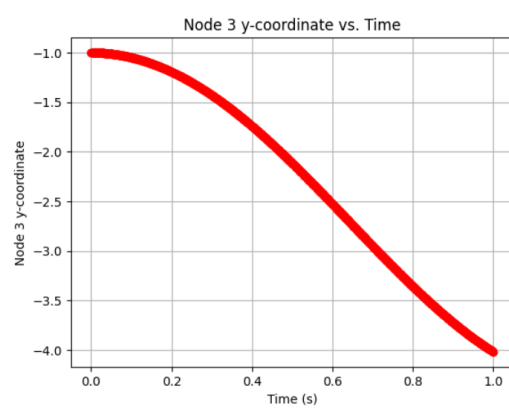
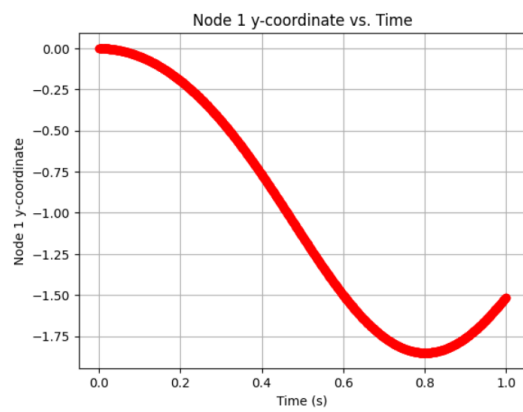
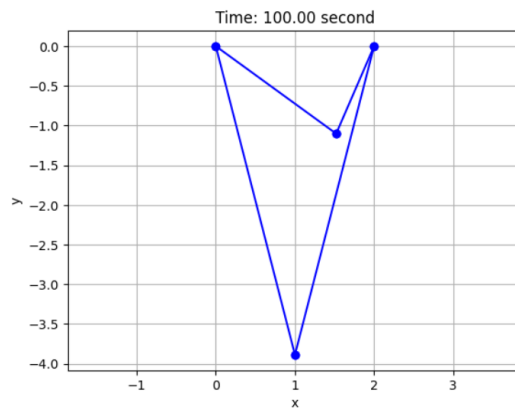
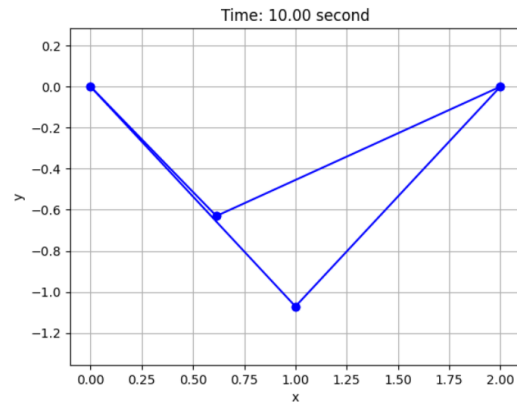
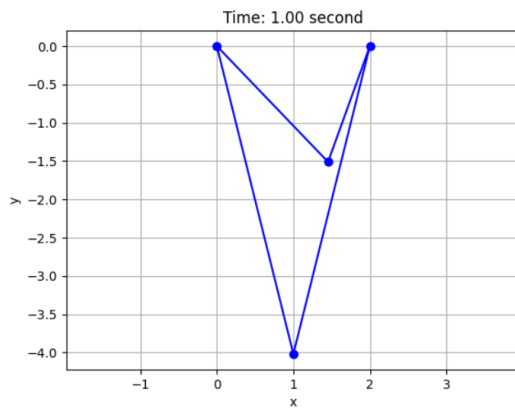
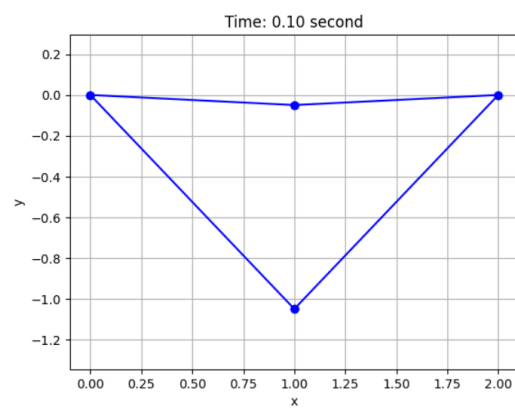
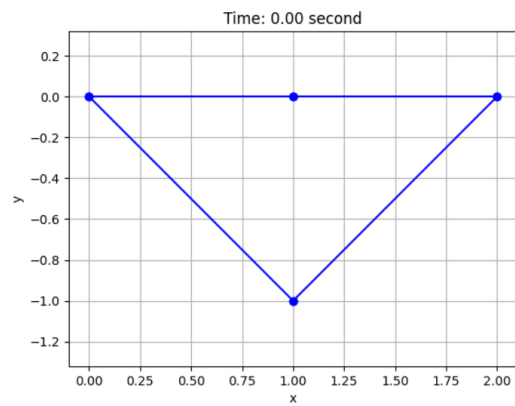
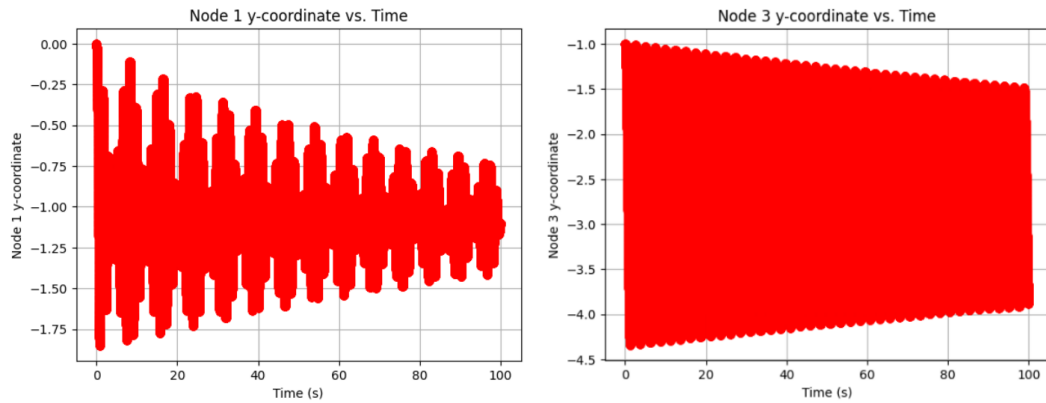


Simulation of (b) by implicit method with $\Delta t = 0.001$





1.

Known : current position \underline{x}_{old} , current velocity \underline{u}_{old} , nodes.txt, spring.txt
 unknown : next position \underline{x}_{new} , next velocity \underline{u}_{new}

nodes.txt : position of each node
 $\begin{bmatrix} x_1 & y_1 \\ x_2 & y_2 \\ \vdots & \vdots \\ x_n & y_n \end{bmatrix} \rightarrow \text{node } i$
 $\Rightarrow \underline{x}_0 = \begin{bmatrix} x_1 \\ y_1 \\ \vdots \\ x_n \\ y_n \end{bmatrix}$

spring.txt
 $\begin{bmatrix} a_1 & b_1 & k_1 \\ \vdots & \vdots & \vdots \\ a_m & b_m & k_m \end{bmatrix} \rightarrow \text{spring } m$
 node a_i and node b_i are connected with spring constant k_i

index matrix $M_{ind} = \begin{bmatrix} 2a_1 & 2a_1+1 & 2b_1 & 2b_1+1 \\ \vdots & \vdots & \vdots & \vdots \\ 2a_m & 2a_m+1 & 2b_m & 2b_m+1 \end{bmatrix}$

stiffness matrix $M_s = [k_1 \ k_2 \ \dots \ k_m]^T$
 mass $m = [m_1 \ m_2 \ \dots \ m_n]^T$

reference spring lengths $l = \begin{bmatrix} \sqrt{(x_0[M_{ind},1] - x_0[M_{ind},3])^2 + (x_0[M_{ind},2] - x_0[M_{ind},4])^2} \\ \vdots \\ \sqrt{(x_0[M_{ind},1] - x_0[M_{ind},3])^2 + (\dots)^2} \end{bmatrix}$
 $M_{ind,i,j} = M_{ind}[i,j]$
 row col.

① Get spring force
 $\underline{f}_s = \text{function } \nabla E_s(x_i, y_i, x_j, y_j, l_k, k)$
 $E_s = \frac{1}{2} k l_k \epsilon^2$, $\epsilon = \frac{\sqrt{(x_i - x_j)^2 + (y_i - y_j)^2}}{l_k} - 1$
 $\underline{f}_s = (k l_k \epsilon) (\nabla \epsilon)$

② Get spring Jacobian
 $\underline{J}_s = \text{function } \nabla^2 E_s(x_i, y_i, x_j, y_j, l_k, k)$

Get total force and Jacobian

$$M\ddot{x} + \frac{\partial E_s}{\partial x} - f_{ext} = 0$$

$$\Rightarrow \underline{f}_{inertia} + \underline{f}_{spring} - \underline{f}_{ext} = 0$$

$[\underline{f}, \underline{J}] = \text{getForceJacobian}(\underline{x}_{new}, \underline{x}_{old}, \underline{v}_{old}, M_s, M_{ind}, m, \Delta t, l)$

$$\underline{f}_{inertia} = \frac{m}{\Delta t} \left[\frac{\underline{x}_{new} - \underline{x}_{old}}{\Delta t} - \underline{v}_{old} \right]$$

$$\underline{J}_{inertia} = \frac{\text{diag}(m)}{\Delta t^2}$$

$$\underline{f}_{spring} = \text{zeros}(\text{len}(\underline{x}))$$

$$\underline{J}_{spring} = \text{zeros}(\text{len}(\underline{x}), \text{len}(\underline{x}))$$

for i in range(len(M_s)):

$$\text{ind} = M_{ind}[i, :]$$

$$x_i = \underline{x}_{new}[\text{ind}[0]], x_j = \underline{x}_{new}[\text{ind}[2]]$$

$$y_i = \underline{x}_{new}[\text{ind}[1]], y_j = \underline{x}_{new}[\text{ind}[3]]$$

$$\underline{f}_{spring}[\text{ind}] += \nabla E_s(x_i, y_i, x_j, y_j, l[i], M_s[i])$$

$$\underline{J}_{spring}[\text{ind}, \text{ind}] += \nabla^2 E_s(x_i, y_i, x_j, y_j, l[i], M_s[i])$$

$$\underline{f}_{ext} = [0 \ -9.81 \ 0 \ -9.81 \ 0 \ -9.81 \ \dots \ 0 \ -9.81]^T$$

$$\underline{J}_{ext} = \text{zeros}(\text{len}(\underline{x}), \text{len}(\underline{x}))$$

$$\underline{f} = \underline{f}_{inertia} + \underline{f}_{spring} - \underline{f}_{ext}$$

$$\underline{J} = \underline{J}_{inertia} + \underline{J}_{spring} - \underline{J}_{ext}$$

④ For all free nodes, we want to find \underline{x}_{new} such that $\underline{f}_{inertia} + \underline{f}_{spring} - \underline{f}_{ext} = 0$ is satisfied.

$\underline{x}_{new}, \underline{u}_{new} = \text{Integrator}(\underline{x}_{old}, \underline{u}_{old}, \text{DOF}_{free}, M_s, M_{ind}, m, \Delta t)$
 $\underline{x}_{new} = \underline{x}_{old}$
 $\text{eps} = 10^{-6}$ # tolerance
 $\text{err} = 1$

while $\text{err} > \text{eps}$:

$\underline{f}, \underline{J} = \text{getForceJacobian}(\underline{x}_{new}, \underline{x}_{old}, \underline{u}_{old}, M_s, M_{ind}, m, \Delta t, l)$

$\underline{f}_{free} = \underline{f}[\text{DOF}_{free}]$

$\underline{J}_{free} = \underline{J}[\text{DOF}_{free}]$

$\Delta \underline{x}_{free} = \underline{J}_{free} \backslash \underline{f}_{free}$

$\underline{x}_{new}[\text{DOF}_{free}] -= \Delta \underline{x}_{free}$

$\text{err} = \|\underline{f}_{free}\|_2$

$\underline{u}_{new} = \frac{\underline{x}_{new} - \underline{x}_{old}}{\Delta t}$

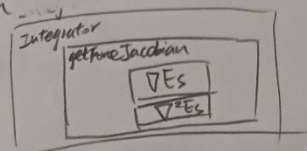
⑤ Main function to solve \underline{x} at each time.

$t = 0 : \Delta t : t_f, \underline{x}, \underline{u} = \text{zeros}(\text{len}(\underline{x}_0), \text{len}(t))$

for i in range($\text{len}(t)-1$):

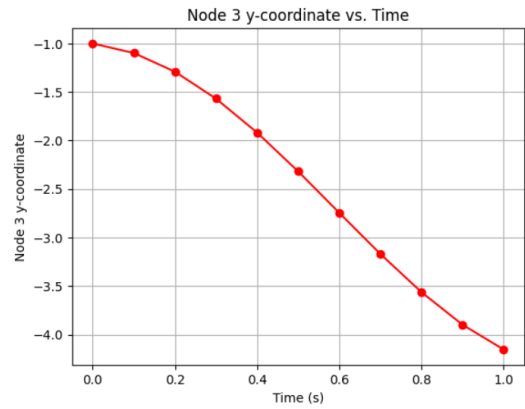
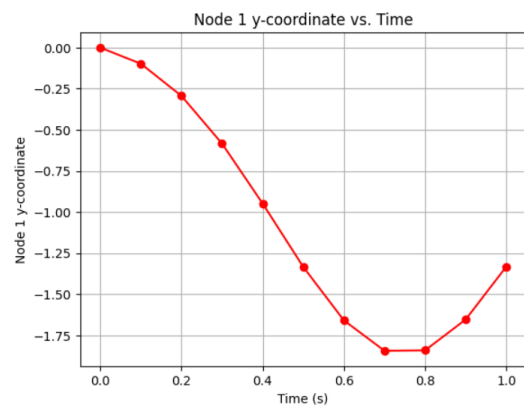
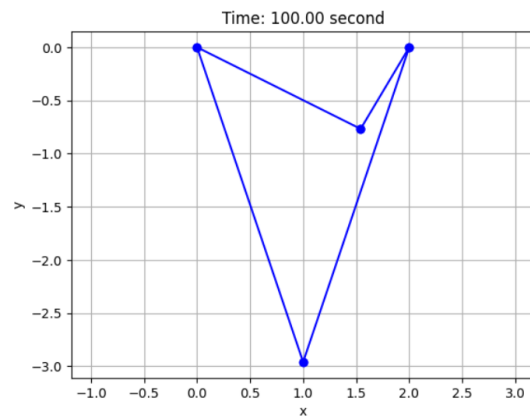
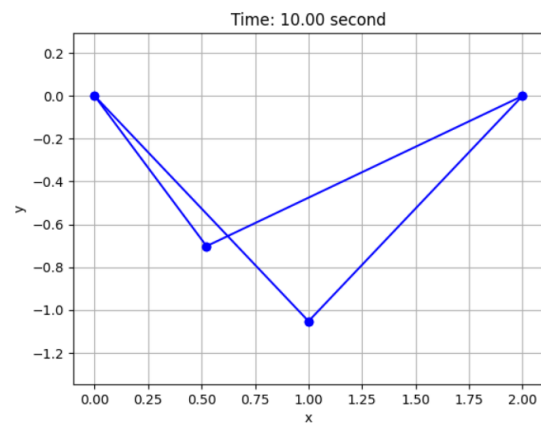
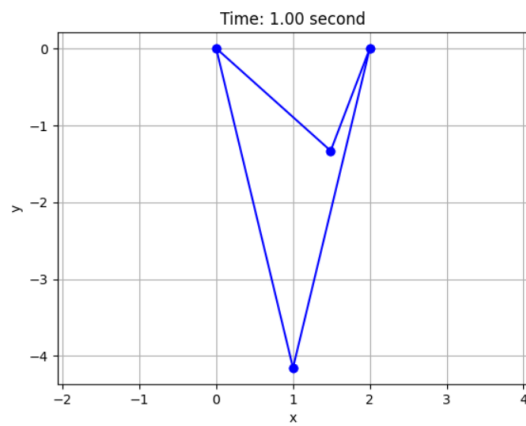
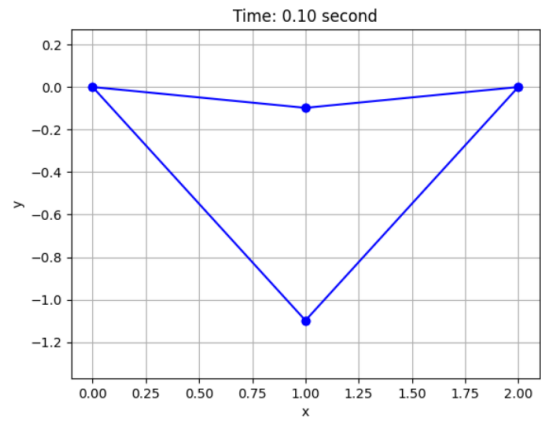
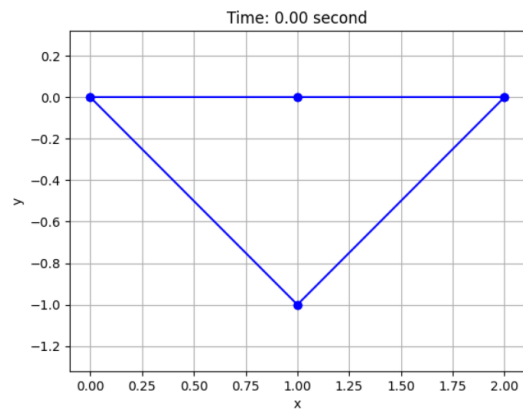
$\underline{x}[:, i+1], \underline{u}[:, i+1] = \text{Integrator}(\underline{x}[:, i], \underline{u}[:, i], \text{DOF}_{free}, M_s, M_{ind}, m, \Delta t)$

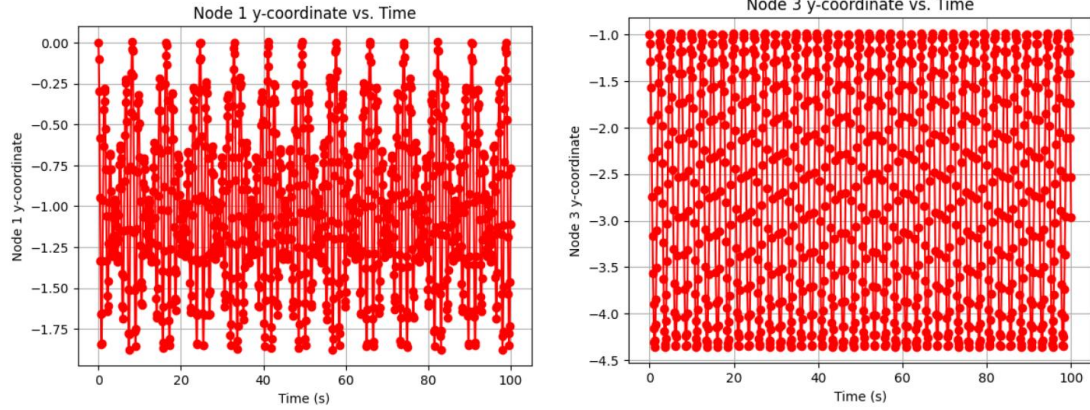
Block diagram



2. I choose $\Delta t = 0.001$ so that the damping effect of implicit method can be minimized but not taking too much time on calculation.

3. Explicit method is preferable for this spring network since there not only is no damping effect but don't diverge at a long sampling time $\Delta t = 0.1$





4. In implicit Euler method, the new position is only related to the old acceleration. If the acceleration of system is increasing, the simulated position won't reach the real position. And, if the acceleration of system is decreasing, the simulated position will go over the real position. This will work like a damper, which will prevent the system from approaching the state without any resistance.

On the other hand, in Newmark- β , the new position is also related to the new acceleration. In addition, the most of time, β equals 0.25 such that the new position is related to the average of new and old acceleration. Therefore, as long as the sampling time is small enough, Newmark- β method can get a good guess of acceleration between current time and next time interval, and a proper next position can be calculated.

5. Simulation of (b) by Newmark- β ($\beta = 0.25$) method with $\Delta t = 0.1$

