

Contact Sensing via Joint Torque Sensors and a Force/Torque Sensor for Legged Robots

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Motivation and Related Works



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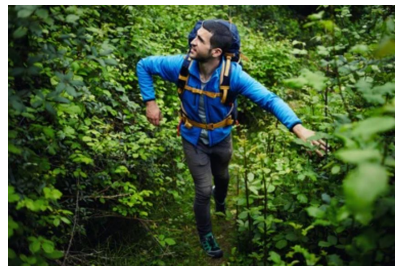
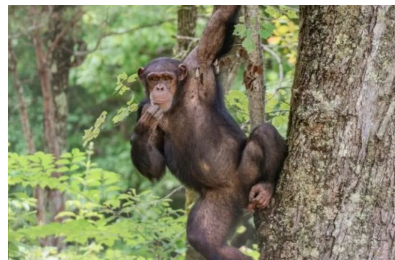
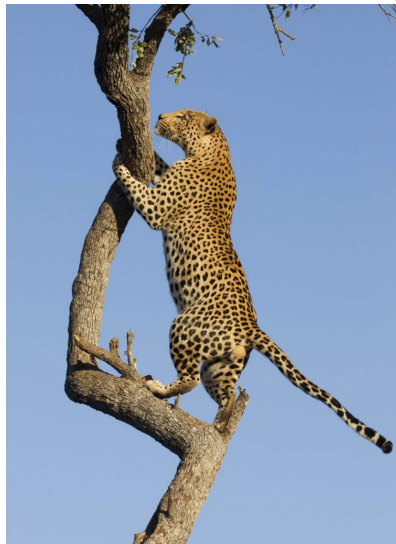


Animals in Complex Environments

Whole-body
sensing

Multi-point contact

Adaptive stability



<https://www.safariventures.com/unraveling-the-secrets-of-leopards-master-hunters-and-tree-climbers/>
<https://explorersweb.com/apes-downclimbing-crucial-for-human-arm-development/>
<https://www.shutterstock.com/image-photo/male-wanderer-walking-through-woods-overcoming-311052977>
https://www.youtube.com/watch?v=H1PEWGF_1lk&ab_channel=ClimbingTechTips

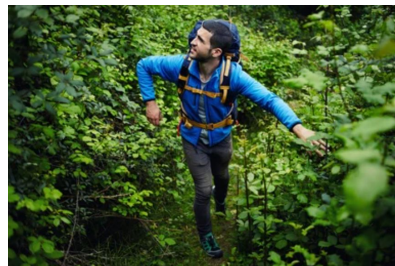
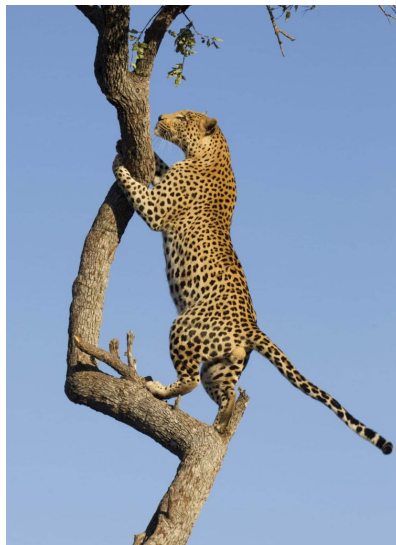


Animals in Complex Environments

Whole-body
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Adaptive stability



Animals excel at this - so why don't robots?

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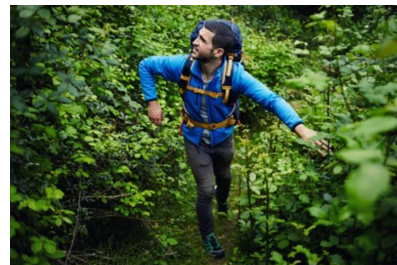
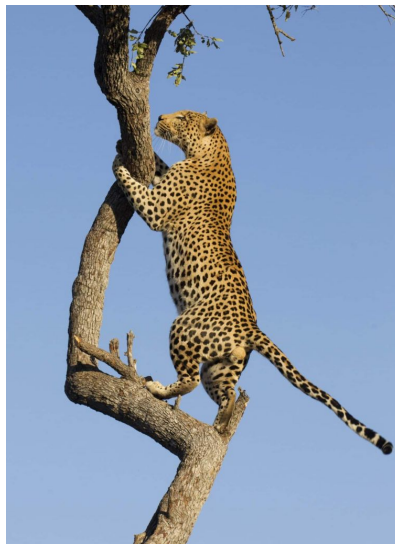


Animals in Complex Environments

Whole-body
sensing

Multi-point contact

Adaptive stability



Animals excel at this - so why don't robots?

Robots need comprehensive awareness to adapt safely.

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<https://explorersweb.com/apes-downclimbing-crucial-for-human-arm-development/>
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https://www.youtube.com/watch?v=H1PEWGf_1lk&ab_channel=ClimbingTechTips



Legged Robots in Complex Environments

Legged robots increasingly operate in **unstructured** environments



Outdoors



Warehouse



Disaster Sites



Search and Rescue

Versatile mobility

https://www.youtube.com/watch?v=cGb3bF6ZwrQ&ab_channel=MichiganRobotics%3ADynamicLeggedLocomotionLab

https://www.youtube.com/watch?v=Q8KWZB4qTY&ab_channel=DEEPRobotics

<https://bostondynamics.com/blog/starting-on-the-right-foot-with-reinforcement-learning/>



The Contact Detection Gap

Detect foot contact but
miss leg collisions.

Damage | Instability
Navigation failure



https://www.youtube.com/watch?v=aX7KypGlitg&list=PPSV&ab_channel=TheIndependent

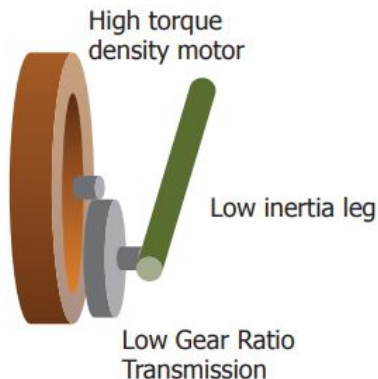


https://www.youtube.com/watch?v=6JqvIRMQU1E&list=PPSV&ab_channel=RobotLocomotionGroup



Current Approaches to Whole-Body Sensing

Torque Sensing



Wensing, TRO 2017

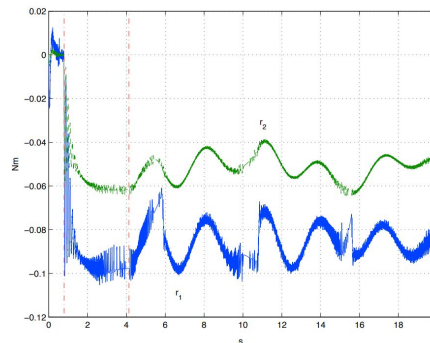
Method

Motor Current
Estimation

Benefits

- Current \propto Torque
- Uses existing hardware in QDDs

Contact Detection

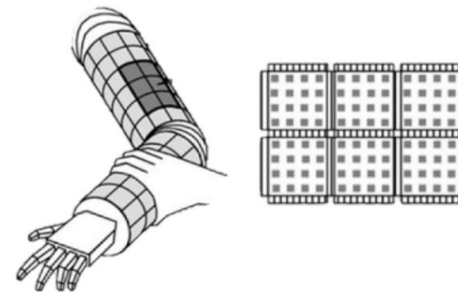


De Luca, ICRA 2005

Momentum
Observer

- Fast detection
- Only encoder

Whole-Body Coverage



Bayer, Micromachines 2022

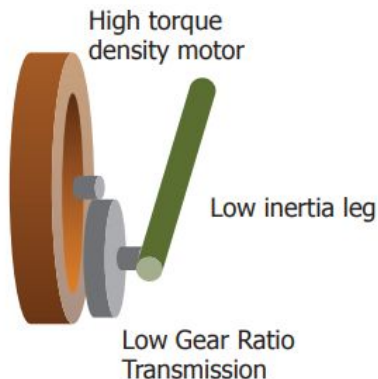
Alternative Sensing
Modalities

- Rich spatial data
- Detects across entire body



Critical Gaps in Existing Methods

Torque Sensing



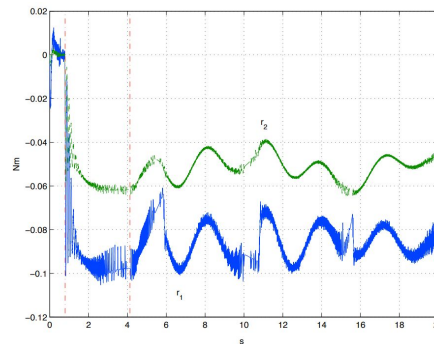
Wensing, TRO 2017

Motor Current
Estimation

Method

Limitations • Not direct measurement

Contact Detection

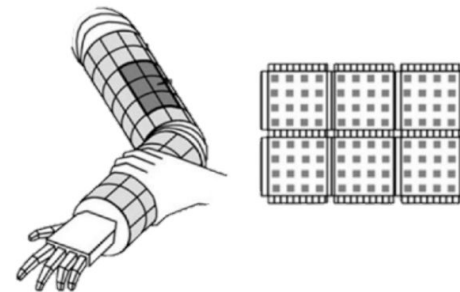


De Luca, ICRA 2005

Momentum
Observer

• Requires friction
modeling

Whole-Body Coverage



Bayer, Micromachines 2022

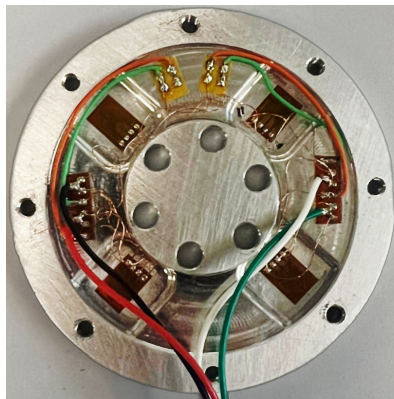
Alternative Sensing
Modalities

• Extensive arrays, fragile



Our Approach: Combined Sensing for Complete Awareness

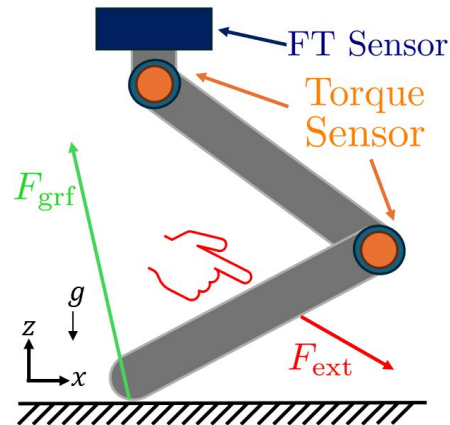
Torque Sensing



Direct Joint
Torque Sensing

- Bypass gearbox friction
- Scales to higher torque

Whole-Body Coverage



Single Hip-Mounted
FT Sensor

- Proximal link detection
- Protected location

Method

Solution

Methodology



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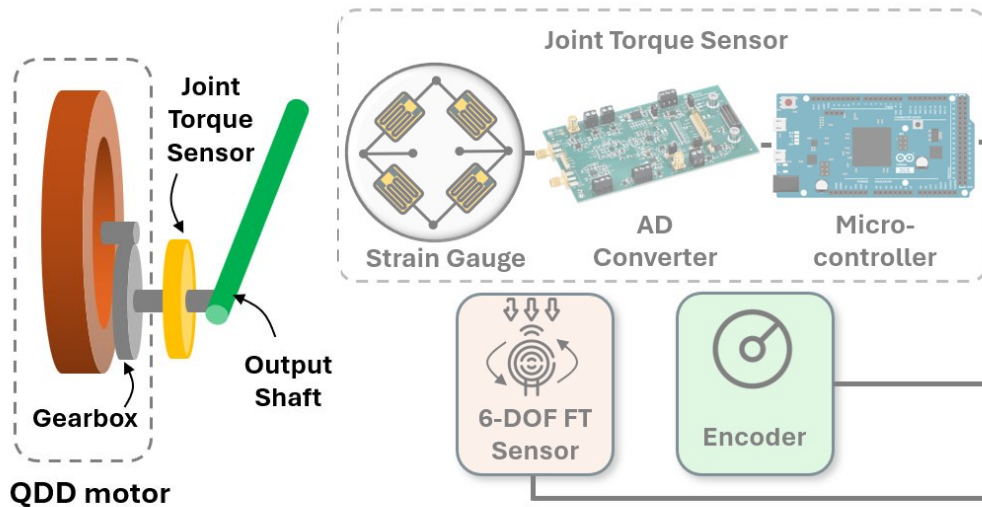


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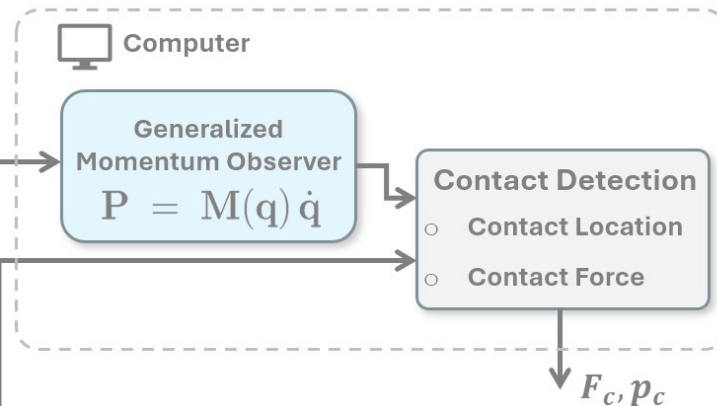


Direct Torque Sensing System Design

(a) Hardware



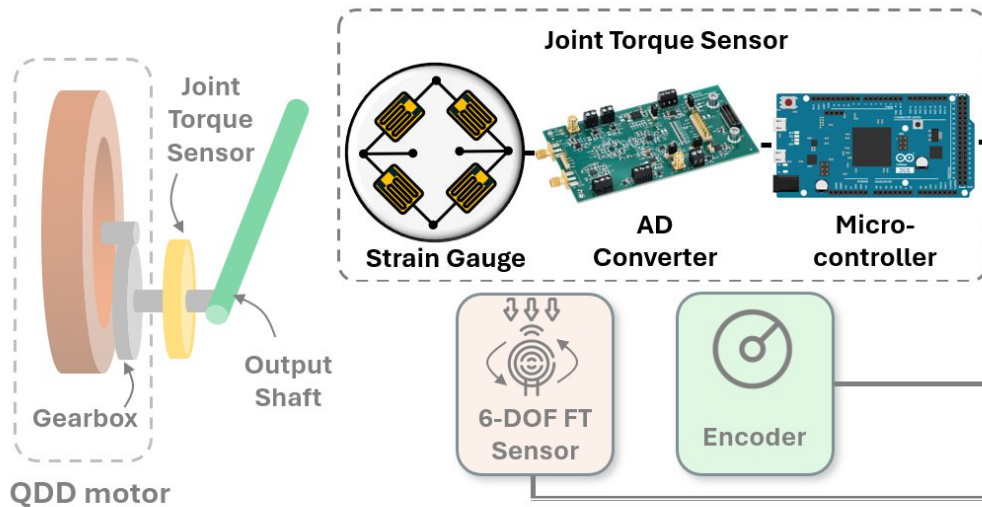
(b) Software



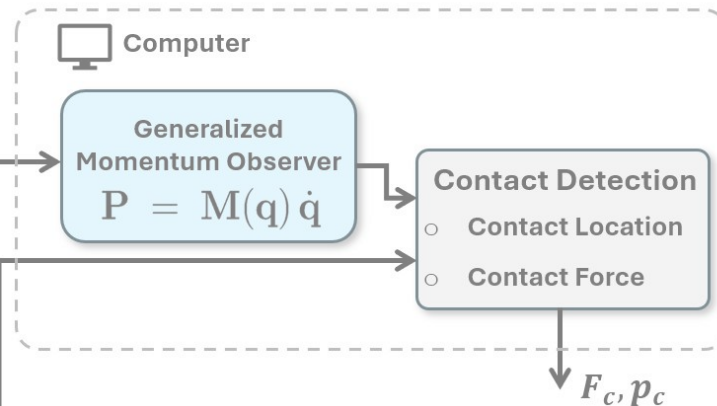


Direct Torque Sensing System Design

(a) Hardware



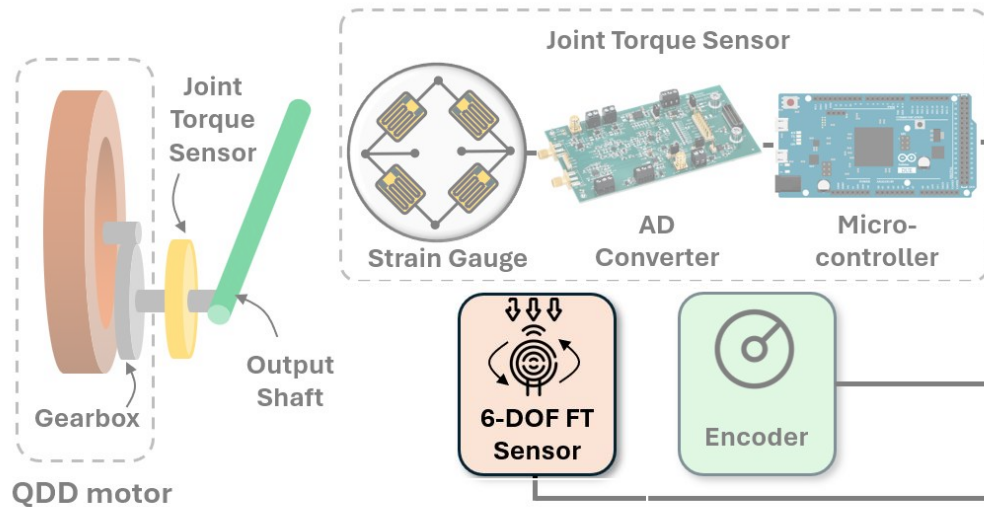
(b) Software



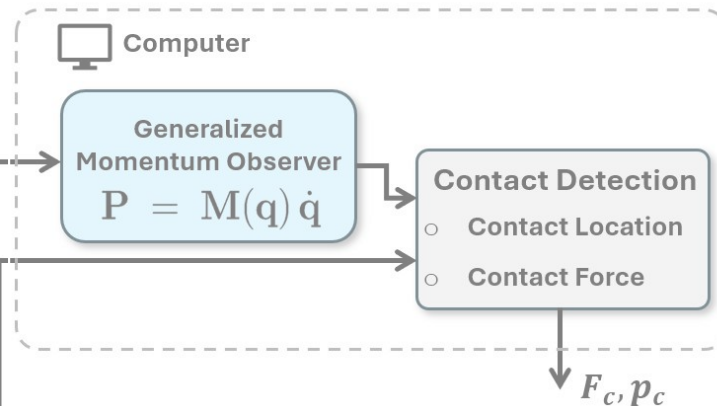


Direct Torque Sensing System Design

(a) Hardware



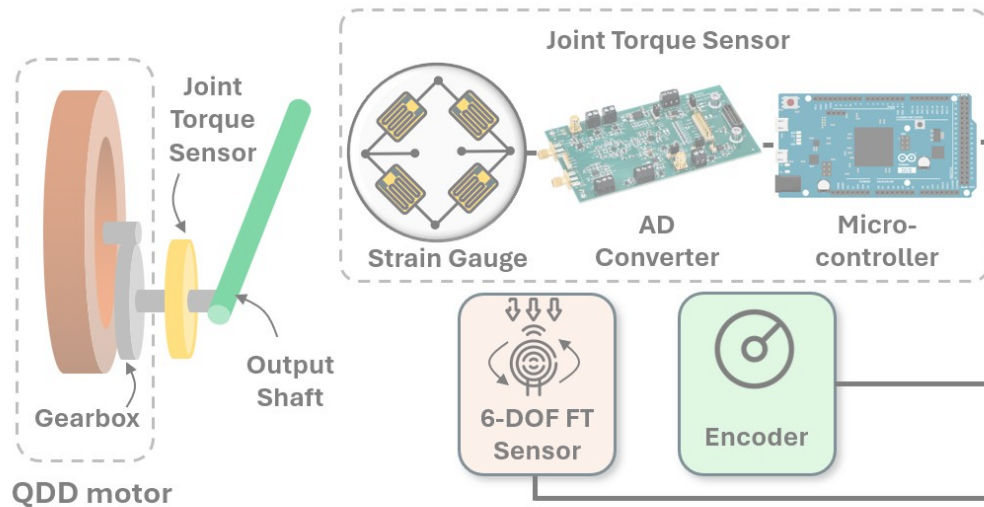
(b) Software



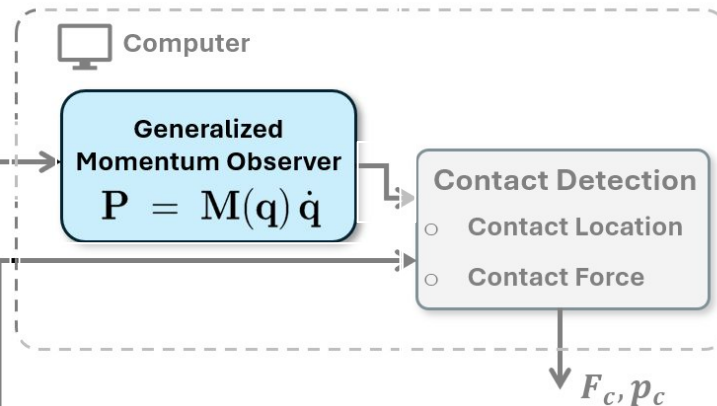


Direct Torque Sensing System Design

(a) Hardware



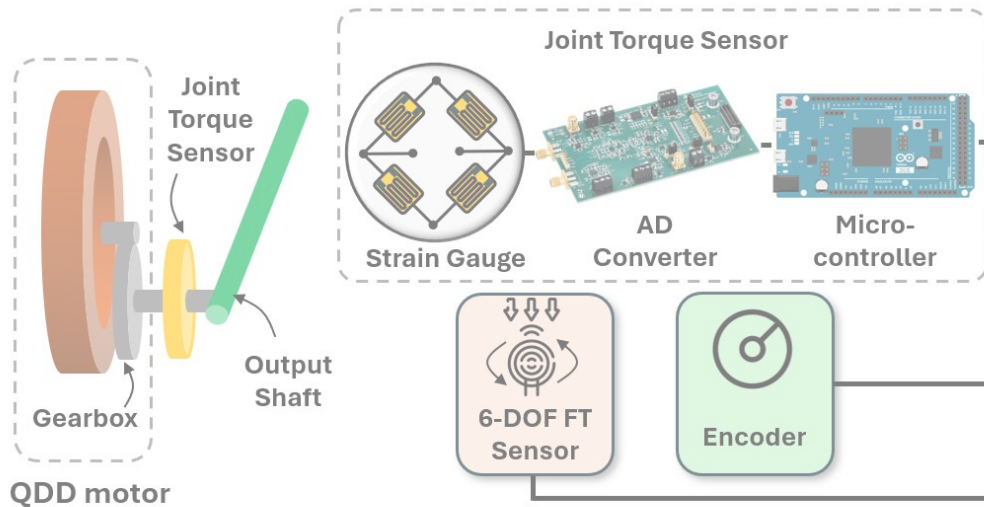
(b) Software



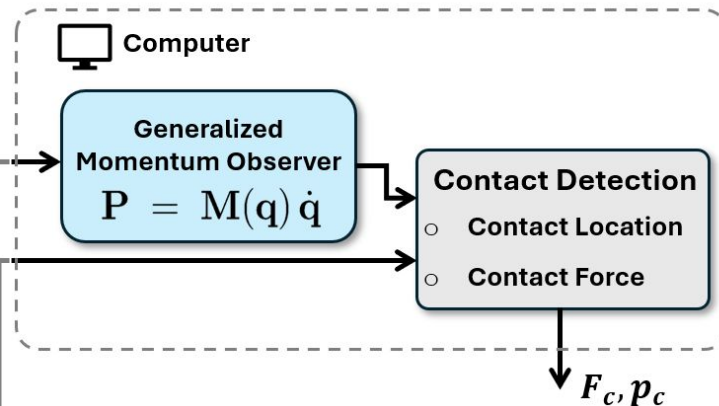


Direct Torque Sensing System Design

(a) Hardware



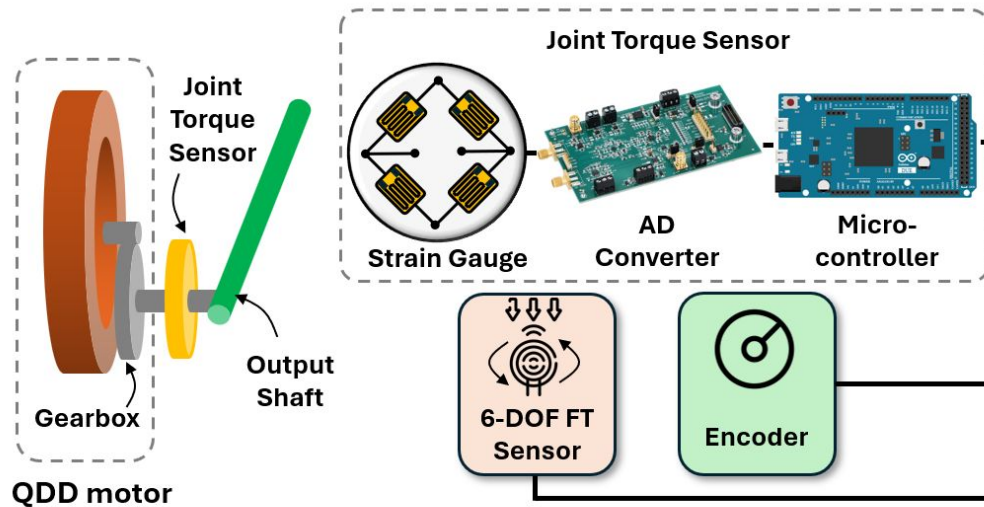
(b) Software



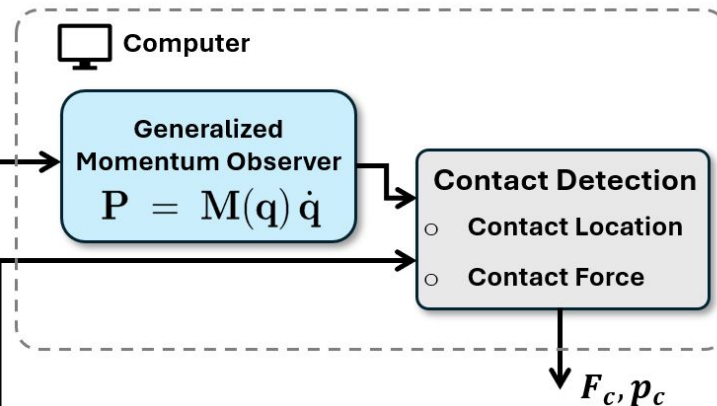


Direct Torque Sensing System Design

(a) Hardware



(b) Software





Robot Dynamics Foundation

$$\mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) + \boldsymbol{\tau}_{\text{fric}} + \boldsymbol{\tau}_{\text{ext}} = \boldsymbol{\tau}_{\text{motor}}$$



Robot Dynamics Foundation

$$\mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) + \boldsymbol{\tau}_{\text{fric}} + \boldsymbol{\tau}_{\text{ext}} = \boldsymbol{\tau}_{\text{motor}}$$

$$- \boldsymbol{\tau}_{\text{fric}}$$

$$- \boldsymbol{\tau}_{\text{fric}}$$



Robot Dynamics Foundation

$$\mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) + \boldsymbol{\tau}_{\text{ext}} = \boldsymbol{\tau}_{\text{motor}} - \boldsymbol{\tau}_{\text{fric}}$$



Robot Dynamics Foundation

$$\mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) + \boldsymbol{\tau}_{\text{ext}} = \boldsymbol{\tau}_{\text{motor}} - \boldsymbol{\tau}_{\text{fric}}$$

$$\boldsymbol{\tau}_{\text{sen}} = \boldsymbol{\tau}_{\text{motor}} - \boldsymbol{\tau}_{\text{fric}}$$



Robot Dynamics Foundation

$$\mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) + \boldsymbol{\tau}_{\text{ext}} = \boldsymbol{\tau}_{\text{sen}}$$



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Robot Dynamics Foundation

$$\mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) + \boldsymbol{\tau}_{\text{ext}} = \boldsymbol{\tau}_{\text{sen}}$$

Generalized Momentum

$$\mathbf{P} = \mathbf{M}(\mathbf{q}) \dot{\mathbf{q}}$$



Robot Dynamics Foundation

$$\mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) + \boldsymbol{\tau}_{\text{ext}} = \boldsymbol{\tau}_{\text{sen}}$$

Generalized Momentum

$$\mathbf{P} = \mathbf{M}(\mathbf{q}) \dot{\mathbf{q}}$$

$$\dot{\mathbf{P}} = \frac{d}{dt} [\mathbf{M}(\mathbf{q}) \dot{\mathbf{q}}]$$



Robot Dynamics Foundation

$$\mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) + \boldsymbol{\tau}_{\text{ext}} = \boldsymbol{\tau}_{\text{sen}}$$

Generalized Momentum

$$\dot{\mathbf{P}} = \mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \dot{\mathbf{M}}(\mathbf{q}) \dot{\mathbf{q}}$$



Robot Dynamics Foundation

$$\mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) + \boldsymbol{\tau}_{\text{ext}} = \boldsymbol{\tau}_{\text{sen}}$$

Generalized Momentum

$$\dot{\mathbf{P}} = \mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \dot{\mathbf{M}}(\mathbf{q}) \dot{\mathbf{q}}$$

$$\dot{\mathbf{M}} = \mathbf{C} + \mathbf{C}^\top$$



Robot Dynamics Foundation

$$\mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) + \boldsymbol{\tau}_{\text{ext}} = \boldsymbol{\tau}_{\text{sen}}$$

Generalized Momentum

$$\dot{\mathbf{P}} = \mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C} \dot{\mathbf{q}} + \mathbf{C}^T \dot{\mathbf{q}}$$



Momentum Observer

$$\mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) + \boldsymbol{\tau}_{\text{ext}} = \boldsymbol{\tau}_{\text{sen}}$$

$$\dot{\mathbf{P}} = \mathbf{M}(\mathbf{q}) \ddot{\mathbf{q}} + \mathbf{C} \dot{\mathbf{q}} + \mathbf{C}^T \dot{\mathbf{q}}$$



Momentum Observer

$$\dot{\mathbf{P}} = \mathbf{C}^\top \dot{\mathbf{q}} - \mathbf{g} + \boldsymbol{\tau}_{\text{sen}} - \boldsymbol{\tau}_{\text{ext}}$$



Generalized Momentum

$$\dot{\mathbf{P}} = \mathbf{C}^\top \dot{\mathbf{q}} - \mathbf{g} + \boldsymbol{\tau}_{\text{sen}} - \boldsymbol{\tau}_{\text{ext}}$$

$$\dot{\mathbf{P}} = \mathbf{u} - \boldsymbol{\tau}_{\text{ext}}$$



Residual for Contact Detection

$$\mathbf{r}(t) = \mathbf{K} \left[\mathbf{P}(t) - \mathbf{p}_{\text{int}}(t) - \mathbf{P}_0 \right]$$

$$\dot{\mathbf{P}} = \mathbf{u} - \boldsymbol{\tau}_{\text{ext}} \quad \rightarrow \quad \mathbf{p}_{\text{int}}(t + \Delta t) = \mathbf{p}_{\text{int}}(t) + \left[\mathbf{u} + \mathbf{r}(t) \right] \Delta t$$

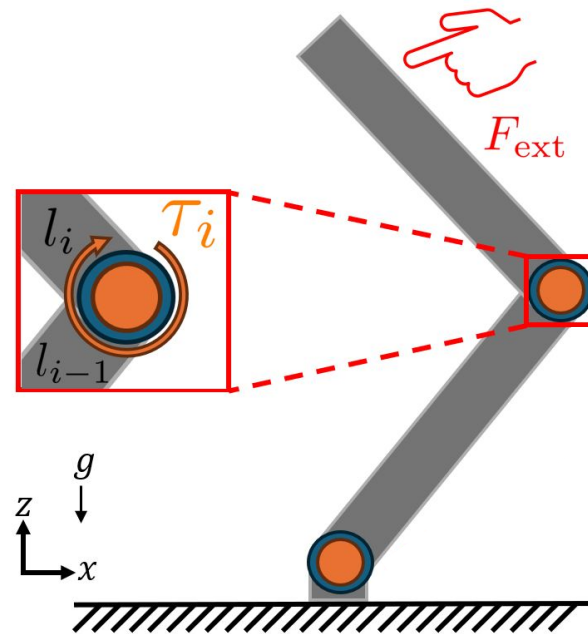


Residual for Collision Link Identification

$$r_i(t) \neq 0 \text{ for } i = 1, \dots, c$$

$$r_j(t) = 0 \text{ for } j = c + 1, \dots, n$$

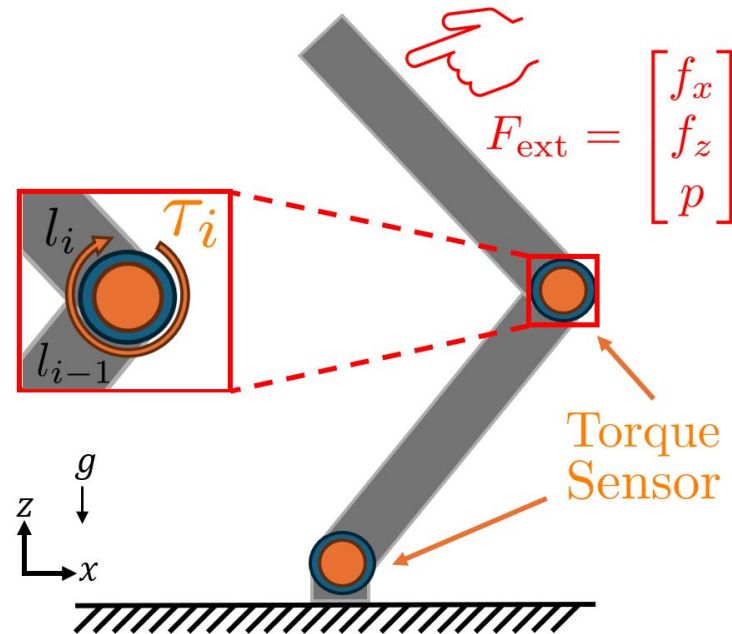
$$c = \max\{i \in \{1, \dots, n\} : |r_i(t)| > \epsilon_{\text{res}}\}$$





The Underdetermined Contact Problem

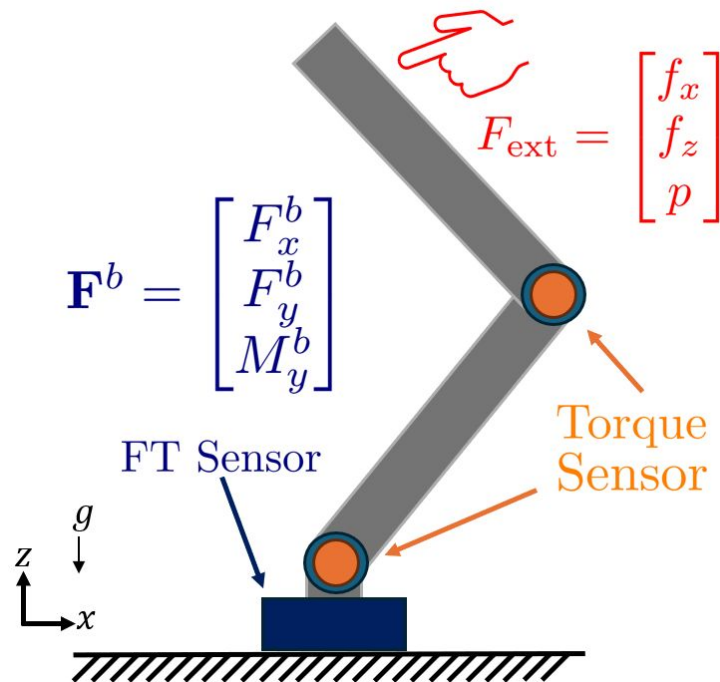
- 3 unknowns
- 2 known measurements
- Underdetermined system





Contact Detection → Contact Localization

- Base FT Sensor - 3 additional measurements
- Proximal to any contactable link



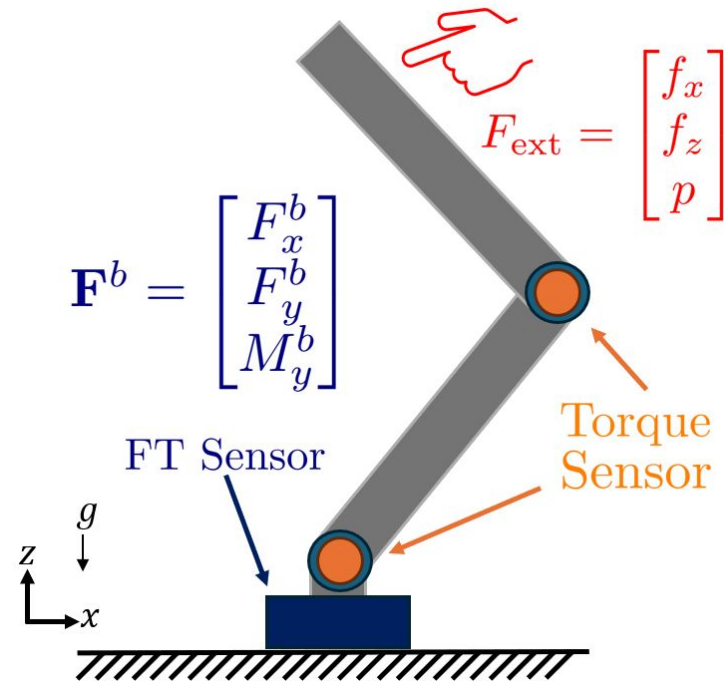


Force Calculation

$$\mathbf{w} = \mathbf{S}(\mathbf{C}\dot{\mathbf{q}} + \mathbf{g} - \mathbf{B} \boldsymbol{\tau}_{\text{sen}})$$

$$\mathbf{F}^u = \mathbf{w} - \mathbf{F}^b$$

$$\mathbf{F}_c = -[F_x^u, F_z^u]^\top$$



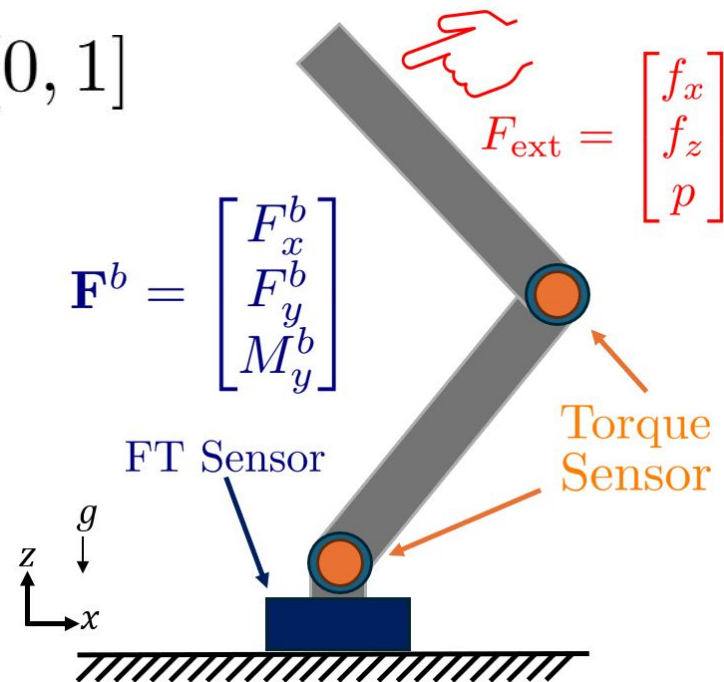


Position Calculation

$$\mathbf{p}_c = \mathbf{p}_1 + \alpha (\mathbf{p}_2 - \mathbf{p}_1), \alpha \in [0, 1]$$

$$M_y^u + \mathbf{p}_c \wedge \mathbf{F}_{xz}^u = 0$$

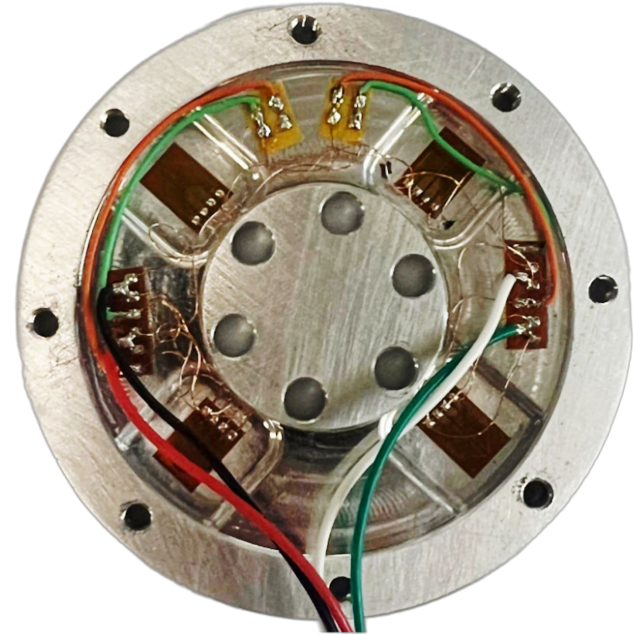
$$\alpha = - \frac{M_y^u + \mathbf{p}_1 \wedge \mathbf{F}_{xz}^u}{(\mathbf{p}_2 - \mathbf{p}_1) \wedge \mathbf{F}_{xz}^u}$$





Custom Joint Torque Sensor Design

- 1 k Ω strain gauges
- Full Wheatstone bridge
- 5 V excitation
- Differential output
- 6061 Aluminum Alloy
- Under \$32





Sensor Calculations

- $GF = 2$ (gauge factor)
- $V_{\text{ex}} = 5\text{V}$ (excitation voltage)
- ϵ = strain

$$\frac{\Delta R}{R} = GF \epsilon$$

$$V_o = V_{\text{ex}} \times \frac{\Delta R/R}{4}$$



Sensor Calculations

- $GF = 2$ (gauge factor)
- $V_{\text{ex}} = 5\text{V}$ (excitation voltage)
- ϵ = strain

$$V_o = V_{\text{ex}} \times \frac{GF \epsilon}{4}$$



Sensor Calculations

$$\text{LSB} = V_{\text{ref}}/2^{24} \qquad V_o = V_{\text{ex}} \times \frac{\text{GF} \epsilon}{4}$$



Sensor Calculations

$$\epsilon_{\min} = \frac{4 V_{\text{ref}}}{\text{GF } V_{\text{ex}} 2^N}$$



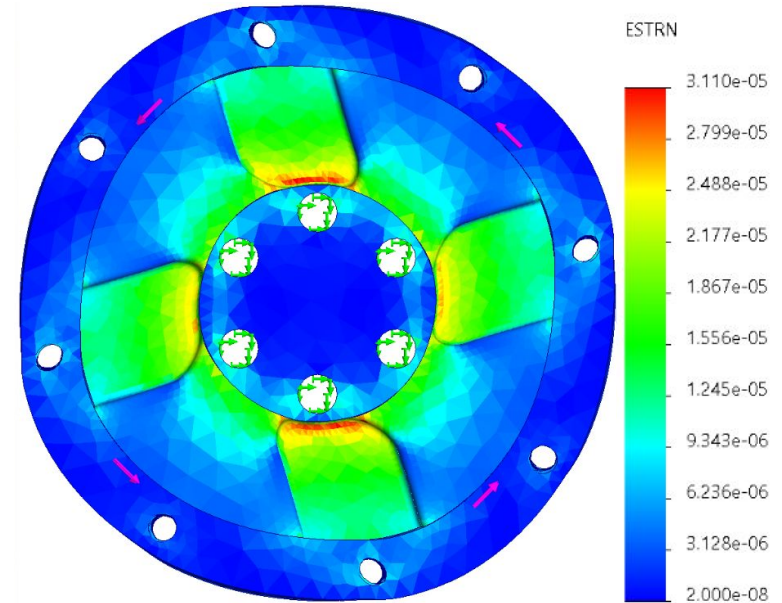
Sensor Calculations

$$\begin{aligned}\epsilon_{\min} &= \frac{4 V_{\text{ref}}}{\text{GF } V_{\text{ex}} 2^N} \approx 5.96 \times 10^{-8} \quad (\text{ideal}) \\ &\approx 1.53 \times 10^{-5} \quad (\text{ENOB})\end{aligned}$$



Finite Element Analysis Validation

- Detects strains under typical torques
 - Ideal = 0.001 Nm
 - ENOB = 0.4 Nm
- 8.5 Nm capacity



FEA with external torque of 0.4 Nm

Experiments and Results



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Simulation Study Overview

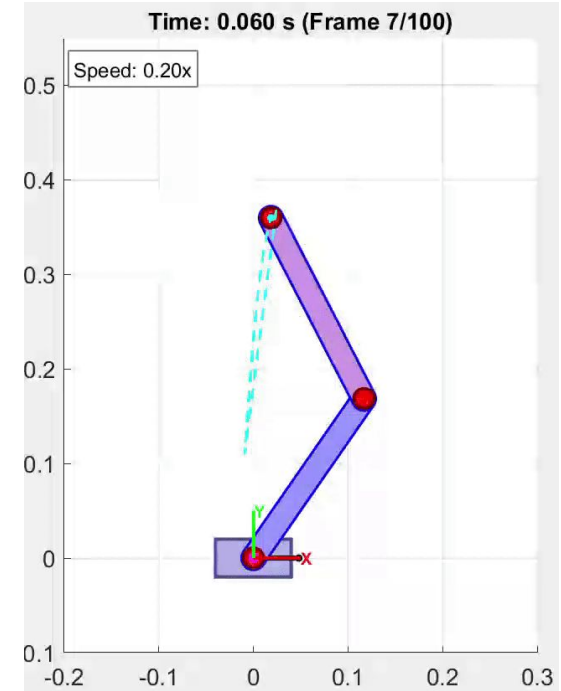
- **Platform:** MATLAB ODE45
- Physical parameters from actual robot
- Virtual joints at base for FT sensor emulation
- PD controller at **1kHz**
- Contact applied at **$t = 0.5s$**
- **Test Scenarios:**
 - Scenario 1: 5N force on Link 1 ($\alpha = 0.5, -\pi/3$ rad)
 - Scenario 2: 7N force on Link 2 ($\alpha = 0.8, -\pi/3$ rad)



Fixed-Base Simulation

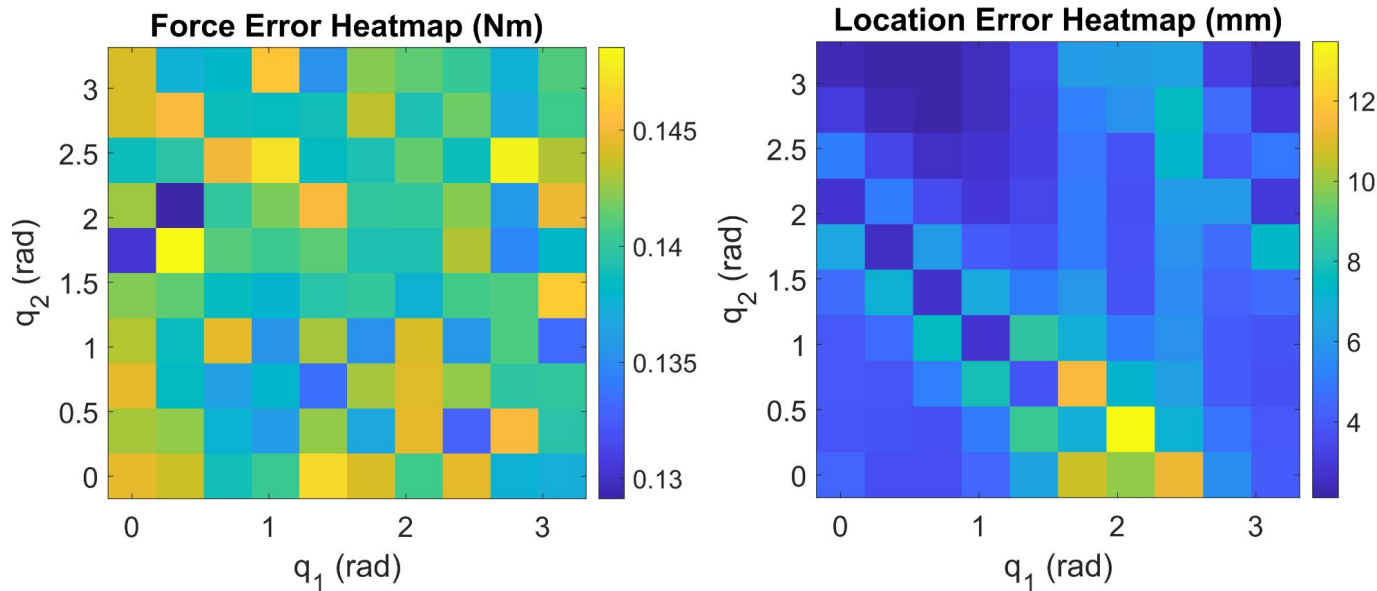
TABLE III: Results of Fixed-Base Simulation

Scenario	Force Errors (N)			Position Errors (mm)		
	F_x	F_z	$ \mathbf{F} $	p_x	p_z	$ \mathbf{p} $
Test 1 Mean	-0.008	-0.008	0.112	1	0	3
STD	0.089	0.090	0.058	4	1	2
Test 2 Mean	0.002	-0.006	0.142	0	2	2
STD	0.108	0.111	0.059	2	1	1





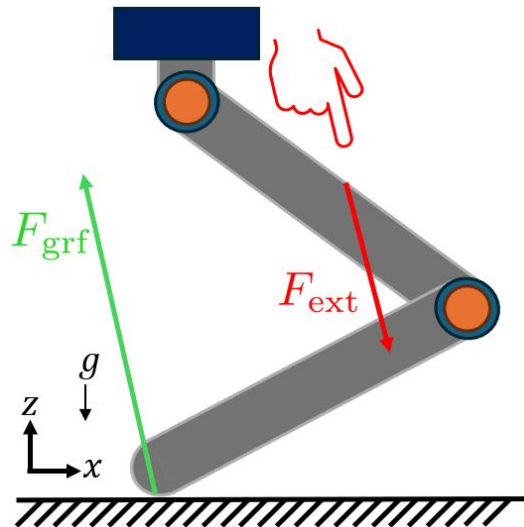
Fixed-Base Simulation Parametric Sweep of Configurations



Results: $<13.5\text{m}$ localization and $<0.15\text{N}$ force error



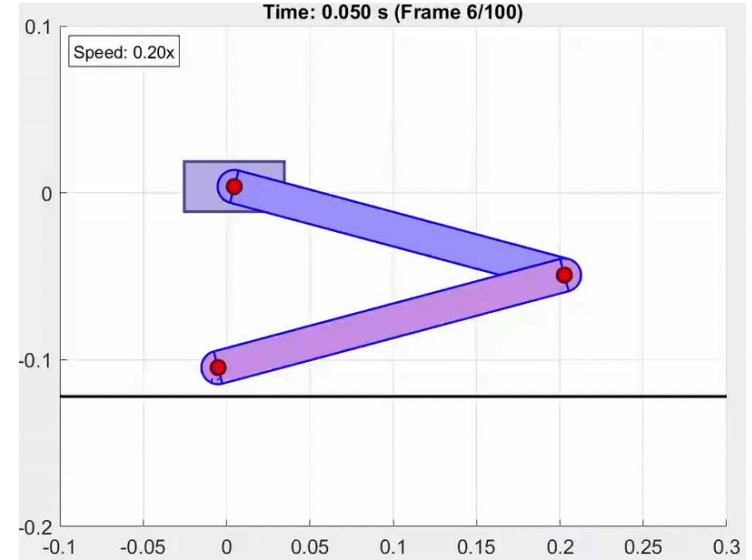
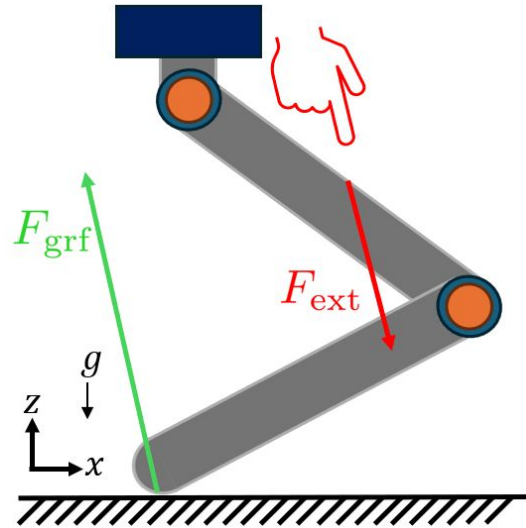
Floating-Base Simulation



- Base can move in x and z directions
- Two additional virtual joints for base translation

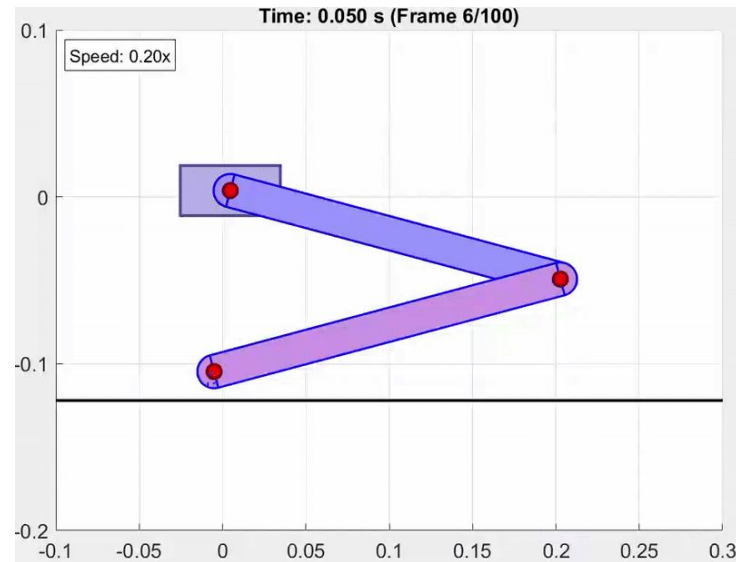
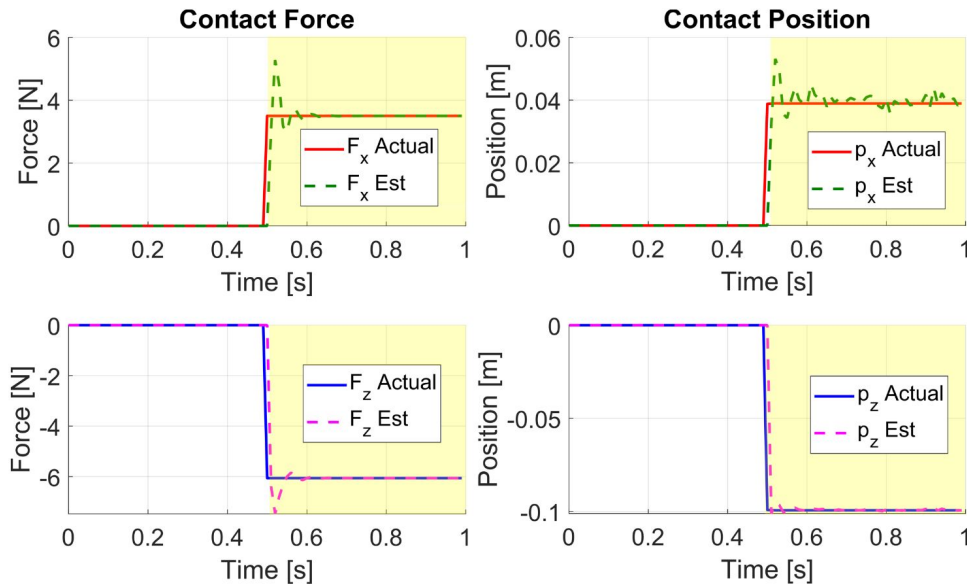


Floating-Base Simulation





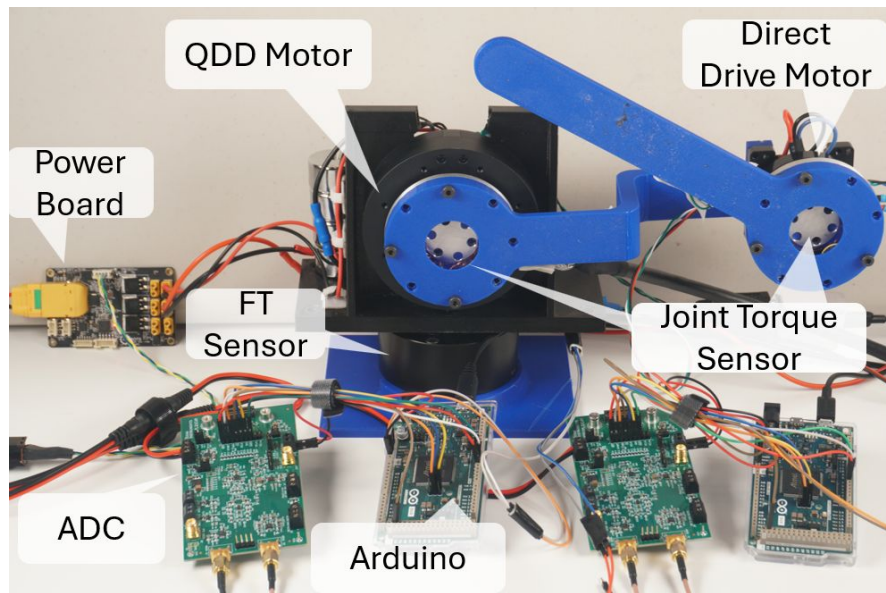
Simulation Performance: Floating Base



Results: Sub-cm localization and $<0.2\text{N}$ force error



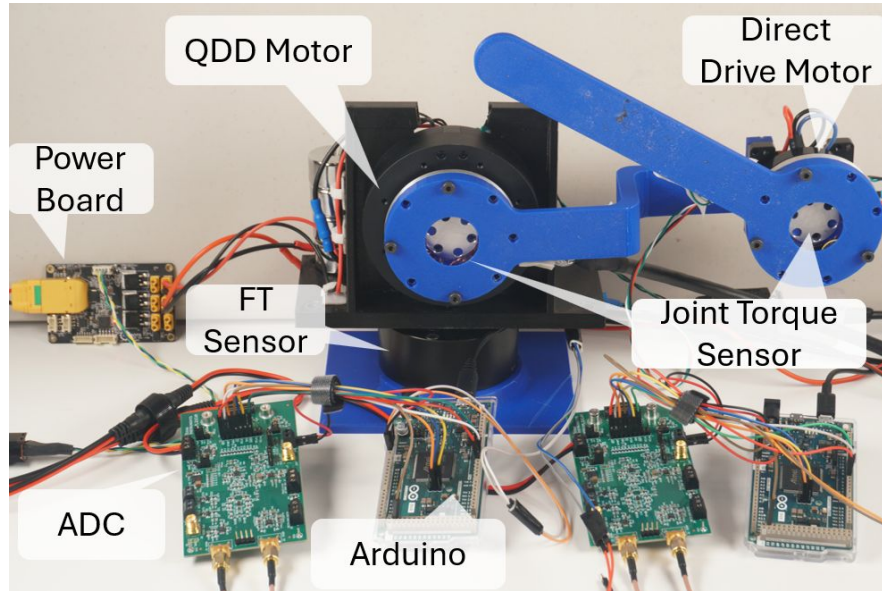
Hardware Experimental Setup: Fixed-Base



- 2-DOF planar leg testbed
- 3-4 kSps, 24-bit ADC
- Static tests: 0.05-0.5kg loads
- Positions: 25%, 50%, 75%, 100%



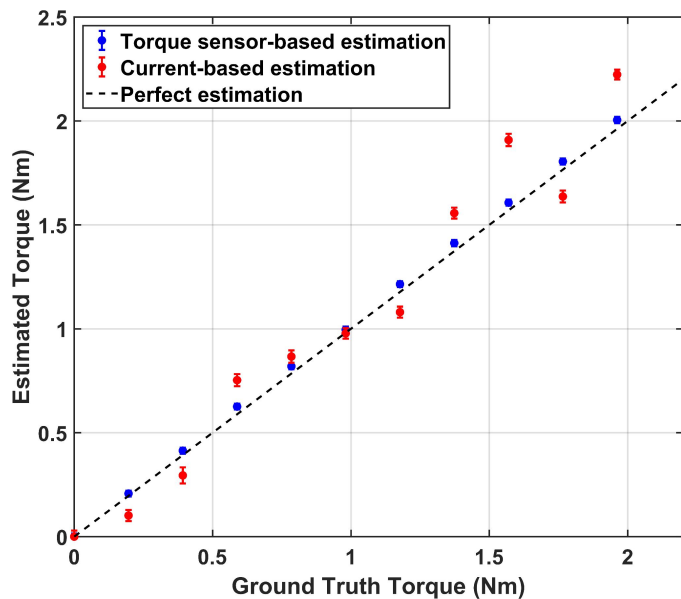
Contact Localization Results: Fixed-Base



Configuration	Load (kg)	Location Error RMS (mm)	Force Error RMS (N)
Link 1	0.1	8.89	0.129
	0.5	7.91	0.174
Link 2	0.05	4.09	0.045
	0.1	4.87	0.106



Joint Torque Sensor Characterization



Sensor 1:

$$y = 0.0115x + 5.0069, \text{ with } R^2 = 0.9999$$

Sensor 2:

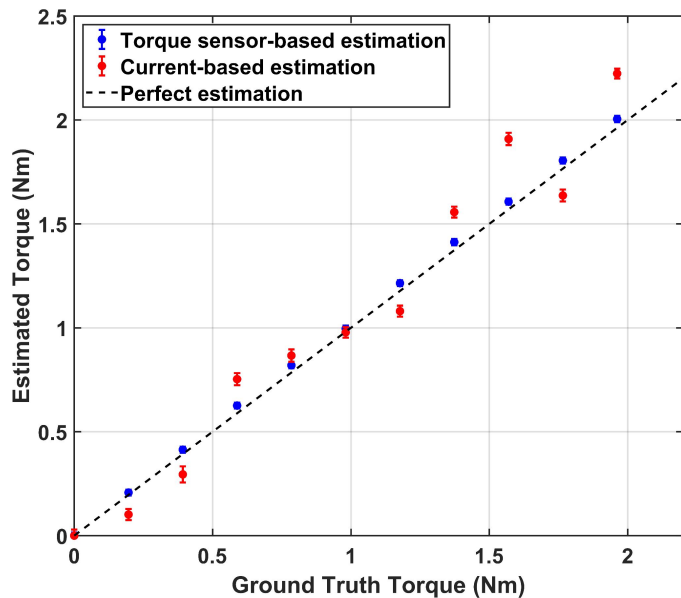
$$y = -0.0108x - 2.3260, \text{ with } R^2 = 0.9991$$

Sensor: **0.0317 RMSE**

Motor Current: **0.1638 RMSE**



Sensor Performance



- 96.4% accuracy relative to ground truth
- MAE: 0.0286 Nm (practical resolution)

Sensor: **0.0317 RMSE**

Motor Current: **0.1638 RMSE**

Conclusions and Discussion



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Summary

- **Why This Matters:** Direct torque sensing, real time, single FT sensor
- **Advantage:** Friction-agnostic approach, scalable to any joint count, simpler than tactile arrays
- **Performance:** 96.4% sensor accuracy, sub-cm localization, $<0.2\text{N}$ force errors
- **Limitation:** Multiple simultaneous contacts, only tested in quasi-static



Future Work

- **Additional sensing modalities:** Handle concurrent collision points
- **Dynamic Testing:** Validation during active locomotion

Q&A

Thanks for Listening!

Jared Grinberg



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