GMRT transients search and related issues

Jayanti Prasad

National Center for Radio Astronomy Pune, India (411007)

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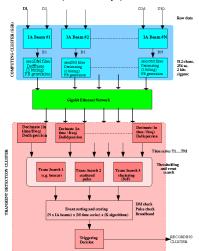
Introduction

A typical transients search pipeline consists of

- Dedispersion
- Matched filtering
- Thresholding
- Oiagnosis

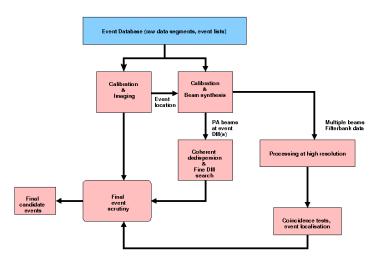
Online

Transient Detection (Real-time Ops)



Offline

Transient Analysis (offline Ops)



False alarms

• The probability of a Gaussian noise signal with zero mean and σ variance, crossing a threshold T (probability of false alarms) is given by

$$P(T) = \int_{T}^{\infty} \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left(-\frac{x^2}{2\sigma^2}\right) = \frac{1}{2} Erfc\left(\frac{T}{\sigma\sqrt{2}}\right) \tag{1}$$

The joint probability of false alarms for N antennas is given by

$$P^{A}(T) = \left[\frac{1}{2} Erfc\left(\frac{T}{\sigma\sqrt{2}}\right)\right]^{N}$$
 (2)

Now if we add the signals from N antennas incoherently then the joint probability of false alarms

$$P^{B}(T) = \frac{1}{2} Erfc\left(\frac{T}{\sigma} \sqrt{\frac{N}{2}}\right)$$
 (3)



If we break N antennas into p incoherent sub-arrays each with N/p antennas

$$P^{c}(T) = \left[\frac{1}{2} Erfc\left(\frac{T}{\sigma} \sqrt{\frac{N}{2p}}\right)\right]^{p} \tag{4}$$

What is the best combination for a given number of antennas N and threshold T?

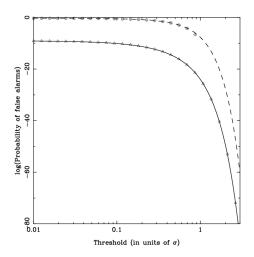


Figure: 1. Probabilities of false alarms $P^A(T)$ (solid line) and $P^B(T)$ (dotted line). . Symbols represent the fraction of events observed above the threshold in a simulated Gaussian noise.

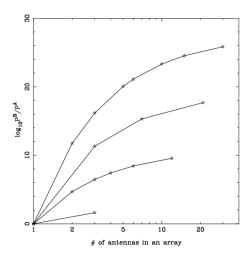


Figure: 2.Probabilities of false alarms P^B and P^A as a function of the number of antennas in a beam for $T=3\sigma$, for a given number of total antennas. The curves from the top are for the total number of antennas N=30,21,12 and 3 respectively.

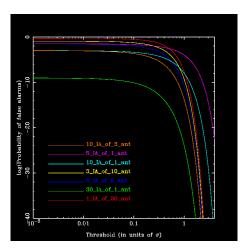


Figure: 3. Probability of false alarms $P^c(T)$ for p incoherent sub-arrays of N antennas. Note that the number of antennas in an IA array is important for high value of threshold.

Single pulse simulations

- How the difference between the actual DM and trial DM changes the
 - location
 - width and
 - Amplitude (SNR)

of a pulse for a given set of parameters $W, \nu, n_{chan}, t_{samp}$ etc.

- How the amplitude of a given pulse changes with the size of smoothing window.
- How zero-dm filtering change the shape and size of a pulse.

Dispersion delay:

$$\tau_f(\text{DM}) \approx K \left[\left(\frac{\text{MHz}}{f} \right)^2 - \left(\frac{\text{MHz}}{f_h} \right)^2 \right] \left(\frac{\text{DM}}{\text{pc cm}^{-3}} \right) \text{sec}$$
 (5)

where $K = 4.154553 \times 10^3$

• Pulse location:

$$\bar{\tau}(\mathsf{DM}) = \frac{\tau_{\mathit{f}_h} + \tau_{\mathit{f}_l}}{2} = \frac{\tau_{\mathit{f}_l}}{2} \tag{6}$$

If the true dispersion measure of a pulse is DM and we dedisperse it with a trial dispersion measure DM+dDM then shift in the location of the pulse is given by

$$\Delta \bar{\tau} = \frac{K}{2} \left(\frac{\text{MHz}}{f_c} \right)^3 \left(\frac{\Delta f}{\text{MHz}} \right) \left(\frac{\text{dDM}}{\text{pc cm}^{-3}} \right) \text{sec}$$
 (7)

If in place of considering the highest frequency channel as the reference i.e., there is no delay for this channel, we consider any other channel f_{ref} as reference

$$au_f(\mathrm{DM}) pprox \mathcal{K} \left[\left(\frac{\mathrm{MHz}}{f} \right)^2 - \left(\frac{\mathrm{MHz}}{f_{\mathrm{ref}}} \right)^2 \right] \left(\frac{\mathrm{DM}}{\mathrm{pc} \ \mathrm{cm}^{-3}} \right) \mathit{sec}$$
 (8)

if $f_{ref} = f_c$, $f_l = f_c - \Delta f/2$, $f_h = f_c + \Delta f/2$ we get

$$\bar{\tau}(DM) = \frac{\tau_{f_h} + \tau_{f_l}}{2} = \frac{K}{2} \frac{3\Delta f^2}{2(f_c^2 - \Delta f^2/4)^2} MHz^2 \left(\frac{DM}{pc \text{ cm}^{-3}}\right)$$
 (9)

then the shift is of the order of Δf^2 .

 Pulse width: If the intrinsic pulse width is W then the observed pulse width can be defined as

$$\mathbf{w} = \mathbf{W} + (\tau_{f_{l}} - \tau_{f_{h}})$$

$$= K \left(\frac{\mathsf{MHz}}{f_{c}}\right)^{3} \left(\frac{\Delta f}{\mathsf{MHz}}\right) \left(\frac{\mathsf{DM}}{\mathsf{pc}\;\mathsf{cm}^{-3}}\right) \mathsf{sec} \tag{10}$$

If the true dispersion measure of a pulse is DM and we dedisperse it with a trial dispersion measure DM+dDM then the change in the width of the pulse is given by

$$\Delta w = K \left(\frac{\text{MHz}}{f_c}\right)^3 \left(\frac{\Delta f}{\text{MHz}}\right) \left(\frac{\text{dDM}}{\text{pc cm}^{-3}}\right) \text{sec} \tag{11}$$

• Pulse amplitude: For a rectangular bandpass function and for a Gaussian shape pulse with width W c the ratio of measured peak flux $S(\delta DM)$ to true flux S to for a DM error δDM is

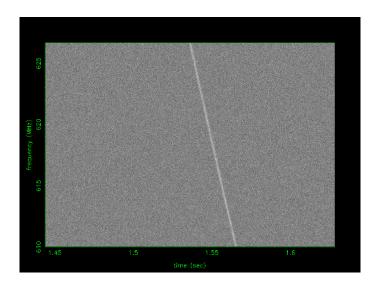
$$\frac{S(\delta DM)}{S} = \frac{\sqrt{\pi}}{2\xi} erfc(\xi) \tag{12}$$

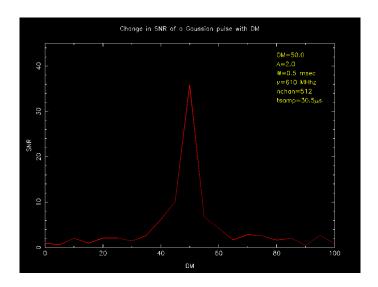
where

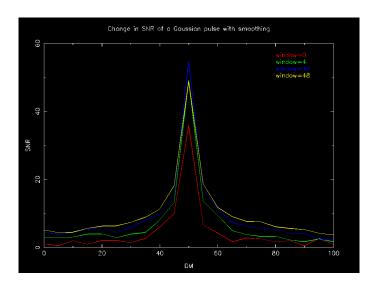
$$\xi = 6.91 \times 10^{-3} \delta DM \frac{\delta \nu}{MHz} \frac{msec}{W} \left(\frac{Ghz}{\nu}\right)^2$$
 (13)

(Cordes & McLaughlin 2003)

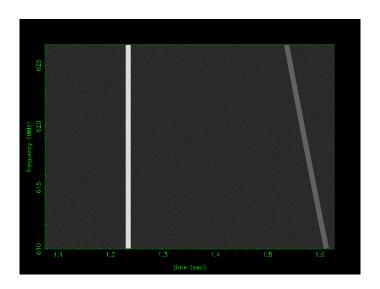
Simulations



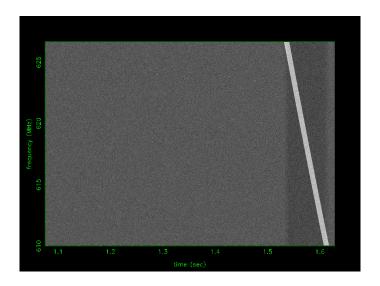




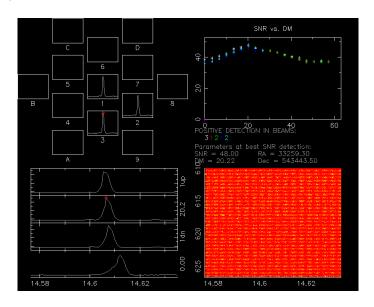
Broad Band RFI



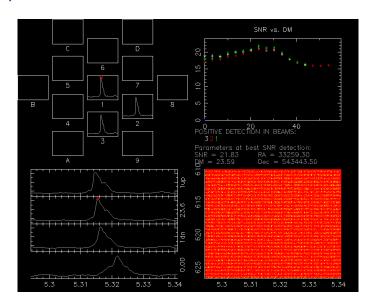
Broad Band RFI removed with zeron DM filtering



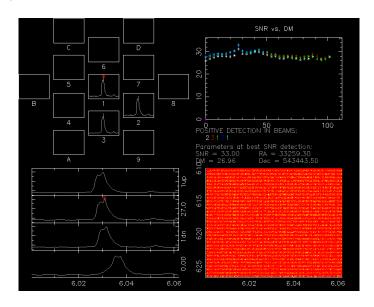
Giant pulse search:



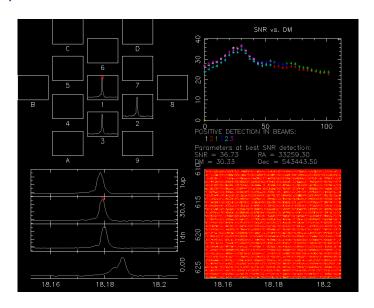
Giant pulse search...



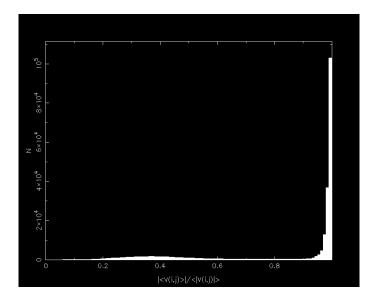
Giant pulse search...



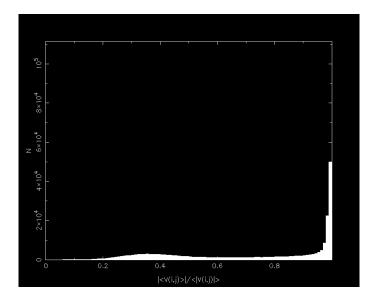
Giant pulse search...



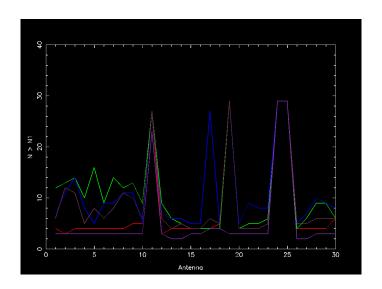
Time averaging visibilities (Flux calibrator)



Time averaging visibilities (Phase calibrator)



Bad Antennas



Thank You!