

Integration of Convection/Diffusion Equations

• So far ...

→ 1st order convection equations (Hyperbolic)

Example: "Linear Convection Equation"

→ Diffusion equations (Parabolic)

Example: "Heat Equation"

• In the presence of both convection & diffusion phenomena, a combined equation is in general parabolic. Example: "Boundary Layer Equations"

• A simpler model equation is the viscous Burgers' equation

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} = \nu \frac{\partial^2 u}{\partial x^2} \quad (1)$$

• Equation (1) was derived to study the internal structure of a weak normal shock in the near-sonic regime.

- The velocity $u(x,t)$ represents the perturbation from a uniform sonic stream ; $u=0$ corresponds to the sonic condition.
- As the equation is parabolic, initial- and boundary conditions must be added to the problem.
- A steady-state, i.e. $\partial u / \partial t \rightarrow 0$, is reached when convection and diffusion are in balance.
- For the following boundary conditions

$$\begin{cases} u(0,t) = u_0 \\ u(L,t) = 0 \end{cases}$$

(2)

an exact steady solution to (1) is given by

$$u(x) = u_0 \bar{u} \frac{1 - e^{-\bar{u} Re_L (1 - \frac{x}{L})}}{1 + e^{-\bar{u} Re_L (1 - \frac{x}{L})}}$$

(3)

where \bar{u} is defined through

$$\frac{\bar{u} - 1}{\bar{u} + 1} = e^{-\bar{u} Re_L} \quad (4)$$

and

$$Re_L = \frac{u_0 L}{\nu} \quad (5)$$

is sort of a Reynolds number defined by the shock width and describes the ratio of convection to diffusion.

• Two limiting cases:

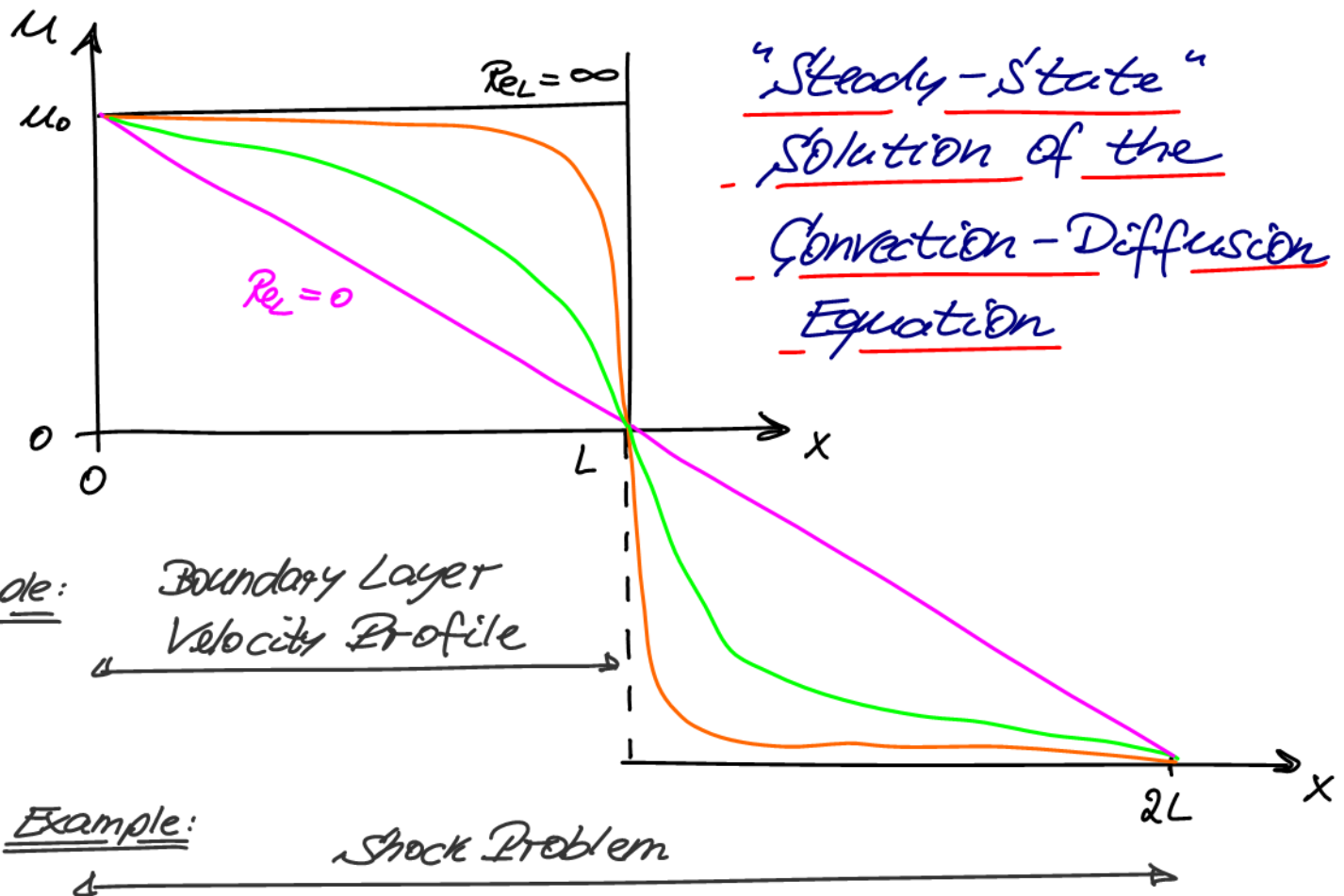
a.) $Re_L \rightarrow 0$

$$\bar{u} \approx \sqrt{\frac{2}{Re_L}} ; u(x) = u_0 \left(1 - \frac{x}{L}\right)$$

b.) $Re_L \rightarrow \infty$

$$\bar{u} \rightarrow 1 \Rightarrow \text{Singular} \\ \text{inviscid} \\ \text{limit}$$

$$\left. \begin{array}{l} u(x) = u_0 \\ u(L) = 0 \end{array} \right\}$$



- One can also devise a simpler model problem, i.e. the linearized Burger's equation

$$\frac{\partial u}{\partial t} + c \frac{\partial u}{\partial x} = \nu \frac{\partial^2 u}{\partial x^2} \quad (6)$$

It can be shown that in this case $\bar{u} = 1$ and that the exact steady-state solution is given by

$$u(x) = u_0 \frac{1 - e^{-Re_L(1-\frac{x}{L})}}{1 - e^{-Re_L}} \quad (7) \quad Re_L = \frac{cL}{\nu} \quad (8)$$

FTCS Method

[Roach, 1972]

FTCS $\hat{=}$ Forward-in-Time and
Centered-in-Space

$$\frac{u_i^{n+1} - u_i^n}{\Delta t} + c \frac{u_{i+1}^n - u_{i-1}^n}{2\Delta x} = \nu \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta x^2} \quad (9)$$

- The analysis of the truncation error TE is straight forward about (ϵ, n)

$$\begin{aligned} \epsilon_i^n &= \cancel{\frac{\partial u_i^n}{\partial t}} + \left(\frac{\Delta t}{2}\right) \frac{\partial^2 u_i^n}{\partial t^2} + \mathcal{O}(\Delta t^2) \\ &+ c \left(\cancel{\frac{\partial u_i^n}{\partial x}} + \left(\frac{\Delta x^2}{3!}\right) \frac{\partial^3 u_i^n}{\partial x^3} + \mathcal{O}(\Delta x^4) \right) \\ &- \nu \left(\cancel{\frac{\partial^2 u_i^n}{\partial x^2}} + \left(\frac{\Delta x^2}{4!}\right) \frac{\partial^4 u_i^n}{\partial x^4} + \mathcal{O}(\Delta x^4) \right) = \mathcal{O}(\Delta t, \Delta x^2) \end{aligned}$$

\Rightarrow The FTCS scheme is consistent and 1st order accurate in time and second order accurate in space.

• Stability:

$$u_i^n = g^n e^{\xi i \beta} \quad (10)$$

Bring (9) in update form ...

$$u_i^{n+1} = u_i^n - \underbrace{\frac{1}{2} \frac{C \Delta t}{\Delta x}}_{\delta} (u_{i+1}^n - u_{i-1}^n) + \underbrace{\frac{V \Delta t}{\Delta x^2}}_{\tau} (u_{i+1}^n - 2u_i^n + u_{i-1}^n)$$

$$g^{n+1} e^{\xi i \beta} = g^n e^{\xi i \beta} - \frac{1}{2} \delta (g^n e^{\xi (i+1) \beta} - g^n e^{\xi (i-1) \beta}) + \tau (g^n e^{\xi (i+1) \beta} - 2 g^n e^{\xi i \beta} + g^n e^{\xi (i-1) \beta})$$

Divide by $u_i^n = g^n e^{\xi i \beta}$

$$g = 1 - \frac{1}{2} \delta (e^{\xi \beta} - e^{\xi (-\beta)}) + \tau (e^{\xi \beta} - 2 + e^{\xi (-\beta)})$$

$$g = 1 - \frac{1}{2} \delta (\cancel{\cos \beta} + \xi \cancel{\sinh \beta} - \cancel{\cos(-\beta)} - \xi \cancel{\sinh(-\beta)}) + \tau (\cancel{\cos \beta} + \xi \cancel{\sinh \beta} - 2 + \cancel{\cos(-\beta)} + \xi \cancel{\sinh(-\beta)})$$

$$g = 1 - \xi \delta \sinh \beta - 2\tau (1 - \cos \beta)$$

$$g = [1 - 2\tau(1 - \cos\beta)] - i \delta \sin\beta$$

$$\|g\|^2 = [1 - 2\tau(1 - \cos\beta)]^2 + \delta^2 \sin^2\beta$$

$$\|g\|^2 = 1 - 4\tau(1 - \cos\beta) + 4\tau^2(1 - \cos\beta)^2 + \delta^2(1 - \cos^2\beta)$$

$$\|g\|^2 = 1 - 4\tau(1 - \cos\beta) + 4\tau^2(1 - \cos\beta)^2 + \delta^2(1 - \cos\beta)(1 + \cos\beta)$$

$$\|g\|^2 = 1 + [4\tau^2(1 - \cos\beta) - 4\tau + \delta^2(1 + \cos\beta)](1 - \cos\beta)$$

$$\|g\|^2 = 1 + [8\tau^2 - 4\tau + (\delta^2 - 4\tau^2)(1 + \cos\beta)](1 - \cos\beta)$$

• Remember that the scheme will be stable if (11)

$$\|g\|^2 \leq 1 \quad \forall \alpha$$

i) $\delta^2 - 4\tau^2 \leq 0$

worst case $\Rightarrow \cos\beta = -1$

$$8\tau^2 - 4\tau = 4\tau(2\tau - 1) \leq 0$$

$$\Rightarrow \boxed{2\tau \leq 1} \Rightarrow \boxed{\delta^2 \leq 1} \quad (12)$$

$$ii) \quad \underline{\tau^2 - 4\tau \geq 0}$$

$$\text{Worst case} \Rightarrow \cos \beta = 1$$

$$\cancel{8\tau^2} - 4\tau + 2(\cancel{\tau^2 - 4\tau^2}) \leq 0$$

$$-4\tau + 2\tau^2 \leq 0$$

$$\boxed{\tau^2 \leq 2\tau} \quad (13)$$

- Combinations of the conditions (12), (13) yields the stability condition for the FTC's scheme as

$$\boxed{\tau^2 \leq 2\tau \leq 1} \quad (14)$$

- In the special case of the inviscid Burger's equation $\frac{\partial u}{\partial t} + c \frac{\partial u}{\partial x} = 0$, the FTC's scheme is unstable.
- With reference to "Integration of Linear Hyperbolic Equations" a stable scheme for the inviscid Burger's equation reads:

$$\frac{u_i^{n+1} - u_i^n}{\Delta t} + C \frac{u_i^n - u_{i-1}^n}{\Delta x} = 0$$

(15)

"Jumped
Burger's
Equation"

Backward Differencing

What's the relation between (15) and (9)?

→ Consider the convective term

$$C \frac{u_i^n - u_{i-1}^n}{\Delta x} = C \frac{u_i^n - u_{i-1}^n}{\Delta x} + C \frac{u_{i+1}^n - u_{i-1}^n}{2\Delta x} - C \frac{u_{i+1}^n - u_{i-1}^n}{2\Delta x}$$

$$= C \frac{u_{i+1}^n - u_{i-1}^n}{2\Delta x} - \frac{1}{2} C \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta x}$$

$$= C \frac{u_{i+1}^n - u_{i-1}^n}{2\Delta x} - \frac{1}{2} (C \cdot \Delta x) \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta x^2} \quad (16)$$

→ (16) in (15) ...

Artificial
Viscosity

$$\frac{u_i^{n+1} - u_i^n}{\Delta t} + C \frac{u_{i+1}^n - u_{i-1}^n}{2\Delta x} = \frac{C \cdot \Delta x}{2} \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta x^2} \quad (17)$$

Dissipation
→ 2nd Derivative

- What makes equation (15) stable is the equivalent "Artificial Viscosity" in (17).

A comparison to (9) suggests that

$$\boxed{J_{AV} = \frac{C \cdot \Delta x}{2}} \quad (18)$$

- We have shown earlier in "Integration of Linear Hyperbolic Equations" that equation (15) is stable for

$$\underline{\mathcal{O} = \frac{C \Delta t}{\Delta x} \leq 1}$$

- Linking equation (17) to the FTCS scheme in (9) and the stability criterion in (14) we find that ...

$$\tau = \frac{J_{AV} \cdot \Delta t}{\Delta x^2} = \frac{C \cdot \cancel{\Delta x}}{2} \frac{\Delta t}{\cancel{\Delta x^2}} = \frac{1}{2} \mathcal{O}$$

$$(14) \Rightarrow \underline{\mathcal{O}^2 \leq 2\tau \leq 1}$$

$$\mathcal{O}^2 \leq \mathcal{O} \leq 1$$

True!

- By looking at (16) we can argue that ...

$$\text{Backward Differencing} = \text{Central Differencing} + \text{Artificial Dissipation} \quad (16a)$$

... and this "shifting operation" gains stability.

- So it appears the following:

Artificial viscosity is required for the numerical stability of Finite Difference approximations of "convective terms".

- But what are the problems that come with it?

- i) Loss of accuracy in truncation error.
- ii) Oscillations in solutions of steep gradients such as shocks.
- iii) Artificial dissipation of physical flow structures, e.g. vortices.

- How does "Artificial Viscosity" cause oscillations?

From (3) and (4) in "Integration of Linear Hyperbolic Equations" we write the truncation error for (15) as

$$\mathcal{E}_i^n = \underbrace{J_{AV} (2 - 1)}_{\mathcal{O}(\Delta x)} \left(\frac{\partial^2 u}{\partial x^2} \right) + \mathcal{O}(\Delta t^2, \Delta x^2) \quad (17)$$

The 2nd order term (as the leading term of the TE) allows oscillations. The stability condition (14) gives us for the FTCS scheme

$$\mathcal{B}^2 \leq 2\tau \leq 1$$

$$\mathcal{B}^2 \leq 2\tau \Rightarrow \frac{c^2 \Delta t^2}{\cancel{\Delta x^2}} \leq 2 \frac{J_{AV} \cancel{\Delta t}}{\cancel{\Delta x^2}}$$

$$\Delta t \leq \frac{2J_{AV}}{c^2} = \Delta t_1 \quad (18)$$

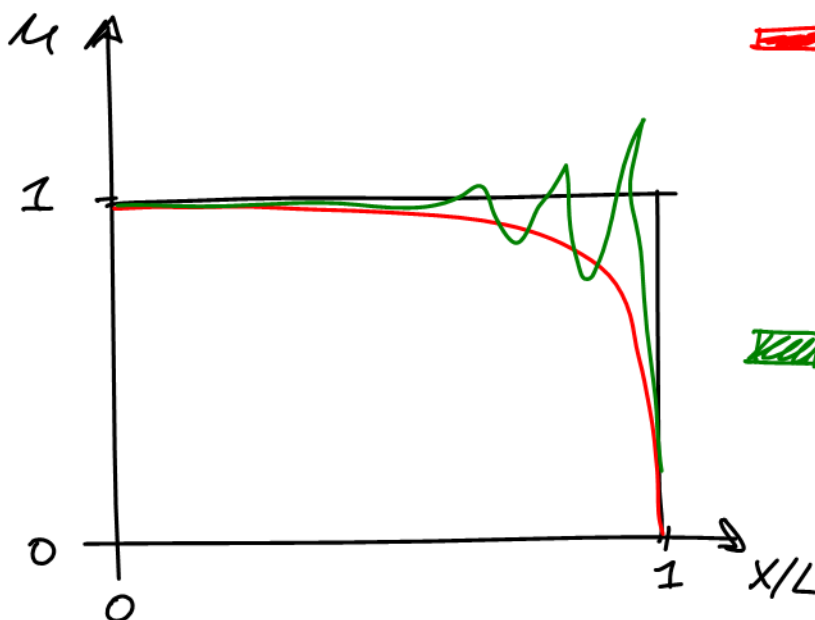
$$2\tau \leq 1 \Rightarrow 2 \frac{J_{AV} \Delta t}{\Delta x^2} \leq 1 \Rightarrow \Delta t \leq \frac{\Delta x^2}{2J_{AV}} = \Delta t_2$$

Keep in mind that in general the scheme

(15) has $\bar{V}_{Av} = \frac{c \cdot \Delta x}{2}$

$$\Rightarrow \Delta t_1 = \frac{\cancel{2} \cdot \cancel{c} \cdot \frac{\Delta x}{\cancel{2}}}{c^2} = \frac{\Delta x}{c} \quad \left. \begin{array}{l} \Delta t_2 = \frac{\Delta x^2}{\cancel{2} \cdot \frac{c \cdot \Delta x}{\cancel{2}}} = \frac{\Delta x}{c} \end{array} \right\} \text{ "Shock Speed"}$$

One can show that oscillations in the solution can be suppressed when additional artificial viscosity \bar{V}_{add} is added to (17). This can become a trial-and-error task, especially when the shock speed c becomes μ in a non-linear case.



■ No oscillations, but artificial viscosity smoothens solution.

■ "Ugly" solution with oscillations.