

Modeling of Risley prisms devices for exact scan patterns

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ABSTRACT

We investigate the scan patterns produced using different pairs of Risley prisms. Combinations of optical wedges with different prism angles (corresponding to different deviations angles of the prisms) are considered to complete the exact modeling of the scanning process using specialized mechanical design programs. While this procedure is somehow elaborate with regard to approximate methods, it has the advantage of providing the exact movement laws of the laser spot on various types of surfaces scanned with this type of refractive device. The study is made with regard to the characteristic parameters of the device, such as θ_1 and θ_2 - the prism angles of the two wedges, ω_1 and ω_2 - the rotating speeds of the two wedges, and the geometry of the scanner (which includes the distance between the two prisms, their orientation, and the distance to the scanned plane). The scanner is approached for a row of values of the characteristic parameters $k=\theta_2/\theta_1$ and $M=\omega_2/\omega_1$ introduced in Marshall's classical work. The results allow for choosing the most appropriate patterns for specific scanning applications.

Keywords: optomechanics, optical devices, scanners, Risley prisms, wedges, modeling, scan patterns.

1. INTRODUCTION

Optical and laser scanners [1] have been developed over time in approximately forty different designs [2], uni- (1-D), bi- (2-D), and tri-dimensional (3-D). Out of these numerous designs, the most important ones are [3]: *polygonal* (prismatic and pyramidal) [4, 5], *oscillatory* (galvanometric [6] and resonant - the latter with fixed frequencies, developed especially as MEMS (Micro-Electrical-Mechanical Systems) [7]), *refractive* (with prisms or lenses), *holographic*, as well as *electro-* and *acousto-optical*.

We have approached previously [8] rotating (monogon [9] or polygonal [10]), as well as galvanometer-based scanners (GSs) [11], both for industrial [9] and biomedical imaging applications, the latter with a focus on Optical Coherence Tomography (OCT) [12-14], for which we have demonstrated the optimal scanning regimes of a galvoscaner [15]. In the present study we are approaching the refractive scanner - with rotating Risley prisms / optical wedges.

The applications of this type of scanners range from micro-devices, by example for endoscope probes [16] - with micro-prisms - to devices for satellite positioning - with large prisms for which optomechanical issues become essential [17]. Their domains of application include: Confocal Microscopy (CM) [18], holography [19], interferometry [20, 21], polarimetry [22], beam shaping [23], spectroscopy [24], and optical attenuators. We have developed for the latter a device with translational prisms [25] as an alternative to optical attenuators using optical choppers [26-28]. Combinations of GSs and Risley prisms were also developed for 3-D scanning.

Scanners with Risley prisms have been approached in early works [31], rigorous analytical analysis were developed [32, 33], and the inverse problem - of determining the positions of the prisms that produce a certain position of the laser spot was approached as well [34]. Constructive solutions were developed for rotational prisms [35], while other devices, by example with titling [36] or with combinations of tilting and rotational wedges were also tested [37].

The scope of our present study is to determine and to analyse the exact scan patterns produced by the classical two Risley prism device. Approximate scan patterns have been determined by Marshall in [38] as Lissajoux figures - using the deviation $D_i=(n-1)\theta_i$, $i=1,2$ of an optical wedge (where θ_1 , θ_2 are the prism angle - Fig. 1). In order to obtain exact scan patterns in our approach we shall utilize a mechanical design program, CATIA V5R20, while we shall maintain

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throughout the study the parameters of the device as they have been defined by Marshall [38]: $k=\theta_2/\theta_1$ and $M=\omega_2/\omega_1$, where ω_1 and ω_2 are the rotating speed of each prism.

This ascertainment of exact scan patterns of Risley prisms scanners, especially using mechanical design programs has not been done yet – to the best of our knowledge. We have completed both the simulations and the experimental validations of these results. Because of space limitations, in this first presentation of our work, a selection of representative modeling and experimental results will be made.

2. SCANNER WITH RISLEY PRISMS

Fig. 1a, b shows one of the configurations of Risley prisms scanners investigated – with the prisms with the vertical facets (perpendicular to the optical axis O.A.) on the exterior of the device. The constructive parameters e – the distance between these facets of the prisms, and L – the distance from the last facet to the screen where the scan patterns will be determined – are pointed out.

Fig. 1c shows the two prisms modeled in CATIA V5R20, as well as the central laser ray that is refracted through the prisms. The refraction angles are marked in Fig. 1a, b, where we also noted the total angular deviation D and the linear deviation Δ – for the emergent ray parallel to the incident one and to the O.A. (for the two identical prisms ($\theta_1=\theta_2$) positioned with all the facets parallel). The prisms can be rotated independently with a certain angular increment, and the coordinates of the spot produced by the central ray of the laser beam on the screen are obtained. From these coordinates, the scan patterns can be determined, as it will be presented in the following.

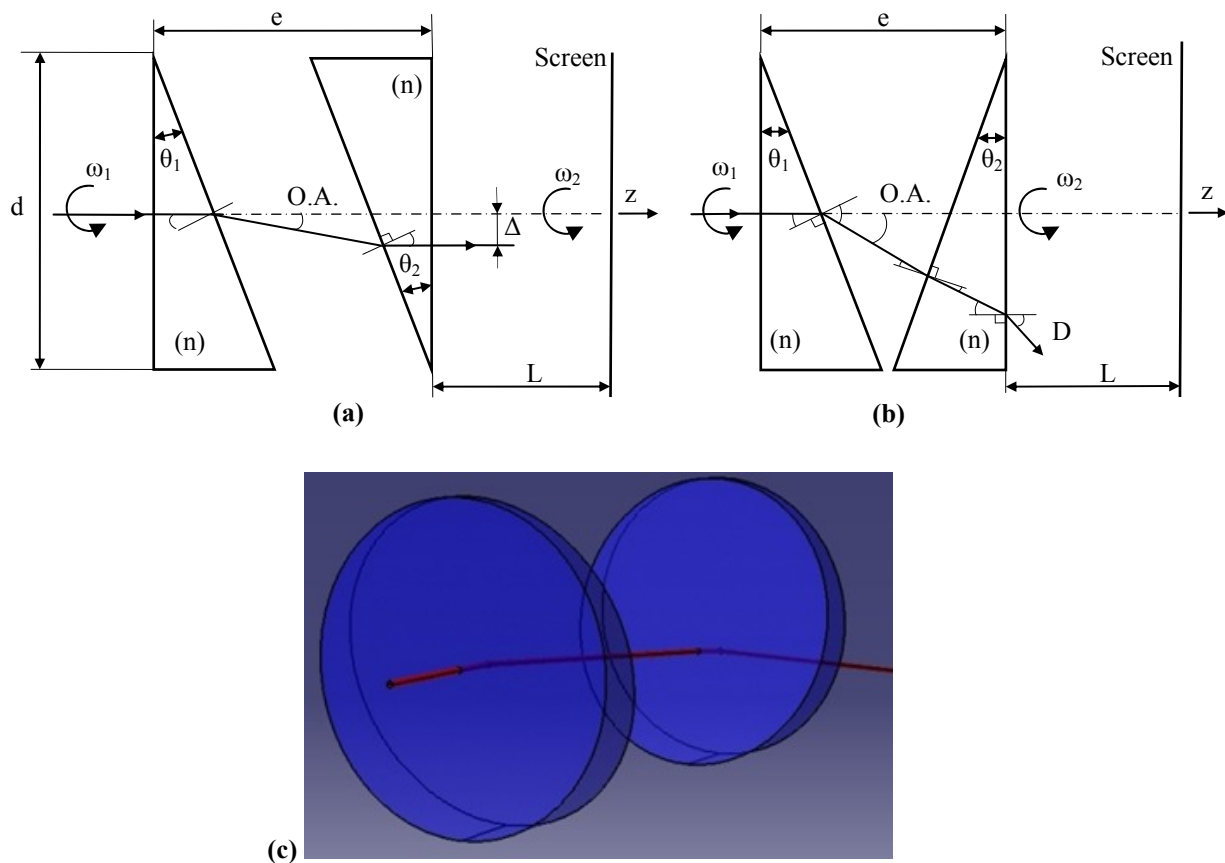


Figure 1. Optical scanner with Risley prisms – configuration with the plane facets on the exterior: (a), (b) central ray for two positions rotated by 180 degrees of the prisms; (c) modeling of the beam propagation using 3D CATIA.

3. METHOD OF TRACING THE SCAN PATTERNS

Fig. 2 shows a first simulation where one of the prisms is maintained fixed – but in different positions (at 0; 90; 180; 270 degrees) – and the other one is situated completely. The mobile prism will thus produce a circle (in each of the positions of the fixed prism). These circles have equal radiuses and their centers are placed on a circle determined by the incremental movement of the fixed prisms. The differences of the radiuses of the circles of centers and of the radiuses of the circles produced can be noticed – between the two cases.

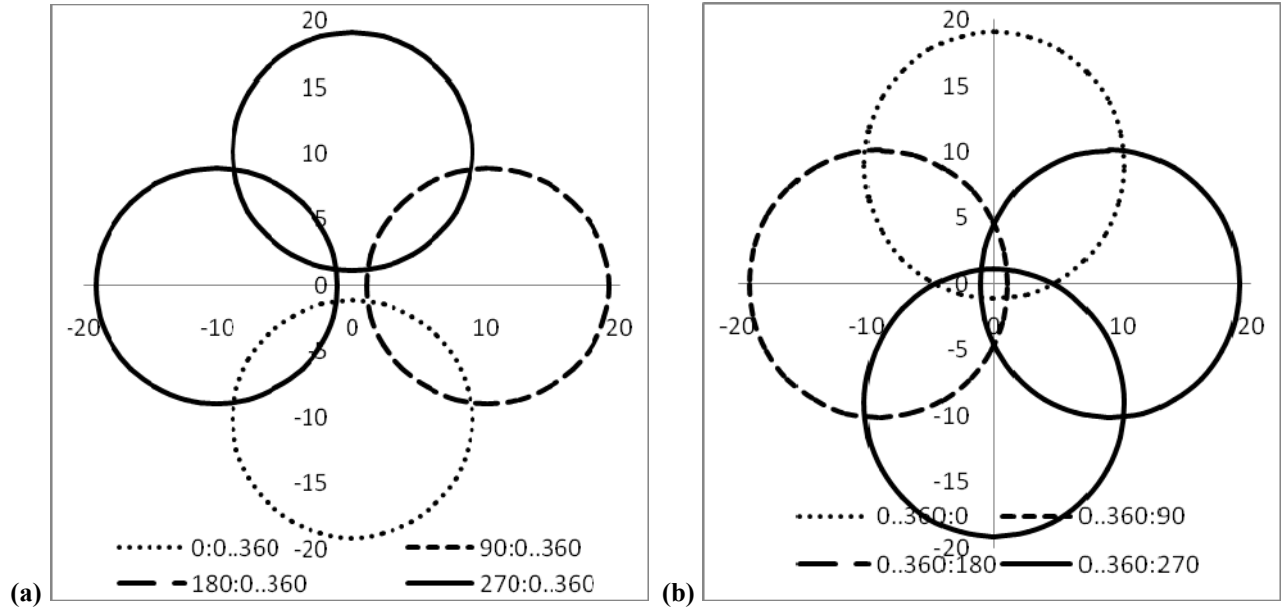


Figure 2. Scan paths produced with two Risley prisms for (a) the first prism fixed at 0; 90; 180; 270 degrees, and the second prism rotational; (b) the first prism rotational, and the second prism fixed at 0; 90; 180; 270 degrees.

Fig. 3 shows the scan patterns produced for a device with identical prisms ($k=1$), but with different angles $\theta_1:\theta_2$ (2:2, 4:4, 6:6, 10:10). Two different situations were considered in Fig. 3a and b: for positive and for negative values of M (equal in module), therefore with the prism rotating in the same sense (a) – with $M=4 \Rightarrow \omega_2=-4\omega_1$.

One may notice the differences in shapes between (a) and (b), as the higher relative speed in (b) produces more loops for the pattern. In the same figure (for the same M), the larger scan pattern produced when increasing θ may be remarked – as roughly the maximum deviation angles are approximately proportional to the angles θ of the prisms.

In the following the patterns will be modeled and analyzed, because of space limitations, for one of these two cases, i.e. for $M>0$. The second case (for $M<0$) is solved similarly. In Section 5 experimental results will be presented – as examples – for both cases.

4. SCAN PATTERNS FOR $M>0$

4.1. For $k=1$ ($\theta_1=\theta_2=2$ degrees), the number of loops increases with M (Fig. 4), while for $M=1$ ($\omega_1=\omega_2$), the two prisms rotate together and thus they generate a circle on the screen. The scanning process was simulated by varying the angular speed ω_2 (of Prism 2), and thus obtaining the variation of the trajectory for $M=1$ to 6.

4.2. By contrast, in the following, in Fig. 5, M was kept constant ($M=4$) and different pairs of prisms were considered, with the pairs of angles: 2:2, 2:4, 2:6, 2:10, 4:2, 4:4, 4:6, 4:10, 6:2, 6:4, 6:6, 6:10, 10:2, 10:4, 10:6, and 10:10 – therefore with k varying accordingly, from 0.2 to 5.

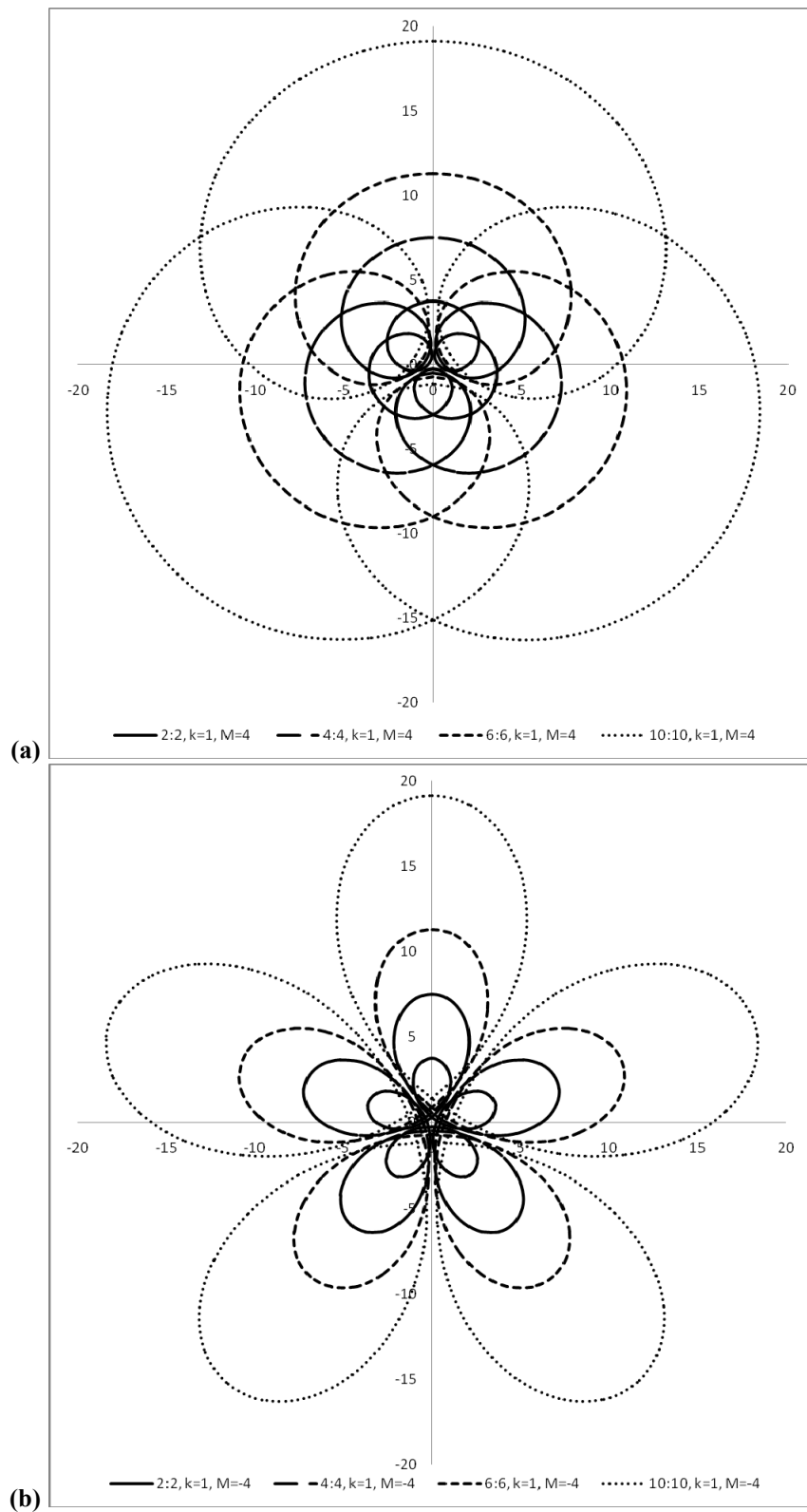


Figure 3. Scan patterns produced with two rotating Risley prisms for different pairs of identical prisms, with increasing angles (the notation $\theta_1: \theta_2$ is used for the angles of a pair of prism that is utilized): (a) $M > 0$ (in particular $M=4$); (b) $M < 0$ ($M=-4$).

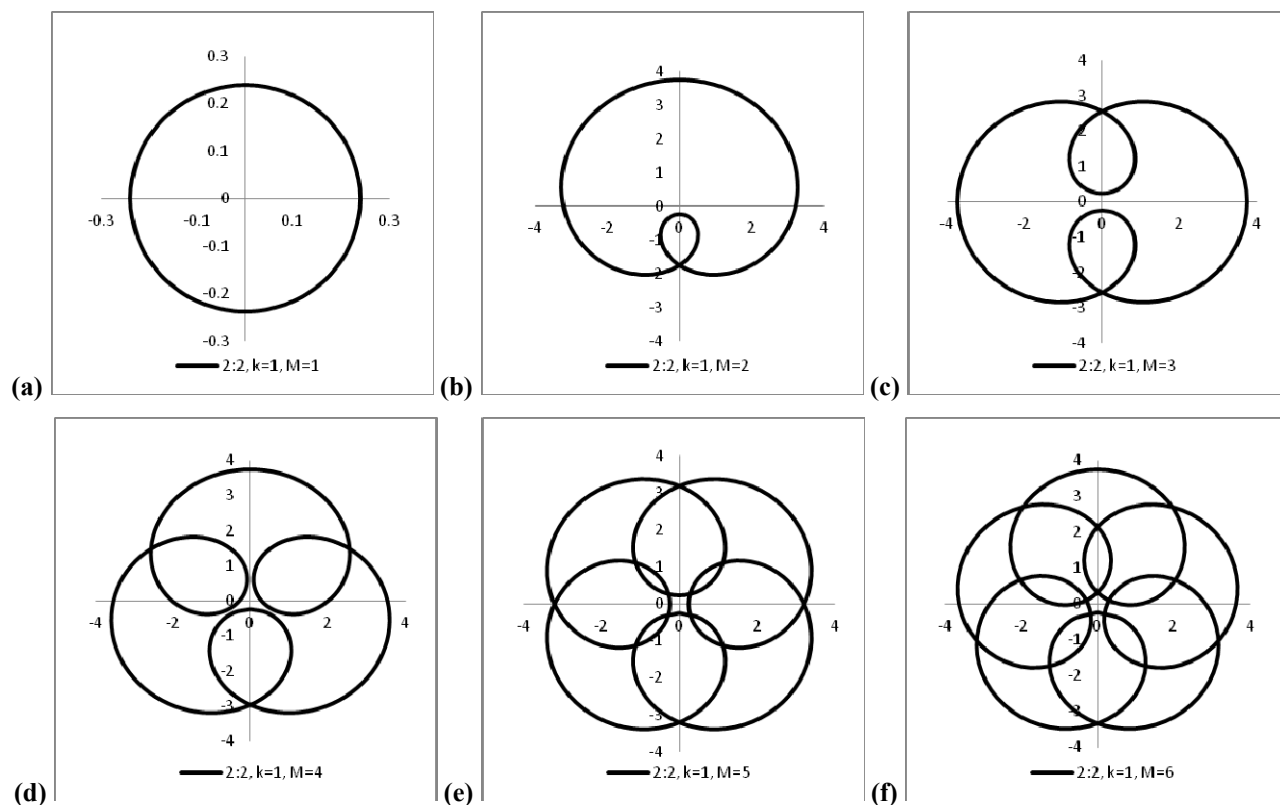
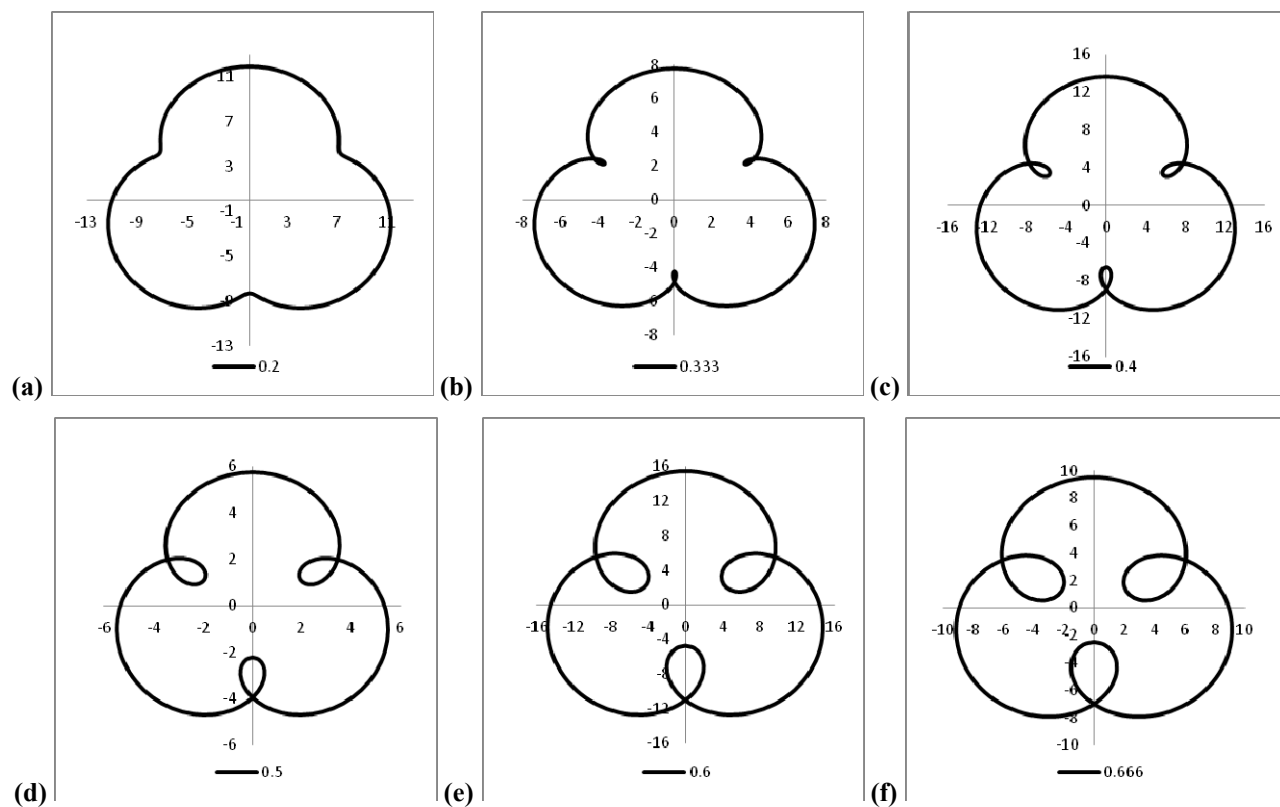


Figure 4. Variation of the scan patterns for the same pair of identical prisms (with the apex of 2 degrees), thus $k=1$, and for increasing values of the relative rotational speeds of the prisms (therefore of M).



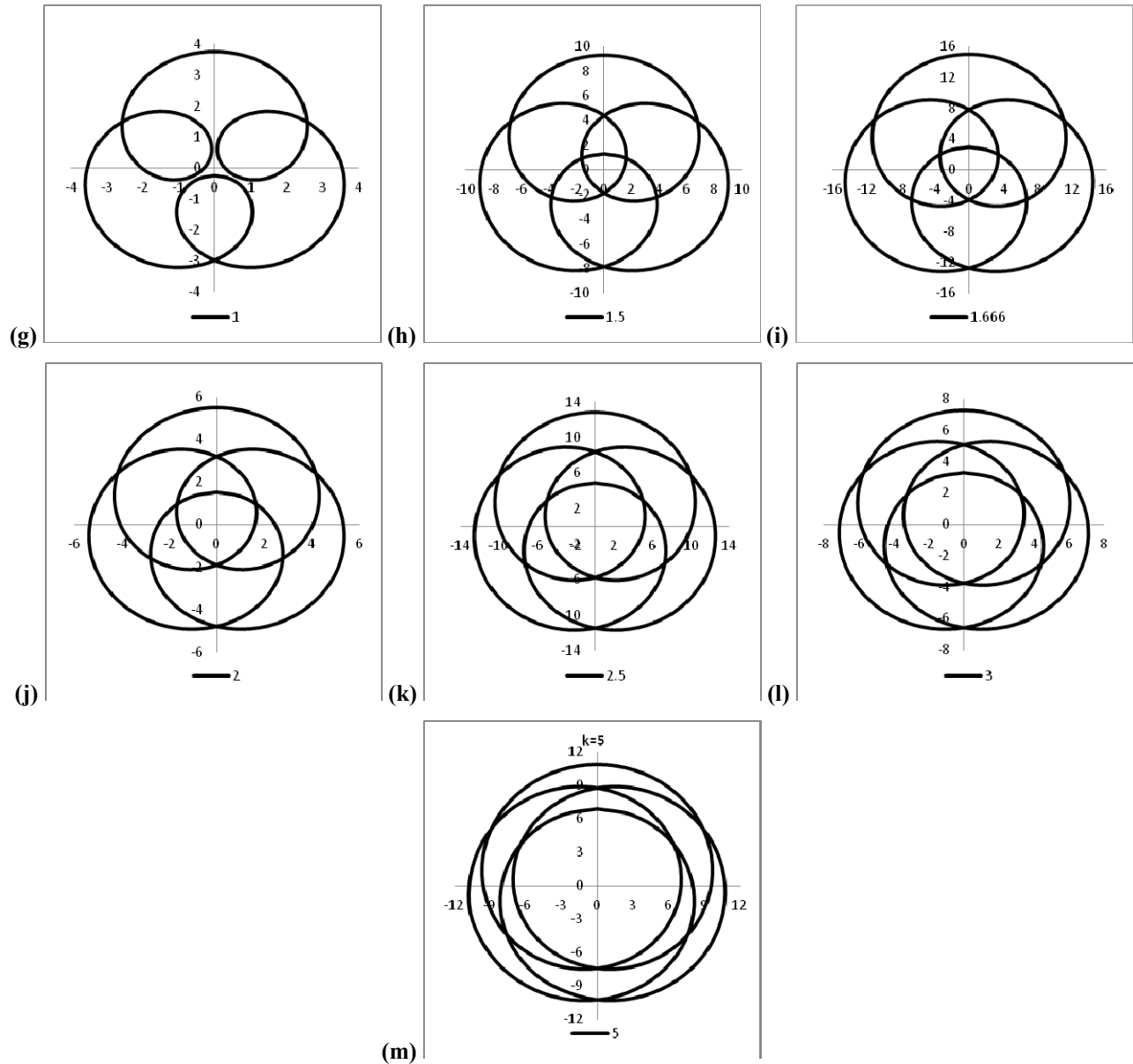


Figure 5. Scan patterns for the same value of M and for an increasing row of values of k .

Several aspects can be concluded: (i) the number of loops increases with k ; (ii) the relative dimensions of the loops (with regard to the total dimension of the scanned space) increases; (iii) this dimension of the scanned space is obviously different – it increases with the sum of the angles of the two prisms, $\theta_1 + \theta_2$.

4.3. To better compare and conclude on the changes in shape of the scan patterns with the two parameters, k and M , in Fig. 6 a parallel is made between the patterns produced for $k=1, 2, 3$ and 5 (the pairs of prisms considered are 2:2, 2:4, 2:6, and 2:10) – and at each k , for two values, of $M=4$ and $M=6$ of the speed ratio.

One may notice at each M the increase in the outer and inner circle of the scan space – respectively the increase in the radiuses of the circle that inscribed and of the circle that is inscribed in the scan pattern. For the same k , the density of the lines increases with M .

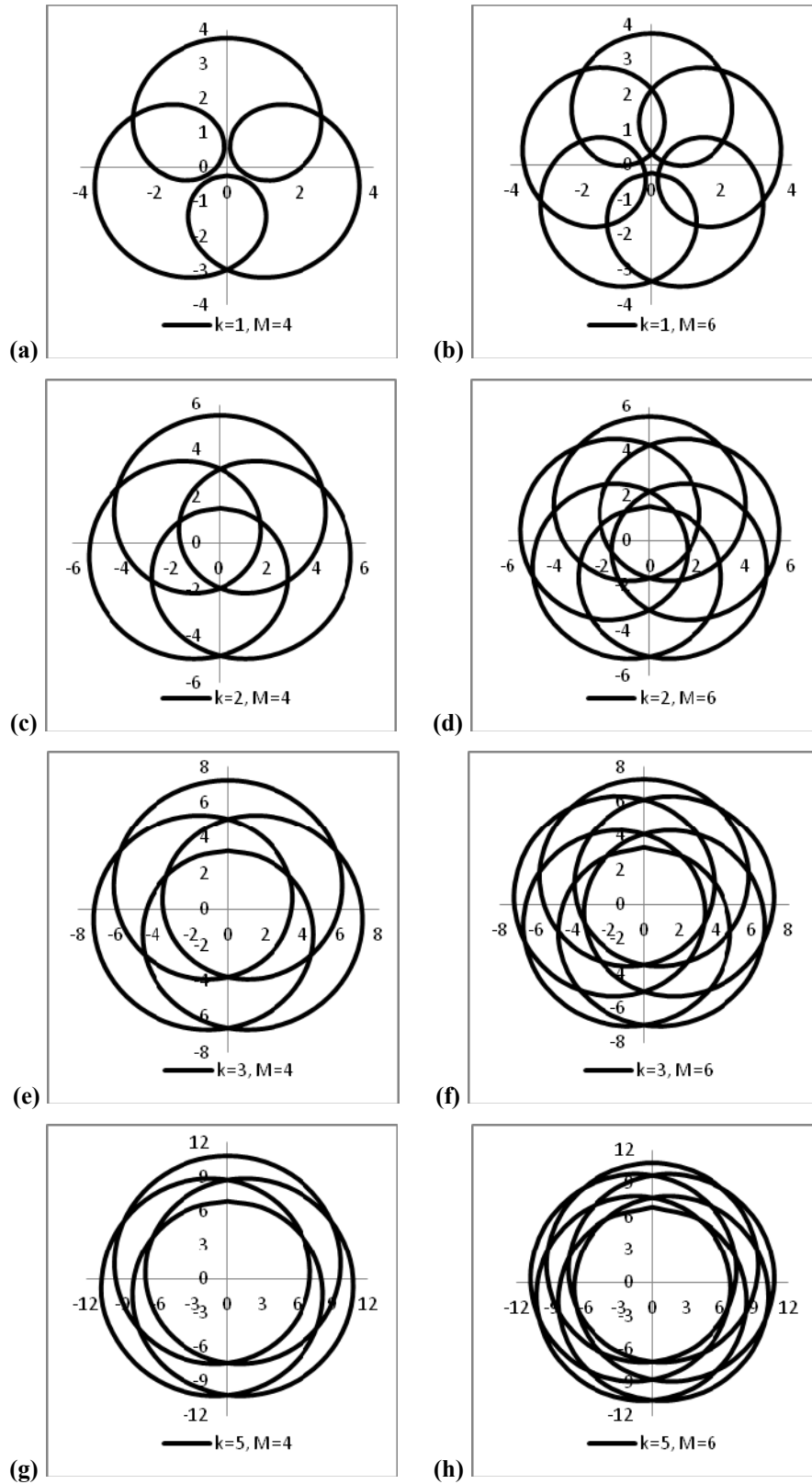


Figure 6. Comparison of the scan patterns produced for increasing k - and for the same k , between two values of M .

4.4. The variation of a scan pattern (obtained for $k=1$ and for $M=6$) is presented in Fig. 7 with regard to the distance L to the screen (double in (b) with regard to (a)) and with regard to the distance e between the prisms – Fig. 1a, b (e is double in (c) with regard to (a)). One may notice that with L the scanned space (the radius of the circle that inscribed it) doubles, while the inner “free” space (not scanned) is increased as well.

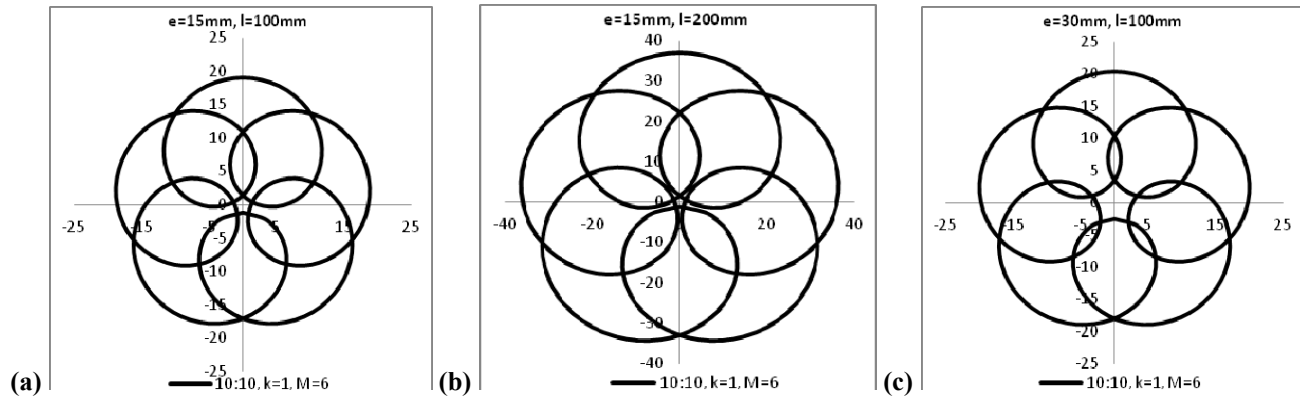


Figure 7. Comparison of the scan patterns produced for the same k and M , but for different values of e and L .

4.5. Combinations between e and L exist to obtain patterns that reach the center $(0, 0)$ of the scanned space, as presented – as an example – in Fig. 8. Actually we have determined that for any $k>1$ there is a distance L for which such a situation can be obtained. The higher is k , the smaller is this distance L – for which we reach the center $(0, 0)$ becomes – for the same distance e between the prisms (Fig. 1a, b). For $k<1$ the trajectory becomes divergent in the center of the pattern (as one may see in Fig. 6a-f), and such a situation – of a trajectory that passes through its center – cannot be reached anymore.

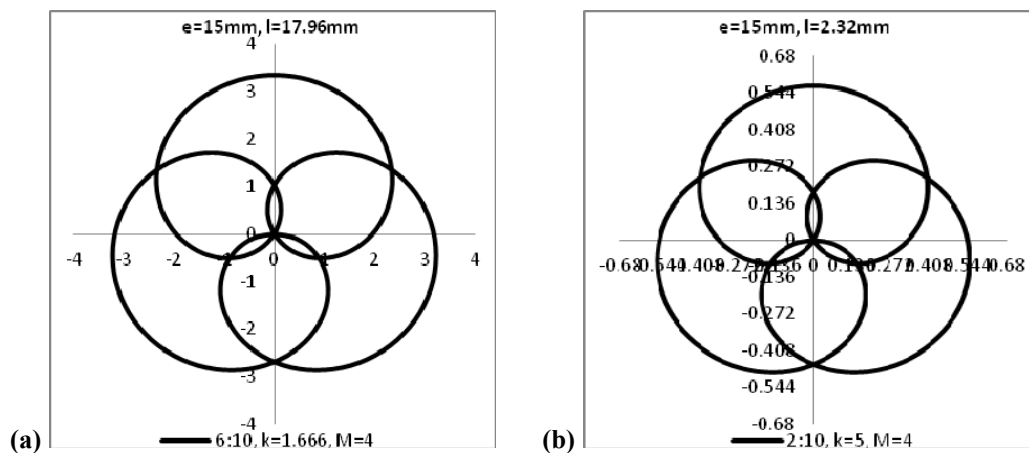


Figure 8. Scan patterns that include the center of the scanned space – for two values of k ($M=\text{cst.}$).

5. SCAN PATTERNS DETERMINED EXPERIMENTALLY

A few examples of patterns determined experimentally with pairs of Risley prisms (ThorlabsTM [38]) for the same k and for the same absolute values of M (but with different signs) are presented in Fig. 9. The experimental results confirm those of the modeling process.

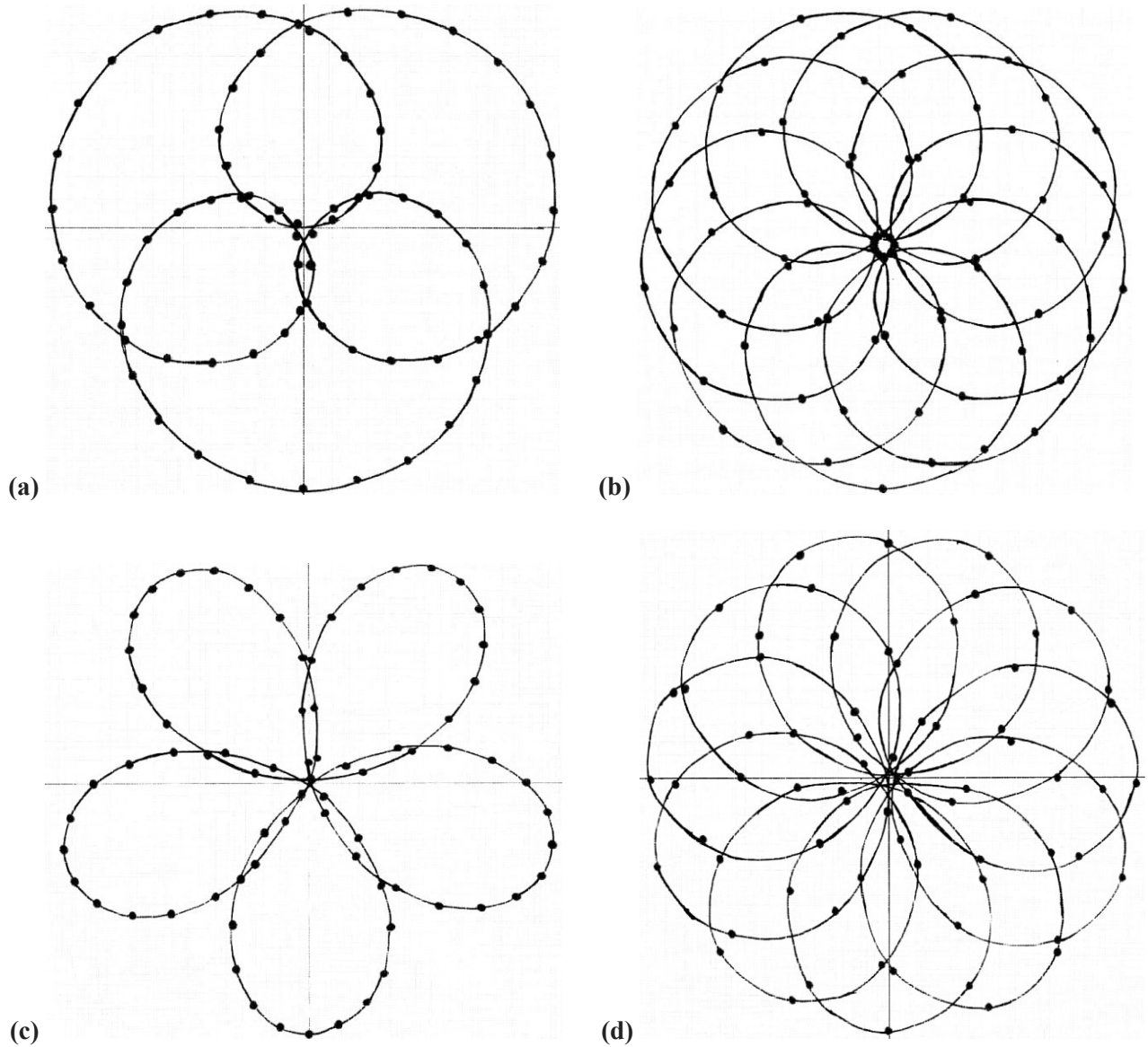


Figure 9. Experimental scan patterns obtained for (a, b) $M>0$: (a) $k=1$, $M=4$; (b) $k=1$, $M=10$, and for (c, d) $M<0$: (a) $k=1$, $M=-4$; (b) $k=1$, $M=-10$.

6. CONCLUSIONS

We have presented some of our results regarding the exact modeling with a mechanical design program, CATIA V5R20, of the scan patterns produced by scanners with rotational Risley prisms. The parameters of the device, in the form they have been introduced by Marshall [38] were utilized: $k=\theta_2/\theta_1$ and $M=\omega_2/\omega_1$. An analysis using these parameters was done in this paper, with a focus on one of the functioning cases, $M>0$, while examples of scan patterns obtained for the other case, for $M<0$, were also presented. Examples of scan patterns obtained experimentally were also presented, as they confirm the results of the modeling process. While we intend to present the entire analysis performed in a future paper, our work will continue with quantifications of these results and with applications of the scanner with Risley prisms in various fields, especially in biomedical imaging, with a focus on OCT, as a possible alternative to generating scan patterns with dual axis galvanometer-based scanners [40].

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