

Heating Element Selection

Choose a compact resistive heater that can be PWM-controlled by an ESP32/RPi. Two common types are **ceramic PTC heaters** and **silicone/nichrome resistive heaters**:

- **PTC ceramic heater** – e.g. a 5 V PTC element that self-regulates at ~40–60 °C ¹. For example, DFRobot offers a “PTC Heating Element – 5V 40°C” (rated 2–3 W) ¹. These plug directly into 5 V and heat to a fixed temperature (no PID needed), but cannot modulate below that setpoint.
- **Flexible heating pad** – e.g. a stainless-steel-fiber pad (5–12 V) that acts as a resistive “gigantic resistor” ². For instance, Adafruit’s 10×5 cm heating pad (5–12 V input) uses conductive fabric that heats uniformly when powered ². This can be PWM-controlled via a MOSFET/SSR.

In practice, a small 5 V/3–10 W heater (PTC or resistive) is enough to warm 1 ft³ by a few °C. Ensure the 5 V supply can deliver >5–10 W ³. For larger heat output, a 12–24 V heater (e.g. 12 V, 30–50 W cartridge or pad) could be used with a MOSFET driver. In all cases **insulate and thermally anchor** the heater to the air stream.

Type	Example/Spec	Voltage	Power	Notes
PTC ceramic block	DFRobot 5 V, ~40°C ±10°C, 2–3 W ¹	5 V	2–3 W	Self-regulating at ~50°C; requires ~5 V supply ¹ . Fast warm-up.
Conductive fabric pad	Adafruit “Electric Heating Pad” (10×5 cm) ²	5–12 V	~5–10 W	Flexible cloth heater; acts as resistor ² . PWM via MOSFET possible.
Nichrome wire coil	Custom coil/cartridge	5–24 V	Up to 50 W	DIY option; design as required and drive via MOSFET.

Power for the heater must exceed its dissipation ³. For example, a 5 V PTC (3 W) would use a 5 V/2 A supply, whereas a 12 V 50 W heater needs 12 V/5 A (plus margin).

Peltier Cooling Unit

Use a thermoelectric (Peltier) cooler sized to handle the ~60 W bulb load. Common modules include **TEC1-12706** (12 V, 6 A, ~60 W rating) or **TEC1-12715** (12 V, 15 A, ~180 W). In practice, a single 12706 can only pump ~20–30 W of heat when the hot/cold side delta-T is large ⁴. For example, a 12 V/5 A TEC1-12706 draws ~60 W and transfers about 20 J/s (20 W) at $\Delta T \approx 45^\circ\text{C}$ ⁴. To remove the 60 W load, **use two Peltier modules** in parallel or a higher-rated unit.

These modules require heatsinking with fan cooling on the hot side. Adafruit sells a “12V 5A Peltier+Heatsink” kit that freezes within a minute at 5 A input (60 W) ⁵. Typical operation: apply 12 V to each Peltier (drawing ~5–7 A), and heat will be pumped from the cold side. Remember: thermoelectric coolers **do not actively**

dehumidify – they just cool air. Moisture is removed only by condensation if the cold plate is below dew point ⁶. (In fact, DOE notes TECs leave absolute humidity unchanged, unlike compressor systems ⁶.)

Peltier Model	Voltage/ Current	Q _{max} @ ΔT=0	Approx. Q @ ΔT~20 °C	Notes
TEC1-12706	12 V, 6 A (60 W)	~60 W	~25–30 W	1–2 modules needed for 60 W load ⁴
TEC1-12710/12715	12 V, 10/15 A	~100/150 W	~40–80 W	Higher capacity; increases cost/size.
12V Peltier kit	12 V, 5 A	~50–60 W	~20–30 W	Adafruit “12V 5A Peltier+Heatsink” ⁵ .

Mount the Peltier with a good thermal paste and a heatsink/fan. A separate small fan or blower should cool the hot side. Because efficiency is low (COP ~0.2–0.3), expect ~100–150 W total electrical draw for two modules.

Sensors (Temperature, Humidity, Fan)

Temperature sensors: Digital sensors like the DS18B20 (one-wire) or I²C sensors (SHT3x/BME280) work well with ESP32/RPi. The DS18B20 is ±0.5 °C accurate from –10 to +85 °C ⁷. Sensirion’s SHT31 (I²C) provides ±0.2 °C and ±2 %RH accuracy ⁸, and also measures humidity. A table of examples:

Parameter	Sensor Example	Interface	Accuracy	Voltage	Notes
Temperature	DS18B20	1-Wire	±0.5 °C (–10–85) ⁷	3–5 V	Many on one bus; waterproof variants exist.
Humidity/ Temp	SHT31-D	I ² C	±2 %RH, ±0.3 °C ⁸	3–5 V	High stability; fast response.
Humidity/ Temp	BME280/ BME680	I ² C/SPI	±3 %RH, ±1 °C	3.3–5 V	Includes pressure/gas (BME680).
Humidity	DHT22 (AM2302)	1-Wire	±2–5 %RH, ±0.5 °C (typ.) ⁹	3–5 V	Inexpensive but slower and less precise.

Use one temperature sensor at the **inlet** and one at the **outlet** of the HVAC coil, plus one **inside-box** (for control feedback). For humidity, an SHT31 or DHT22 inside the box suffices. For example, the SHT31 breakout from DFRobot offers 0–100% RH accuracy ±2% ⁸.

Fan speed/RPM sensor: Most brushless DC (BLDC) fans include a tachometer output (open-collector) driven by an internal Hall-effect sensor ¹⁰. This output pulses (typically two pulses per revolution) proportional to RPM ¹⁰. You can read this with a digital input (or measure the PWM duty if using a 4-pin fan). Many 50–60 mm fans have 3 or 4 pins: +V, GND, tachometer, (and PWM in 4-pin). No extra hardware is

needed if the fan has a tach pin ¹⁰. Otherwise, a small external Hall sensor and magnet can be added on the fan hub.

Airflow (Fan)

A low-power DC fan circulates air through the coils and box. A **50×50×10 mm brushless fan** (~12 V, 0.1–0.2 A) is suitable. For example, the SXDOOL 50 mm slim fan (12 V, 0.10 A) runs ~4500 RPM and moves ~11.2 CFM ¹¹ ¹². This replaces 1 ft³ in under 10 s (≈6 s for 8.6 CFM ¹¹). The image below shows a typical 50×50 mm axial fan (~11 CFM at 12 V):

Figure: Example 50×50×10 mm DC brushless fan (12 V, ~10–12 CFM, ~0.1 A). Such a fan can recirculate 1 ft³ of air in a few seconds ¹¹ ¹².

If stronger airflow or pressure is needed, a slightly larger 60 mm fan (~15–20 CFM) could be used. Ensure the fan voltage matches your supply (12 V fans are common). The fan should be PWM-controllable for variable speed. Use the tachometer signal (or measure PWM duty) for speed feedback if required.

Power Supply Sizing

Use separate regulated supplies (or a multi-output unit) for the high-power (heater, Peltier, fan) and low-power (logic) circuits:

- **Peltier & Fan:** A 12 V DC supply rated for ~10–15 A (120–180 W) covers two 60 W Peltier modules (up to ~120 W) and fan(s). In practice, two TEC1-12706 at 5 A each draw 10 A total (120 W) for ~40–50 W cooling ⁴. Allow headroom, so e.g. a 12 V, 15 A supply.
- **Heater:** If using a 5 V heater (PTC or pad) up to 10 W, use a 5 V/2–3 A supply. If using a higher-voltage heater (e.g. 12 V, 30–50 W), the same 12 V/15 A supply can serve it (via MOSFET) plus Peltier. Always ensure supply capacity exceeds maximum draw ³.
- **Microcontroller/Sensors:** A 5 V/3 A (or 3.3 V via regulator) supply for the ESP32 (max ~0.5–1 A), sensors, and any logic. The MCU (ESP32/RPi) itself runs on 5 V (and has onboard regulators) or 3.3 V.

For example, one could use a single **12 V 15 A** supply for Peltier, fan, and 12 V heater, and a **5 V 3 A** buck converter for the microcontroller and 5 V heater. Heaters and Peltier can share the 12 V supply (with separate MOSFET switches).

Power connections should include decoupling capacitors and proper safety fuses. High-current MOSFETs (logic-level gate) or relays will switch the heater and Peltier. Follow general guidelines: “Ensure the power supply’s capacity is greater than the heater’s maximum dissipation” ³ and use adequate heat sinking.

Thermal Load Calculations

Use basic heat-transfer to size components:

- **Air heat capacity:** 1 ft³ ≈ 0.0283 m³ of air ($\rho \approx 1.2 \text{ kg/m}^3$) has mass ≈0.034 kg. With specific heat $c_p \approx 1005 \text{ J/kg} \cdot \text{K}$, heating 1°C requires $Q \approx 0.034 \cdot 1005 \cdot 1 \approx 34 \text{ J}$. Thus a 60 W (60 J/s) bulb raises the box air by

$\approx 60/34 \approx 1.8^\circ\text{C}$ per second (if perfectly insulated and no losses). In reality, insulation and cooling moderate this. As a reference, 6 ft³ of air ($\approx 0.17\text{ m}^3$, $\approx 0.191\text{ kg}$) has $\sim 192\text{ J}/^\circ\text{C}$ ¹³, so 1 ft³ has $\sim 32\text{ J}/^\circ\text{C}$.

- **Required heater power:** If the box or incoming air ever falls below 20°C (cold ambient), the heater must supply the deficit. For a ΔT of, say, 5°C in 1 ft³, heat needed is $\sim 34 \cdot 5 = 170\text{ J}$. A 5 W heater would take $\sim 34\text{ s}$ to add that much, whereas a 50 W heater only $\sim 3.4\text{ s}$. Typically use enough power to respond on the order of seconds, so 5–10 W is reasonable for fine tuning.
- **Cooling capacity (Peltier):** To offset the 60 W lamp, the Peltier must extract $\sim 60\text{ W}$ plus any heat leaks. As noted, one TEC1-12706 can only move $\sim 20\text{--}30\text{ W}$ at high ΔT ⁴. With two in parallel (each $\sim 5\text{ A}$), you might pump $\sim 50\text{ W}$, which could barely balance the lamp. Thus planning two or more modules is prudent. The exact required cooling is: *Lamp 60 W + heater power (if on) – ambient insulation losses*. If losses are small (well-insulated), aim for $\sim 60\text{ W}$ net cooling at 20°C difference.
- **Air flow rate:** Good mixing requires modest circulation. For a 1 ft³ box, even 1 CFM (cubic foot per minute) replaces the volume in 1 min. A 10 CFM fan cycles it in 6 s. A typical 50 mm fan at 4500 RPM gives $\sim 9\text{--}11\text{ CFM}$ ¹¹, which is ample. If one desires a $\Delta T < 5^\circ\text{C}$ between inlet and outlet, use the heat flow formula: $\dot{Q} = \dot{m} c_p \Delta T \Rightarrow \dot{V} = \frac{\dot{Q}}{\rho c_p \Delta T}$ where $\rho c_p \approx 1200\text{ J}/\text{m}^3 \cdot \text{K}$. For $\Delta T \approx 5^\circ\text{C}$ and $\dot{Q} \approx 60\text{ W}$, this gives $\dot{V} \approx 60 / (1.2 \cdot 1005 \cdot 5) \approx 0.01\text{ m}^3/\text{s}$ ($\approx 21\text{ CFM}$). In practice, even a lower flow is acceptable because the Peltier setpoint will adjust the coil temperature to maintain 20°C .
- **Heat load of 60 W bulb:** The bulb dumps 60 J each second into the air. If no cooling, the air would heat rapidly ($\approx 1.8^\circ\text{C}/\text{s}$ as above). The control system must react on a similar timescale. This sets the needed bandwidth: e.g. a 5 W heater raises temperature $\sim 0.15^\circ\text{C}/\text{s}$. The Peltier(s) must be able to ramp down the temperature at $\sim 60\text{ W}$ (all on) or ramp up if the bulb is turned off.

In summary: roughly $34\text{ J}/^\circ\text{C}$ in the air, $60\text{ J}/\text{s}$ heat input, so expect multi-second temperature transients. Select heater/Peltier powers to achieve $< 10\text{ s}$ correction times (5–50 W range).

Control Strategy (Fuzzy Logic + LLM)

The low-level control loop can be a **fuzzy logic controller (FLC)** that reads temperature/humidity errors and adjusts actuator powers. For instance, define fuzzy variables like *Temp_Error* = (CurrentTemp – 20°C) and *Humid_Error* = (CurrentRH – 50%). Example fuzzy rule (from typical HVAC design ¹⁴):

- *If (Temp_Error is Positive_High) and (Humid_Error is Normal) then (Cooling is High).*
- *If (Temp_Error is Negative) and (Humid_Error is Low) then (Heating is Medium).*
- *If (Humid_Error is Positive_High) and (Temp_Error is Low) then (Dehumidifier action = High).*

The FLC would have membership functions for “High/Normal/Low” temperature and humidity, and outputs for fan speed, heater power, and cooling power. After fuzzification and rule evaluation, outputs are defuzzified (e.g. to PWM duty). Fuzzy control easily handles the nonlinear and coupled T/RH relationships

¹⁴ .

On top of the fuzzy controller, an LLM (e.g. a small GPT-style model) could serve as a **supervisory or adaptive layer**. While specific published architectures for HVAC+LLM are scarce, one approach is: use the LLM to analyze long-term data or high-level commands and adjust fuzzy rules or setpoints. For example, the LLM could take natural-language queries (“cool faster in high humidity”) or processed sensor logs and suggest tweaking membership functions or priorities. In robotics, LLMs have been used as a “layer” that interprets intent and guides control algorithms ¹⁵; similarly here it could interpret user instructions or learn occupant comfort preferences.

In this prototype, a plausible architecture is a two-tier control loop:

1. **Fuzzy controller (real-time):** Takes instantaneous T/RH errors and outputs heater/cooler/fan settings.
2. **LLM-assisted logic (supervisory):** Runs on higher-level patterns. E.g., periodically query an LLM with recent sensor trends (“humidity rising while temperature stable”) and let it adjust control parameters or issue higher-level directives. The LLM could also handle system diagnostics (“why is humidity not dropping?”) by reasoning over the model.

(Literature on LLMs in HVAC is very limited. We did not find direct sources for HVAC-specific LLM control. Most LLM-control work so far is in robotics as a natural-language interface ¹⁵. Thus the above strategy is a reasoned suggestion rather than a standard practice.)

Prototype Build Plan

1. **Assemble box and load:** Build or repurpose a 1 ft³ insulated box. Mount the 60 W filament bulb securely inside as the heat source.
2. **Install coils:** Place the **cooling Peltier assembly** first in the airflow path (exiting the box), followed by the **heating element** (electric heater coil/pad). Ensure both can be switched on/off and mounted with adequate ventilation. Use thermal paste and heatsinks/fans on the Peltier’s hot side.
3. **Mount fan:** Install the variable-speed DC fan downstream of the heating coil to drive air through the coils and back into the box. Wire the fan to a PWM-capable pin.
4. **Sensor placement:**
5. *Temp sensors:* Place one at the coil inlet (box-air side), one at the outlet (coil exhaust), and one inside the box. For example, use DS18B20 probes in thermowells.
6. *Humidity sensor:* Place an SHT31 or DHT22 inside the box near the air outlet of the fan.
7. *Fan tach:* Use the fan’s tach output wire (3rd pin) to the microcontroller (or attach a small Hall sensor).
8. **Electronics:** Connect heater, Peltier(s), and fan each to a suitable MOSFET or driver channel on the ESP32. Provide a common ground. Power the ESP32 (5 V) from the 5 V rail (with regulator), and all high-power loads from the 12 V supply. Use decoupling and flyback diodes as needed.
9. **Firmware setup:** Write ESP32 code (or Raspberry Pi software) to read sensors and control actuators:
10. Calibrate sensors and verify readings.
11. Implement fuzzy logic: define membership functions (e.g. triangular “Cold/OK/Hot” and “Dry/OK/Humid”) and rulebase (e.g. from HVAC examples ¹⁴). Use a fuzzy library or code the inferencing.
12. Test manual control loops first (e.g. simple on/off thermostat) to verify heater/cooler.
13. **Integrate LLM (optional):** If using an LLM, set up a service (e.g. a locally-run small transformer model) that the controller can query. For initial prototype, you might script rule adjustments instead.
14. **Testing and tuning:** With the system assembled, run tests:
15. Verify **heating response** (turn off Peltier, run heater, see temperature rise).

16. Verify **cooling response** (turn on Peltier with lamp on, see temperature drop).
17. Tune fuzzy rules to reach 20 °C/50%RH stably: e.g. if overshoot occurs, adjust output gains or membership thresholds.
18. Observe humidity control: ensure that cooling coil causes condensation (dehumidification) if RH rises, and if RH falls too low, furnace is triggered to warm air (since warmer air holds more moisture).
19. Log performance and iterate on fuzzy rules or add learning heuristics with LLM insights.
20. **Safety and measurement:** Include over-temperature cutoffs and monitor current draw. Keep wires neat and double-check insulation (especially around heater and Peltier connections).
21. **Documentation:** Label all parts and connections. Prepare a short user guide describing how to calibrate the system (e.g. initial rule tuning) and interpret the LLM messages (if used).

Each step should be done incrementally: verify sensor readings first, then individual actuator control, and finally the integrated fuzzy-LLM loop. In the end, the system should maintain the box at 20 °C/50 %RH within reasonable accuracy (± 1 °C, $\pm 5\%$ RH). Use inexpensive prototyping parts as listed above (links to examples provided) to keep the system compact and cost-effective.

Sources: Component specs and concepts above are drawn from product datasheets and application notes ¹ ⁴ ⁸ ¹⁰ ² ¹⁴, as cited. These informed the selection of heating elements, Peltier modules, sensors, and control approaches.

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