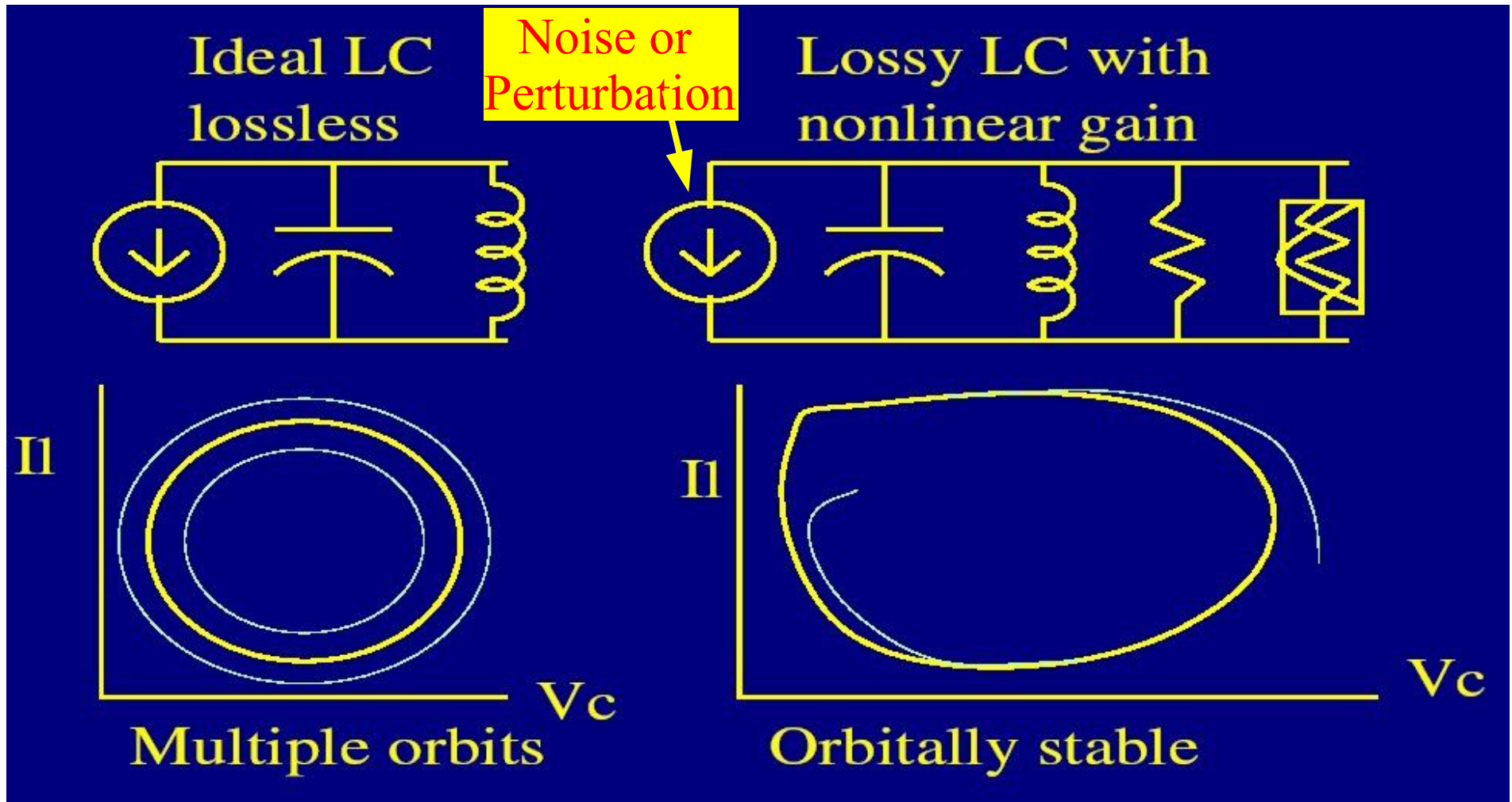
- Basics of oscillator operation
- Perturbation analysis of oscillators: the PPV/NISF
- Phase noise and jitter basics
- Injection locking
- Oscillator/PLL jitter due to interference noise
- Phase noise examples and design guidelines
- PLL noise analysis and examples

Basic Features of Oscillator Operation

Why Oscillators are a Special Simulation Challenge

- **Computation/size/accuracy**: much greater than for amps/mixers
 - long startups, tiny timesteps needed
 - inefficient for even 1-transistor oscillators
 - integrated RF: 100s to 1000s of transistors
 - errors dependent on size of timesteps, integration method, ...
 - fundamental cause: **marginal phase stability** of all oscillators
 - numerical errors integrate over time
- Using SPICE directly for oscillator phase simulation should be avoided if you have alternatives

Amplitude Stability and Nonlinearity

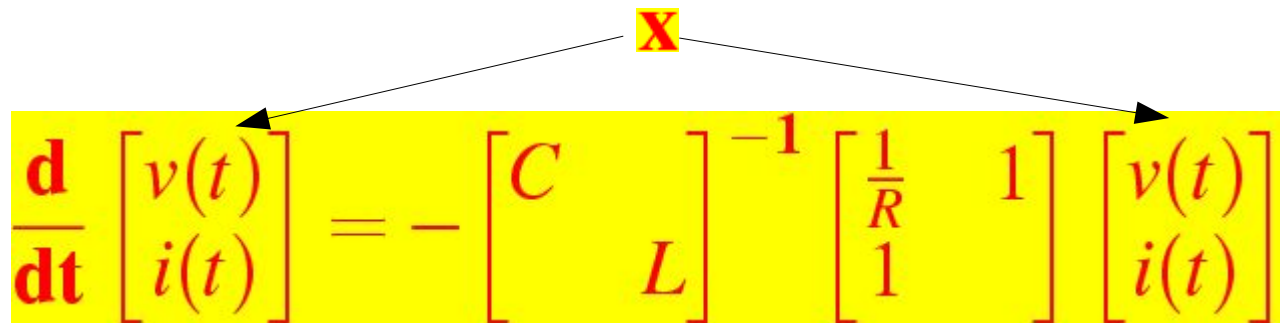


For **quantitative analysis**: nonlinearity cannot be ignored –
fundamental to oscillator operation

Perturbation Analysis of Oscillators

Quantitative Perturbation Analysis

- Mathematically, circuits are nonlinear differential equations
 - Eg, for an RLC tank (using KCL and KVL):



The diagram shows a yellow box containing the differential equation for an RLC tank circuit. Above the box, the state vector \mathbf{x} is shown in a yellow box. Two arrows point from \mathbf{x} to the variables $v(t)$ and $i(t)$ in the vector on the right side of the equation.

$$\frac{d}{dt} \begin{bmatrix} v(t) \\ i(t) \end{bmatrix} = - \begin{bmatrix} C & \\ & L \end{bmatrix}^{-1} \begin{bmatrix} \frac{1}{R} & 1 \\ 1 & \end{bmatrix} \begin{bmatrix} v(t) \\ i(t) \end{bmatrix}$$

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x})$$

Quantifying Oscillator Response

How does the oscillator (VCO) respond to “inputs”?

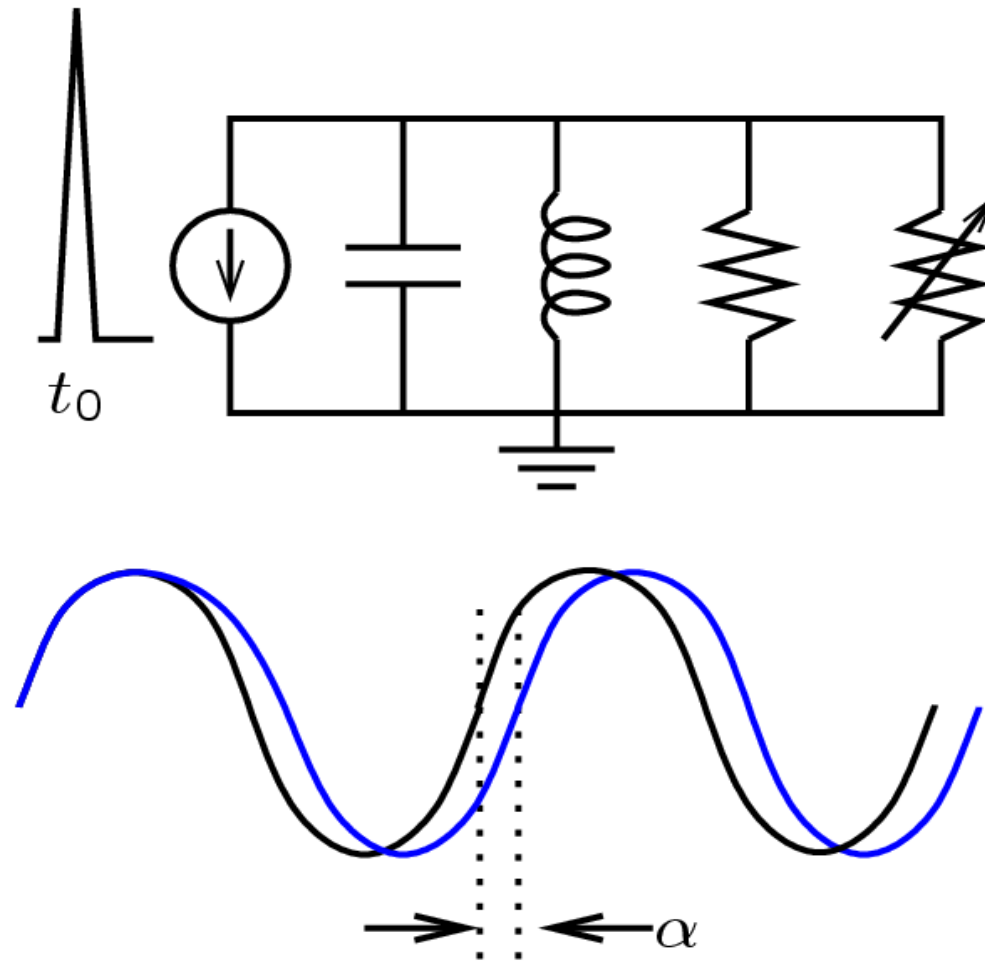
$$\dot{x}(t) = f(x) + \underbrace{b(t)}_{\text{input perturbation}}$$

■ No perturbation \Rightarrow perfect periodic solution $x_s(t)$

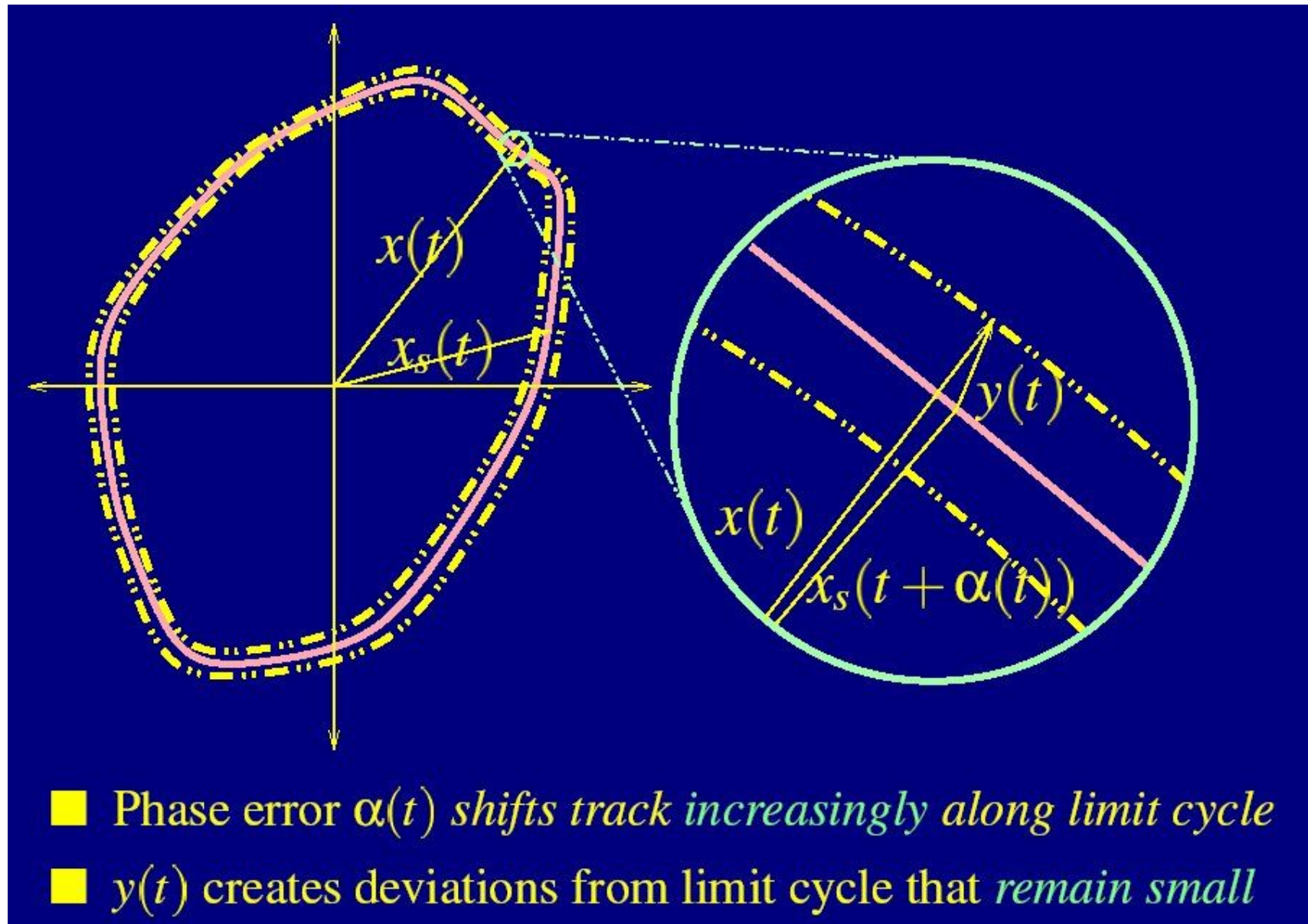
■ Small $b(t)$ perturbation:

$$x(t) = x_s\left(t + \underbrace{\alpha(t)}_{\text{growing phase error}}\right) + \underbrace{y(t)}_{\text{small}}$$

Phase Response to Delta Function



Oscillator: Response to “Inputs”



Nonlinear Differential Equation for Phase

$$\dot{\alpha} = \mathbf{v}_1^T(\mathbf{t} + \alpha(\mathbf{t})) \cdot \mathbf{b}(\mathbf{t})$$

- Simple differential equation governs phase
 - **nonlinear** (because PPV is **periodic**)
 - **scalar** (much smaller than oscillator equations)

[Demir Mehrotra Roychowdhury 97, 98, 01]

The Perturbation Projection Vector (PPV): a Nonlinear ISF (NISF)

- $v_1(t)$: **“nonlinear transfer or sensitivity function”**
relating “input” to oscillator phase response
 - (via nonlinear differential equation on previous slide)
 - $v_1(t)$: the PPV (Perturbation Projection Vector) or NISF (nonlinear ISF)
- In general, PPV/NISF does NOT equal the tangent vector of the phase plane plot
 - ie, **not equal to the ISF** [Hajimiri 98]
 - but **intuition is similar**: sensitivity of phase/jitter to external perturbations as a function of time

PPV/NISF vs the ISF

- Similarities

- PPV/NISF and ISF identical for high-Q negative resistance oscillators
- (still important to use the NONLINEAR phase equation)

- Differences

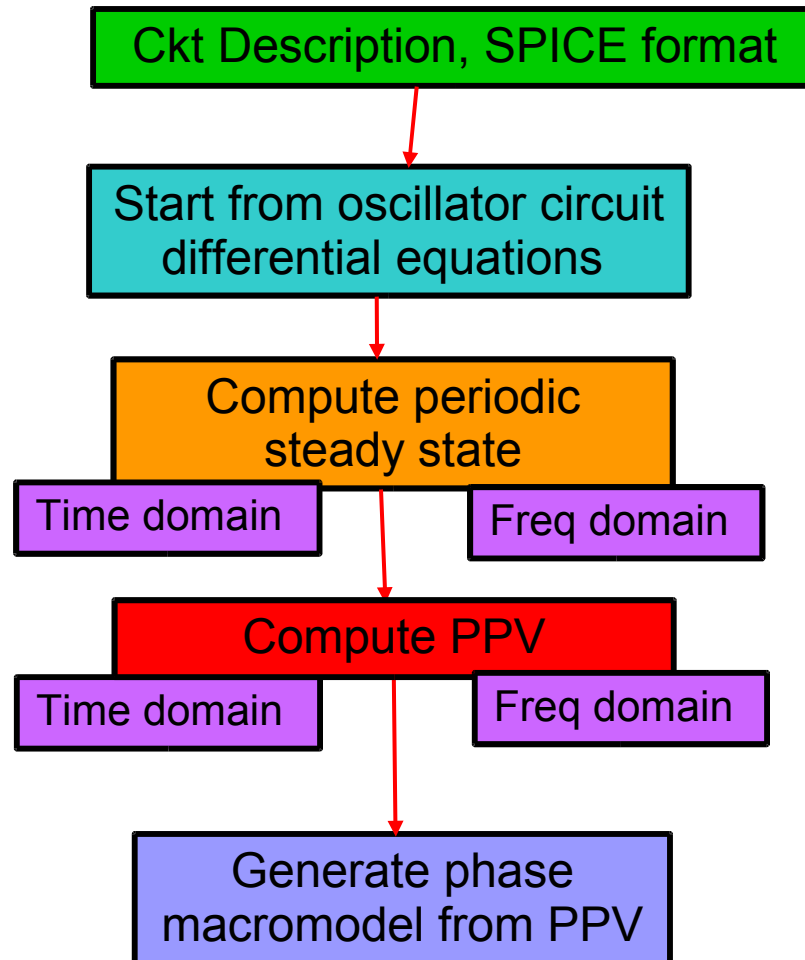
- PPV/NISF and ISF are **NOT IDENTICAL** for most other oscillators, including ring oscillators
- Applications where the **difference matters** (greatly):
 - Phase noise/jitter due to random noise
 - Injection locking
 - Jitter from interference noise (power/ground noise)

Computing the PPV/NISF

- PPV/NISF can be computed efficiently from oscillator steady-state quantities
 - Find the periodic steady-state of oscillator
 - using, eg, HB, shooting, etc.
 - Various matrix computations
 - can be performed efficiently for large oscillators

[Demir Roychowdhury TCAD 03]

PPV/NISF: Computation Techniques



Phase Noise and Jitter

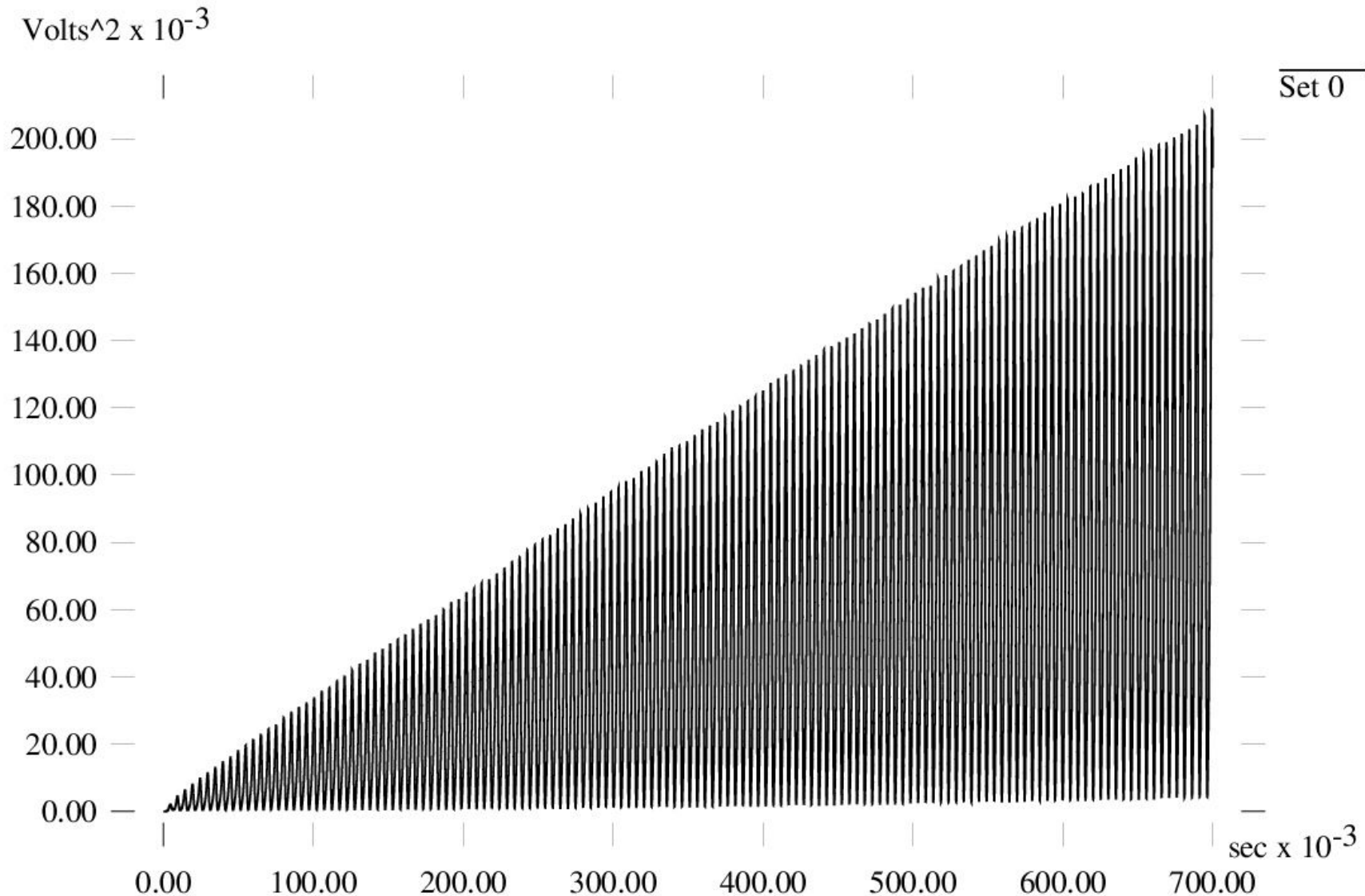
Using the PPV/NISF to find jitter and phase noise spectrum

- Noise: perturbation to oscillator comes from **thermal, shot, flicker noise** sources
 - $b(t)$ is **random** (eg, white Gaussian)
 - Now concerned with **noise power** (a.k.a noise variance)
- Phase deviation $\alpha(\tau)$ now also random
 - Variance = $E[\alpha^2(\tau)]$ is **mean-squared jitter**

Mean-squared Jitter

- Key result: mean-squared jitter grows linearly with time
 - $E[\alpha^2(\mathbf{t})] = \mathbf{c}t$
 - (technically: random walk or Brownian motion)
 - **c: growth rate of mean-squared jitter**
 - Crucial scalar parameter
 - Depends on PPV/NISF and device (thermal/shot/etc) noises
 - Expression available for c [Demir et al TCAS-1 2000]

Linear rise of mean-square jitter: Monte-Carlo simulation

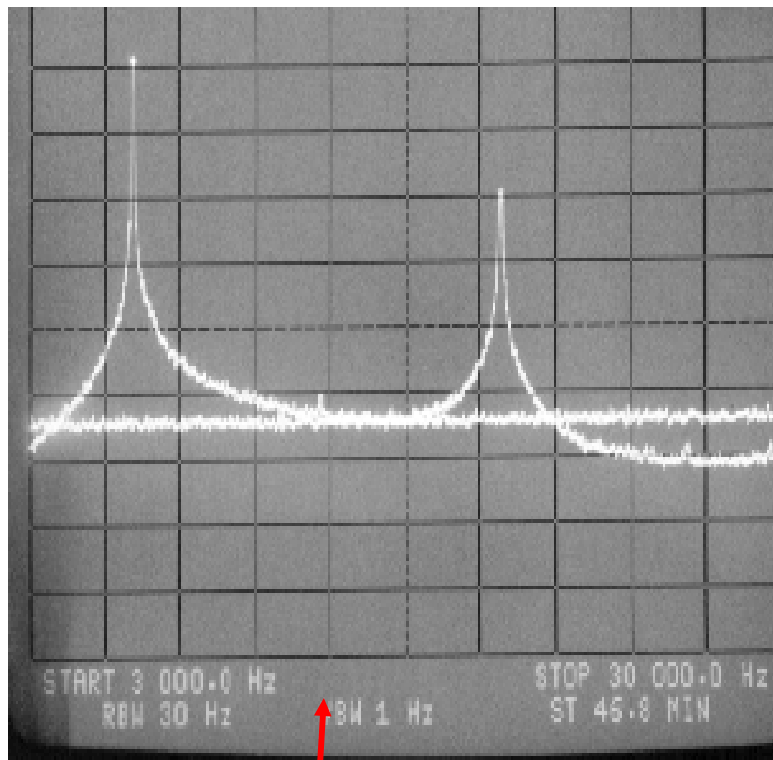


Phase Noise Spectrum

- **Measured spectrum** is of voltage/current
 - of, eg, $\sin(\omega t + \alpha(t))$; not of the phase $\alpha(t)$ itself!
- Spectrum is directly related to jitter growth-rate c
- Shape is **Lorenzian** – broadens as c increases
 - No explosion at center frequency

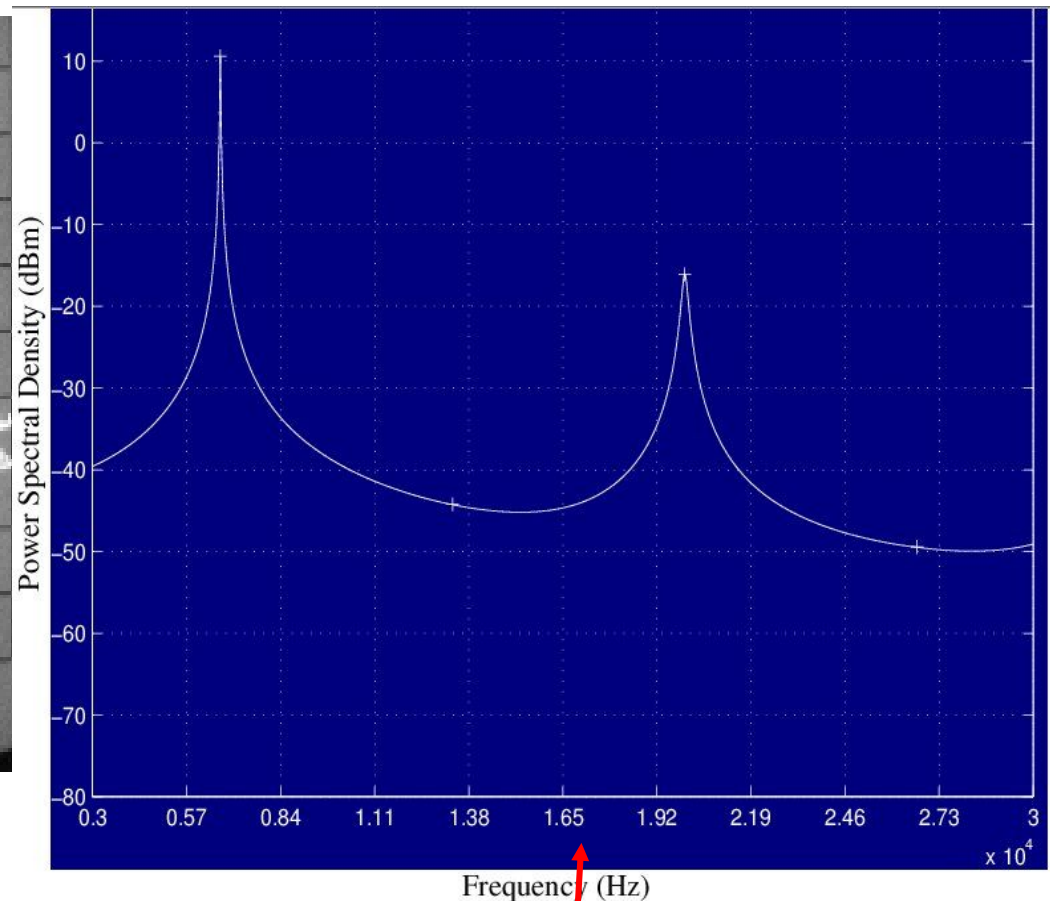
Spectrum Does Not Explode at Carrier

PPV/NISF-based nonlinear theory resolves contradiction in Leeson's model



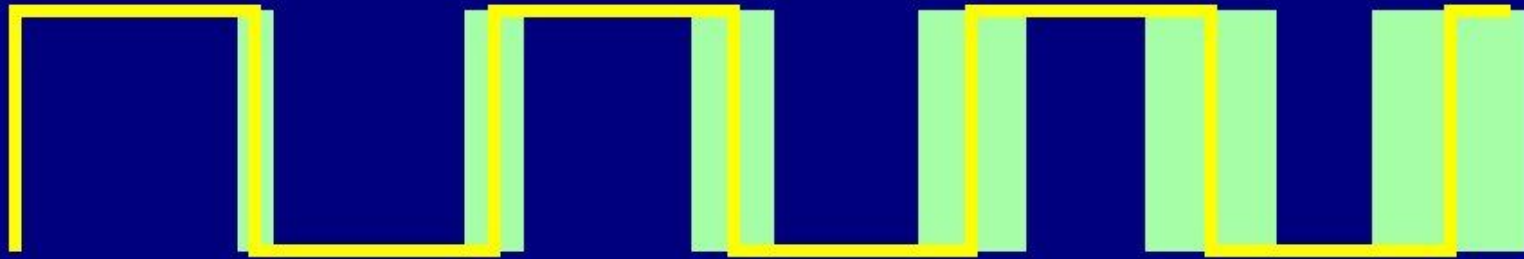
Measured

[Toth TCAS-1 1992]

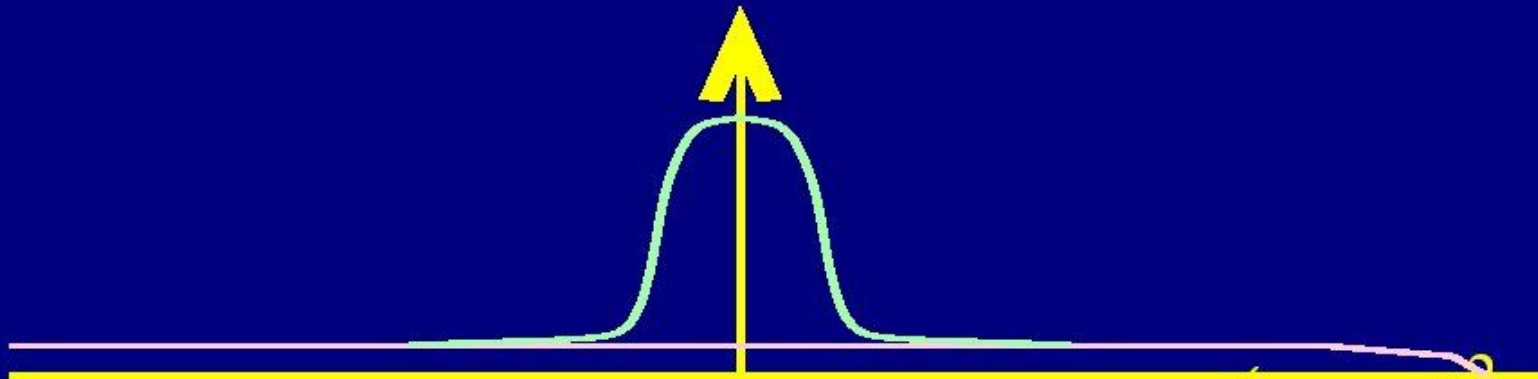


Computed from PPV

Timing Jitter and Phase Noise Spectrum



■ Timing jitter variance (per cycle) = cT



■ *Lorenzian spectrum:* $\mathcal{L}(f_m) = 10 \log_{10} \left(\frac{f_0^2 c}{\pi^2 f_0^4 c^2 + f_m^2} \right)$

Injection Locking

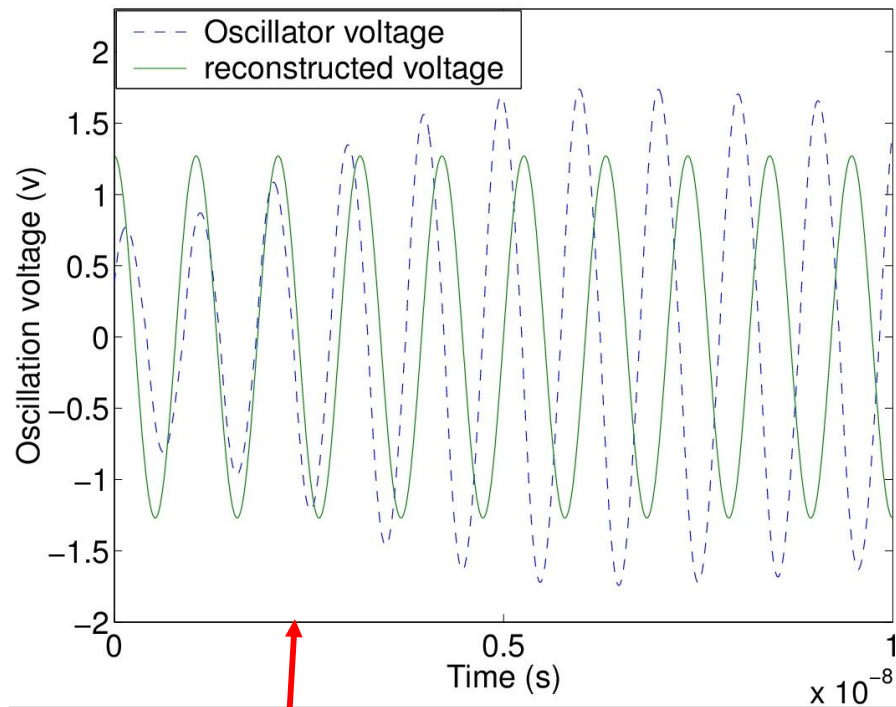
Injection Locking in Oscillators

- Oscillator's frequency “**locks**” to frequency of external input
 - external frequency “**over-rides**” oscillator natural frequency
 - if frequencies close enough, even if input is very small
- **Universal** phenomenon: **grandfather clocks, fireflies** flashing, **lasers**, etc
- Impact: can be both good and bad
 - exploited in RF/mixed-signal design
 - undesired locking due to parasitic coupling a concern
- Can take extremely long to simulate in SPICE

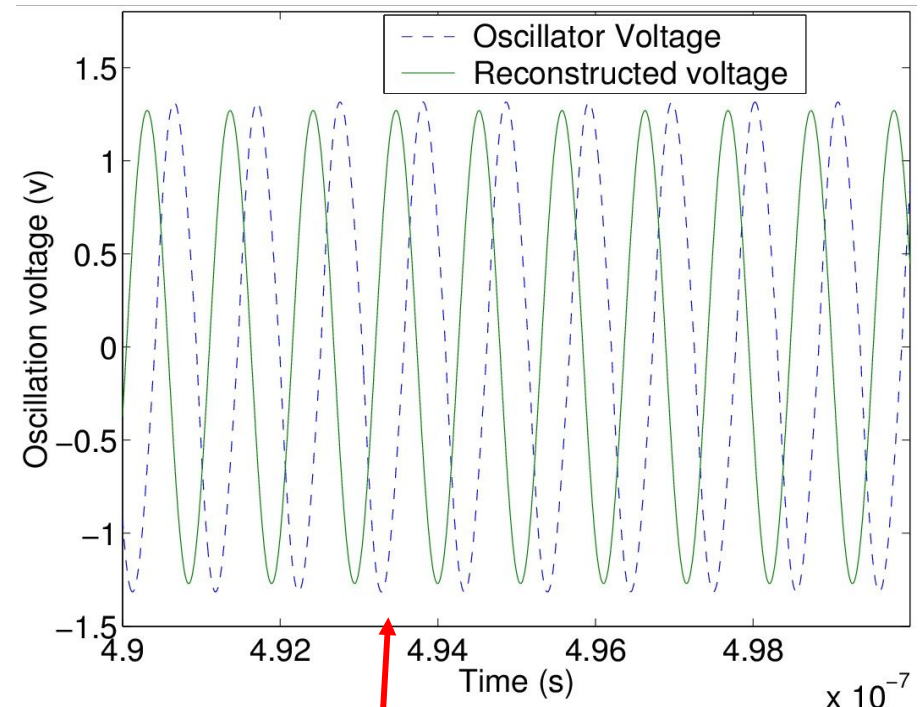
Predicting Injection Locking

- Find nonlinear phase error $\alpha(t)$ due to $b(t)$
 - $b(t)$ is now the deterministic injection signal
 - Use the nonlinear differential equation based on PPV/NISF to calculate $\alpha(t)$
 - Linear equations don't work: injection locking is a fundamentally nonlinear phenomenon
 - If $\alpha(t) = (w_1 - w_0)t$, the oscillator is **injection locked**
- Much faster/more accurate than SPICE simulation

Colpitts Oscillator: Injection Locking



Initially unlocked



Eventually Locked

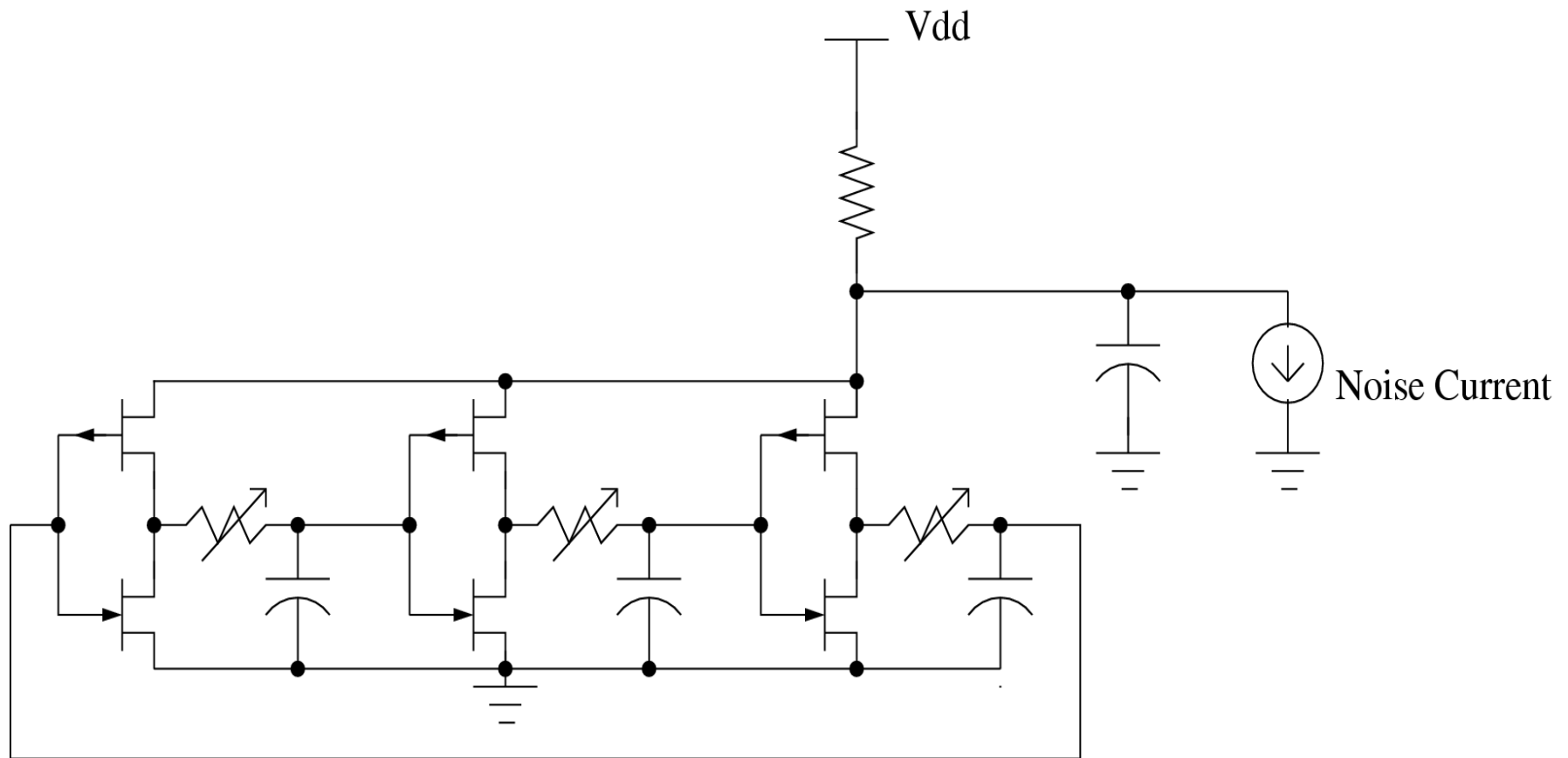
Full (SPICE) simulation, vs waveform reconstructed from $\alpha(t)$
(2 orders of magnitude speedup)

Jitter Induced by Power/Ground Noise

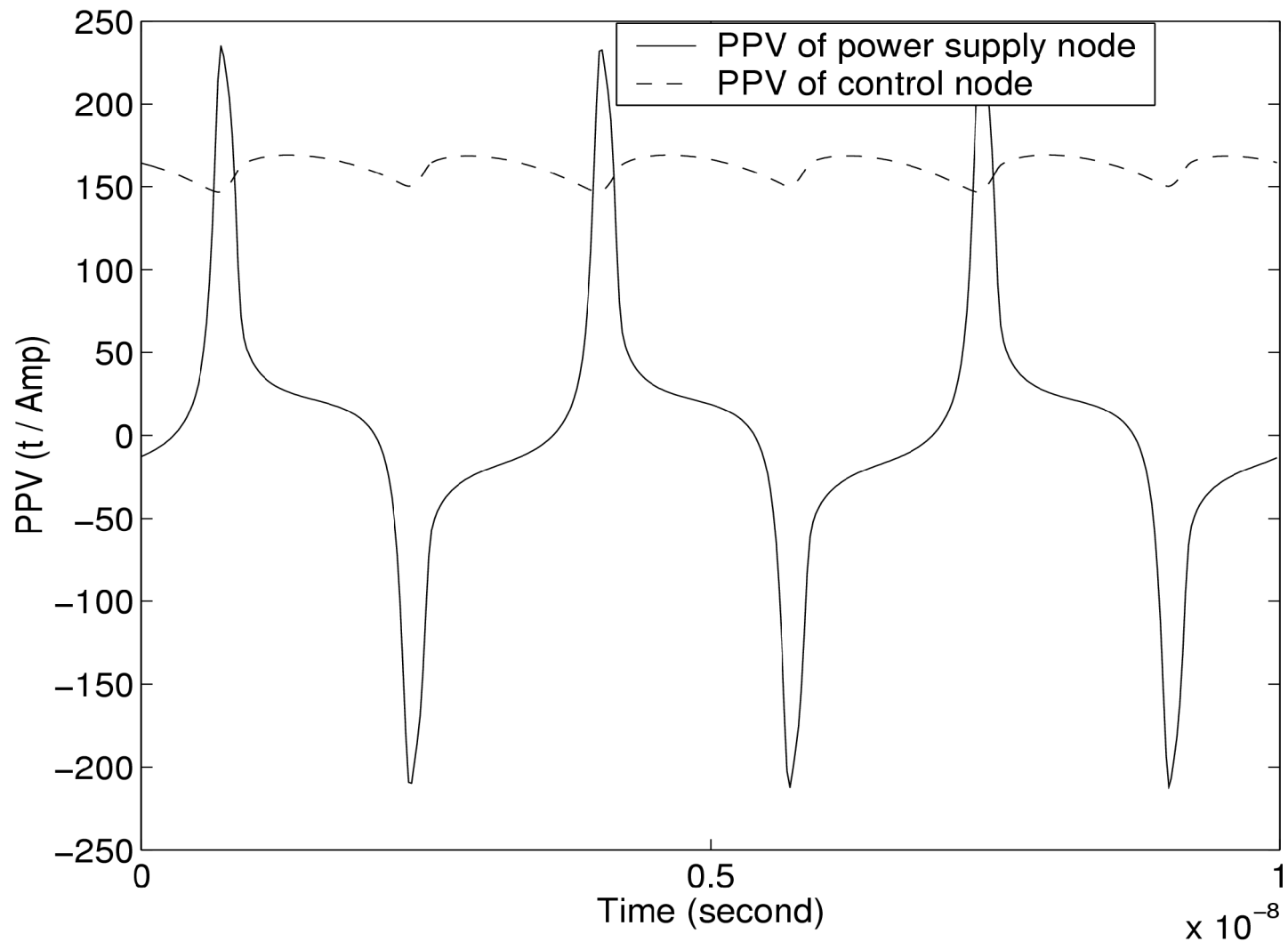
Interference: “Deterministic Noise”

- Power/ground noise: not “truly” random
 - caused by interference from other circuits
 - **not Gaussian, not stationary**: “spikes” of noise
 - can be relatively large (15-20% of VDD)
- Use **nonlinear phase equation** (again)
 - deterministic input
 - PPV component supplies **design insight**

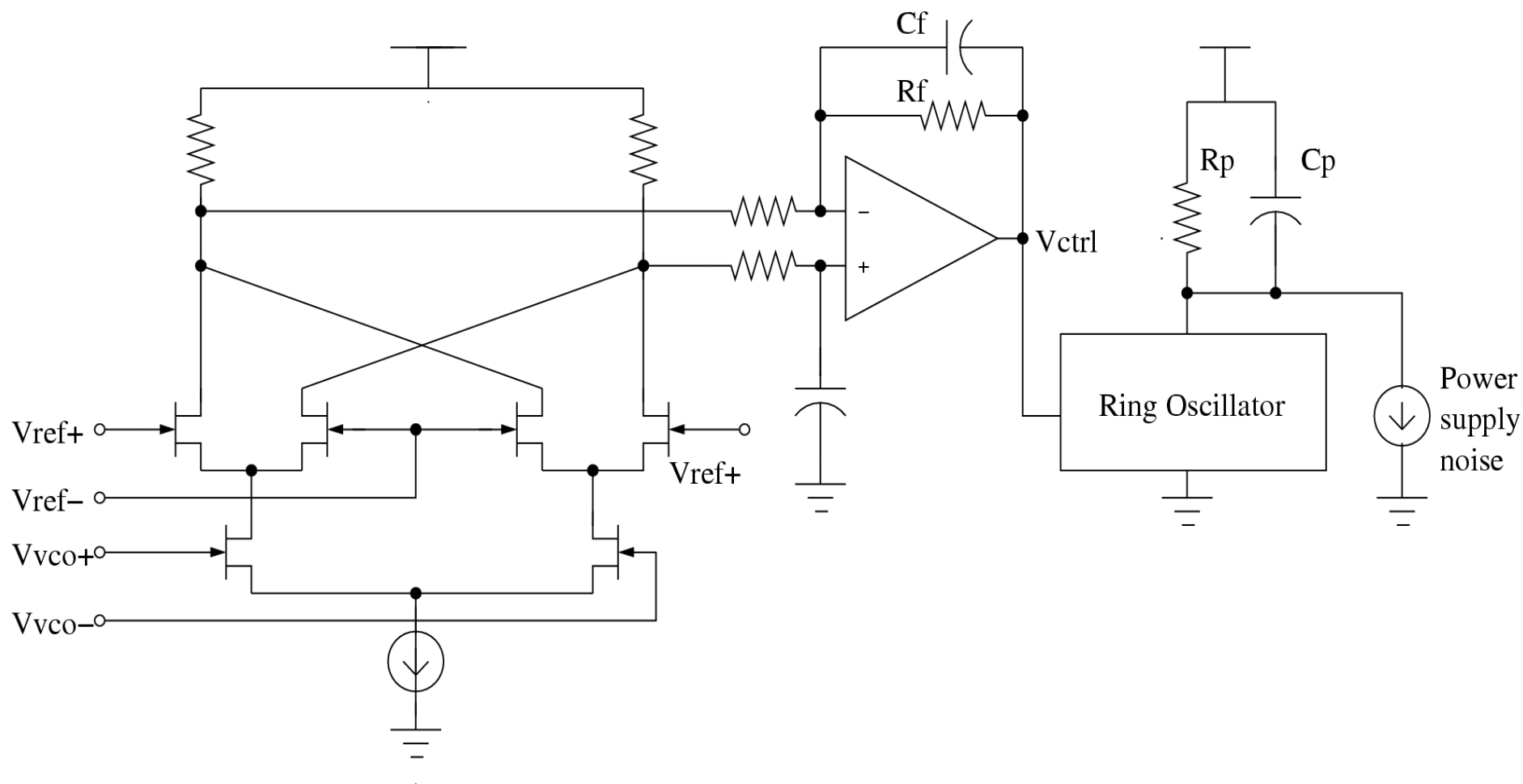
Example: Simple Ring-Oscillator VCO



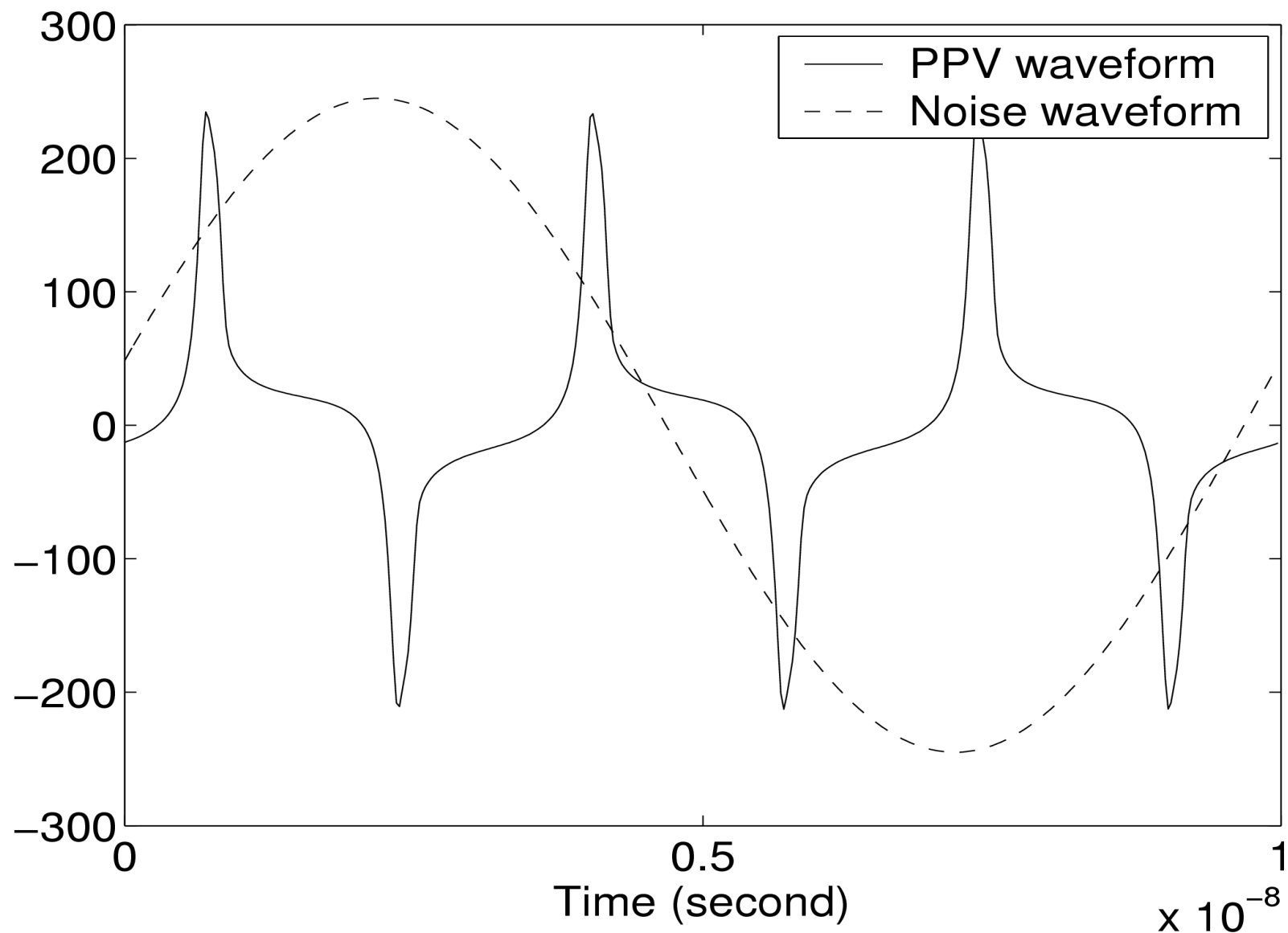
VCO Perturbation Projection Vectors: Control Node and Power Supply Components



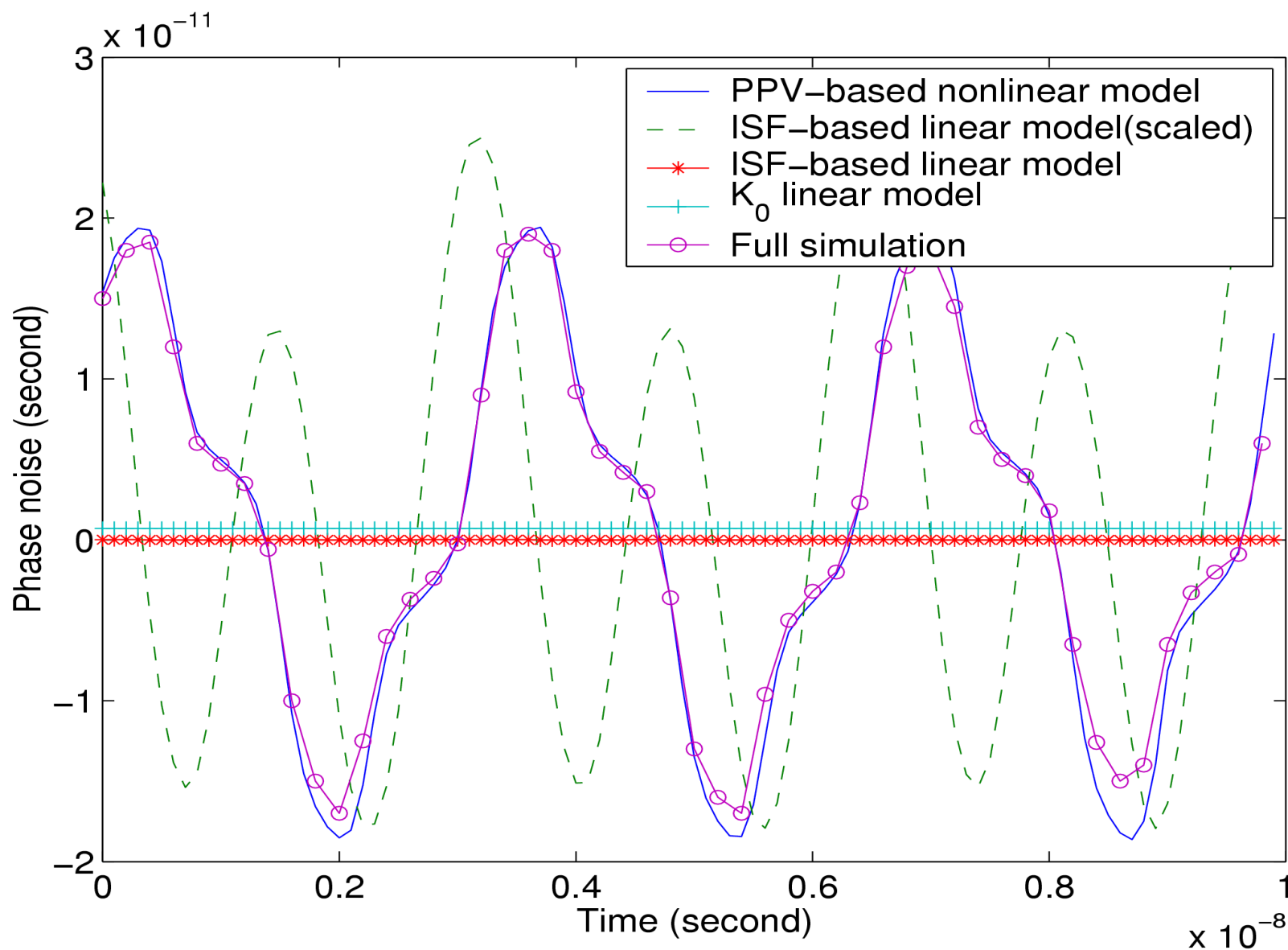
Simple Ring-Oscillator-based Phase-Locked Loop



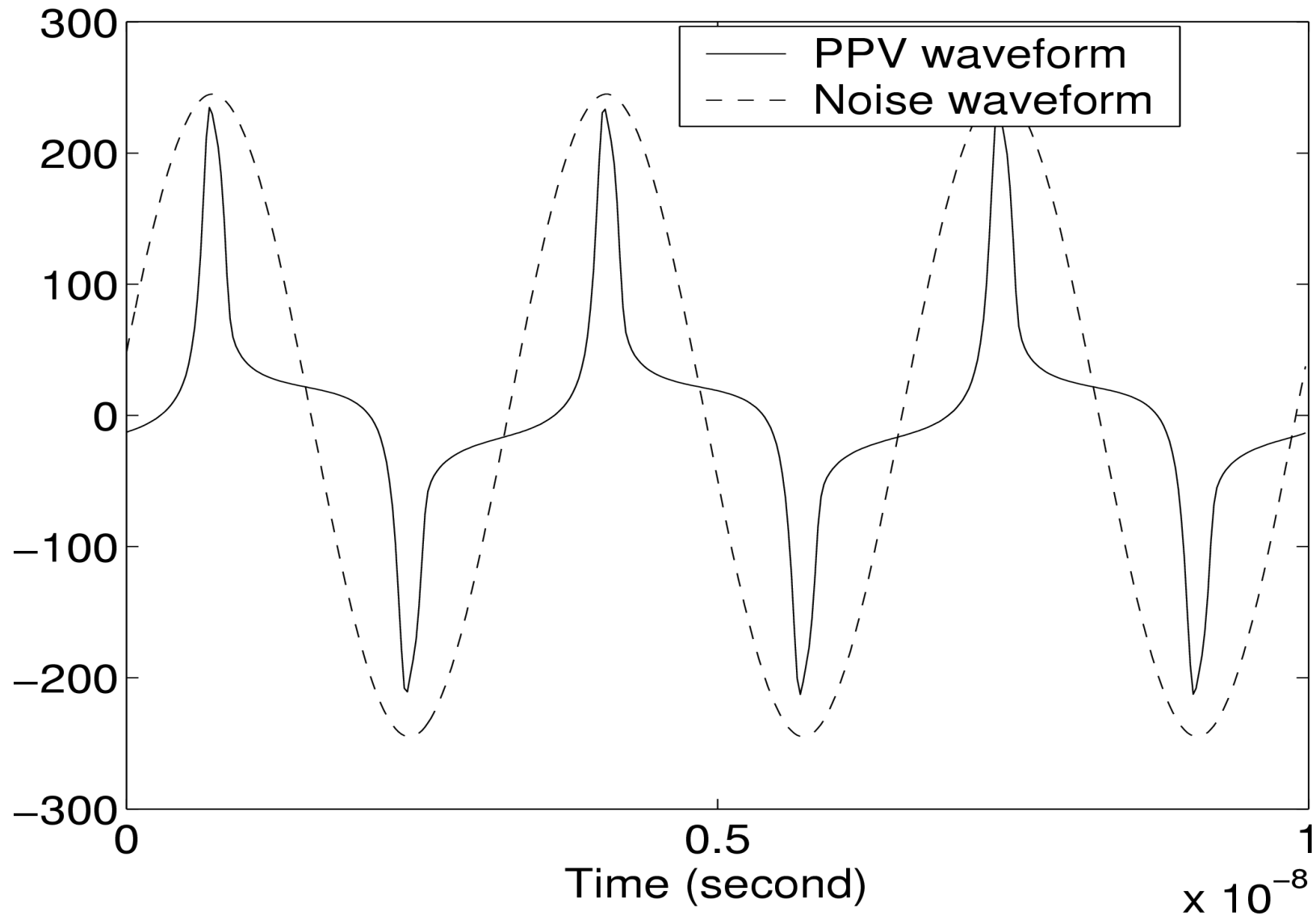
Expected Impact of 1st harmonic Supply Noise



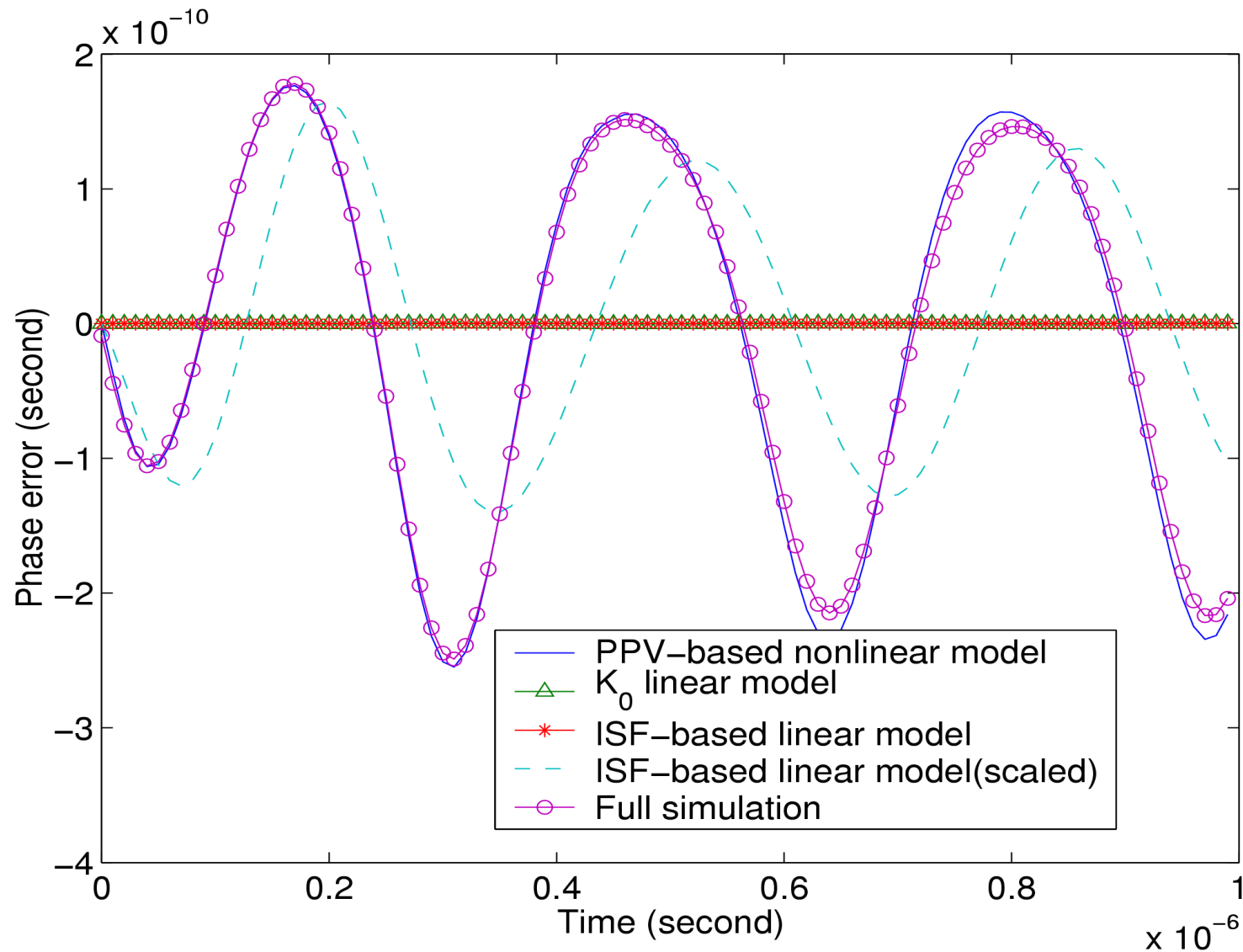
PLL Phase Reponse to Periodic Supply Noise



Expected Impact of 3rd Harmonic Supply Noise



3rd Harmonic Supply Noise: Phase Macromodel vs Full PLL simulation



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