

# CUSF Flow Simulation Workshop

Jack Brewster

CUED 14/06/2018

# Overview

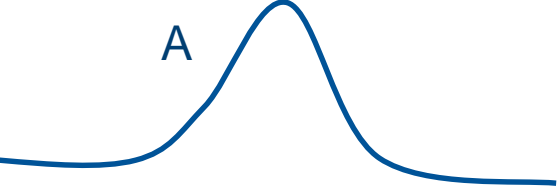
1. Introduction
2. Theory: Finite Volume (FV) methods
3. OpenFoam: Supersonic wedge
4. OpenFoam: Supersonic sphere
5. Theory: Finite Element (FE) methods
6. FEniCS: Cylinder flow
7. Future

# The governing equations in fluid mechanics can often be recast as an advection equation.

- The governing equations in fluid mechanics can often be written as:

$t=0$

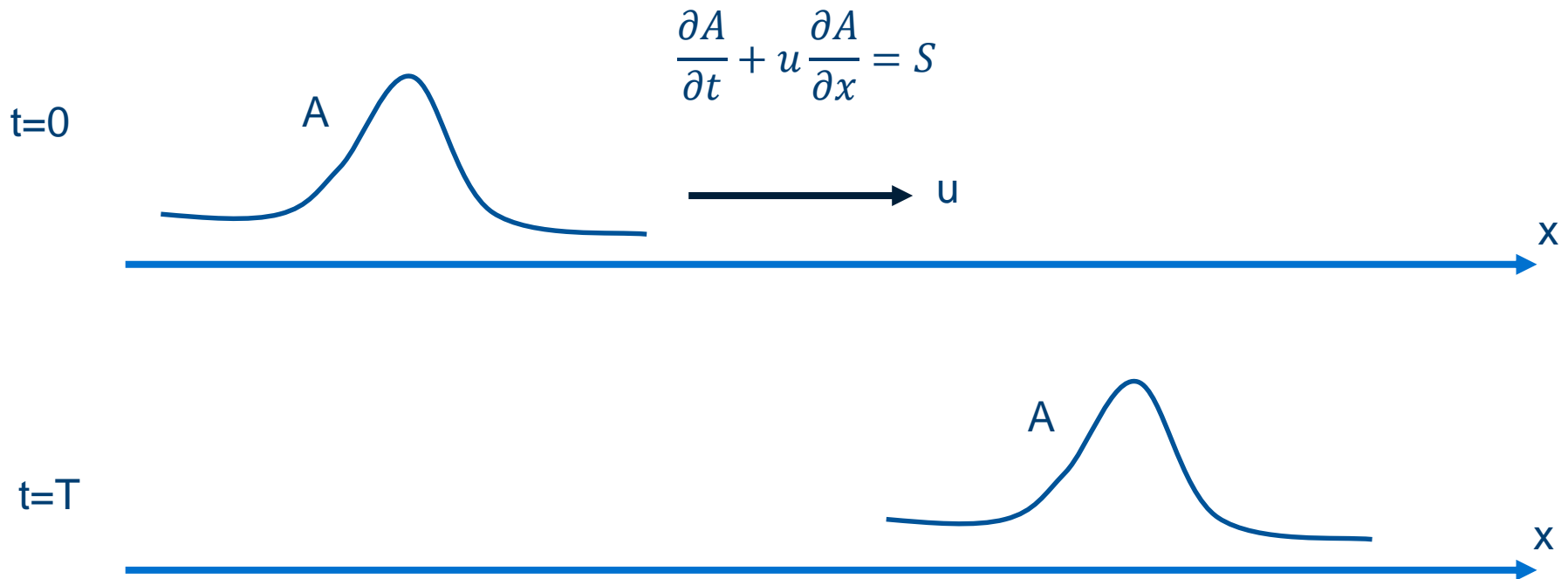
$A$


$$\frac{\partial A}{\partial t} + u \frac{\partial A}{\partial x} = S$$

$x$

# The governing equations in fluid mechanics can often be recast as an advection equation.

- The governing equations in fluid mechanics can often be written as:



# There are three families of methods for solving PDEs.

1. Finite Difference

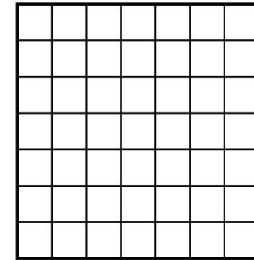
2. Finite Volume

3. Finite Element

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## 1. Finite Difference – the intuitive approach

$$\frac{\partial A}{\partial t} \approx \frac{A_{t+\delta t} - A_t}{\delta t}, \quad \frac{\partial A}{\partial x} \approx \frac{A_{x+\delta x} - A_x}{\delta x}$$



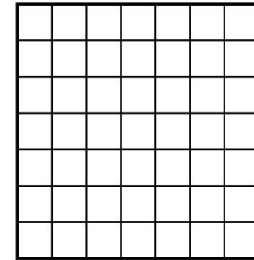
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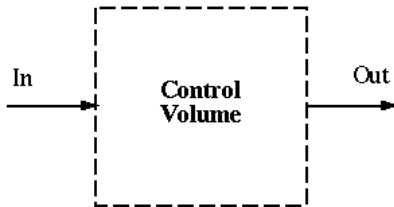
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## 2. Finite Volume – the engineer's approach



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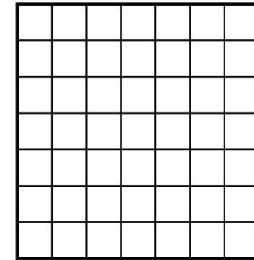
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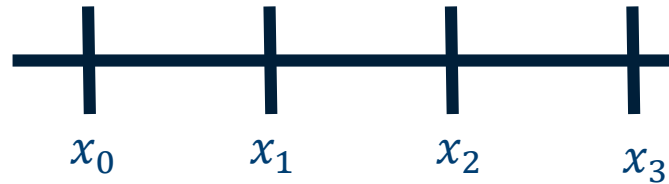
## 3. Finite Element – the mathematician's approach





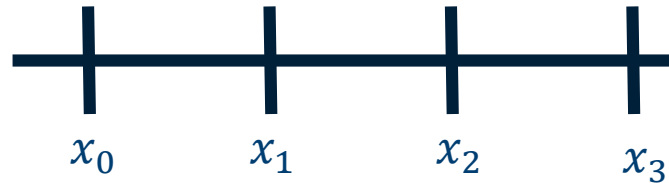
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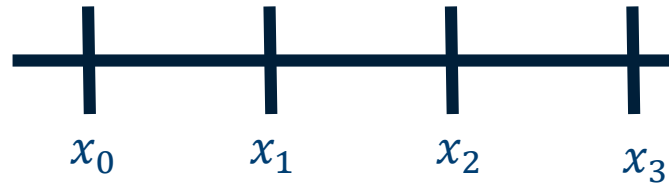
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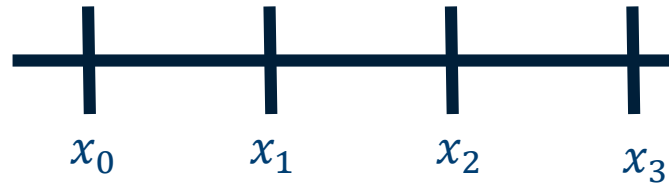
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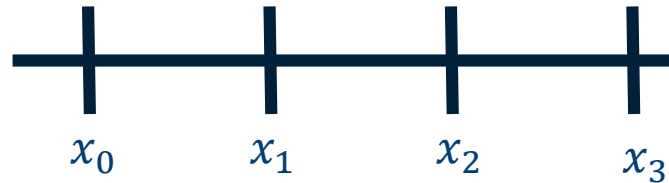
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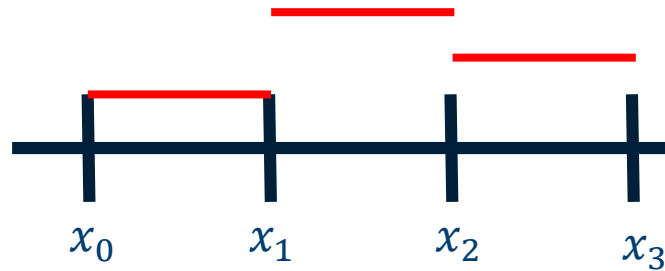
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- Divide by cell volume to get average:  $\frac{\partial \bar{A}}{\partial t} = \frac{1}{\Delta x} [Au]_{x_1}^{x_0} + \bar{S}$
- Replace the time derivative with finite difference:  $\frac{\bar{A}_{t+\delta t} - \bar{A}_t}{\delta t} = \frac{1}{\Delta x} [Au]_{x_1}^{x_0} + \bar{S}$

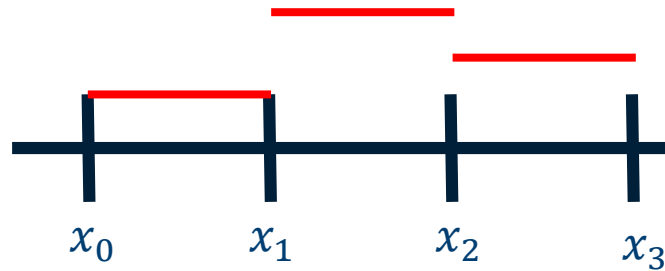
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- We interpret  $\bar{A}$  as the value at the cell centre

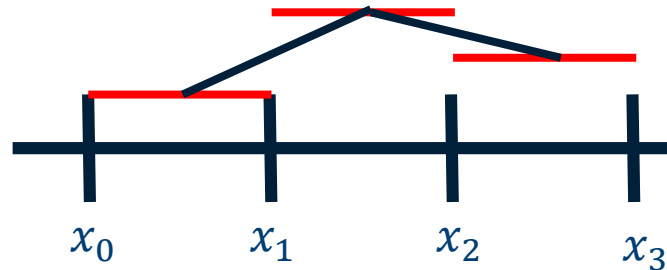


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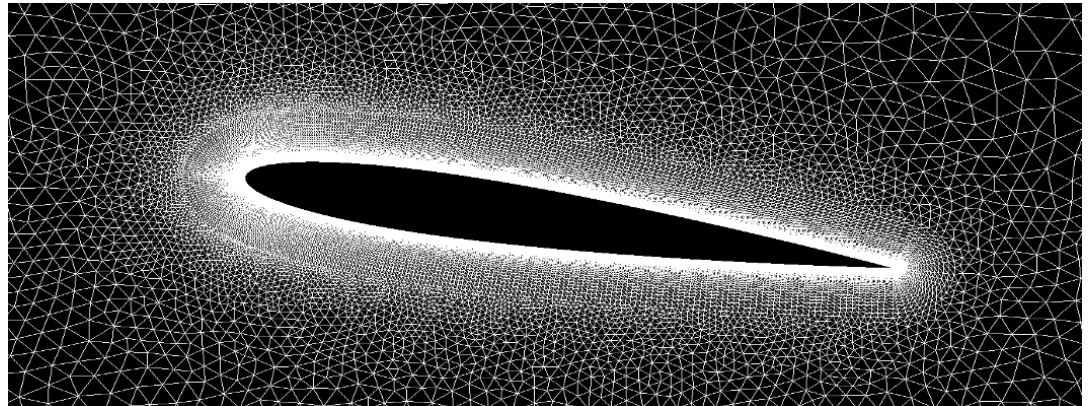
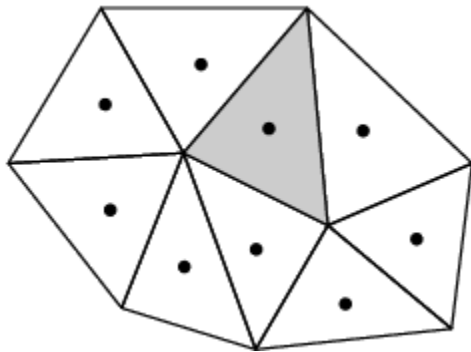


- When plotting we interpolate between the cells



This readily extends to 2 and more dimensions.

- In 2 or 3 dimensions the governing equation becomes:  $\frac{\partial A}{\partial t} + \nabla \cdot (A\mathbf{u}) = S$
- And the flux balance becomes  $\frac{\partial \bar{A}}{\partial t} = \frac{1}{\text{vol}(\text{cell})} \int_S A\mathbf{u} \cdot \mathbf{n} dS + \bar{S}$

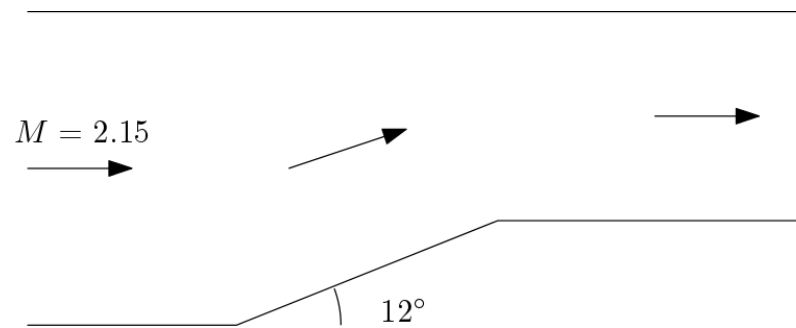




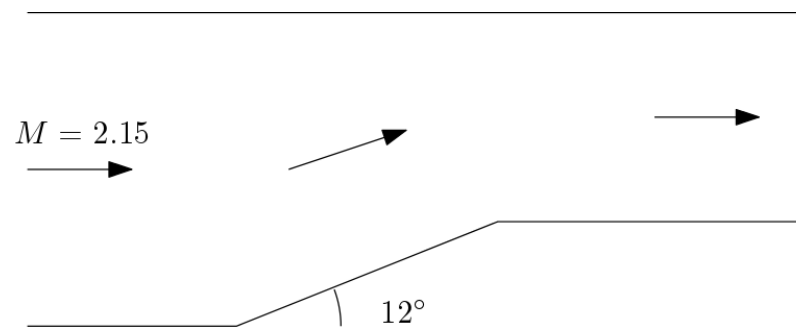
# What is OpenFoam?

- OpenFoam is a series of tools and Finite Volume solvers:
- Meshing tools:
  - `blockMesh`
  - `snappyHexMesh`
- Solvers:
  - `rhoCentralFoam`
  - `sonicFoam`
  - `icoFoam`

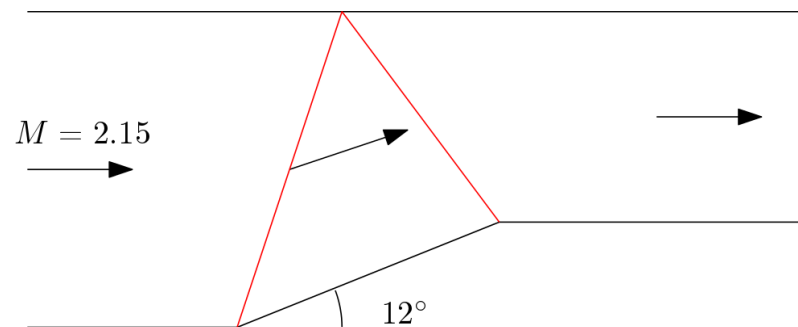
- Going to look at inviscid supersonic flow



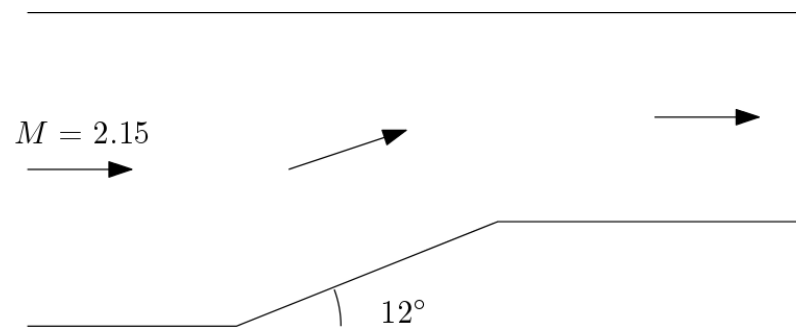
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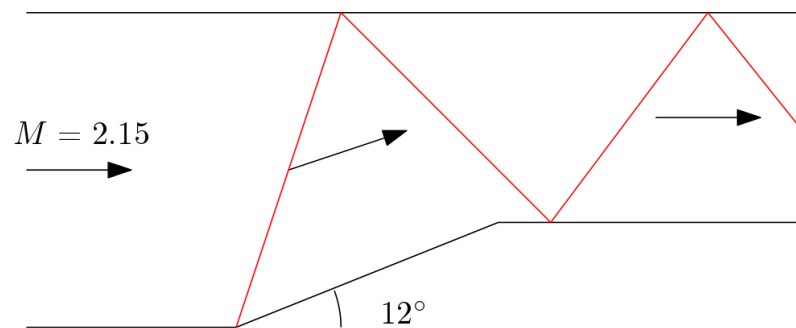
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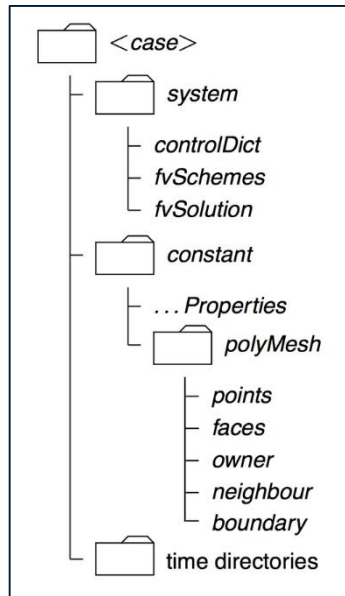


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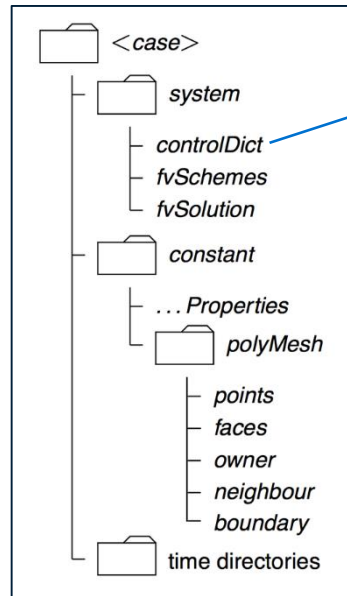
# Implementing the wedge.

- `git clone https://github.com/jb803/workshop.git`
- Go into `Reflection/incomplete`
- The OpenFoam case structure:



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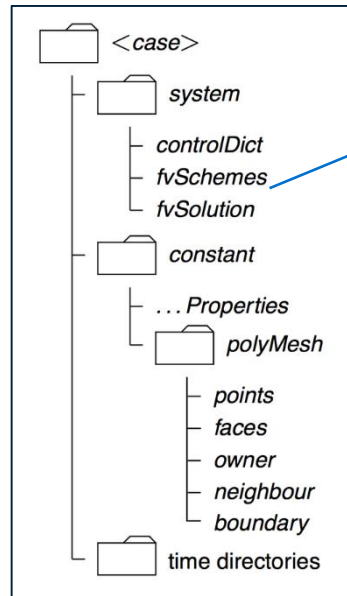
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Controls size of timesteps.  
How often to write output etc.

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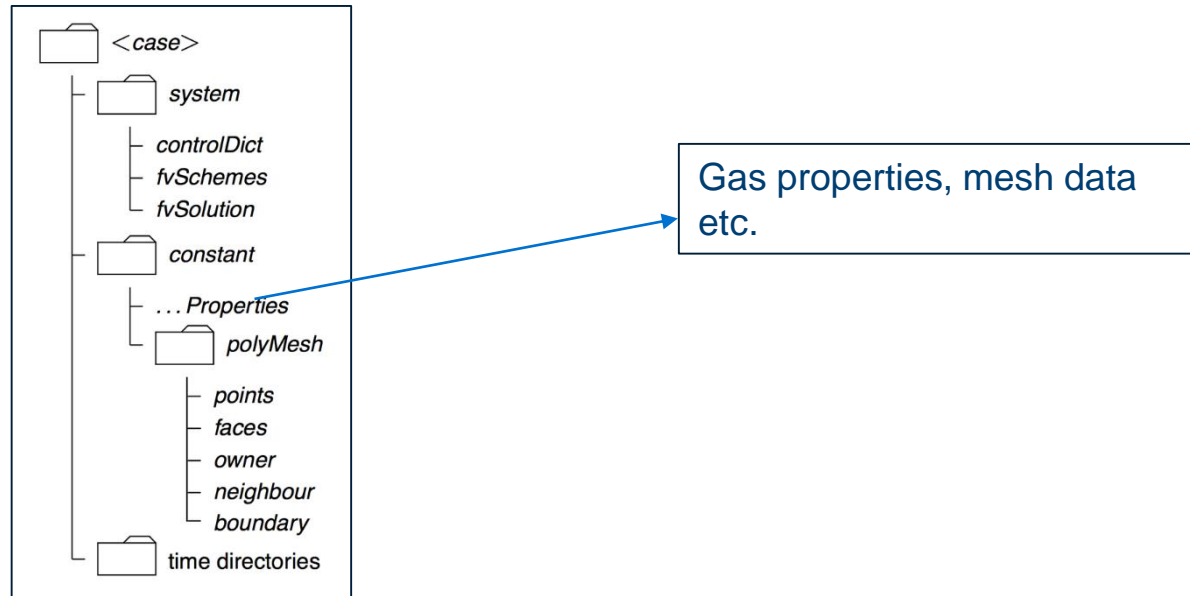
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How to calculate fluxes.  
**Very** solver specific. Copy  
from the examples directory.

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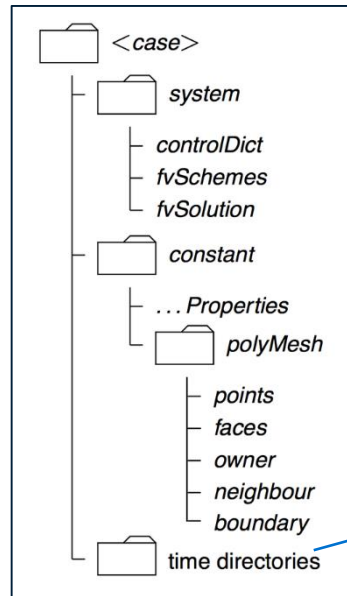
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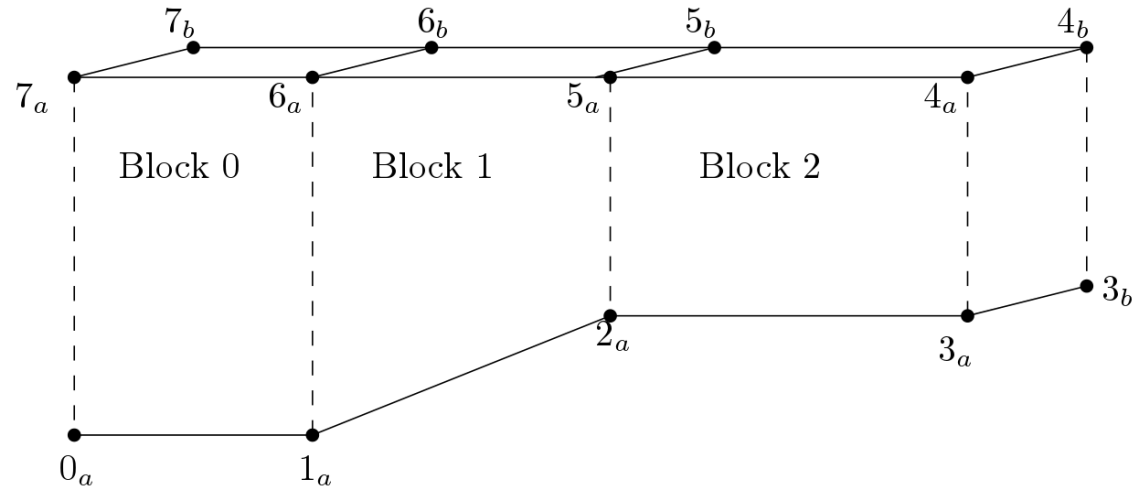
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Values of the velocity,  
pressure and temperature  
fields at each timestep.

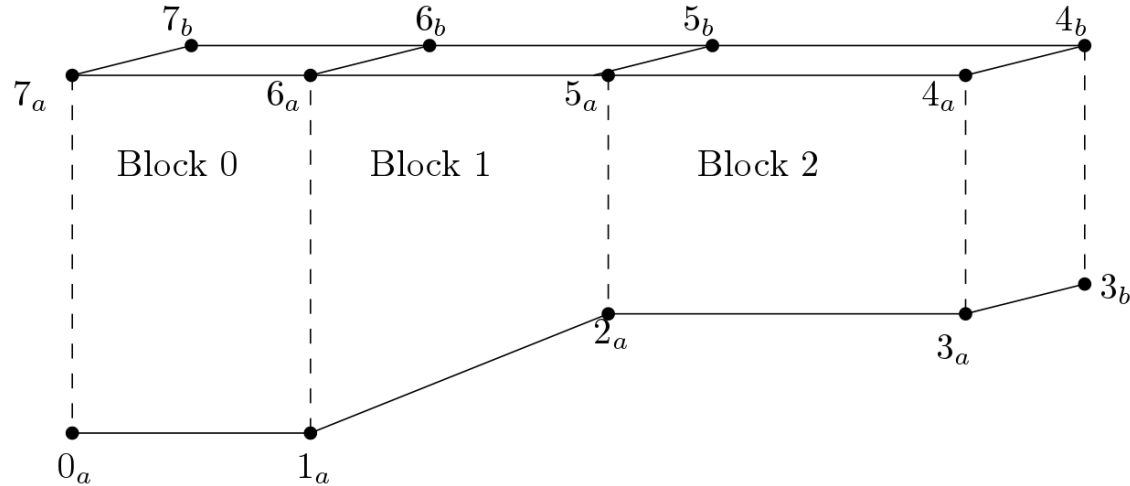
## Creating the mesh.

- The mesh is made from a series of 'blocks'



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- To create this mesh we will use the `blockMesh` tool.



## Creating the mesh.

- We generate the mesh with: `blockMesh`
- We check the mesh with: `checkMesh`
- We visualise with: `paraFoam`

- $a = \sqrt{\gamma RT}$

## Interactive: Running rhoCentralFoam

- Edit `controlDict`
- Run `rhoCentralFoam`

# Interactive: Visualisation with paraFoam

- Run `paraFoam`

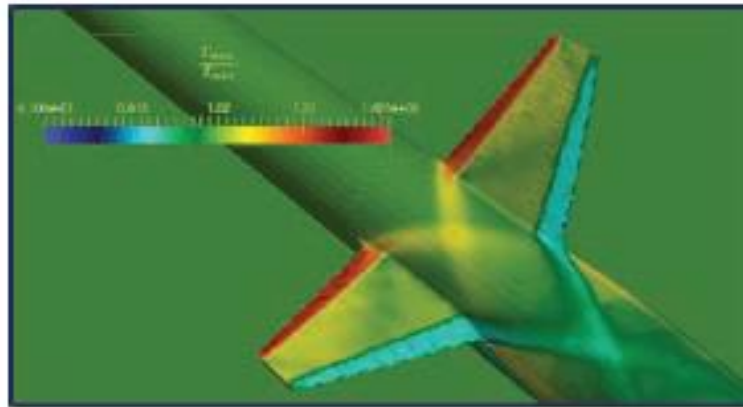


# Interactive: Bonus questions

1. What happens when you increase the mesh resolution?
2. What happens when you decrease the mesh resolution?
3. What is the largest Courant number you can achieve?
4. What happens if you adjust the slope of the wedge?
5. How could we improve the mesh?
6. What is the exit Mach number?

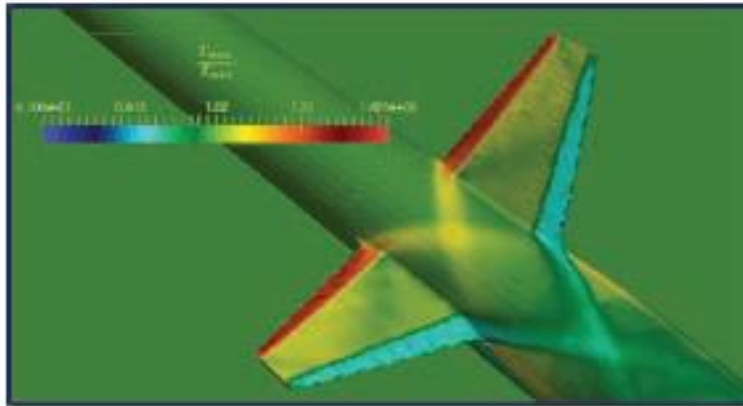
- Historically, CUSF has been more interested in external flows

e.g



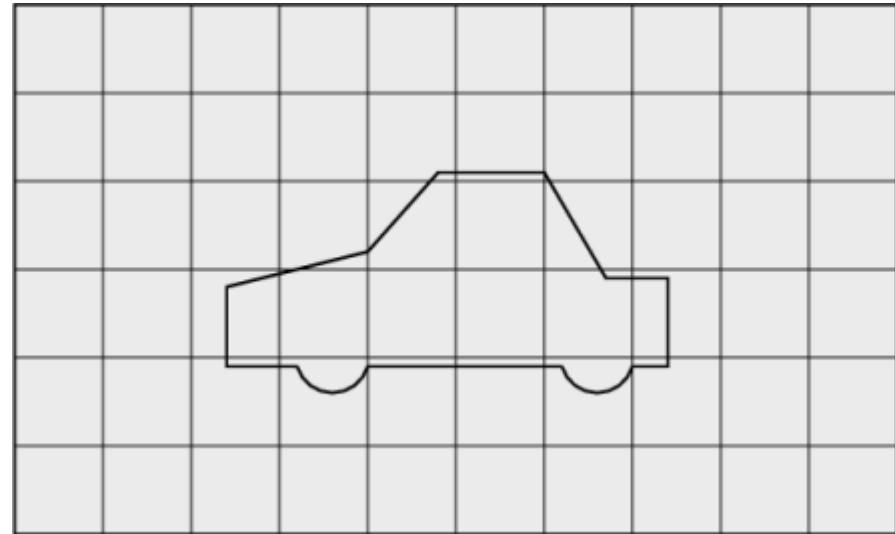
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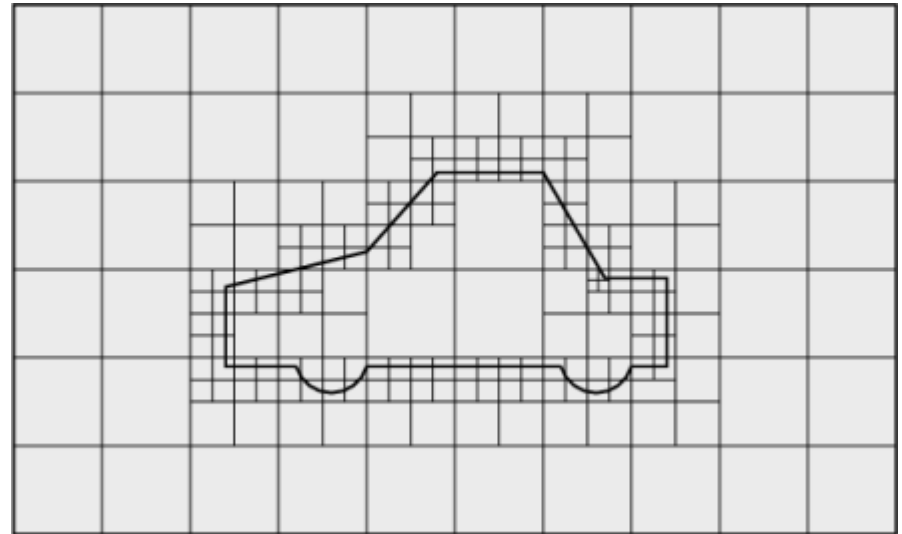


- This requires a more elaborate meshing process: `snappyHexMesh`

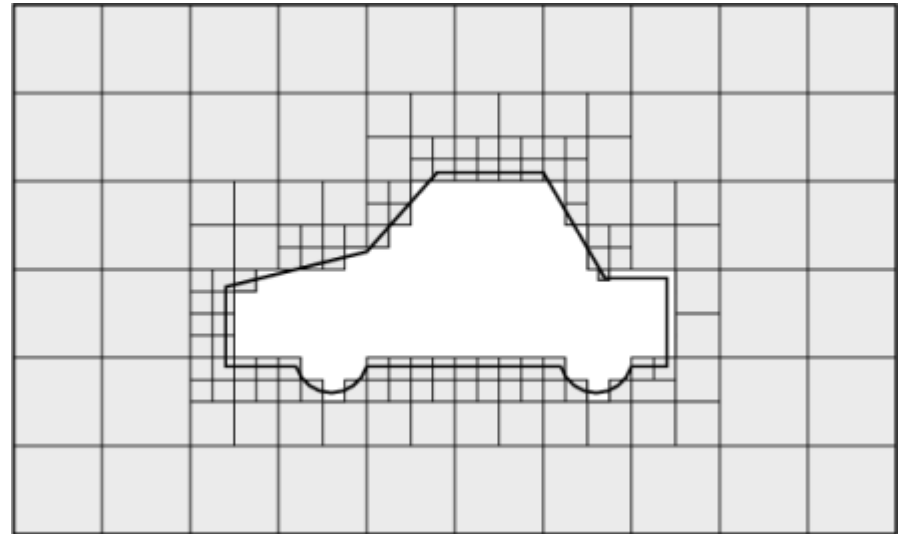
- Take a block mesh and an STL file



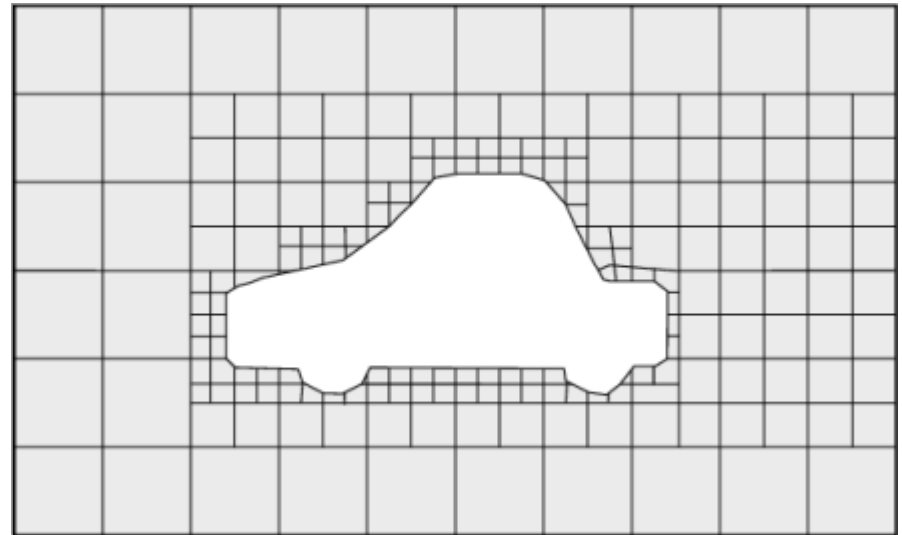
- Take a block mesh and an STL file
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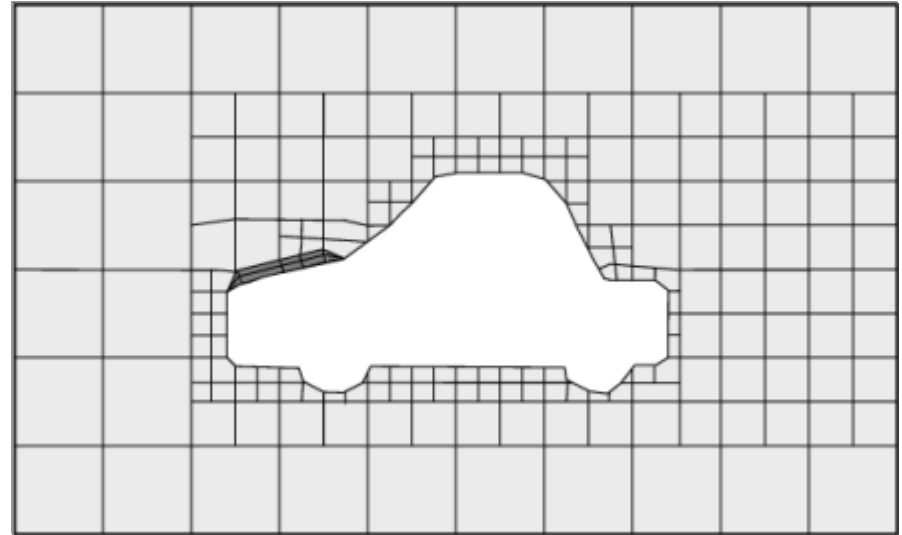
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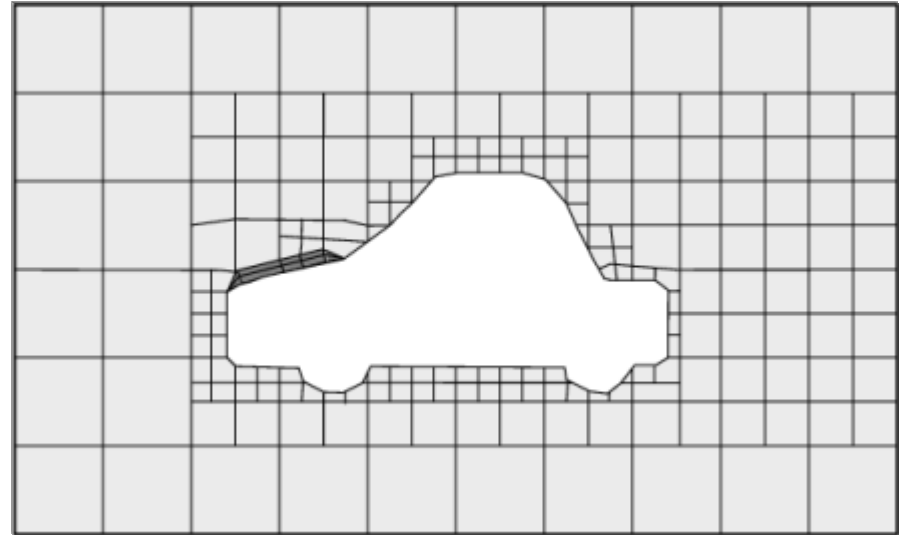


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- Controlled by `snappyHexMeshDict`
- Before running we must:
  - `blockMesh`
  - Prepare the STL: `extractSurfaceFeatures`
  - `snappyHexMesh`
- To look at the mesh: `paraFoam`
- When happy with the mesh: `snappyHexMesh -overwrite`

- `sonicFoam` is a bit more robust for this problem.
- The `fvScheme` and `fvSolution` files are different to those of `rhoCentralFoam`
- Run with `sonicFoam`
- Visualise with `paraFoam`

## Interactive: Bonus questions

- What do you notice about how long it takes to get a solution?
- What's happening in the wake of the cylinder?
- If you use rhoCentralFoam (copy fvScheme and fvSolution from the reflection case) what happens?
- What's the largest timestep you can do with sonicFoam?
- Let sonicFoam run for a long time: do you notice anything about the time per iteration?

# The future of CFD will be with Finite Element

- Finite element naturally handles higher order approximations within cells e.g. quadratic, cubic
- Finite elements are well suited for finding **adjoints** which is becoming an import design tool.

## How does it work?

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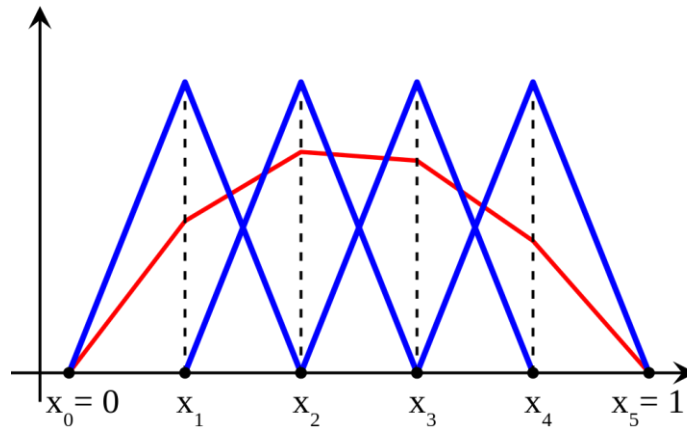
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- We realise:  $\frac{d^2 f}{dx^2} v = \frac{d}{dx} \left( \frac{df}{dx} v \right) - \frac{df}{dx} \frac{dv}{dx}$
- The integral becomes:  $\int -\frac{df}{dx} \frac{dv}{dx} - v g(x) dx = 0 + b.terms$

## How does it work?

- The boundary terms need to be dealt with cleverly but we will ignore them here.

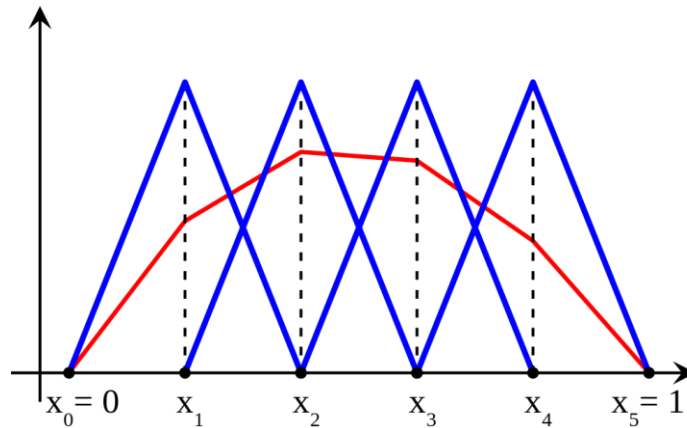
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- $\rightarrow f = \sum F_i \phi_i$  and so  $\sum \int -F_i \frac{d\phi_i}{dx} \frac{dv}{dx} - v g(x) dx = 0$

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- This gives:  $\sum_{i,j} \int -F_i \frac{d\phi_i}{dx} \frac{d\phi_j}{dx} - \phi_j g(x) dx = 0$
- This is a matrix equation for the vector containing all the  $F_i$

## Why is this useful?

- For certain conditions, the FE solution is **proven** to be the best solution for a given mesh and set of basis functions.
- We can choose very high order basis functions e.g. cubic (spectral element)
- We've relaxed the smoothness requirements on the solution

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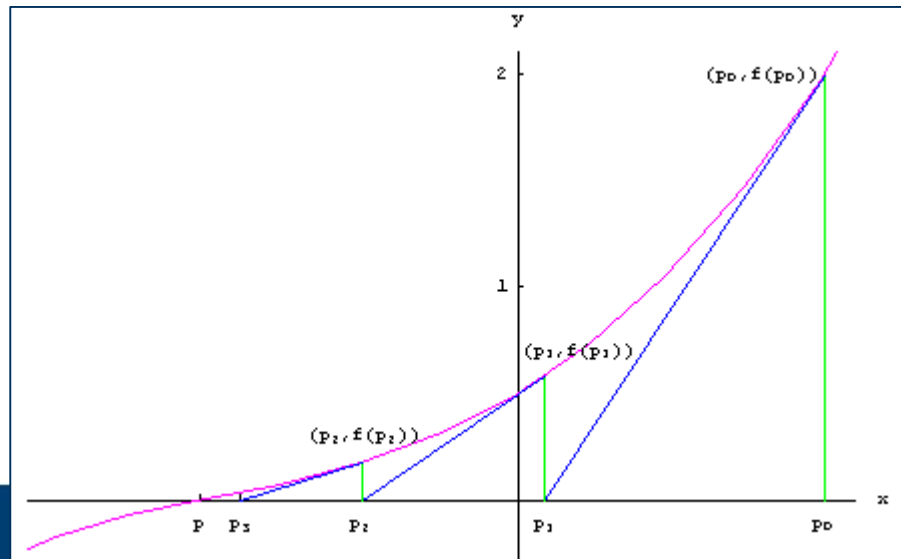
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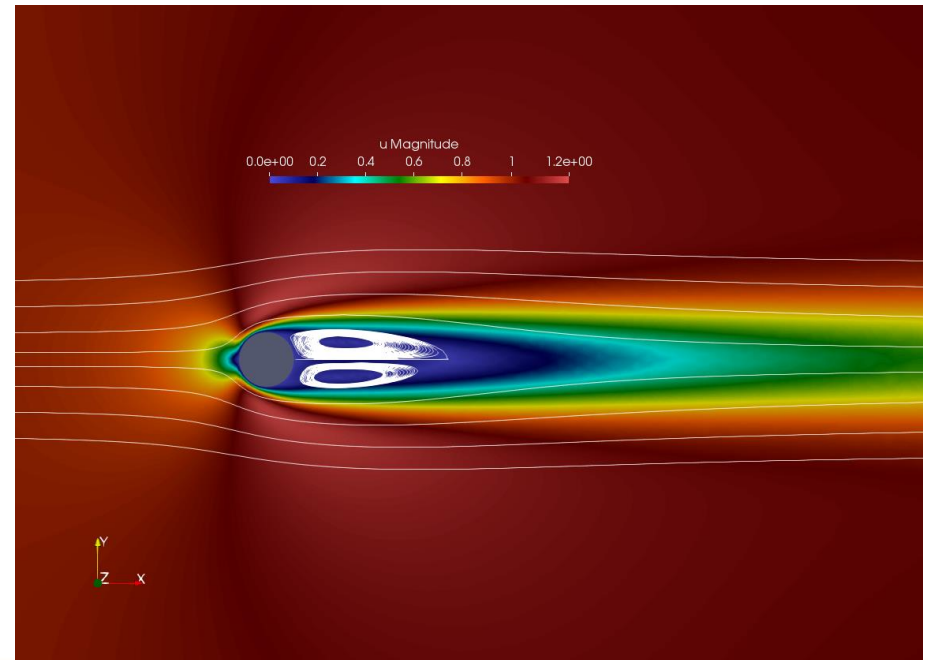


- We're going to solve the full Navier-Stokes at low Reynolds number with a Newton-Method



- Run `python FEDemo.py`
- Visualise the flow with `paraview`

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- Visualise the flow with `paraview`
- If we could inject momentum anywhere – where should we do it? How would you find out?

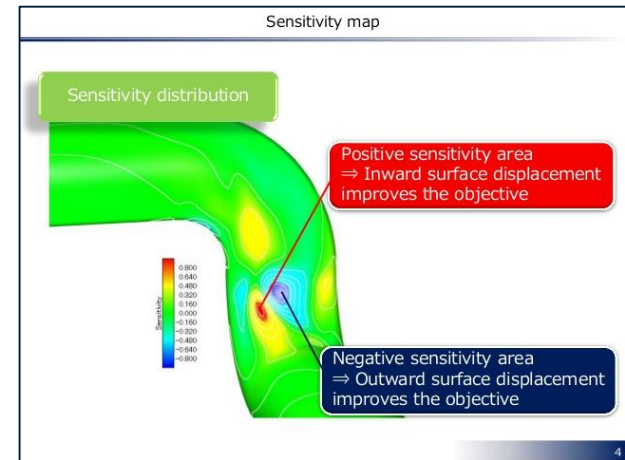






- $J = -\nabla \mathbf{u} \cdot \nabla \mathbf{u}$       therefore  $\delta J = -2\nabla \mathbf{u} \cdot \nabla \delta \mathbf{u}$
- The perturbation to the flow satisfies:  $\mathbf{u} \cdot \nabla \delta \mathbf{u} + \delta \mathbf{u} \cdot \nabla \mathbf{u} + \nabla \delta p - \nu \nabla^2 \delta \mathbf{u} = \delta f$
- We multiply by an adjoint state,  $\mathbf{u}^+$ , and apply divergence theorem (integrate by parts)
- Gives  $\delta J = \delta f \cdot \mathbf{u}^+$  provided  $\mathbf{u}^+$  is divergence free and satisfies:
$$-\mathbf{u} \cdot \nabla \mathbf{u}^+ + \mathbf{u}^+ \cdot \nabla^T \mathbf{u} - \nabla p^+ - \nu \nabla^2 \mathbf{u}^+ = +2\nu \nabla^2 \mathbf{u}$$
- In finite elements the discrete representation of this is found by transposing the Jacobian

- OpenFoam and Ansys are implementing adjoint solvers at the moment.
- Adjoint solvers are the current big thing in CFD.
- Finite element methods and their close cousin spectral elements are set to be the future of CFD. Higher order polynomials can do a lot more with a smaller number of DOFs



[https://www.youtube.com/watch?v=GLe3j0l11\\_k](https://www.youtube.com/watch?v=GLe3j0l11_k)