

Year 4 — Topics in Fluid Mechanics

Based on lectures by Dr Graham Benham

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Michaelmas 2022

These notes are not endorsed by the lecturers, and I have modified them (often significantly) after lectures. They are nowhere near accurate representations of what was actually lectured, and in particular, all errors are almost surely mine (especially the typos!).

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The course is split up as follows,

Lecture 1

- Thin Film and Lubrication Theory (5 Lectures)
- Flow in porous media (6 Lectures)
- Convection and Turbulence (5 Lectures)

4 Problem Sheets.

We will have all our work revolving around the Navier Stokes equations,

$$\begin{aligned}\rho(\mathbf{u}_t + (\mathbf{u} \cdot \nabla)\mathbf{u}) &= -\nabla p + \mu \nabla^2 \mathbf{u} \\ \nabla \cdot \mathbf{u} &= 0\end{aligned}$$

Then we can nondimensionalise $\mathbf{x} = L\hat{\mathbf{x}}$, $t = \frac{L}{U}\hat{t}$, $\mathbf{u} = U\hat{\mathbf{u}}$, $p = \frac{\rho U^2}{L}\hat{p}$. We nondimensionalise,

$$\text{Re}(\mathbf{u}_t + (\mathbf{u} \cdot \nabla)\mathbf{u}) = -\nabla p + \nabla^2 \mathbf{u}$$

A low Reynolds number is slow, sticky flows like honey, while high Reynolds numbers are fast and sloshy. However, for high Reynolds number something goes wrong, we need to non-dimensionalise using, $p = \rho U^2 p$. Then we get,

$$\mathbf{u}_t + (\mathbf{u} \cdot \nabla)\mathbf{u} = -\nabla p + \frac{1}{\text{Re}} \nabla^2 \mathbf{u}$$

1 Thin Film and Lubrication Theory

1.1 Slider Bearing

Consider some object sitting above some impermeable surface. This is a problem about flow in narrow gaps, so we have $\varepsilon = H/L \ll 1$. So we need to re-nondimensionalise our system. We have $x \sim 1$ and $z \sim \varepsilon$, so our incompressibility condition goes to,

$$u_x + w_z = 0$$

The pressure scales like $p \sim 1/\varepsilon^2$. Therefore the rest of our Navier Stokes equations goes to,

$$\varepsilon^2 \text{Re}[\mathbf{u}_t + (\mathbf{u} \cdot \nabla)\mathbf{u}] = -p_x + \varepsilon^2 u_{xx} + u_{zz}$$

and the vertical equation becomes,

$$\varepsilon^4 \text{Re}[w_t + (\mathbf{u} \cdot \nabla)w] = -p_z + \varepsilon^4 w_{xx} + \varepsilon^2 w_{zz}$$

The key assumption is ε is small, but also $\varepsilon^2 \text{Re}$ is small.

Therefore, the governing equation becomes,

$$\begin{aligned} u_{zz} &= p_x = p'(x) \\ p_z &= 0 \end{aligned}$$

and the boundary conditions, we have the no slip condition, so $u = 0$ and the impermeability, $w = 0$ on $z = 0$. On $z = h(x)$, we have the no slip says that $u = 1$ and $w = uh'(x)$. We also have atmospheric pressure, so $p = 0$ on $x = 0$ and $x = 1$.

These equations are solvable, $u = \frac{1}{2}p'z(z - h) + z/h$ and mass conservation says, $u_x + w_z = 0$,

$$\begin{aligned} \int_0^h u_x dz + [w]_0^h &= 0 \\ \frac{\partial}{\partial x} \int_0^h u dz - uh'|_{z=h} + uh'|_{z=0} &= 0 \\ \frac{d}{dx} \int_0^h u dz &= 0 \\ \frac{d}{dx} \left[\frac{1}{2}h + \frac{1}{2}p'(-\frac{1}{6}h^3) \right] &= 0 \end{aligned}$$

Then this is solvable for p .

Exercise. Do this for 3D. We have $\nabla_H = (\partial_x, \partial_y, 0)$ and then we get,

$$\nabla_H \cdot [h\mathbf{i} - \frac{1}{6}h^3 \nabla_H p]$$

and suppose $\mathbf{u} = (1, 0, 0)$ on $z = h(x, y)$.

1.2 Free Surface

The kinematic condition on the free boundary is,

$$\frac{D}{Dt}[S - z] = 0 \quad z = S$$

what also about accumulation? Like rainfall or something being sprayed, then,

$$\frac{D}{Dt}[S - z] = a \quad z = S$$

and so we have,

$$w = S_t + uS_x + vS_y - a \quad z = S.$$

What if we apply similar to $z = b$ and define $h = S - b$, then we can integrate conservation of mass like before and get,

$$\frac{\partial h}{\partial t} + \nabla_H \cdot \int_0^h \mathbf{u}_H dz = 0$$

where $\mathbf{u}_H = (u, v, 0)$.

1.3 Free Surface Stress

We consider the tangent and normal to the surface,

$$\hat{\mathbf{n}} = \frac{(-S_x, 1)}{(1 + S_x^2)^{\frac{1}{2}}} \quad \hat{\mathbf{t}} = \frac{(1, S_x)}{(1 + S_x^2)^{\frac{1}{2}}}$$

Then we have continuous stress at $z = S(r)$ and we have for say, a droplet, as an example, $\sigma_{nn} = p_a$, $\sigma_{nt} = 0$. What are these defined as, $\sigma_{nn} = \sigma_{ij}n_i n_j$, in suffix notation. We defined $\sigma_{ij} = -p\delta_{ij} = \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$ and so,

$$\begin{aligned} \sigma_{nn} &= \sigma_{11}n_1n_1 + \sigma_{13}n_1n_3 + \sigma_{31}n_3n_1 + \sigma_{33}n_3n_3 \\ &= -p + [\tau_1(S_x^2 - 1) - 2\tau_3S_x]/(1 + S_x^2) \end{aligned}$$

where $\tau_1 = 2\mu u_x$ and $\tau_3 = \mu(u_z + w_x)$. Similarly,

$$\begin{aligned} \sigma_{nt} &= \sigma_{11}n_1t_1 + \sigma_{13}n_1t_3 + \sigma_{31}n_3n_1 + \sigma_{33}n_3t_3 \\ &= \frac{[\tau_3(1 - S_x^2) - 2\tau_1S_x]}{1 + S_x^2} \end{aligned}$$

We now consider dimensional scalings, $x \sim L$, $z \sim \varepsilon L$, $S \sim \varepsilon L = K$. We will scale stress by $\tau^* = \frac{\mu U}{H}$, that is, $\tau_1 \sim \varepsilon \tau^*$, $\tau_3 \sim \tau^*$ and $p - p_a \sim \frac{\mu U}{L\varepsilon^2} = \frac{\tau^*}{\varepsilon}$. That means,

$$\sigma_{nn} = -\frac{p}{\varepsilon} + [\varepsilon\tau_1(\varepsilon^2S_x^2 - 1) - 2\varepsilon\tau_3S_x]/(1 + \varepsilon^2S_x^2)$$

where $\tau_1 = 2u_x$ and $\tau_3 = u_z + \varepsilon^2w_x$ and similarly,

$$\sigma_{nt} = \frac{[\tau_3(1 - \varepsilon^2S_x^2) - 2\varepsilon^2\tau_1S_x]}{1 + \varepsilon^2S_x^2}$$

and so $\tau_3 = 0$ implies that $u_z = 0$ and $p = 0$ on $z = S$.