

# CP1 for NPRE 501

Jin Whan Bae

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## 1 Problem Definition

Table 1 lists the constants used in the problem.

Parameter	Value	[Unit]
Diameter	6	[cm]
<b>Radius</b>	<b>3</b>	[cm]
Geometry	Sphere	
k	15	$[\frac{W}{mK}]$
Density	8000	$[\frac{kg}{m^3}]$
Specific Heat	500	$[\frac{J}{kgK}]$
$\alpha$	<b>3.75e-6</b>	$[\frac{m^2}{s}]$

Table 1: Problem Constants. Derived constants are in bold.

Differential Equation:

$$\frac{1}{\alpha} \cdot \frac{dT}{dt} = \frac{1}{r^2} \frac{d}{dr} r^2 \frac{dT}{dr}$$

Boundary Conditions:

$$T(0, t) = finite \quad OR \quad \frac{dT}{dr}(r = 0, t) = 0$$

$$\frac{dT}{dr}(r = R) = 0$$

Initial Condition:

$$T(r, 0) = \frac{T_0}{2} (1 - \cos(\frac{\pi \cdot r}{R}))$$

## 2 C. Numerical Solution

$$\frac{1}{\alpha} \cdot \frac{dT}{dt} = \frac{2}{r} \frac{dT}{dr} + \frac{d^2T}{dr^2}$$

Applying the finite difference method, central for r and explicit for t:

$$\frac{1}{\alpha} \cdot \frac{T_k^u - T_k^{u-1}}{\Delta t} = \frac{2}{r_k} \left( \frac{T_{k+1}^{u-1} - T_{k-1}^{u-1}}{2\Delta r} \right) + \frac{T_{k-1}^{u-1} - 2T_k^{u-1} + T_{k+1}^{u-1}}{\Delta r^2}$$

where u is the temporal step and k is the spacial step.

Solving for  $T_k^{u+1}$ :

$$T_k^{u+1} = T_k^u + \alpha \frac{\Delta t}{\Delta r \cdot r} (T_{k+1}^u + T_{k-1}^u) + \alpha * \frac{\Delta t}{(\Delta r)^2} (T_{k+1}^u - 2T_k^u + T_{k-1}^u)$$

Applying neuman boundary condition at r=0:

$$\frac{dT(0, t)}{dr} = 0$$

$$\frac{T_1^u - T_{-1}^u}{2\Delta r} = 0$$

$$T_1^u = T_{-1}^u$$

This gives:

$$T_0^{u+1} = T_0^u + \alpha * \frac{\Delta t}{(\Delta r)^2} (2T_1^u - 2T_0^u)$$

Applying neuman boundary condition at r=R (k=K at r=R):

$$-k \frac{dT(R, t)}{dr} = 0$$

$$\frac{T_{K+1}^u - T_{K-1}^u}{2\Delta r} = 0$$

$$T_{K+1}^u = T_{K-1}^u$$

This gives:

$$T_K^{u+1} = T_K^u + \alpha * \frac{\Delta t}{(\Delta r)^2} (2T_{K-1}^u - 2T_K^u)$$

## 3 Appendix A

### 3.1 a. Final Temperature Distribution in the Sphere

The final temperature distribution will be a cosine curve with the highest point at  $r = 0$ , gradually going down to the minimum value at  $r = R$ .

## 4 Appendix B

### 4.1 Analytical solution for solving $T(r,t)$ directly

$$\frac{1}{\alpha} \cdot \frac{dT}{dt} = \frac{1}{r^2} \frac{d}{dr} r^2 \frac{dT}{dr}$$

Boundary Conditions:

$$T(0, t) = \text{finite}$$

$$\frac{dT}{dr}(r = R) = 0$$

Initial Condition:

$$T(r, 0) = \frac{T_0}{2} \left(1 - \cos\left(\frac{\pi \cdot r}{R}\right)\right)$$

set:

$$T(r, t) = \frac{\bar{T}}{r}$$

$$\frac{1}{\alpha} \cdot \frac{d\bar{T}}{dt} \frac{1}{r} = \frac{1}{r^2} \frac{d}{dr} r^2 \left( \frac{d\bar{T}}{dr} \frac{1}{r} - \frac{1}{r^2} \bar{T} \right)$$

$$\frac{1}{\alpha} \cdot \frac{d\bar{T}}{dt} = \frac{1}{r} \frac{d}{dr} \left( \frac{d\bar{T}}{dr} r - \bar{T} \right)$$

$$\frac{1}{\alpha} \cdot \frac{d\bar{T}}{dt} = \frac{1}{r} \left( \frac{d^2\bar{T}}{dr^2} r + \frac{d\bar{T}}{dr} - \frac{d\bar{T}}{dr} \right)$$

$$\frac{1}{\alpha} \cdot \frac{d\bar{T}}{dt} = \frac{d^2\bar{T}}{dr^2}$$

turns into a cartesian problem.

Applying Separation of Variables:

$$\bar{T}(r, t) = \Gamma(t)\Psi(r)$$

Boundary Conditions:

$$\Psi(r = 0) = finite$$

$$\frac{d\Psi}{dr}(r = R) = 0$$

Applying the new variables, dividing both sides by  $\Gamma(t)\Psi(r)$ , and setting it to a new variable  $-\beta^2$ :

$$\frac{1}{\alpha\Gamma} \cdot \frac{d\Gamma}{dt} = \frac{d^2\Psi}{dr^2} \frac{1}{\Psi} = -\beta^2$$

Solving for  $\Psi$  first:

$$\frac{d^2\Psi}{dr^2} \frac{1}{\Psi} = -\beta^2$$

$$\frac{d^2\Psi}{dr^2} + \beta^2\Psi = 0$$

$$\Psi(r) = C_1 \sin(\beta r) + C_2 \cos(\beta r)$$

Applying the first boundary condition, interpreting as  $\frac{d\Psi}{dr}(r = 0) = 0$ ,  $C_1 = 0$

Applying the second boundary condition,

$$0 = -C_2\beta\sin(\beta R)$$

$$\sin(\beta R) = 0$$

$$\beta R = \pi, 2\pi, 3\pi \dots$$

$$\beta_n = \frac{n\pi}{R} \quad \text{where } n = 0 \text{ to } \infty$$

Solving for  $\Gamma(t)$ :

$$\frac{1}{\alpha\Gamma} \cdot \frac{d\Gamma}{dt} = -\beta_n^2$$

$$\frac{1}{\alpha\Gamma} \cdot \frac{d\Gamma}{dt} = -\beta_n^2\alpha\Gamma$$

$$\Gamma(t) = A_1 e^{-\alpha\beta_n^2 t}$$

This makes  $\bar{T}(r, t)$ :

$$\bar{T}(r, t) = A_n e^{-\alpha\beta_n^2 t} \sin(\beta_n r)$$

$$\beta_n = \frac{n\pi}{R} \quad \text{where } n = 0 \text{ to } \infty$$

Solving back for  $T(r, t)$ :

$$T(r, t) = \frac{A_n}{r} e^{-\alpha\beta_n^2 t} \sin(\beta_n r)$$

Applying initial condition and orthogonality:

$$T(r, 0) = \frac{A_n}{r} \sin(\beta_n r) = \frac{T_0}{2} (1 - \cos(\frac{\pi \cdot r}{R}))$$

$$A_n = \frac{\int_0^R \frac{T_0 r^3 \sin(\beta_n r)}{2} (1 - \cos(\frac{\pi \cdot r}{R})) dr}{\int_0^R r^2 \sin^2(\beta_n r) dr}$$

The analytical solution is:

$$T(r, t) = \frac{\int_0^R \frac{T_0 r^3 \sin(\beta_n r)}{2} (1 - \cos(\frac{\pi r}{R})) dr}{r \int_0^R r^2 \sin^2(\beta_n r) dr} e^{-\alpha \beta_n^2 t} \sin(\beta_n r)$$

$$\beta_n = \frac{n\pi}{R} \quad \text{where } n = 0 \text{ to } \infty$$

## 4.2 Analytical solution by defining new temperature

$$T'(r, t) = T(r, t) - T_{ss}$$

$$T'(r, t) + T_{ss} = T(r, t)$$

where  $T_{ss}$  is:

$$0 = \frac{1}{r^2} \frac{d}{dr} r^2 \left( \frac{dT_{ss}}{dr} \right)$$

$$\frac{C_1}{r^2} = \frac{dT_{ss}}{dr}$$

$$-\frac{C_1}{r} + C_2 = T_{ss}$$

applying BC:

at  $r = 0$ , finite, makes  $C_1 = 0$

$$T_{ss} = C_2$$

Plugging the new definition into the original differential equation:

differential equation becomes:

$$\frac{1}{\alpha} \left( \frac{dT'}{dt} + \frac{dT_{ss}}{dt} \right) = \frac{1}{r^2} \frac{d}{dr} r^2 \left( \frac{dT'}{dr} + \frac{dT_{ss}}{dr} \right)$$

Considering

$$\frac{dT_{ss}}{dt} = \frac{dT_{ss}}{dr} = 0$$

,

$$\frac{1}{\alpha} \cdot \frac{dT'}{dt} = \frac{1}{r^2} \frac{d}{dr} r^2 \cdot \frac{dT'}{dr}$$

Boundary Conditions:

$$T'(0, t) = finite$$

$$\frac{dT'}{dr}(r = R) = 0$$

Initial Condition:

$$T'(r, 0) = \frac{T_0}{2} (1 - \cos(\frac{\pi \cdot r}{R})) - C_2$$

set:

$$T'(r, t) = \frac{\overline{T'}}{r}$$

$$\frac{1}{\alpha} \cdot \frac{d\overline{T'}}{dt} \frac{1}{r} = \frac{1}{r^2} \frac{d}{dr} r^2 \left( \frac{d\overline{T'}}{dr} \frac{1}{r} - \frac{1}{r^2} \overline{T'} \right)$$

$$\frac{1}{\alpha} \cdot \frac{d\overline{T'}}{dt} = \frac{1}{r} \frac{d}{dr} \left( \frac{d\overline{T'}}{dr} r - \overline{T'} \right)$$

$$\frac{1}{\alpha} \cdot \frac{d\overline{T'}}{dt} = \frac{1}{r} \left( \frac{d^2 \overline{T'}}{dr^2} r + \frac{d\overline{T'}}{dr} - \frac{d\overline{T'}}{dr} \right)$$

$$\frac{1}{\alpha} \cdot \frac{d\overline{T'}}{dt} = \frac{d^2\overline{T'}}{dr^2}$$

turns into a cartesian problem.

Applying Separation of Variables:

$$\overline{T'}(r, t) = \Gamma(t)\Psi(r)$$

Boundary Conditions:

$$\Psi(r = 0) = finite$$

$$\frac{d\Psi}{dr}(r = R) = 0$$

Applying the new variables, dividing both sides by  $\Gamma(t)\Psi(r)$ , and setting it to a new variable  $-\beta^2$ :

$$\frac{1}{\alpha\Gamma} \cdot \frac{d\Gamma}{dt} = \frac{d^2\Psi}{dr^2} \frac{1}{\Psi} = -\beta^2$$

Solving for  $\Psi$  first:

$$\frac{d^2\Psi}{dr^2} \frac{1}{\Psi} = -\beta^2$$

$$\frac{d^2\Psi}{dr^2} + \beta^2\Psi = 0$$

$$\Psi(r) = C_1\sin(\beta r) + C_2\cos(\beta r)$$

Applying the first boundary condition, interpreting as  $\frac{d\Psi}{dr}(r = 0) = 0$ ,  $C_1 = 0$

Applying the second boundary condition,

$$0 = -C_2\beta\sin(\beta R)$$

$$\sin(\beta R) = 0$$



$$\beta R = \pi, 2\pi, 3\pi \dots$$

$$\beta_n = \frac{n\pi}{R} \quad \text{where } n = 1 \text{ to } \infty$$

Solving for  $\Gamma(t)$ :

$$\frac{1}{\alpha\Gamma} \cdot \frac{d\Gamma}{dt} = -\beta_n^2$$

$$\frac{1}{\alpha\Gamma} \cdot \frac{d\Gamma}{dt} = -\beta_n^2 \alpha\Gamma$$

$$\Gamma(t) = A_1 e^{-\alpha\beta_n^2 t}$$

This makes  $\overline{T'}(r, t)$ :

$$\overline{T'}(r, t) = A_n e^{-\alpha\beta_n^2 t} \sin(\beta_n r)$$

$$\beta_n = \frac{n\pi}{R} \quad \text{where } n = 1 \text{ to } \infty$$

Solving back for  $T'(r, t)$ :

$$T'(r, t) = \frac{A_n}{r} e^{-\alpha\beta_n^2 t} \sin(\beta_n r)$$

Applying initial condition and orthogonality:

$$T'(r, 0) = \frac{A_n}{r} \sin(\beta_n r) = \frac{T_0}{2} (1 - \cos(\frac{\pi \cdot r}{R})) + C_2$$

$$A_n = \frac{\int_0^R r^3 \sin(\beta_n r) (\frac{T_0}{2} \cdot (1 - \cos \frac{\pi r}{R}) + C_2) dr}{\int_0^R r^2 \sin^2 \beta_n r dr}$$

The analytical solution is:

$$T'(r, t) = \frac{\int_0^R r^3 \sin(\beta_n r) (\frac{T_0}{2} \cdot (1 - \cos \frac{\pi r}{R}) + T_{ss}) dr}{\int_0^R r^2 \sin^2 \beta_n r dr} e^{-\alpha\beta_n^2 t} \sin(\beta_n r)$$

$$\beta_n = \frac{n\pi}{R} \quad \text{where } n = 1 \text{ to } \infty$$

$$T = \frac{\int_0^R r^3 \sin(\beta_n r) \left( \frac{T_0}{2} \cdot (1 - \cos \frac{\pi r}{R}) + T_{ss} \right) dr}{\int_0^R r^2 \sin^2 \beta_n r dr} e^{-\alpha \beta_n^2 t} \sin(\beta_n r) + T_{ss}$$

Since the solution from section 4.1 with  $n = 0$  covers the steady state case, this problem is redundant and provides no new insight into the problem from section 4.1.

### 4.3 Code1

```
<institution>
  <name>NO_ddd</name>
  <config><NO_ddd/></config>
  <reactor_list>
    <val>lwr</val>
    <val>sfr</val>
    <val>nox_lwr</val>
  </reactor_list>
```