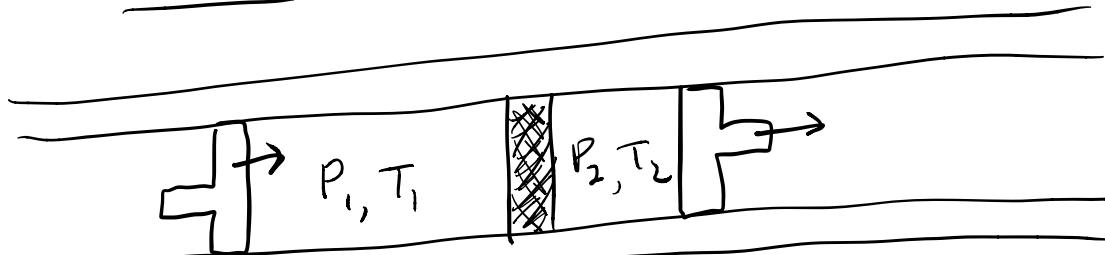


PHYS 425 - w2l1

Joule-Thomson Expansion.

Last Time



$$\rightarrow \boxed{\mu_{JT} = \frac{T \left(\frac{\partial V}{\partial T} \right)_P - V}{C_P}}$$
$$\mu_{JT} > 0 \Rightarrow T_2 < T_1 \quad (\text{cooling})$$
$$\mu_{JT} < 0 \Rightarrow T_2 > T_1 \quad (\text{heating})$$

To go further, need to model how real gases behave \rightarrow need eq'n of state.

(a) ideal gas (non-interacting)

$$PV = Nk_B T \quad \left(\frac{\partial V}{\partial T} \right)_P = \frac{Nk_B}{P} = \frac{V}{T}$$

$$T \left(\frac{\partial V}{\partial T} \right)_P - V = T \left(\frac{V}{T} \right) - V = 0.$$

\therefore for ideal non-interacting gas $\mu_{JT} = 0$

$$\therefore T_1 = T_2$$

(b) Van der Waals Gas

1. Don't assume gas particles are point particles. Assume that they are hard spheres.

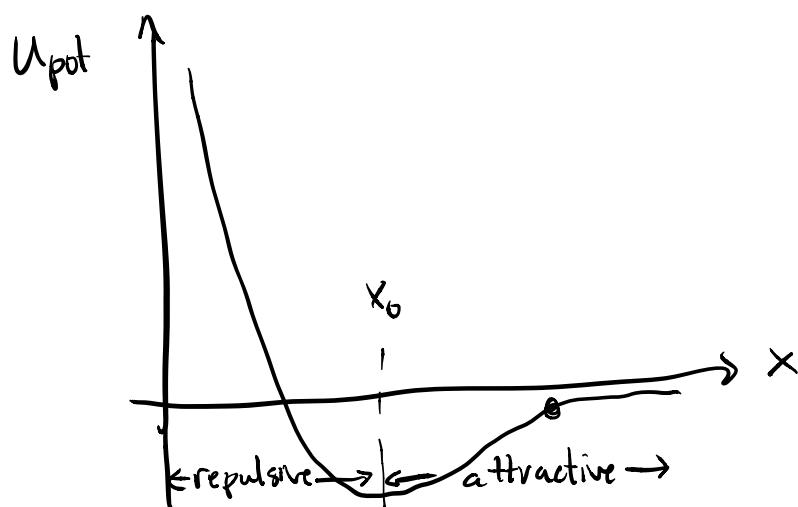
\therefore when added to a closed volume they occupy some space

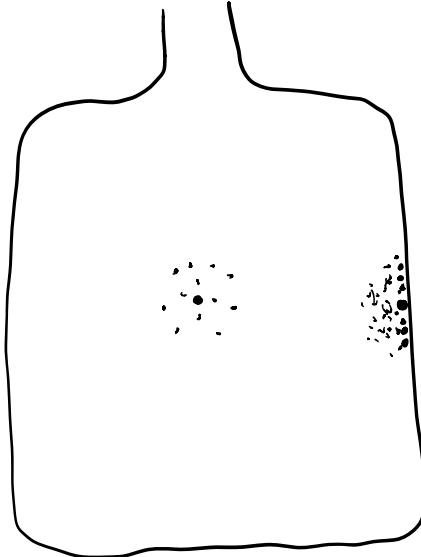
$$V \rightarrow V - Nb'$$

\uparrow
no. of particles

b' is excluded volume due to finite size of gas particle.

2. Assume that there is a short range attraction between particles.





- particles in centre
don't feel net
force to left or
right

- particles near container
wall feel net force
inwards b/c of
absence of particles
near container wall.

■ The net inward force on surface particles

$$\propto \frac{N}{V}$$

■ No. of surface particles also $\propto \frac{N}{V}$ (density)

\therefore pressure on vessel walls $P \rightarrow P - a' \left(\frac{N}{V} \right)^2$

$$P = \frac{Nk_B T}{V} \quad (\text{ideal gas})$$

$$P = \frac{Nk_B T}{V-Nb'} - a' \left(\frac{N}{V} \right)^2$$

Van der Waal's
Eq'n of state.

$$\begin{aligned}\therefore \frac{P}{k_B T} &= \frac{N}{V \left(1 - \frac{Nb'}{V}\right)} - \frac{a'}{k_B T} \left(\frac{N}{V}\right)^2 \\ &= \frac{N}{V} \left(1 - \frac{Nb'}{V}\right)^{-1} - \frac{a'}{k_B T} \left(\frac{N}{V}\right)^2\end{aligned}$$

If excluded volume $Nb' \ll V$

then

$$\left(1 - \frac{Nb'}{V}\right)^{-1} \approx 1 - (-1) \frac{Nb'}{V} = 1 + \frac{Nb'}{V}$$

$$\therefore \frac{P}{k_B T} \approx \frac{N}{V} \left(1 + \frac{Nb'}{V}\right) - \frac{a'}{k_B T} \left(\frac{N}{V}\right)^2$$

$$\text{or } \frac{PV}{Nk_B T} \approx 1 + \frac{Nb'}{V} - \frac{a'}{k_B T} \frac{N}{V} = 1 + \underbrace{\frac{N}{V} \left(b' - \frac{a'}{k_B T}\right)}$$

\downarrow
 van der
 waals
 correction.

$$\text{on RHS make approx } \frac{N}{V} \approx \frac{P}{k_B T}$$

$$\frac{PV}{Nk_B T} \approx 1 + \frac{P}{k_B T} \left(b' - \frac{a'}{k_B T} \right)$$

$\frac{\partial V}{\partial P}$

$$V = \frac{Nk_B T}{P} \left[1 + \frac{1}{k_B T} \left(b' - \frac{a'}{k_B T} \right) P \right]$$

Now evaluate $\left(\frac{\partial V}{\partial T} \right)_P$

$$\left(\frac{\partial V}{\partial T} \right)_P = \frac{Nk_B}{P} \left[1 + \frac{1}{k_B T} \left(b' - \frac{a'}{k_B T} \right) P \right]$$

$$+ \frac{Nk_B T}{P} \left[- \frac{1}{k_B T^2} \left(b' - \frac{a'}{k_B T} \right) P \right. \\ \left. + \frac{1}{k_B T} \left(\frac{a'}{k_B T^2} \right) P \right]$$

$$= \frac{Nk_B}{P} \left[1 + \frac{1}{k_B T} \left(b' - \frac{a'}{k_B T} \right) P - \frac{1}{k_B T} \left(b' - \frac{a'}{k_B T} \right) P \right. \\ \left. + \frac{a' P}{(k_B T)^2} \right]$$

$$\therefore \left(\frac{\partial V}{\partial T} \right)_P = \frac{Nk_B}{P} \left[1 + \frac{a' P}{(k_B T)^2} \right]$$

Recall:

$$\mu_{JT} = \frac{T \left(\frac{\partial V}{\partial T} \right)_P - V}{C_P}$$

$$T \left(\frac{\partial V}{\partial T} \right)_P - V = \frac{Nk_B T}{P} \left[\cancel{1 + \frac{a' P}{(k_B T)^2}} \right]$$

$$= \frac{Nk_B T}{P} \left[\cancel{1 + \frac{1}{k_B T} \left(b' - \frac{a'}{k_B T} \right) P} \right]$$

$$= \frac{Nk_B T}{P} \left[\frac{2a' P}{(k_B T)^2} - \frac{b' P}{k_B T} \right]$$

$$= N \left(\frac{2a'}{k_B T} - b' \right)$$

$$M_{JT} = \frac{N \left(\frac{2a'}{k_B T} - b' \right)}{C_p}$$

low temp, $\frac{2a'}{k_B T}$ term dominates.

$$M_{JT} \approx \frac{2Na'}{C_p k_B T} > 0 \Rightarrow \text{get cooling}$$

high temp, b' term dominates

$$M_{JT} \approx -\frac{Nb'}{C_p} < 0 \Rightarrow \text{get heating}$$

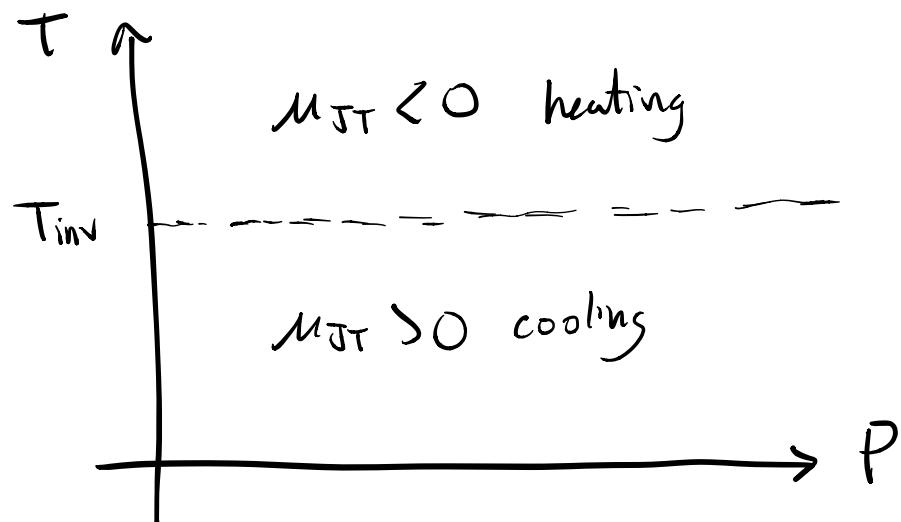
At the inversion temp T_{inv} , $M_{JT} = 0$

$$\frac{2a'}{k_B T_{inv}} - b' = 0$$

$$\therefore T_{inv} = \frac{2a'}{k_B b'}$$

Below T_{inv} , get cooling b/c $\mu_{JT} > 0$

Above T_{inv} , get heating b/c $\mu_{JT} < 0$



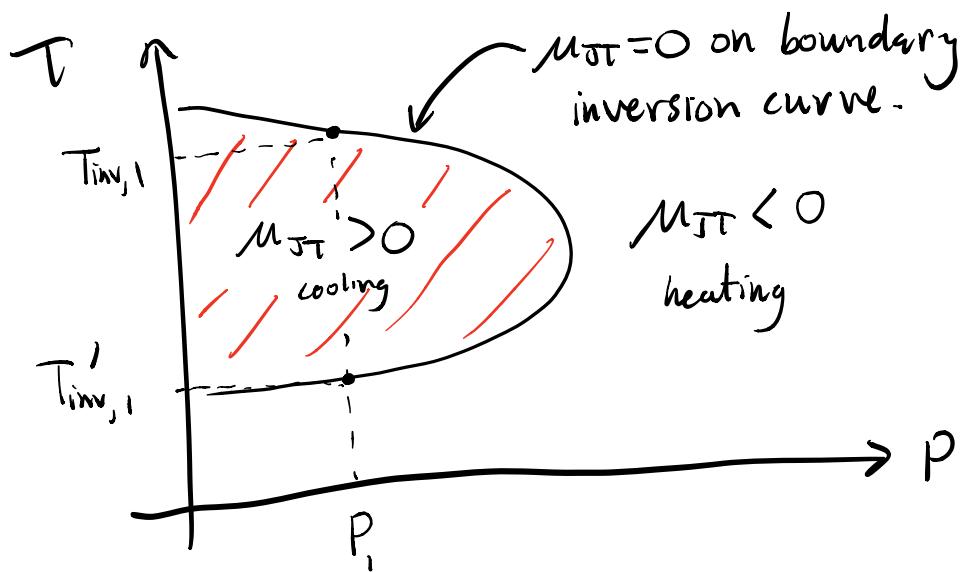
In practice μ_{JT} depends also on pressure.

In an assignment #2, you will calc μ_{JT} for van der Waals eq'n more carefully.

In your calc, won't make the approx.

$$\left(1 - \frac{N}{V}b'\right)^{-1} \approx 1 + \frac{N}{V}b'$$

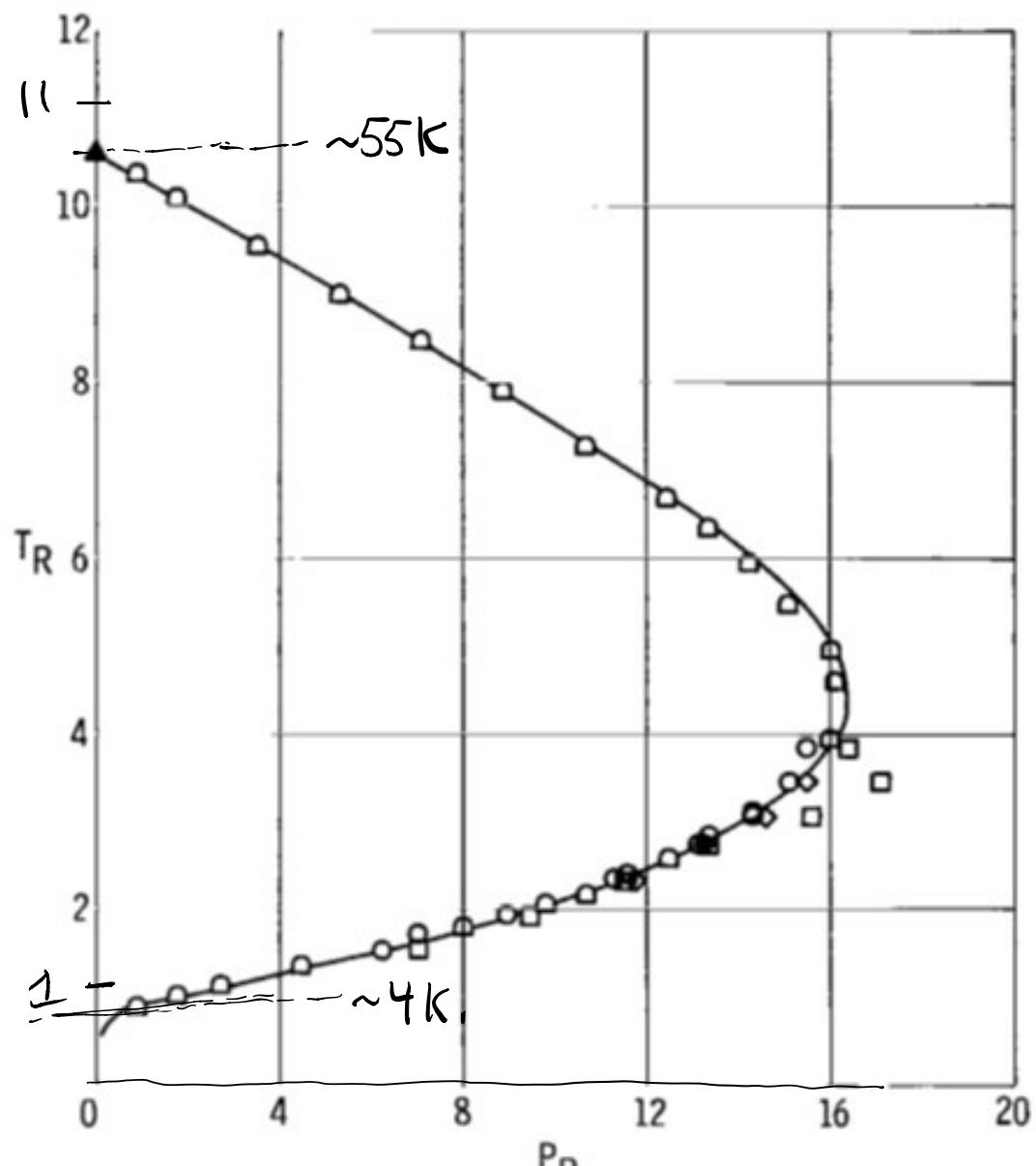
$$\therefore \frac{N}{V} \approx \frac{P}{k_B T} \text{ on RHS}$$



Can liquify ${}^4\text{He}$ using a Joule-Thomson expansion. At 1 atm of pressure, the boiling temp. of liquid ${}^4\text{He}$ is about 4.2 K.

It wasn't part of the video, but below is the actual inversion curve for ${}^4\text{He}$. In this plot, $T_R = \frac{T}{T_c}$ where $T_c = 5.2\text{ K}$

$$\left\{ \begin{aligned} P_R &= \frac{P}{P_c} \text{ where } P_c = 0.227 \frac{\text{MN}}{\text{m}^2} \\ &= 0.227 \text{ MPa} \end{aligned} \right.$$



(a) Helium. $P_C = 0.22746 \text{ MN/m}^2$; $T_C = 5.2 \text{ K}$.