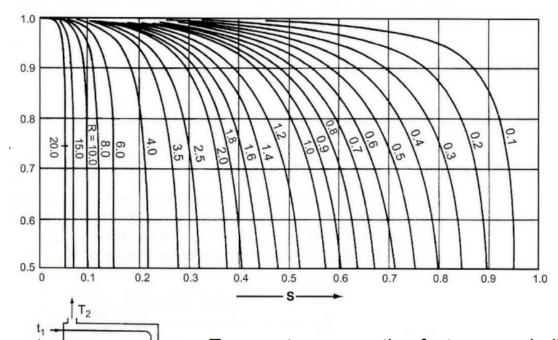
```
> restart;
> #Equations
   R := (T \text{ hot1} - T \text{ hot2}) / (T \text{ cold2} - T \text{ cold1});
   S := (T \text{ cold2} - T \text{ cold1})/(T \text{ hot1} - T \text{ cold1});
   A req := Q/(F*U*DeltaT LM);
   DeltaT LM := ((T \text{ hot2} - T \text{ cold1}) - (T \text{ hot1} - T \text{ cold2}))/ln(
   (T hot2-T cold1)/(T hot1-T cold2));
   T hot2 := -(Q-m \text{ hot*c hot*T hot1})/(m \text{ hot*c hot}); #Kelvin
   T_{cold2} := (c_{cold*m}_{cold*T}_{cold1} + Q) / (m_{cold*c}_{cold1})
                                           R := \frac{T_{hot1} - T_{hot2}}{T_{cold2} - T_{cold1}}
                                           S := \frac{T_{cold2} - T_{cold1}}{T_{bott} - T_{cold1}}
                                         A_{req} \coloneqq \frac{Q}{F \, U DeltaT_{-}}
                               DeltaT_{LM} := \frac{T_{hot2} - T_{cold1} - T_{hot1} + T_{cold2}}{\ln\left(\frac{T_{hot2} - T_{cold1}}{T_{hot1} - T_{cold2}}\right)}
                                     T_{hot2} := -\frac{-m_{hot} c_{hot} T_{hot1} + Q}{m_{hot} c_{hot}}
                                     T_{cold2} := \frac{c_{cold} m_{cold} T_{cold1} + Q}{m_{cold} c_{cold}}
                                                                                                             (1)
> #1 is in
   #2 is out
   print("====Specifications====");
   Q := 10*1000; #W
   m \text{ hot } := 90/1.204/60; \#kg/s
   c hot := 1.006*1000; #J/kg/K (Isobaric)
   T hot1 := 20 + 273; #Kelvin
   c cold := 4.2*1000; #J/kg/K (Isobaric)
```

T cold1 := 8 + 273; #Kelvin

```
print("=====Estimated=====");
  m__cold := 1.5; #Kelvin
  U__o_ass := 82; #W/m2/K
                                "====Specifications====="
                                       Q := 10000
                                   m_{hot} := 1.245847176
                                     c_{_{hot}} \coloneqq 1006.000
                                       T_{hot1} := 293
                                      c_{cold} := 4200.0
                                       T_{cold1} := 281
                                 "====Estimated====="
                                       m_{cold} := 1.5
                                       U_{o\_ass} := 82
                                                                                          (2)
> R;
  s;
  A_req;
  T hot2;
  T cold2;
                                       5.026639800
                                      0.1322751417
                                       1488.610389
                                          FU
                                       285.0212061
                                                                                          (3)
                                       282.5873017
```

The "correction factor" F



Temperature correction factor: one shell pass; two or more even tube passes.

```
> F := 0.98; #VERY ROUGH, NEED TO MEASURE PROPERLY
                                F := 0.98
                                                                       (4)
> U := U o ass; #TEMPORARY ASSUMPTION
  A req; #m2
  DeltaT LM;
                                U := 82
                               18.52427065
                               6.717674465
                                                                       (5)
> L tube := 1.5; #tubes
  D internal := 0.02; #m
  D external := 0.025; #m
  #Fin type, Helical
  1 f := 0.005; \#m
  t f := 0.001; #m
  p_{f} := 0.003; \#m
  \#((L \text{ tube}*(1/p f)*A f)+A b*(L \text{ tube}*(1/p f)))
  r f1 := D external/2;
  1 fc := 1 f + t f/2; #corrected fin hight to account for
```

```
transfer in tip
  r__f2c := r__f1 + l__fc;
  A_f := 2*Pi*(r_f2c^2 - r_f1^2);
  N__fin := L__tube/p__f;
  A_b := Pi*D_ external*(L_ tube - N_ fin*t_ f);
  A o one tube := A f*N fin + A b;
  N tt := A req/A o one tube;
                                    L_{tube} := 1.5
                                  D_{internal} := 0.02
                                  D_{external} := 0.025
                                    l_f := 0.005
                                    t_f := 0.001
                                    p_f := 0.003
                                r_{fl} := 0.012500000000
                               l_{fc} := 0.0055000000000
                                r_{f2c} := 0.018000000000
                               A_f := 0.001054004335
                                N_{fin} := 500.0000000
                               A_b := 0.07853981635
                             A_{o \text{ one tube}} := 0.6055419838
                                N_{H} := 30.59122430
                                                                                  (6)
> #Chosen Layout is a triangular with 30 degrees rotation.
  #Number of passes is 2
  N p := 6;
  psi_n := 0.17;
  C 1 := 0.866;
  L tp := 1.25 * D external; #Based on TEMA standards
                                     N_p := 6
                                    \psi_n := 0.17
```

 $C_{_{I}} := 0.866$

```
L_{tp} := 0.03125
                                                                             (7)
 D__ctl := L__tp*(4*C__1*N__tt/3.14159265/(1-psi__n))^(1/2);
                              D_{ad} := 0.1992156305
                                                                             (8)
> L bb := 0.0127; #Baffle bypass clearance
                                 L_{bb} := 0.0127
                                                                             (9)
  D__s := D__ctl + L__bb + D__external;
  L B := 0.8*D s; #Baffle spacing
                              D_s := 0.2369156305
                              L_{p} := 0.1895325044
                                                                            (10)
> P_v := L_tp * cos(3.14159265/6);
  N__r := D__ctl / P__v;
  BaffleCut := 0.25; #%
  N tcc := (1-BaffleCut)*N r;
                             P_{v} := 0.02706329388
                              N_r := 7.361100662
                               BaffleCut := 0.25
                              N_{tcc} := 5.520825496
                                                                            (11)
> T coldAvg := (T cold1 + T cold2)/2;
                             T_{coldAv\sigma} := 281.7936508
                                                                            (12)
> #properties of water, tube side
  rho_t := 999.70; #kg/m3
  mu t := 1.308*10^{(-3)}; #Pa*s
  k t := 0.58; \#W/m/K
  C_pt := 4200; \#J/kg/K
                                 \rho_t := 999.70
                             \mu_t := 0.0013080000000
                                  k_{t} := 0.58
                                 C_{nt} := 4200
                                                                            (13)
> #Calculating Tube side cross-sectional flow area
  N__per_pass := N__tt/N__p;
  A internal := (3.14159/4)*D internal^2; #m2
  A_t := N per pass * A internal; #m2
```

```
N_{per pass} := 5.098537383
                            A_{internal} := 0.0003141590000
                              A_{\downarrow} := 0.001601751406
                                                                                 (14)
> #Water key equations
  v t := m cold/(rho t*A t);
  Re t := (rho t*v t*D internal)/mu t;
  Pr t := (C pt*mu t)/k t;
  mu corr := 1;
  Nu t := 0.023*Re t^0.8*Pr t^0.4*(mu corr);
  h_i := (Nu_t *k_t)/D_internal; #W/m^2/K
                                v_{\perp} := 0.9367559344
                                \Re_{t} := 14319.18819
                                Pr_{t} := 9.471724138
                                    \mu_{corr} := 1
                                N_{c} := 119.4082050
                                h_i := 3462.837945
                                                                                 (15)
> #properties of air, shell side
  rho_s := 1.204; \#kg/m3 (air at 20C)
  mu s := 1.825*10^{(-5)}; \#kg/m/s
  k s := 0.02514; \#W/m/K
  C ps := 1007;
                                   \rho_{\rm s} := 1.204
                              \mu_s := 0.00001825000000
                                  k_{\rm s} := 0.02514
                                   C_{ps} := 1007
                                                                                 (16)
> Q air := m hot/rho s;
  A face := L tube*(D ctl + D external);
  u f := Q air/A face;
  u_ max := u__f*(L__tp/(L__tp - D__external));
                                Q_{air} := 1.034756791
                               A_{face} := 0.3363234458
                                u_{c} := 3.076671591
                               u_{\text{max}} := 15.38335796
                                                                                 (17)
```

```
> Pr s := C__ps*mu__s/k__s;
  Re_s := rho_s * u_max * D_external/mu_s;
  Nu_s := 0.134*Re_s^0.681*Pr_s^0.33*((p_f-t_f)/1_f)^0.2*
  (p f/t f)^0.1134;
  h__s := Nu__s * k__s/D_ external;
                            Pr_{s} := 0.7310163087
                             \Re_{s} := 25372.00408
                             N_{c} := 113.7847026
                             h_{s} := 114.4218969
                                                                          (18)
> #Defining Thermal Conductivity Variables
  k tube := 50; \#W/m/K
  k fin := 205; \#W/m/K
  Rf o := 0.0003526; \#m2*K/W
  Rf i := 0.00018; \#m2*K/W
                                 k_{tube} := 50
                                 k_{fin} := 205
                              Rf_o := 0.0003526
                               Rf_i := 0.00018
                                                                          (19)
> #Fin equations
  m := simplify(((2*h_s)/(k_fin * t_f))^(1/2));
  eta_f := tanh(m * 1_f) / (m * 1_f);
  N fin := L tube/p f;
                              m := 33.41124344
                             \eta_{\ell} := 0.9908000928
                             N_{g_n} := 500.00000000
                                                                          (20)
> #Outside area calculations
  A_f := A f;
  A b := A b;
 A f total := N__fin * A__f * N__tt;
 A b total := A b * N tt;
 A o := A f total + A b total;
                            A_f := 0.001054004335
                            A_{i} := 0.07853981635
                            A_{f total} := 16.12164151
```

```
A_{b \ total} := 2.402629138
                             A := 18.52427065
                                                                         (21)
> #Internal Area calculations
  A__i := 3.14159 * D__internal * L__tube * N__tt;
                             A_i := 2.883152530
                                                                         (22)
> eta_o := (eta_f * A_f_total + A_b_total)/A_o
                            \eta_a := 0.9919933360
                                                                         (23)
> #Calculating all thermal resistances
  R shell conv := 1/eta o/h s; #Air side convection
  R__tube_conv := 1/(h__i*(A__i/A__o)); #Water side convection
  R wall cond := (D external * ln(D external/D internal))/(2*
  k tube);
  R_ fouling := (Rf_ i * (A_ o/A_ i))+(Rf_ o /eta_ o);
                         R_{shell\ conv} := 0.008810125643
                         R_{tube\ conv} := 0.001855416143
                         R_{wall\_cond} := 0.00005578588780
                          R_{fouling} := 0.001511946913
                                                                         (24)
> #Calculating U
  R total := R shell conv + R tube conv + R wall cond +
  R fouling;
                           R_{total} := 0.01223327459
                                                                         (25)
  U__o_calc := 1/R__total; #W/m2/K
  print("======
                            U_{o \ calc} := 81.74426174
                                                                         (26)
> #Tube side pressure drop
  f t := 0.0035 + 0.264/Re t^0.42;
  L__total := L__tube * N p;
 K := 1.8*N p;
  DP__t_friction := 4*f__t*(L__total/D__internal)*(rho t*v t^2/2)
  DP t return := K*(rho t*v t^2)/2;
```

```
DP_t := DP_t_friction + DP_t_return;
                               f_t := 0.008243710754
                                   L_{total} := 9.0
                                   K := 10.8
                             DP_{t \ friction} := 6508.604064
                             DP_{t \ return} := 4737.141506
                               DP_{t} := 11245.74557
                                                                                (27)
> #Shell side pressure drop using Kern's method
  A__s := (L__tp - D__external)*D__s*L__B/L tp;
  G__s := m__hot/A_ s;
  u_s := G_s/rho_s;
  d__e := 1.10/D__external*(L__tp^2 - 0.917*D__external^2);
  Re s := G s*d e/mu s;
                              A_s := 0.008980642557
                                G_{s} := 138.7258393
                                u_s := 115.2207968
                               d_e := 0.01775125000
                               \Re_{s} := 134934.6332
                                                                                (28)
```

