

ABSTRACT

Title of dissertation:

**PURITY MONITORING TECHNIQUES AND ELECTRONIC
XENON TIME PROJECTION CHAMBERS**

Jon Balajthy, Doctor of Philosophy, 2017

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**Professor Carter Hall
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PURITY MONITORING TECHNIQUES AND ELECTRONIC ENERGY DEPOSITION
XENON TIME PROJECTION CHAMBERS

by

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Dissertation submitted to the Faculty of the Graduate School of the
University of Maryland, College Park in partial fulfillment
of the requirements for the degree of
Doctor of Philosophy
2017

Advisory Committee:
Professor Carter Hall, Chair/Advisor

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Preface

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Dedication

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Chapter 1: Cosmology Overview

1.1 Standard Model of Cosmology

The standard model (SM) ties together observations and theories of particle physics into a coherent and predictive picture that is well verified by experiment. In the same way, the standard model of cosmology (Λ -CDM) combines the observations of astronomers and cosmologists in the context of general relativity. Although the standard model paints a comprehensive picture of particles that have been observed, it accounts for only 4.9%[4] of the mass-energy content of the Λ -CDM model.

The Λ -CDM model is built on the foundation of the Robertson-Walker metric:

$$ds^2 = -c^2 dt^2 + a(t)^2 [dr^2 + S_\kappa(r)d\Omega] \quad (1.1)$$

$$S_\kappa(r) = \begin{cases} R_0 \sinh(r/R_0) & \text{for } \kappa = 1 \\ r & \text{for } \kappa = 0 \\ R_0 \sin(r/R_0) & \text{for } \kappa = -1 \end{cases} \quad (1.2)$$

This metric assumes an isotropic and homogenous universe, but allows for both time dependent expansion and uniform curvature. The unitless “scale factor”, $a(t)$, describes the expansion and contraction of the spatial part of the metric. The curvature of space is characterized by a radius of curvature R_0 and the parameter κ , which is 0 if the universe is flat

and otherwise indicates the sign of the curvature.

The time-dependence in the scale factor can now be described to first and second order. The Friedmann equation is a solution to Einstein's field equations that relates the rate of change in the scale factor to the energy density of the universe, ε :

$$H^2 \equiv \left(\frac{\dot{a}}{a} \right)^2 = \frac{8\pi G}{3c^2} \varepsilon - \frac{\kappa c^2}{R_0^2 a^2}, \quad (1.3)$$

where G is the gravitational constant. Equation 1.3 also introduces the Hubble constant, H , which describes the expansion rate of the scale factor. The second order equation is obtained through an application of the first law of thermodynamics for an adiabatically expanding universe. This gives the fluid equation, which connects the change in energy density to pressure:

$$\dot{\varepsilon} + 3 \frac{\dot{a}}{a} (\varepsilon + P) = 0 \quad (1.4)$$

By combining equations 1.3 and 1.4, the acceleration equation is found:

$$\frac{\ddot{a}}{a} = -\frac{4\pi G}{3c^2} (\varepsilon + 3P). \quad (1.5)$$

In an empty universe where ε is zero, the time evolution of the scale factor is trivial. The curvature can be either flat or negative, but a positive curvature would lead to a non-physical result in equation 1.3. In a flat, empty universe the scale factor would be static, and in a negatively curved universe, the scale factor would increase at a constant rate for all time. To describe the time-evolution of the scale factor in a universe where $\varepsilon \neq 0$, there is one further puzzle piece required. A universe can contain multiple component energy densities which will each contribute a unique pressure. The relation between the total energy density

and pressure is given by the equation of state:

$$P = \sum_w w \epsilon_w, \quad (1.6)$$

where w is a parameter specific to each component.

The total energy density is equal to the sum of the component densities, ϵ_w . These are often normalized to the critical density, $\epsilon_c = \frac{3c^2}{8\pi G} H(t)^2$ and expressed as density parameters, $\Omega_w = \epsilon_w / \epsilon_c$. The components of interest in this universe are radiation (which includes relativistic matter), non-relativistic matter, and a contribution from the cosmological constant, Λ (also referred to as dark energy), for which $w = 1/3, 0, -1$ respectively. Radiation and matter both act to slow down the expansion rate of the universe, while Λ acts to accelerate it. This can be seen more clearly by examining the scale factor in the case of a universe with a single component energy density. The time dependences of the scale factor for single component universes are shown in Table 1.1.

Single Energy Component	$a(t)$
Negative Curvature	t/t_0
Matter	$(\frac{t}{t_0})^{2/3}$
Radiation	$(\frac{t}{t_0})^{1/2}$
Λ	$e^{H_0(t-t_0)}$

Table 1.1: Here is shown the time dependence of the scale factor, a , in various single energy component universes.

Matter, radiation, and Λ themselves have different dependences on $a(t)$. Matter density is related to the number density of particles, so as $a(t)$ increases, ϵ_{matter} will decrease like $1/a(t)^3$. In addition to its dependence upon number density, $\epsilon_{radiation}$ also has a dependence upon the frequency of the radiation. Since an increasing $a(t)$ stretches the radiation's wavelength, thereby decreasing its frequency, $\epsilon_{radiation}$ will gain an additional factor of $1/a(t)$ in its time dependence, so $\epsilon_{radiation}$ will decrease proportional to $1/a(t)^4$ [69].

The most widely accepted and best supported model for the current universe has no curvature, is old enough that the radiation component has become negligible, and contains a comparable density of matter and Λ . This model is referred to as the Λ -CDM model.

1.2 The Cosmic Microwave Background

The various parameters for the Λ -CDM model are best constrained by measurements of the cosmic microwave background by the Planck experiment, which constrains Ω_{matter} to 0.3089 ± 0.0062 and Ω_Λ to 0.6911 ± 0.0062 [4]. The Planck experiment, along with its predecessors, aimed to create a detailed map of the cosmic microwave background. This background is a snapshot of the universe from only 350,000 years after the big bang.[69] Before that time, the universe was hot enough that electrons could not bind to protons to form atoms, and the scattering rate of photons off of this plasma was high enough for them to thermalize into a blackbody spectrum. Once the scattering rate of high energy photons dropped below the expansion rate of the universe, electrons and protons began forming atoms, which in turn lowered the scattering rate even more. This caused the blackbody photons to rapidly become decoupled from the matter, thus preserving their blackbody spectrum. These photons are what today form the cosmic microwave background (CMB).

Due to random fluctuations, there were anisotropies in the primordial plasma, which tended to fall toward areas with higher densities. This caused the over-densities to become amplified until eventually the increased radiation pressure would overtake the force of gravity, causing the plasma to rebound and expand until the now falling pressure was overtaken the gravitational pull of the over-density. This process led to a “ringing” in the primordial plasma, which is referred to as baryon acoustic oscillations (BAO). BAO began at the end of the inflationary period and ended after the epoch of recombination, when photons decoupled from protons and electrons.

BAO can be seen today as ripples in the CMB. These ripples can be most clearly seen in the angular correlation power spectrum of the CMB shown in Figure 1.1. The highest peak at $l \approx 200$, corresponds to about 1° , the angular scale at which the plasma had time to fall into its first compression before photon-decoupling. The second peak corresponds to the scale at which plasma had time to compress and rebound to its first rarefaction. The higher- l peaks show this processes repeating itself, with odd numbered peaks corresponding to compressions and even numbered peaks corresponding to rarefactions.

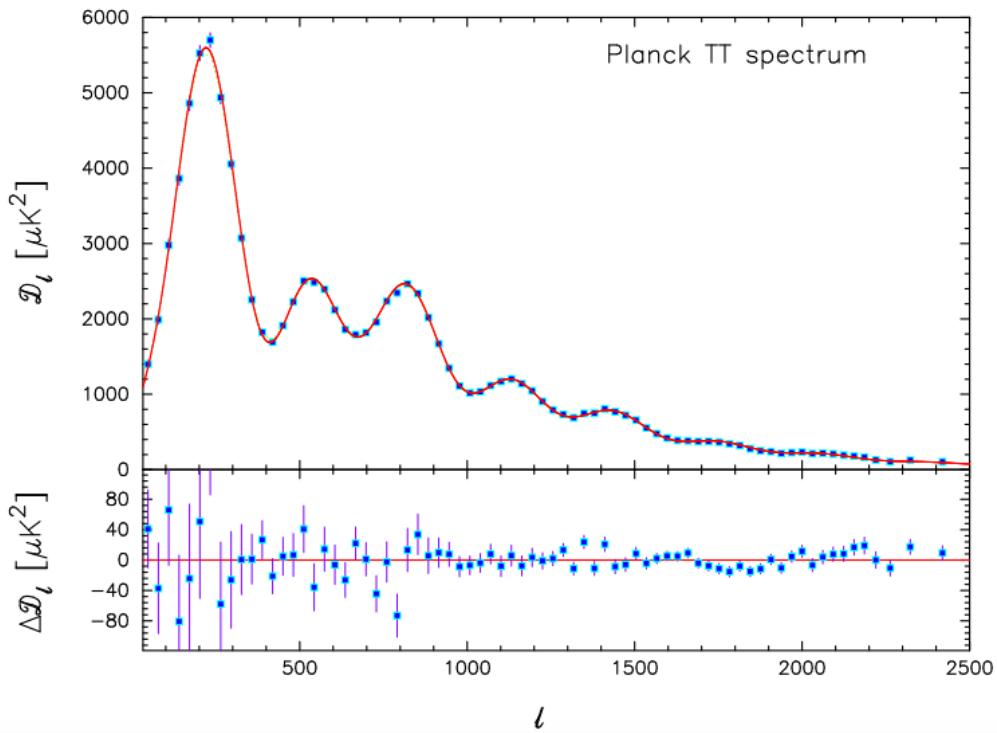


Figure 1.1: Angular correlation power spectrum of the CMB as measured by the Planck experiment. The red line shows the best fit spectrum assuming the Λ -CDM model. [4]

1.3 Dark Matter

There is one piece of the Λ -CDM puzzle that is conspicuous in its absence from the description so far. Cold Dark Matter (“CDM” in “ Λ -CDM”) is one of the key elements

of the model. Without a driving force external to the photon-baryon plasma, the baryon acoustic oscillations would decay exponentially. The prominence of the third peak relative to the first and second points to the need for an additional form of matter. This matter would be out of equilibrium with the plasma, and so would collapse into the primordial over-densities, but not experience a restorative pressure. As the baryons oscillate, this “dark matter” would continue to accumulate, strengthening the gravitational well. This matter would necessarily couple strongly to neither itself, nor the photons or baryons in the plasma.

1.3.1 Galaxy Clusters

The evidence for dark matter from the CMB is relatively recent. Astronomers have been chasing the missing matter problem for almost a century. The first conclusive evidence for what is now known as dark matter came from Fritz Zwicky’s observations of the velocity distribution of galaxies in the Coma Cluster in 1933[81], although calculations by Jan Oort of stellar velocities in the Sombrero galaxy hinted that something was amiss a year earlier in 1932[64]. Assuming that the galactic velocities in the Coma cluster are in a stationary state, the virial theorem can be applied:

$$\bar{V} = -2\bar{K}, \quad (1.7)$$

where \bar{V} is the average total potential energy of the system, and \bar{K} is the average total kinetic energy of the system. Assuming a spherically symmetric system governed by Newtonian gravity, Zwicky then made the following approximations for his calculations:

$$V \approx \frac{-3GM}{5R} \quad (1.8)$$

$$K \approx \frac{1}{2} M \bar{v}^2, \quad (1.9)$$

where M is the total mass of the cluster, and \bar{v} is the velocity of galaxies in the cluster, averaged over time and mass. Using observations of the doppler shift of the light coming from galaxies within the cluster, Zwicky was able to measure the component of the velocities along the line of sight. He then made the assumption that the velocities are isotropic in order to extrapolate to the overall distribution, $\bar{v} = \bar{v}_{LS}$.

Using this method, Zwicky placed a conservative limit of $M > 4.5 \cdot 10^{13} \odot$ on the mass of the Coma cluster. Comparing this result to the amount of light coming from the cluster, he found that the mass-to-light ratio was more than 100 times larger than typical values for local stellar systems. This was the first indication that a large percentage of matter in the universe is not luminous[81].

1.3.2 Galactic Rotation Curves

Continuing from the early measurements of the spiral galaxies by Jan Oort, it was further observed that the other galaxy types also display strong evidence of containing dark matter[70]. A spiral galaxy is well approximated by a flat disk. This makes it possible to measure its galactic rotation curve, or the orbital velocity as a function of radius. Measurements of galactic rotation curves provide some of the most clear and compelling evidence for both the existence and behavior of dark matter on galactic scales.

Measurement's of the luminosity of galaxies show that the density of visible matter tends to decrease exponentially with radius from the galactic center:

$$I(R) = I_0 e^{-R/R_s}, \quad (1.10)$$

where R is the radius from the galactic center, and R_S is the a length scale specific to each galaxy. For the Milky Way R_S is about 4 kpc[69]. This exponential drop would lead rotation curves proportional to $1/\sqrt{R}$. In contradiction to this, spectroscopic measurements of stars near the galactic center and the H α line outside of the optical radius, show that the rotation curves of spiral galaxies tend to become flat at large radii[68, 70]. Beginning with Vera Rubin in 1980 [68] and continuing with Massimo Persic and Paolo Salucci [70] among others, researchers went on to characterize the rotational velocities of spiral galaxies by a “universal rotation curve” (URC).

The URC has two components, one from the luminous, exponentially decreasing disk and the other from a “dark halo” which surrounds the galaxy. This dark halo can be thought of as a gas which permeates and surrounds the disk. As a function of R/R_{opt} , the mass and velocity contributions from this component are:

$$V_d^2 = V^2(R_{opt})(1 - \beta)(1 + a^2) \frac{x^2}{x^2 + a^2}, \quad (1.11)$$

$$M_h(x) = G^{-1}V^2(1)R_{opt}(1 - \beta)(1 + a^2) \frac{x^3}{x^2 + a^2}. \quad (1.12)$$

Both β , the fraction of disk mass inside of the optical radius, and a , the radius of the halo core are completely determined by the luminosity in this model. The URC fits the observed data very well (on average fitting errors are within 1%).

More recently, models based on n-body simulations of cold dark matter have become more popular. The most well known of these is the Navarro-Frenk-White (NFW) model. These models produce good fits to high-luminosity galaxies such as the Milky Way, but tend to produce cusps at the galactic center and have trouble replicating the flat cores observed in dwarf galaxies. It is possible that this tension could be resolved by gravitational fluctuations

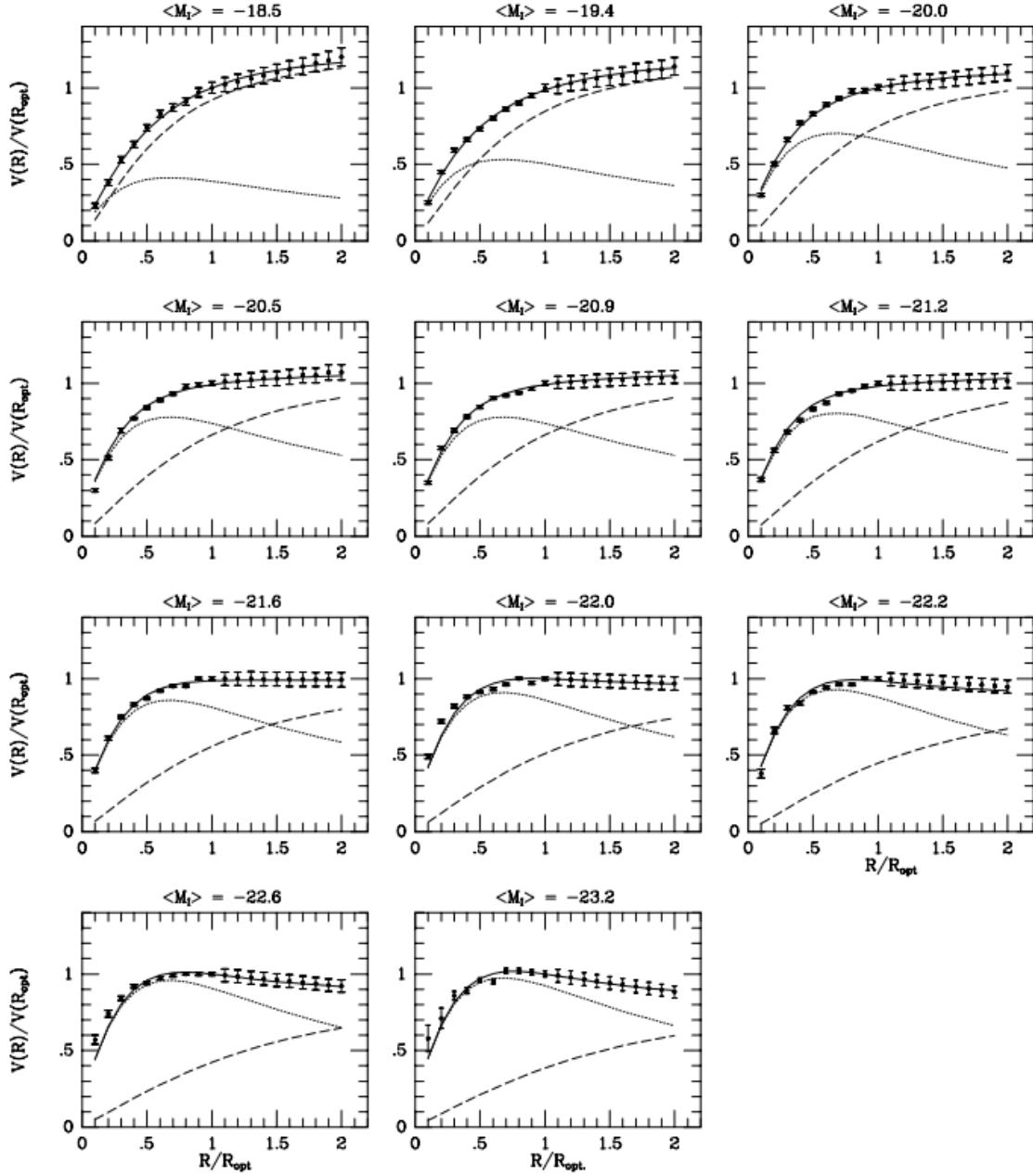


Figure 1.2: URC (solid lines) fit to average rotation curves surveyed spiral galaxies. The subfigures show bins in luminosity each of which contain about 50 individual rotation curves. Also shown are the contributions from the luminous disk (dotted line) and dark halo (dashed line)[70].

or by substructure within the halo at the center of these dwarf galaxies, but the “Cusp-Core” problem remains an active area of study[63, 78].

1.3.3 Modified Newtonian Dynamics

The agreement between observation of galactic rotation curves and cluster dynamics is quite remarkable, however there is an alternate hypothesis to dark matter that fits the data equally well in many of these cases. Modified Newtonian Dynamics (MOND) postulates that the force of gravity as described by Newton and Einstein is incomplete. In 1983, Milgrom showed that an interpolating function, μ , could be added to Newton’s second law to describe the dynamics of galaxies and clusters without the need for dark matter.

$$m_g \mu(a/a_0) \vec{a} = \vec{F} \quad (1.13)$$

This interpolating function would be ≈ 1 at large accelerations, $a \gg a_0$, reproducing the classical equation of motion, but would approach $\mu x = x$ when $a \ll a_0$, where $a_0 = 2 \times 10^{-8} \text{ cm} \cdot \text{s}^{-2}$ is a fundamental constant[17, 61].

Following their initial paper in 1983, M. Milgrom and J. Bekenstein reformulated MOND as a classical, lagrangian based field theory, known as AQUAL. In 2004 Bekenstein again reformulated MOND in the context of general relativity. This new tensor-vector-scalar covariant theory is referred to as TeVeS[17]. Both of these theories can produce good fits to galactic rotation data in many cases, but among other problems, neither can fully describe cluster dynamics without the addition of some dark matter[17, 25].

1.3.4 Gravitational Lensing

One of the single most compelling pieces of evidence for dark matter, especially in relation to MOND theories, comes from gravitational lensing data of galactic cluster 1E

0657-56, more commonly known as the bullet cluster. This cluster consists of two sub-clusters that recently collided and passed through each other. One of these subclusters displays a distinct bow shock that enabled researchers to make a precise measurement of its Mach number, thereby also measuring its velocity. The measured Mach number, $3.2^{+0.8}_{-0.6}$ corresponds to a velocity of $4500^{+1100}_{-800} \text{ km/s}$ [57].

During the collision, the gas from the two subclusters would be expected to experience much stronger drag than the stellar matter. This expectation was confirmed by x-ray imaging data from Chandra, which showed that the gas was lagging behind the stars. Further comparison to a mass mapping using gravitational lensing reveals additional matter populations centered near the stellar matter, which are taken to be the dark matter halos of the two subclusters. Fitting a King mass profile ($\rho = \rho_0(1 + r^2/r_c^2)^{-3/2}$) to the lensing data, Markevitch et. al. calculated the density of the dark matter, and limited the self interaction cross section to $\sigma/m < 1 \text{ cm}^2 \text{ g}^{-1}$ [57].

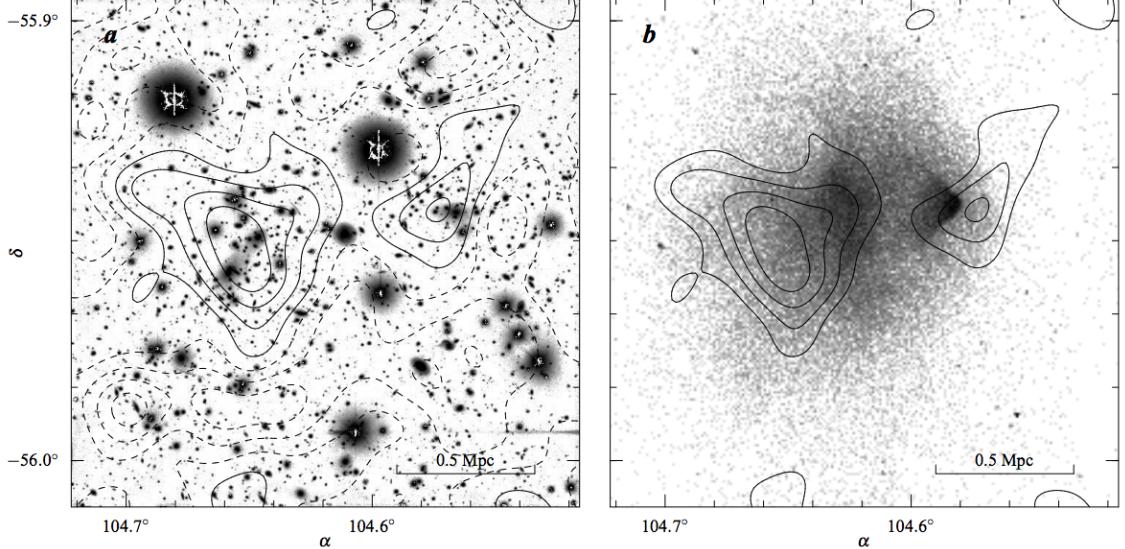


Figure 1.3: Comparison of the location of dark matter, stellar matter, and x-ray gas in the bullet cluster. The mass density from lensing data, indicated by the solid black lines is imposed over optical (left) and x-ray (right) maps[57].

1.4 Dark Matter Candidates

1.4.1 Baryonic Dark Matter

Now that the existence of cold dark matter has been well motivated, the next step is to investigate what it might be. A reasonable starting point is to look at types of matter that are already known to exist, and ask whether they could exist in high enough abundances to explain the observations of galaxy and cluster dynamics as well as angular correlations in the CMB.

Within the standard model, the first place to look for dark matter is baryonic matter. It is possible, for instance, that the dark halo is, at least partially, composed of large structures of baryonic material such as brown dwarfs or planets. These massive compact halo objects (MaCHO's) should be observable through gravitational lensing. As a MaCHO passes between an observer on Earth and a background star, the light from that galaxy will be temporarily distorted through gravitational lensing. The EROS-2 experiment conducted a survey of the large Magellanic clouds and found insufficient lensing events to allow MaCHO's as a primary constituent of the Milky Way's dark halo[75].

A more general constraint on baryonic dark matter comes from measurements of big bang nucleosynthesis (BBN). BBN refers to the epoch at which the temperature of the universe dropped below the binding energy of deuterium (2.22 MeV). This happened when the universe was about 5 minutes old. During this epoch, the primordial abundances of light nuclei are set as the protons and neutrons are allowed to combine into energetically favored states. The ratios of these abundances are highly dependent on η , the baryon-photon ratio, so the measurement of them, combined with constraints on the photon density from CMB measurements would give a precise value for the baryon density[69]. Current measurements of D/H place the baryon density at $\Omega_b h^2 = 0.02202 \pm 0.00046$ [27].

This result is within 1σ of the measurement from the Planck experiment, and taking the reduced Hubble constant to be $h = 0.678$, it indicates that baryons make up only 4.8% of the energy-density of the universe[4].

1.4.2 Neutrinos

The remaining candidate for standard model dark matter is the neutrino. Before the CMB decoupled, neutrinos went through a similar process which left the universe filled with neutrinos that had been in thermal equilibrium with the extremely hot and dense early universe. From the annihilation cross-section, the number density of the cosmic neutrino background (CNB) can be calculated to be 3/11 that of CMB photons[69],

$$n_\nu = 3.36 \times 10^8 \text{ m}^{-3}. \quad (1.14)$$

In order for the CNB to fit the mass density requirement for dark matter, the mass of neutrinos would have to be about 4 eV.[69] Current constraints from Planck show that the combined mass of neutrinos is $< 0.23 \text{ eV}$ [4], so neutrinos are not heavy enough to explain the majority of observed dark matter.

1.4.3 Axions

Currently, the two most popular CDM candidates are Axions and WIMPs. Axions are particularly interesting because they were first theorized as part of a solution to the strong CP problem, and so could simultaneously solve two unsolved problems in physics. Charge-parity (CP) is only conserved by QCD if the vacuum angle, θ , is 0. However, θ should be able to take any value, so CP is not predicted to be conserved. Experimental measurements of the neutron electric dipole moment (nEDM) show that CP is, in fact, a good symmetry of QCD. The current limit on nEDM is about $2 \times 10^{-26} \text{ e} \cdot \text{cm}$, which in turn limits θ to

$\leq 10^{-9}$ [15, 33]. This unexpectedly small value of θ points to a tension within QCD. To relieve this tension, R. Peccei and H. Quinn proposed a new spontaneously broken global symmetry, $U_{PQ}(1)$, and showed that if the Higgs potential for at least one quark is invariant under $U_{PQ}(1)$, then θ is guaranteed to relax to 0. The pseudo-Nambu-Goldstone boson that is associated with the spontaneous breaking of $U_{PQ}(1)$ is known as the axion [33, 66].

The axion as a candidate for CDM is compelling in that it interacts only very weakly with standard model particles. Axions are expected to have mass, but be light enough that those produced thermally in the big bang would be too hot to fill the role of CDM. However, populations of axions can be formed non-relativistically in the early universe through vacuum realignment and topological effects in string theory. Axion dark matter created through realignment would be expected to have a mass $m_a > 6 \mu eV$, assuming the initial value of θ was of order unity. If the initial value of θ was much smaller than 1, the axion mass could be less than $6 \mu eV$ [33].

Axion searches focus primarily on the tree-level axion-photon coupling, which has the Lagrangian term $\mathcal{L}_{a\gamma\gamma} = g_{a\gamma\gamma} \mathbf{E} \cdot \mathbf{B}$. In the core of a star, the conversion of photons to axions can compete with the production of photons and stream energy away from the core. This would reduce the pressure and causing the star to compress and heat up, and in so doing, shorten the life of the star. Observations of horizontal branch stars limit the coupling constant for this process to $g_{a\gamma\gamma} < 10^{-10} GeV^{-1}$, and excludes axion mass in the range $10^{-3} eV < m_a < 2 eV$ [33, 40].

In the laboratory, the conversion of axions to photons, and vice versa can be induced in a cavity containing a strong magnetic field. The CAST experiment at CERN used such a cavity to search for axions streaming from the sun. By adding a precisely tuned pressure of helium gas to the cavity, they maximized their sensitivity, and placed a limit of $g_{a\gamma\gamma} < 2.2 \times 10^{-10} GeV^{-1}$ for axions with mass $m_a < 0.4 eV$ [33, 40].

The previously cited limits are on axions that were formed in the cores of stars. These

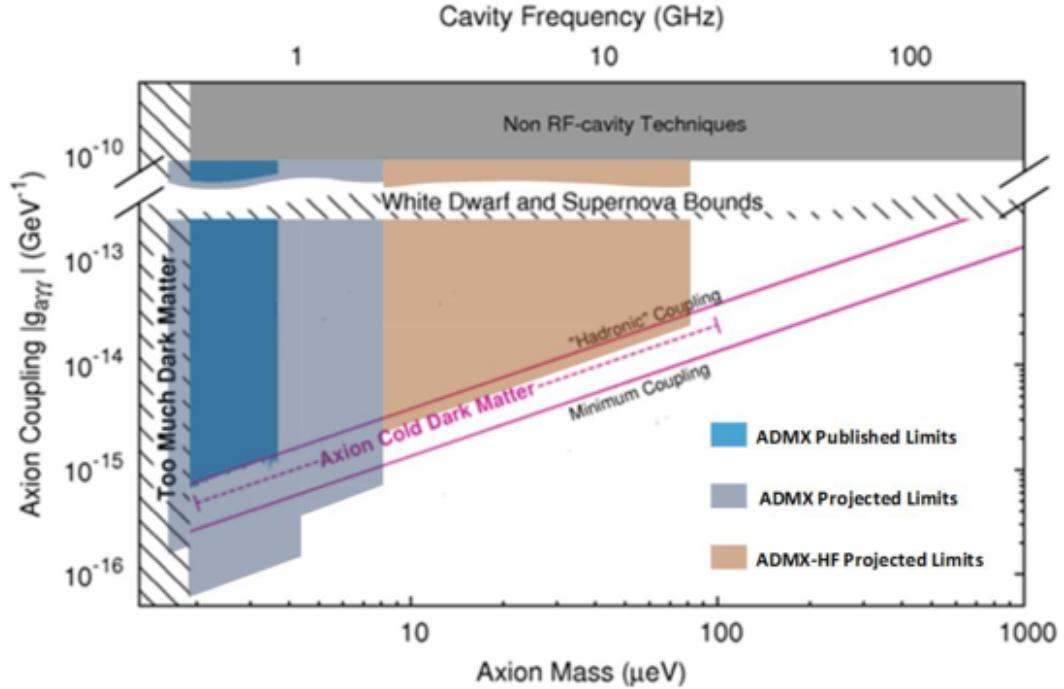


Figure 1.4: Long term projected limits of the ADMX and ADMX-HF experiments. [73]

axions, if they existed, would not be able to fill the CDM role. Currently, the only experiment that would be sensitive to dark matter axions is the Axion Dark Matter Experiment (ADMX). This experiment aims to convert axions from the local dark halo into photons using a microwave resonant cavity permeated with a strong magnetic field. In this scenario, a DM axion would interact with a virtual photon from the magnetic field to convert into a real RF photon which can be detected. ADMX and it's sister experiment ADMX-HF are looking for axion dark matter in the mass range $2\mu eV$ to $100\mu eV$ and are expected to be able to probe most of the allowable axion CDM phase space[33, 73].

1.4.4 WIMPs

The other leading candidate for CDM is what is referred to as the Weakly Interacting Massive Particle, or WIMP. “WIMP” is a somewhat generic term for a massive particle that couples to standard model particles only through the weak nuclear force. This generic WIMP particle is usually denoted as χ . Many extensions to the standard model, in particular supersymmetric models, include at least one flavor of WIMP. In the very early universe WIMPs will be in equilibrium with the primordial plasma. Just as with CMB photons and CNB neutrinos, once the temperature drops and the universe expands the number and temperature of WIMPs will fall out of equilibrium and the particles remaining will persist as a cosmic relic[38, 47].

When the temperature of the universe is higher than the WIMP mass, m_χ (roughly 10 GeV to 1 TeV) both the WIMP number density, n_χ , and temperature will be in thermal equilibrium. Once the temperature drops below the WIMP mass, the number density will fall out of equilibrium and will pick up a Boltzmann suppression factor of $e^{-m_\chi/T}$. Once the scattering rate of cosmic WIMPs drops below expansion rate of the universe, χ particles will no longer be able to find each other to annihilate, and n_χ will freeze out, becoming the relic density that exists today[38].

This relic density is determined by the mass of χ , as well as its self-annihilation cross section, σ_A , but is much more strongly dependent upon the cross section.[38, 47] If σ_A is on the scale of the weak force, the density parameter for relic WIMPs will be on the order of what is required for Ω_{CDM} . This is considered one of the most compelling reasons to consider WIMPs as CDM candidates, and has been referred to as the “WIMP miracle”[19, 38, 47].

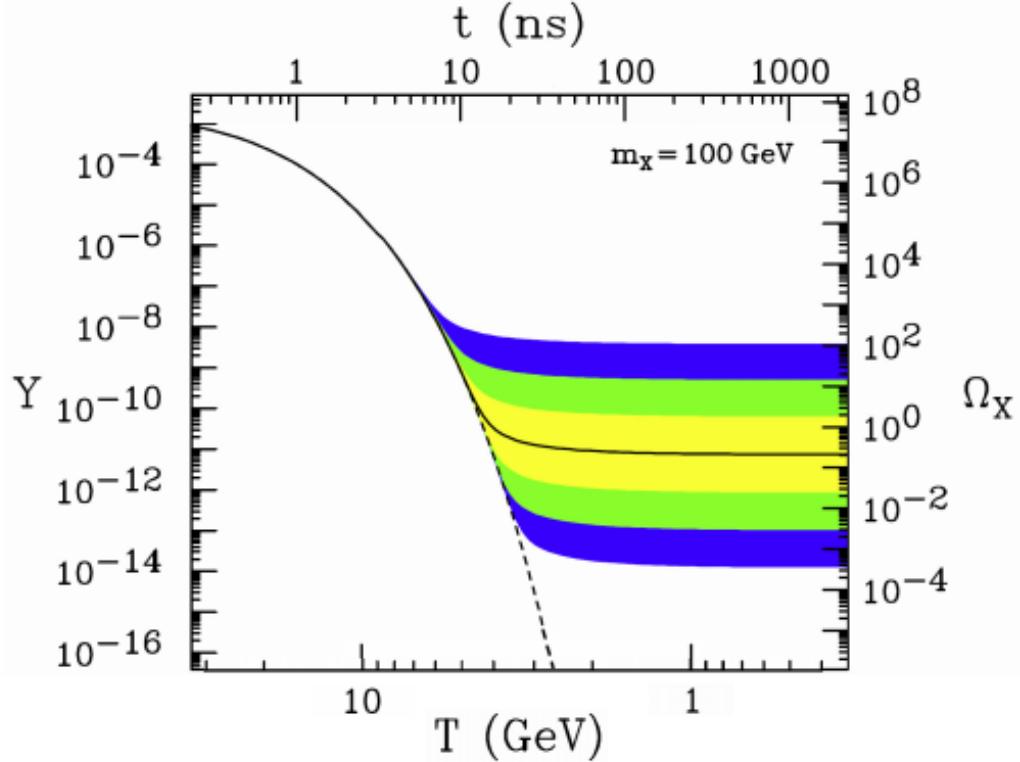


Figure 1.5: WIMP number density in the early universe. The solid line corresponds to the cross section required to account for 100% of CDM. The colored bands indicate variations by factors of 10, 100 and 1,000[38].

The creation of the relic density is described by the Boltzmann equation:

$$\frac{dn_\chi}{dt} = -3Hn_\chi - \langle \sigma_A v \rangle (n_\chi^2 - n_{eq}^2). \quad (1.15)$$

In equation 1.15, the first term on the right hand side is from the expansion of the universe, the n_χ^2 term is from self annihilation, and the n_{eq}^2 is the creation of WIMPs from standard model particles.[38, 47] The value of n_{eq} is what the number density of WIMPs would be in thermal equilibrium in a static universe. Equation 1.15 has no closed form solution and is solved numerically. There is, however, some insight that can be drawn from some rough analysis[19, 38].

The equilibrium number density for non-relativistic dark matter is given by a simple Boltzmann distribution, $n_\chi = g_\chi \frac{m_\chi T}{2\pi} e^{-m_\chi/T}$. [19] Freeze out will occur when the expansion rate of the universe, H , exceeds the annihilation rate of WIMPs, $\Gamma = n_\chi \langle \sigma_A v \rangle$. In rough terms, the freeze out temperature can be defined as the temperature at which H and Γ are equal.[19, 38] In the early universe, it is appropriate to make the approximation $H \approx 1.66g_*^{1/2}T^2$ [47]. In this case the equation $H = \Gamma$ can be rewritten to give the WIMP density at freezeout:

$$n_{\chi,f} \approx g_\chi \frac{m_\chi T_f}{2\pi} e^{-m_\chi/T_f} \approx \frac{1.66g_*^{1/2}T_f^2}{\langle \sigma_A v \rangle} \quad (1.16)$$

The ratio of $x_f \equiv m_\chi/T_f$ remains roughly constant between different WIMP models and has a value of about 1/20. After freeze out, the ratio of n_χ to entropy density, s , is constant. In the early universe, $s \approx 0.4g_*T^3$. Holding (n_χ/s) constant from freeze out to the present day yields the following expression for the current energy density, $n_{\chi,0}$:

$$n_{\chi,0} \approx \frac{1.66g_*^{1/2}T_f^2}{\langle \sigma_A v \rangle} \cdot \frac{s_0}{0.4g_*T_f^3} \quad (1.17)$$

Taking the current entropy density to be $s_0 = 4000 \text{ cm}^{-3}$ yields the following energy density for relic WIMPs:

$$\Omega_\chi h^2 \approx \frac{3 \cdot 10^{-27} \text{ GeV cm}^3}{\langle \sigma_A v \rangle} \quad (1.18)$$

Plugging in a typical weak annihilation cross section of about $10^{-25} \text{ cm}^3 \text{ s}^{-1}$ for $\langle \sigma_A v \rangle$ gives $\Omega_\chi h^2 \approx 0.03 \text{ GeV s}$ which is close enough to the expected value CDM, $\Omega_{CDM} h^2 = 0.1188 \text{ GeV s}$ [4] to make WIMPs an extremely exciting candidate to explain much, if not all, of the non-baryonic dark matter in the universe[38, 47].

1.5 WIMP Direct Detection

The relic density of WIMPs is determined by the cross-section for annihilation into standard model particles, a process which might be observed today by looking for high energy particles coming from high density regions of space such as galactic nuclei. The hypothetical interaction between WIMPs and standard model particles can also be run in two other directions. Production of WIMP dark matter from standard model particles can be searched for using modern particle colliders such as the LHC at CERN, and the scattering of relic dark matter can be probed for using large, low-background detectors. These three methods of detection are referred to as “indirect detection”, “production”, and “direct detection” respectively. Direct detection is of particular interest because it probes the existing relic dark matter background that is postulated by the Λ -CDM model.

1.5.1 Cross Section

The first ingredient needed to calculate the expected interaction rate in a given experiment is the scattering cross section. The WIMP-nucleus scattering cross section will have some dependence on the momentum transfer, q , and can be written[71]:

$$\sigma(q) = \sigma_0 F^2(q), \quad (1.19)$$

where σ_0 is the energy independent, 0-momentum limit of the cross section, and $F(q)$ is an energy dependent form factor. The 0-momentum cross section can be broken into a spin dependent (SD) part and a spin independent (SI) part[51, 71]:

$$\begin{aligned} \sigma_{0,SI} &= \frac{4\mu_A^2}{\pi} [Zf_p + (A-Z)f_n]^2 \\ \sigma_{0,SD} &= \frac{32G_F^2\mu_A^2(J+1)}{\pi J} [a_p\langle S_p \rangle + a_n\langle S_n \rangle]^2 \end{aligned} \quad (1.20)$$

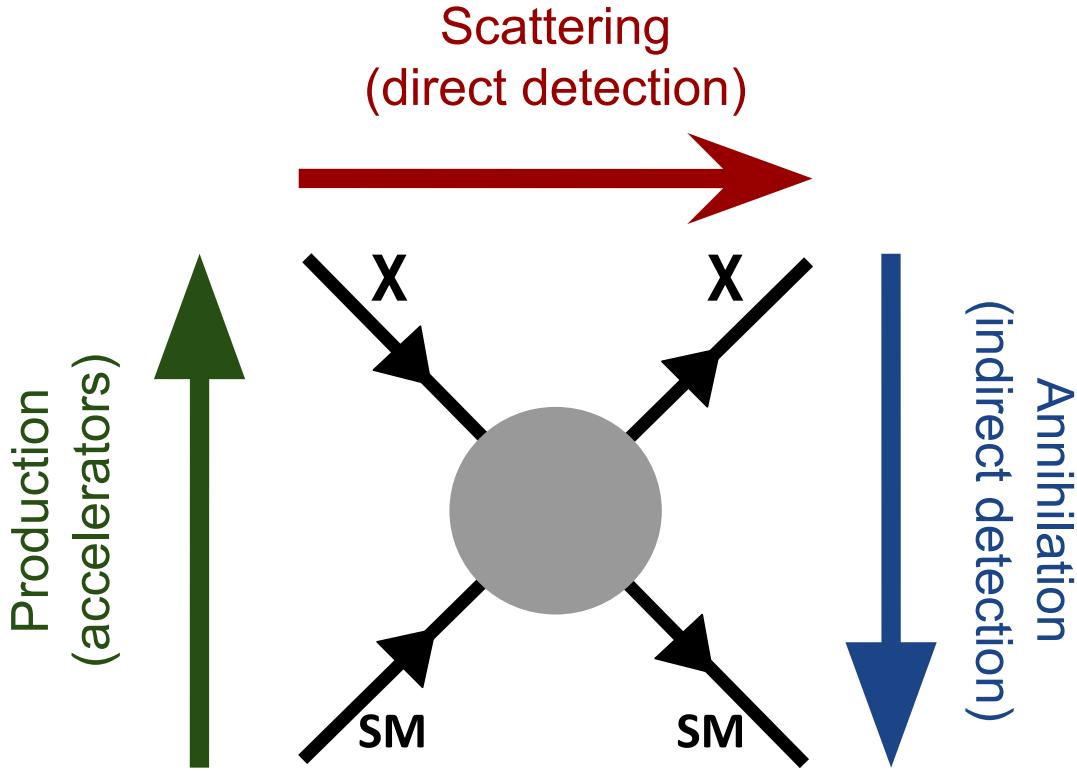


Figure 1.6: Cartoon of the WIMP-standard model interaction. The green, red, and blue arrows indicate in which direction time is being run for production, scattering, and annihilation, respectively.

Here, $f_{p,n}$ and $a_{p,n}$ are the SI and SD coupling constants of WIMPs to protons and neutrons, μ_A is the reduced mass of the interaction, Z is the atomic number, A is the atomic mass, J is the nuclear spin, and $\langle S_{p,n} \rangle$ is the average spin of protons or neutrons in the nucleus. It is typically assumed that $f_p \approx f_n$, so the SI cross section reduces to:

$$\sigma_{0,SI} = \frac{4\mu_A^2}{\pi} f_n^2 A^2. \quad (1.21)$$

The $\mu_A^2 A^2$ dependence in equation 1.21 is a result of the non-relativistic nature of the interaction leading the incident WIMP to scatter coherently off of the nucleus as a whole as opposed to the individual nucleons. This is an important result because it indicates a large

benefit to using heavy nuclei as experimental target media. For instance, a detector which uses xenon as its target medium ($A \approx 131$) will be over 10 times more sensitive to a 100 GeV WIMP than an argon based detector ($A \approx 40$) with the same mass of target material.

Another important result is that the SD cross section does not have the same $\mu_A^2 A^2$ dependence, and in many nuclei the nucleon spins cancel entirely leaving that isotope insensitive to WIMP interactions. In the case of xenon, the only isotopes that have non-zero spin and a non-negligible natural abundance are ^{131}Xe ($J=3/2$) and ^{129}Xe ($J=1/2$), which together make up just under half of the natural xenon abundance. Since for xenon has an even number of protons, $\langle S_p \rangle$ is very close to zero (-0.009 for ^{131}Xe and 0.028 for ^{129}Xe). The neutron part of the SD cross section in ^{129}Xe and ^{131}Xe is about 2,000 and 400 times that of a single-neutron, respectively. We can compare this to the SI cross section of xenon, which is $> 5 \times 10^7$ times larger than the single-nucleon cross section. This suppression of the SD cross section in comparison with the SI cross section has led to much less stringent limits on spin independent interactions than on spin dependent interactions as can be seen in the results from the LUX detector in figure 1.7.

1.5.2 Recoil spectrum

The WIMP halo is expected to have only a small amount of bulk rotation; that is it is expected to be more akin to a gravitationally bound ideal gas than an accretion disk. The velocities of WIMPs in such a halo roughly modelled by a Maxwellian distribution[71]:

$$f(\vec{v}_{halo}) = e^{-v_{halo}^2/v_0^2}/k, \quad (1.22)$$

with $v_0 = 220 \pm 20$ km/s being the local circular velocity around the galactic center and k being a normalization constant. In the lab frame the observed velocity of an incident WIMP will be $\vec{v}_i = \vec{v}_E + \vec{v}_{halo}$. Here, \vec{v}_E is the velocity of the earth with respect to the galaxy which

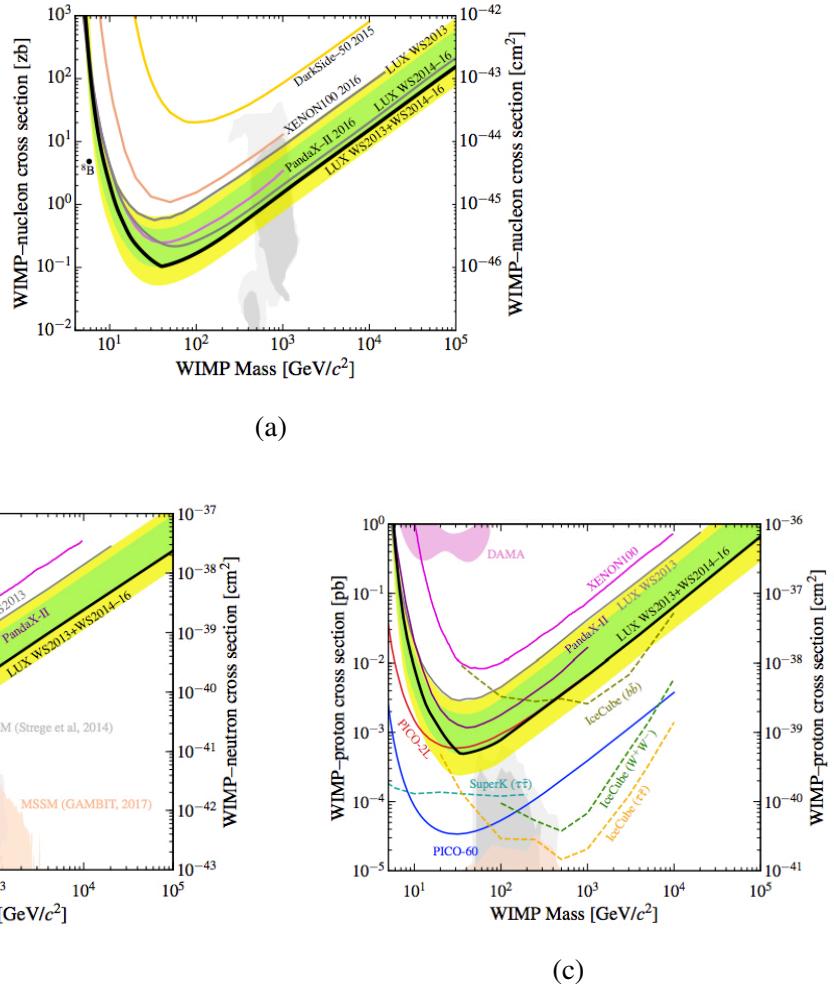


Figure 1.7: Limits on the SI single-nucleon (a), SD single neutron (b), and SD single proton (c) cross sections. These limits were taken from the LUX experiment's full exposure (332 days). The SI limit is roughly 5 orders of magnitude better than the SD neutron limit, which itself is about 2 orders of magnitude better than the SD proton limit. The solid black lines show the experimentally measured limits, and the green and yellow regions show the 1- and 2- σ expectations. Figures were taken from [5] and [56].

is the sum of \vec{v}_0 , the sun's peculiar velocity, \vec{v}_s , and the orbital velocity of the earth around the sun, $\vec{u}_E(t)$ [59, 71]:

$$\vec{v}_E(t) = \vec{v}_0 + \vec{v}_{sun} + \vec{u}_E(t). \quad (1.23)$$

The contribution to $\vec{v}_E(t)$ from the velocity of the sun with respect to the galactic center ($|\vec{v}_0 + \vec{v}_{sun}|$) is about 232 km/s, and $\vec{u}_E(t)$ acts to add a 6% annual modulation. This modulation would presumably introduce a detectable effect in the scattering rate of WIMPs. The DAMA/LIBRA NaI scintillation detector[20] has observed with 9.3σ confidence annual modulation in their 2-6 keV, single-scatter event rate. This result, however, is in significant tension with other experimental limits (see for instance figure 1.7c).

We can use this velocity distribution to write the scattering rate as a function incident velocity, v_i . This will give the total number of WIMP-nucleus scattering events per unit time per gram of material with atomic weight, A :

$$dR(v_i) = \frac{N_A}{A} n_\chi f(\vec{v}_i - \vec{v}_E) \sigma v_i d^3 \vec{v}_i, \quad (1.24)$$

with N_A being Avagadro's number and n_χ being the local number density of WIMPs.

The velocity of a WIMP in the lab frame is highly non-relativistic. This being the case, collisions between WIMPs and the target nuclei of earth-bound detectors can be well modeled by classical elastic scattering. The recoil energy, E_R , for elastic scattering of a non-relativistic WIMP of mass M_χ off of a nucleus of mass M_A is given by[71]:

$$E_R = \frac{E_i r}{2} [1 - \cos(\theta)], \quad (1.25)$$

where $E_i = \frac{1}{2} M_\chi v_i^2$ is the energy of the incident WIMP, θ is the recoil angle, and $r = 4M_\chi M_A / (M_\chi + M_A)^2$ is a kinematic factor.

For a WIMP with a given v_i , the nuclear recoil energy will be even distributed between

0 and $E_i r$. These uniform distributions can then be weighted by $dR(v_i)$ and then integrated over v_i to give the total differential scattering rate:

$$\frac{dR}{dE_r} = \int_{E_{min}}^{E_{max}} dR(v_i)/E_i r \quad (1.26)$$

For the limits of integration we could take into account the escape velocity of the galaxy, but setting $E_{max} = \infty$ yields a good approximation and makes evaluation of the integral simpler. Only WIMPs with incident energy equal to or greater than E_R/r will contribute to the scattering rate at E_R , so we will set $E_{min} = E_R/r$. Under this approximation, the normalization constant in equation 1.22 becomes $k = (\pi v_0^2)^{3/2}$. If we make the further assumption that $\vec{v}_E = 0$, we can write:

$$\begin{aligned} dR(v_i) &= \frac{R_0}{2\pi v_0^4} e^{-v_i^2/v_0^2} v_i (4\pi v_i^2 dv_i) \\ &= \frac{2R_0}{v_0^4} e^{-v_i^2/v_0^2} v_i^3 dv_i \end{aligned} \quad (1.27)$$

where,

$$R_0 = \frac{2N_A}{\sqrt{\pi}A} n_\chi \sigma_0 v_0, \quad (1.28)$$

for constant cross section. Equation 1.26 then becomes:

$$\frac{dR}{dE_r} = \frac{R_0}{E_0 r} \frac{2}{v_0^2} \int_{E_R/r}^{\infty} e^{-v_i^2/v_0^2} v_i dv_i. \quad (1.29)$$

If we make a change of variables to energy space, this integral becomes:

$$\frac{dR}{dE_r} = \frac{R_0}{E_0 r} \int_{E_R/r}^{\infty} e^{-E_i/E_0} dE_i, \quad (1.30)$$

which easily evaluates to:

$$\frac{dR}{dE_r} = \frac{R_0}{E_0 r} e^{-E_r/E_0 r} \quad (1.31)$$

Here we see that R_0 will give the total scattering rate.

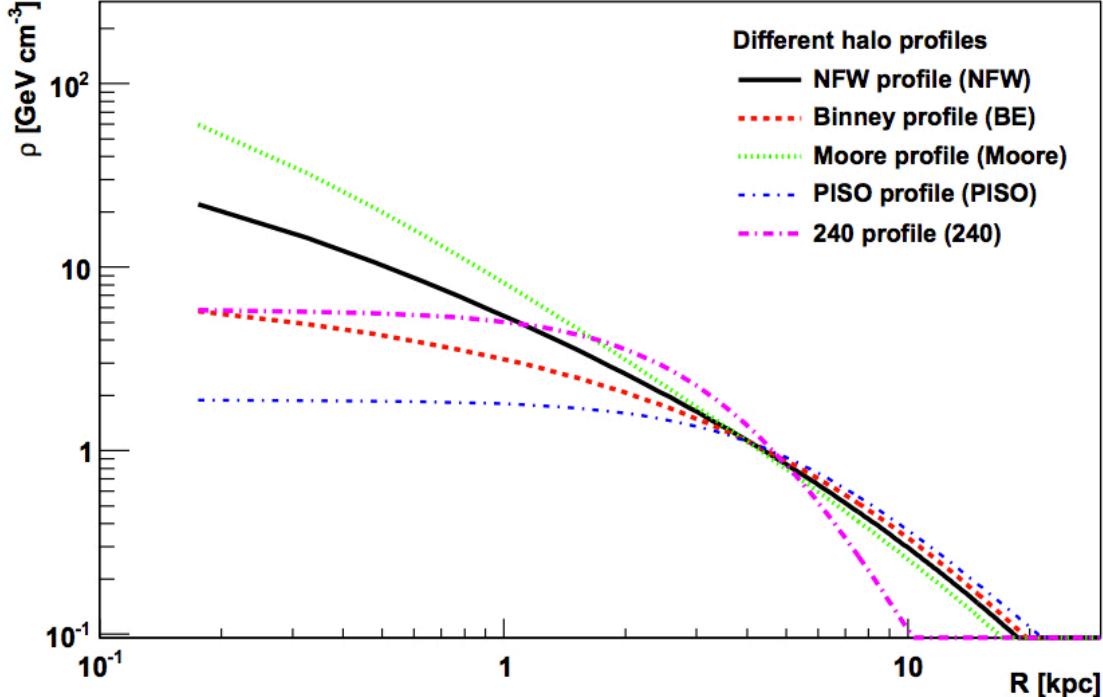


Figure 1.8: Various theoretical halo profiles. The sun is at about 8 kpc. The significant variance of ρ_χ for the different models limits the accuracy of scattering rate estimates for direct detection experiments. Figure from [78].

From measurements of the galactic rotation curve, the local dark matter density is expected to be approximately $0.2\text{-}0.4 \text{ GeV cm}^{-3}$. This value is highly dependent on theoretical profile model and could be as high as 0.7 GeV cm^{-3} given a nonuniform halo density[78]. Here we assume a middling value of 0.4 GeV cm^{-3} . If we take $M_\chi = 100 \text{ GeV}/c^2$, and $M_A = 122 \text{ GeV}/c^2$ (xenon atomic mass), we have $r = 0.99$ and $E_0 = 27 \text{ keV}$. In

this case the total scattering rate in counts· day⁻¹·kg⁻¹ will be:

$$R_0 = \frac{2}{\sqrt{\pi}} \frac{(1000 \text{ g/kg}) \times (6.022 \times 10^{23} \text{ atoms/mole})}{131 \text{ g/mole}} \frac{0.4 \text{ GeV/cc}}{100 \text{ GeV}/c^2} \sigma_0 (7.34 \times 10^{-4} c) \\ \approx \left(\frac{131}{A} \right) \left(\frac{\sigma_0}{1 \text{ pb}} \right) (0.4 \text{ counts/kg/day}). \quad (1.32)$$

So for a xenon detector and a WIMP-nucleus cross section of 1 picobarn, there would be about one event every 25 days per kilogram of detector material.

The effect of the finite galactic escape velocity, $V_{esc} = 540 \text{ km/s}$, can be approximated by introducing a cutoff to equation 1.31. Very nearly all of the WIMPs with velocity greater than V_{esc} should have left the halo, so maximum recoil energy will be $E_{max} = \frac{r}{2} M_\chi v_{esc}^2$. For xenon detectors:

$$E_{max} = \frac{1}{(1 + M_A/M_\chi)^2} (790 \text{ keV}). \quad (1.33)$$

Detectors which have energy thresholds greater than E_{max} will be completely insensitive to WIMPs of that mass. In addition to the hard cut off at $E_{esc}r$, the exponential nature of equation 1.31 means that detectors will be significantly less sensitive to WIMPs for $E_0r < E_{threshold}$. For xenon:

$$E_0r = \frac{1}{(1 + M_A/M_\chi)^2} (131 \text{ keV}). \quad (1.34)$$

This means that a xenon detector with a 20 keV threshold will begin to lose sensitivity for $M_\chi < 20 \text{ GeV}/c^2$, and will be completely insensitive to WIMPs with $M_\chi < 3 \text{ GeV}/c^2$. This places a large incentive for direct detection experiments to have a very low threshold.

In the derivation of equation 1.31, we assumed a constant scattering cross section. This, however, neglects the nuclear form factor, $F(q)$, which was introduced in equation 1.19. This form factor takes into account the nuclear wave-function, which becomes important

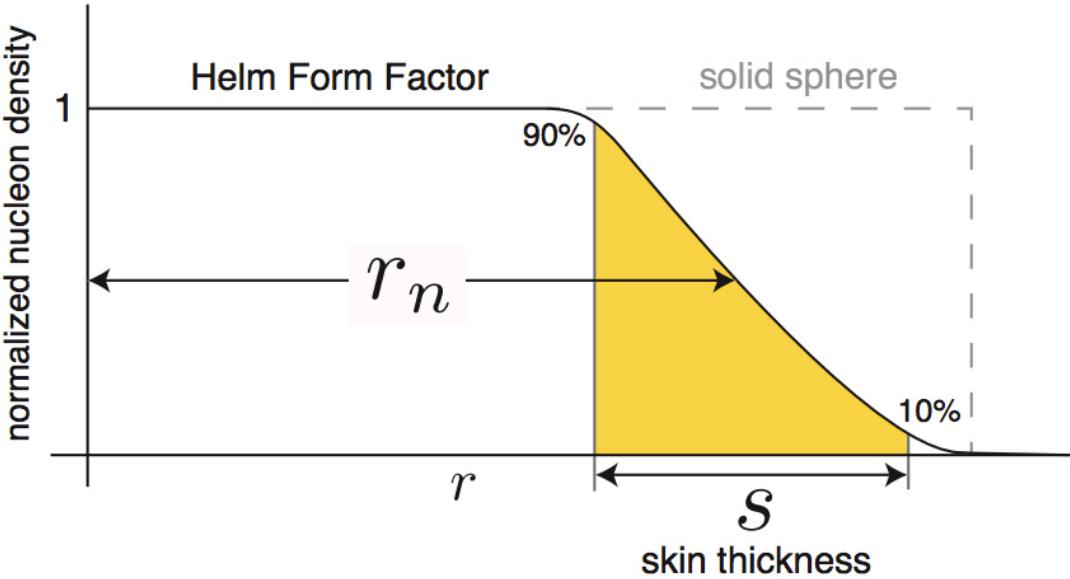


Figure 1.9: Helm approximation of the nucleon density. This approximation has the form of a solid sphere with a Gaussian falloff of thickness, S . Figure from [37].

at higher momentum transfers where coherent scattering begins to break down. Under the Born approximation and for spherically symmetric nucleon density, ρr , the form factor is:

$$F(q) = \frac{4\pi}{q} \int \rho(r) \sin(qr) r dr. \quad (1.35)$$

The most common approximation for the nucleon distribution the Helm approximation-a solid sphere which convolved with gaussian to create a smooth fall off at the edge[45]. Plugging this into equation 1.35 yields:

$$F(q) = \frac{3[\sin(qr_n) - qr_n \cos(qr_n)]}{(qr_n)^3} e^{-(qs)^2/2}, \quad (1.36)$$

where r_n is the nuclear radius and the skin width, s , is the width of the Gaussian fall off in the Helm approximation. The skin width is usually taken to be $s = 0.9$ fm[55], and the nuclear radius can be approximated $r_n \approx 1.14A^{1/3}$.

When the de Broglie wavelength, h/q , becomes comparable to the nuclear radius, r_n , coherent scattering will break down. This causes a drastic fall in the scattering rate. Xenon, for instance, will lose coherence at about 100 keV, while smaller elements will maintain the benefit of coherent scattering to significantly higher energies. This effect will compete against benefit from the A^2 dependence of $\sigma_{0,SI}$. Ultimately the low-momentum benefit of xenon as a target medium, together with self-shielding effects which will be described later, makes xenon the most popular and promising target material for direct detection experiments.

1.6 Thesis Outline

In this chapter, we discussed the evidence for particulate cold dark matter in general. We then discussed the motivation and proposed detection techniques for Weakly interacting massive particles (WIMPS). In the next chapter, we will continue to narrow our focus to liquid xenon time projection chambers as WIMP detectors. This will include a discussion of the microphysics behind energy deposits in liquid xenon, as well as the design, construction, and operation of the LUX and LZ dark matter detectors.

In chapter 3 we will discuss a technique for monitoring the purity of liquid xenon. We have improved on an existing technique using novel methods of optimization. We detail the empirical studies that went into this optimization, as well as the theoretical motivation behind them.

Chapter 4 will describe the LUX post-run04 calibration campaign. There are several internal sources novel to the LUX detector which were injected during this timeframe. We will catalog these sources, and present signal corrections derived from them. We will also describe a systematic pathology in the charge signals, as well as our attempt to account for it.

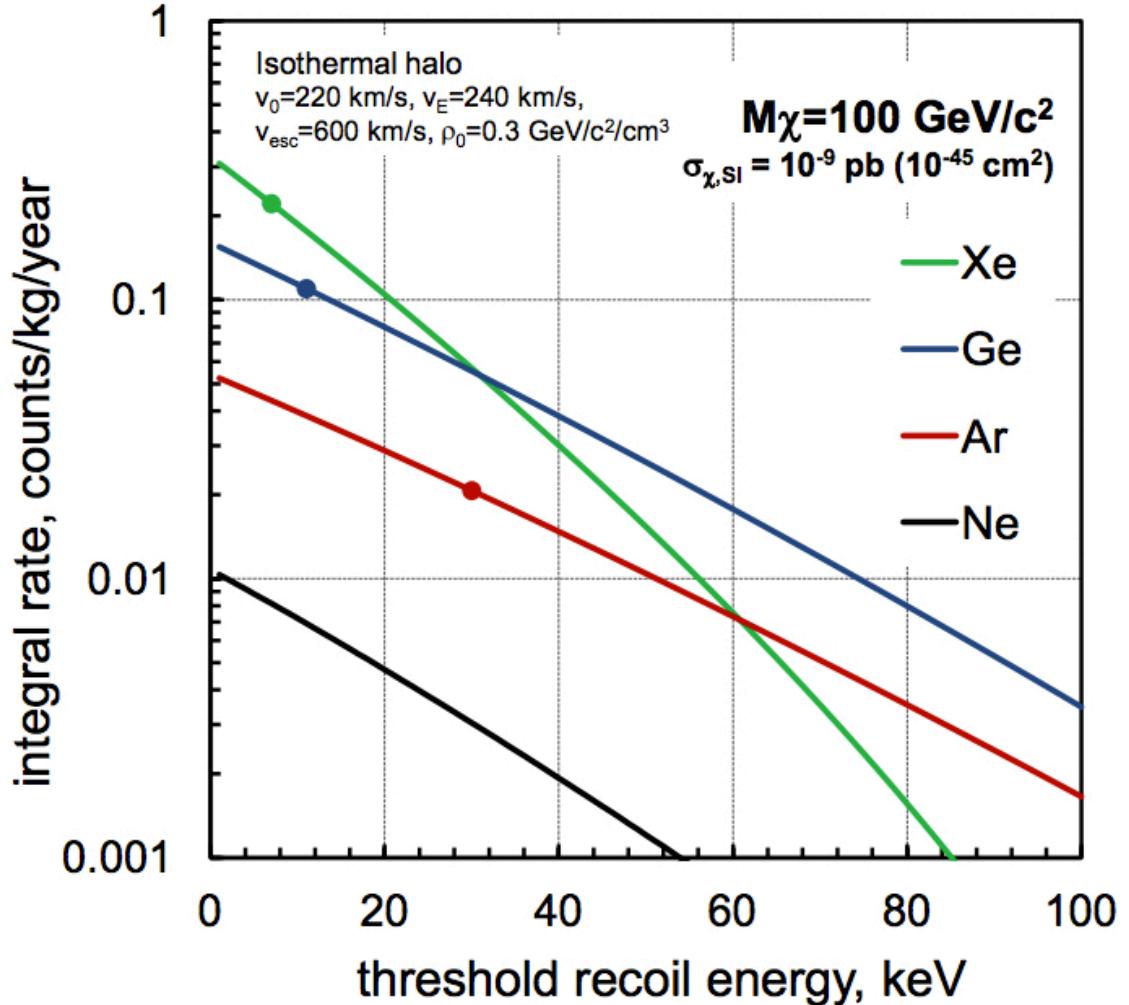


Figure 1.10: WIMP scattering rate as a function of energy taking into account the nuclear form factor. Xenon's large size is a double edge sword. At low energy, the A^2 dependence of $\sigma_{0,SI}$ wins out and xenon has a significant advantage over competing media. At large momentum transfers, however, decoherence dominates, forcing xenon to fall much more quickly than argon, neon, or germanium. Figure from [26].

Finally, chapter 5 will describe in detail the results from the novel ^{14}C injection that occurred during the post run04 injection campaign. We will derive charge and light yields, as well as recombination fluctuations from energies ranging from 5-140 keV. We will also present a comparison to the theoretical spectrum.

Chapter 2: The LUX and LZ experiments

Currently the most stringent limits on WIMP mass and cross section are set by the Large Underground Xenon (LUX) detector. The LUX-ZEPLIN (LZ) detector will be the successor to LUX and will have roughly 200 times greater sensitivity than LUX. LUX and LZ are two-phase xenon time-projection chambers (TPC's) designed to detect relic WIMPs in the local galactic halo scattering off of the target xenon nuclei.

If a WIMP interacts with one of the target atoms, it will deposit energy in the form of freed electrons, light, and heat. Two arrays of photo-multiplier tubes (PMT's) at the top and bottom of the detector detect the light emitted from this interaction as primary scintillation (S1). The electrons are drifted through an electric field to the top of the liquid where they are extracted and cause secondary scintillation light (S2) which is also detected by the PMT's. The x-y position of this event can be reconstructed mapping the relative signals from the S2 in the top PMT array. The depth of the event is given by the time separation between the S1 and S2. The relative size of the S1 and S2 will be different depending on whether the interaction was with the xenon nucleus or an orbital electron. A WIMP will interact coherently with the nucleus, so it is 132 times more likely to interact with a xenon nucleus than with an electron. Since most of the background events in LUX are from gammas and betas, which interact with the orbital electrons, the ratio of S2 to S1 can be used to efficiently discriminate between background and signal.

LUX is currently located at the Sanford Underground Research Facility in Lead South Dakota. It is 4850 feet underground (4300 m w.e.). The detector itself is immersed in

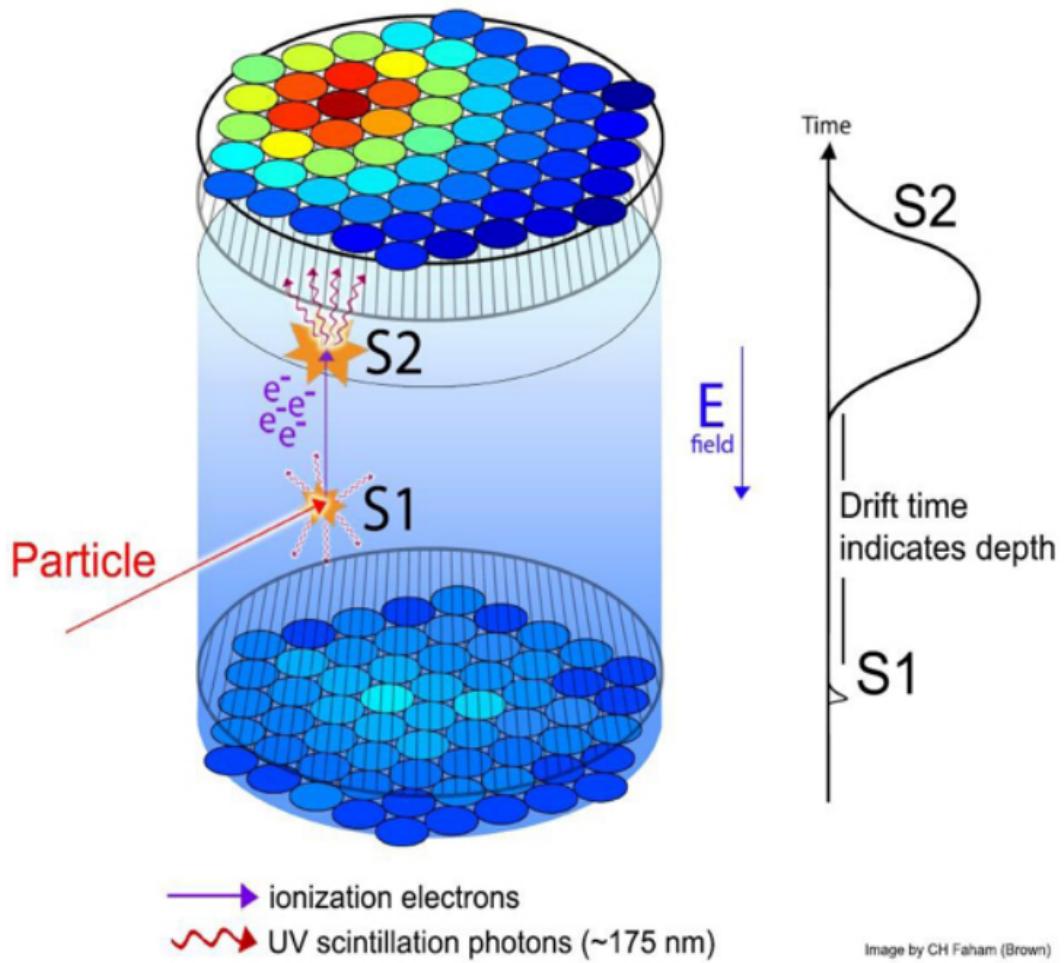


Figure 2.1: Schematic drawing of an event in the LUX detector.[6]

a large water tank to shield it from neutrons and gammas. LUX contains about 370 kg of xenon, and uses a fiducial volume containing about 118 kg as its WIMP target. The remaining xenon acts as a shield from external gammas and betas.

2.1 The libNEST Model of the LUX Detector

2.1.1 Detector Resolution for Charge and Light Signals

The S1 detector resolution, $\sigma_{\gamma,det}$ is composed of three parts; the binomial variance due to the finite light collection efficiency, ε_γ :

$$\sigma_{S1,col}^2 = N_\gamma G1(1 - G1), \quad (2.1)$$

an additional variance due to a nonzero probability, P_{DPE} , that the PMT will experience double-photoemission[36]:

$$\sigma_{S1,DPE}^2 = G1 \cdot N_\gamma P_{DPE}(1 - P_{DPE}), \quad (2.2)$$

and the variance due to finite PMT resolution, σ_{PMT} :

$$\sigma_{S1,PMT}^2 = N_\gamma G1 \sigma_{PMT}^2 \quad (2.3)$$

For LUX we have $G1 \approx 0.095$, $P_{DPE} \approx 0.2$, and $\sigma_{PMT} \approx 0.50$. Put together, this gives:

$$\begin{aligned} \sigma_{S1}^2 &= N_\gamma G1(1 - G1 + P_{DPE}(1 - P_{DPE}) + \sigma_{PMT}^2) \\ &\approx 0.125N_\gamma \text{ (phd}^2\text{)}, \end{aligned} \quad (2.4)$$

or:

$$\sigma_{\gamma,det} = \sigma_{S1}/G1 = 3.7 \sqrt{N_{gamma}} \text{ (phd)} \quad (2.5)$$

2.2 Electric Field Model

[9]

2.3 Efficiency Corrections

In run 4, the position-dependent efficiency corrections for the LUX S1 and S2 signals were obtained from a combination of tritium and ^{83m}Kr calibration data using a procedure referred to as KrypCal[50].

2.4 Electron Trains in LUX Run04

Chapter 3: Building, Optimizing, and Maintaining a Xenon Cold-Trap Sampling System

3.1 Technical Overview

A cold trap sampling system is designed to flow a sample of xenon with trace amounts of impurities through a section of liquid nitrogen cooled plumbing, to a mass-spectrometer for purity analysis. This document will deal particularly with krypton, but the method described also works for most simple impurities such as helium, argon, nitrogen, oxygen, methane, etc.. Less volatile impurities such as water and large hydrocarbons tend to freeze along with the xenon, so are not detected.

The operating principle is similar the that of freeze distillation. The bulk xenon is frozen to the cold plumbing leaving only the xenon ice vapor pressure at the output of the cold-trap. The flow of krypton is left largely unaffected. The resulting mixture which exits the cold-trap can be up to 10^9 times enriched in krypton. A cold-trap used in conjunction with a residual gas analyzer (RGA) whose sensitivity is about one part in 10^6 , is able to measure concentrations of krypton in a xenon sample down to the order of one part in 10^{15} .

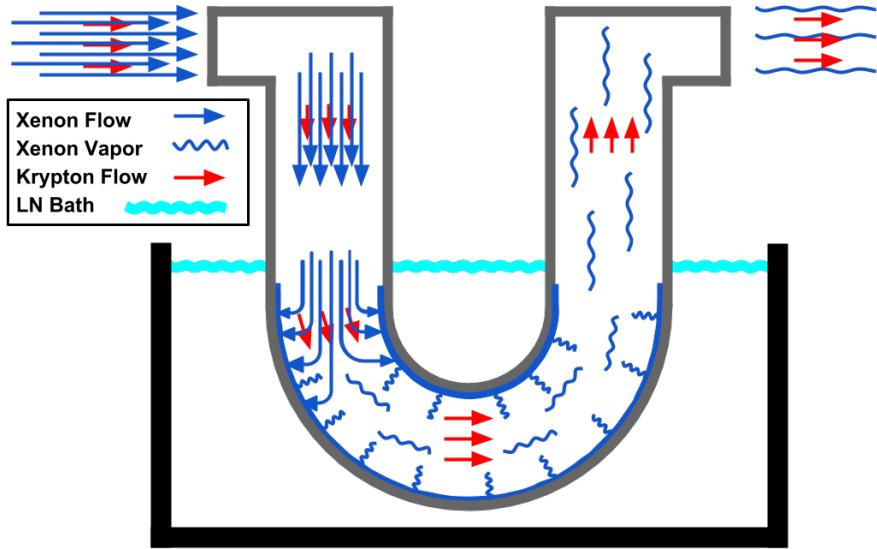


Figure 3.1: Cartoon version of what happens during a cold trap analysis.

3.1.1 System Construction

A cold trap sampling system should be laid out as described by figure 3.26. There will likely be additional transfer lines needed for collecting samples, recovering xenon, etc., but figure 3.26 fully describes the plumbing necessary to analyze a sample of xenon.

The system should have 100% metal-seals such as VCR or CF. Elastomer internals have the potential to become contaminated with krypton and destroy the sensitivity of the system and so should be limited. Traditionally, hardware used for this type of system is as follows:

- The plumbing should be entirely composed of UHP stainless steel.
- The sample bottle, SB, is a 1 gallon Swagelok DOT compliant sample cylinder.
- The valves, V1 through V7 are some type of high purity shutoff valve. For automated systems, the Swagelok DF series diaphragm valves with pneumatic actuators are

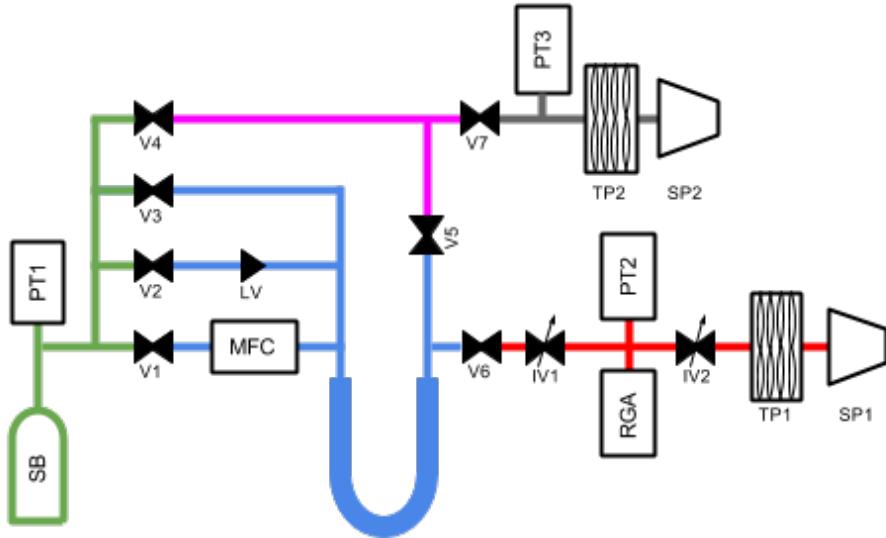


Figure 3.2: Plumbing diagram of a general purpose cold-trap sampling system. The green section is referred to as the sample volume, the blue section is the cold trap volume, and the red section is the RGA volume. These are the sections used during analysis of a xenon sample. The pink section is the bypass line which serves two purposes. It is used to relieve pressure in the cold trap while the system is warming and acts as the access line to the pump-out turbo pump, TP2.

used. When possible, it is better to use the Swagelok B series bellows valves with the spherical copper stem tip option, since the DF series has a polymer seat, however these are more difficult to automate.

- The sample pressure transducer is a capacitance manometer such as the MKS Baratron with a full scale of at least 3,000 Torr.
- The leak valve, LV, is a metering valve.
- The mass flow controller, MFC, should be metal sealed, and have a full range of about 10 SLM. The Celerity UNIT1660 is a good example. Although no longer in production, they are fairly easy to find used.

- The cold trap itself is some UHP stainless steel plumbing that is bent or welded into a shape that allows it to be submerged in a liquid nitrogen bath. Currently, the optimal cold-trap geometry is a 1/2 inch “stocking” trap, as described in section 3.3.1.
- Traditionally IV1 has been a Swagelok B series bellows valves with the spherical copper stem tip option, however it’s likely that the regulating stem tip would be better suited to the task.
- PT2 and PT3 are any cold cathode or inverted magnetron gauge that have an operating range of at least 10^{-8} to 10^{-4} Torr.
- The residual gas analyzer, RGA, is the SRS RGA200.
- IV2 needs to have a significantly lower impedance than IV1, so some type of 2.75” CF sealed all-metal vacuum valve should be used. A Varian UHV right angle valve, part No. 9515027 has been used in the past with good results.
- TP1 and TP2 are turbo-molecular pumps with pumping speed of at least 70 liters per second. The Varian V70, V81, and V84 have all been used with good results.
- SP1 and SP2 are the backing pumps for TP1 and TP2. They should be at least equivalent to the Agilent model SH110 scroll pump.

3.1.2 Operational Outline

The exact steps required for a particular analysis can be quite complex, and some detailed example procedures can be found in appendix ???. A general outline of the operation of a cold trap sampling system is as follows:

1. A xenon sample is collected and stored in the sample volume until the beginning of analysis.

2. The system begins with all the valves closed.
3. The cold trap is immersed in a liquid nitrogen bath, and base layer of xenon ice is formed.
4. Baseline pressures are measured by the RGA by opening V6, exposing the RGA volume the the xenon ice vapor pressure present in the cold trap volume. Usually these baselines are established over a period of ten or more minutes.
5. Leaving V6 open, V1 or V2 is opened, allowing the xenon sample to freeze into the cold trap at a controlled flow rate. This will usually takes several minutes.

As described in figure 3.1, the xenon pressure at the RGA will remain constant during this step, but there will be a flow of krypton at the output of the cold-trap which will cause a rise in the krypton partial pressure in the RGA volume. It is this partial pressure pressure rise that will be analyzed to give the concentration of krypton in the xenon sample.

6. After the sample volume has been exhausted, V1(2) will be closed, and the krypton partial pressure is allowed fall back to its prior value.

At this point, the purity analysis of the xenon sample has been completed, but the system is not in a safe state. Only a microscopic amount of xenon has been pumped out through TP1, so the full mass of the xenon sample is frozen in the cold trap. If this is allowed to vaporize without proper precautions, the RGA and TP1 could be damaged by over-pressure. It is therefore extremely important to isolate the RGA volume from the cold-trap volume before allowing the cold-trap to rise above liquid-nitrogen.

7. Close V6.

If the sample mass was large enough, there could be enough xenon ice in the cold trap to damage the system instrumentation or even cause the plumbing system to rupture once it

warms to the gas phase. This is why it is important to have rupture disks installed on the cold trap. To avoid damage to the system, the cold trap volume should be vented to the sample volume. Valve V3 provides a path from the input of the cold trap to the sample volume without the added impedance of the MFC or LV.

8. Open V3.

This is where the bypass line comes in. With a cold-trap made from 1/2" plumbing, it is likely that an ice blockage will form once the xenon flow has stopped. This ice blockage could cause a dangerous pressure differential between the input and output of the trap. By opening the bypass line, the output of the cold trap has a second path to the sample volume.

9. Open V4 and V5.

The system is now in a safe state and the cold trap can be allowed to warm back to room temperature. The remaining xenon can then be recovered or discarded as desired, after which the system should be pumped to vacuum before collecting the next sample. It is important to note that this pump-out should be done using TP2, since the RGA volume should be kept at vacuum except for maintenance. The bypass line, as configured, allows the cold-trap volume and sample volume to be pumped out independent of one another.

3.2 Idealized Cold Trap Response

In order to optimize the sensitivity of the cold-trap system, it is good to have an understanding of the basics of vacuum physics. A vacuum system can be analogized to an electrical circuit, with pressure taking the place of voltage, flow rate (Q) taking the place of current, and impedance (Z) taking the place of resistance. This analogy gives us with the equation:

$$\Delta P = Q \cdot Z \quad (3.1)$$

An important note here: in this document we use the generic P to denote a pressure at any specific point in the system, but reserve PP_s to represent the partial pressure of some species, s , as measured by the RGA. For instance, PP_{Kr} will refer to partial pressure of ^{84}Kr as it is measured by the RGA, whereas $P_{Kr,CT}$ will be used to represent the krypton pressure present in the cold trap.

Returning to the vacuum equations, it is now useful to define a new quantity, S , which is called the “volumetric flow rate” or “pumping speed”. S is defined:

$$S \equiv Av = \frac{dV}{dt} = Q/P, \quad (3.2)$$

where A is the cross-sectional area of the pipe, and v is the flow velocity, and dV is the volume of gas which passes a point in the system in time dt . An effective pumping speed can be calculated for any point in the vacuum system through the equation:

$$1/S_{eff} = 1/S_p + Z_{total}, \quad (3.3)$$

where S_p is the speed of the pump which is acting on the system, and Z_{total} is the total impedance between the pump and the specified point in the system. We can then calculate the steady-state pressure at any point in the system[58]:

$$P = Q/S_{eff}. \quad (3.4)$$

3.2.1 Vacuum Impedances

The calculation of system impedances depends on which flow regime a gas resides. The flow regime is determined by whether a given gas molecule interacts primarily with other molecules, or with the walls of the vacuum chamber. The flow regime can be characterized

by the Knudsen number, $K \equiv \lambda/d$, where λ is the mean free path, and d is the inner diameter of the vacuum chamber. For $K \gg 1$, a gas molecule is very likely to encounter the wall of the system before encountering another gas molecule; this is the molecular flow regime. When $K \ll 1$, the system is in the viscous flow regime where a gas molecule will be interacting predominantly with other gas molecules. If K is $O(1)$, the system is in what is referred to as the intermediate regime.[58]

In the molecular flow regime the impedance of a system element will depend on the geometry of the element, and on the molecular weight and temperature of the gas in question, but it will not depend on the pressure of that gas. For instance, the impedance of an aperture with area A will be given by:[58]

$$Z = \sqrt{\frac{2\pi M}{8kTA^2}}. \quad (3.5)$$

In the intermediate regime, the impedance picks up a complicated pressure dependence that can not be exactly calculated. Xenon gas inside the cold trap is at 1.8×10^{-3} Torr and 77 Kelvin.[39] In a 0.5" diameter cold trap the xenon has a Knudsen number of 0.6. This puts this section of plumbing in the intermediate gas flow regime rather than the molecular flow regime, and limits the accuracy of any results calculated using the molecular flow approximation. The role of vacuum equations in this document is to provide qualitative predictions on how the krypton pressure at the RGA will behave in response to changes in system parameters. The exact response of the system is always characterized empirically, as will be described in section ???. For this purpose, the molecular flow approximation will suffice to motivate and direct our empirical investigations.[58]

The particular impedances of interest here are impedance between the cold-trap and the RGA (Z_1) and the impedance between the RGA and TP1 (Z_2). IV1 and IV2 are in place so that Z_1 and Z_2 can be fine tuned to an optimal arrangement. This optimization will be

described further in section ??, but first there is a hard constraint that must be placed on the relative values of Z_1 and Z_2 .

The RGA has a maximum operating pressure of 1×10^{-6} Torr, although we have found that operating at about 1×10^{-5} Torr is possible with minimal degradation of the CDEM. When analyzing xenon samples with a concentration of about one part per million or less, the xenon partial pressure, PP_{Xe} , will dominate the absolute pressure at the RGA. PP_{Xe} is sourced by the vapor of the xenon ice in the cold trap, which is $P_{ICE} = 1.8 \times 10^{-3}$ Torr, and so needs to be reduced by a factor of about 100 or more between the cold-trap and the RGA[39].

There are several compounding factors that come into play when deciding exactly what PP_{Xe} should be. These will be discussed in later sections, so we will take it as given here that the sensitivity is optimized between $PP_{Xe} = 5 \times 10^{-6}$ Torr, and $PP_{Xe} = 2 \times 10^{-5}$ Torr, and is largely unaffected by deviations within this range. For the sake of simplicity, we will usually demand that PP_{Xe} to be the default pressure that the system plumbing gives when IV1 and IV2 are maximized. For the system described above, the this pressure will be about 1×10^{-5} Torr.

To avoid saturation and mass-dependent effects of the RGA, we often use the doubly-ionized peak of the xenon-124 isotope as our measure PP_{Xe} . This peak appears at 62 amu, and so will be referred to as PP_{Xe62} . When the system is properly adjusted, PP_{Xe62} should be around 1,000 pTorr, or 1×10^{-9} Torr.

Returning to the vacuum equations we will see that although we have artificially defined PP_{Xe} , Z_1 and Z_2 are not fully determined by this choice. By using equations 3.1 and 3.4, and the requirement that $PP_{Xe} = 1 \times 10^{-5}$ Torr, we place a constraint on the impedances:

$$Q_{Xe,RGA} = PP_{Xe} S_{RGA} = \frac{P_{ICE} - PP_{Xe}}{Z_1} \approx \frac{P_{ICE}}{Z_1}, \quad (3.6)$$

where $1/S_{RGA} = 1/S_{TP1} + Z_2$. This gives,

$$S_{RGA} \cdot Z_1 = \frac{P_{ICE}}{PP_{Xe}} = 180. \quad (3.7)$$

S_{RGA} is usually dominated by Z_2 . Depending on the model of pump used, the speed of the turbo pump for xenon is around 50 liters per second. The impedance of cylindrical plumbing with a diameter of 1.5 inches is about $\frac{1}{320}s/L$ per centimeter of plumbing.[58] In a typical system there will be the equivalent of about 5 feet of plumbing between the RGA and TP1, so the nominal value of Z_2 will be roughly 0.48 seconds per liters for xenon, indicating a maximum S_{RGA} of 2.1 liters per second.[58] This means the fully-open value of Z_1 should be about 85 seconds per liter for xenon. The exact numerical value of S_{RGA} and Z_1 are largely unimportant, and when optimizing the system impedances as described in section ??, we will work in units relative to the fully open state, rather than liters per second.

3.2.2 Setting System Impedance

The sensitivity of a cold trap sampling system depends upon Z_1 and S_{RGA} . We can adjust IV1 and IV2 to change Z_1 and S_{RGA} , but wish to do so in a reproducible way. To this end, we look to the left hand side of equation 3.7 and see that PP_{Xe} is proportional to $1/S_{RGA}Z_1$. If we adjust IV1 while holding IV2 constant, we can use PP_{Xe} as a measurement of Z_1 relative to its fully open state. Once Z_1 has been adjusted to a desired set-point, we can use IV2 to adjust S_{RGA} until PP_{Xe} is restored to its pre-adjustment value.

For example, take the RGA trace shown in figure 3.3. In this case, $PP_{Xe62} = 710 \pm 30$ pTorr when IV1 and IV2 are both fully open (region *I* in the figure). This state will be referred to as the 1x impedance state. In region *II* of figure 3.3 IV1 is partially closed until Z_1 has increased by a factor of 19 ± 2 . This has the effect of decreasing PP_{Xe62} from

710 ± 30 pTorr in region *I* to 38 ± 5 pTorr in region *III*. In Region *IV*, S_{RGA} is incrementally reduced by adjusting IV2 until PP_{Xe62} returns to 710 ± 40 pTorr. This final state (region *V*) will be referred to as the 19x impedance state.

Equation 3.5 shows that Z_1 will have a dependence on the molecular mass of the gas in question. The \sqrt{M} dependence means that the impedance for ^{84}Kr ($Z_{1,Kr}$) will be about 18% lower than the impedance for ^{124}Xe . This is another reason to work in units of relative impedance rather than absolute impedance. A factor of 19 increase in impedance to xenon will mean that the impedance for krypton will also have increased by a factor of 19.

3.2.3 Generalized Cold Trap System Response

The operating principle of cold-trap sampling is that while the xenon gets frozen into the cold-trap, the trace gasses, such as krypton pass through. Another way to put this is that at the output of the cold trap the xenon is frozen to a constant pressure, while krypton mass flow is conserved. In practice, the conservation is not perfect, so we add a throughput constant, $\alpha \equiv Q_{Kr,RGA}/Q_{Kr,CT}$, where $Q_{Kr,CT}$ is the flow rate into the cold trap, and $Q_{Kr,RGA}$ is the equilibrium flow rate of krypton out of the trap, and the flow rate of xenon into the cold-trap ($Q_{Xe,CT}$) is constant. $Q_{Kr,CT}$ is equal to $Q_{Xe,CT}$ times the concentration of krypton in the xenon sample, Φ_{Kr} . These relations put together, give us the following equation:

$$Q_{Kr,RGA} = \alpha Q_{Xe,CT} \Phi_{Kr}. \quad (3.8)$$

Plugging this into the vacuum equations, we can find the relationship between the parameter of interest, Φ_{Kr} , and the measurable quantities, Q_{Xe_0} and $PP_{Kr,eq}$:

$$PP_{Kr,eq} = \frac{\alpha}{S_{RGA}} Q_{Xe,CT} \Phi_{Kr}. \quad (3.9)$$

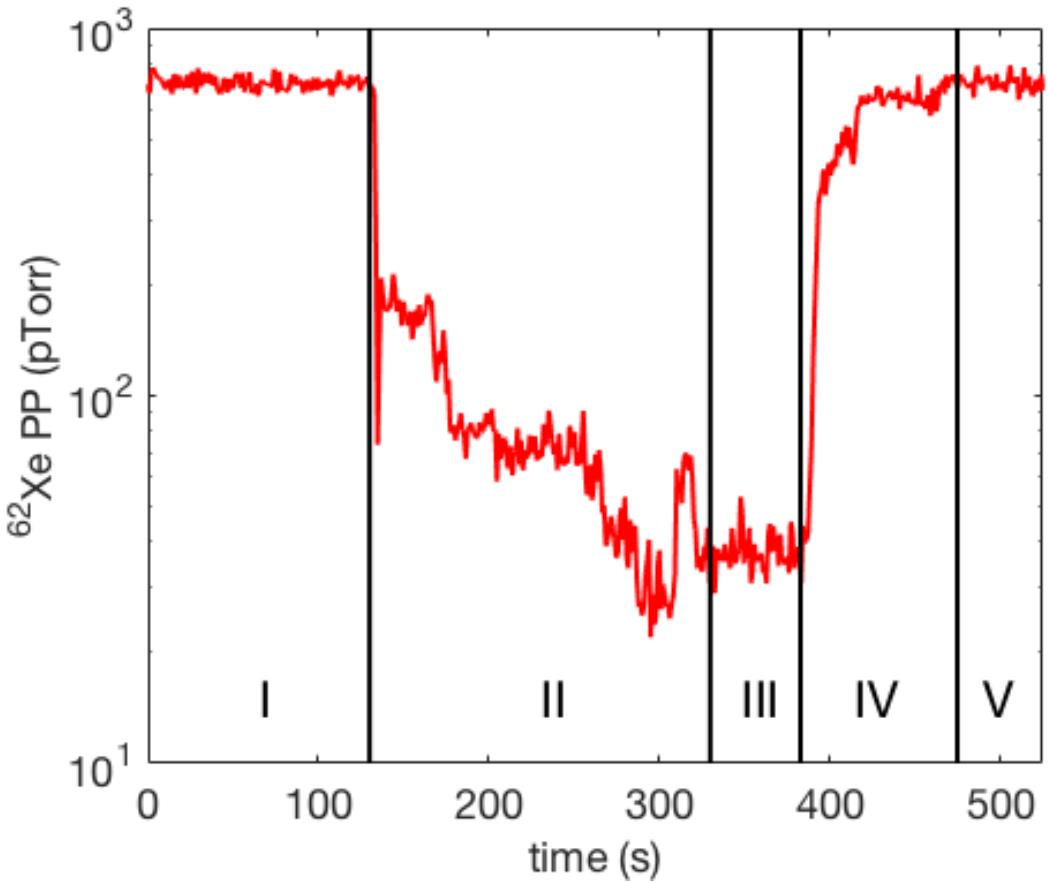


Figure 3.3: Adjustment of impedance to 19x state. Region *I* shows the fully-open, 1x impedance state of the system. In region *II*, Z_1 is manually reduced using IV1, until region *III*, where PP_{Xe62} has dropped to 1/19th of its value in the 1x impedance state. In region *IV*, PP_{Xe62} is carefully increased back to its initial value by slowing down the effective pumping speed, S_{RGA} . In region *V*, PP_{Xe62} has returned to its initial value, and the system is in the 19x impedance state.

This relation shows the proportionality between partial pressure, and flow-rate times concentration that was found experimentally in [54] and [31]. By imposing the constraint from equation 3.7 we can see how altering the system impedance is expected to affect $PP_{Kr,eq}$, the equilibrium pressure of krypton at the RGA:

$$PP_{Kr,eq} = \frac{\alpha}{180} Z_1 Q_{Xe,CT} \Phi_{Kr}. \quad (3.10)$$

From the vacuum equations, we can also find the expected response of the system to an impulse of krypton. To do so, we would like to make the assumption that the RGA volume and the cold trap volume have a vanishingly small internal impedance, which means that the pressure at the input is equal to the pressure at the output. This is reasonable for the RGA volume which is constructed of 1.5 inch plumbing. However, we find that the bends in the cold trap plumbing cause this approximation to break down in when the xenon ice extends past the first leg of the trap. The effects of this breakdown will be discussed in a later section, but for now we will remain in the limit of small xenon flow rate and small xenon sample size where the approximation does provide largely valid predictions.

In a volume with no internal impedance, the amount of krypton contained by that volume is defined as $P_{Kr}V$. If the volume is being evacuated at a constant volumetric rate, S , while at the same time being sourced by some time-dependent flow rate, $Q(t)$ the amount of krypton will change according to the equation:

$$V \frac{dP_{Kr}}{dt} = Q(t) - SP_{Kr}. \quad (3.11)$$

The response of $P_{Kr}(t)$ to an impulse of flow, $Q(t) = P_0 V \delta(t)$ is then:

$$P_{Kr}(t > 0) = P_0 e^{-t/\tau}, \quad (3.12)$$

where $\tau = V/S$. The time dependent $P_{Kr}(t)$ can then be found by convolving $Q(t)$ with this impulse response.

Applying this impulse response to the RGA volume (V_{RGA}) and cold trap volume (V_{CT}), we can find an expected time dependence of the krypton RGA pressure, $PP_{Kr}(t)$. The flow rate into the RGA volume is equal to the flow rate out of the cold trap volume, so it is given

by:

$$Q_{Kr,RGA}(t) = \frac{P_{Kr,CT}(t)}{Z_1 + 1/S_{RGA}} \approx P_{Kr,CT}(t)/Z_1, \quad (3.13)$$

where $P_{Kr,CT}(t)$ is the time-dependent pressure of krypton in the cold trap volume. So to calculate the expected $PP_{Kr}(t)$, we must first calculate $P_{Kr,CT}(t)$. This can be done by convolving the known flow of krypton into the trap, $Q_{Kr,CT} = \Phi Q_{Xe,CT}(t)$, with the impulse response of the cold trap volume. We can then convolve the resulting $Q_{Kr,RGA}(t)$ with the response of the RGA volume to predict the overall response of the system to the input flow rate.

The response time for the cold trap volume will be given by:

$$\tau_{CT} = V_{CT} \frac{1}{Z_1 + 1/S_{RGA}} \approx V_{CT} Z_1, \quad (3.14)$$

and the response time for the RGA volume will be given by:

$$\tau_{RGA} = V_{RGA}/S_{RGA}. \quad (3.15)$$

The condition $Z_1 S_{RGA} = 180$ from equation 3.7, combined with the fact that in a typical system, $V_{RGA} \approx V_{CT}$, means that the RGA volume is expected to respond much more quickly than the cold trap volume. Therefore the overall response of the system will be dominated by the response of the cold trap, and the shape of PP_{Kr} will be well approximated by the shape of $P_{Kr,CT}$.

In this document we use flow rate profiles for xenon of the form:

$$Q_{Xe,CT}(t) = \begin{cases} Q_0 & \text{for } t \leq T \\ 0 & \text{otherwise} \end{cases} \quad (3.16)$$

If $Q_{Xe,CT}(t)$ is given by equation 3.16, the instantaneous krypton pressure in the cold trap will be given by:

$$\frac{P_{Kr,CT}(t)}{\Phi Q_0 Z_1} = \begin{cases} 0 & \text{for } t < 0 \\ 1 - e^{-\frac{t}{\tau_{CT}}} & \text{for } 0 \leq t \leq T \\ (1 - e^{-\frac{T}{\tau_{CT}}})e^{-\frac{t-T}{\tau_{CT}}} & \text{for } t > T \end{cases} \quad (3.17)$$

Applying the response of the RGA volume gives the result:

$$\frac{PP_{Kr}(t)}{\Phi Q_0 / S_{RGA}} = \begin{cases} 0 & \text{for } t < 0 \\ 1 - e^{-\frac{t}{\tau_{RGA}}} - \frac{e^{-\frac{t}{\tau_{CT}}} - e^{-\frac{t}{\tau_{RGA}}}}{1 - \tau_{RGA}/\tau_{CT}} & \text{for } 0 \leq t \leq T \\ e^{-\frac{t-T}{\tau_{RGA}}} (1 - e^{-\frac{T}{\tau_{RGA}}} - \frac{e^{-\frac{T}{\tau_{CT}}} - e^{-\frac{T}{\tau_{RGA}}}}{1 - \tau_{RGA}/\tau_{CT}}) \dots \\ + \frac{e^{\frac{T}{\tau_{CT}}} - 1}{1 - \tau_{RGA}/\tau_{CT}} (e^{-\frac{t}{\tau_{CT}}} - e^{-\frac{t}{\tau_{RGA}} + T(1/\tau_{RGA} - 1/\tau_{CT})}) & \text{for } t > T \end{cases} \quad (3.18)$$

When $\tau_{RGA} \ll \tau_{CT}$, the right side of equation 3.18 reduces to the right side of equation 3.17. Combining this with the constraint from equation 3.7 yields:

$$PP_{Kr}(t) = \frac{Z_1 Q_0}{180} \Phi \begin{cases} 0 & \text{for } t < 0 \\ 1 - e^{-\frac{t}{\tau_{CT}}} & \text{for } 0 \leq t \leq T \\ (1 - e^{-\frac{T}{\tau_{CT}}})e^{-\frac{t-T}{\tau_{CT}}} & \text{for } t > T \end{cases} \quad (3.19)$$

Equation 3.19 does a good job in predicting the shape of PP_{Kr} when Q_0 and Z_1 are small as seen in figure 3.4. A fit to equation 3.19 produces a best fit time constant of 12.2 seconds. We measure the volumes spaces in our system by volume sharing with a known volume. The volume of the cold trap used in this trace was 183.8 cc, which would point to $Z_1 = 66.7$ seconds per liter and $S_{RGA} = 2.70$ liters per second.

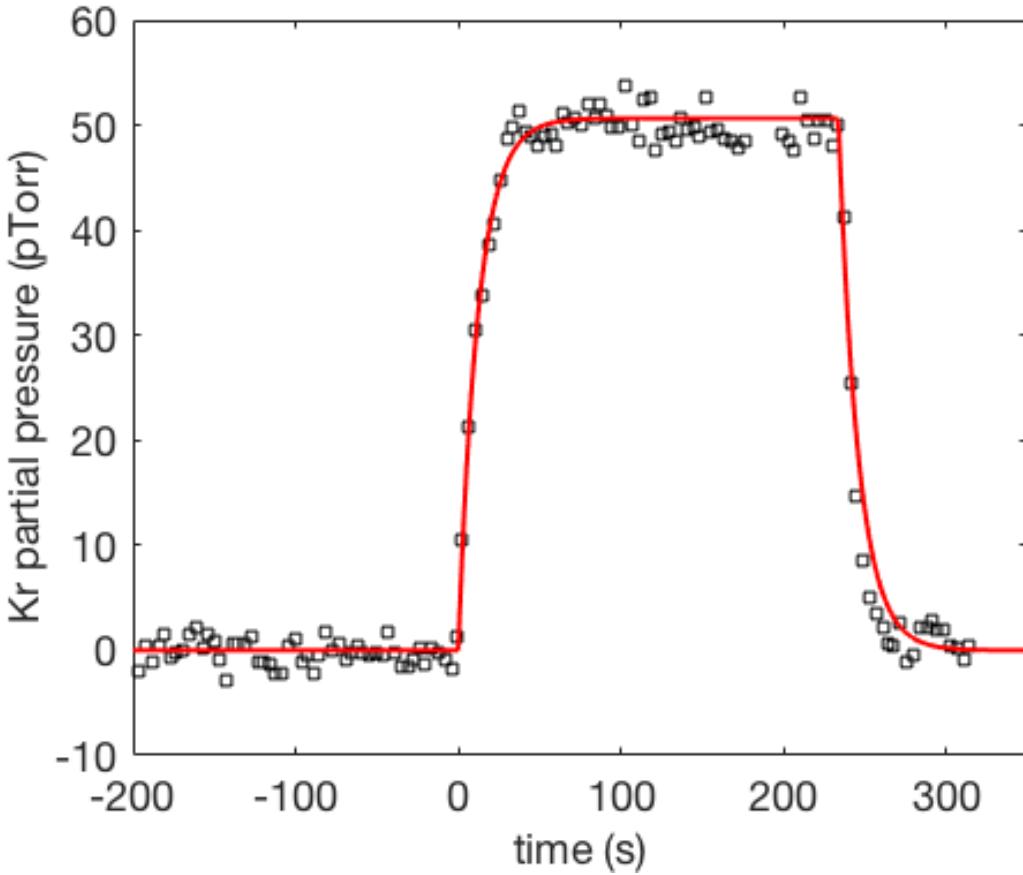


Figure 3.4: RGA trace with nominal impedance settings. Corrected for RGA gain, the equilibrium pressure of this trace is 50.8 ± 0.4 pTorr. Φ was known to be 750 ± 75 parts per trillion (ppt) in liters of krypton per liter of xenon. The xenon flow rate used was 0.36 standard liters per minute (SLM).

3.3 Actual Behavior of a Cold Trap System

Equation 3.19 will prove itself powerful in characterizing $PP_{Kr}(t)$, as well as in providing motivation for the direction of our attempts at optimizing the cold trap system for the measurement of trace krypton contamination. It is, however an idealized equation that relies on some tenuous assumptions.

The vacuum approximation is not perfect, and there are large deviations from the molecular flow model presented in the previous section. We postulate that these deviations arise

from interactions between the flow of krypton and the formation of the xenon ice. The input of the trap has viscous xenon flow where the krypton is interacting primarily gaseous xenon atoms, while at the output of the trap, the xenon is closer to the molecular flow regime where the krypton atoms will be interacting more often with the stainless steel plumbing. More importantly, there is a transition region where the xenon is actively being frozen. This rapid phase transition of the xenon has complicated effects on the flow of krypton through the trap which result in krypton getting trapped inside the ice.

This trapped krypton is the physical basis for the throughput parameter, α , presented in section 3.2.3. We consider two possible mechanisms for this entrapment; diffusion and entrainment. We take diffusion to be the passive absorption of krypton by already-formed xenon ice. This process will be governed by Fick’s laws, and so will be proportional to the krypton pressure at the surface of the ice, as well as the surface area of the ice present. We use the term entrainment somewhat loosely as a catch-all term for any effect that causes krypton to be encased in newly formed xenon ice as it is frozen. The major observable distinction between these two mechanisms is that entrainment will only occur when the xenon is actively being flowed into the trap, while diffusion can occur even over static ice. In this section we will present marginal evidence for both of these mechanisms and will characterize how the entrapment of krypton depends on xenon flow rate, system impedance, and the geometry of the cold trap.

3.3.1 Cold Trap Geometry

Before we analyze the performance of a cold trap sampling system, we must first select a geometry of cold trap to characterize. Historically we have used a 1.5 inch “U trap” (#6 in figure 3.5), but we have found that other geometries may serve us better. In general, we are looking for a trap that has a large capacity for xenon and a high krypton throughput.

We started by making variations of the our then-standard 1.5 inch U trap. We made a two additional U traps; one using 3/8 inch diameter plumbing and one using 0.5 inch plumbing. We measure the throughput parameter, α , using the “left-over” method, which will be described in a later section. Our flow rate for these tests was controlled using a variable leak valve, through which a 500cc sample bottle was being exhausted. This does not give produce a constant flow rate, but does keep it to < 0.3 SLM, putting these trials in the low flow regime where the throughput does not have a dependence on xenon flow rate. This will again be shown in a later section. The throughput appears to be larger for smaller diameter traps. The 1.5 in diameter trap was measured to have a throughput of $(86.5 \pm 3.5)\%$, which is in good agreement with our experience with 1.5 inch U traps. The 0.5 in trap had a significantly higher throughput of $(92.5 \pm 2.5)\%$, and the 3/8 inch trap throughput being about $(90 \pm 5)\%$. The other modification we made to the 1.5 inch U trap was to weld three of them in parallel, similar to trap #1 from figure 3.5, except with the bottle portion made using 1.5 inch tubing. The throughput of the 1.5 in triple trap was $(70 \pm 6)\%$, a significant reduction from the single U trap.

Moving on from the 1.5 inch U trap modifications, we decided to use 0.5 in plumbing in the construction of our traps. It sees about half of the krypton entrapment as the 1.5 inch trap and does not clog after $< 10g$ of flow, as we found with the 3/8 inch trap. We did have some trouble with warm xenon gas breaking through to the output of the cold trap at higher flow rates. We welded a series of five traps with adding bends in the plumbing in order to increase the length of plumbing immersed in the LN. These traps are shown in 3.5. We measure α for each of these cold traps, this time regulating the xenon flow with an MFC set to 3.3 SLM. 3.3 SLM is in the high-flow regime, so α will be decreased from the low-flow values. These measured values of α are shown in table ???. Refer to figure 3.5 for the description of the numbered cold traps. The results show that, while the additional bends do add more capacity to the trap, they can also reduce the krypton throughput.

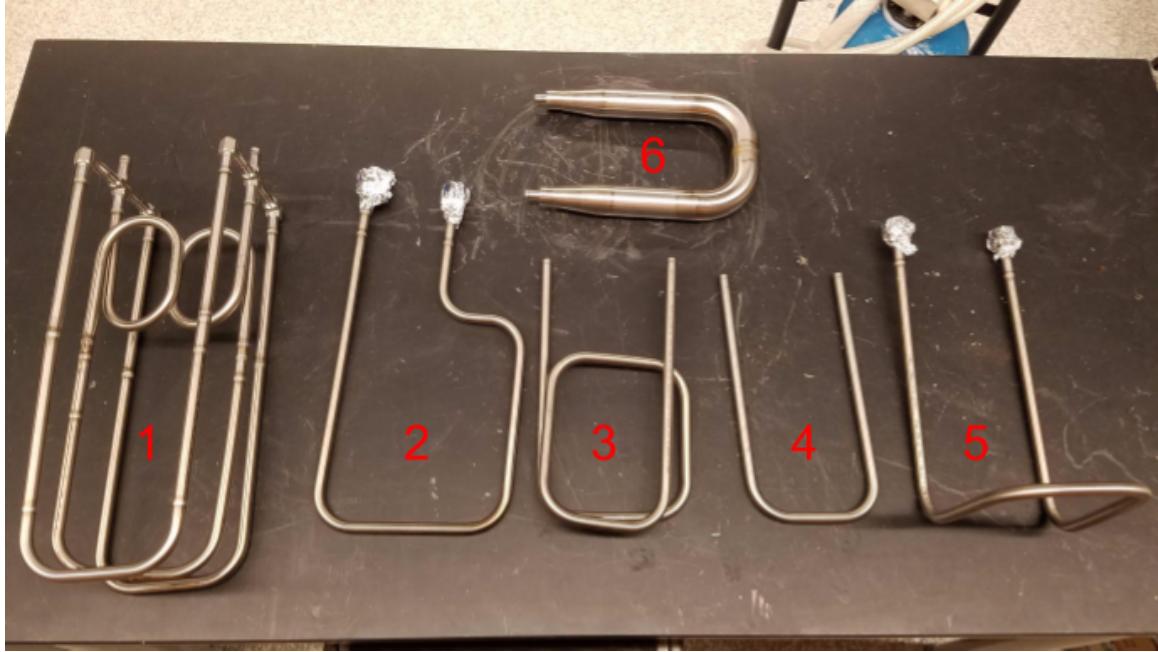


Figure 3.5: Various cold trap geometries considered. We will refer to these geometries as follows: 1- Triple trap (0.5 inch). 2- Stocking trap. 3- Coil trap. 4- U trap (0.5 inch). 5- Boot trap. 6- U trap (1.5 inch). Not shown: 3/8 inch U trap. 1.5 inch triple trap.

Trap #	1	2	3	4	5
α	0.70	0.76	0.38	0.84	0.38

Table 3.1: Throughput parameters measured for various cold trap geometries.

Table ?? indicates that trap #2 has the best throughput apart from the U trap (trap 4#). We have dubbed this the “stocking trap” because of its resemblance to a stocking, as well as because we first installed it on the system on Christmas, 2015. The stocking trap is capable of freezing about 120 grams of xenon before break-through, and only retains about 50% more krypton than the 0.5 inch U trap. For the rest of this document, when we refer to “the 0.5 inch diameter cold trap”, we will in fact be referencing the stocking trap, whereas when we refer to “the 1.5 inch diameter cold trap”, we will be referring to the 1.5 inch U trap.

3.3.2 Formation of Xenon Ice

The xenon ice forms in a short segment of plumbing relative to the approximately one foot length of the cold trap. The enthalpy of sublimation for xenon is about 15.95 kJ/mol at 77 kelvin.[39]. There is an additional 2.73 kJ/mol required to bring the xenon gas temperature down from 295 to 77 kelvin. A 0.36 SLM flow rate is equal to 0.267 mmol/sec of xenon, which requires 5.0 Watts to freeze. If we take the thermal conductance of stainless steel to be 10 W/m K, the maximum cooling power of a 12.7 mm diameter, 1.24 mm thick cold trap will be 70 W/mm.

We must also consider the heat transfer from the LN to the stainless steel trap. The heat transfer rate from LN to a stainless steel surface is highly dependent upon the temperature difference between the bulk LN and the surface. This temperature dependance has a maximum, referred to as the critical heat flux, where the LN changes from “nucleate boiling” to “film boiling”. Film boiling takes place when the LN boils rapidly enough to create an insulating layer, or “film”, of nitrogen gas between the LN bath and the stainless steel surface. The critical heat flux of Stainless steel to LN is on the order of 10 W/cm^2 , putting the maximum heat transfer to our 12.7 mm (0.5 inch) diameter cold trap at about 4 W/mm, making it the limiting factor in the heat transfer to the plumbing.[67] Similarly, a 1.5 inch diameter trap would have a heat transfer of about 12 W/mm, and a 0.25 inch trap would have a heat transfer of about 2 W/mm.

The above estimates of the heat transfer indicate that at flow rates < 1 SLM, all of the xenon should be frozen within the first centimeter or so of cold plumbing. We can approximately measure the length of the ice-forming region in two ways. First, the length of this region is inferred by observing the bubble formation within the liquid nitrogen bath. As the xenon flow is frozen inside of the trap the heat is transferred to the LN bath, and the liquid nitrogen that is in contact with the ice forming region boils. In order to visually

inspect the formation of xenon ice, we also installed a quartz window on the input and output of a cold trap. At low flow rates (< 1 SLM), both of these methods indicate that the ice formation region is less than about 1 cm in length. When viewing the ice formation through a window, there is a clear collar of xenon ice that forms in the input side of the trap at the level of the LN bath, and there is no visible ice formation anywhere else. When observing the outside of the trap, the LN appears to boil where the plumbing enters the bath but nowhere else. In this low-flow regime, the ice collar will expand in depth as more xenon is added until it fully clogs the trap. Flowing at about 0.3 SLM, a 1.5 inch trap will clog after about 400g of xenon has been frozen, while a 0.5 inch trap will clog after only about 70g at 2 SLM.



(a) Ice collar forming.



(b) Fully clogged trap

Figure 3.6: Two images of how ice is formed in a cold trap. The left image shows a thick collar of ice beginning to form. This collar contains > 100 grams of xenon ice. The right shows the collar after it has fully clogged the 1.5 inch diameter cold trap. This plug has roughly 400 grams of xenon is.

At higher flow rates (> 1 SLM), the ice no longer forms a collar, but rather a sleeve along the inside of the trap. This is likely due to the xenon ice forming an insulating layer over the stainless steel, thereby reducing the cooling power of that segment of plumbing

to the point where it is no longer able to freeze the xenon. In the high flow regime, the LN will still only boil along a short segment of plumbing, but this segment can be seen to migrate along the trap from input to output. Eventually, enough of the trap surface is covered that the trap is no longer able to maintain a constant xenon temperature at the output and the xenon pressure at the RGA rises. We call this effect xenon break-through, and is avoided whenever possible. The xenon pressure is already set to be higher than the operational pressure of the RGA, so any significant increase above this set-point could cause damage to the RGA. Additionally, either from physical effects inside the cold trap or from electronics effects of the RGA becoming over-pressured, PP_{Kr} tends to drop in the xenon break-through region limiting the usefulness of any data taken in the region.

In addition to the considerations from actively forming xenon ice, there are also issues and dependencies that arise from ice that was formed in the cold trap prior to beginning flow. In the high-pressure in which we operate the RGA, the RGA electronic baseline offset is highly dependent on the pressure of xenon. This means we need the xenon pressure to be extremely stable over the course of the xenon flow, otherwise we may see a false krypton signal caused by a rising electronic offset. To this end, we must form a small kernel of ice prior to an analysis run so that once xenon flow starts the electronic baseline at a xenon ice pressure will already have been established.

To see the possible effects of failing to maintain a stable xenon pressure we look to figure 3.8. In looking for a genuine krypton signal, we can check that the mass abundances are correct. The 84 amu line should be roughly 3 times more prominent than the 83 amu line. Additionally, there should be no pressure at 87 amu, so this line will be a good tracer for the baseline offset. For the purposes of this plot, we do a standard normalization ($P_{norm} = \frac{P - \mu}{\sigma}$) on all four pressure traces in order to put them on the same scale. The xenon pressure was not well controlled for this run and rose by roughly 2σ when the flow was started. We also saw a corresponding 2σ rise in both of the krypton traces as well as the 87

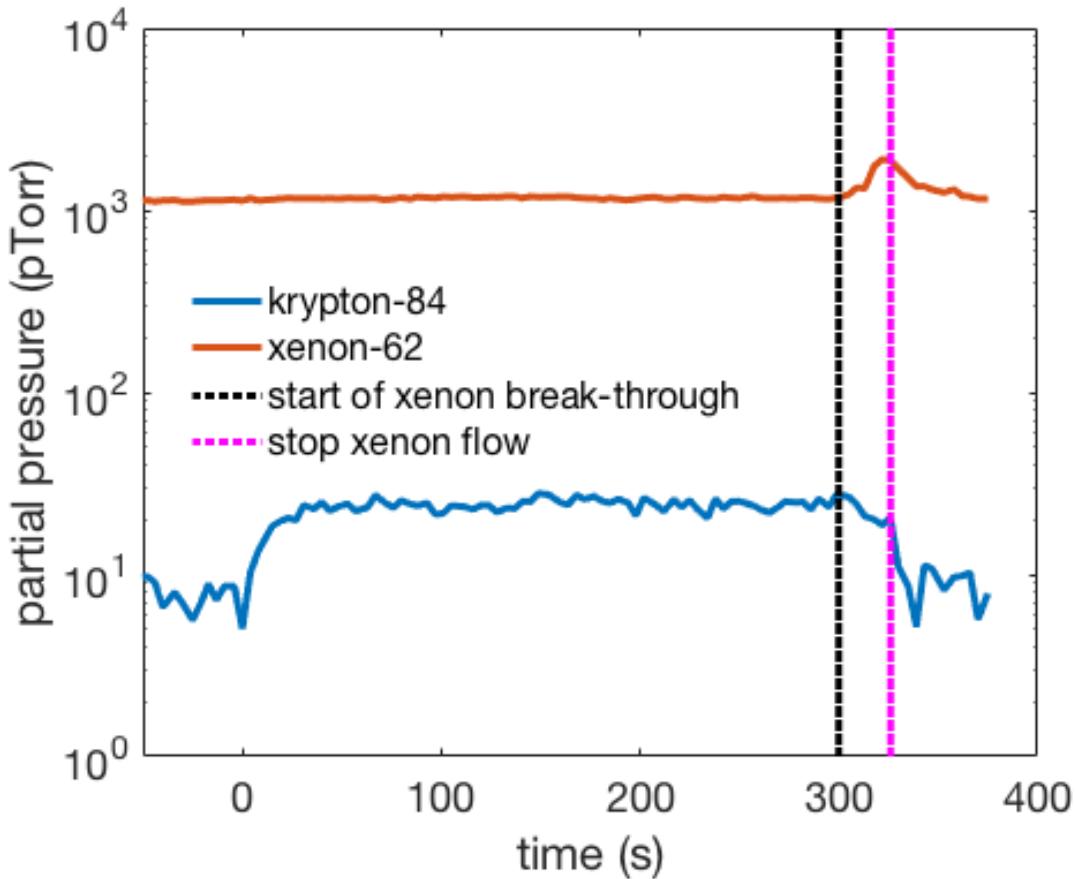


Figure 3.7: Break-through of xenon to the RGA, through a 0.5 inch trap. 4 SLM xenon flow was started at $t=0$ seconds, and xenon breakthrough occurred 300 ± 5 seconds later. This means that about 120 grams of xenon ice formed before flow was shut off; approximately double the amount in an ice plug formed in the low flow regime.

amu baseline-tracker line. The rise in the krypton lines are clearly not genuine, but rather an artifact of a shifting electronic baseline offset. These false signals are extremely dangerous in that they can mimic a genuine signal in excess of 10 times our limit of sensitivity. To insulate ourselves against this possibility, we always track multiple krypton masses, and use their signal ratios as a quality check. We also track a baseline tracer such as 87 amu and xenon pressure. If either of these has a statistically significant rise during the analysis run we mark the measurement as untrustworthy.

We maintain xenon pressure during an analysis run by forming an initial kernel of ice,

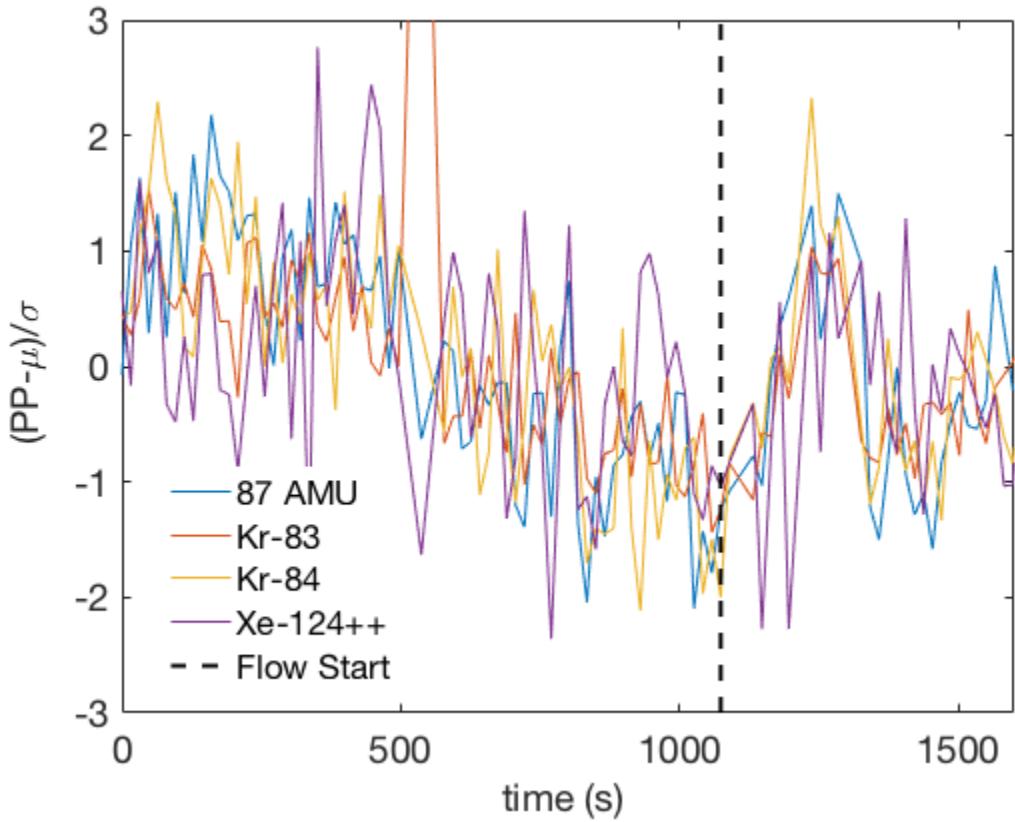


Figure 3.8: Data from an analysis run with poorly controlled xenon pressure. The krypton-83 and -84 lines, as well as a baseline tracer at 87 amu all tracked the drifting xenon pressure exactly.

onto which the rest of the xenon will be frozen. The way this kernel is distributed through the trap has some effects on the response of the trap. We examine three methods of forming the ice kernel, along with their impacts of the ultimate sensitivity of the system.

We begin with the simplest method of forming an ice kernel. We inject roughly 10 standard cc's of xenon into the input of the trap in order to form the base of the ice collar. This procedure does not, however, adequately maintain xenon pressure during xenon flow. When we flow xenon at a rate of 2.5 SLM, we see a rise in both the electronic baseline and the xenon partial pressure of, on average, 4.2σ . By dumping xenon into the ice collar, we are increasing the temperature of the collar, and therefore are increasing the vapor pressure above it. We might expect that this high-vapor pressure xenon will be frozen at some point

further along the trap, thereby maintaining the pressure at the output. However, this xenon elevated xenon pressure seems to be low enough that it will not readily freeze to the cold stainless steel of the trap, and will maintain its elevated pressure all the way through the trap.

To prevent the xenon vapor pressure from rising, we modify our kernel formation technique in order to provide nucleation points for sublimation in the middle and output of the cold trap. We do this by filling the warm cold trap with the full sample pressure of xenon, usually about 2,000 Torr. We then isolate the trap and immerse it in the LN bath allowing this 2,000 Torr of xenon to freeze along the full length of the immersed plumbing. We then add an output kernel by injecting about 10 standard cc into the output of the trap, through V5. Using this method of kernel formation prior to flowing at 2.5 SLM, the change in xenon pressure and baseline offset are reduced to an average of $-0.85 - \sigma$.

Although this method appears to be successful in eliminating, it brings with it two problems. The first problem is that as the LN bath evaporates, the height of the bath may lower below the output kernel. If this happens, the xenon partial pressure at the RGA will rise, leading to a rising baseline. To counter, this we form the kernel with the trap not yet fully submerged in the bath. Once the kernel has been formed, we immerse the trap the rest of the way.

The second problem with this modified technique is that the ice sleeve can interfere with the krypton throughput, thereby reducing PP_{Kr} . This seems to only occur if a large enough amount of xenon (500 standard cc) is used in the formation of the kernel. If we use only about 50 standard cc of xenon, this effect seems to go away without loss in baseline stability.

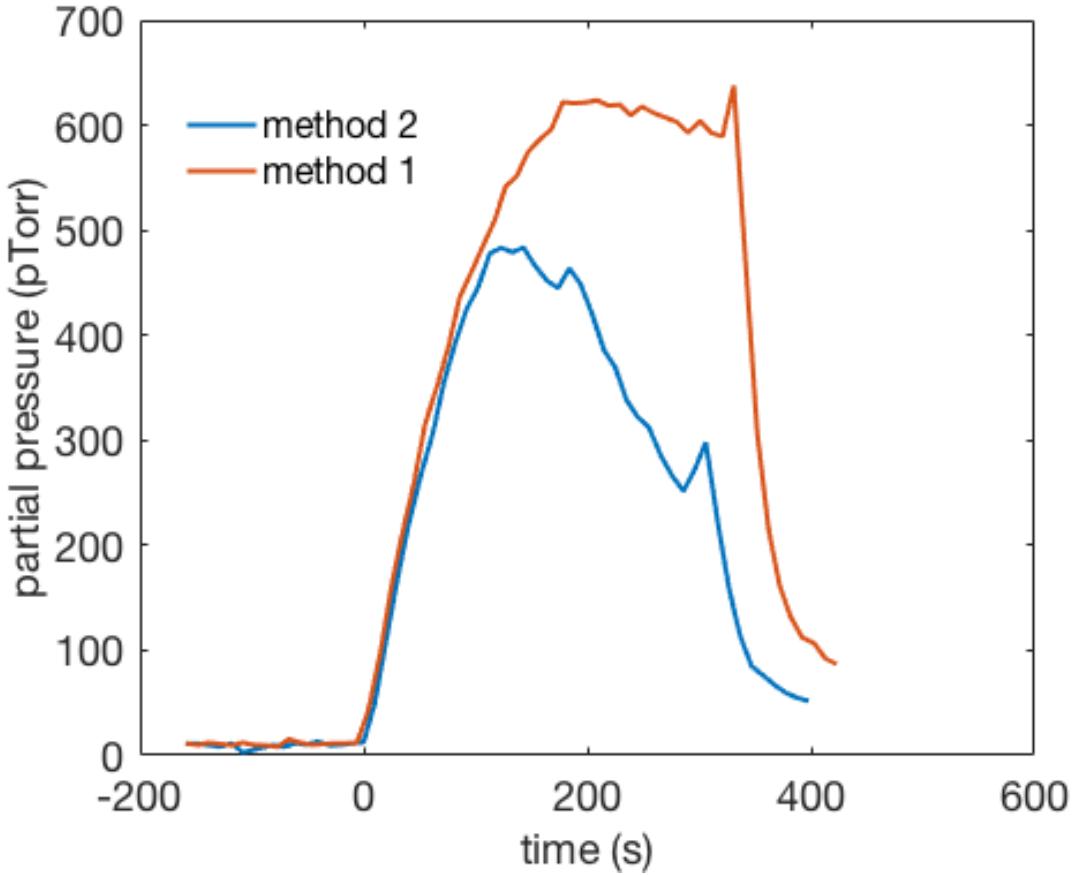


Figure 3.9: Krypton trace using the initial and modified method's prior to 2.5 SLM xenon flow, and a 90x impedance setting. For the method 2 trace we used 2500 Torr (600 standard cc) to for the kernel. This trace begins on the trend as method 1, but sees a sharp turn over and maxes out at only 63% of the method 1 peak.

3.3.3 Flow Rate Dependance

As mentioned previously, there are two distinct regimes of xenon flow in a cold trap sampling system: the low flow regime in which all of the xenon ice is formed within millimeters of the LN surface level, and the high flow regime in which the xenon ice forms a sleeve, which eventually can reach the output side of the trap and cause the RGA xenon pressure to rise. In the low flow regime, the response of the sold trap system to flow rate is extremely linear. In the high flow regime this linearity breaks down. As the ice

sleeve rounds bends in the trap the interaction between the krypton flow and the xenon ice formation changes. These changes work to lower the krypton pressure at the RGA from the exponential response predicted in equation 3.19, as can be seen in figure 3.10.

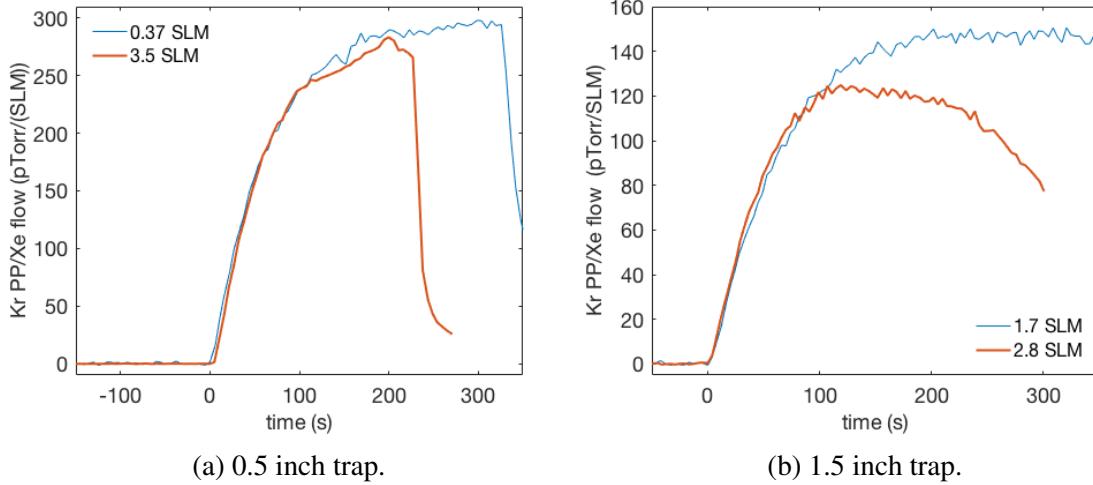


Figure 3.10: Krypton pressure traces resulting from high and low xenon flow regimes. Note the two sharp kinks in the 0.5 inch trend. These correspond to sharp 90-degree bends in the tubing of the trap which were formed using a standard tube-bender. The rounded turns in the 1.5 inch trend correspond to the more gentle bends in the 1.5 inch tubing. These bends are built by welding two elbow pieces together. These measurements were taken in the 15x impedance state.

We do not have a satisfactory explanation as to the physical basis of this drop in krypton pressure at the RGA. Speculations could be made, but in the end we are only interested in how this phenomenon will affect our sensitivity to krypton. To characterize the impacts that flow rate has on the krypton response, we run tests at various flow rates and track the maximum pressure the krypton trace reaches at each setting. We also repeated this flow-rate scan for several impedance states. Above about 2 SLM, the turn-over effect shown in figure 3.10 begins competing with the idealized response described in equation 3.19. This effect is more pronounced at higher impedance settings, but can be clearly seen even in the 1x impedance scan above about 6 SLM.

The turn-over effect is so dominant in the flow rate dependence of α , that it obscures other possible effects. The usual method of calculating the equilibrium krypton pressure,

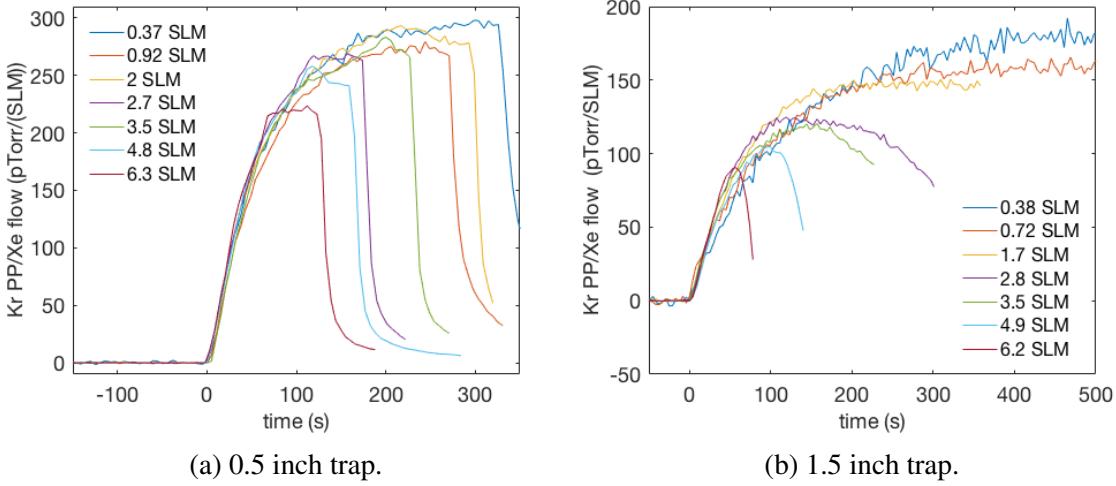


Figure 3.11: Krypton RGA traces normalized to xenon flow rate at various flow rate settings. These traces are all measurements of identical xenon, with an impedance setting of 15x. The response of the system to flow rate appears to be largely linear until about 2 SLM. After this point the Kr trace falls increasingly down from the low-flow traces.

$PP_{Kr,eq}$ is to flow xenon until $PP_{Kr}(t)$ levels off to a constant value. The data in this constant region is then averaged to find $PP_{Kr,eq}$. However, the turn-over effect can create a false plateau in the $PP_{Kr}(t)$ data which invalidates this flat-top averaging method. To account for this effect we can look only at the portion of $PP_{Kr}(t)$ before the first turn-over. This will be data from the time when ice is forming only in the first segment of the cold trap, before the ice sleeve grows around the first bend. If we fit the exponential response from equation 3.19 to this first segment of $PP_{Kr}(t)$, we can estimate what $PP_{Kr,eq}$ would be without the turnover effect.

At low flow rates, the extrapolated values of $PP_{Kr,eq}$ are equal to the flat-top averages. This is expected, since the xenon flow is in the regime where all of the ice is formed in the first leg of the trap, and the turn-over effect does not come into play. At higher flow rates, when the turn-over effect begins to turn on, the two $PP_{Kr,eq}$ values begin to diverge. The exponential fit values continue on a linear trend, while the flat top averages fall off of this linear trend. Returning to equation 3.10 we see that $PP_{Kr,eq}$ can only remain linear with

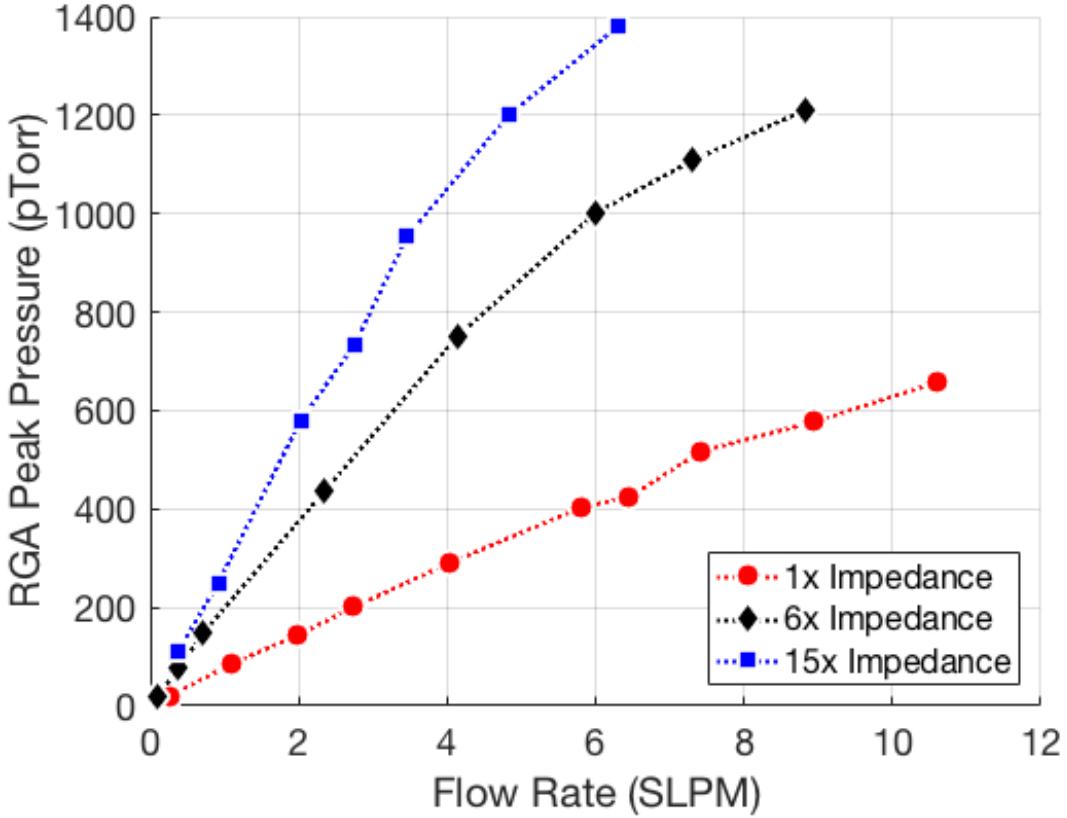


Figure 3.12: Peak krypton RGA pressure as a function of flow rate, and at varying impedance settings. The data for this plot was taken with a 0.5 inch diameter cold trap.

flow rate if α has no flow rate dependence. From the fact that the exponential fit values do remain linear, we conclude that α is not inherently affected by xenon flow rate, but rather picks up an effective flow rate dependence because of the turn-over effect.

3.3.4 Impedance Dependence

The predictions of equation 3.19 also break down at high system impedances, although perhaps in a more well-behaved way than in the case of high xenon flow rates. Just as with increased xenon flow rate, the α parameter will increase at higher impedance settings. However, as opposed to its turn-over induced, effective dependence on flow rate, α appears

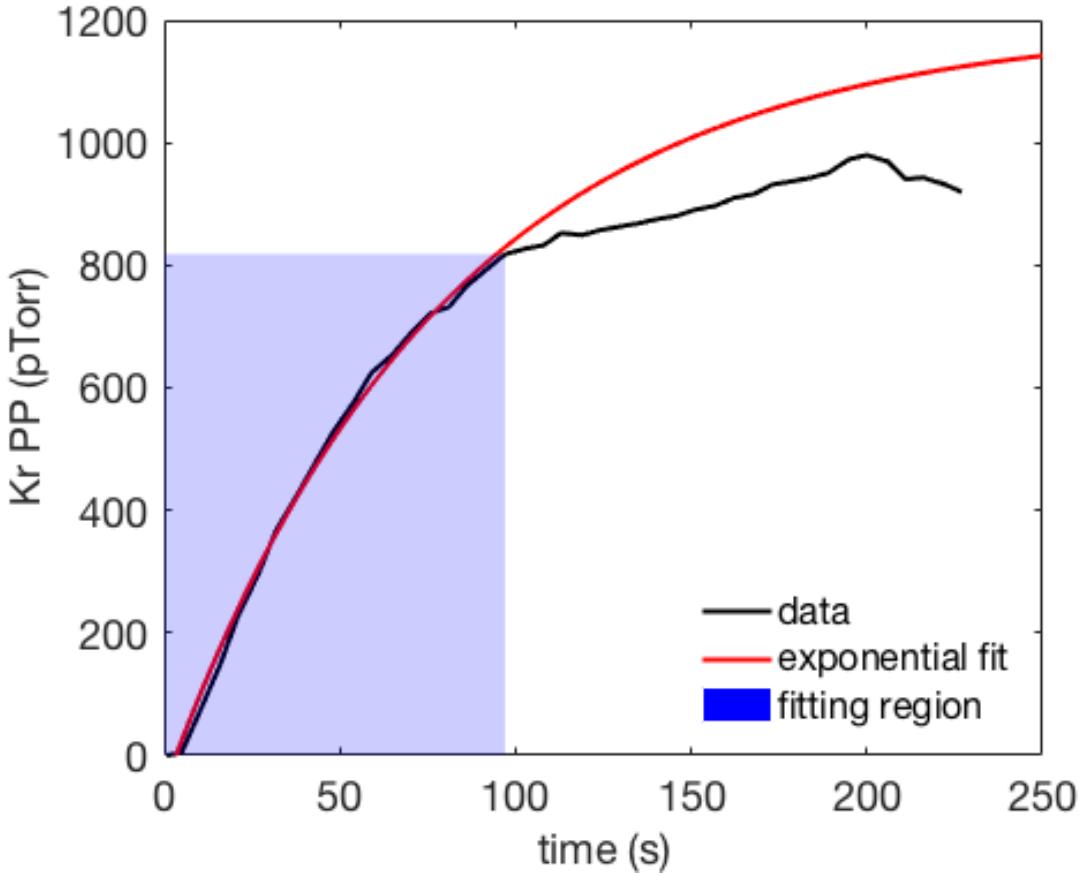


Figure 3.13: An example of fitting an exponential response to the first part of $PP_{Kr}(t)$. This is the same data plotted in figure 3.10a

to have a more fundamental relation to impedance that can be used to characterize the physical basis of the entrapment of krypton in the cold trap.

Consider the pressure trace shown in figure 3.15; the xenon flow rate, Q_0 and krypton concentration, Φ were identical to the krypton trace in figure 3.4, and the impedance, Z_1 was set to be 45 time higher. This trace deviates significantly from what would be expected by increasing Z_1 in equation ???. Both the system response time and equilibrium pressure are expected to increase proportional to Z_1 from equations 3.14 and 3.10, but had a significantly smaller increase. $PP_{Kr,eq}$ increased from 50.8 ± 0.4 to 399.9 ± 1.7 pTorr; a factor of 7.9. The overall response time, τ , increased from 12.7 ± 0.7 to 93.4 ± 1.8 seconds; a factor

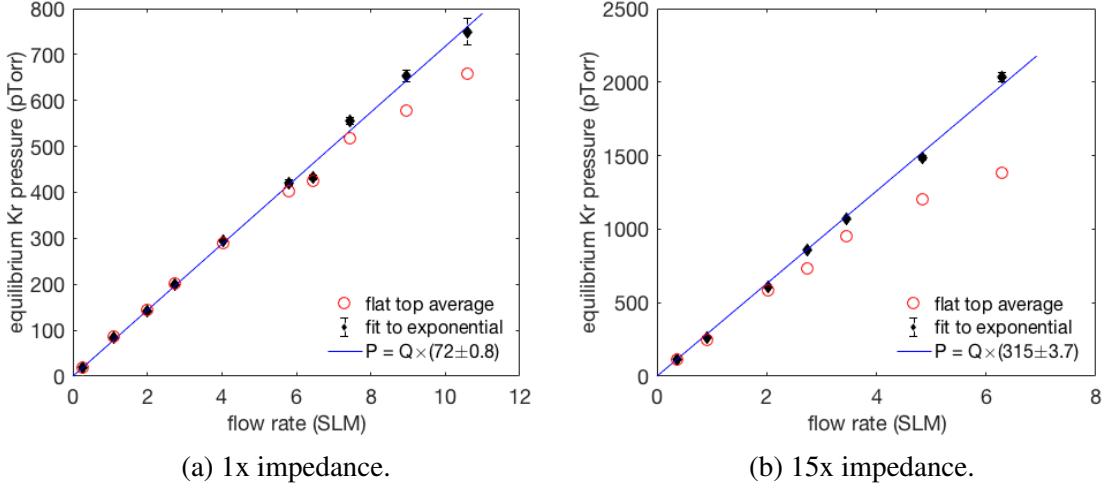


Figure 3.14: Comparison of the flat-top averaged $PP_{Kr,eq}$ the extrapolated equilibrium value calculated from a fit to an exponential response.

of 7.4.

It is an interesting point of fact that the discrepancy in both $PP_{Kr,eq}$ and τ from the predicted results are approximately the same. In fact, although $PP_{Kr,eq}$ and τ do not remain proportional to Z_1 , they do remain proportional to each other. One explanation for this would be that our measurements of Z_1 and S_{RGA} are incorrect, and the impedances are not being increased as much as we have calculated. However, this would only satisfy the proportionality of $PP_{Kr,eq}$ and τ if the throughput parameter, α is constant with impedance.

In order to measure α , we can measure the concentration of krypton in xenon which is left over from an analysis. After flowing a sample into the cold trap for analysis, the sample bottle will be left empty, and all of the xenon (minus a microscopic amount that gets pumped out past the RGA) will be frozen in the cold trap. Along with this frozen xenon will be the krypton that was trapped. We can then transfer this new mixture back into the sample bottle and run a second pass analysis. The ratio of $PP_{Kr,eq}$ from the second pass to the first pass will be equal to the fraction of krypton which gets trapped in the cold

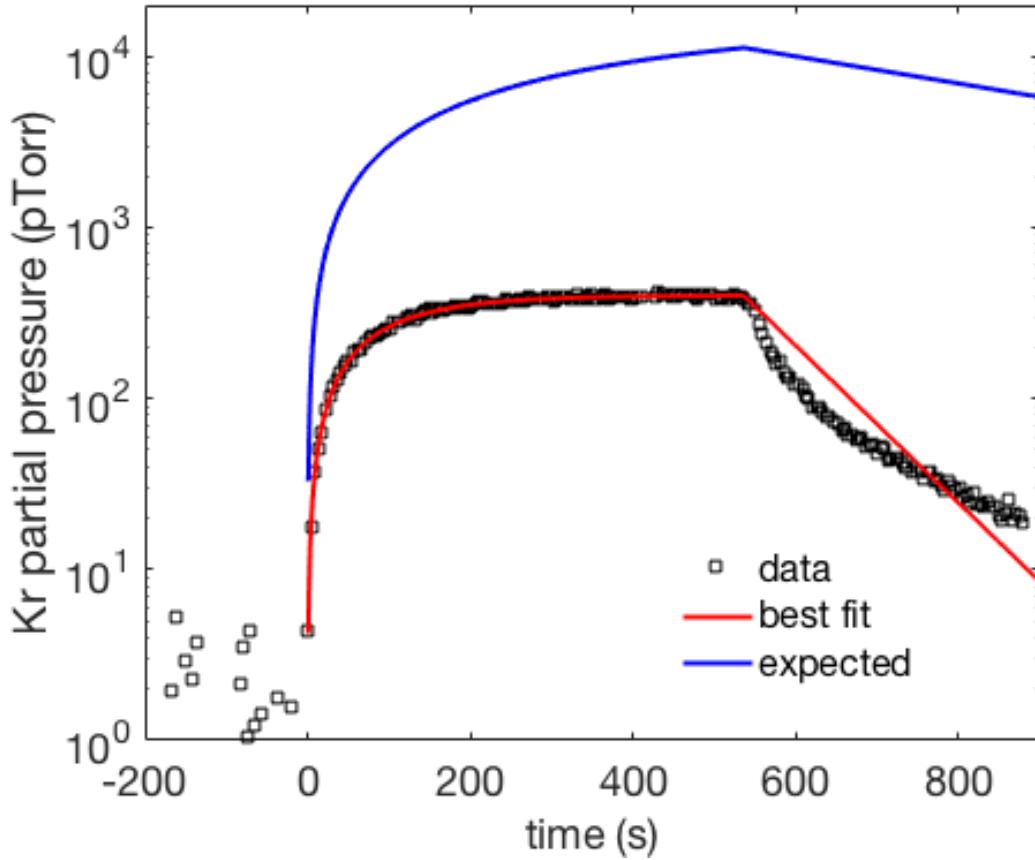


Figure 3.15: RGA trace with 45x impedance settings.

trap. This ratio will also be equal to $1-\bar{\alpha}$. It may be that the throughput parameter during the transient rising section of $PP_{Kr}(t)$ will be different from the equilibrium value. In this case, the averaged $\bar{\alpha}$ will differ from the equilibrium value of α which is presented in section 3.2.3.

Measurements of $\bar{\alpha}$ over a series of impedance settings show that the throughput is decreasing at higher impedances. This means that the fact that $PP_{Kr,eq}$ is not linear in Z_1 , as is predicted by equation 3.19, cannot be fully explained by faulty impedances measurements.

Now that we have established that the krypton throughput is reduced at higher impedances,

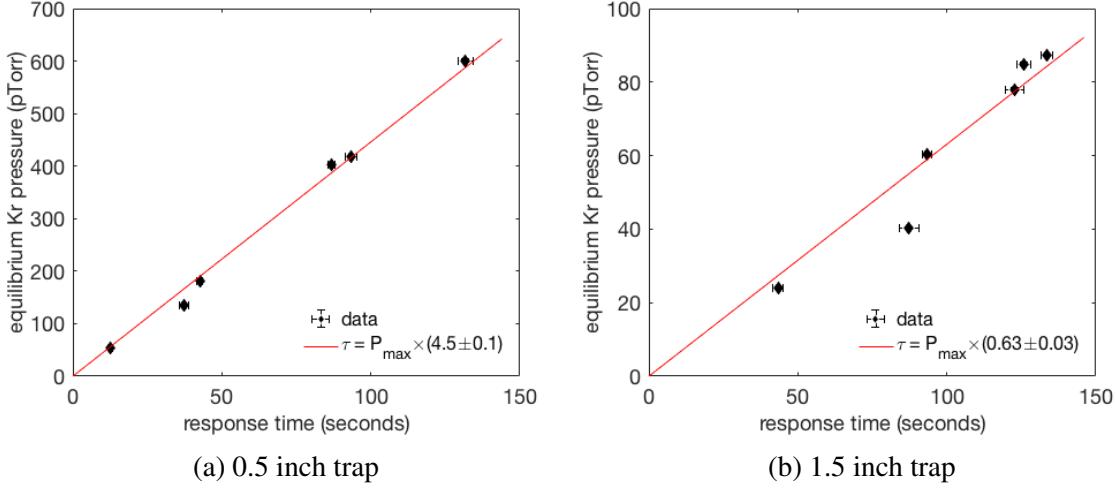


Figure 3.16: Linearity of the characteristic response time, τ , and the equilibrium krypton pressure, $PP_{Kr,eq}$.

we return to our idealized model from section 3.2.3 and attempt to incorporate a finite throughput into our equations. For simplicity, we will make the assumption that the pressure in the RGA volume responds instantaneously to the pressure in the cold trap volume ($P_{Kr,CT}$), so at any moment, t , $PP_{Kr}(t) = P_{Kr,CT}(t)/180$. We start by rebuilding the differential equation for $P_{Kr,CT}(t)$ this time adding a term for entrainment:

$$V \frac{dP_{Kr,CT}}{dt} = \Phi Q_{Xe,CT}(t) - P_{Kr,CT}(t)/Z_1 - Q_{trap}(t), \quad (3.20)$$

where $Q_{trap}(t)$ represents the rate at which krypton is becoming trapped in the xenon ice at a given time. In the constant flow, equilibrium limit we can write Q_{trap} in terms of α :

$$P_{Kr,CT}/Z_1 = \Phi Q_{Xe,CT} - Q_{trap} = \alpha \Phi Q_{Xe,CT}, \quad (3.21)$$

which can be rewritten:

$$Q_{trap} = (1 - \alpha) \Phi Q_{Xe,CT} = \left(\frac{1}{\alpha} - 1\right) P_{Kr,CT}/Z_1. \quad (3.22)$$

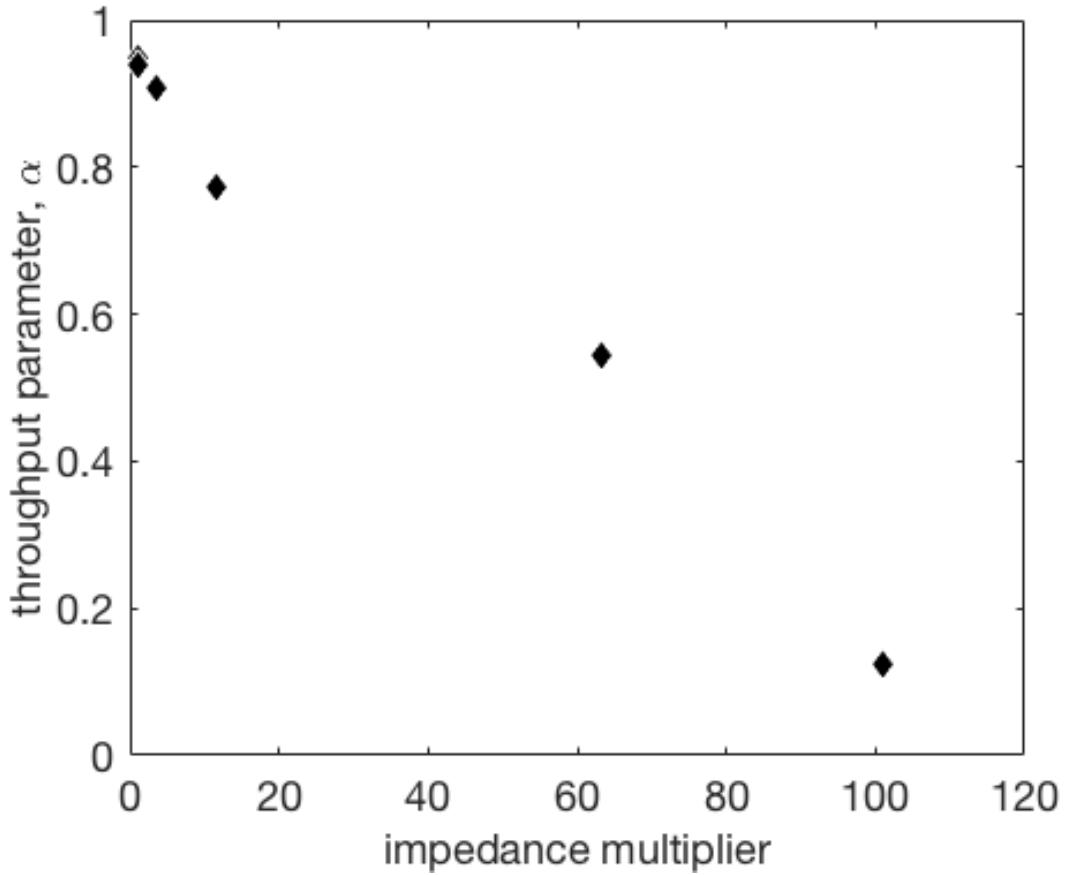


Figure 3.17: Left-over method of calculating $\bar{\alpha}$. The decreasing trend in the throughput indicates that error in the impedance measurements cannot fully explain the observed deviation from equation 3.19.

We do not know a priori how α and Q_{trap} will behave in the non-equilibrium case. The simplest assumption to make is that α remains constant over the full time range in which xenon is flowing. In this case the entrapment rate, entrapment rate takes the form of a virtual leak with constant volumetric pumping rate:

$$Q_{trap}(t) = S_{trap}P_{Kr,CT}(t), \quad (3.23)$$

where,

$$S_{trap} = \frac{1}{Z_1} \left(\frac{1}{\alpha} - 1 \right). \quad (3.24)$$

Rewriting equation 3.20 with this assumption we get a new exponential response equation for $P_{Kr,CT}(t)$:

$$V \frac{dP_{Kr,CT}}{dt} = \Phi Q_{Xe,CT}(t) - \left(\frac{1}{Z_1} + \frac{1}{Z_1} \left(\frac{1}{\alpha} - 1 \right) \right) P_{Kr,CT}(t) \quad (3.25)$$

$$= \Phi Q_{Xe,CT}(t) - \frac{1}{\alpha Z_1} P_{Kr,CT}(t) \quad (3.26)$$

After accounting for a constant throughput parameter, the overall response time constant of the cold trap will have a linear dependence on the throughput parameter:

$$\tau = \alpha Z_1 V. \quad (3.27)$$

This agrees with the linearity between τ and $PP_{Kr,eq}$ shown in figure 3.16. To make this explicit, we can use equation 3.27 to rewrite equation 3.10:

$$PP_{Kr,eq} = \frac{\tau}{180V} Q_{Xe,CT} \Phi_{Kr}. \quad (3.28)$$

A further assumption we could make is that S_{trap} does not have a dependence on Z_1 . Under this assumption, we can begin to make predictions about how α will behave as a function of impedance. Writing equation 3.25 in terms of S_{trap} gives:

$$V \frac{dP_{Kr,CT}}{dt} = \Phi Q_{Xe,CT}(t) - \left(\frac{1}{Z_1} + S_{trap} \right) P_{Kr,CT}(t), \quad (3.29)$$

which means:

$$\frac{1}{\tau} = \frac{1}{Z_1 V} + \frac{S_{trap}}{V} \quad (3.30)$$

$$\tau = V \frac{Z_1}{1 + Z_1 S_{trap}} \quad (3.31)$$

Another way to put this is that the overall response time is the inverse sum of the idealized output time constant, and the entrapment time constant:

$$\frac{1}{\tau} = \frac{1}{\tau_{out}} + \frac{1}{\tau_{trap}}, \quad (3.32)$$

where $\tau_{out} = Z_1 V$ and $\tau_{trap} = V / S_{trap}$. Equation 3.32 indicates that when $\tau_{out} \ll \tau_{trap}$ the cold trap response will have the idealized linear dependence on Z_1 . However, in the limit $\tau_{out} \gg \tau_{trap}$, the response will approach a constant in Z_1 .

Substituting equation 3.30 into equation 3.28, we get:

$$PP_{Kr,eq} = \frac{1}{180} Q_{Xe,CT} \Phi_{Kr} \frac{Z_1}{1 + S_{trap} Z_1}. \quad (3.33)$$

We fit this equation to the $PP_{Kr,eq}$ data taken at various impedance settings. We approximate the corresponding Z_1 values in the following way. We calculate Z_1 at the 1x impedance setting using equation 3.27, where τ is the best fit value to $PP_{Kr}(t)$, and α is measured using the left-over method. The rest of the Z_1 values are calculated by multiplying the 1x impedance value by the scaling factor measured in the adjustment of the xenon pressure described in section 3.2.2. For the 0.5 inch trap, we take $V = 183.8$ cc. For the 1.5 inch trap, we did not measure the volume, so assume that Z_1 at 1x impedance is the same for both traps.

The data for Z_1 versus $PP_{Kr,eq}$ fits reasonably well to equation 3.33. For the 0.5 inch

trap, the best fit $S_{trap} = 0.89 \pm 0.12$ cc/s and $\tau_{trap} = 207 \pm 30$ s. For the 1.5 inch trap, $S_{trap} = 2.6 \pm 0.5$ cc/s and $\tau_{trap} = 180 \pm 30$ s.

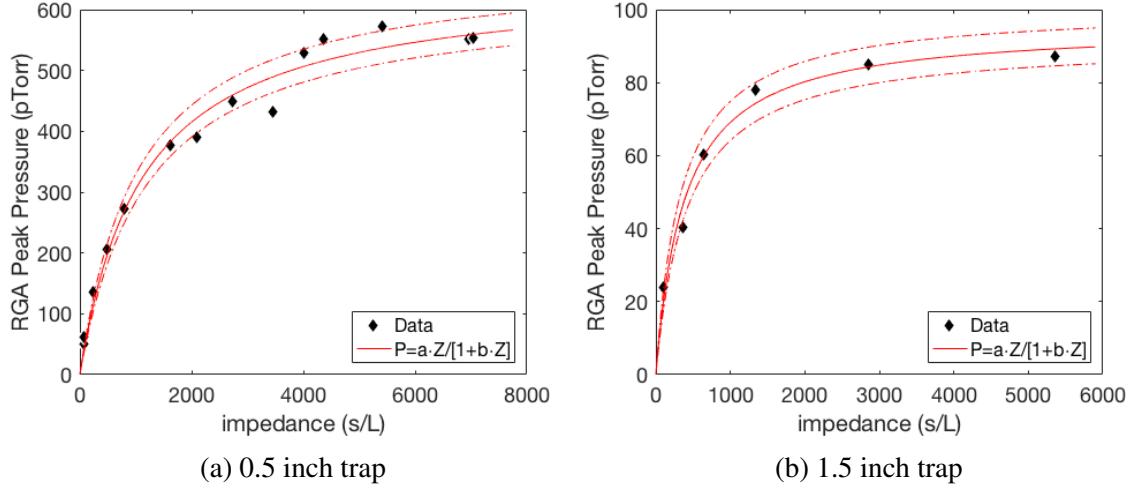


Figure 3.18: Equilibrium krypton pressure as a function of impedance. This fitting model is derived from the assumption that S_{trap} is independent of impedance. The data fits this model reasonably well.

3.3.5 Post Flow Behavior

To this point we have largely ignored the behavior of $PP_{Kr}(t)$ after the xenon flow has been stopped, but this data contains interesting features that are worth investigating. The most obvious feature is the departure from the exponential decay expected from equation 3.19. In figure 3.15 we see that after the flow is turned off, the krypton pressure begins to drop much faster than the trend expected from the fit to the rising portion (τ_{rise}) but turns over and eventually levels off to an exponential trend with a significantly longer time constant than expected.

Our best explanation for the quickly falling transient behavior is that the volume of the cold trap becoming effectively larger when the flow is turned off. While a macroscopic amount of xenon is being flowed into the cold trap, the input side of the cold trap will not be in equilibrium with the output side. As mentioned previously, the input side of the cold

trap will be in viscous flow, while the output will be near vacuum. In this arrangement, the krypton pressure in the vacuum state ($P_{Kr,CT}$) will be physically restricted from expanding past the ice-forming region, effectively reducing the volume of the cold trap. Once flow has stopped, this molecular-flow krypton will be allowed to expand into the full cold-trap volume, and in so doing, will lower $P_{Kr,CT}$. To confirm this effect, we conduct two trials with identical impedance, flow rate, and sample mass. In the first trial we use a 502cc, 0.5 inch diameter cold trap. In the second test, we add a 500cc stainless steel sample bottle to the output of the trap. Since the sample bottle is already in the vacuum state before the xenon flow is turned off, the volume difference should be much smaller, and therefore the transient drop should be much smaller.

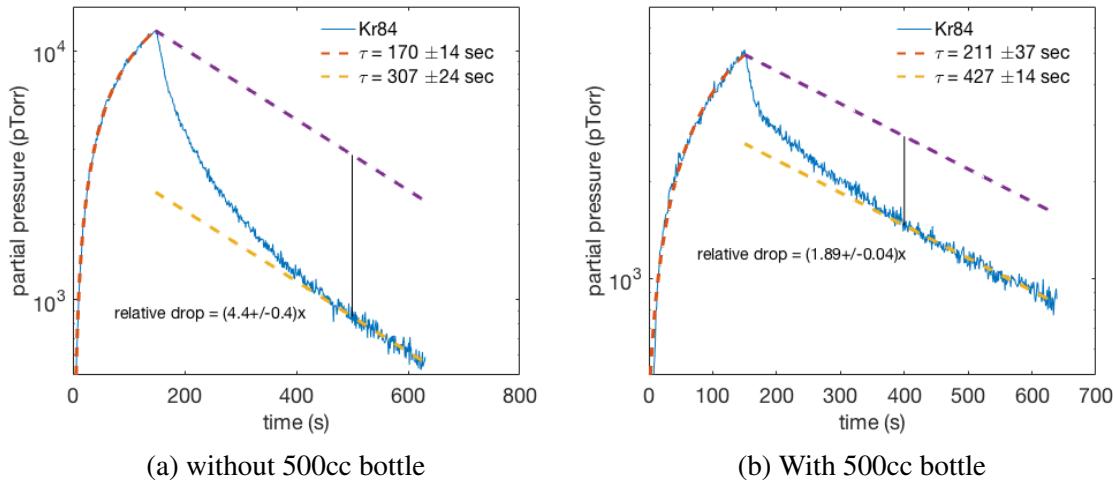


Figure 3.19: Trials with and without a 500cc sample bottle connected to the output of the cold trap. These runs were both done at 3SLM, and at 19x impedance.

After running these trials at 3SLM and 19x impedance, we find that when the 500cc bottle is attached, $P_{Kr,CT}$ drops by $(47 \pm 1)\%$ in the transient region. When the bottle is not connected, this drop is $(77 \pm 2)\%$. We calculate these drops by fitting an exponential decay to the region of $P_{Kr,CT}(t)$ after it has leveled off from the transient region. We then take the difference between this trend and a trend with the same time constant which passes through

the last point of $P_{Kr,CT}$ before the xenon flow was stopped. It should also be noted here that the rise time and fall time are both longer in the trial with the bottle attached, but not as much as might be expected from doubling the cold trap volume. In fact, the rise times are only about 1 standard deviation apart. It may be that the added impedance of the valve used to connect the bottle to the cold trap limits communication between the two volumes. Also, we ran these trials in the high xenon flow regime in which the ice formation region will move along the length of the cold trap over the course of the run. This should make the effective volume increase more pronounced but may obscure tests pertaining to the rise and fall time constants.

We also used the post flow region of the data to test whether or not there was diffusion occurring in the cold trap. We ran several tests in which we would close V6 in order to shut off the P/Z_1 term in equation 3.25. In this way we hoped to measure the rate at which $P_{Kr,CT}$ is reduced purely by diffusion into static xenon ice.

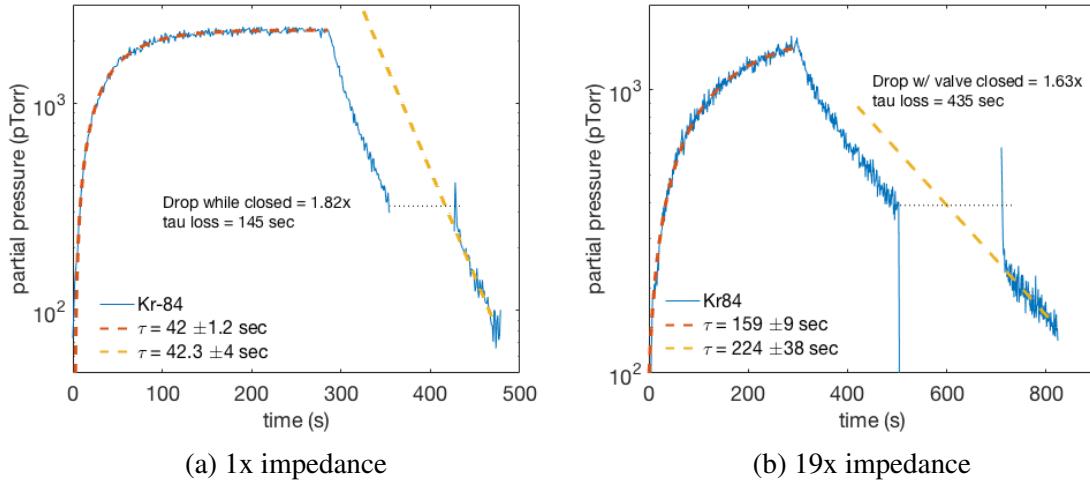


Figure 3.20: Trials at 1x and 19x impedance, each at 0.3 SLM. Each trial has a period of time during post-flow in which V6 was closed; a 70 second period in the 1x case and a 210 second period in the 19x case. In both trials, the fractional drop in pressure while V6 was closed was roughly the same. The post-flow transient drop was calculated to be $(26 \pm 10)\%$ for the 1x impedance run and $(34 \pm 8)\%$ for the 19x impedance run. The “tau loss” indicated on the plots are extrapolated time constants assuming the pressure drop with V6 closed is due to some exponential decay.

The results were somewhat ambiguous; we did find that the krypton pressure dropped while V6 was closed, but the fractional drop was on the order of about (1.7 ± 0.2) regardless of the amount of time V6 was left closed (Δt). This is more indicative of a separate issue having to do with the process of closing and reopening V6 than it is of diffusion. We would expect that more krypton would diffuse into the ice the longer it was left in this static state. We chose longer Δt 's to correspond to higher impedances. It is possible that there was an impedance-dependent diffusion which our choice of Δt happened to cancel out, however an impedance-dependent diffusion would disagree with the results from the previous section.

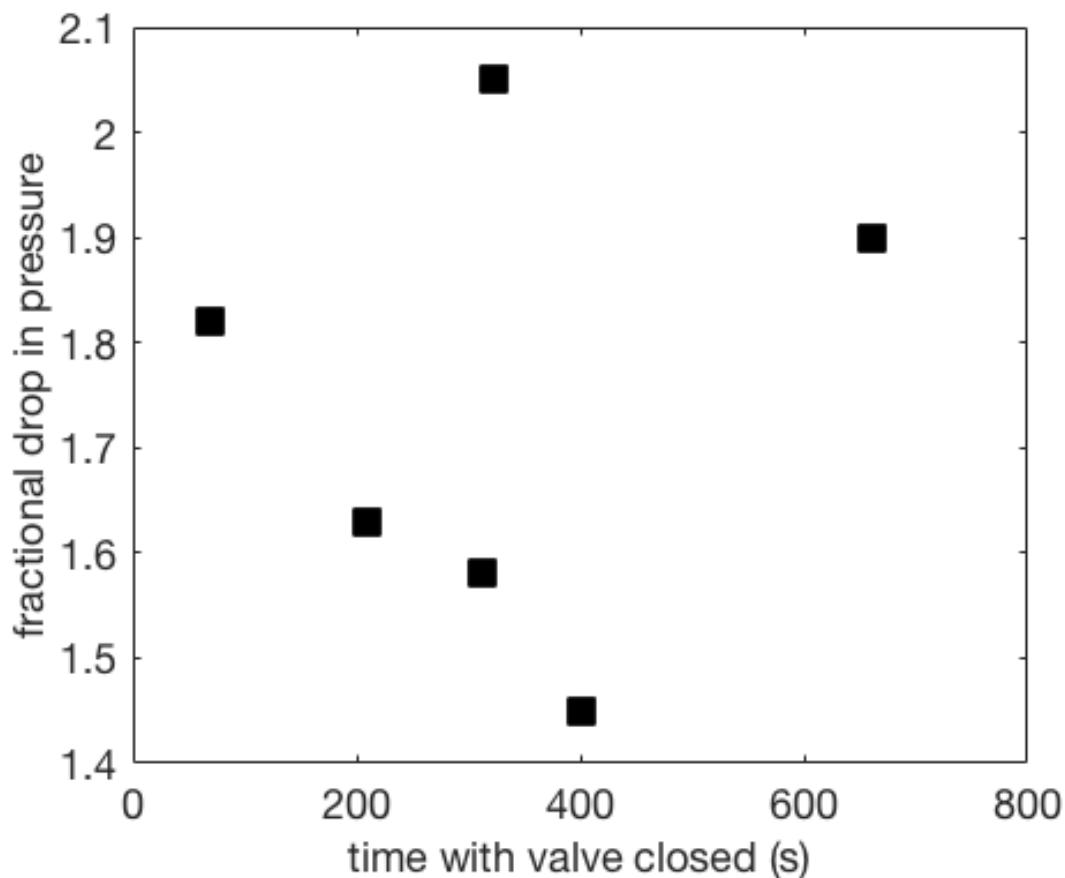


Figure 3.21: Lost krypton pressure as a function of the length of time with V6 closed. There does not seem to be a clear trend.

The question remains as to why the long term post-flow decay rate of $P_{K,CT}(t)$ is so

much lower than the best-fit rate of the rising data. The obvious answer would be in τ 's proportionality to the volume of the cold trap. If V sees an effective increase after the xenon flow is turned off, then τ would see an increase of the same relative size. This matches the data from figure 3.20b in which the fractional increase in τ is 1.4 ± 0.3 , and the fractional increase in volume calculated from the post-flow transient drop in pressure is 1.5 ± 0.2 .

There is still some tension with the data. First, we don't see a post-flow change in τ in the 1x impedance plot (figure 3.20a) like we see in the 19x impedance plot. Also, we see no clear evidence of krypton entrapment occurring when the xenon flow has been turned off, leaving only entrainment-like effects. These should turn off in the post flow region, allowing τ to approach its predicted value. In the case of figure 3.20b, the expected value is approximately $1.4 \times 19 \times 42 \text{ sec} = 1120 \text{ sec}$ after accounting for the impedance factor and effective volume increase. Instead, we see no evidence of this turn-off at all.

3.3.6 Diffusion and Entrainment

In the previous sections we constructed a model where the krypton entrapment rate behaves in the manner of a constant volumetric pumping speed. This model provides a decent representation of the data, but we are left to ask what this model can tell us about the physical source of the entrapment. We have two postulations as to the source of krypton entrapment; diffusion and entrainment.

Diffusion is governed by two equations- Fick's two laws of diffusion. In one dimension, these are:

$$J = -\frac{d\phi}{dx} \quad (3.34)$$

$$\frac{\partial\phi}{\partial t} = D\frac{\partial^2\phi}{\partial x^2} \quad (3.35)$$

Here J is the amount of substance per unit area per unit time, D is the diffusion coefficient, and ϕ is the concentration of krypton at a certain depth, x , and certain time, t . The boundary concentration at $x = 0$ will be given by the pressure of krypton above the ice and the solubility constant, K :

$$\phi(0, t) = P_{Kr,CT}(t)K \quad (3.36)$$

We can then use equation 3.34 to write the entrapment rate of krypton due to diffusion:

$$Q_{diffusion}(t) = -AD\frac{d\phi}{dx}(x = 0, t), \quad (3.37)$$

where A is the surface are of xenon ice.

To get an idea for the time dependence of the diffusion rate, we'll consider the simplified case of a constant $P_{Kr,CT}$ above a static sheet of unchanging thickness, L , and surface area, A . Diffusion in this scenario could fall into two regimes. for large values of D , the krypton will penetrate quickly, the ice will approach saturation, and the boundary conditions will be $\phi(x > 0, t = 0) = 0$, $\phi(x = 0, t) = P_{Kr,CT}K$, and $\frac{\partial\phi}{\partial x}(x = L, t) = 0$. In this regime, equation 3.35 can be solved using a Fourier series of a rectangular wave with wavelength of $4L$, height of $-P_{Kr,CT}K$, and DC offset of $P_{Kr,CT}K$:

$$\phi(x, t = 0) = P_{Kr,CT}K[1 - \frac{4}{\pi} \sum_{n_{odd}} \frac{\sin(\frac{n\pi x}{2L})}{n}]. \quad (3.38)$$

After we feed this series through equation 3.35, we see that each term in the series will pick up a time dependence of $e^{-(\frac{n\pi}{2L})^2 Dt}$. This means that the higher order terms will quickly fall away leaving only the first order term remaining:

$$\phi(x, t \rightarrow \infty) = P_{Kr,CT}K[1 - \frac{4}{\pi} \sin(\frac{\pi x}{2L}) e^{-(\frac{\pi}{2L})^2 Dt}]. \quad (3.39)$$

In this limit, the krypton entrapment rate will be:

$$Q_{diffusion}(t) = P_{Kr,CT}K \frac{2AD}{L} e^{-(\frac{\pi}{2L})^2 Dt}. \quad (3.40)$$

The second regime of diffusion is if D is very small, and the krypton does not penetrate a significant distance into the ice. In this regime, the ice can be considered a semi-infinite line with boundary conditions, $\phi(x = 0, t) = P_{Kr,CT}K$, $\phi(x > 0, t = 0) = 0$, and $\phi(x \rightarrow \infty, t) = 0$. This problem can be solved using Laplace transformation:[24]

$$\mathcal{L}\{f(x, t)\} \equiv \hat{f}(x, p) = \int_0^\infty e^{-pt} f(x, t) dt. \quad (3.41)$$

The transformation has the nice feature of leaving spacial derivatives unchanged, while transforming away time derivatives:

$$\mathcal{L}\left\{\frac{\partial f(x, t)}{\partial t}\right\} = \int_0^\infty e^{-pt} \frac{\partial f(x, t)}{\partial t} dt = p\hat{f}(x, p) - f(x, t = 0) \quad (3.42)$$

For the boundary conditions above, the transformation of equation 3.35 is:

$$p\hat{\phi} = D \frac{\partial^2 \hat{\phi}}{\partial x^2}, \quad (3.43)$$

the solution to which is:

$$\hat{\phi}(x, t) = c_1 e^{-x\sqrt{p/D}} + c_2 e^{x\sqrt{p/D}}. \quad (3.44)$$

In order to satisfy the boundary condition at infinity, c_2 must be 0, and in order to satisfy

the boundary condition at $x = 0$, we know $c_1 = P_{Kr,CT}K/p$. This leaves:

$$\hat{\phi}(x, t) = \frac{P_{Kr,CT}K}{p} e^{-x\sqrt{p/D}}. \quad (3.45)$$

Transforming back to t space, we get:

$$\phi(x, t) = P_{Kr,CT}K[1 - erf(x/\sqrt{4Dt})]. \quad (3.46)$$

This means the entrapment rate of krypton in this diffusion regime will be:

$$Q_{diffusion}(t) = P_{Kr,CT}K\sqrt{\frac{D}{\pi t}}. \quad (3.47)$$

The krypton entrapment rate in both of these regimes is proportional to $P_{Kr,CT}$, and so could be written as $Q_{diffusion}(t) = S_{diffusion}P_{Kr,CT}$. However, in both cases the volumetric pumping speed, $S_{diffusion}$, would have a time dependence, which goes against our model from the previous section, and so would seem not to fit the data.

We have less of a grasp on how we expect entrainment will behave, however we can create a simple toy model where the entrainment rate is proportional to the xenon flow rate and the pressure of krypton present in the trap:

$$Q_{entrainment} = \beta P_{Kr,CT} Q_{Xe,CT}, \quad (3.48)$$

where β is some constant of proportionality. Under this model we can rewrite equation 3.20:

$$V \frac{dP_{Kr,CT}}{dt} = \Phi Q_{Xe,CT}(t) - P_{Kr,CT}(t)/Z_1 - \beta P_{Kr,CT}(t) Q_{Xe,CT}(t). \quad (3.49)$$

In the equilibrium region, this would give:

$$P_{Kr,CT} = \frac{\Phi Q_{Xe,CT}}{1/Z_1 + \beta Q_{Xe,CT}}, \quad (3.50)$$

or:

$$PP_{Kr,eq} = \frac{Z_1}{180} Q_{Xe,CT} \Phi \frac{1}{1 + \beta Z_1 Q_{Xe,CT}}. \quad (3.51)$$

Comparing this to equation 3.10 we see that in this model, $\alpha = 1/[1 + \beta Z_1 Q_{Xe,CT}]$. Equation 3.51 has the same impedance dependence as equation 3.33, however figure 3.14 shows that α does not have a dependence on xenon flow rate.

Again we are left with a dearth of satisfying explanations. Neither our predictions for the behavior of diffusion or entrainment flesh out in the data.

3.3.7 Model Overview

The formation of xenon ice is a complicated process, and its interaction with a time-dependent krypton pressure is likely even more so. It is perhaps unreasonable to expect such overly simplified models as we have posed thus far would suffice in describing this process adequately. That being said, in this section, we have developed some toy models that are able to predict the system's behavior to some extent. The two most important takeaways are in how the krypton RGA pressure responds to system impedance and xenon flow rate. Above about 2 SLM flow rate, the xenon ice begins to form past the first bend in the cold trap plumbing. When this happens, $PP_{Kr}(t)$ begins to drop off of its ideal trend.

The $PP_{Kr}(t)$ has a monotonically increasing response to increases in Z_1 , although it begins to asymptote to a constant value above roughly 100x impedance. Practical considerations will likely win out at high impedances, making the optimal setting at somewhere less than 100x. The exponential response time constant of the cold trap also asymptotes to

a constant, so as the impedance is increased to be much greater than 100x, the characteristic response time of the RGA volume will likely begin to compete.

There is very little we can say about what is physically happening inside the cold trap the causes krypton to become trapped in the xenon ice. The overall effect seems to mimmic a leak with a constant volumetric flow rate, S_{trap} that is independent of both flow rate and impedance. We have found no evidence that diffusion of krypton into the ice plays a major role, and all of our test point to some effect that is dependent on active xenon flow, but whose rate is not affected by changes to the xenon flow rate.

3.4 Analysis Scheme

The physical value we are interested in measuring is the concentration of an impurity, specifically krypton, in a sample of xenon gas. This value is typically referred to as Φ and cited in units of grams of krypton per gram of xenon. The calculation of Φ is done using the RGA partial pressure data collected between steps 3 and 7 of the procedure outlined in section 3.1.2. An example of this data is shown in figure 3.22.

There are four distinct time-intervals in figure 3.22 labelled I through IV.

- I is the period of time after ice has been formed (step 3), but before the xenon flow has been started (step 5). During this interval, both xenon and krypton traces should be constant; if they are trending or otherwise varying systematically, there is some problem that needs to be addressed before continuing. The average krypton pressure over this interval is used as the baseline value and will be subtracted from the analysis pressure. The average xenon pressure can be used as a measure of the RGA gain, since the physical xenon pressure will not change between sample analyses.
- II is the period of time after xenon flow has been started (step 5), but before the krypton pressure has reached its equilibrium value. Given a long enough cold trap the

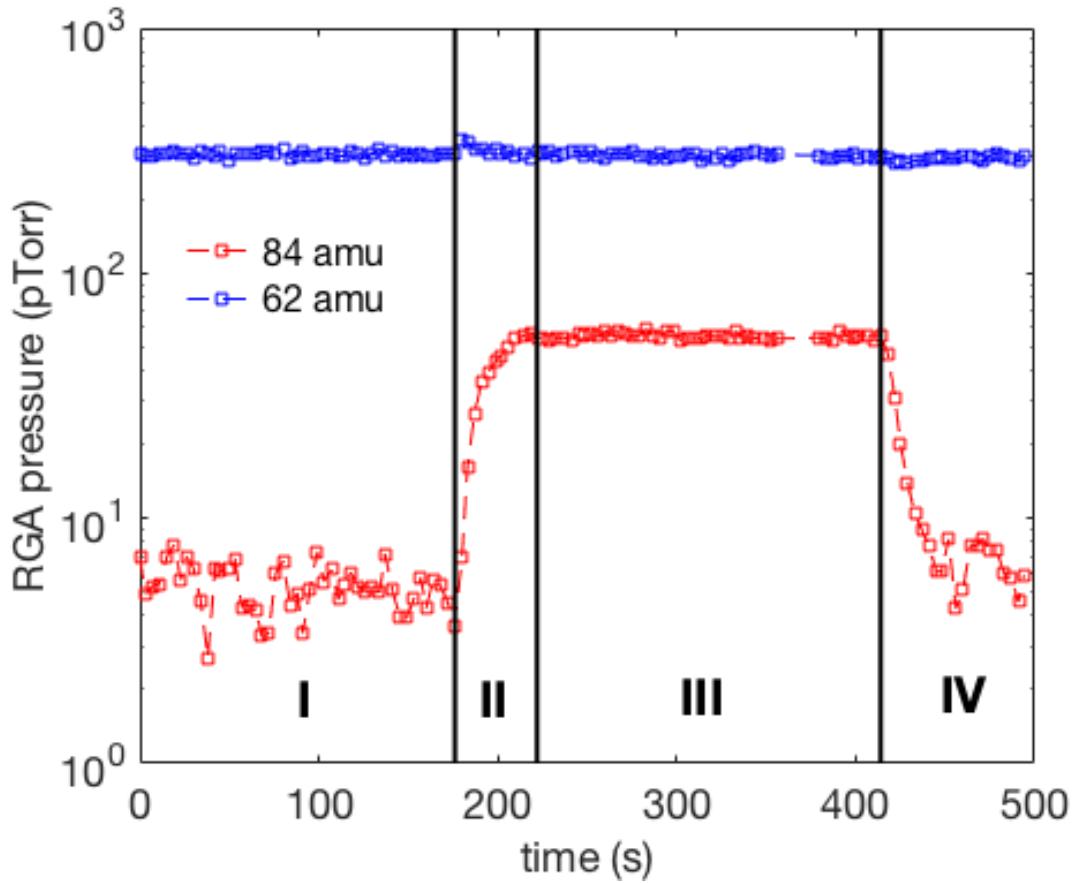


Figure 3.22: The RGA-measured partial pressures of the 84 amu krypton peak and doubly ionized Xe-124 which appears as a peak at 62 amu. The four time intervals indicate: static baseline, rising Kr trace, steady-state Kr pressure, and post-flow Kr pressure fall.

krypton pressure during this step would fit a 1-exponential model, but the geometry of the cold trap can cause kinks in the trace. It is common for there to be a small transient effect in the xenon pressure as is seen here. This is likely due to the ice temperature increasing due to the added heat load from the flowing xenon. This transient effect can illicit an electronic response in the RGA baseline pressure which will mimmic a small krypton signal. The mitigation of this effect will be described in a later section.

- III is the period of time during which the krypton pressure is at its equilibrium value.

This equilibrium pressure is determined by the flow rate of the xenon, the sensitivity of the system, and Φ .

- IV is the period of time after the xenon flow has been stopped (step 6). During this period the krypton pressure will fall away exponentially before it eventually returns to the baseline value.

When the flow of krypton has equilibrated throughout the system, Φ can be related to the flow rate and RGA krypton partial pressure through the following equation:

$$\Phi = \frac{PP_{Kr}}{CQ_{Xe,CT}}, \quad (3.52)$$

where C is a calibration constant which encapsulates the sensitivity of the system, $Q_{Xe,CT}$ is the instantaneous flow rate of xenon into the cold trap, and PP_{Kr} is the krypton pressure. It is possible that there is a physical background seen by the RGA at the mass of interest (84 amu for the case of krypton), but we are only interested in the pressure which is extracted from the xenon sample. To account for any non-zero baseline we subtract out $\bar{PP}_{Kr,0}$, the average krypton pressure measured by the RGA during region I.

When paired with a concurrent flow-rate measurement, $Q_{Xe,i}$, each RGA data point, $PP_{Kr,i}$, collected in region III will give an individual measurement of the purity of the xenon sample, ϕ_i :

$$\phi_i = \frac{1}{C} \frac{PP_{Kr,i} - \bar{PP}_{Kr,0}}{Q_{Xe,i}}. \quad (3.53)$$

We take the average of these individual purity measurements as the final result of the analysis:

$$\Phi = \overline{\phi_i}, \quad (3.54)$$

with N being the number of RGA data points collected in region III. The random uncer-

tainty on this purity result is taken to be the standard error:

$$\sigma_\Phi = \frac{\sigma_\phi}{\sqrt{N}}, \quad (3.55)$$

where σ_ϕ is the standard deviation of the collection of ϕ_i 's. This method of analysis has been previously shown to be linear with purity. [29, 31, 54]

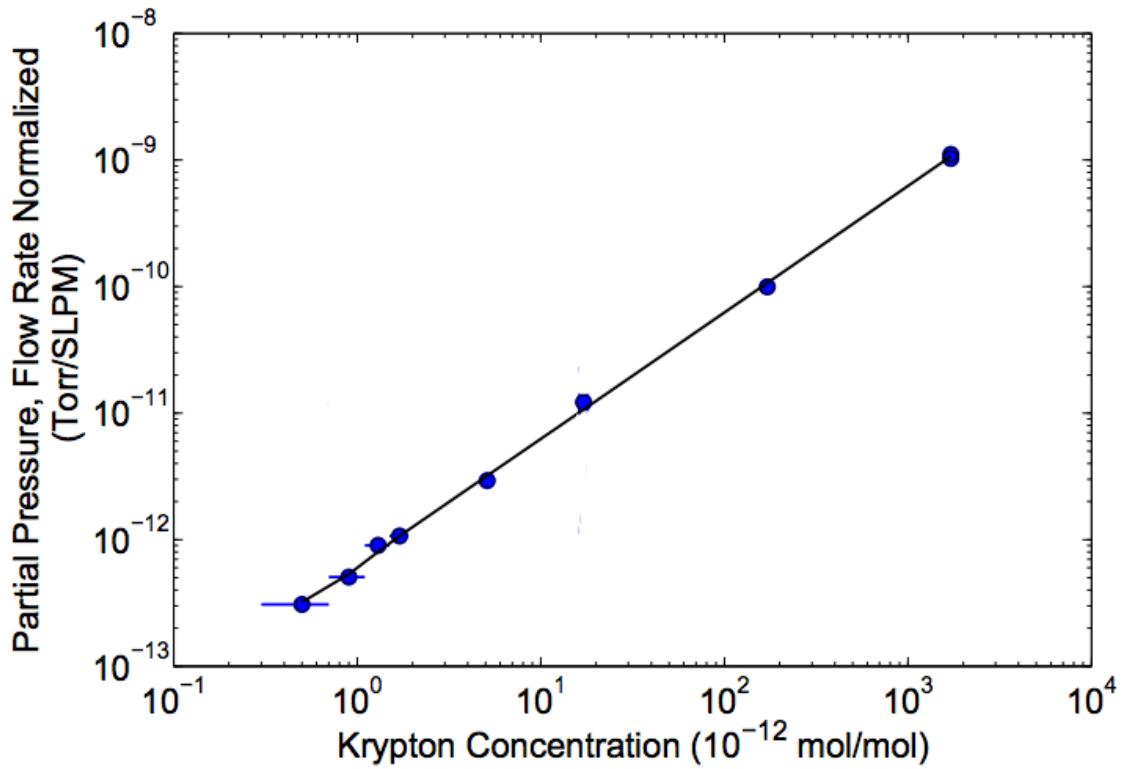


Figure 3.23: The linearity of the averaging analysis method. The slope of this line will be equal to the calibration constant, C .[31]

In order to maximize the krypton sensitivity, we operate in a high-impedance mode (described in later sections) which increases the rise and fall time of the krypton pressure. This being the case, we wish to allow $PP_{Kr,i}$ to be drawn from the non-equilibrium regions II and IV, as well as region III. This In these cases we assume a more general version of

equation 3.52:

$$PP_{Kr}(t) = C\Phi f_Q(t), \quad (3.56)$$

where $f_Q(t)$ is some function which defines the shape of the krypton pressure trace, given a specific flow rate profile, $Q_{Xe,CT}(t)$. $\Phi f_Q(t)$ represents the flow of krypton out of the cold trap, $Q_{Kr,RGA}(t)$, and can be thought of as the input krypton flow, $Q_{Kr,CT} = \Phi Q_{Xe,CT}$, modified by the response of the system. Equation 3.56 will be valid as long as the response is linear with concentration. For example, consider the krypton trace shown in figure 3.22. The flow rate profile for this trace is:

In section 3.2 we find that an ideal system is expected to have an exponential response to flow. Convolving equation 3.16 with an exponential response yields the following shape function

$$f_Q(t) = Q_0 \begin{cases} 0 & \text{for } t \text{ in region I} \\ 1 - \exp(-\frac{t-t_1}{\tau}) & \text{for } t \text{ in region II or III} \\ \exp(-\frac{t-t_2}{\tau}) & \text{for } t \text{ in region IV} \end{cases} \quad (3.57)$$

Fitting this shape function to the data in figure 3.22 gives $\tau = 11.6$ seconds. It should be noted here that the pressure trace shown in figure 3.24a does not fit this shape. This is because the response of the system to flow becomes non-linear at high flow rate and high impedances. Figure 3.24b shows that response does remain linear in concentration even when it is not linear in flow.

We now integrate equation 3.56 between some t_1 and t_2 :

$$\int_{t_1}^{t_2} PP_{Kr} dt = \Phi F_{Q,t_1,t_2}, \quad (3.58)$$

where:

$$F_{Q,t_1,t_2} \equiv \int_{t_1}^{t_2} f_Q(t) dt. \quad (3.59)$$

In terms of the discrete RGA measurements, $PP_{Kr,i}$ this becomes:

$$\Phi = \frac{1}{F_{Q,t_1,t_2}C} \sum_{i=1}^N (PP_{Kr,i} - \bar{PP}_{Kr,0}) \Delta t_i. \quad (3.60)$$

$F_{Q,t_1,t_2}C$ is a constant of proportionality which can be measured by analyzing a xenon sample with a known Φ . However, this constant will only hold so long as $Q_{Xe,CT}(t)$, t_1 , and t_2 are identical between the analysis and calibration runs. To ensure consistency, it is best practice to calibrate after every sample analysis. These calibrations should follow the procedure described in section ?? and should use the left-over sample xenon which is recovered from the cold trap as the base “clean” xenon. This can be done as long as the initial concentration of krypton in the xenon sample is much less than the target concentration of the calibration xenon.

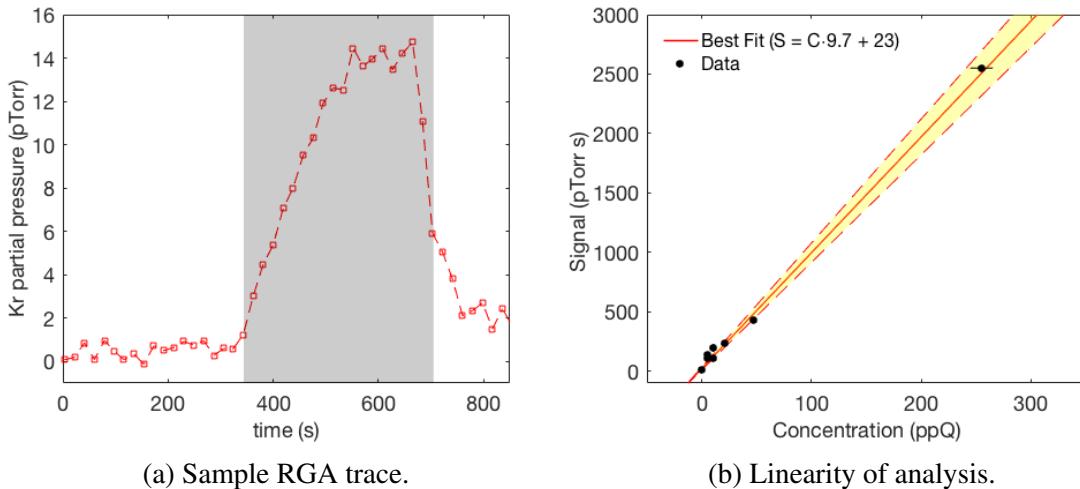


Figure 3.24: Linearity of the integration-style analysis described in equation 3.60. The krypton signals used in these measurements never reached an equilibrium value. The xenon flow profile for these measurements was a square pulse. The height of this pulse was set using an MFC, and the time-width of the pulse was defined by the size of the xenon sample used. t_1 was defined as the start of the xenon flow, plus 20 seconds, and t_2 was defined as the stop of the xenon flow, plus 20 seconds.

The random uncertainty of purity results calculated using equation 3.60 are harder to

estimate than those calculated using equation 3.54. The fluctuations around each datapoint cannot be measured directly, so they are estimated using the baseline data collected in region I. The fluctuations of the RGA tend to increase at higher partial pressure, as shown in figure 3.25. We take the baseline fluctuations, σ_0 , to be equal to the standard deviation of the region I data points. The random uncertainty of each data point, $PP_{Kr,i}$, is then taken to be:

$$\sigma_i = \sigma_0 * (1 + 0.009 * PP_{Kr,i}). \quad (3.61)$$

The propagation of this error to Φ is then:

$$\sigma_\Phi^2 = \frac{1}{F_{Q,t_1,t_2}^2 C^2} \sum_{i=1}^N (\sigma_i^2 + \sigma_0^2/N_B) \Delta t_i^2, \quad (3.62)$$

where N_B is the number of data points used in the calculation of $\overline{PP}_{Kr,0}$ and σ_0 .

3.5 System Parameters and Optimization

Optimizing a cold-trap sampling system is a matter of maximizing the signal to noise ratio, which comes down to minimizing the fluctuations in the RGA baseline and maximizing the system response to krypton. There are several knobs and dials to turn to achieve this, but adjusting one of the knobs might change how one of the dials affects the sensitivity. This section will attempt to catalog the affect of these adjustments in an empirical way and will describe the optimal arrangement.

3.5.1 RGA Parameters

The first and simplest adjustments to be made are to the RGA electronics. These adjustments can be made quickly and easily, and are largely independent from the other knobs and dials. There is a long list of internal RGA parameters which should be understood

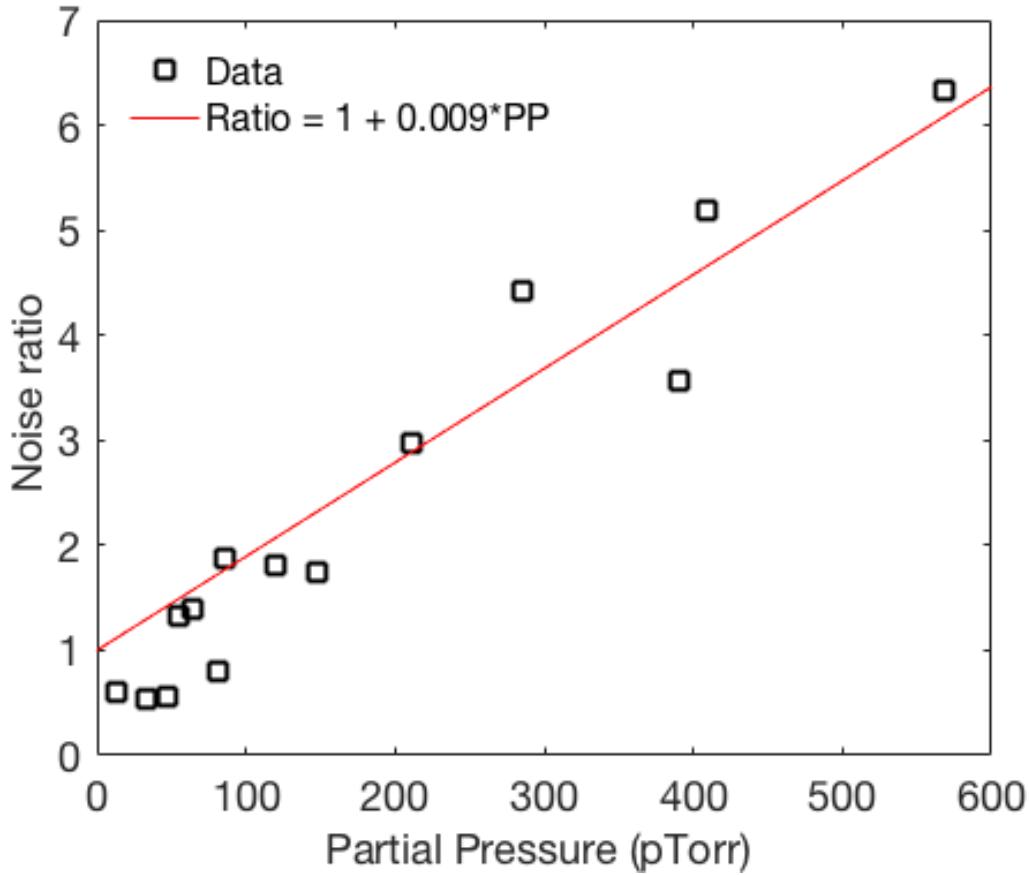


Figure 3.25: The trend in RGA fluctuations as a function of partial pressure. The noise ratio is defined as the fraction by which the RGA fluctuations increase when the partial pressure is increased from its baseline value ($\text{Noise ratio} \equiv \sigma(\text{PP})/\sigma(\text{baseline})$).

before operating a cold trap system. These can be found in chapter 6 of the RGA manual. The two parameters that have the greatest effect on the sensitivity to krypton are the noise floor and the high-voltage setting of the continuous dynode electron multiplier (CDEM).

The noise floor sets the scan speed of the RGA; the lower the noise floor setting, the longer the RGA will spend integrating current on a single mass point. The practical effects are threefold. The obvious first implication is that with a low noise floor, it will take much longer to collect a single data point. At a noise floor setting of 0 the RGA will sit on a mass point for more than 5 seconds, and at a noise floor setting of 3 it will sit for less than

0.5 seconds per mass. For high-sensitivity analysis, it is better to have the noise floor set as low as possible, which will give you fewer data points which have a smaller variance. This will reduce the amount of time spent communicating with the RGA, as well as the amount of down time between communications.

At higher noise floors, there tends to be an offset in the baseline. While we usually try to account for this by using baseline-subtracted pressures in purity calculations, it is possible that the shifted baseline is not additive to the pressure signal. This is indicated by the krypton signal in the LUX run04 data decreasing artificially. There is also evidence from the SLAC system that the baseline is not strictly additive to a physical pressure signal.

Setting the voltage on the CDEM is a balancing act. Increasing the voltage increased the signal amplification. Above a certain CDEM voltage, however, the random fluctuations in the RGA baseline rise faster than the gain, and if the voltage is set too high, the xenon ice vapor pressure will begin saturate the CDEM, degrading and possibly damaging it. The CDEM voltage should be high enough that the largest xenon peaks such as 132 and 133 should be at saturation but not so high that the doubly ionized peaks such as 66 amu saturate.

The health of the CDEM can be tracked using one of the xenon ice peaks, assuming the MG and SP parameters are not changed. MG is the CDEM gain factor and SP is the mass sensitivity factor used to convert the RGA current to partial pressure. The physical values may change over time, but the parameter stored in the RGA memory will not change unless a head-calibration is run. In particular, as the CDEM degrades, the gain will fall. A drift in the gain will be seen most easily as a drop in the measured xenon ice pressure. Since the vapor pressure of xenon ice at 77 Kelvin is physically constant, if this pressure reading drops, it indicates that the gain has dropped. To maintain the CDEM gain, the xenon peak at 62 amu should be monitored. Whenever this value drops, the voltage should be increased until the pressure returns to its initial value.

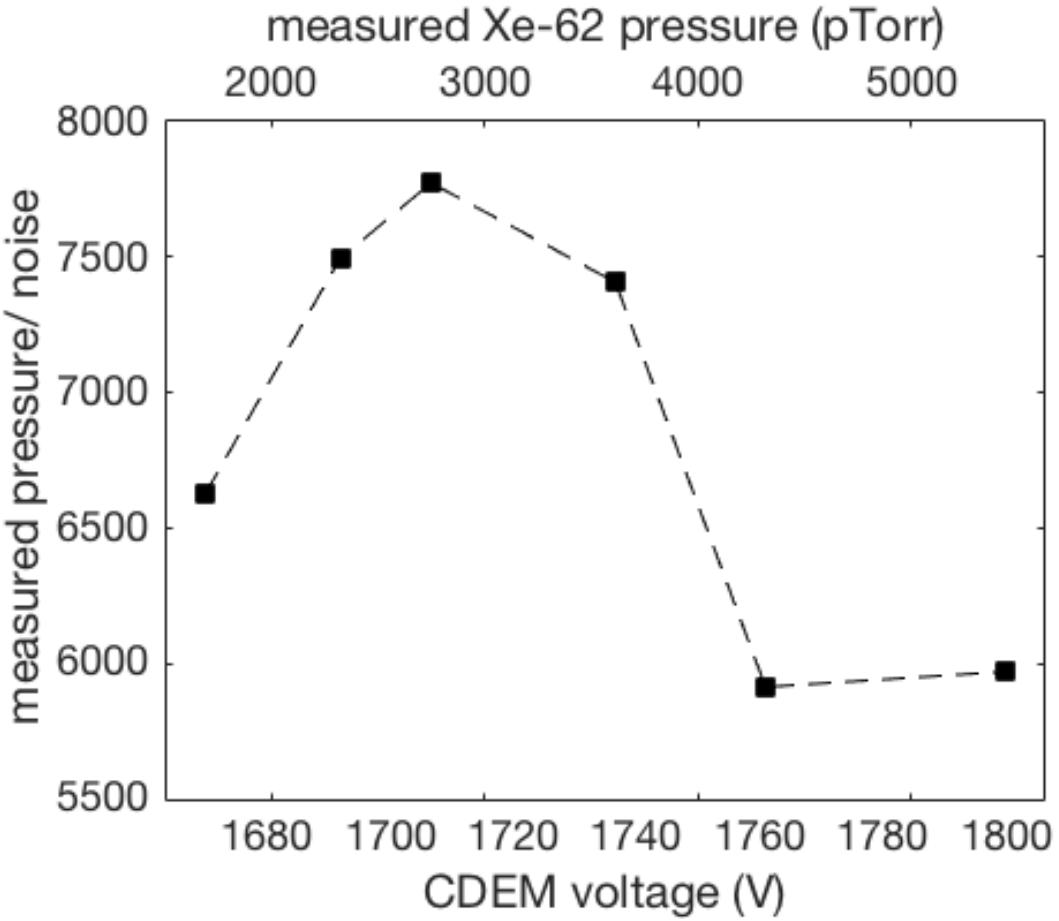


Figure 3.26: RGA sensitivity as a function of CDEM voltage.

3.5.2 Impedance and Flow Rate Settings

Consider the idealized pressure trace shown in figure 3.12, which is the result of a rectangular flow rate profile into a system which has an instantaneous response. The flat top of this trace will have a height given by equation 3.10:

$$PP_{Kr,eq} = \frac{\alpha}{180} Z_1 Q_{Xe,CT} \Phi_{Kr}. \quad (3.63)$$

The width of this pulse will be given by the amount of xenon used in the analysis ($V_{SB} \Delta P_{Xe,SB}$) divided by the flow rate of the xenon into the cold trap $Q_{Xe,CT}$. Assume N is the number of

data points included in the analysis. Using a constant RGA sampling rate of r we find:

$$N = \frac{rV_{SB}\Delta P_{Xe,SB}}{Q_{Xe,CT}}. \quad (3.64)$$

By increasing the flow, we get something of a tradeoff. The pressure which we are trying to measure will increase proportionally to $Q_{Xe,CT}$. However the number of data-points in our analysis will also decrease proportionally to $Q_{Xe,CT}$, thereby increasing the uncertainty. Since uncertainty only has a dependence on \sqrt{N} , we will end up winning in signal-to-noise ratio, which will increase proportional to $\sqrt{Q_{Xe,CT}}$.

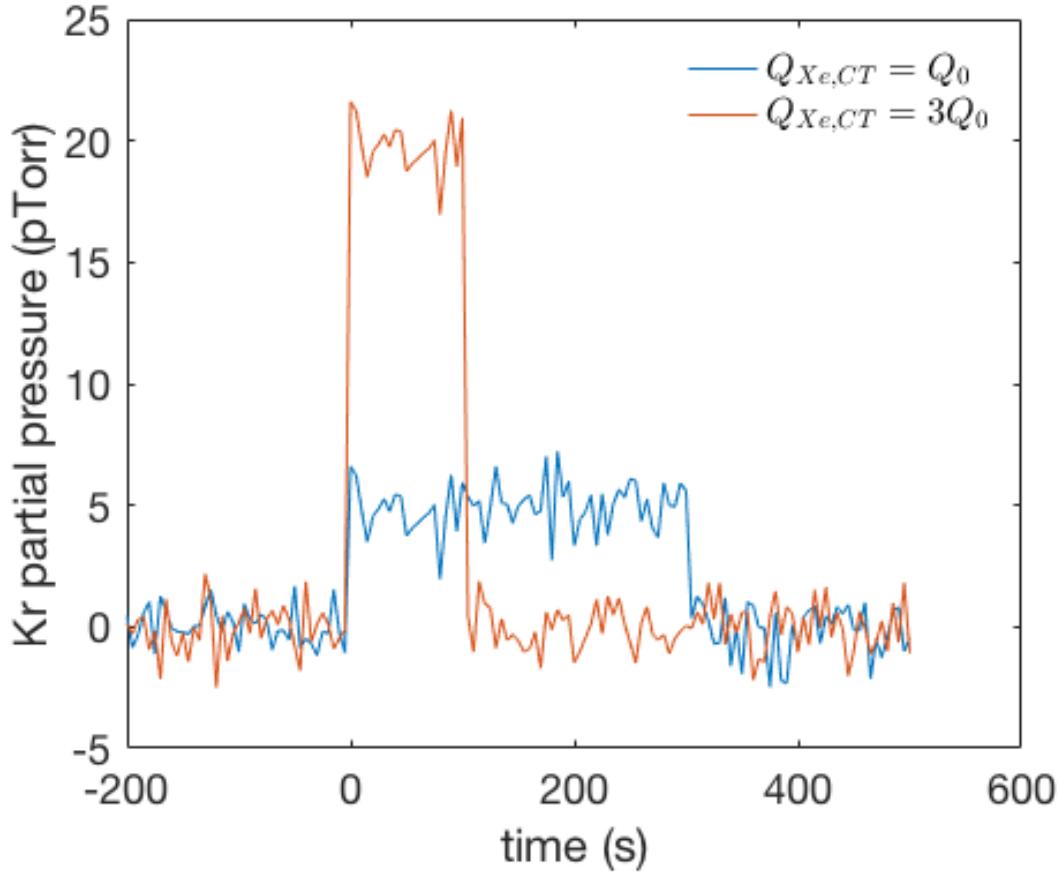


Figure 3.27: Peak krypton RGA pressure as a function of flow rate.

The dependence of our idealized signal-to-noise on $\sqrt{Q_{Xe,CT}}$ argues for the use of as

high a xenon flow rate as possible. Unfortunately, we don't live in an ideal world, and there are forces conspiring against us in the high-flow limit. In section 3.3.3 we saw that at flow rates above about 2 SLM, the krypton throughput begins to fall. This effect will compete with, and may even overwhelm the statistical benefit we get from increasing the flow rate.

We are in a similar situation with our impedance setting. We have shown in section 3.3.4 that it is possible to amplify PP_{Kr} by modifying the impedances of IV1 and IV2. Figure 3.28 show a krypton signal which is nearly buried in electronic RGA noise can be increased more than ten-fold by adjusting the impedances. This amplification is not perfect, and comes at the cost of longer rise times and decreased krypton throughput. Even with these competing effects, the krypton equilibrium pressure remains monotonically increasing in Z_1 as far as we have been able to measure.

To this point we have not yet developed a fully armed and operational model as to the physical chemistry governing the freezing of the xenon and the flow of xenon. The toy models we have developed provide some useful insights as to how to optimize the system, but significant tension with the data. In order to find the optimal settings for our cold trap system we turn instead to brute-force, empirical methods. We conduct a series of analysis-style runs at varying impedances and flow rates. The analysis procedure is standardized such that the only variables remaining are impedance and flow rate. The krypton concentration, RGA setting, and even ice-kernel formation procedure is identical for all the tests in the series. We choose an impedance setting and then scan through a series of flow rates. Once we are satisfied that we have located the optimal flow rate for that impedance, we move on to the next impedance setting.

For each setting, we conduct an integration-style analysis on the $PP_{Kr}(t)$ data to get an

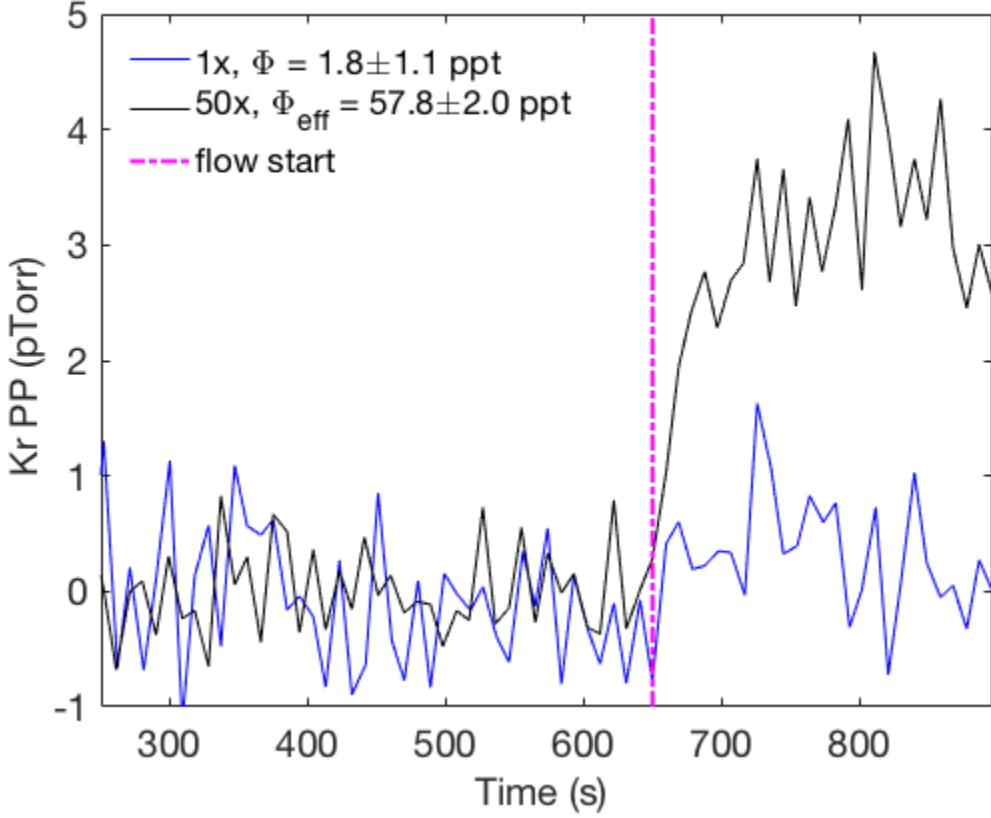


Figure 3.28: Amplification of krypton signal by increasing the impedance settings to the 50x state. Identical flow rates and xenon samples were used with the only difference being the impedance settings. Φ is the measured krypton concentration in the 1x impedance setting and corresponding calibration. Φ_{eff} is the equivalent measurement in the 50x state, using the 1x calibration number.

integrated pressure signal:

$$X_{Z,Q} = \sum_{i=1}^N (PP_{Kr,i} - \overline{PP_{Kr,0}}) \Delta t_i, \quad (3.65)$$

along with its corresponding uncertainty, $\sigma_{Z,Q}$. We use the $X_{Z,Q}$'s and $\sigma_{Z,Q}$'s to extrapolate a sensitivity, ($\phi_{sens}(Z, Q)$) for each setting:

$$\phi_{sens}(Z, Q) = \Phi_{sample} \frac{\sigma_{Z,Q}}{X_{Z,Q}}, \quad (3.66)$$

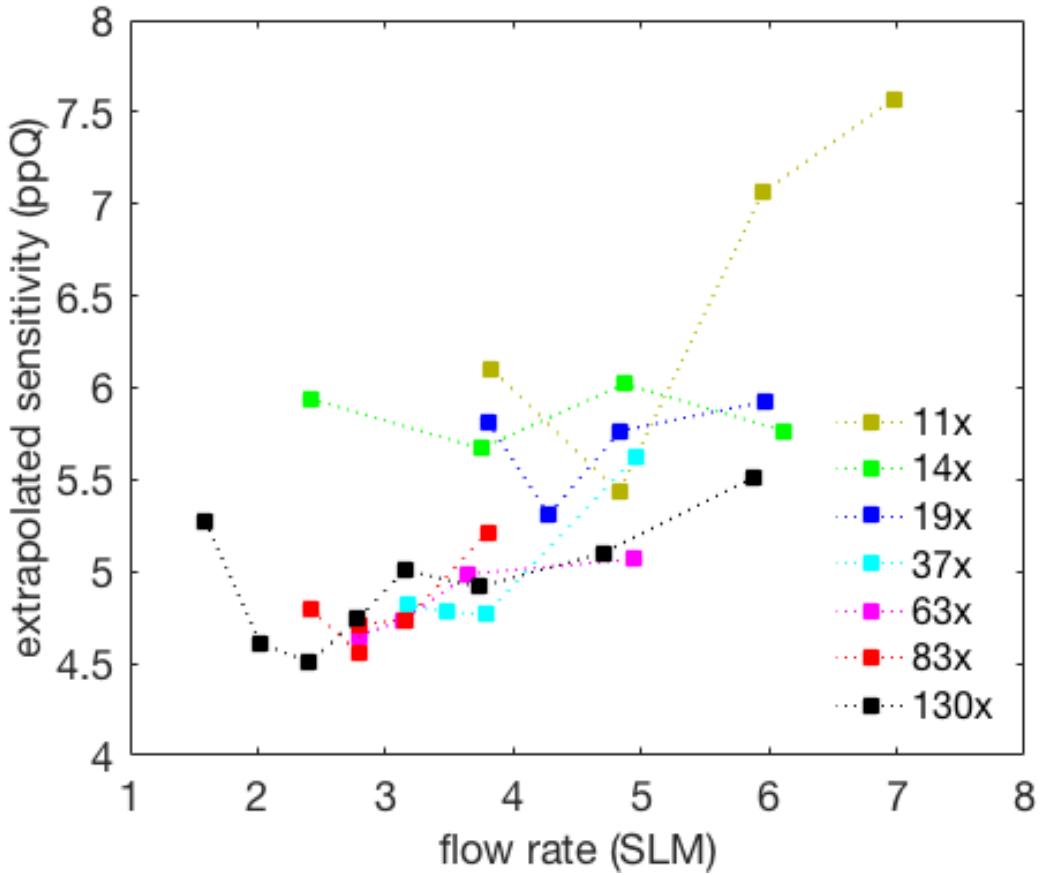


Figure 3.29: Scan across impedance and flow rate setting in search of the optimal settings.

where Φ_{sample} is the known concentration of the xenon sample.

The minimum extrapolated sensitivity we measured during this scan was 4.5 ppQ, at 130x impedance and a flow rate of 2.4 SLM. Past about 30x impedance, the we find only a small benefit in increasing the impedance. The benefit of going from 37x impedance to 130x impedance is only about a 6% drop in extrapolated sensitivity, whereas the benefit to going from 11x to 37x is a 22% drop. Additionally, the optimal settings are all in the high xenon flow regime, but the high-impedance optimizations are near the transition point. The optimal flow for the 130x impedance is only 2.5 SLM, putting it essentially on the transition point between high and low flow regimes.

For the purposes of our final system optimization, we want to set the impedance as high as possible but will not go to the full 130x for reasons of practicality. With higher set points, the impedance becomes increasingly difficult to set repeatably. This, combined with the marginal impedance dependence above the 30x set-point leads us to aim for an impedance set-point of 90x. The optimal flow rate at this impedance is between 2.5 and 3 SLM, so we use 2.5 SLM as our MFC set-point.

3.6 Preparation of Calibration Xenon

Once the system has been optimized using a largely arbitrary mixture of xenon and krypton, the next key step is to measure the response of the system to a series of mixtures referred to as calibration xenon which have well known concentrations of krypton. Once this response is known, the system can be used to measure concentrations of unknown mixtures. To this end, the preparation of a mixture of xenon and krypton with a well known concentration is essential.

The first ingredient in the preparation of this mixture is extremely pure xenon. This is obtained by using the cold trap system itself to clean a small amount of stock xenon. As was explained previously, the cold trap analysis works because all but a microscopic amount of xenon is retained by the cold trap, while gasses such as krypton pass through largely unaffected. This means that the xenon that remains in the cold trap after an analysis has significantly lower krypton content than before the analysis. Depending on the system parameters, the post-run xenon will contain as little as 1/15th the krypton as the pre-run xenon. Using the system described by figure 3.32, it takes about 3 hours to purify 100g of typical stock xenon with a concentration of 1 part in 10^9 down to < 1 part in 10^{15} ,

Once the xenon has been cleaned it is transferred to an appropriate mixing system, described by figure 3.30. The relative volumes of this system must be extremely well

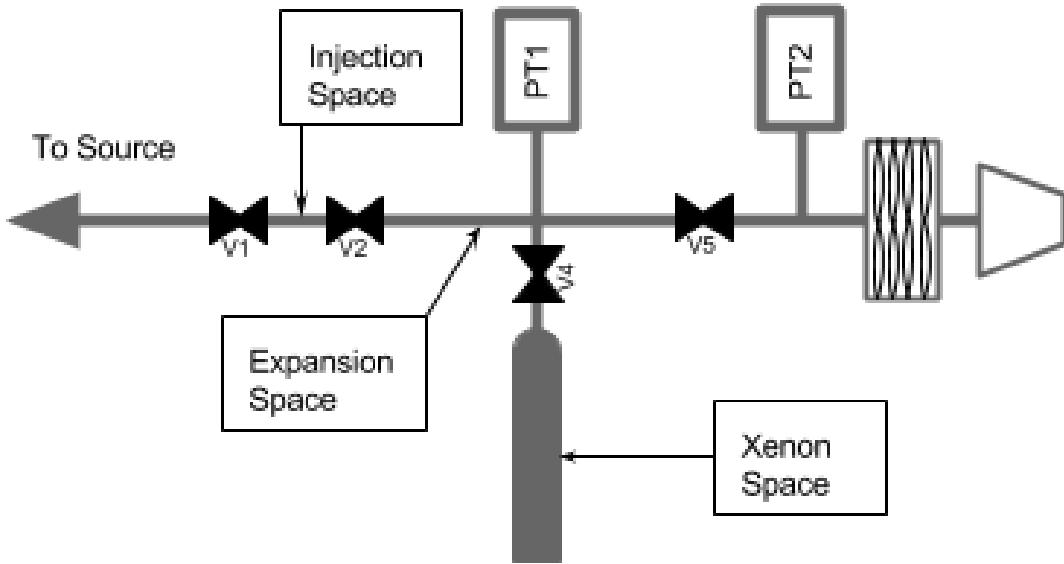


Figure 3.30: Plumbing diagram of a generalized mixing system.

known, so they are measured using volume sharing. First the full system, including injection, expansion, and xenon spaces, is filled with roughly 2000 torr of xenon as measured by pressure transducer 1. Then the expansion space is pumped to vacuum, leaving a well known pressure in both the injection and xenon spaces. Valve 4 is opened to expose the gas within the xenon space to the expansion space. The resulting pressure on PT1 gives the volume of the expansion space relative to the xenon space. Through the ideal gas law, when temperature is constant and mass is conserved, pressure times volume will remain constant:

$$P_1 V_{Xe} = P_2 (V_{Xe} + V_{inj}) \quad (3.67)$$

Therefore, the volume of the expansion space relative to the xenon space can be calculated using:

$$\frac{V_{inj}}{V_{Xe}} = \frac{P_1 - P_2}{P_2}. \quad (3.68)$$

The relative size of the injection space is then found in the same way. The absolute volumes

can be measured by expanding from the expansion space into a space with an already known volume. Typically we use Swagelok DOT-compliant sample cylinders as our xenon space. These are fabricated to have a specified volume, so we calculate the absolute volume of the expansion and injection spaces by referencing this specified volume.

To prepare the calibration xenon, the injection space is filled to some known pressure with pure krypton. The krypton is then opened to the expansion space in order to reduce the pressure, and then the expansion space is pumped out using a the turbo-pump until PT2 reads $< 1 \times 10^{-6}$ torr. This expansion is repeated until the desired krypton pressure is reached. After the final expansion volume pump-out, the xenon space is opened to the injection volume, and the new xenon/krypton mixture is frozen back into the xenon volume using liquid nitrogen. The krypton concentration (Φ_{Kr}) of the calibration xenon in grams krypton per grams xenon is given by:

$$\Phi_{Kr} = \frac{a^N P_{Kr,0} V_{inj} \rho_{Kr}}{P_{Xe} V_{Xe} \rho_{Xe}}, \quad (3.69)$$

where the expansion ratio, a , is given by $V_{inj}/(V_{inj} + V_{expansion})$, N is the number of expansions, $P_{Kr,0}$ and P_{Xe} are the krypton and xenon pressures initially injected into the system, and $\rho_{Kr} = 3.4692$ g/liter and $\rho_{Xe} = 5.4535$ g/liter are the krypton and xenon gas densities.[53]

Except for the densities, which are assumed to be exact, the pressures and volumes usually have comparable fractional uncertainties, with the exception of V_{inj} , which will be slightly dominant. After a few expansions this dominance becomes more pronounced. If we keep in mind the definition of a from above, we find the following expression for the

uncertainty on Φ_{Kr} :

$$\sigma_\Phi^2 = \Phi_{Kr}^2 \left[\left((N+1) \frac{\sigma_{V_{inj}}}{V_{inj}} \right)^2 + \left(N \frac{\sigma_{V_{exp}}}{V_{exp}} \right)^2 + \left(\frac{\sigma_{P_{Kr}}}{P_{Kr}} \right)^2 + \left(\frac{\sigma_{P_{Xe}}}{P_{Xe}} \right)^2 + \left(\frac{\sigma_{V_{Xe}}}{V_{Xe}} \right)^2 \right]. \quad (3.70)$$

This expression is not a perfect estimation of the error on the uncertainty. Typically either V_{inj} will be used to measure V_{exp} , or vice versa. To incorporate the effects of correlated uncertainties, we can run the calculations for volume measurements and concentrations many times, randomly varying the pressure measurements and reference volume according to their respective uncertainties.

The final injection pressure must be kept above 0.01 torr to ensure the krypton remains above the molecular flow regime. This sets a lower limit on the concentration of calibration xenon that can be produced through this method. With an injection volume of 5cc and a xenon volume of 4000cc, the lowest concentration than can be produced from pure krypton is about 5 ppB. In order to produce calibration xenon with smaller concentrations, the pure krypton is replaced with the ppB level calibration xenon, which is diluted into clean xenon through the same process outlined in the previous paragraph.

3.7 Sensitivity Demonstration at SLAC

With our system optimized to the best of our ability, we predict that we will be able to measure krypton contamination in a xenon sample of roughly 5 ppQ gram per gram. Our procedure will utilize the results from all of our optimization studies. The RGA CDEM voltage was set such that the highest xenon peaks were saturating the data collection, and the doubly ionized ^{124}Xe peak was reading 2300 pTorr. For our setup, this was 1750 Volts. The xenon flow rate used was 2.5 SLM, and the impedance was set to 90x. We used the modified technique of forming the ice kernel, using only 50 standard cc and forming the

kernel prior to fully submerging the trap in the LN bath. This technique was described in section 3.3.2.

For all of the tests in this demonstration we used a single sample of xenon. To initially prepare this sample, we filled our 4073 ± 5 cc sample volume (the green section in figure 3.26) with 2720 ± 14 Torr of xenon. Using the method described in section 3.6, we cleaned this xenon to the point where were no longer able to detect krypton. Into this clean xenon we mixed very small amounts of xenon which was previously-prepared with 274 ppB “cocktail xenon”. After every analysis run, we would refreeze this xenon into SB, and then do whatever combination of cleaning and mixing was necessary to prepare for the next desired test.

3.7.1 Blank Runs

We analyze the RGA data from the 84 amu peak ($PP_{Kr,i}$) according to equation 3.60, leaving off the constant term:

$$X = \sum_{\text{flow start}+20\text{sec}}^{\text{flow stop}} (PP_{Kr,i} - \overline{PP_{Kr,0}}) \Delta t_i. \quad (3.71)$$

The error propagation for this is:

$$\sigma_X^2 = \sum_{\text{flow start}+20\text{sec}}^{\text{flow stop}} (\sigma_i^2 + \sigma_0^2/N_B) \Delta t_i^2, \quad (3.72)$$

where σ_i is defined by equation 3.61. As before, $\overline{PP_{Kr,0}}$ is the average of the RGA readings at 84 amu prior to starting flow, σ_0 is the standard deviation of these points, and N_B is the number of these points used. We will only include the data in the closed time interval starting 20 seconds after flow was started and ending at the time the flow stopped. This X will be the figure of merit we use in establishing our limit of sensitivity. We will measure X

for a series of prepared concentrations of xenon, Φ . If our system is working as predicted, the data (Φ, X) will fit to a line with a slope equal to $F_{Q,t_1,t_2} C$.

Before demonstrating that the system is capable of a positive measurement, we first show that it is capable of measuring 0 ppQ. To do this we start with our newly cleaned xenon, and run a series of “blank” measurements in which we do not mix krypton into the xenon. The values of X in these blank runs should fluctuate around 0 $pTorr \cdot s$, although there may be some offset due to RGA baseline issues. Our measurements bear this out. We ran 15 blank runs. The average value of X for these runs was 10 pTorr seconds, and the standard deviation was 31 pTorr seconds. The average uncertainty on these points is $\sigma_X = 26.2 \pm 0.8$ pTorr seconds.

There was one significant outlier in our blank data which had a value of 118 ± 35 pTorr seconds. We decided not to use this datapoint because the RGA baseline was acting up and had a clear periodicity. We made sure that our other measurements were taken on top of an unvarying baseline.

3.7.2 Mixing of ppQ Level Samples

The previously mentioned 274 ppB cocktail xenon⁷ was prepared using a separate system at the University of Maryland. The volumes of this system were measured by volume sharing as described in section 3.6. The pressure gauge used was an MKS Baratron 722b capacitance manometer. The accuracy of the 722b pressure gauge is 0.5% of the reading. We also observe a constant zero offset of the gauge to be 0.8 ± 0.5 Torr which will be subtracted from the pressure readings. The absolute reference volume was a 500cc Swagelok DOT-compliant sample cylinder. The output of this bottle was modified to accommodate a 1/4 inch VCR B-series bellows valve. We take the volume of this space to be 500 ± 10 cc. This reference volume doubled as the xenon space.

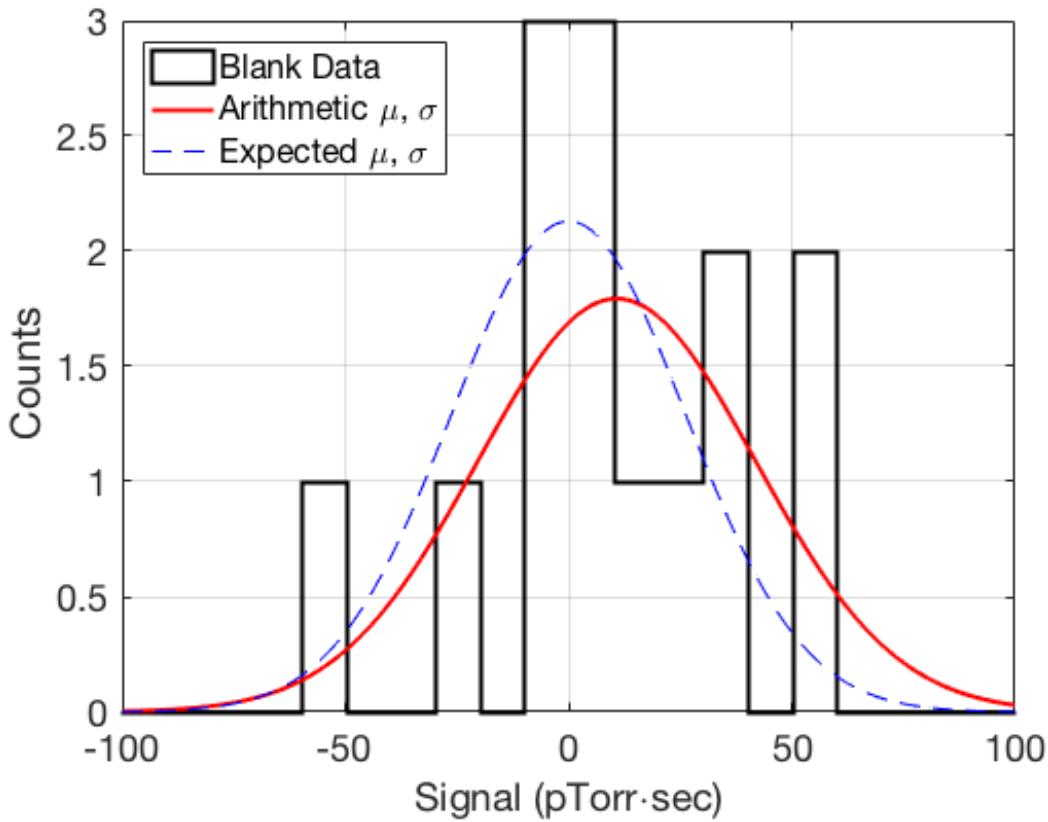


Figure 3.31: Histogram of measurements of xenon which has < 1 ppQ of krypton.

The volume of the injection space was measured to be 16.00 ± 0.25 cc. The expansion ratio is $a = 0.0261 \pm 0.0008$. The starting xenon pressure was 841 ± 4 Torr in the 500cc xenon space. We injected an initial krypton pressure of 638 ± 3 Torr in the injection space. We expanded three times before mixing it with the xenon yielding a mixture with 276 ± 25 ppB (g Kr)/(g Xe).

The second-order mixings to dilute the 276 ppB cocktail xenon were done in-situ in the SLAC system. The SLAC sampling system is diagramed in figure 3.32. The blue boxes and corresponding arrows indicate the various isolated spaces in the system, the volumes for which are listed in table ???. The spaces of interest for mixing are spaces 1, 3, 4, 5, 6, and 7. The cocktail xenon is stored in space 6, the clean xenon is held in spaces 1, and the

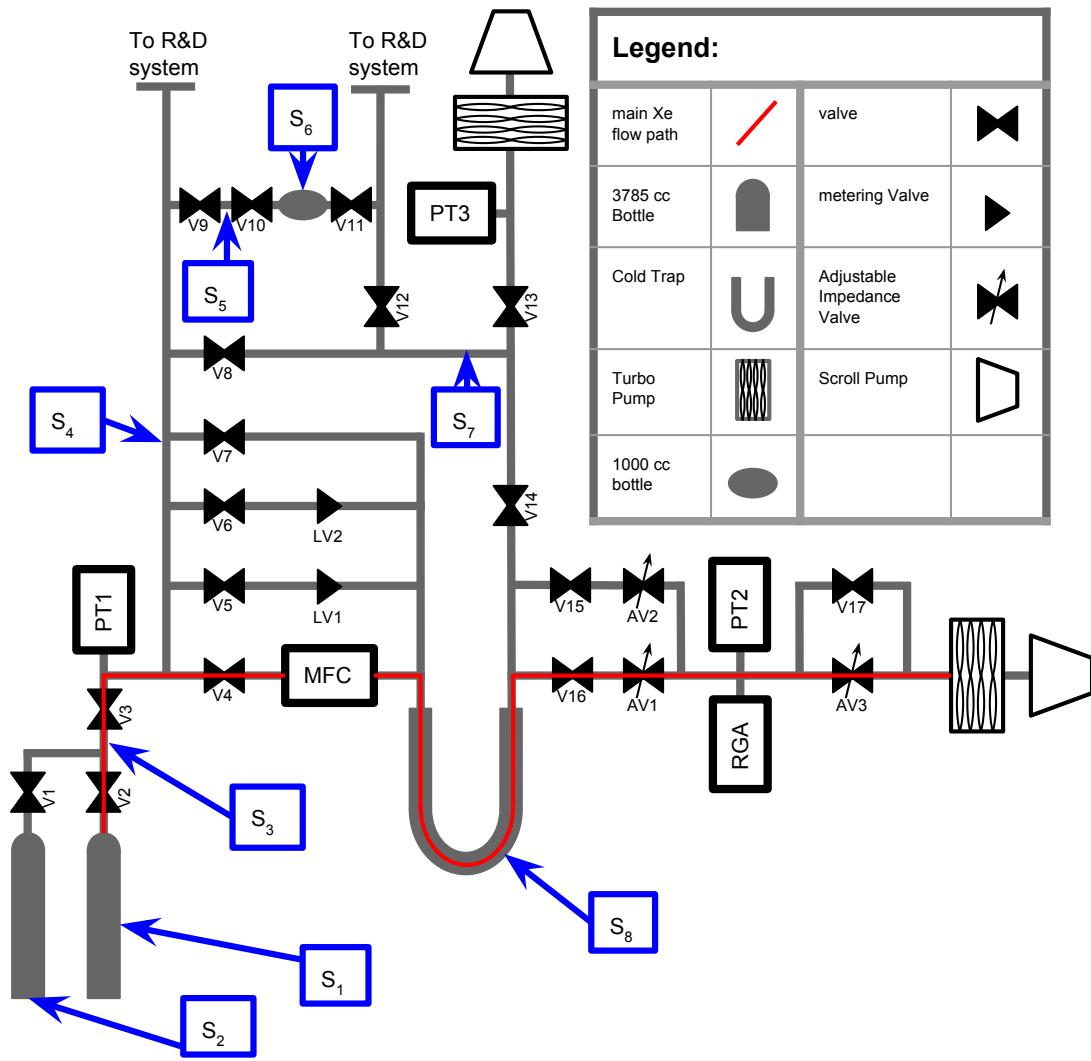


Figure 3.32: P&ID of the SLAC sampling system.

injection volume is space 5. As our primary expansion volume we used space 4 and used spaces 7 and 3 to increase the volume as needed.

The cocktail xenon was initially at a pressure of 128.0 ± 0.6 Torr. Since we do not have a pressure gauge on space 6, every time we volume share with the injection volume, we calculate the new pressure contained in space 6. This calculation is simply the old pressure multiplied by the volume ratio $(4.9 \text{ cc})/(4.9 \text{ cc}+1000 \text{ cc})=0.0049$.

The procedure for mixing follows the same outline as in section 3.6. We select a desired

Space #	Volume (cc)	\pm (cc)
1	3864	10
2	3837	10
3	23.9	1.4
4	186.3	1.9
5	4.92	0.09
6	1000	5
7	93.8	1.6
8	221.0	4.9

Table 3.2: List of SLAC system volumes. Refer to figure 3.32 for descriptions of spaces.

Φ (ppQ)	\pm (ppQ)	Expansion Spaces	N_{exp}	N_{inj}	P_{inj} (Torr)
4.92	0.49	5+7	2	1	128
4.90	0.49	5+7	2	1	127.4
10.8	1.1	5	2	1	126.8
21.6	2.2	5	2	2	126.3,125.8
46.1	4.9	(5),(5+3)	1,1	1*	125.2
10.7	1.1	5	2	1	124.6
255	24	5+7+3	1	1	124.0

Table 3.3: Parameters of the sample concentrations used to demonstrate the sensitivity of the SLAC system. The indicated uncertainties do not include the 7% systematic uncertainty from the cocktail xenon concentration.

sample concentration (Φ_{Kr}), choose the appropriate expansion space (V_{exp}), expand the required number of times (N_{exp}), and then mix the remaining cocktail xenon into the clean sample xenon. The resulting concentration will be given by:

$$\Phi_{Kr} = \frac{(274 \text{ ppB}) \cdot (4.9 \text{ cc}) \cdot P_{inj}}{(4073 \text{ cc}) \cdot (2720 \text{ Torr})} \left(\frac{4.9 \text{ cc}}{4.9 \text{ cc} + V_{exp}} \right)^{N_{exp}} \quad (3.73)$$

The actual values used in the preparation of our ppQ level samples are listed in table ???. The total expansion volume will be equal to the sum of volumes indicated in the “Expansion Spaces” column. There are two samples with slightly altered mixing procedures. The 21.6 ppQ sample was prepared by completing two consecutive injections using the same mixing parameters in order to approximately double the previous 10.3 ppQ concentration. The

46.1 ppQ sample was prepared in a slightly more complex way. We first filled the injection volume (space 5) and expanded once into space 4 as usual. However, after pumping out the expanded cocktail xenon in space 4, we expanded into both space 4 and space 3. We then pumped out spaces 4 and 5, and mixed our clean sample xenon with the cocktail xenon that had expanded into space 3. The calculation for this concentration is then:

$$\Phi_{Kr} = \frac{(274 \text{ ppB}) \cdot (24.4 \text{ cc}) \cdot (125.2 \text{ Torr})}{(4073 \text{ cc}) \cdot (2720 \text{ Torr})} \frac{4.9 \text{ cc}}{189.2 \text{ cc}} \frac{4.9 \text{ cc}}{213.6 \text{ cc}} \quad (3.74)$$

3.7.3 Measurements of ppQ Level Samples

With the measurability of 0 established, and low-concentration xenon samples in hand, we move to measure the sensitivity limit of the SLAC sampling system. To do this we first measure X as described in equation 3.71 for each of the samples listed in table ??, and then fit a line to the set of (Φ_{Kr}, X) . The data and best-fit line are shown in figure 3.33. The slope of the best fit line is 10.1 ± 1.4 pTorr seconds/ ppQ, and the intercept is 22 ± 12 pTorr seconds.

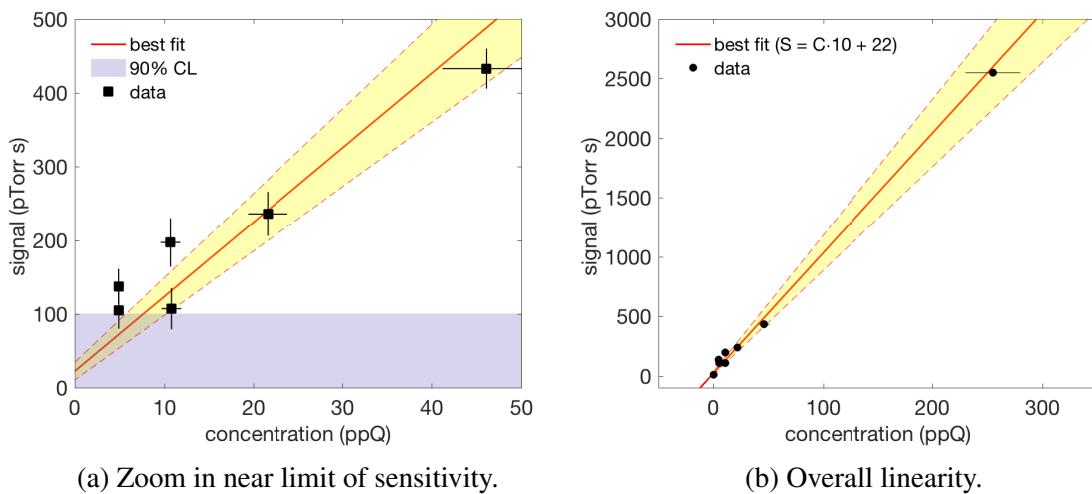


Figure 3.33:

The limit of sensitivity will be defined as the concentration at which 90% of analyses will produce results greater than $1-\sigma$ above a 0 ppQ measurement. Our 0 ppQ measurements have a signal of 10 ± 31 pTorr seconds. The lowest-concentration measurements (< 30 ppQ) deviate off of the best fit line by 46 pTorr seconds, so the 90% confidence limit at any concentration will be 59 pTorr below the best fit line. Putting this together, we are looking for the concentration at which the best fit line drops crosses 100 pTorr seconds. This puts our limit of sensitivity at 7.7 ± 2.0 ppQ.

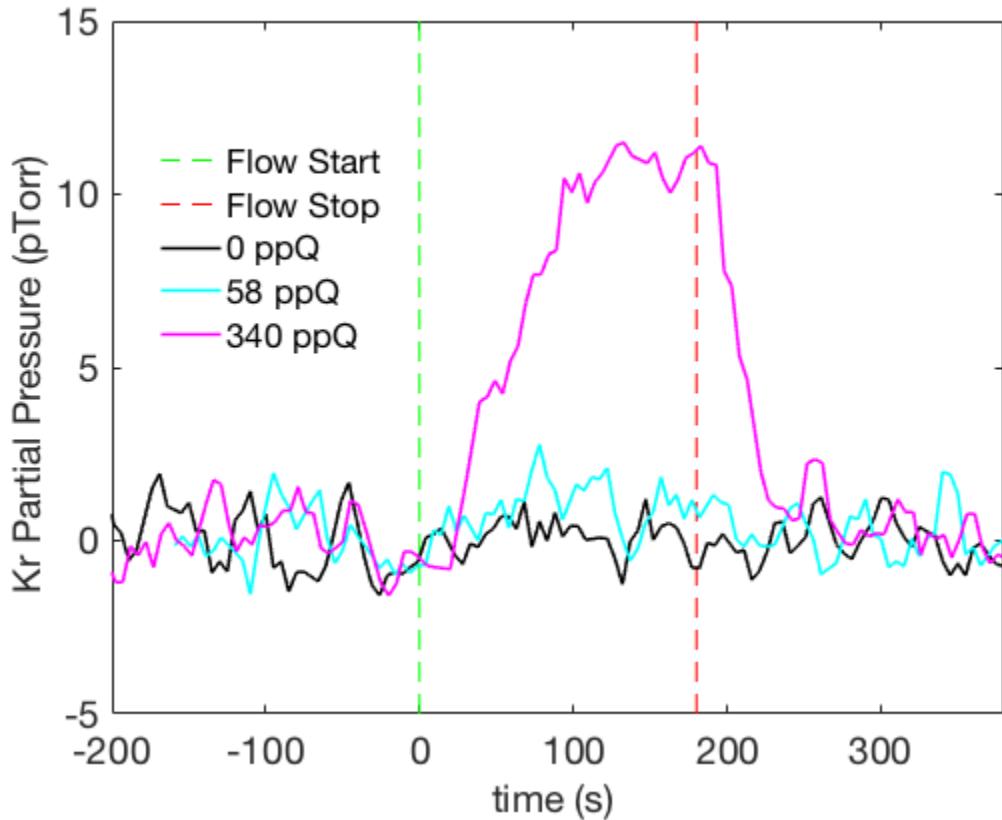


Figure 3.34: Krypton pressure vs time traces near the limit of sensitivity.

Chapter 4: LUX Post-Run 04 Calibration Campaign

After the LUX Run4 WIMP-search was completed in June of 2016, the response of the detector was exercised using ER and NR calibration sources. The usual ER calibrations of krypton-83m[48, 49] and tritiated methane (CH_3T)[8] were performed, along with NR calibrations using the deuterium-deuterium (DD) neutron generator[7, 77]. In addition to these standard calibrations, there were additional techniques and sources used which were novel to the LUX detector.

The first novel calibration performed was a modification to the DD NR calibration. The rest of these new calibrations were to the ER response and will be the primary focus of this chapter, but we will pause here briefly to discuss the DD calibrations. The NR response of the LUX detector was measured using a beam of neutrons which was directed into the cryostat. These neutrons were generated using a commercially available DD generator,

Source	Date	$\tau_{1/2}$ (days)	Energy (keV)	Rate (Hz)
DD	-8/7, 8/22-8/23	-	(<355)	-
Kr-83m	8/2, 8/8, 8/10, 8/17, 8/25, 8/31	0.076	41.5	130
Xe-131m	8/9	12	163.9	10
CH_3T	8/18	0.3	0-18.1	50
$^{14}\text{CH}_4$	8/23	0.3	0-156	100
Rn-220	8/27, 8/29	0.3		50
Ar-37	8/31	0.3	35	70

Table 4.1: Table of sources which were used during the post-Run04 calibration campaign.

and were collimated using a gas filled conduit which was suspended in the water tank. Because the neutrons entering the detector have a known energy and direction, it is then possible to calculate the precise recoil energy of a neutron from the beam scattering off of a xenon nucleus, assuming the scattering angle is known. The calculation is the same for neutron-nucleus scattering as for WIMP-nucleus scattering:

$$E_R = \frac{E_n r}{2} [1 - \cos(\theta)], \quad (4.1)$$

where θ is the scattering angle in the center of mass frame, and $r = 4M_A M_n / (M_A + M_n)^2$. The scattering angle in the lab frame can be easily measured for events where the scattered neutron interacts with a second xenon atom before exiting the detector, and for large nuclei such as xenon, the approximation $\theta_{CM} \approx \theta_{LF}$ can be made. The result of this procedure is a continuous NR recoil spectrum where the energy of each event is precisely known. These events will be located along the beam line, so will all be at roughly the same drift time. By moving the conduit up and down, the detector NR response as a function of drift time can be mapped out[7, 77].

The novel modification to the DD calibration in the post-run 04 campaign was to first scatter the neutrons off of a D₂O target before sending them into the conduit. The only neutrons of a single, known, scattering angle will pass through the conduit, so this procedure effectively converts the 2.45 MeV mono-energetic neutron source to a 272 keV mono-energetic neutron source. The main portion of the post-Run4 DD campaign ended on August 7th, although there was a final brief period of testing between August 22nd and 23rd[77].

On August 9th, ^{131m}Xe became the first of the non-standard, post-Run4 ER sources to be injected. Xenon-131m is a gamma-emitter with an energy of 163.93 keV and a half life of 11.84 days.[2]. The xenon-131m was collected from an iodine-131 pill in an otherwise

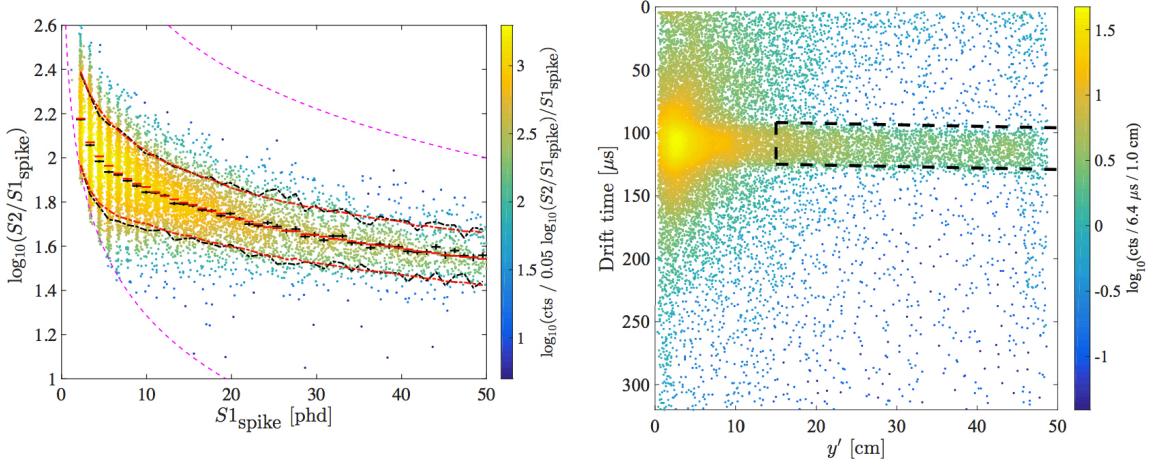


Figure 4.1: Plots of the measured neutron beam line (left) and the NR recoil band (right) from a previous LUX D-D calibration. The y' coordinate in the beam line plot is a transformation of the standard LUX x and y coordinates, such that it measures the horizontal distance along the beam line. The NR recoil band plot shows the continuous nature of the recoil spectrum. Figures taken from [7]

empty stainless steel bottle and was injected using the tritium injection described in [8]. The 12 day half life of this source meant that all subsequent sources in the month long campaign have the ^{131m}Xe line as a background. The ^{131m}Xe line is sufficiently separated in energy from most of the other sources, so that this background will not have a significant effect. However, the ^{131m}Xe line is only 8 keV above the ^{14}C Q value of 156 keV and so obscures the highest-energy portion of the ^{14}C beta spectrum. This has two major effects on our analysis of the carbon-14 data. First, it limits us from probing the energy deposition properties of liquid xenon near the endpoint of the spectrum, and second, it provides an extremely useful reference point which can be used in energy calibration, efficiency corrections, and characterization of detector pathologies.

The tritium calibration was started on the 18th, and the second new ER source, ^{14}C was injected five days later on the 23rd. Both of these sources rely on the injection of radio-labelled methane and are purified out by the LUX getter with a time constant of about 10 hours. This means that the tritium will have been reduced by about 12 e-folds, or a factor of 150,000, by the time the ^{14}C was injected. Since the amount of tritium events in this

injection was about 1 million, there should be an overlap of <10 events in the ^{14}C injection.

The next source injected was radon-220. There were two injections, each with peak activity of about 50 Hz on the 27th and 29th. Radon-220 is part of the thoron-232 decay chain, which ends with the stable lead-208. The transition time from ^{220}Rn to ^{208}Pb is dominated by the β^- decay of ^{212}Pb to ^{212}Bi , which has a half life of about 10.6 hours.

A 70 Hz injection of ^{37}Ar took place on the 31st, about 3 days after the second radon-220 injection. This meant that there was about 1 Hz of ^{212}Pb remaining in the detector. The most common and most energetic ^{37}Ar decay will deposit 2.8 keV into the xenon via x-ray. The low energy of the decay means that the ^{37}Ar events will be well separated from the MeV-level alphas and betas of ^{212}Pb and its daughters. The high rate and 35 day half life of the injected ^{37}Ar meant that this was the final injection performed in the post-Run4 campaign, and was in fact the last physics data collected by the LUX detectors.

The rest of this chapter will focus on the ^{131m}Xe , ^{37}Ar , and ^{14}C sources. We will also present a review ^{83m}Kr and ^3H . This particular suite of sources is exciting in the fact that it includes two continuous beta spectra, which can be used to map out xenon ER yields from 140 keV down to threshold, as well as three ER lines that can be used to correct for position dependent detector efficiency and examine systematic pathologies.

4.1 Data Selection

There were several preliminary data selection cuts applied to isolate the ^{37}Ar K-capture, ^{131m}Xe , ^{83m}Kr , ^3H , and ^{14}C events. The time interval which these events were drawn from is August 17th until September 3rd. In figure 4.2 this corresponds to the third krypton injection at T=16.6 days, until the end of data taking. The periods of DD generator and ^{220}Rn activity were excluded (from T=21.4 to 22.3 days and T= 26.8 to 30.5 days, respectively). There was also a period of time after the ^{14}C calibration, from T=24.5 to 26.8 days, where

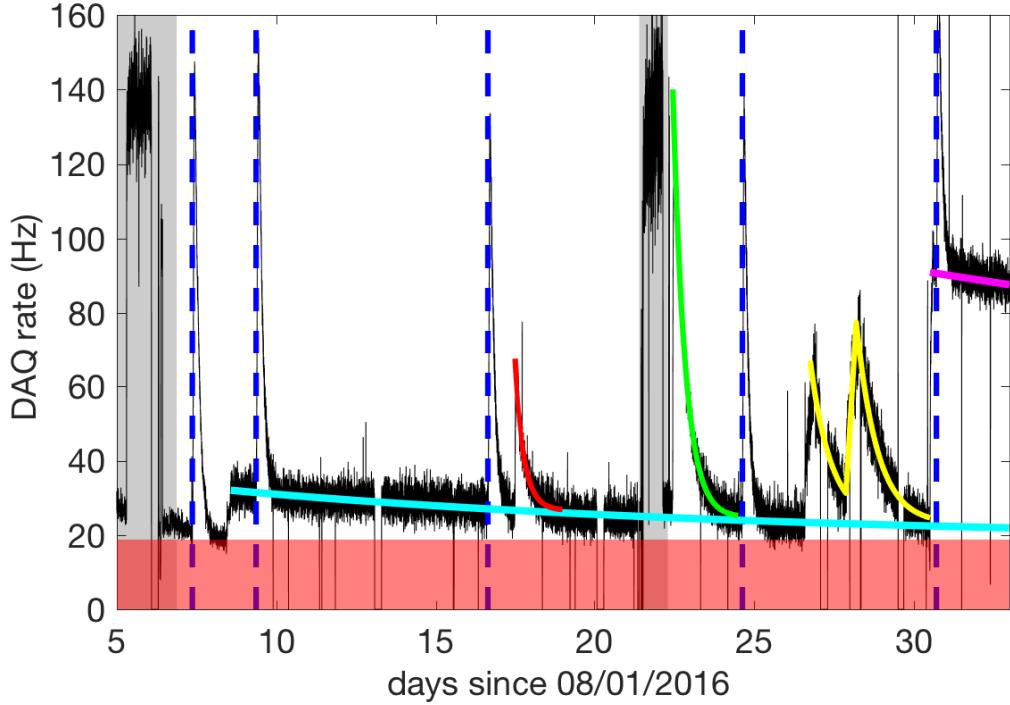


Figure 4.2: The black line shows the DAQ rate for the post-run04 injection campaign. The red shaded region shows the constant baseline, while the grey shaded regions show the DD NR-calibration campaign. The vertical dashed blue lines show the times of standard $^{83}\text{Kr}_m$ injections. The cyan, red, green, yellow, and magenta lines trace the ^{131m}Xe , ^3H , ^{14}C , ^{220}Rn , and ^{37}Ar activities, respectively.

one of the PMT's was misbehaving. This time period, which included the fourth krypton injection, was also rejected.

4.1.1 Single-Scatter Cut

The fully processed LUX data is organized into events. These events span a 500 microsecond window on either side of an initial trigger and is subdivided into ten “pulses” which are categorized as S1, S2, single-liquid-electron, single-photoelectron, or other. We would like to make a selection cut on single scatter events; events in which there is exactly one interaction within the detector which is located at a point position. The simplest cut one can make to this end is to keep only those events which contain exactly one S1, which

is followed by exactly one S2. This cut, however, turns out to have an energy dependence, especially above 100 keV, which will alter the shape of our continuous spectra.

We can quantify this energy dependence by looking at the Xe-131m peak. A cut on single-S1 events will only accept about 77% of Xe-131m events, while a cut on single-S2 will accept only about 68%. Combining these cuts forms a naive single scatter cut, and accepts only about 61% of the xenon-131m events. Conversely, the single scatter cut for carbon-14 events from threshold up to about 50 keV has greater than 90% acceptance.

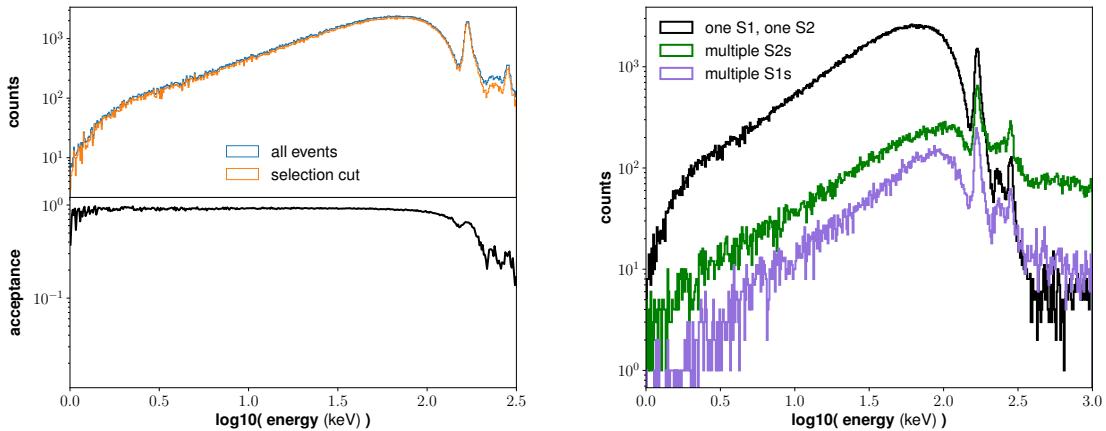


Figure 4.3: Visualization of the energy dependence of a single-scatter cut on carbon-14 and Xe-131m events. The loss of such a cut quickly rises above about 50 keV, to the point where there is less than 10% acceptance above about 500 keV.

The loss of acceptance at higher energy is largely dominated by the same pathology that is thought to cause S2 tails, which will be discussed in a later section. Electron trains are extended streams of electrons which are extracted from the liquid surface, persisting for millisecond time-scales. These trains seem to be seeded by S2s, and have a larger effect on higher-energy events. When an electron train is large enough, several of these electrons can pile up in a single pulse causing it to be classified as an S2. These secondary S2s will cause the event to fail the single scatter cut, and since the high-rate tails are more

likely at higher energy, this will introduce an energy-dependence to the single-scatter cut.

For these reasons, we developed a more nuanced cut that allows for any number of S1s and S2s to be present. We first enforce the condition that there is at least one S1 before the first S2. We then cut on the ratio of the area of the first S2 to the sum of all of the S2 areas contained in the event. The idea is that we want the first S2 to contain greater than 93% of the total S2 area, while allowing for subsequent smaller S2s to be present. We apply the cut to the S1s, however we only include S1s that occur before the first S2 in our total area sum.

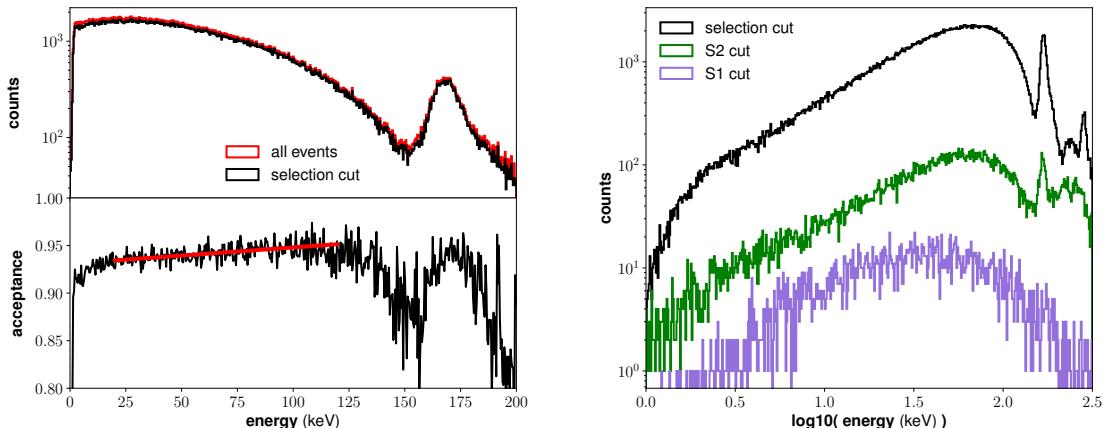


Figure 4.4: Visualization of the modified single scatter cut. This cut has a significantly better acceptance than the 1-S1, 1-S2 cut shown in figure 4.3. The acceptance of Xe131 events has been improved from 61% to about 92%. Similarly the acceptance for C-14 events is greater than 90% across the entire energy range. There is a slight slope of 0.17 MeV^{-1} to the acceptance of C-14 events which is indicated by the red best-fit line in the lower left panel.

This cut has a significantly better acceptance than the 1-S1, 1-S2 cut. The acceptance of Xe131 events is improved from 61% to about 92%. Similarly the acceptance for C-14 events is greater than 90% across the entire energy range. There is a slight slope of 0.17 MeV^{-1} to the acceptance of C-14 events which is indicated by the red best-fit line in the lower left panel. This slope will introduce a systematic error in our measurement of the carbon-14 non-statistical shape factor, which will be described in section 5.1.3.

4.1.2 Radial Selection Cut

We would like to be able to eliminate events close to the wall from our analysis. The LUX Run4 and post-Run4 drift field was highly non-uniform in the z-coordinate, so there must be a drift time dependence added to any radial event-selection cut. There is, to a lesser degree, some non-uniformity in the radial and azimuthal directions as well. Since we would like to make a radially symmetric selection cut, we can to, first order, ignore the radial dependence. The radial cut was defined by first dividing the detector into $5\mu\text{s}$ drift time bins. Each drift time bin was re-centered around the mean S2-space x and y positions. These re-centered positions were then divided into 36 ϕ bins. We used the assumption that the argon-37 events will be distributed uniformly in radius-squared to define the cut position for each of these ϕ bins. We define $r_{cut}(dT, \phi)$ such that 77% of events in the associated bin will have $r < r_{cut}(dT, \phi)$. The true radius of this event should be $\sqrt{0.77}R_{wall} = (0.877) \cdot (25 \text{ cm}) = 21.9 \text{ cm}$. The values of $r_{cut}(dT, \phi)$ should then all be about 3 cm from the wall. We apply this cut in each drift time bin (dT_i) by performing a linear interpolation between the values of $r_{cut}(dT_i, \phi)$ and cutting out events with radii greater than the interpolated values.

4.1.3 Electric Field Selection Cut

In the next chapter, we will be interest in making measurements as a function of field. To that end, we have divided the detector into 13 electric field bins. To construct these bins, we first assign an electric field value to each event by using the SciPy “LinearNDInterpolator” tool[46] on the the field-map described in section 2.2. We select electric-field bins such that the assigned field of each event, \mathcal{E} , is within 10% of the center of some field bin,

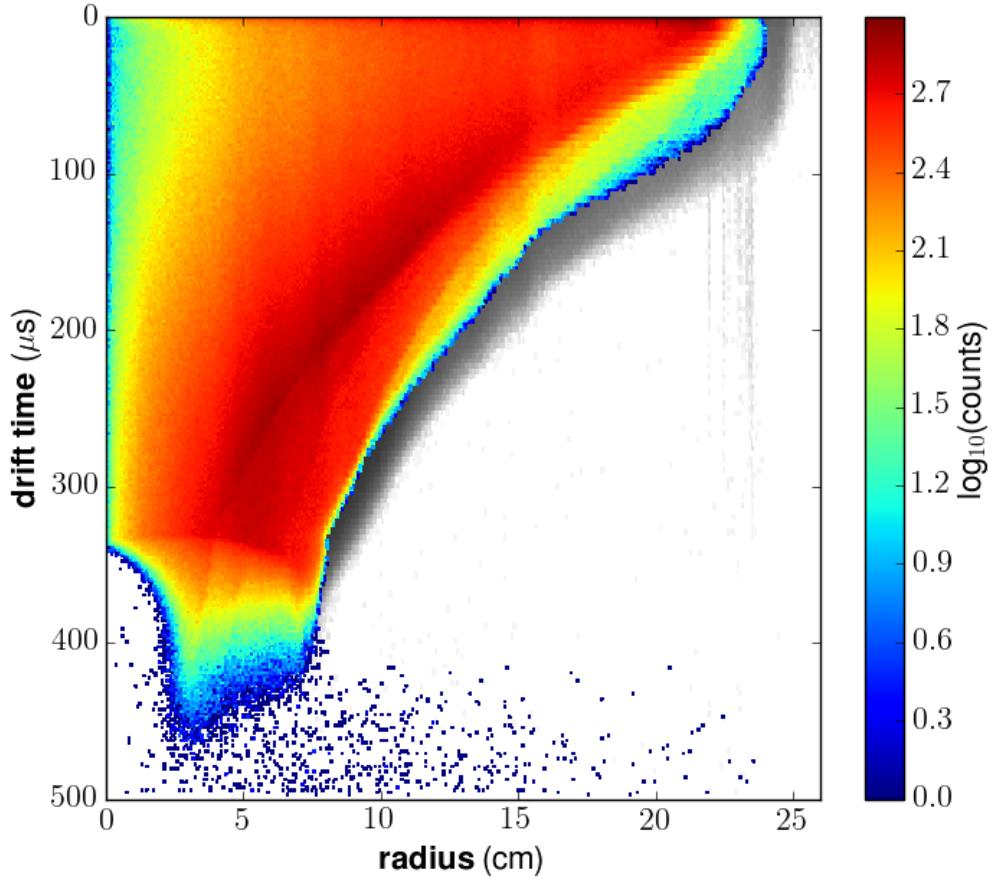


Figure 4.5: Visualization of the radial cut derived from the ^{37}Ar data. The greyscale maps show the data without any position cuts, while the overlaid heat-maps show the selected by the radial cuts.

\mathcal{E}_{ctr} . The electric field cut applied to the i^{th} bin would then be:

$$0.9 \cdot \mathcal{E}_{ctr,i} < \mathcal{E} < 1.1 \cdot \mathcal{E}_{ctr,i}. \quad (4.2)$$

For any given drift time slice there will be a wide range of mapped field values. These will be near their minimum at the center of the detector and will increase dramatically as they approach the wall. Another way of saying this is that events in a given electric field

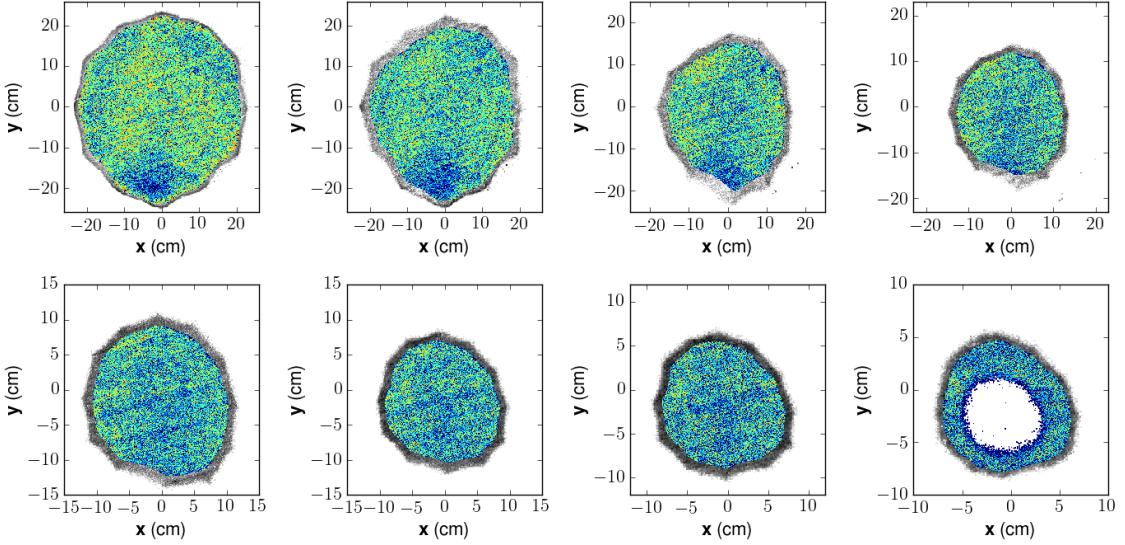


Figure 4.6: Selected $5 \mu\text{s}$ drift time slices used in the ^{37}Ar drift time section cut. The greyscale maps show the data without any position cuts, while the heat-map shows the selected by the radial cuts. From top left to bottom right, the drift time of the cuts are $20 \mu\text{s}$, $50 \mu\text{s}$, $100 \mu\text{s}$, $150 \mu\text{s}$, $200 \mu\text{s}$, $250 \mu\text{s}$, $300 \mu\text{s}$, and $350 \mu\text{s}$. The linear diagonal lines that can be seen in the heat-maps are physical features created by the grids.

slice will be drawn from a large range of drift times. We would like to limit the range of drift times that events in an electric field slice, so we institute a further cut on our electric field bins. We find the overall trend in electric field by fitting a Gaussian to the electric field distribution in a series of drift time slices. We then interpolate between these fits to find a function, $F_{dT}(\mathcal{E}_{peak})$ which gives the drift time value associated with a given peak electric field. For each i^{th} electric field bin we can now impose the following drift time cut:

$$F_{dT}(1.1 \cdot \mathcal{E}_{ctr,i}) < dT < F_{dT}(0.9 \cdot \mathcal{E}_{ctr,i}) \quad (4.3)$$

The selection of the various $\mathcal{E}_{ctr,i}$ began with the LUX Run03 average electric field of 180 V/cm. We then worked up in steps of 22.2% and down in steps of 18.8% to generate a set of non-overlapping bins that satisfied equation . We do allow different bins to overlap in

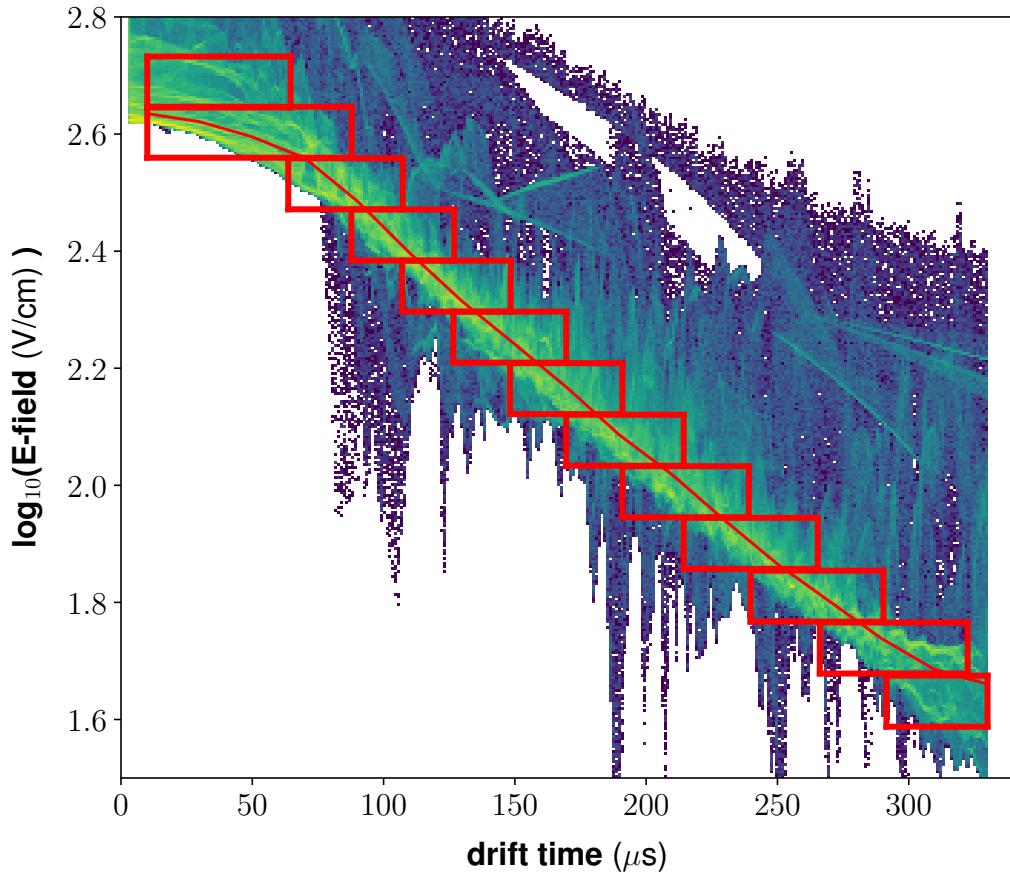


Figure 4.7: Electric field selection bins.

drift time, but the separation in field ensures that each bin is made up of an independent set of events. We did not include events above 10 microseconds or below 330 microseconds in drift time. The selected bins are shown in figure 4.7, and the selected bin centers, along with the mean field value and its standard deviation is shown in table ??.

\mathcal{E}_{ctr}	dT_{min}	dT_{max}	$\langle \mathcal{E} \rangle$	$\sigma_{\mathcal{E}}$
43	291	330	43.2	2.5
53	266	322	52.6	2.9
65	240	290	64.8	3.7
80	214	265	79.8	4.6
98	191	239	97.8	5.6
120	170	214	119.6	6.9
147	148	191	146.7	8.3
180	127	170	180	10
220	107	148	219	13
269	88	127	268	15
329	64	107	329	19
403	10	88	405	22
491	10	65	484	28

Table 4.2: Selected electric field bin centers, along with the maximum and minimum drift time allowed for each bin. Also shown is the mean and standard deviation of electric fields for events in each bin.

4.2 Argon-37 Non-Gaussianities

Argon-37 provides three useful low-energy ER calibration lines. It decays through electron capture to ^{37}Cl with a half life of 35 days. The long half life, combined with the fact that argon is chemically inert means that once injected, it will be on the order of a year before it has been sufficiently removed. That being the case, it was only injected immediately prior to LUX decommissioning[22, 44].

The ^{37}Ar source was produced through stimulated α emission of a ^{40}Ca target using a neutron beam. The ^{37}Ar sample used in LUX was produced by irradiating an aqueous solution of CaCl_2 with neutrons from an AmBe source. The gas above this solution was then collected and purified to obtain the gaseous sample of ^{37}Ar [22]. This sample was injected into the LUX xenon circulation using the same system as the ^{83m}Kr calibrations[49].

The three lines in the ^{37}Ar decay are from the capture K-shell, L-shell, and M-shell electrons. The different captures have branching ratios of 0.9, 0.09, and 0.009 and will

deposit x-rays with energies of 2.8224 keV, 0.2702 keV, and 0.0175 keV, respectively. The L-shell and M-shell captures are below the LUX threshold and so are of limited use to the work presented in this document. The K-capture x-ray will produce about 76 scintillation electrons, which will produce an S1 signal of about 6.7 phd. This is a small enough signal that there will be some non-Gaussian distortion in the S1 spectrum due to threshold effects. The charge yield for the K-capture is about 50 electrons/keV. With a 70% extraction efficiency, there will be about 100 electrons extracted from an argon-37 event, which would produce an S2 of roughly 2500 phd assuming a single electron size of 25 phd. This is large enough that the S2 spectrum should be free of threshold effects.

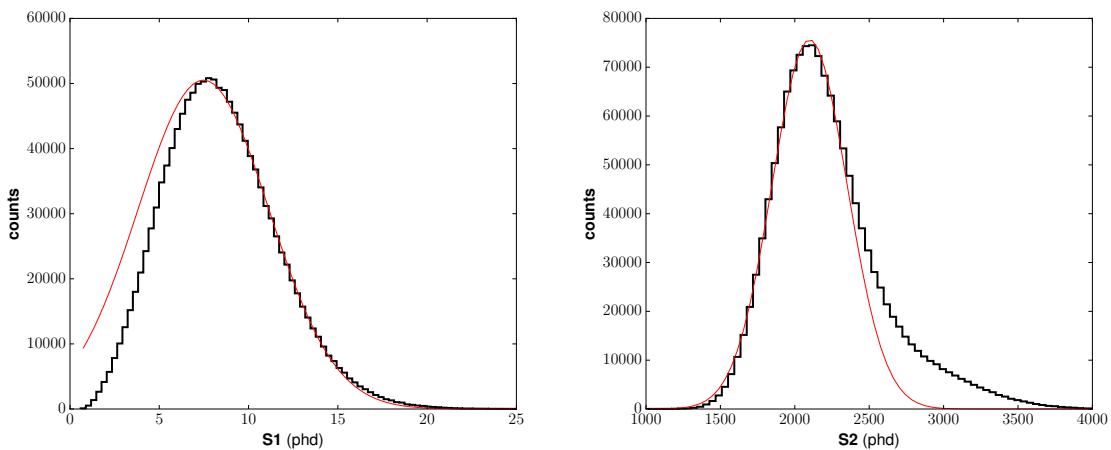


Figure 4.8: The S1 and S2 spectra for the LUX ^{37}Ar injection (black histograms), along with gaussian fits (red lines). Events with drift times between 105 and 170 μs . The S1 spectrum clearly does not behave like a gaussian on the low energy side of the spectrum. The S2 spectrum does have a gaussian shape up until about 1σ above the mean at which point a pathological tail takes over. These S2 tails are a known issue and will be characterized in a later section.

The high rate and long lifetime of the argon-37 injection also meant that there was a huge number of events. From the injection on August 31st until the end of data-taking on September 3rd there were about 8.8 million argon-37 events. The fact that we have such a high-statistics dataset, combined with the spatially uniform nature of injection sources means that we can very finely probe the position-dependence of the detector response.

This feature will be used to measure the S2 efficiency corrections and in defining our radial cut.

4.3 Signal Corrections fo Post-Run04 Data

4.3.1 S2 Efficiency Correction from ^{37}Ar

In Run4, the position-dependent efficiency corrections for the LUX S1 and S2 signals were obtained from a combination of tritium and ^{83m}Kr calibration data. This method which was described in section 2.3, relies, in part, on the fact that the S2 yields for small energy deposits have a minimal dependence on electric field. The first step in the KrypCal procedure is to measure the position dependence of the tritium peak S2 value. In order to derive the detector efficiency part of the position dependence, the field effect must first be removed. This field dependence is itself dependent on the energy of the events that contribute to the S2 peak. Since tritium is a beta spectrum, events with many energies will contribute to this peak, so an approximation is made that all of these events occur at 2.5 keV.

It is here that we see a huge benefit in using the ^{37}Ar K-capture peak instead of the tritium beta spectrum in deriving the S2. Because ^{37}Ar is a mono-energetic line source rather than a continuous beta spectrum, we know that all of the events making up the S2 peak will come from a 2.8224 keV event, and no assumption or approximation need be made.

The first step is to divide the detector into bins of 10 microseconds. We set the highest drift time bin edge to be at 5 microseconds, which is the approximate position of the gate grid. The lowest bin edge is set to 485 microseconds, although our analysis will only include events above 330 microseconds in drift time, which corresponds to the bottom of the detector at $x=y=0$ cm.

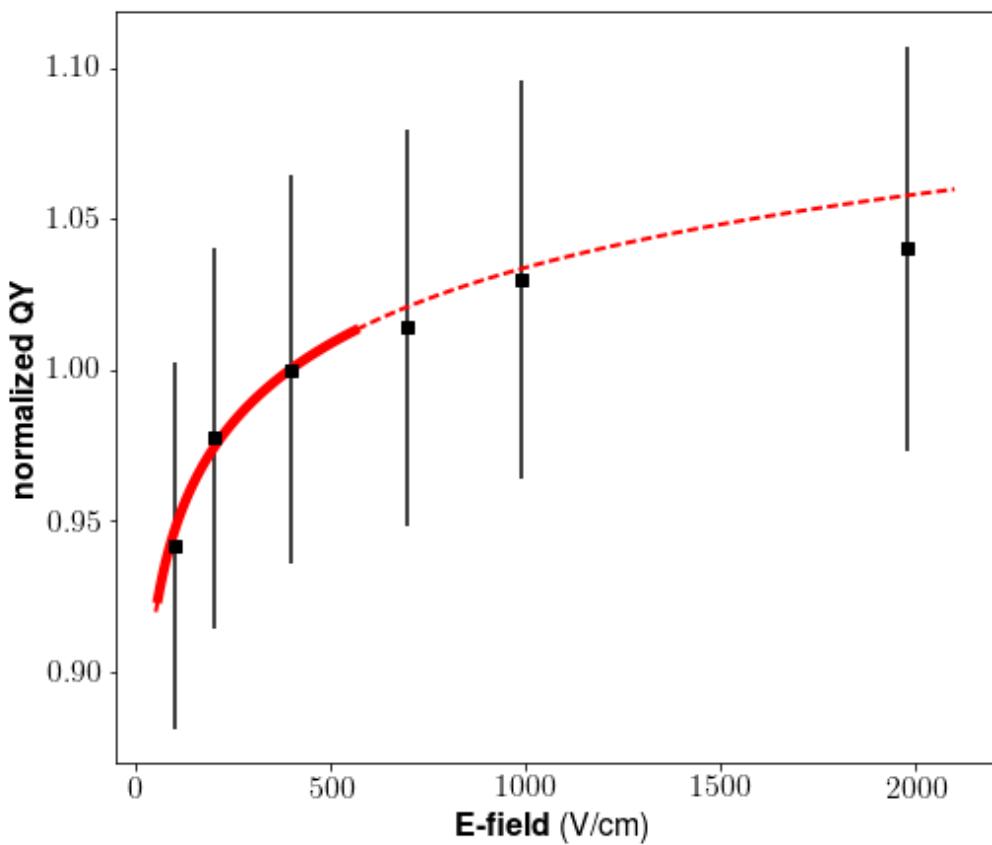


Figure 4.9: NEST model of the ^{37}Ar vs the measurements from PIXeY[22]. The solid portion of the line indicates the range of fields in the LUX post-Run4 calibration data. There is about a 10% variation due to electric field in the LUX post-Run4 data. The NEST v0.98 model traces the trend in the PIXeY data quite well.

Each drift time bin is then divided into a 22x22 x-y grid. The radial extent of events is highly dependent on drift time, so the density in x and y of events near the top of the detector is much less than the density near the bottom of the detector. Events from the bottom of the detector are focused from about 25 cm in real space to about 9 cm in S2 space. This means that the S2 from a wall event (25 cm radius) near the bottom of the detector will appear to have a radius of about 10 cm. An x-y bin with edge-width of 2

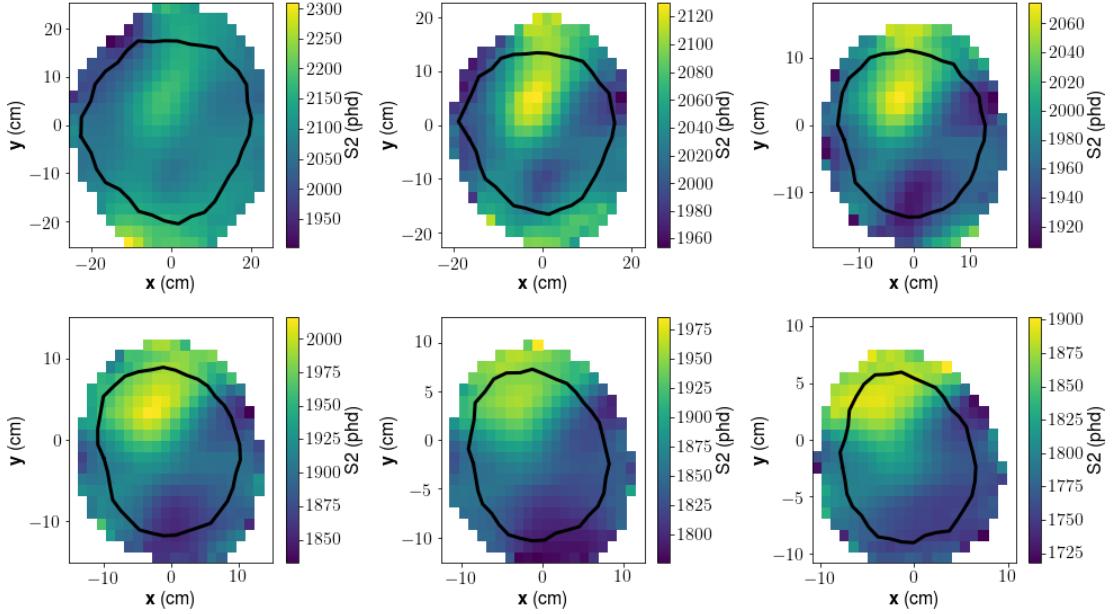


Figure 4.10: Measured Ar-37 S2 means in selected drift time bins. The bins from top left to bottom right are 50, 100, 150, 200, 250, and 300 microseconds. The black outline indicates the x-y position of the radial selection cut at the given drift time. The measurements of the S2 mean outside of this border exist because of the smearing applied in the calculation.

cm at the top of the detector will have an effective width of about 5 cm at the bottom of the detector. To account for these effects, we scale the x-y grid for each drift bin by the maximum radius of events within that bin. The 10 microsecond drift bin has an x-y grid that spans from -25.2 to 25.2 cm, while the 330 microsecond grid goes from -9.4 to 9.4 cm.

When calculating the mean values, we treat the drift time bins independently but allow the x-y bins to smear together. We draw a circle with a radius equal to 2.5 times the bin width around the center of each x-y bin. We include all of the events within that circle in our calculations for that bin. For each bin we calculate the mean S2 ($S2_{H3,ijk}$), where i is the x-index, j is the y-index, and k is the drift time index, as well as the mean electric field using values interpolated from a field-map described in section 2.2. The electric field value is used to generate an expected S2 value from NEST, ($S2_{NEST,ijk}$).

The S2 measurements need to be normalized to the top center of the detector. We

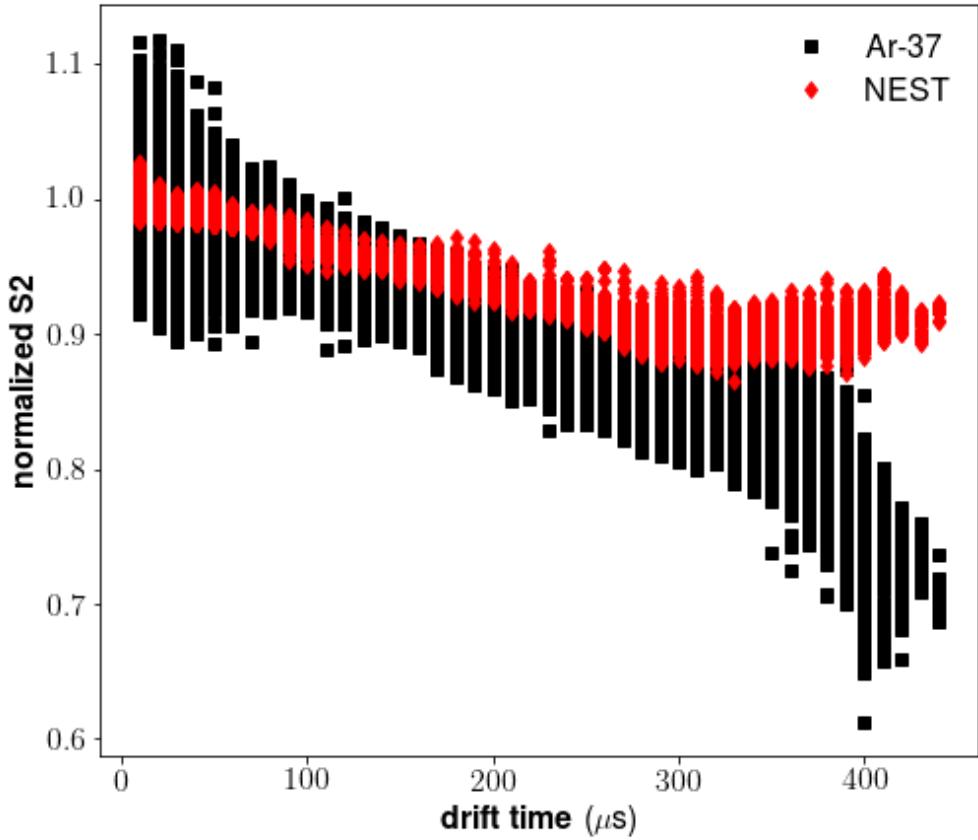


Figure 4.11: The black markers here show the measured S2 means, normalized to the top center of the detector. The red markers show the expected variation due to electric field alone. The S2 efficiency correction can be thought of as the red values divided by the black values.

calculate the S2 value in this region by taking the average of bins from the top three drift time slices that lie inside a radius of 10 cm from the center of the detector. The S2 correction is then defined:

$$C_{S2,ijk} = \frac{S2_{NEST,ijk}}{S2_{H3,ijk}} \cdot \frac{S2_{H3,top}}{S2_{NEST,top}}, \quad (4.4)$$

where $S2_{NEST,top}$ and $S2_{H3,top}$ are the values calculated at the center top of the detector.

Figure 4.12 shows a comparison of the S2 corrections measured using the procedure described in this section and those measured using the KrypCal procedure. Below about

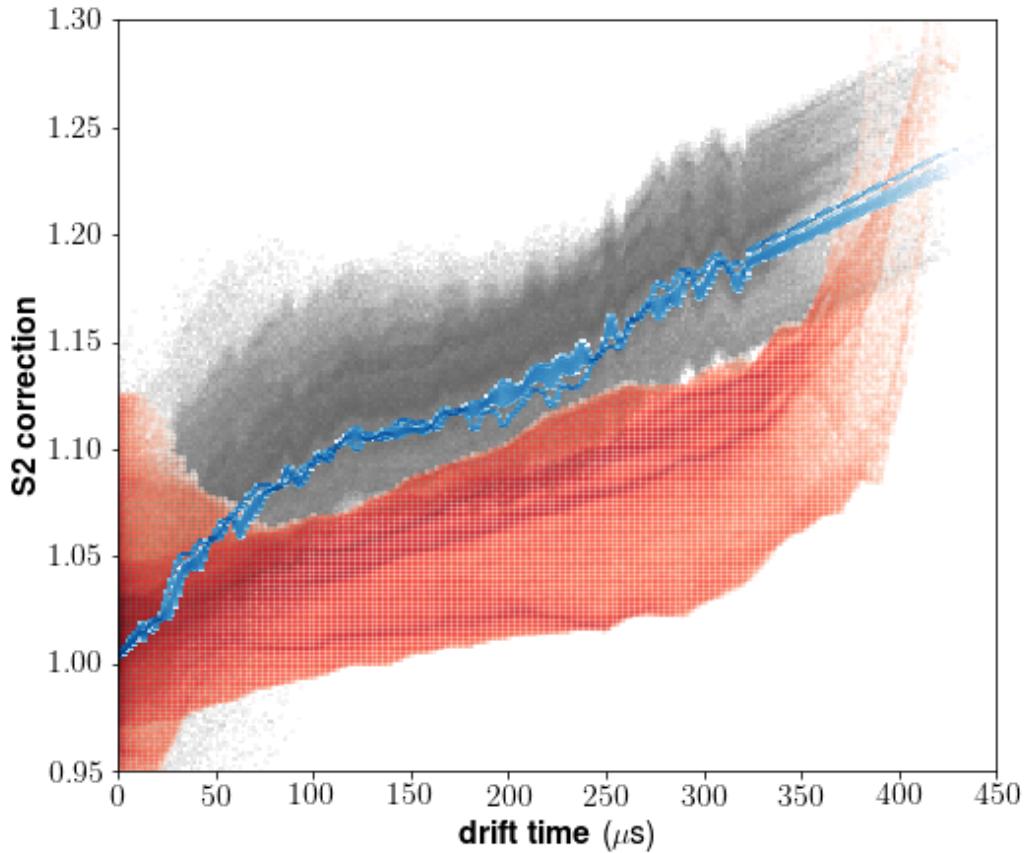


Figure 4.12: The KrypCal z-only (blue) and xyz (grey) S2 corrections compared to the Ar-37 S2 correction (red). At drift times greater than about 100 microseconds the two methods are in decent agreement. At smaller drift times, however, there is a steep trend observed in KrypCal that is not present in the corrections measured using Ar-37.

100 microseconds in drift time, the slope from the two corrections methods are in good agreement. For drift times less than 100 microseconds, the KrypCal corrections see a significantly larger slope than those measured using argon-37. There are fewer assumptions that go into the argon-37 S2 corrections. In particular, the assumption that the peak of the tritium spectrum can be approximated by a mono-energetic peak has the potential to introduce systematic effects. A change in the electric field may induce enough of a change

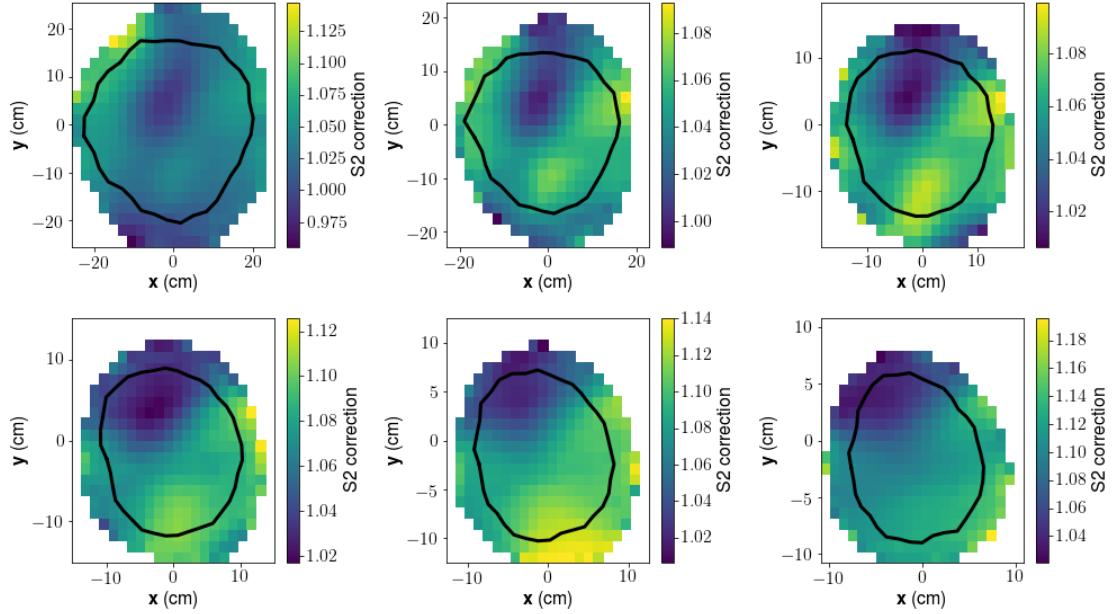


Figure 4.13: Measured S2 corrections for the same drift time bins as in figure 4.10.

to the charge and light yields that the energy of events in the peak of the tritium S2 spectrum is dependent on electric field.

We test this by looking at simulated tritium events which were generated using charge and light yields which will be presented in the next chapter. We take the mean input energy of events in a 200 phd window centered on the maximum of the uncorrected S2 spectrum. At the top of the detector, where electric field equals 491 V/cm, the energy of events in the peak of the S2 spectrum is 4.0 keV. At the bottom of the detector where the electric field is 43 V/cm, the energy of the S2 peak is 20% higher at 4.8 keV. At these energies, the charge yield has a steep dependence with energy, so there will likely be non-negligible systematic effects introduced by assuming the tritium S2 dependence can be approximated using a constant energy. This clearly highlights the advantage of using the mono-energetic Ar-37 peak to measure the S2 position-dependent efficiency.

4.3.2 S1 corrections from Xenon-131m + Krypton-83m Doke Plot

In a detector with a non-uniform electric field, the S1 efficiency correction is more complicated to measure than the S2 correction. In order to limit the effects of electric field variation, we would like to use a low-energy calibration source because the field dependence of charge and light yields is smallest at low energies. This is also the energy scale with the lowest light yield and combined with the typically low light-collection efficiency of liquid xenon TPC's (roughly 9-10% for LUX), these low-energy sources suffer from threshold effects in their S1 spectra. The KrypCal procedure feeds the S2 efficiency correction measured using tritium data into the krypton-83m S2 spectrum. This yields a field-dependent S2 spectrum which is used to measure the position-dependent recombination of krypton-83m data. This recombination measurement is then fed into the krypton-83m S1 spectrum in order to get a measurement of the S1 position-dependent efficiency.

Here we test an alternate method for measuring the S1 efficiency corrections which utilizes both the xenon-131m and krypton-83m calibration data. This method takes advantage of the fact that the field dependence of the charge and light yields is completely contained in the recombination probability. This means that when the data is plotted on a Doke-style plot, variation in the electric field will only work to move points along a line and will not change the line's parameters. The aim of this method, then, is to use a Doke-style plot to directly measure the light correction efficiency (G_1) in each of our (x, y, dT) bins which were described in the previous section. This method relies on the same recombination model the KrypCal assumes but, unlike KrypCal, does not require prior knowledge of the initial exciton to ion ratio, α .

We use the same method to measure the krypton-83m and xenon-131m S1 and S2 means for each voxel as was used in section 4.3.1 to measure the S2 means of argon-37. Once these means ($S1_{Kr83m,ijk}$, $S1_{Xe131m,ijk}$, $S2_{Kr83m,ijk}$, and $S2_{Xe131m,ijk}$) have been

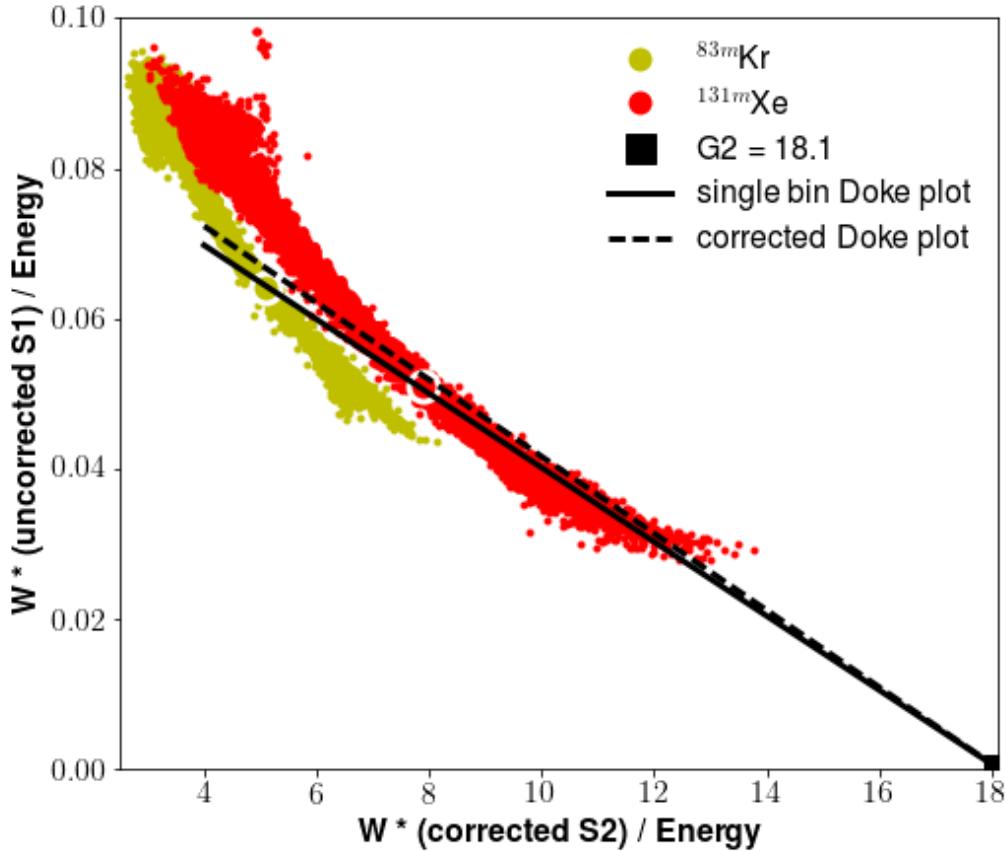


Figure 4.14: Doke plots of xenon-131m and krypton-83m for the bins described in section 4.3.1. By forcing G_2 to be constant, we perform a single-parameter fit to find G_1 in each bin. The solid black line shows the best fit line for the selected bin, and the dashed line represents G_1, G_2 as measured at the center of the detector.

measured, we use them to measure G_1 and G_2 at the center of the detector. We define the center of the detector as the mean drift time of argon-37 events, which is calculated to be 162.2 microseconds. We select bins that are within 20 microseconds drift time of the detector center and have a radius less than 5 cm. We take the average of the uncorrected S1 values, and the average of the corrected S2 values ($S_{2,ijk} \cdot C_{S2,ijk}$). We then construct our

Doke-plot using:

$$X_{center} = W \cdot S2_{center} \cdot C_{S2,center} / E \quad (4.5)$$

$$Y_{center} = W \cdot S1_{center} / E,$$

where $W = 1/73$ is the average work function for ionization and scintillation in liquid xenon, and E is the energy of the calibration line. We draw a line through the points $(X_{Xe131m,center}, Y_{Xe131m,center})$ and $(X_{Kr83m,center}, Y_{Kr83m,center})$. The x-intercept of this line will be taken to be $G2_{center}$, and the y-intercept will be $G1_{center}$.

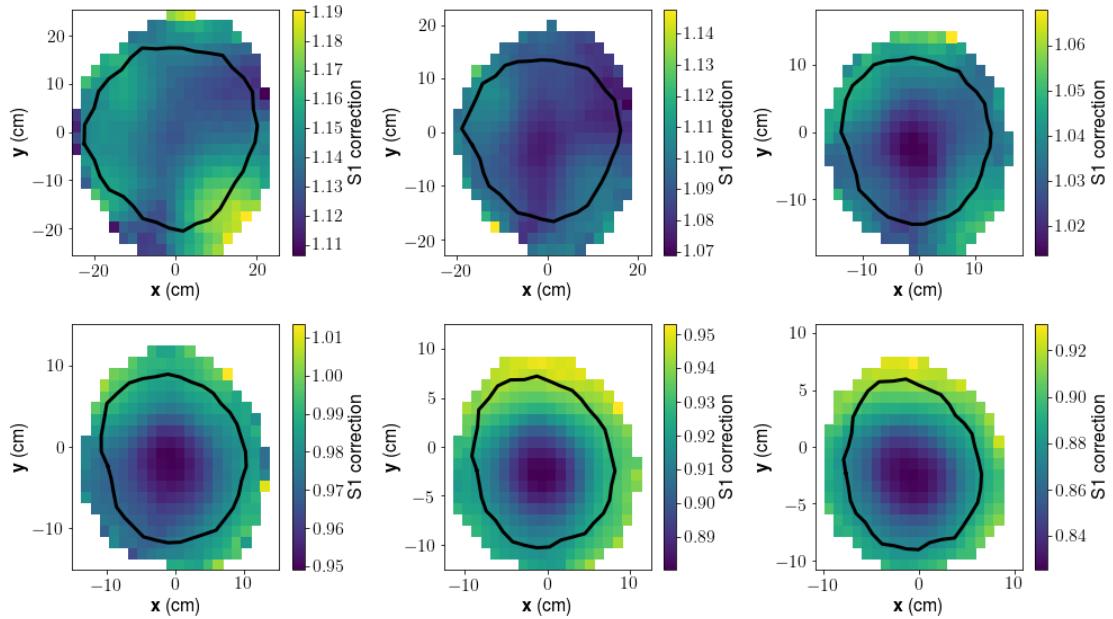


Figure 4.15: Measured S1 corrections for the same selected drift time bins as in figure 4.10.

The value of $G1$ for the individual voxels is calculated in the same manner as was done for the detector center. We define the points (X_{ijk}, Y_{ijk}) for krypton-83m and xenon-131m in the same way we defined (X_{center}, Y_{center}) . Here, instead of analytically drawing a line through the two points, we fix the x-intercept to $G2_{center}$ and allow the y-intercept to float in order to find the best-fit $G1_{ijk}$. These values of $G1_{ijk}$ are direct measurements of the

position-dependent S1 efficiency, so by normalizing them to the detector center we can easily write the S1 efficiency correction:

$$C_{S1,ijk} = \frac{G1_{center}}{G1_{ijk}} \quad (4.6)$$

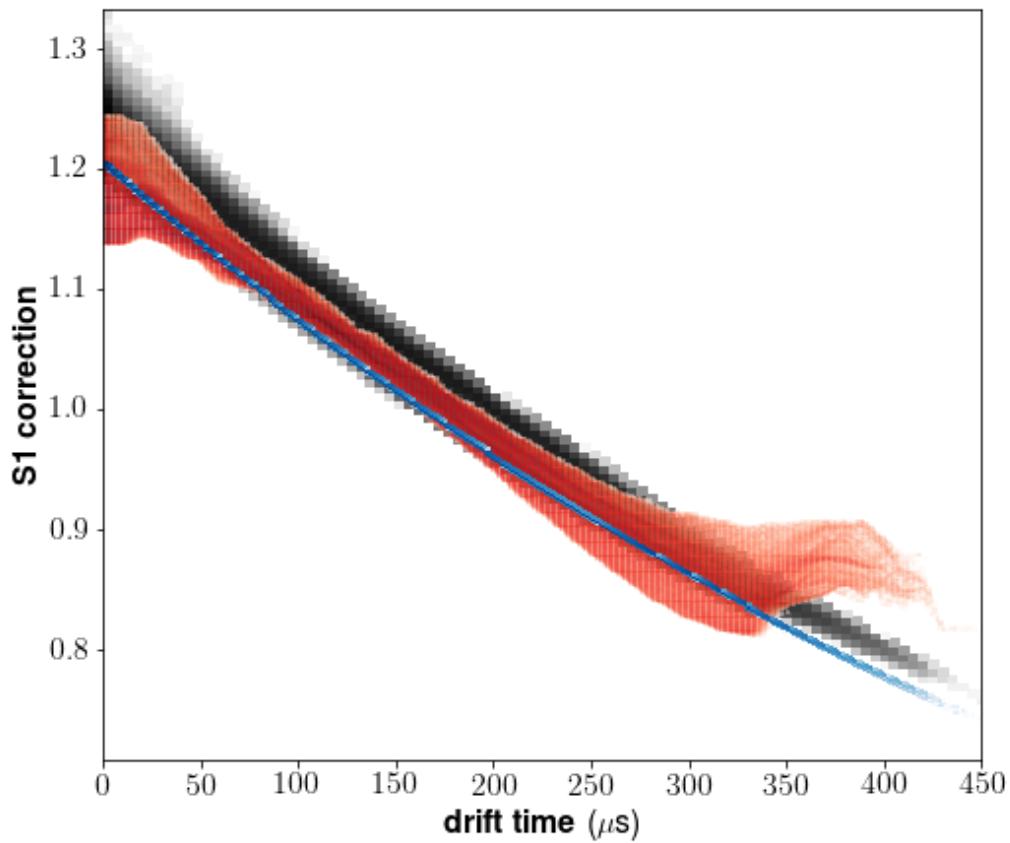


Figure 4.16: Comparison of the KrypCal z-only (blue) and xyz (grey) S1 corrections with the Doke-style S1 corrections introduced in this section (red).

This method of deriving the S1 efficiency correction is more consistent with KrypCal than the argon-37 S2 corrections were. This is more or less expected, since the two methods

rely on the same physical assumption. The primary discrepancy between the two would be expected to come from the fact that both methods require the S2 correction as an input. The roughly 5% discrepancy in the S2 correction is subdominant to both the variation in both recombination and S1 efficiency, so it has only a minor effect on the measurement of the S1 correction.

4.3.3 Applied Corrections

Now that we have measured a new set of corrections we would like to apply them to our data in order to see how they compare to the existing KrypCal corrections. To do this we need to interpolate between the measured $C_{S2,ijk}$ and $CS1,ijk$ to find a set of corrections for arbitrary x, y, and dT.

In order to ensure that there is no out-of-bounds interpolation error, we set the corrections values of any empty bins equal to that of their nearest non-empty neighbor. For each drift time bin we apply a bivariate spline in x and y, taking $C_{S2,ijk}$ and $CS1,ijk$ to be located at the center of their respective bins. After that we apply a linear interpolation in drift time between the values of the x-y splines. Again we assume the values are located at the centers of their respective drift time bins.

With the newly corrected data in hand, we now check to see how we did. We first need to measure the final G1 and G2 for both types of corrections to do this we finely slice the detector in drift time and generate a Doke-style plot using the same procedure as in the previous section. This time we include the krypton-83m and xenon-131m points from all of the drift time slices when fitting our line, and we allow both G1 and G2 to float. We do not include the argon-37 point in the fit because they are too close to threshold and are not expected to lie on the Doke-plot line.

The results of these fits are shown in figure 4.17. In this plot the lines labeled “z” and

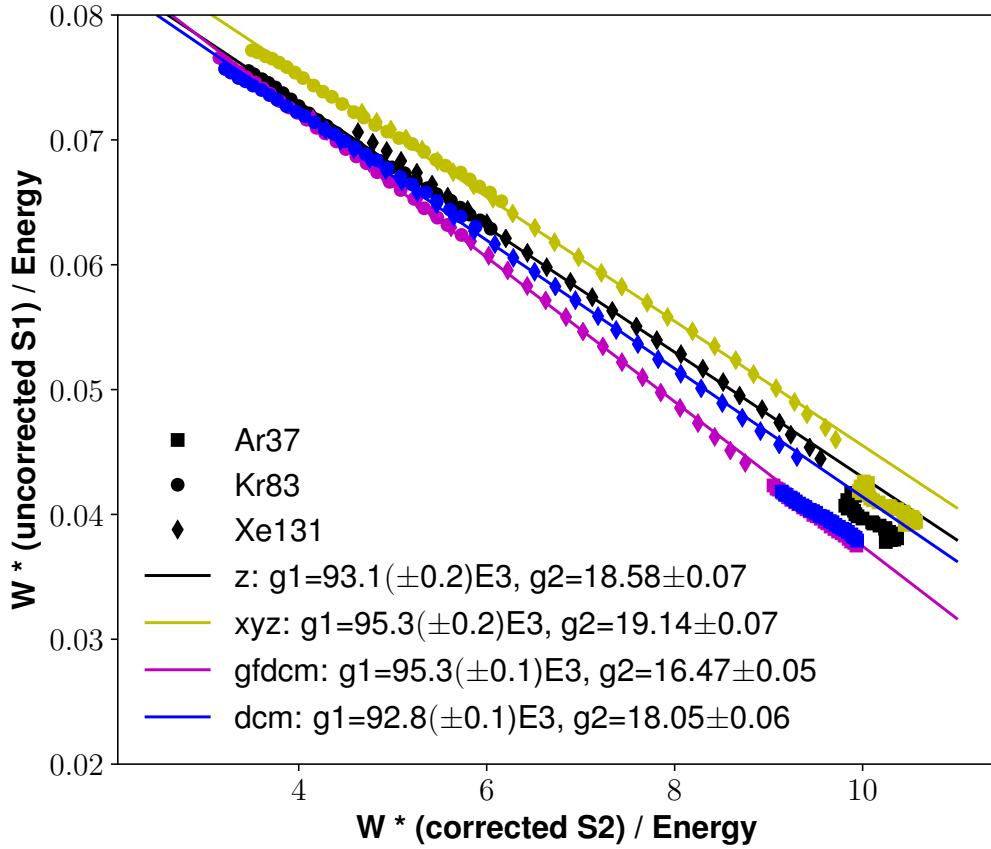


Figure 4.17: Doke-style plot for the various corrections methods considered. See text for explanation of the various lines.

“xyz” are KrypCal corrections. The line labeled “dcm” is using the corrections derived in the previous two sections. The “dc” in “dcm” is shorthand for “Doke-corrected”, and the “m” indicates that the S1 and S2 averages in the various bins were calculated by arithmetic mean. We also generated a set of corrections which fit a Gaussian peak to the S1 and S2 distributions in the individual bins, but the two methods yielded equivalent results, so we discarded the latter for the sake of simplicity. The newly derived corrections do improve the fit to a Doke line. The rms offset of the fitting points from their best fit lines is 5.6% and 5.2% for “z” and “xyz”, respectively, and is 4.3% for both “dcm” and “gfdcm”. This

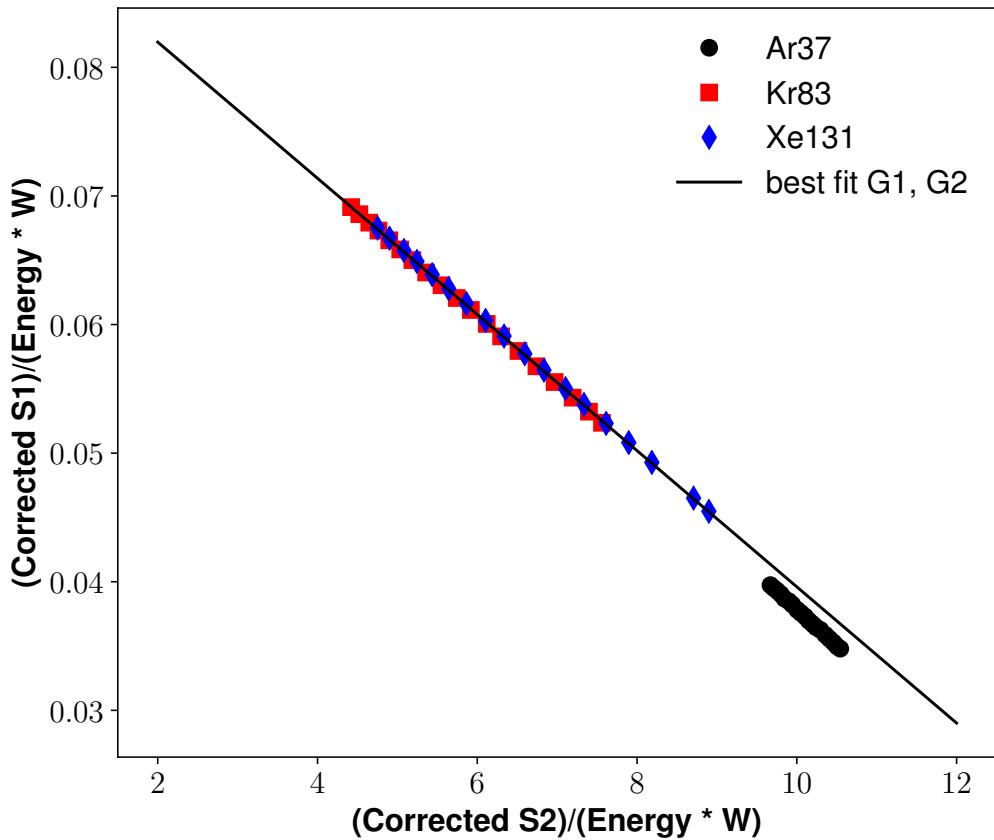


Figure 4.18: Simulated version of figure 4.17 generated using the libNEST code. We set $G1=0.0928$ and $G2=17.49$ in this plot. This plot was generated without the model of the S2 tail, which will be introduced in the next section.

improvement indicates that the corrections method laid out in the previous sections does a better job at flattening out the position dependence of the detector efficiency.

Figure 4.18 shows a simulation of the plots in figure 4.17. The $G1$ and $G2$ values used for this simulation were $G1=0.0928$ and $G2=17.49$. The best-fit line in 4.18 is able to reproduce these values within about 0.1%, yielding $G1=0.0926 \pm 0.0001$, and $G2=17.48 \pm 0.04$. The measured $G1$ is off of the true value by about 2-sigma; this is likely due to a small systematic effect in the libNEST code. This 0.1% effect is highly subdominant

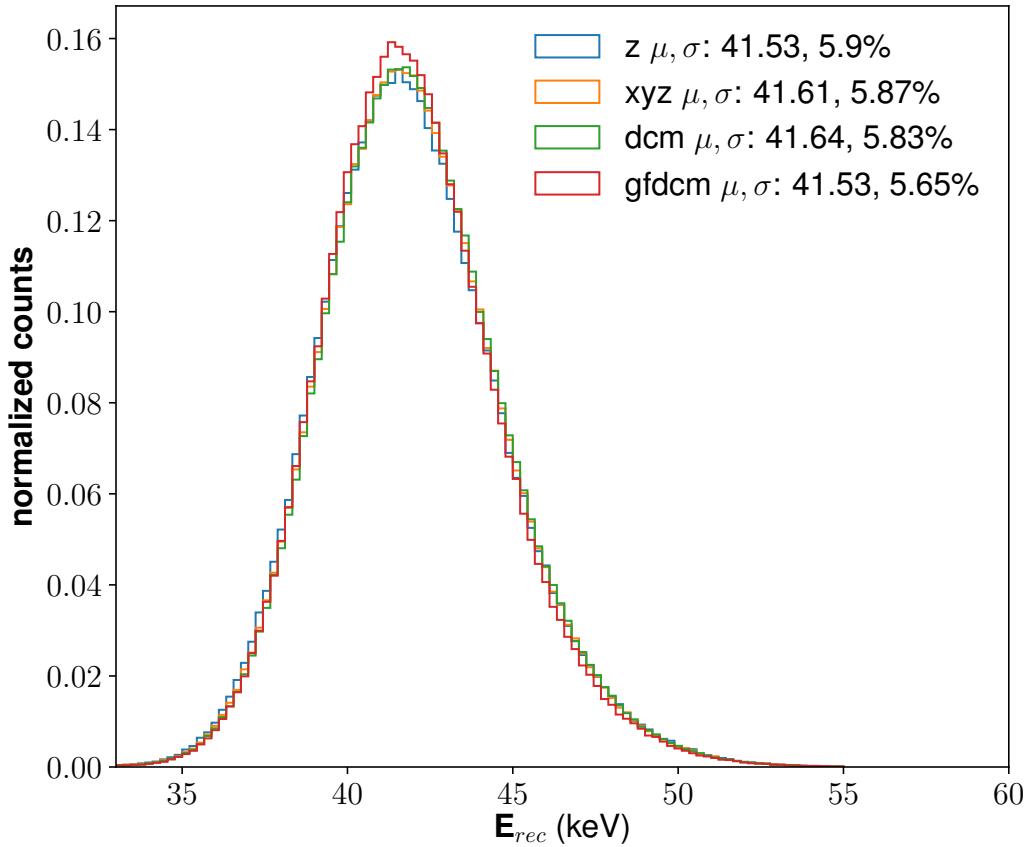


Figure 4.19: Reconstructed energy spectrum for the 41.5 keV krypton-83m spectrum. The μ indicates the peak location and is in units of keV. σ indicates the width/energy of the spectrum.

to other uncertainties in our measurements, so we will neglect it. The argon-37 K-capture points are systematically below the best fit line by, on average 4.5%. For comparison, the argon-37 points in figure 4.17 are below their best fit lines by 8% for “z” corrections, 1% for “gfdcm” corrections, and 9% for “dcm” corrections.

The line in figure 4.17 labeled “gfdcm” also uses the corrections derived in the previous two sections. The difference between this data and the “dcm” data is that it uses a different measure of S2. The “dcm” data, along with “z” and “xyz”, uses the “pulse-finder” area as

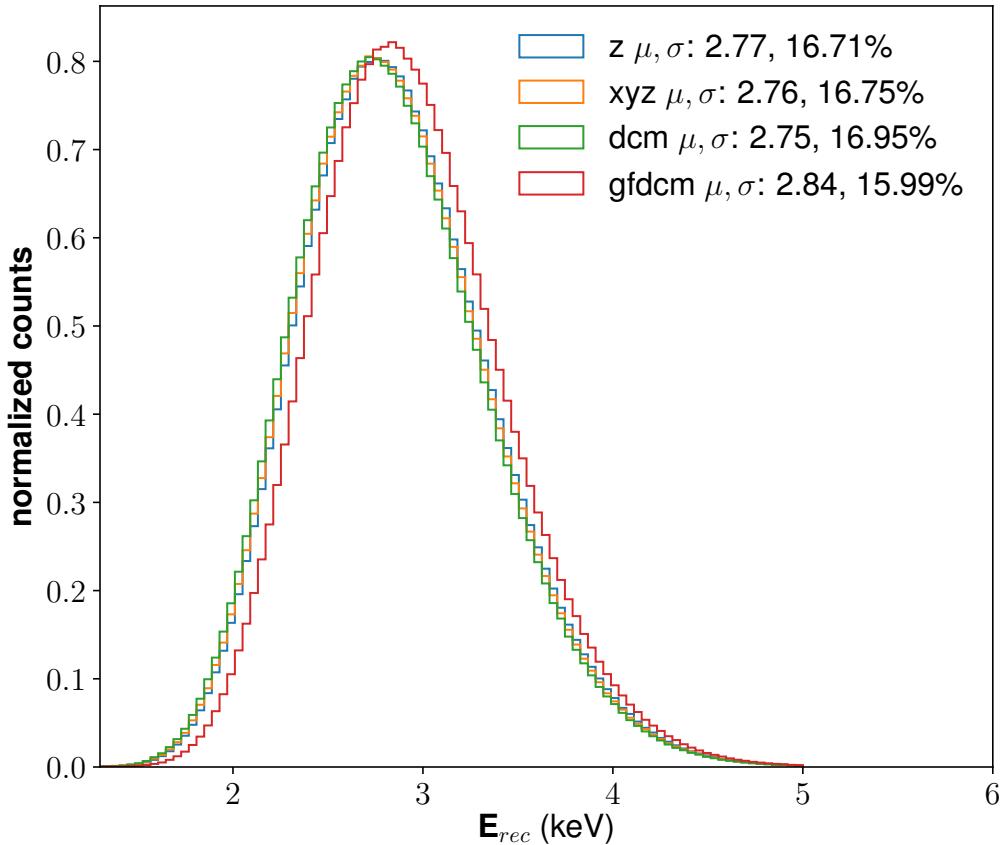


Figure 4.20: Reconstructed energy spectrum for the 2.8224 keV argon-37 spectrum. The μ indicates the peak location and is in units of keV. σ indicates the width/energy of the spectrum.

the measure of S2. This is just a raw sum of the S2 waveform. The “gfdcm” data uses the area under a Gaussian function (hence the “gf”) which has been fit to the S2 waveform as the measure of S2 size.

The first observation we take from figure 4.17 is that there is a systematic variation in the argon-37 points, causing them to be “S” shaped. This effect is not present in the “dcm” or “gfdcm” plots, and so provides further evidence that the steep trend in the KrypCal S2 correction near the top of the detector does not represent a genuine efficiency effect. The

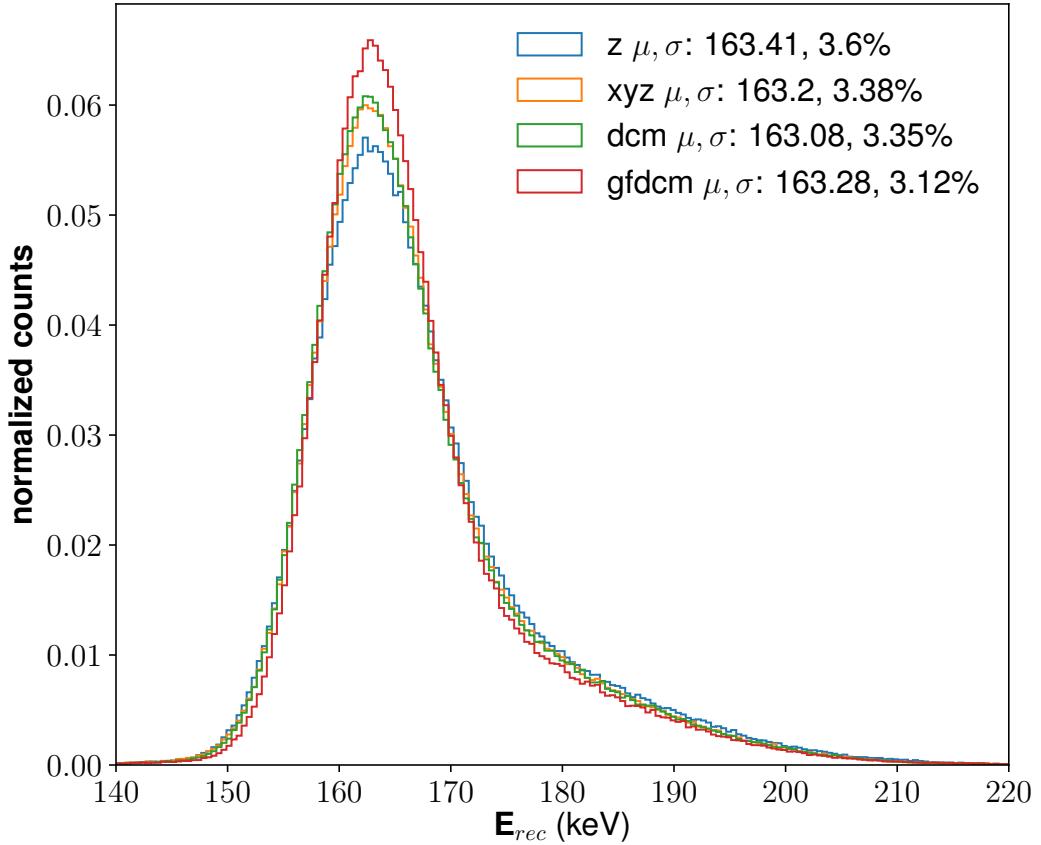


Figure 4.21: Reconstructed energy spectrum for the 163.93 keV xenon-131m spectrum. The μ indicates the peak location and is in units of keV. σ indicates the width/energy of the spectrum.

argon-37 populations in the “z”, “xyz”, and “dcm” plots are also offset from the best fit line. This is not entirely unexpected since the argon-37 S1 spectrum is bumping against threshold, although the size of the offset is larger than expected.

We use the G1 and G2 values taken from to generate reconstructed energy spectra for xenon-131m, krypton-83m, and argon-37. We find that “z”, “xyz”, and “dcm” generate a roughly equivalent energy spectrum for argon-37 and krypton-83m, both in the peak location and resolution. For xenon-131m, “dcm” and “xyz” are roughly equivalent and “z”

produces a spectrum which is wider by about 7.5%.

Interestingly, the “gfdcm” corrections produce significantly narrower spectra than any of the others, for all three calibration lines. Additionally, it produces the only argon-37 spectrum whose energy is higher than the true value of 2.8224 keV. This is important because the reconstructed energy for argon-37 should be artificially high because the low energy side of the spectrum is hidden by threshold. TMoving forward, we will focus on the following three corrections methods:

- “dcm”, because it produces ever-so-slightly better Doke plot and energy spectra than “z” and “xyz”
- “gfdcm”, because it produces the straightest Doke-plot and best energy spectra out of any of the methods tested
- “z”, in order to be consistent with, and to create applicable results for existing LUX analysis

4.4 Model of the Pathological S2 Tails

The energy spectra shown in figures 4.20, 4.19, and 4.21 all have a clear non-Gaussian tail toward high energy. These tails are propagated from a pathological effect in the S2 signals and are thought to be caused by the electron-trains described in section 2.4. The S2 tails are present both during the LUX Run04 WIMP-search and in the post-Run04 calibration campaign.

We look for insight into this issue by comparing the S2 spectra of argon-37, xenon-131m, and krypton-83m at different drift times, as in figure 4.22. We find that the relative amplitude and slope of the tails do not change significantly at different energies or drift bins. From this we conclude that the tails will be approximately proportional to the initial

S2 size. This is good news because it means that the combined energy model presented in section ?? will still be expected to hold. We also see from figure 4.23 that the shape and size of the argon-37 tails do not change when additional activity, in the form of krypton-83m events, is added to the detector.

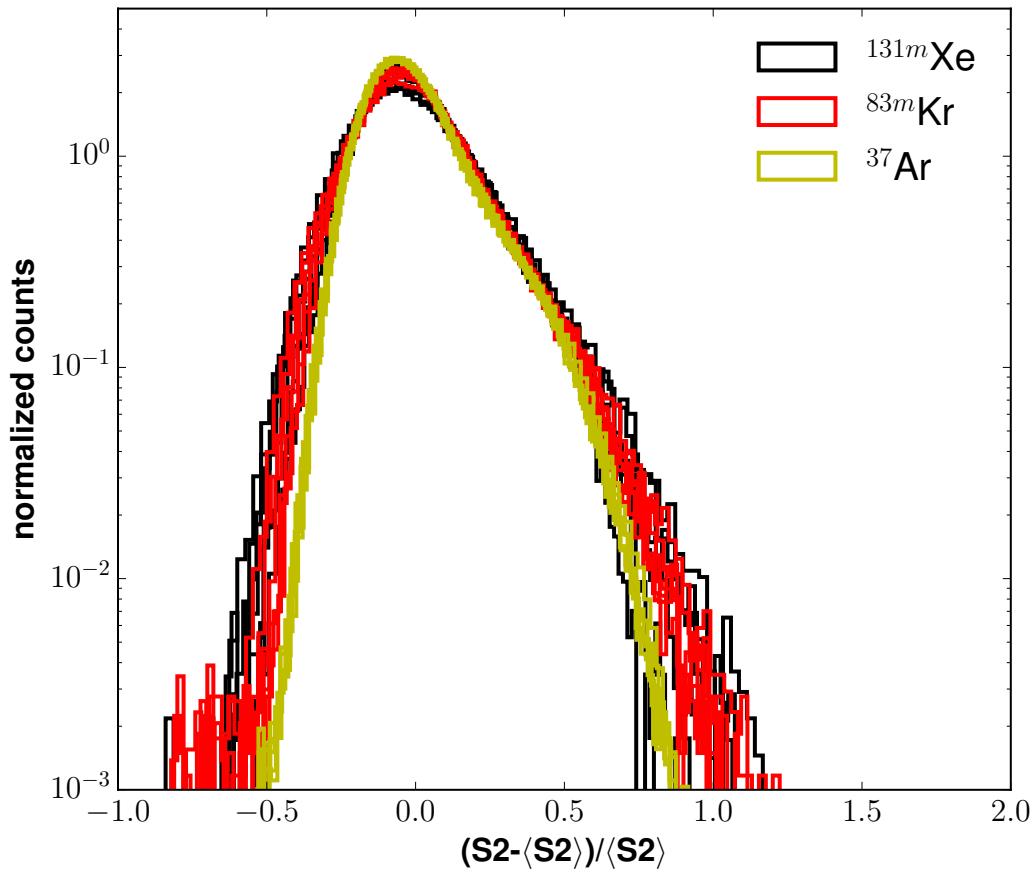


Figure 4.22: Mean-subtracted and normalized S2 spectra for argon-37, krypton-83m, and xenon-131m. The spectra are divided into 6 drift time bins from 40 to 310 microseconds. We see in this plot that the fractional size of the S2 tails is roughly constant in both energy and drift time.

To first order, the effect of the pathological tails will be absorbed into the measurement of G2. In calculations where the detector resolution are important, such as in the measurement of recombination fluctuations or when dealing with continuous energy spectra, a

more nuanced understanding may be required. To this end, we aim to develop an empirical model which will allow us to estimate the systematic effects of this pathology.

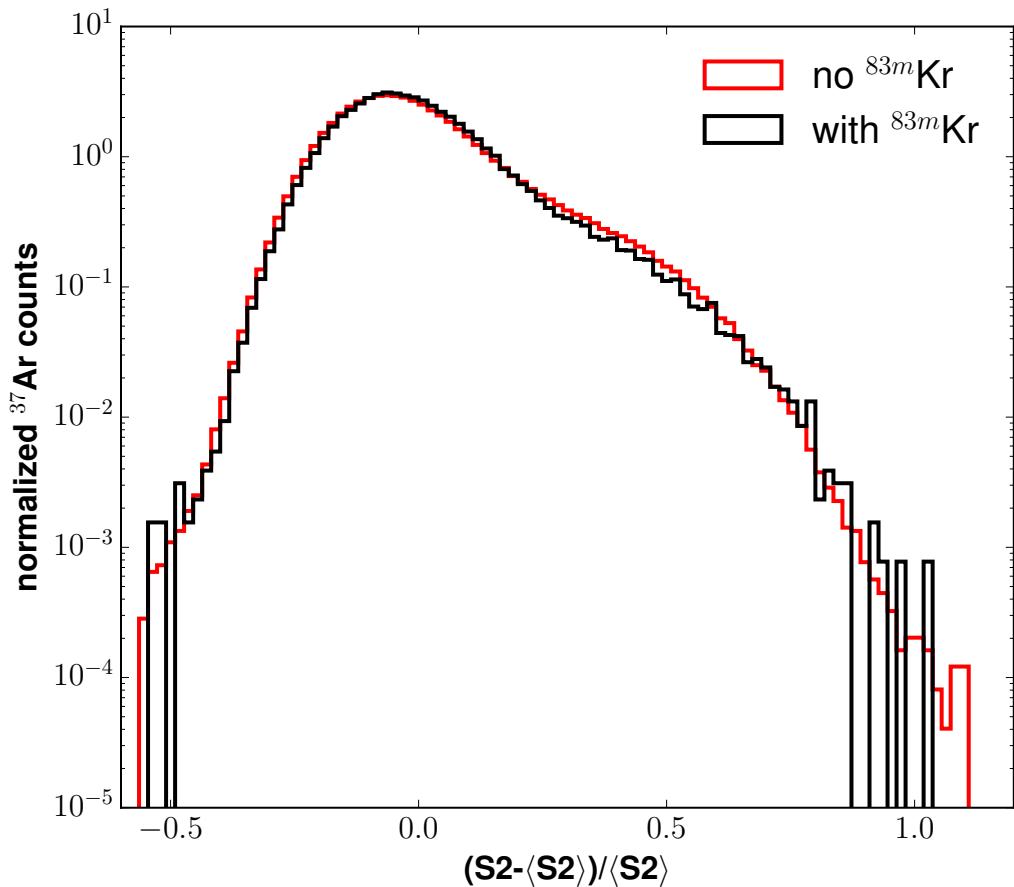


Figure 4.23: Mean-subtracted and normalized S2 spectra for argon-37. We show the spectrum both during a krypton-83m calibration (black), and when no additional activity is present (red).

The model of S2 tails will be implemented as an adjustment to the libNEST model by adding some random number of electrons to number of electrons extracted from the liquid. The expected value for the number of extracted electrons before the tail is added is given by:

$$\langle N_{e,extr} \rangle = \varepsilon N_e / C_{S2}(x, y, dT), \quad (4.7)$$

where ε is the extraction efficiency, $C_{S2}(x, y, dT)$ is the efficiency correction for the event, and N_e is the number of electrons generated in the liquid. To simulate the effect of the S2 tails, we will alter $N_{e,extr}$ to give $N'_{e,extr}$, which will then continue to propagate through the libNEST model as usual. The resulting S2 spectra generated will hopefully reproduce the shape of the S2 spectra we observe in data.

We have a few observations in hand that help to motivate the development of a model of the S2 tails. First, it appears that not all events possess additional tail area, so we will try a model that assigns some probability, P_{tail} , that an event will be given additional area. We see from figure 4.22 that the size of the tails approximately follows an exponential distribution, and that the amplitude of the distribution is roughly proportional to the S2 size. With these observations we develop the model of S2 tails as follows:

1. Generate a random test variable, T , uniformly distributed between 0 and 1.
2. If $T > P_{tail}$, we set $N'_{e,extr} = N_{e,extr}$
3. If $T \leq P_{tail}$, we draw another random number n_{tail} from an exponential distribution whose mean is equal to b_{tail} . We then set $N'_{e,extr} = N_{e,extr}(1 + n_{tail})$.

This model is then dependent on three parameters, P_{tail} , b_{tail} , and the “true” value of G2, which needs to be input into the libNEST model. The G2 values as measured in figure 4.17 will artificially high because of the pathological S2 area added by the tails. By varying these three parameters, we can optimize the model until it reproduces the observed energy spectra.

We use our argon-37 and xenon-131m spectra as reference, calculating the χ^2 difference between the libNEST S2 and reconstructed energy spectra, and those measured in data. We first scan across the parameters to locate the approximate location of the optimal parameters. This grid scan uses a modified model for computational convenience. Instead

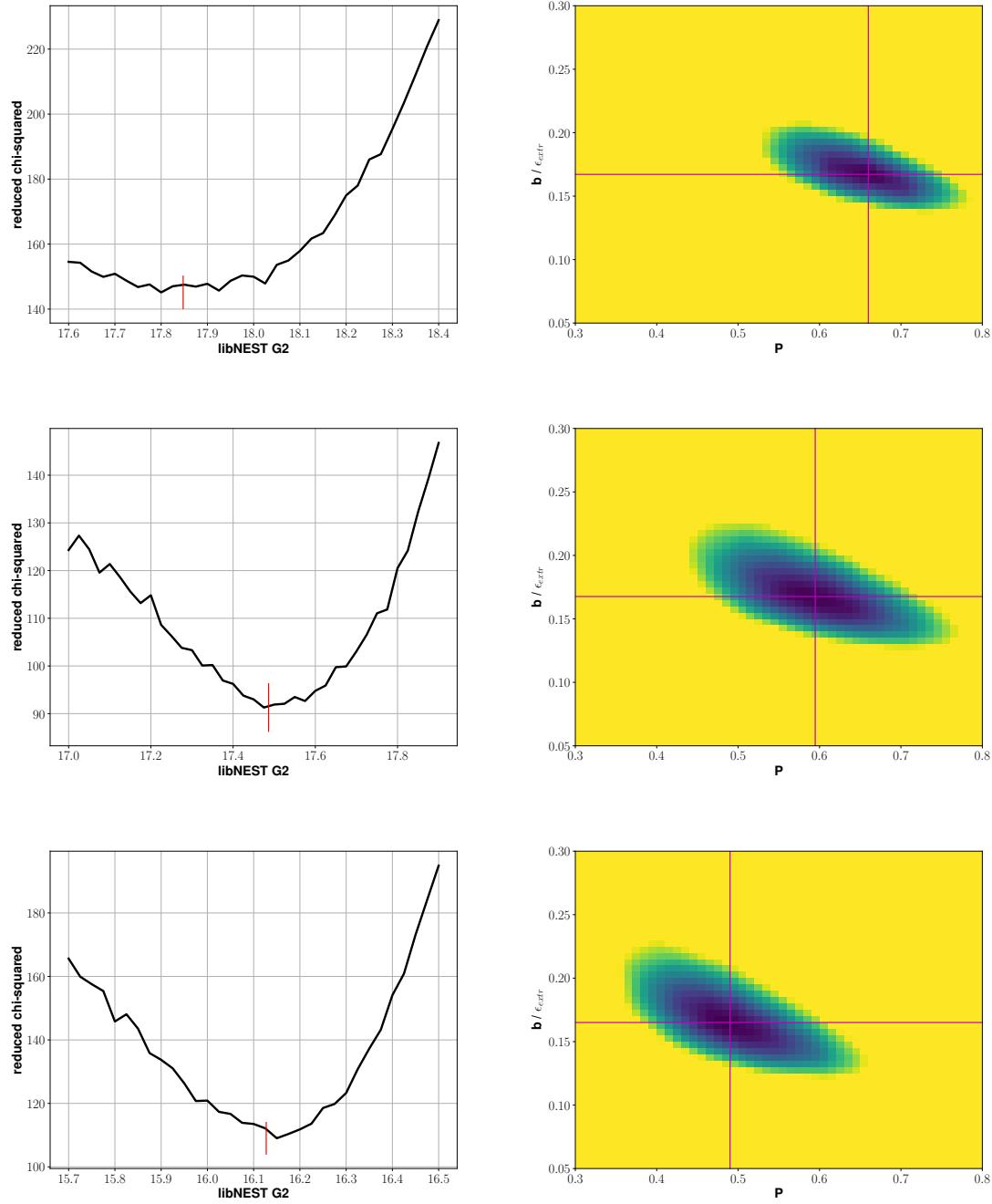


Figure 4.24: Best fit results for the tail model for “z” (top), “dcm” (middle), and “gfdcm” (bottom) corrected data. The red and magenta lines indicate the best fit values calculated using the Metropolis algorithm.

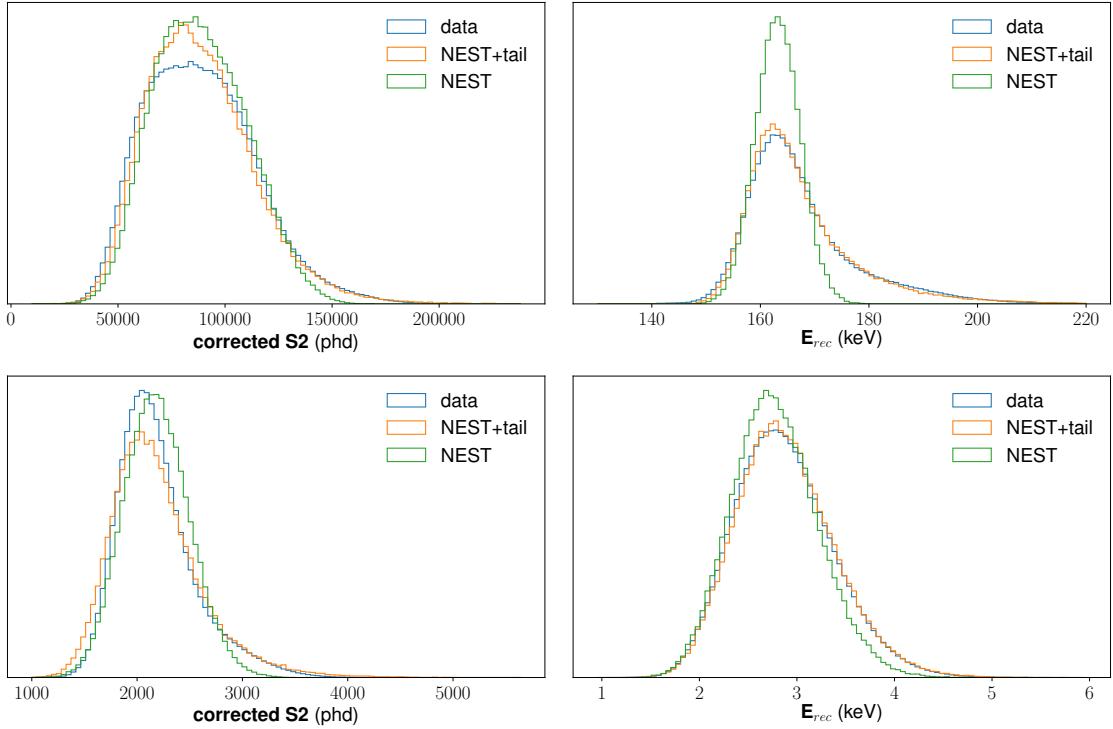


Figure 4.25: Best-fit spectra for “z” corrected data. The top plots are for the xenon-131m data, and the lower plots are for the argon-37 data. The green histogram, labeled “NEST”, is the libNEST simulation with no S2 tail model added. The orange histogram, labeled “NEST+tail” is the libNEST model, plus the model of the S2 tails described in this section. The blue histogram shows what is observed in data. The spectra are calculated for 50 to 300 microseconds drift time.

of adding the tail area to to $N_{e,extr}$, we add it to the final S2 area. Since this modified is applied after the extraction efficiency is modeled, the fractional tail area, $n_{S2,tail}$ will be drawn from an exponential distribution with a mean of b_{tail}/ε .

After the grid scan locates the approximate minimum, we then apply the Metropolis algorithm to fine tune the fit[3, 60]. For this algorithm, we use the model as we initially described it. For each iteration, we draw a new set test parameters from a normal distribution centered at the values of the previous iteration. These normal distributions have standard deviations of 0.005 for b_{tail} , 0.01 for P_{tail} , and 0.05 for $G2_{true}$. We then accept the new values of the parameters with a probability of $P_{accept} = \min(1, \exp(-(\chi_i^2 - \chi_{i-1}^2)/2))$. We

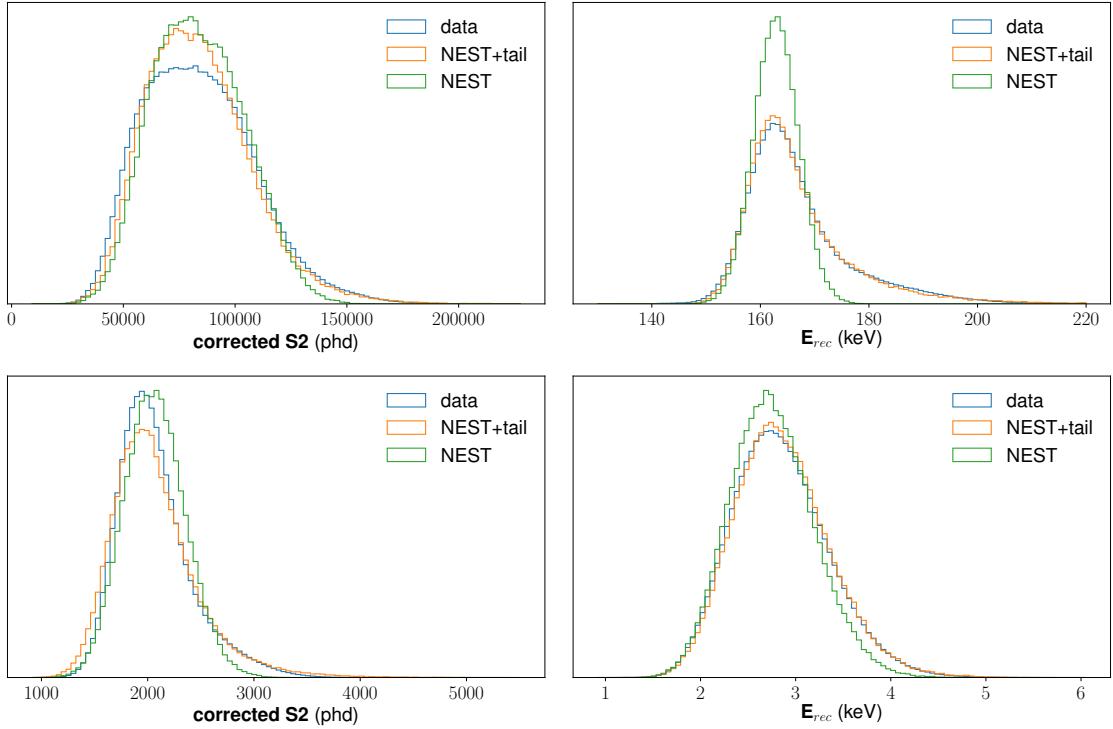


Figure 4.26: Best-fit spectra for “dcm” corrected data. The top plots are for the xenon-131m data, and the lower plots are for the argon-37 data. The green histogram, labeled “NEST”, is the libNEST simulation with no S2 tail model added. The orange histogram, labeled “NEST+tail” is the libNEST model, plus the model of the S2 tails described in this section. The blue histogram shows what is observed in data. The spectra are calculated for 50 to 300 microseconds drift time.

run at least 1000 iterations and allow for a burn-in period of 200 iterations. We take the best-fit values of the parameters to be equal mean of the iterations excluding the burn-in period.

Correction	b_{tail}	\pm	P_{tail}	\pm	$G2_{true}$	\pm
z	0.112	0.003	0.73	0.02	17.6	0.05
dcm	0.116	0.004	0.63	0.02	17.36	0.04
gfcdcm	0.109	0.004	0.53	0.02	16.02	0.03

Table 4.3: Best fit results for the S2 tail model.

We apply this fitting method to the three corrections methods we are testing; “z”, “dcm”, and “gfcdcm”. The results of the fit are shown in figure 4.24, as well as in table 4.3. The data

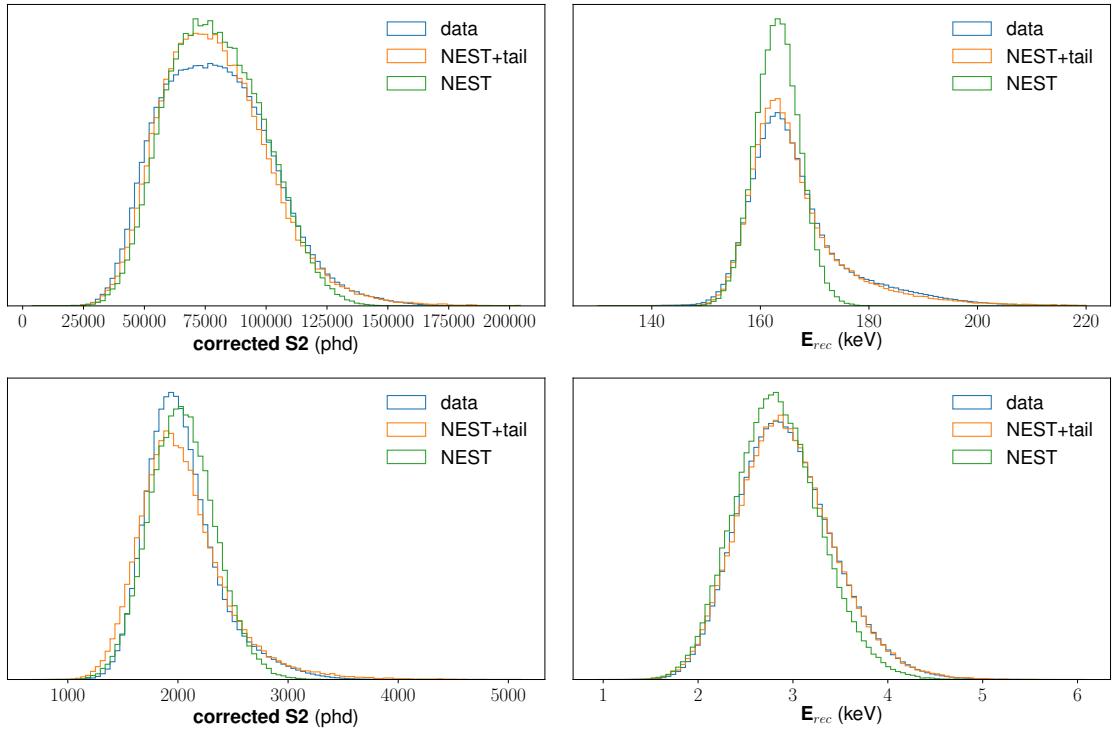


Figure 4.27: Best-fit spectra for “gfdcm” corrected data. The top plots are for the xenon-131m data, and the lower plots are for the argon-37 data. The green histogram, labeled “NEST”, is the libNEST simulation with no S2 tail model added. The orange histogram, labeled “NEST+tail” is the libNEST model, plus the model of the S2 tails described in this section. The blue histogram shows what is observed in data. The spectra are calculated for 50 to 300 microseconds drift time. In order to account for an error in the yields, the peak location of the simulated S2 spectrum is adjusted to match that of the data spectrum.

and NEST+tail energy histograms are in good agreement, indicating that our tail model is successful. There is some disagreement in the S2 spectra near the peak value. This is likely explained by incorrect values for the input recombination fluctuations. We will aim to better measure this input value in the next chapter.

Chapter 5: Detector Response to ^{14}C Beta Decay

The carbon-14 calibration follows the same preparation and injection procedure as the tritium calibration, which has been described in previous papers[8, 30, 50]. Both of these calibration sources have half-lives greater than the lifetime of the experiment, so we rely on the LUX gas processing system to chemically remove the injected activity. We have previously characterized our ability to remove radio-labelled methane from the LUX detector and found that tritiated-methane (CH_3T) is removed with a decay time of about 7-10 hours, leaving no observed residual activity in the detector. Carbon-14 labelled methane ($^{14}\text{CH}_4$) is chemically identical to CH_3T and so we find it to have the same removal characteristics. The tritiated methane is removed with a time constant of 8.2 hours, and the carbon-14 labeled methane is removed with a time constant 9.1 hours. This variation in removal time is within reason given the variation in previous trials with tritiated methane.

The endpoint of the carbon-14 spectrum is obscured by the xenon-131m line. We do not assume that gammas and betas behave in the same way in liquid xenon, so we need to cut out the xenon-131m events in order to measure the energy deposition properties of carbon-14. At 145 keV, the xenon distribution falls to less than 5% of the carbon-14 distribution, so we will only include events with reconstructed energy < 145 keV in our measurement of the carbon-14 yields and recombination..

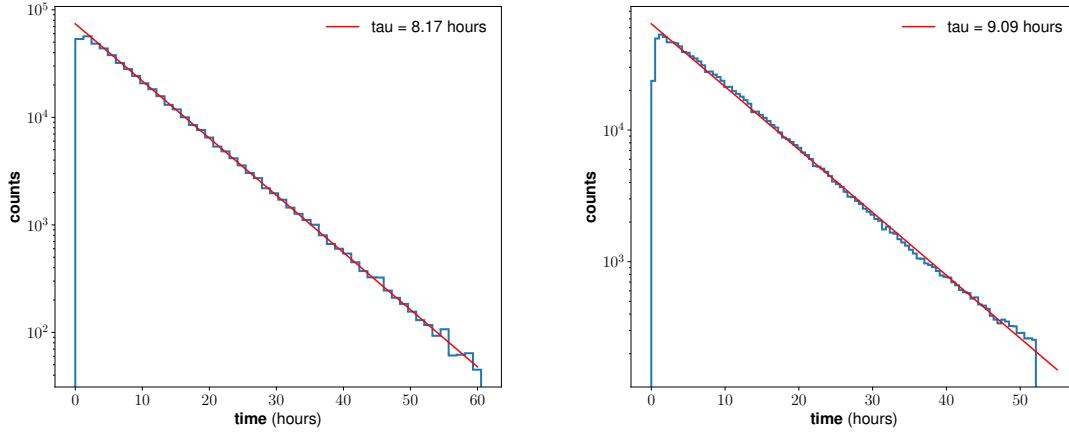


Figure 5.1: Purification of methane radio-labeled with tritium (left), and carbon-14 (right). The tritiated methane is removed with a time constant of 8.2 hours, and the carbon-14 labeled methane is removed with a time constant 9.1 hours.

5.1 The Theoretical ^{14}C Beta-Spectrum

The shape of the theoretical spectrum of the carbon-14 beta decay has been of interest in the context neutrino mass experiments[79], where the goal is to measure the precise endpoint, and in liquid scintillator experiments, which have ^{14}C as a major background and so need to model the spectrum with high precision[13, 18]. This decay also is of interest in theoretical nuclear physics because it has an abnormally long half life[41, 42, 52]. The transition of ^{14}C to the ground state of ^{14}N is an allowed Gamow-Teller ($0^+ \rightarrow 1^+$) transition. The 5730 year half-life, and corresponding comparative half life, $\log_{10}(f_t) = 9.04$, makes it empirically consistent with second-forbidden transitions[52, 79].

This extended half life indicates an anomalously small Gamow-Teller nuclear matrix element of $\langle GT \rangle \approx 2 \times 10^{-3}$. This points to cancellation in the lowest order terms of the nuclear matrix element and means that higher order terms must be taken into consideration. These higher-order terms may introduce momentum-dependent deviations from the allowed spectral shape. There have been several experiments[13, 18, 52, 72, 79] which

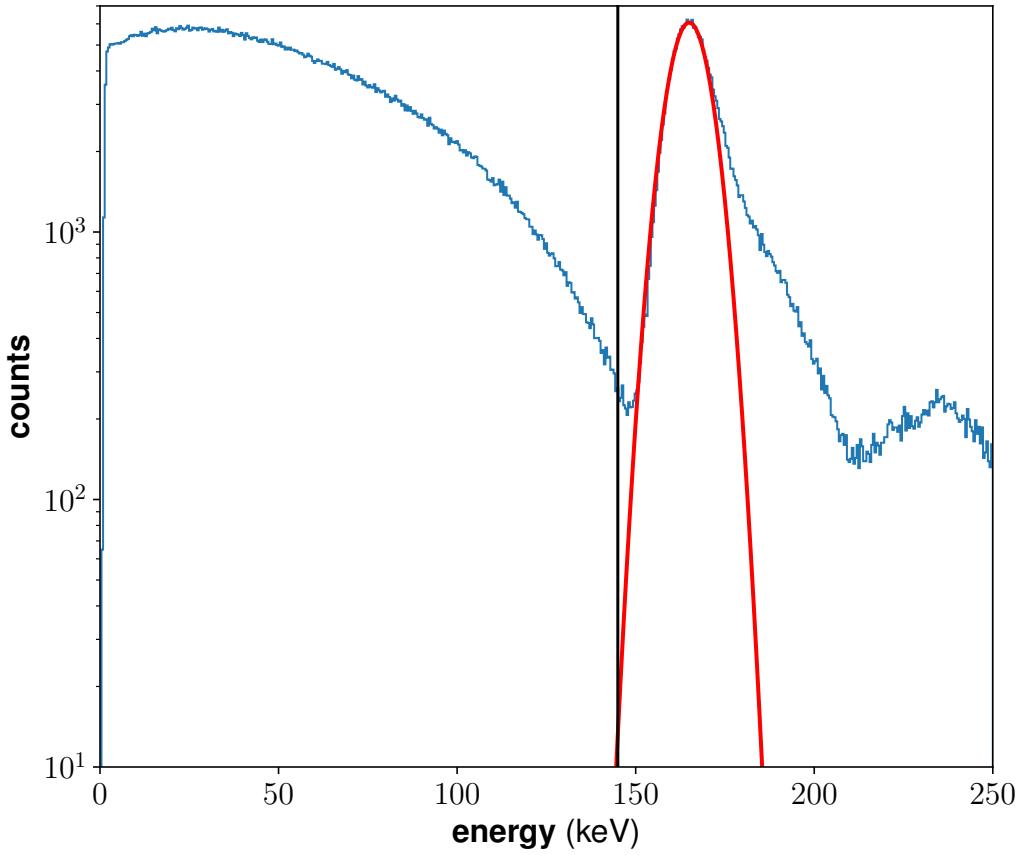


Figure 5.2: Reconstructed energy spectrum of the carbon-14 calibration. The blue histogram was generated using all of the events in the dataset, including both carbon-14 and Xe-131m. Most of the events are in the smooth carbon-14 beta spectrum, which extends from 0 to 156 keV, but the Xe-131m line is clearly visible at 164 keV. The red curve shows a Gaussian fit to the xenon-131m spectrum, excluding the high energy side. The black line shows our energy cut at 145 keV.

have made measurements of the spectral shape which are consistent with non-statistical corrections to the allowed shape. These results are in some tension with each other, as well as with previous measurements which show a purely allowed spectral shape[62].

5.1.1 The Allowed Spectrum

Carbon-14 decays to the ground state of nitrogen-14 by way of an allowed Gamow-Teller, 0^+ to 1^+ transition. This decay has a Q-value of 156 keV and a half life of 5730 years. In general, the theoretical spectrum for this decay takes the form[52]:

$$\frac{dN}{dE} = \frac{1}{2\pi^3} \xi C(E) F(Z, E) pE(E_0 - E)^2 \quad (5.1)$$

Here, p and E are the momentum and total energy of the emitted beta, and E_0 is the endpoint energy of the spectrum. In equation 5.1 we have neglected the neutrino mass as well as a radiative correction term which is expected to have $< 1\%$ effect on the shape of the spectrum[79]. The initial distribution of momentum between the electron and neutrino is proportional to $pE(E_0 - E)^2$. This is derived by the phase space density of free particles and will be referred to as the phase space factor. The Fermi function $F(Z, E)$ contains information about the interaction between the emitted beta and the daughter nucleus. The terms ξ and $C(E)$ represent the energy independent and energy independent parts of the nuclear matrix element.

5.1.2 The Fermi Function

As the emitted beta travels away from the daughter nucleus, the two interact and either increase or decrease the momentum of the beta, depending on its charge. In the case of ^{14}C , the beta has a negative charge and has to climb up out of the electric potential created by the ^{14}N daughter nucleus. The resulting observed beta spectrum will then be pulled to lower energy than the initial phase space factor. This modification to the spectrum if known as the Fermi function, $F(Z, E)$. The traditional derivation of $F(Z, E)$ begins by assuming the daughter nucleus is a fixed point charge and then evaluates the electron wave-function

given the resulting field. The wave function is only evaluated down to the nuclear radius, R , in order to avoid divergence[80]:

$$F(Z, E) = 2(\gamma + 1)\Gamma(2\gamma + 1)^{-2}(2pR)^{2(\gamma - 1)}e^{\pi\alpha ZE/p}|\Gamma(\gamma + i\alpha ZE/p)^2|^2 \quad (5.2)$$

There is also a much simpler closed-form solution in the low-Z, non-relativistic approximation[76]:

$$F_{NR}(Z, E) = \frac{x}{1 - \exp(-x)}, \quad (5.3)$$

where $x = 2\pi Ze^2/\hbar v$. Here, Z is the atomic number of the daughter nucleus, e is the electron charge, and v is the final velocity of the beta particle.

Electrons in the higher-momentum part of the spectrum will have velocities exceeding $0.5c$, so the non-relativistic approximation may not hold. This being the case, we consider the Bethe-Bacher approximation, which estimates the relativistic correction[21, 76]:

$$F_{BB}(Z, E) = F_{NR}(Z, E)[W^2(1 + 4\gamma^2) - 1]^S, \quad (5.4)$$

where $W \equiv E/m_e c^2$, $\gamma \equiv \alpha Z$, and $S \equiv (1 - \gamma^2)^{1/2} - 1$. The full relativistic Fermi function can be estimated by a series expansion on powers of (αZ) [79, 80]. This sum is of limited use to us here because it becomes invalid at low kinetic energy and in fact diverges at zero.

The final correction to the Fermi function we consider is the correction for screening of the Coulomb potential by the orbital electrons. This essentially amounts to a shift in the origin of $F(Z, E)$ [34, 79]:

$$F_S(Z, E) = \frac{E' p'}{Ep} F(Z, E'), \quad (5.5)$$

where $E' = E - V_0$ and p' is the associated momentum. For the ^{14}C beta decay, $V_0 = 495\text{eV}$ [79].

Figure 5.3 compares the non-relativistic approximation to the various corrections described in this section. We can see that the Wilkinson expansion differs from $F_{NR}(7, E)$ by less than a percent down to a few eV, at which point it diverges. The Bethe-Bacher approximation is similarly very close to $F_{NR}(7, E)$, but it does not display the same pathological behavior at the origin. The correction for electron screening peaks at 1.5% at a kinetic energy of $T = 3.5\text{keV}$. Because of the pathology in the Wilkinson expansion, we will take our Fermi function to be the combination of equations 5.4 and 5.5:

$$F(Z, E) = \frac{E' p'}{Ep} F_{NR}(Z, E') [(E'/m_e c^2)^2 (1 + 4\gamma^2) - 1]^S, \quad (5.6)$$

with $F_{NR}(Z, E)$ as defined in equation 5.3 and E' and p' as defined for eqaution 5.5.

5.1.3 The Shape Factor

For a typical allowed decay, the shape factor is dominated by interference between the Gammow-Teller axial matrix element, $\langle GT \rangle$ and the weak magnetism matrix element, $\langle WM \rangle$. Such a shape factor has the form[23, 41, 52, 79]:

$$C(E) \approx 1 + \frac{4}{3M} \frac{\langle WM \rangle}{\langle GT \rangle} [E - E_0/2 - m_e^2/E], \quad (5.7)$$

where M is the nucleon mass, m_e is the electron mass, and E_0 is the endpoint energy of the beta-spectrum. Usually the energy dependence of $C(E)$ is small enough that it can be neglected, but in the ^{14}C beta decay the suppressed decay rate means that $\langle GT \rangle$ is small enough to make its consideration necessary. Under the conserved vector current hypothesis (CVC), the weak magnetism matrix element can be analogized to that of an M1 electromagnetic transition ($\langle WM \rangle = \langle M1 \rangle$) for the purpose of calculating the expected shape factor. The ground state of ^{14}C is an element of an isospin triplet, together with the ^{14}O ground

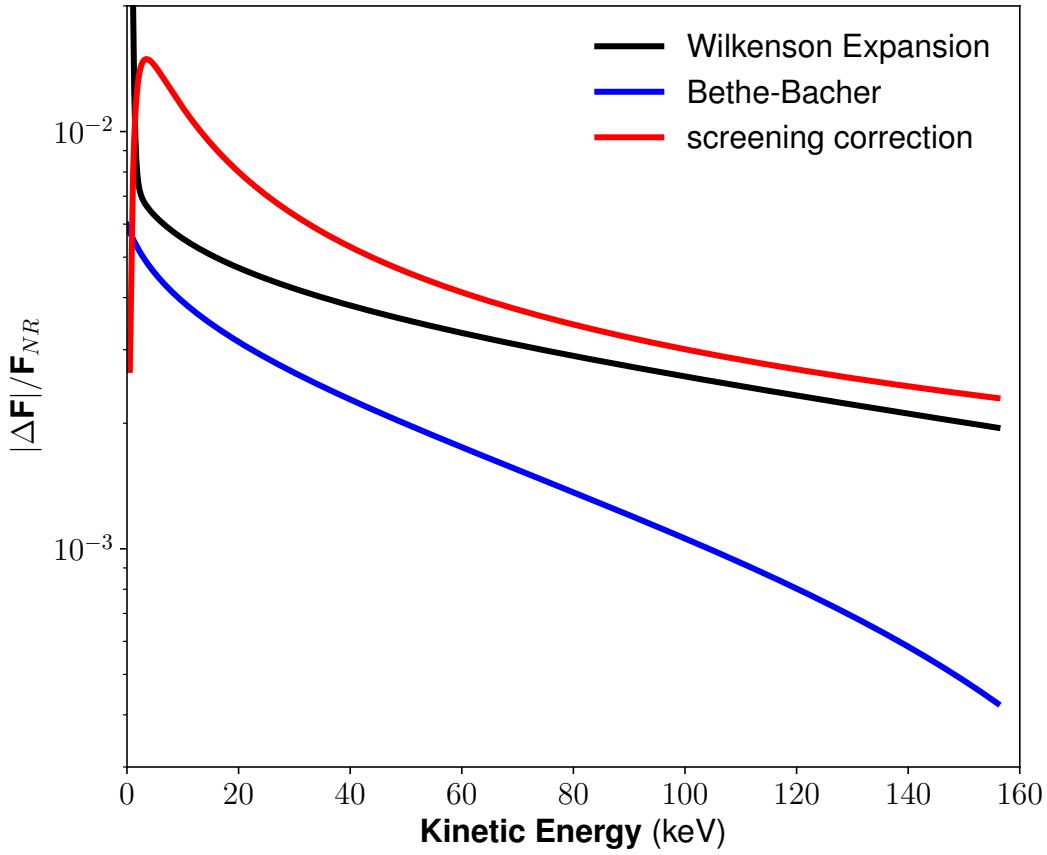


Figure 5.3: Correction factors for the ^{14}C beta Fermi function. We compare the non-relativistic approximation, $F_{NR}(7, E)$ to the relativistic corrections described in section 5.1.2, as well as the non-relativistic function after having been adjusted to account for screening by the orbital electrons. Plotted is $|F'(7, E) - F_{NR}(7, E)|/F_{NR}(7, E)$, where $F'(7, E)$ are the adjusted Fermi functions as indicated in the legend.

state and the first excited state of ^{14}N . The M1 transition is the same as that of the first excited state of ^{14}N transitioning to the ground state.

There have been several calculations of the predicted shape factor[41, 42, 79]. These typically use a more general form of the $C(E)$ which takes into account terms which have

been neglected from equation 5.7:

$$C(E) = 1 + aE + \mu_1 \gamma_1 b/E + cE^2, \quad (5.8)$$

where $\gamma_1 = [1 + (\alpha Z)^2]^{1/2}$ and μ_1 is a special Coulomb function. The coefficients a , b , and c can be calculated using the appropriate matrix elements. The matrix elements are typically calculated using model wave functions for the ^{14}C and ^{14}N ground states.

The first measurement of the ^{14}C shape factor was made by Sonntag et. al. in 1970[72]. In units of MeV, his measured shape factor was, $C(E) = 1 - 9.14E + 1.53/E + 7.66E^2$. Genz et. al.[42] used this result in part to derive phenomenological wave functions which replicate the shape factor. Later experiments and theoretical calculations have rejected this shape factor.

Wietfeldt et. al. found their data to be consistent with a shape factor of $C(E) = 1 + aE$, with $a = -0.45 \text{ MeV}^{-1}$ [79]. This result is very close to their own theoretical calculation of $a = -0.38 \pm 0.04 \text{ MeV}^{-1}$, along with theoretical calculations by Garcia and Brown[41], and Calaprice and Holstein[23]. However, the best-fit value of a was inconsistent depending on what range of energies was fit, and a second measurement of the spectrum 2 years later yielded a best fit parameter of $a = -0.63 \pm 0.05 \text{ MeV}^{-1}$.

The Borexino collaboration attempted to measure the shape of the ^{14}C beta spectrum using their counting test facility (CTF). They assumed the same functional form as the Wietfeldt paper and excluded all $a < -0.72 \text{ MeV}^{-1}$ with 90% confidence[13].

Most recently, V. Kuzminov and N. Osetrova measured the shape factor of the ^{14}C beta decay using a wall-less proportional counter[52]. They assumed a shape factor with the form, $C(E) = 1 + \beta(Q - T)$, with Q being the endpoint energy and T being the kinetic energy of the electron. They measured $\beta = 1.24 \pm 0.04 \text{ MeV}^{-1}$, which is in agreement with a theoretical calculation by Genz et. al.[42]. This result is equivalent to $a =$

-0.68 ± 0.02 MeV $^{-1}$ in a Wietfeldt-style shape factor and is very close to both the Borexino measured limit, as well as the second Wietfeldt measurement.

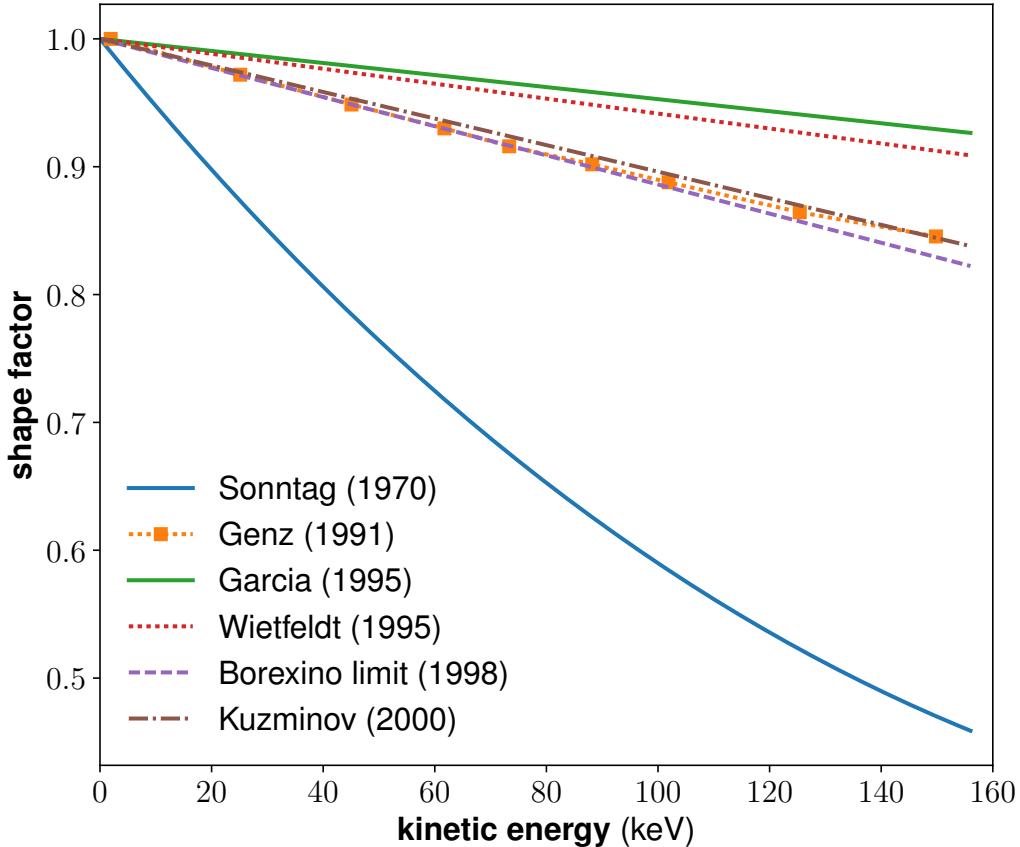


Figure 5.4: Various measurements and theoretical calculations of the ^{14}C shape factor. They have all been normalized to equal 1 at kinetic energy=0 keV. The Sonntag[72], Wietfeldt[79], Borexino[13], and Kuzminov[52] lines are all experimental measurements, while the Genz[42] and Garcia[41] lines are theoretical calculations. It is clear that the Sonntag result is strongly disfavored by all subsequent experiments and theoretical calculations. This figure also shows Genz, Borexino, Kuzminov, as well as the second Wietfeldt result (not shown) all converging around $C(E) \approx 1 - (0.7 \text{ MeV}^{-1})E$. It would be difficult, however, to claim this as consensus because the only true measurement in this subset is the Kuzminov line. Neither the Borexino paper nor the Wietfeldt paper claim a strong measurement of the shape factor.

5.2 Accounting for Finite Detector Resolution

The carbon-14 injection was based on the tritium calibration, which was first performed in August of 2013, after the first LUX data run was completed. The data from this calibration was used to calculate the energy deposition properties of electronic recoils in liquid xenon. To this end, a method was developed by Attila Dobi which deconvolved the effects of detector-resolution from the interesting physics involved in the process[8, 30].

5.2.1 Gaussian Energy Resolution and Continuous Beta Spectra

This deconvolution of detector resolution is necessary because of the continuous nature of beta spectra. We do not know the true deposition energy, E_{true} , of any given event and only have access to the reconstructed energy, $E_{rec} = W(n_\gamma + n_e)$, where $n_\gamma \equiv \frac{S_{1c}}{G1}$ and $n_e \equiv \frac{S_{2c}}{G2}$, where the subscript “c” indicates an efficiency-corrected value. In the Run03 measurements, the reconstructed energy of any event would be drawn from a Gaussian distribution centered at the true deposition energy, with the width of this distribution being the energy resolution, σ_E .

When this Gaussian smearing is applied to a continuous spectrum with a non-zero slope, it will create a systematic offset the measured reconstructed energy from the true energy. We take the spectrum shown in figure 5.5 as an example. The true energy of the events is distributed at discrete energies, 10, 20, 30, up to 150 keV. We apply Gaussian smearing with a constant resolution of $\sigma_E = 6$ keV to give us our reconstructed energy spectrum. When we take a small slice in reconstructed energy, from 79.75 to 80.25 keV, we find that the average true energy of events in this slice is systematically offset to 79.53 ± 0.09 keV. This offset is due to the negative slope of the true energy spectrum. The lower energy bins are more prominent than the higher energy ones, and therefore will have more events smear into our reconstructed energy slice.

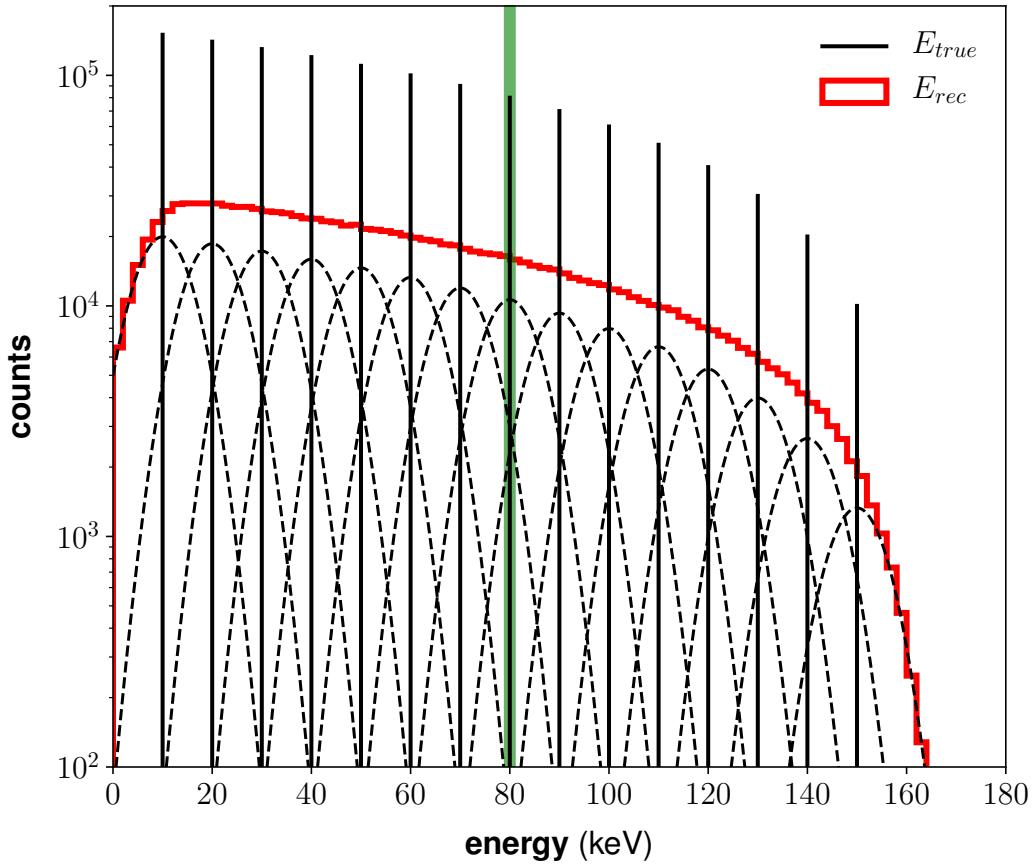


Figure 5.5: Smearing of a discrete, linearly falling spectrum. The true energy of the events is distributed at $(10, 20, 30, \dots, 150)$ keV, as indicated by the solid black lines. The number of events at each energy decreases linearly. We then apply Gaussian smearing with a flat resolution of 6 keV to the true energy (dashed lines). The reconstructed energy (red histogram) shows the resulting spectrum. The average true energy of events in a slice from $79.75 \text{ keV} < E_{rec} < 80.25 \text{ keV}$ (green area) is 70.65 ± 0.09 keV. This average is offset from the selected energy due to smearing.

It is possible to calculate this offset explicitly by integrating the contribution from each individual Gaussian. The number of events contributed to our reconstructed energy slice

by the i^{th} true energy bin will be given by:

$$\begin{aligned}
A_{80,i} &= \int_{79.75}^{80.25} N_i G(x; E_{true,i}, \sigma_E) dx \\
&= \int_{79.75}^{80.25} \frac{N_i}{\sqrt{2\pi\sigma_E^2}} \exp\left(\frac{-(x-E_{true,i})^2}{2\sigma_E^2}\right) dx \\
&= \frac{N_i}{2} \left(\operatorname{erf}\left(\frac{80.25-E_{true,i}}{\sqrt{2\sigma_E^2}}\right) - \operatorname{erf}\left(\frac{79.75-E_{true,i}}{\sqrt{2\sigma_E^2}}\right) \right)
\end{aligned} \tag{5.9}$$

where, $N_i = C(16 - i)$ is the number of events generated for the i^{th} discrete energy, and C is a scaling constant. The expected mean true energy, v_{80} , of events in the slice will then be given by:

$$v_{80} = \frac{\sum_i E_{true,i} A_{80,i}}{\sum_i A_{80,i}} \tag{5.10}$$

For the stated values of N_i , $E_{true,i}$, and σ_E , equation 5.10 yields $v_{80} = 79.56$ keV, which is consistent with the result found in the previous paragraph.

Equation 5.9 can be used to recenter an arbitrary reconstructed energy bin. This correction will be most important for energy regions where the spectrum in question is steeply changing and at its endpoints. For instance, if we take a reconstructed energy slice of our toy spectrum from 149.75 to 150.25 keV, the predicted low-energy bias goes from 0.44 keV as it was for the 80 keV slice, to 3.5 keV. This prediction is consistent with the measured bias of 3.4 ± 0.2 keV.

We can generalize equations 5.9 and 5.10 to apply to decays with continuous energy spectra. If the energy resolution of the detector, $\sigma_E(E)$, and the shape of the spectrum, $\frac{dN}{dE}$, are both known, equations 5.9 and 5.10 can be rewritten:

$$A(E; E_1, E_2) = \frac{1}{2} \frac{dN}{dE} \left(\operatorname{erf}\left(\frac{E_2-E}{\sqrt{2\sigma_E(E)^2}}\right) - \operatorname{erf}\left(\frac{E_1-E}{\sqrt{2\sigma_E(E)^2}}\right) \right), \tag{5.11}$$

and:

$$v(E_1, E_2) = \frac{\int A(E, E_1, E_2) EdE}{\int A(B_1, B_2) dE}, \quad (5.12)$$

where E_1 and E_2 are the edges of the reconstructed energy slice. The calculated $v(E_1, E_2)$ can then be used to recenter the arbitrary reconstructed energy bin to the average true energy of events in that bin.

5.2.2 Gaussian Smearing in the Combined Energy Model

In the previous section, we presented a method for calculating the average true energy, $v(E_1, E_2)$, of beta-events in a reconstructed energy bin, given precise knowledge of the beta-decay spectrum and detector resolution. The question remains whether the events within that bin are representative of its average true energy. Specifically, we would like to derive a relationship between the average number of photons and electrons measured from events in the bin ($\langle n_\gamma \rangle_i$ and $\langle n_e \rangle_i$) and the average number of photons and electrons that would be produced by a mono-energetic decay located at $v(E_1, E_2)$ ($\langle N_\gamma \rangle_v$ and $\langle N_e \rangle_v$).

There are many factors to take into account when considering this question. First, we would again need to know the shape of the beta spectrum. In addition to the combined energy resolution, we also need knowledge of the individual electron and photon resolutions, which we will define as $\sigma_{e,det}$ and $\sigma_{\gamma,det}$ respectively. We also need to consider the energy-dependent charge yield ($QY \equiv \langle N_e \rangle / E_{true}$) and light yield ($LY \equiv \langle N_\gamma \rangle / E_{true}$), as well as the size of the fluctuations in the recombination process, σ_R .

In figure 5.6 we have applied detector resolution to a toy spectrum comprised of 3 discrete energies, 45, 50, and 55 keV. We simulate a steeply falling spectral shape by distributing the events in a ratio of (4:2:1) between the stated energies. We calculate $\langle N_\gamma \rangle$ and $\langle N_e \rangle$ using a constant electron fraction, $y \equiv \frac{\langle N_e \rangle}{E_{true}/W} = 0.5$, where the work function, $W = 1/73$. We apply recombination fluctuations with a magnitude of $\sigma_R=214.3$ quanta,

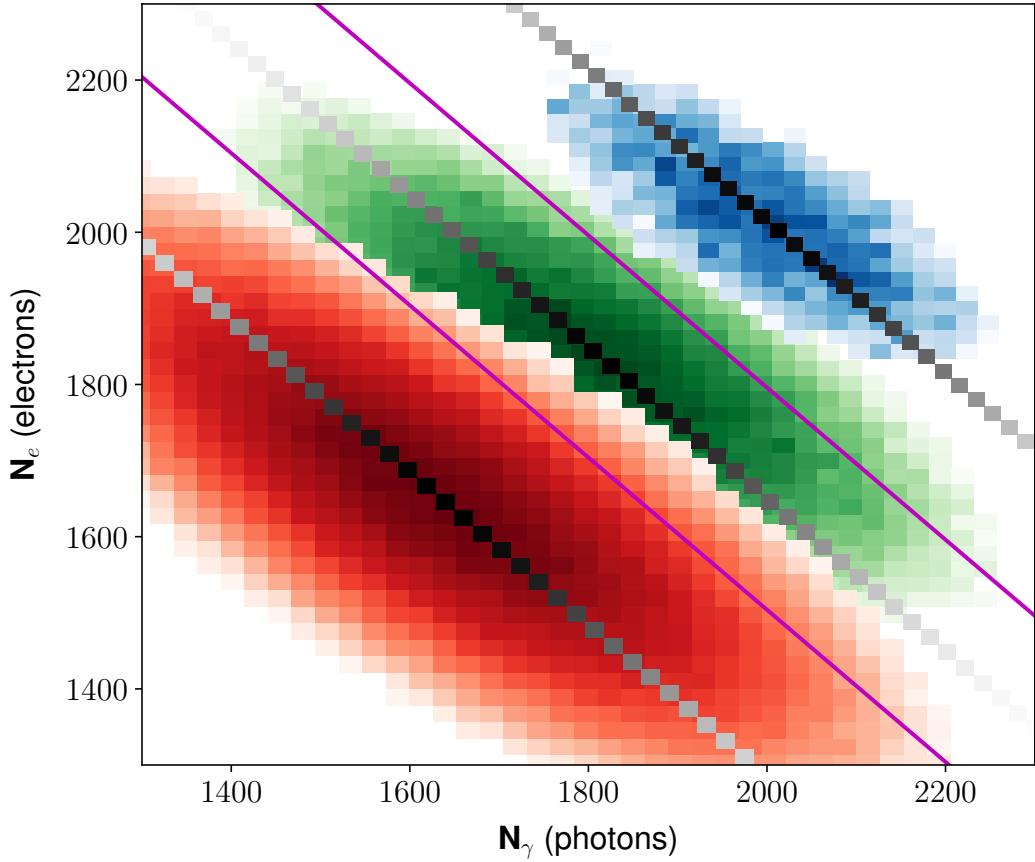


Figure 5.6: Detector resolution applied to a toy spectrum using the combined-energy model. Events are generated at 45 (red), 50 (green), and 55 (blue) keV. The greyscale diagonals indicate smearing along lines of constant energy. The blue, green, and red populations show the distribution of events after detector resolution is modeled.

which is the predicted value for a 50 keV decay from [30]. This gives $N_e = N(\langle N_e \rangle, \sigma_R)$ and $N_\gamma = E_{true}/W - N_e$, where $N(\mu, \sigma)$ is a random normal distribution. To produce the measured values of n_e and n_γ , we apply electron and photon resolutions of $\sigma_{e,det} = 1 \cdot \sqrt{N_e}$ and $\sigma_{\gamma,det} = 4 \cdot \sqrt{N_\gamma}$, which are roughly characteristic of the LUX detector.

We investigate the effect of detector resolution on this toy spectrum by selecting events that fall between 48 and 52 keV in reconstructed energy. As expected from the previous

section, the average true energy, $v(48,52) = 49.24 \pm 0.08$ keV, has a downward bias from 50 keV. This is consistent with predictions from the previous section.

An important observation to make here is that σ_R is expected to be correlated with $\sigma_{e,det}$ and $\sigma_{\gamma,det}$. Consider two events from the 50 keV population, one with $N_e = \langle N_e \rangle + \sigma_R$ and one with $N_e = \langle N_e \rangle - \sigma_R$. The first event would have about 27% more electrons than the second, while the second event would have about 27% more photons than the first. Taking into account the dependence of $\sigma_{e,det}$ and $\sigma_{\gamma,det}$ on N_e and N_γ we find that the second event would have a 19% larger combined energy resolution than the first. Events drawn from the 50 keV population will therefore be biased to lower values of n_γ and higher values of n_e because the population is narrower and therefore more dense in this region. In our toy model look at events from the 50 keV population that are selected by our reconstructed energy slice and find that the average N_γ of these events is 1816 ± 3 photons, while the true mean of N_γ for events in the 50 keV population is 1825 photons. The opposite effect is seen when looking at N_e , whose mean is 1833 ± 3 electrons for binned events.

This bias will be offset, at least to some degree by an opposing effect on the 45 and 55 keV populations. These populations will also be wider at high values of N_γ , and so our reconstructed energy slice will select more events from these regions than from the associated low- N_γ regions. In our slice we find that the 45 keV line contributes events with an average N_γ of 1770 ± 5 photons. This is compare to the true average of 1642.5 photons. Similarly, the 55 keV line contributes events with an average N_γ of 2027 ± 12 photons, compared to its true average of 2007.5 photons.

For the model we have described, it turns out that all of the competing effects on N_γ and N_e cancel out, and the averages for events in our reconstructed energy slice are consistent with what is expected for the measured value of $v(48,52) = 49.24 \pm 0.08$ keV. The expected (N_γ, N_e) for a decay with energy 49.24 ± 0.08 is $(1797, 1797) \pm (3, 3)$ quanta, while the observed values were $(1799, 1796) \pm (3, 3)$ quanta. The effects also cancel for a slice

centered at 55 keV, but a small offset of 7 ± 3 quanta is observed in a slice at 45 keV.

We also modified the model to allow for a changing electron-fraction. We set $y = 0.52$, 0.5, and 0.48 for the 45, 50, and 55 keV populations, respectively. With this modified model, the observed averages in the 50 and 55 keV bins are no longer consistent with what is expected from the measured v . This indicates that any smearing correction to be applied to map $(\langle n_\gamma \rangle, \langle n_e \rangle)$ to $(\langle N_\gamma \rangle, \langle N_e \rangle)$ will be largely determined by the energy dependence of electron and photon yields.

$E_{rec,i}$ (keV)	v (keV)	\pm	$\langle N_\gamma \rangle_i$	$\langle N_\gamma \rangle_v$	\pm	$\langle N_\gamma \rangle_{obs}$	\pm	$\langle n_\gamma \rangle$	\pm
constant y	-	-	-	-	-	-	-	-	-
45	45.39	0.06	1642.5	1657	2	1650	2	1627	2
50	49.24	0.08	1825.0	1797	3	1799	3	1840	3
55	53.65	0.12	2007.5	1958	4	1758	4	2035	5
falling y	-	-	-	-	-	-	-	-	-
45	45.39	0.06	1576.8	1590	2	1590	2	1567	2
50	49.27	0.08	1825.0	1799	3	1792	3	1830	3
55	53.64	0.12	2087.8	2036	5	2018	5	2093	5

Table 5.1: Measurements of the average number of photons generated by our toy model. $E_{rec,i}$ is the center of the respective reconstructed energy slice. Each slice extends 2 keV to either side of $E_{rec,i}$. $\langle N_\gamma \rangle_i$ indicates the predicted number of photons for an event with energy equal to $E_{rec,i}$. $\langle N_\gamma \rangle_v$ is the predicted number of photons generated by an event with energy equal to the measured value of v . $\langle N_\gamma \rangle_{obs}$ is the average number of photons generated by events that were observed to fall into the energy slice. $\langle n_\gamma \rangle$ is the average of the measured number of photons in the slice.

In table 5.1 we show the results of the predicted number of photons in an energy slice versus the observed averages of the true number of photons from the event, $\langle N_\gamma \rangle$, as well as of the measured number of photons, $\langle n_\gamma \rangle$. We have not shown the results for the number of electrons because any offsets should be anti-symmetric to the photon offsets.

The ultimate purpose of this exercise is to find an expression for the ratio of the observable $\langle n_\gamma \rangle$ to the underlying physics contained in $\langle N_\gamma \rangle_v$. Any offset of $\langle N_\gamma \rangle_{obs}$ will be absorbed into an overall correction factor of $C_\gamma \equiv \frac{\langle N_\gamma \rangle_v}{\langle n_\gamma \rangle}$. The predicted true average number

of photons is given by:

$$\langle N_\gamma \rangle_v \equiv vLY, \quad (5.13)$$

where LY is the light yield in photons per keV.

The prediction for the measured mean, $\langle n_\gamma \rangle$, is more difficult to calculate. Without recombination fluctuations, the number of photons and electrons, N_γ and N_e , from an event with energy E would follow a 2-dimensional Gaussian:

$$G_E(N_\gamma, N_e) = \frac{1}{2\pi\sigma_{e,det}\sigma_{\gamma,det}} \exp\left(-\frac{(N_e - \langle N_e \rangle)^2}{2\sigma_{e,det}^2} - \frac{(N_\gamma - \langle N_\gamma \rangle)^2}{2\sigma_{\gamma,det}^2}\right). \quad (5.14)$$

In this case, we could calculate $\langle n_\gamma \rangle$ by integrating the overlap of the distributions from the three energy populations with the energy slice:

$$\langle n_\gamma \rangle_{E_1, E_2} = \frac{\sum_i N_i \int_{-\infty}^{\infty} \int_{E_1/W-N_e}^{E_2/W-N_e} N_\gamma G_{E_i}(N_\gamma, N_e) dN_\gamma dN_e}{\sum_i N_i \int_{-\infty}^{\infty} \int_{E_1/W-N_e}^{E_2/W-N_e} G_{E_i}(N_\gamma, N_e) dN_\gamma dN_e}. \quad (5.15)$$

When recombination fluctuation are present, we will also have to integrate over the size of the recombination fluctuation, R , which is measured in quanta. The distribution of events at a given energy, E , then becomes:

$$D_E(N_\gamma, N_e) = \frac{1}{(2\pi)^{3/2}\sigma_{e,det}\sigma_{\gamma,det}\sigma_R} \times \int_{-\infty}^{\infty} \exp\left(-\frac{R^2}{2\sigma_R^2} - \frac{(N_e - (\langle N_e \rangle - R))^2}{2\sigma_{e,det}^2} - \frac{(N_\gamma - (\langle N_\gamma \rangle + R))^2}{2\sigma_{\gamma,det}^2}\right) dR \quad (5.16)$$

We would then replace $G_{E_i}(N_\gamma, N_e)$ with $D_{E_i}(N_\gamma, N_e)$ in equation 5.15 to find the photon smearing correction.

We can generalize equation 5.15 for use with continuous spectra by replacing the sum

over the energy states with an integral as we did in equation 5.12:

$$\langle n_\gamma \rangle_{E_1, E_2} = \frac{\int \frac{dN}{dE} \int_{-\infty}^{\infty} \int_{E_1/W-N_e}^{E_2/W-N_e} N_\gamma D_E(N_\gamma, N_e) dN_\gamma dN_e dE}{\int \frac{dN}{dE} \int_{-\infty}^{\infty} \int_{E_1/W-N_e}^{E_2/W-N_e} D_E(N_\gamma, N_e) dN_\gamma dN_e dE}. \quad (5.17)$$

Similarly for the electron smearing correction we would have:

$$\langle n_e \rangle_{E_1, E_2} = \frac{\int \frac{dN}{dE} \int_{-\infty}^{\infty} N_e \int_{E_1/W-N_e}^{E_2/W-N_e} D_E(N_\gamma, N_e) dN_\gamma dN_e dE}{\int \frac{dN}{dE} \int_{-\infty}^{\infty} \int_{E_1/W-N_e}^{E_2/W-N_e} D_E(N_\gamma, N_e) dN_\gamma dN_e dE}. \quad (5.18)$$

Before moving on, it is important to compare our results with the work done for the Run03 tritium injection[8, 30]. We have derived an equivalent expression for energy-smearing, but our equations 5.17 and 5.18 are in tension with the Run03 corrections applied to n_e and n_γ . The Run03 work derived smearing corrections for n_e and n_γ using a method equivalent to the energy smearing corrections described by equations 5.11 and 5.12, treating the two as independent variables. The populations of N_e and N_γ for events selected by an energy slice are not expected to be independent of one another, so we now believe the Run03 corrections for the individual channels are in error. If we had binned in N_e as opposed to E_{rec} , equations 5.11 and 5.12 would be appropriate to correct for the smearing of N_e , however, a new set of corrections would have to be derived for E_{rec} .

5.3 Detector Resolution in Post-Run04

We have a good hold on the beta spectra for both tritium and carbon-14 and on the detector resolutions, but LY , QY , and σ_R are the precise quantities we are attempting to measure in this document. This means that we will need to apply an iterative process to measure the energy deposition properties. A first pass analysis would give us the preliminary values of LY , QY , and σ_R , from which we would calculate how to deconvolve the

detector resolution from the recombination physics.

In this section will develop a method of smearing corrections which can be used on the LUX Post-Run04 data. We will extract preliminary measurements of LY , QY , and σ_R using the existing NEST model. We will use these measurements to adjust the NEST model in order to refine our final measurements, which will be presented in section 5.5.

5.3.1 Non-Gaussian Smearing

The results from the previous sections, shown in equations 5.11, 5.12, 5.16, 5.17, and 5.18 provide a powerful correction method for experiments with Gaussian detector resolution. Unfortunately, the resolution of LUX Run04 and post-Run4 data is not Gaussian. The pathological S2 tails make the S2 and energy resolution approximately exponential to the high-energy side while leaving it roughly Gaussian on the low-energy side.

The altered shape of the energy resolution makes equations 5.11 and 5.16 incorrect. It should be possible to re-derive expressions for $A(E_1, E_2)$ and $D_E(N_\gamma, N_e)$ by using a non-Gaussian functional form for the smearing of energy and N_e :

$$A(E, E_1, E_2) = \int_{E_1}^{E_2} \frac{dN}{dE} S_E(x; E, \dots) dx, \quad (5.19)$$

$$D_E(N_\gamma, N_e) = \int G(R; 0, \sigma_R) G(N_\gamma; \langle N_\gamma \rangle, \sigma_{\gamma, det}) S_e(N_e; \langle N_\gamma \rangle, \dots) dR, \quad (5.20)$$

where $G(x; \mu, \sigma)$ is the typical one-dimensional Gaussian distribution, $S_E(x; E, \dots)$ is a generalized smearing function for energy, centered at E and evaluated at x , and $S_e(N_e; \langle N_\gamma \rangle, \dots)$ is the generalized resolution function for N_e .

A good candidate for both S_E and S_e is the Crystal Ball function[65]. This function, as well as the Gaussian-Exponential function, a more numerically efficient alternative to the

crystal ball function[28], have both been applied to LUX Run04 data with some success. The Crystal Ball function was first developed to model the resolution of the Crystal Ball detector and is a continuously-differentiable piecewise function, which combines a Gaussian with a power-law tail:

$$f_{CB}(x; \alpha, n, \bar{x}, \sigma) = \begin{cases} e^{-\frac{(x-\bar{x})^2}{2\sigma^2}} & \text{for } \frac{x-\bar{x}}{\sigma} > -\alpha \\ \left(\frac{n}{|\alpha|}\right)^n e^{-\frac{|\alpha|^2}{2}} \left(\frac{n}{|\alpha|} - |\alpha| - \frac{x-\bar{x}}{\sigma}\right)^{-n} & \text{for } \frac{x-\bar{x}}{\sigma} \leq -\alpha \end{cases} \quad (5.21)$$

The Gaussian-Exponential function replaces the power-law tail with an exponential tail, making it a clear analytic analog to the model of the S2 tails developed in section 4.4:

$$f_{GE}(x; \bar{x}, \sigma, k) = \begin{cases} e^{-\frac{(x-\bar{x})^2}{2\sigma^2}} & \text{for } \frac{x-\bar{x}}{\sigma} > -k \\ e^{\frac{k^2}{2} + k(\frac{x-\bar{x}}{\sigma})} & \text{for } \frac{x-\bar{x}}{\sigma} \leq -k \end{cases} \quad (5.22)$$

5.3.2 Numerical De-Smeared with libNEST

Either of the equations shown in 5.21 and 5.22 would make the calculation of the smearing corrections extremely cumbersome. Additionally, if there is additional correlation between $\sigma_{e,det}$, $\sigma_{\gamma,det}$, and σ_R that we have not accounted for the correction factors we calculate would be wrong. For these reasons, we elect to instead calculate the smearing corrections for E_{rec} , N_γ , and N_e numerically. In the libNEST code, we have a well-developed and well-tested model of the LUX detector resolution that is perfectly suited to this purpose. The libNEST code also models the energy threshold, which will also have an effect on the observed spectral shape but was not included in our calculations up to this point. With the addition of the model of the S2 tails developed in section 4.4, we will also be able to characterize and quantize the systematic effects that they introduce to our yields

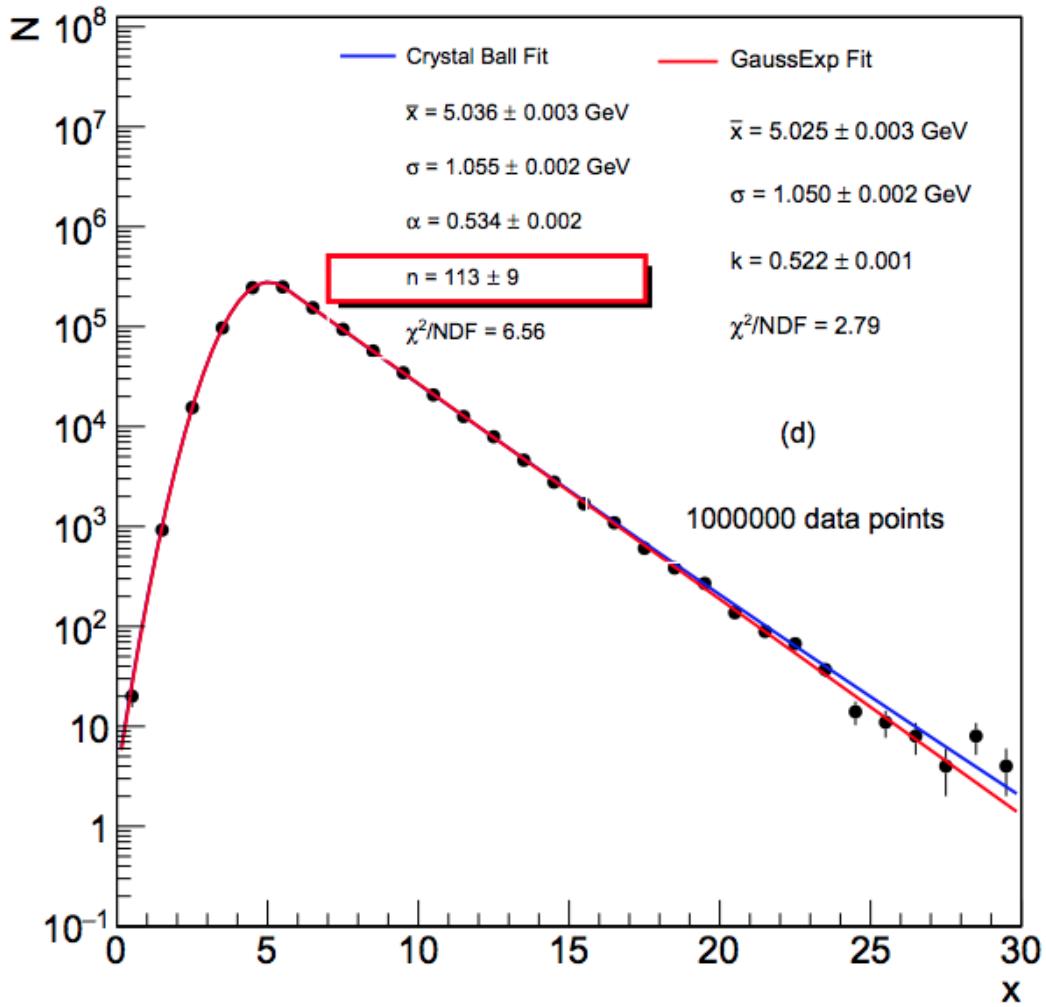


Figure 5.7: Comparison of fits to data using the Crystal Ball function and the Gaussian-Exponential. Figure taken from [28].

and recombination measurements.

We will begin by defining a set of energy bins to go along with the electric field bins we defined in section 4.1.3. Then we will use the existing libNEST yields and recombination

model to extract a set of corrections for energy, N_e , and N_γ :

$$C_{E,ij} = \frac{\langle E_{input} \rangle_{ij}}{\langle E_{rec,NEST} \rangle_{ij}} \quad (5.23)$$

$$C_{\gamma,ij} = \frac{LY_{NEST}(\langle E_{true} \rangle_{ij}, \langle \mathcal{E} \rangle_j) \cdot \langle E_{input} \rangle_{ij}}{\langle n_{\gamma,NEST} \rangle_{ij}} \quad (5.24)$$

$$C_{e,ij} = \frac{QY_{NEST}(\langle E_{true} \rangle_{ij}, \langle \mathcal{E} \rangle_j) \cdot \langle E_{input} \rangle_{ij}}{\langle n_{e,NEST} \rangle_{ij}} \quad (5.25)$$

Here, $\langle \rangle_{ij}$ indicates an averaged value over events selected by both the i^{th} reconstructed energy bin and j^{th} electric field bin, as defined in section 4.1.3. E_{input} is the input energy of the events, and $n_{\gamma,NEST} = S1_{NEST}/G1$ and $n_{e,NEST} = S2_{NEST}/G2$ are the output charge and light signals after the yields, recombination, detector efficiency, and detector resolution have all been simulated. $G1$ and $G2$ are the overall light and charge efficiencies used in the libNEST model and will be set to be equal to those measured in the data. LY_{NEST} and QY_{NEST} are the input light and charge yields for events with an energy equal to $\langle E_{input} \rangle_{ij}$. In the existing libNEST model there is no explicit value defined for $LY_{NEST}(E, \mathcal{E})$ and $QY_{NEST}(E, \mathcal{E})$, but rather a combination of other parameters come together to reproduce LY and QY as a function of electric field and energy. For this reason, we will approximate $LY_{NEST}(\langle E_{input} \rangle_{ij}, \langle \mathcal{E} \rangle_j)$ and $QY_{NEST}(\langle E_{input} \rangle_{ij}, \langle \mathcal{E} \rangle_j)$ by generating a flat spectrum in libNEST, and measuring:

$$LY_{NEST}(\langle E_{input} \rangle_{ij}, \langle \mathcal{E} \rangle_j) \approx \langle N_{\gamma,NEST} \rangle_{ij} / \langle E_{input} \rangle_{ij} \quad (5.26)$$

$$QY_{NEST}(\langle E_{input} \rangle_{ij}, \langle \mathcal{E} \rangle_j) \approx \langle N_{e,NEST} \rangle_{ij} / \langle E_{input} \rangle_{ij},$$

where $N_{\gamma,NEST}$ and $N_{e,NEST}$ are the true number of photons and electrons simulated in the event, before detector resolution is applied, but after the recombination is simulated. The modified version of libNEST which will be used to calculate the corrections for the

final measurements will use explicit functions for $LY_{NEST}(E, \mathcal{E})$ and $QY_{NEST}(E, \mathcal{E})$, so the approximation shown in equation 5.26 will not be necessary.

We will apply these corrections to the average S1 and S2 signal measured in each reconstructed energy bin in order to produce the measured, un-smeared averages $\langle E_{true} \rangle_{ij}$, $\langle n_e \rangle_{ij}$, and $\langle N_\gamma \rangle_{ij}$:

$$\langle E_{true} \rangle_{ij} = C_{E,ij} \cdot \langle E_{rec} \rangle_{ij} \quad (5.27)$$

$$\langle N_\gamma \rangle_{ij} = C_{\gamma,ij} \cdot \langle n_\gamma \rangle_{ij} \quad (5.28)$$

$$\langle N_e \rangle_{ij} = C_{e,ij} \cdot \langle n_e \rangle_{ij} \quad (5.29)$$

where we have taken $W = \frac{1}{73.0 \pm 1.1}$ keV per quanta.

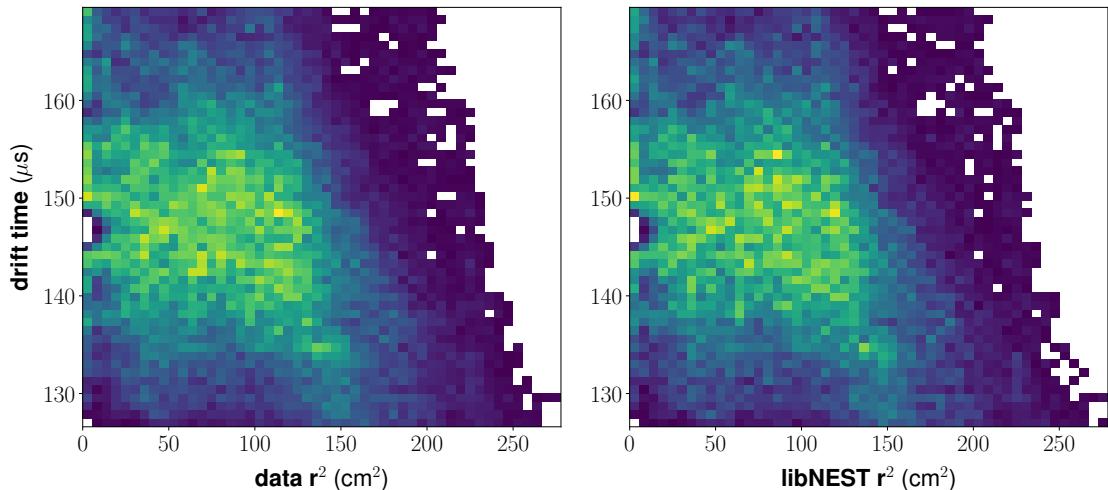


Figure 5.8: Selected carbon-14 events in the 180 V/cm electric field bin. Events from data are shown on the left, and libNEST simulated events are on the right.

5.3.3 Preliminary Measurement of QY

As an example, we will examine the measured corrections for the 180 V/cm field bin, using the “gfdcm” corrected data. A 2D-histogram of the radius-squared and drift time of the selected events for both data and libNEST simulation is shown in figure 5.8. The x-position, y-position, efficiency-correction factors, drift time, and electric field of the simulated events are all randomly drawn from the population of data events, so the two histograms in figure 5.8 are identical, except for random fluctuations. We define our re-

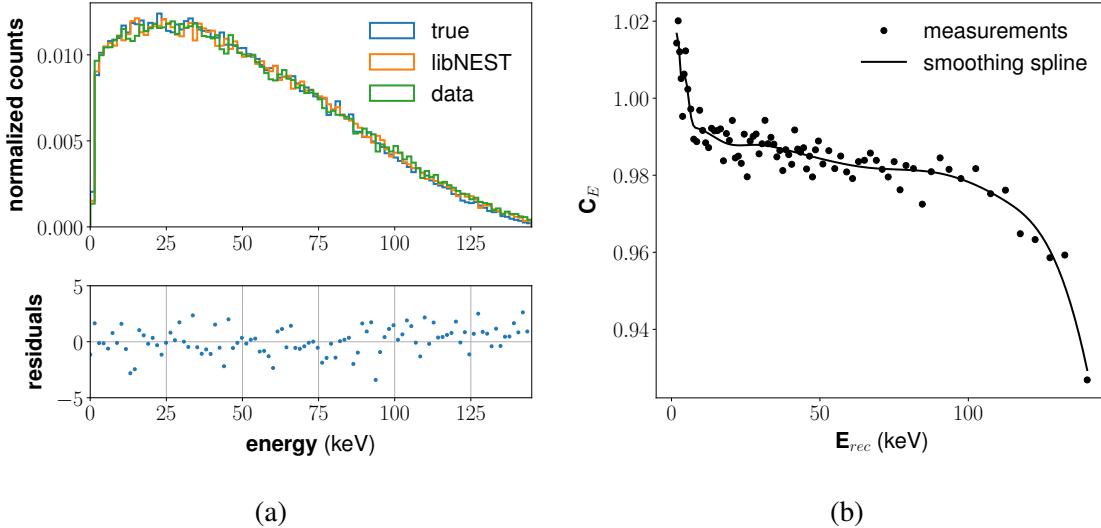


Figure 5.9: Carbon-14 spectrum (left) and the calculated energy smearing correction (right). The residuals show a comparison of the data spectrum with the libNEST simulated spectrum. There is decent agreement over the entire energy range, with the reduced chi-squared coming out to 1.4. The square markers in the right-hand plot show the calculated values of the correction factor, and the continuous black line shows the smoothing spline.

constructed energy bins such that there is an approximately constant number of events in each bin. From 1.5 to 5 keVee, we bin in steps of 0.5 keVee. We allow this region to have fewer counts in order to minimize the spread in energies within the bin. From there we incrementally increase the bin width to account for the falling $\frac{dN}{dE}$. The bin widths and their associated energy regions are shown in table 5.2.

Energy Range (keV)	1.5-5.0	5-50	50-80	80-95	95-135	135-145
Bin Width (keV)	0.5	1	2	3	5	10

Table 5.2: Reconstructed energy bin widths and their associated energy ranges

We first examine the measured carbon-14 energy spectrum and how it compares to the simulated spectrum which is shown in figure 5.9a. There is decent agreement between simulation and data; other than a possible small upward slope above 100 keV, there is no clear systematic trend in the residuals, and the reduced chi-squared is 1.4.

We calculate the energy smearing correction for each reconstructed energy bin as described in equations 5.23 and 5.26. Using the SciPy.interpolate “UnivariateSpline” tool with the smoothing factor set to 0.0005 [46], we smooth our newly measured set of $C_{E,i,180}$. We make adjustments to the smoothing factor as needed to make the spline well-conditioned and to make sure it picks up the first and last points.

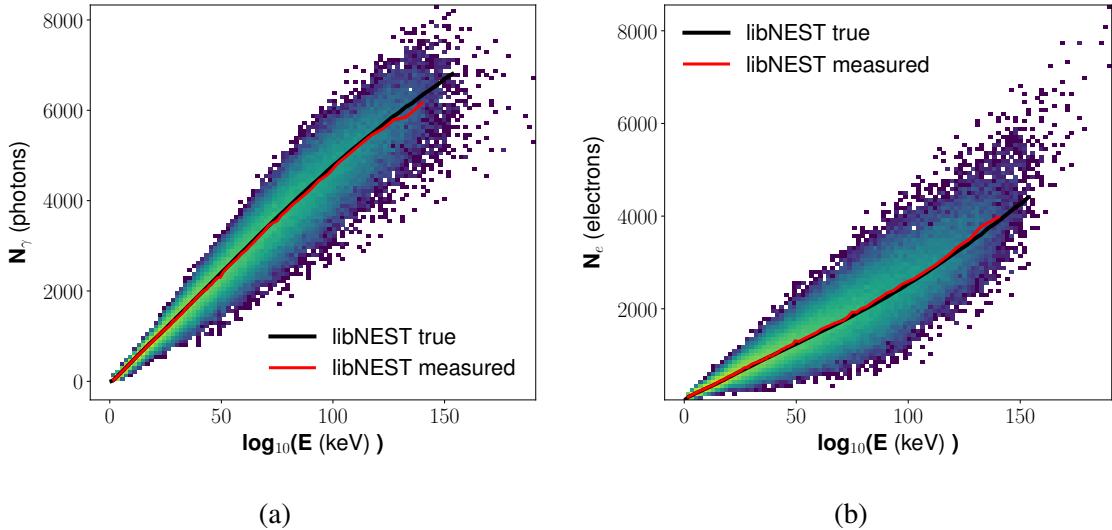


Figure 5.10: The red lines show the measurements of $\langle S1_{NEST}/G1 \rangle_{i,180}$ (a) and $\langle S2_{NEST}/G2 \rangle_{i,180}$ (b) for the preliminary carbon-14 model. The black lines show $\langle N_\gamma \rangle_{i,180}$ (a) and $\langle N_e \rangle_{i,180}$ (b).

The next step is to measure the smearing corrections for S1 and S2. Figure 5.10 (a) and (b) show the simulated bands of $n_{\gamma,NEST} = S1_{NEST}/G1$ and $n_{e,NEST} = S2_{NEST}/G2$

versus reconstructed energy. We first aim to measure the peak value of $n_{\gamma,NEST}$ in our set of reconstructed energy bins. In each of these bins, we take the arithmetic mean ($\bar{n}_{\gamma,NEST}$) and standard deviation ($\text{std}(n_{\gamma,NEST})$) of the $n_{\gamma,NEST}$ population. To reject the events which are most severely affected by the pathological tails, a further cut is made:

$$\bar{n}_{\gamma,NEST} - \text{std}(n_{\gamma,NEST}) < n_{\gamma,NEST} < \bar{n}_{\gamma,NEST} + 2 \cdot \text{std}(n_{\gamma,NEST}) \quad (5.30)$$

We then fit a Gaussian to the population of $n_{\gamma,NEST}$ which pass this cut. The peak value of this Gaussian in the i^{th} bin is taken to be $\langle n_{\gamma,NEST} \rangle_{i,180}$. We follow a similar procedure to find $\langle n_{e,NEST} \rangle_{i,180}$, but the selection cut is instead:

$$\bar{n}_{e,NEST} - 2 \cdot \text{std}(n_{e,NEST}) < n_{e,NEST} < \bar{n}_{e,NEST} + \text{std}(n_{e,NEST}) \quad (5.31)$$

With $\langle n_{\gamma,NEST} \rangle_{i,180}$ and $\langle n_{e,NEST} \rangle_{i,180}$ in hand, we now calculate C_γ and C_e using equations 5.24 and 5.25.

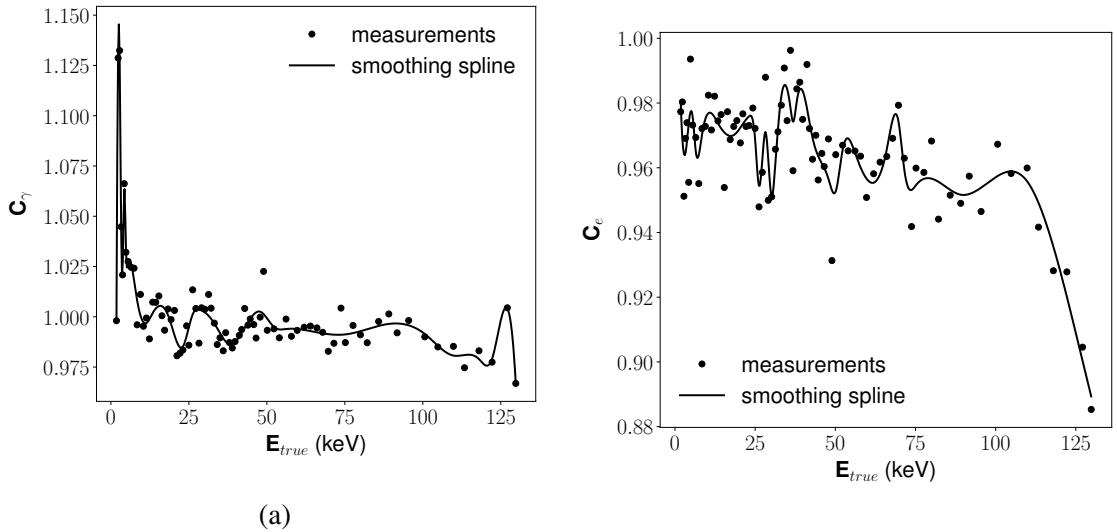


Figure 5.11: This figure shows the smearing correction for S1 (a) and S2 (b). The square markers show the calculated values of the correction factors, and the continuous black lines show the smoothing spline.

We calculate $\langle n_\gamma \rangle_{i,180}$ and $\langle n_e \rangle_{i,180}$ using the same method we used to calculate $\langle n_{\gamma,NEST} \rangle_{i,180}$ and $\langle n_{e,NEST} \rangle_{i,180}$. Finally, we can now obtain $\langle N_\gamma \rangle_{i,180}$ and $\langle N_e \rangle_{i,180}$ using equations 5.28 and 5.29, respectively. It is then simple to calculate the charge and light yield that we will use in our updated libNEST model:

$$LY_{i,180} = \frac{\langle N_\gamma \rangle_{i,180}}{\langle E_{true} \rangle_{i,180}} \quad (5.32)$$

$$QY_{i,180} = \frac{\langle N_e \rangle_{i,180}}{\langle E_{true} \rangle_{i,180}} \quad (5.33)$$

Figure 5.12 shows the results of our yields measurements. In these results, we have taken the size of the smearing correction to be our systematic error ($\sigma_{syst} = |1 - C|$). In defining these errors, we want to account for statistical fluctuations in the correction factor and one that is steeply sloped. If, for example, $|1 - C_{e,i}|$ is much greater than $|1 - C_{e,i-1}|$, then $|1 - C_{e,i}|$ is likely a better estimate of $\sigma_{e,syst,i}$ than $|1 - C_{e,i-1}|$. For this reason, we define $\sigma_{syst,i} = \max(|1 - C_{i-1}|, |1 - C_i|, |1 - C_{i+1}|)$.

The fitting error is taken as the statistical error and is shown as dark green error-bars in (c), and dark blue error-bars in (d). The light-colored error-bars in (c) and (d) show the systematic plus statistical uncertainties. Below about 15 keV there is good agreement between the existing NEST model (shown as the black lines in (c) and (d)) and the measurements. In this region, LY and QY was tuned by the measurements using LUX Run03 tritium, so good agreement is expected. Above this value, there are no measurements of beta-decay yields, and the discrepancy between data and NEST is large.

In the combined energy model, we assume that $LY + QY = 1/W$, where $1/W = 73 \pm 1.1$ quanta per keV. It is not necessary to define both LY and QY when generating a simulated event; we can instead define only QY and allow $LY = 73 - QY$. It would also be possible to

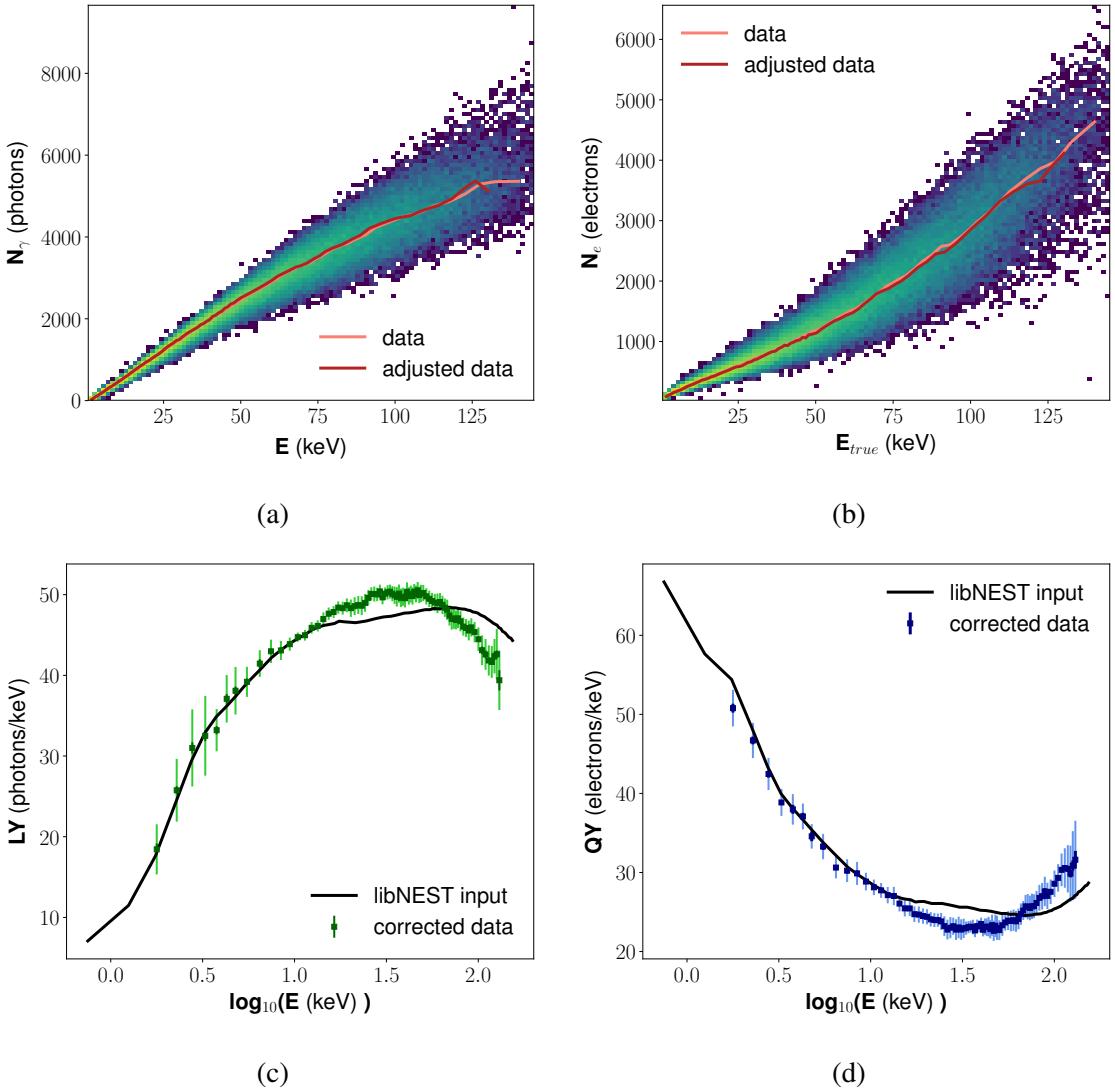


Figure 5.12: Preliminary measurements of $\langle N_\gamma \rangle_{i,180}$ (a) and $\langle N_e \rangle_{i,180}$ (b), along with the associated calculations of LY (c) and QY (d). In the top plots, (a) and (b), the heat-maps shows the measured, unadjusted populations of $n_\gamma = S1c/G1$ and $n_e = S2c/G2$. The light red lines show the unadjusted peak values versus unadjusted energy. The dark red lines show these trends after the smearing corrections are applied. The lower plots show the fully adjusted measurements of $LY = \langle N_\gamma \rangle_{i,180} / \langle E_{true} \rangle_{i,180}$, and $QY = \langle N_e \rangle_{i,180} / \langle E_{true} \rangle_{i,180}$. The light colored error-bars show the systematic+statistical uncertainty, while the darker error-bars show the statistical uncertainty alone. The black lines show the existing NEST values of LY and QY .

define LY and let $QY = 73 - LY$, but measurements of LY tend to have larger uncertainties because the $S1$ signal has a smaller gain than the $S2$ signal.

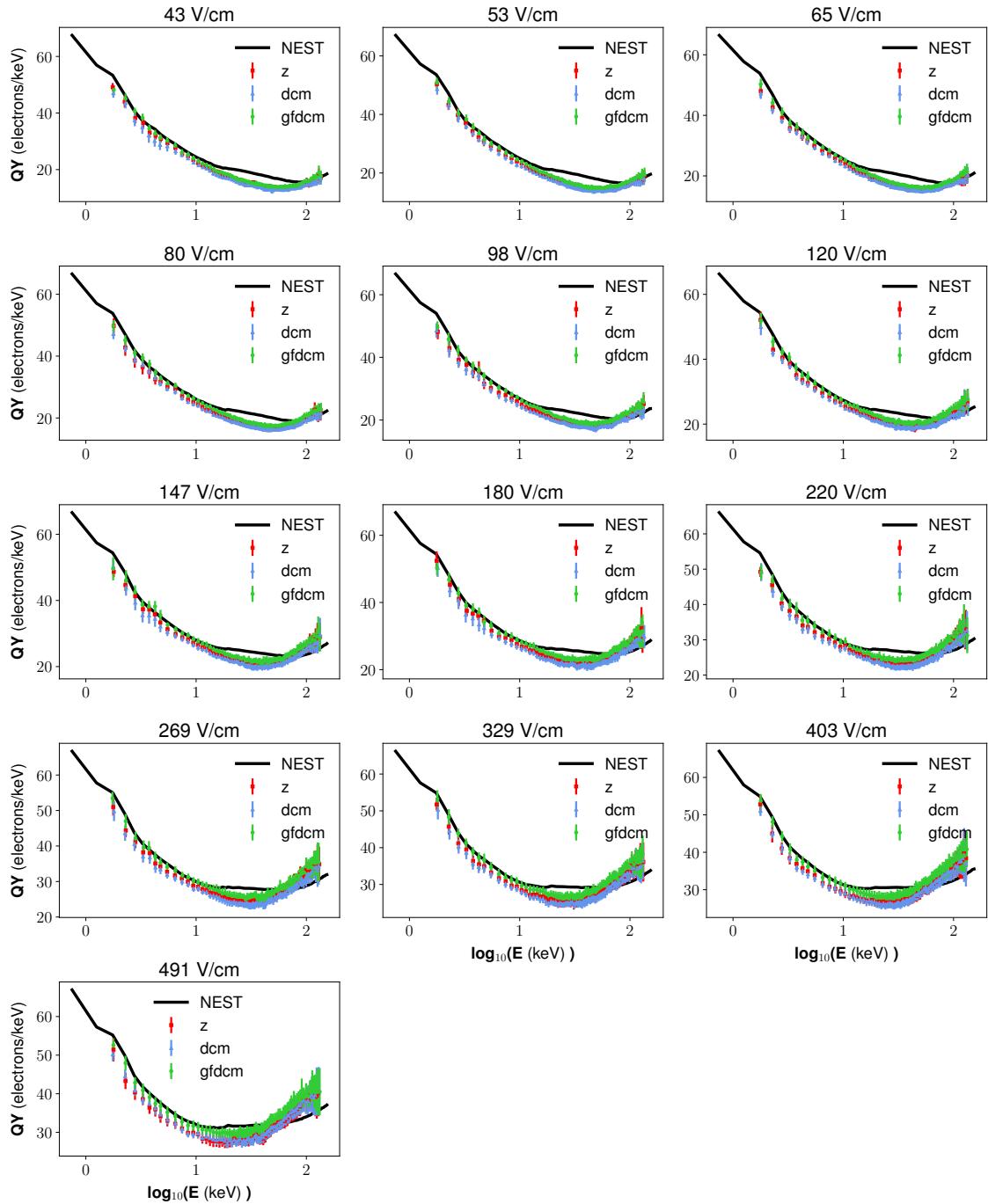


Figure 5.13: Preliminary carbon-14 charge yield for the three efficiency corrections being studied, in each of the 13 electric field bins defined in 4.1.3. The x-axis here represents the true event energy, obtained by applying the smearing corrections. The charge yields measured here will be used to fine-tune the NEST model in order to obtain a more accurate set of corrections.

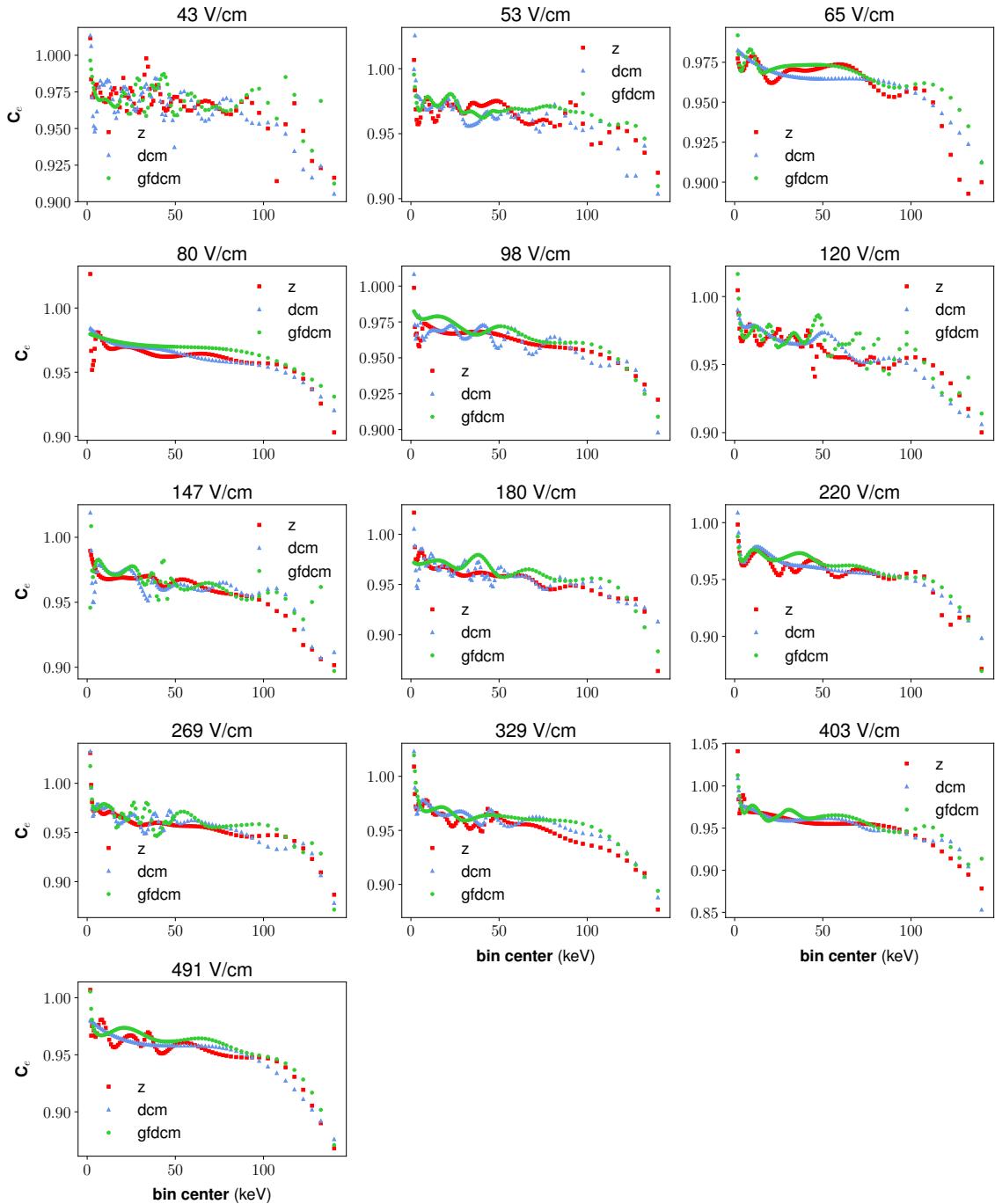


Figure 5.14: Carbon-14 energy smearing correction factors for the three efficiency corrections being studied, in each of the electric field bins. The x-axis shows the central value the reconstructed energy bin for which the correction factor is calculated.

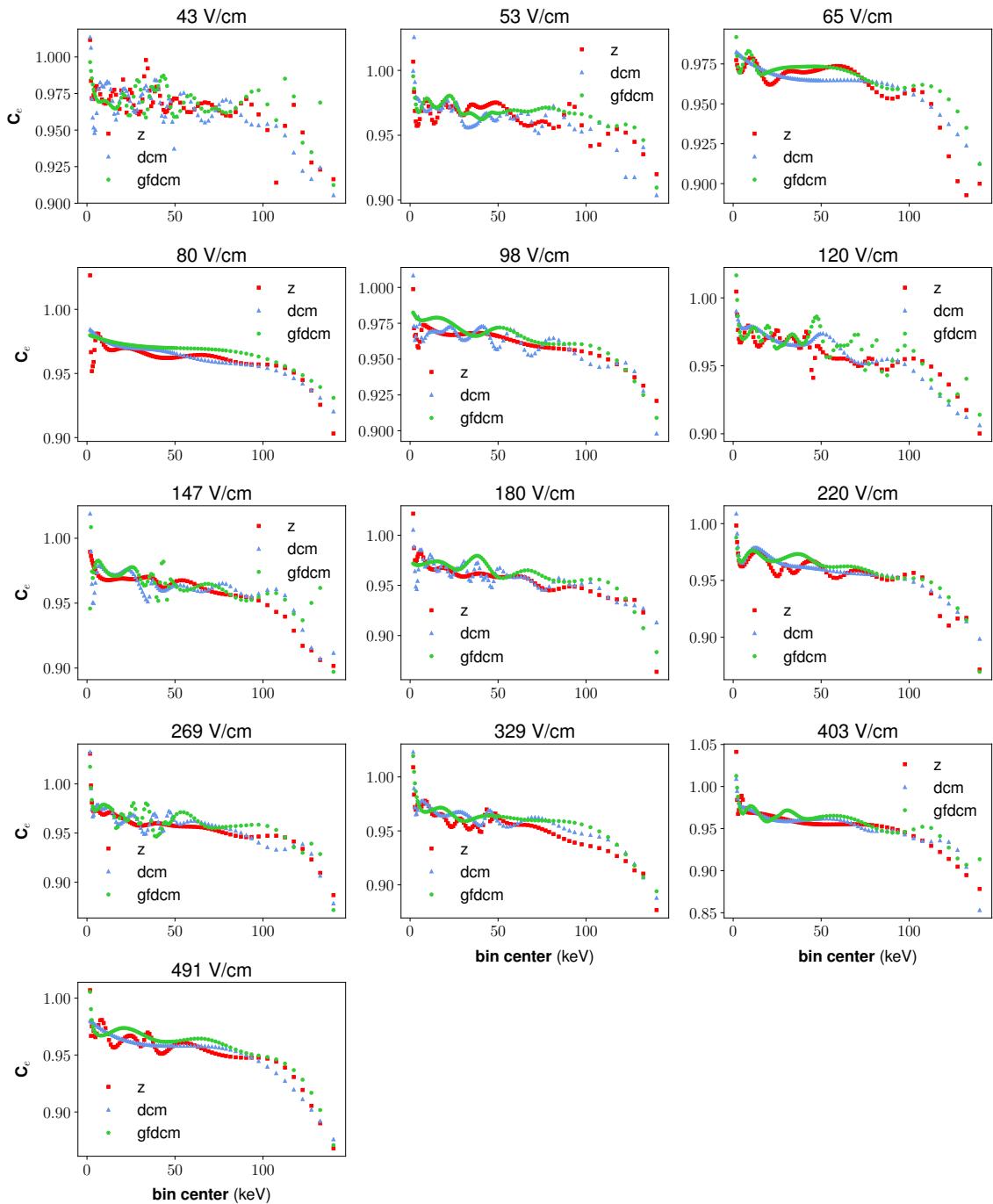


Figure 5.15: Carbon-14 S2 smearing correction factors for the three efficiency corrections being studied, in each of the electric field bins. The x-axis shows the central value the reconstructed energy bin for which the correction factor is calculated.

The measured values of QY_{ij} for all of the electric field bins is shown in figure 5.13. The smearing corrections that go into calculating these values are shown in figures 5.14 and 5.15. We have shown the results measured using the three corrections-types described in section 4.3; “z”, “dcm”, and “gfdcm”. The “gfdcm” measurements of QY are systematic higher than the other two corrections types and are more consistent with the Run03 values.

The same procedure that was used for carbon-14 was also performed on the post-Run04 tritium data. The reconstructed energy bins used for tritium are described in table 5.3. The results for tritium in the 180 V/cm electric field bin are shown in figure. 5.16. The energy spectrum, including the threshold, is well modeled by libNEST. The reduced chi-squared difference between the libNEST and data spectra on an energy range from 0 to 20 keV is 1.5.

Energy Range (keV)	1-2	2-6	6-10	10-14	14-18
Bin Width (keV)	0.5	0.2	0.5	1	2

Table 5.3: Tritium reconstructed energy bin widths and their associated energy ranges.

The smearing corrections are obtained in the same way as for carbon-14. The effect of the threshold on the smearing corrections can be most clearly seen in the first few energy bins, where C_γ drops sharply from about 0.8 to 1.1 in the space of two energy bins. The S2 correction, C_e , also sees a large jump in these bins; it falls from about 1.4 to 0.98. The resulting charge yield measurements are in good agreement both with those for carbon-14 and with the existing libNEST model. In the next section, we will combine the charge yields from carbon-14 and tritium with measurements from other experiments in order to find an equation for $QY_{NEST}(E, \mathcal{E})$.

5.3.4 Preliminary Energy- and Field-Dependent Charge Yield Model

The first step in finding an expression for $QY_{NEST}(E, \mathcal{E})$ is to choose a functional form. Historically, NEST has relied heavily on sigmoids to express the energy and field dependence of physical quantities:

$$F(x) = p_1 + \frac{p_2 - p_1}{1 + (x/p_3)^{p_4}} \quad (5.34)$$

For the purpose of characterizing the charge yield, we found that a combination of two asymmetric sigmoids is best able to reproduce the measurements at all fields and energies:

$$QY_{NEST}(E, \mathcal{E})|_{\mathcal{E}_1} = m_1 + \frac{m_2 - m_1}{(1 + (E/m_3)^{m_4})^{m_9}} + m_5 + \frac{0 - m_5}{(1 + (E/m_7)^{m_8})^{m_{10}}}, \quad (5.35)$$

where m_1 through m_{10} will be allowed to vary with electric field. The m_6 parameter is set to 0 in order to break degeneracy. The m_9 and m_{10} are oddly defined in this equation because they were a later addition after fits to a double symmetric sigmoid failed to produce good enough results. The remaining nonzero parameters will be fit to the preliminary measurements of QY versus $\langle E_{true} \rangle$ in each of the electric field bins, giving us a set of 13 measurements for each parameter.

We first fit to the measurements from the “gfdcm” data and found that the m_8 parameter (among others) was roughly constant over all the field bins. We repeated the fit holding m_8 equal to the error-weighted average of 4.00. After obtaining a new set of best-fit parameters, we repeated the fit again this time also holding m_9 to its average value of 0.288. We repeated this process for $m_2 = 76.9$, $m_5 = 37.5$, and $m_3 = 0.837$, but after this point all of the remaining parameters had clear trends in electric field. Each remaining parameter’s trend in electric field was fit to a single symmetric sigmoid, as shown in equation 5.34.

Figure 5.21 the best-fit function for the 180 V/cm field bin. The brown and orange

points show the “gfdcm” QY data for post-Run04 tritium and carbon-14, respectively. The other data shown is used most to constrain the high and low energy regions of the fit. The lavender stars, teal “X’s”, and green markers are all from LUX Run03 [8, 10, 11]. The Run03 and post-Run04 measurements are all in good agreement. The blue square markers are from measurements of Compton scattering in neriX detector[43]. We do not include these points in the preliminary fits, but we will incorporate them when developing a final model of the yields. The full set of measurements will be discussed in detail in section ??.

We also repeated these fits for the “dcm” data. We set $m_8 = 4.29$, $m_9 = 0.334$, $m_2 = 77.3$, and $m_5 = 42.8$. The m_3 parameter was noisy throughout the bins, but had a general trend upward in electric field. Instead of holding it constant, we fit it to an exponential. We then proceeded to fit m_1 , m_7 , m_4 , and m_{10} to sigmoids as we did for the “gfdcm” data. The results of these fits are shown in figures 5.24, 5.25, 5.26, and 5.27. We will use these fits when modeling both the “dcm” and “z” style corrections.

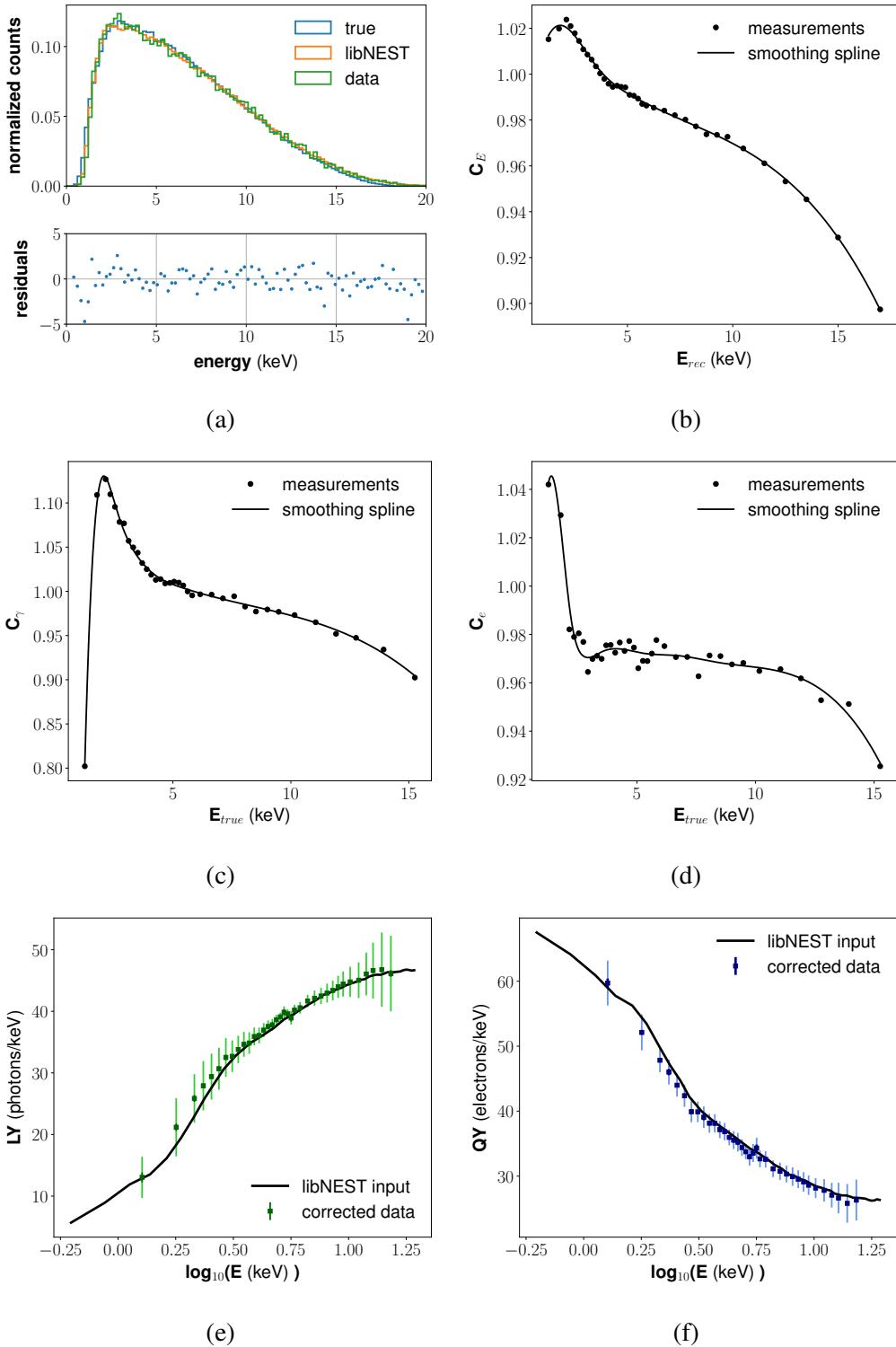


Figure 5.16: Calculations for preliminary tritium yields in the 180 V/cm drift bin, using the “gfdcm” data corrections. These plots are analogous to those previously shown for carbon-14.

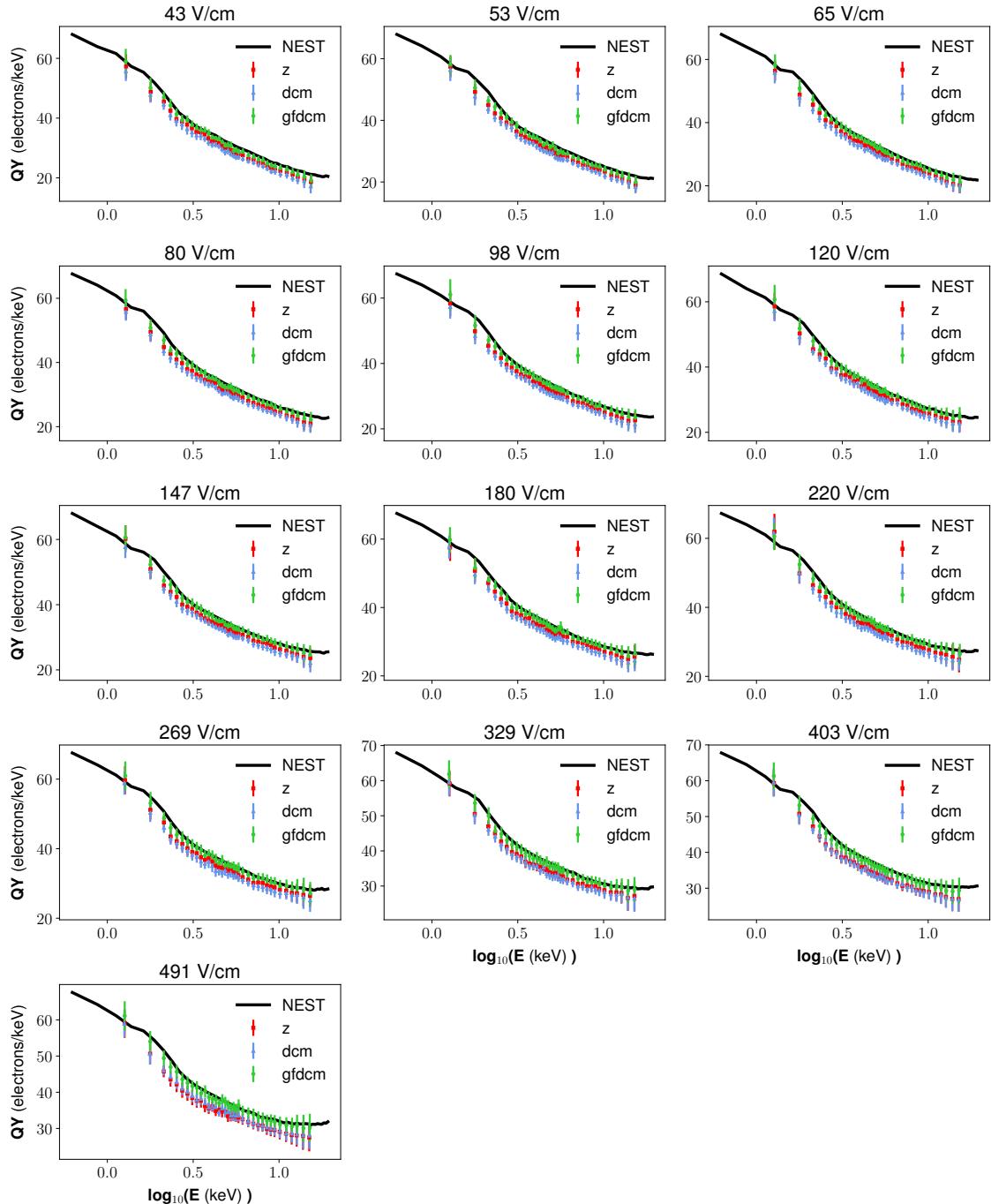


Figure 5.17: Preliminary tritium charge yield for the three efficiency corrections being studied, in each of the 13 electric field bins defined in 4.1.3. The x-axis here represents the true event energy, obtained by applying the smearing corrections. The charge yields measured here will be used to fine-tune the NEST model in order to obtain a more accurate set of corrections.

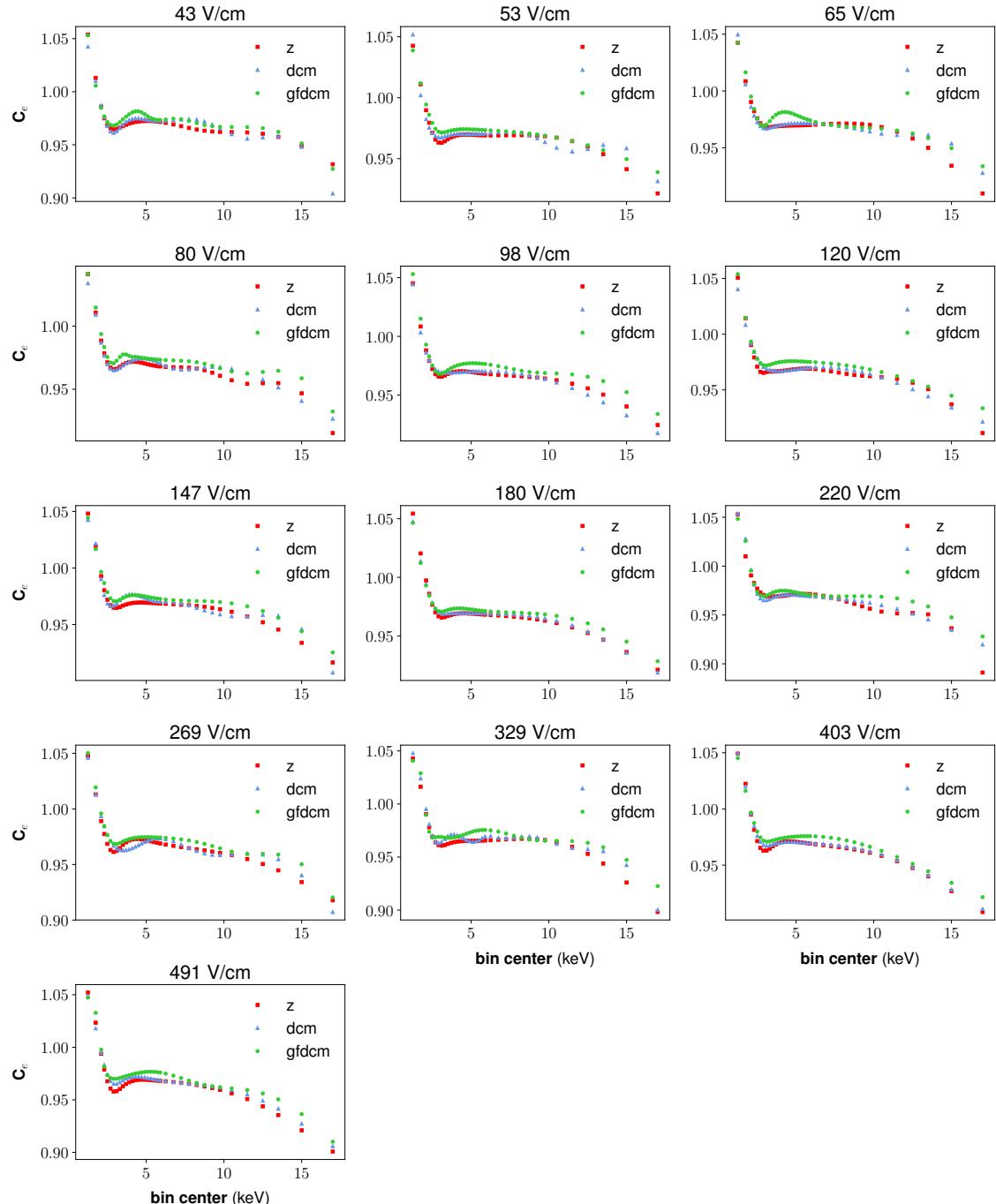


Figure 5.18: Tritium energy smearing correction factors for the three efficiency corrections being studied, in each of the electric field bins. The x-axis shows the central value the reconstructed energy bin for which the correction factor is calculated.

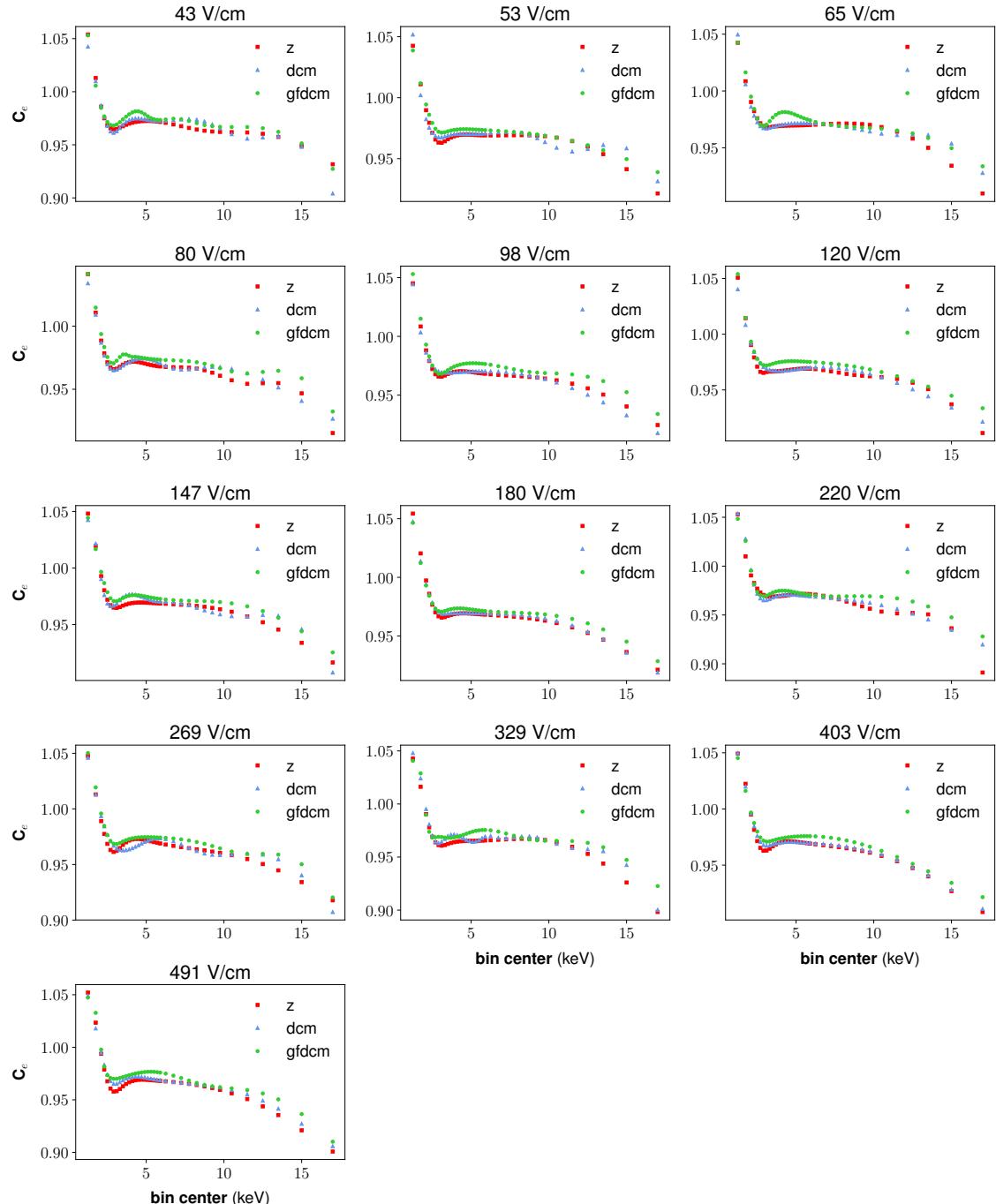


Figure 5.19: Tritium energy smearing correction factors for the three efficiency corrections being studied, in each of the electric field bins. The x-axis shows the central value the reconstructed energy bin for which the correction factor is calculated.

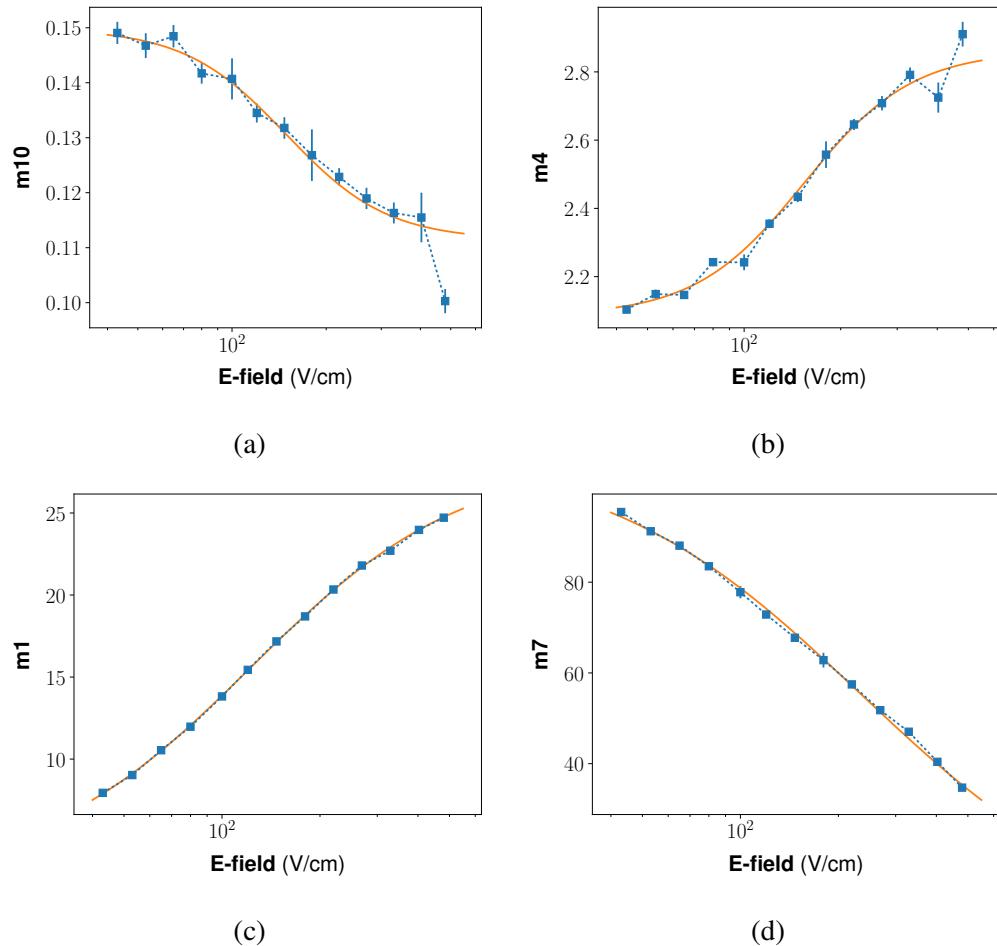


Figure 5.20: Sigmoid fits to the QY parameters which could not be held constant. The blue markers show the measured parameters for the “gfdcm” data. The orange lines show fits to the parameters as functions of electric field.

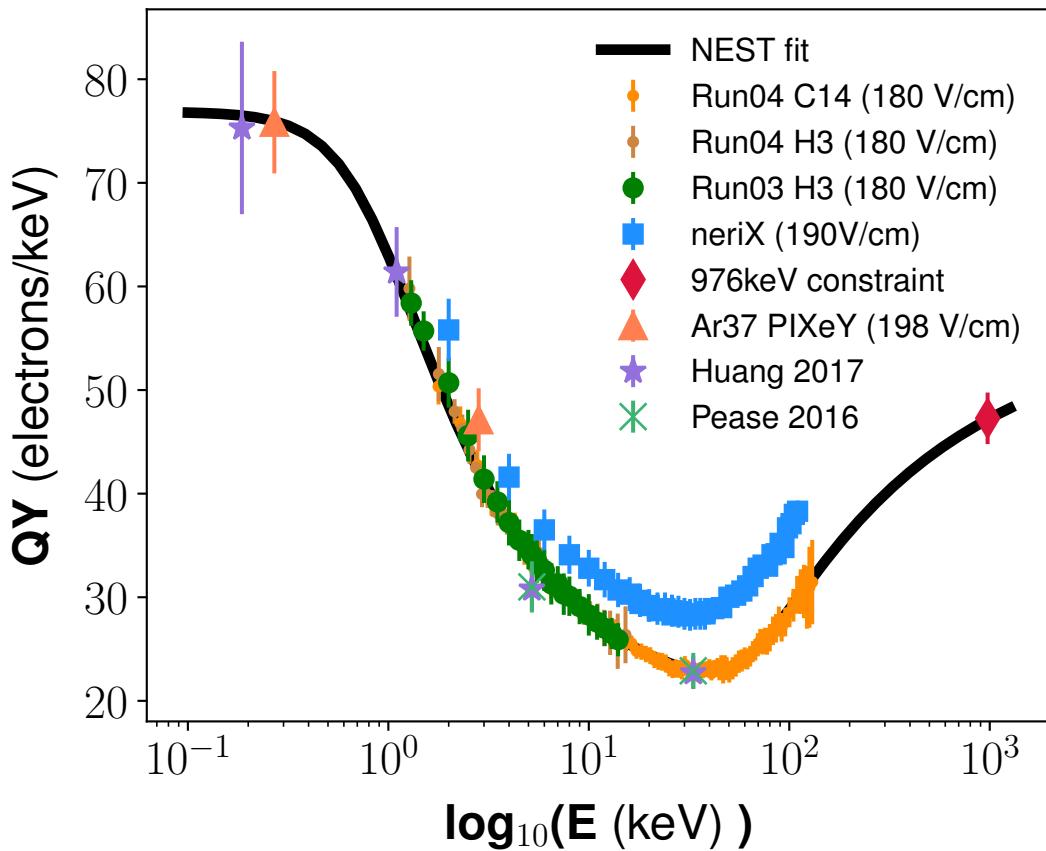


Figure 5.21: Best fit QY for “gfdcm” data in the 180 V/cm electric field bin. The orange points are the post-Run04 carbon-14 measurements, and the brown points are the post-Run04 tritium measurements. The datasets labeled “Run03 H3”, “Huang 2017”, and “Pease 2017” are all from LUX Run03 measurements. The blue squares are not included in the fit. The other datasets are described in section 5.6.

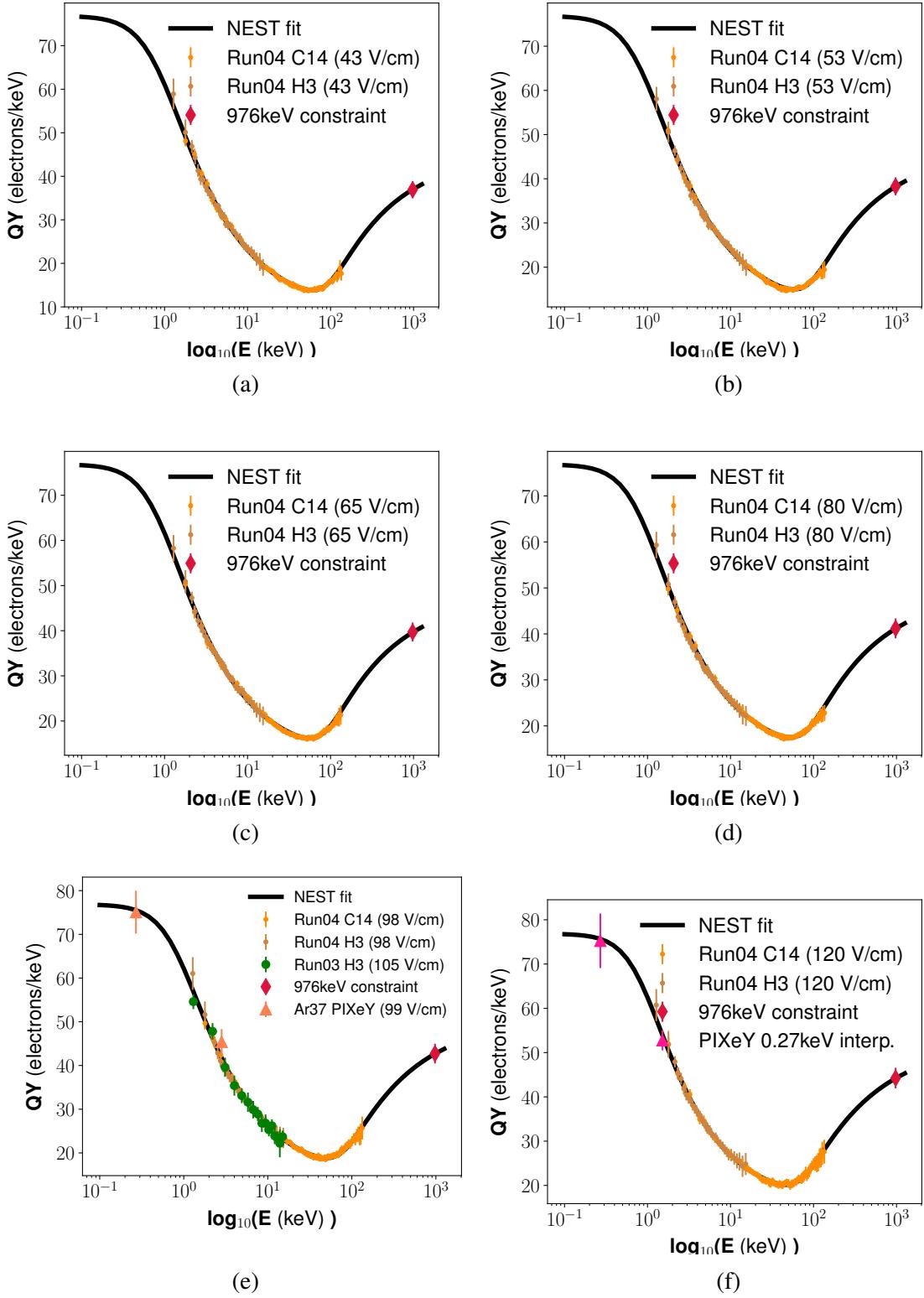


Figure 5.22: Best fit QY for “gfdcm” data in the 43, 53, 65, 80, 98, and 120 V/cm electric field bins. The orange points are the post-Run04 carbon-14 measurements, and the brown points are the post-Run04 tritium measurements. The other datasets are described in section 5.6.

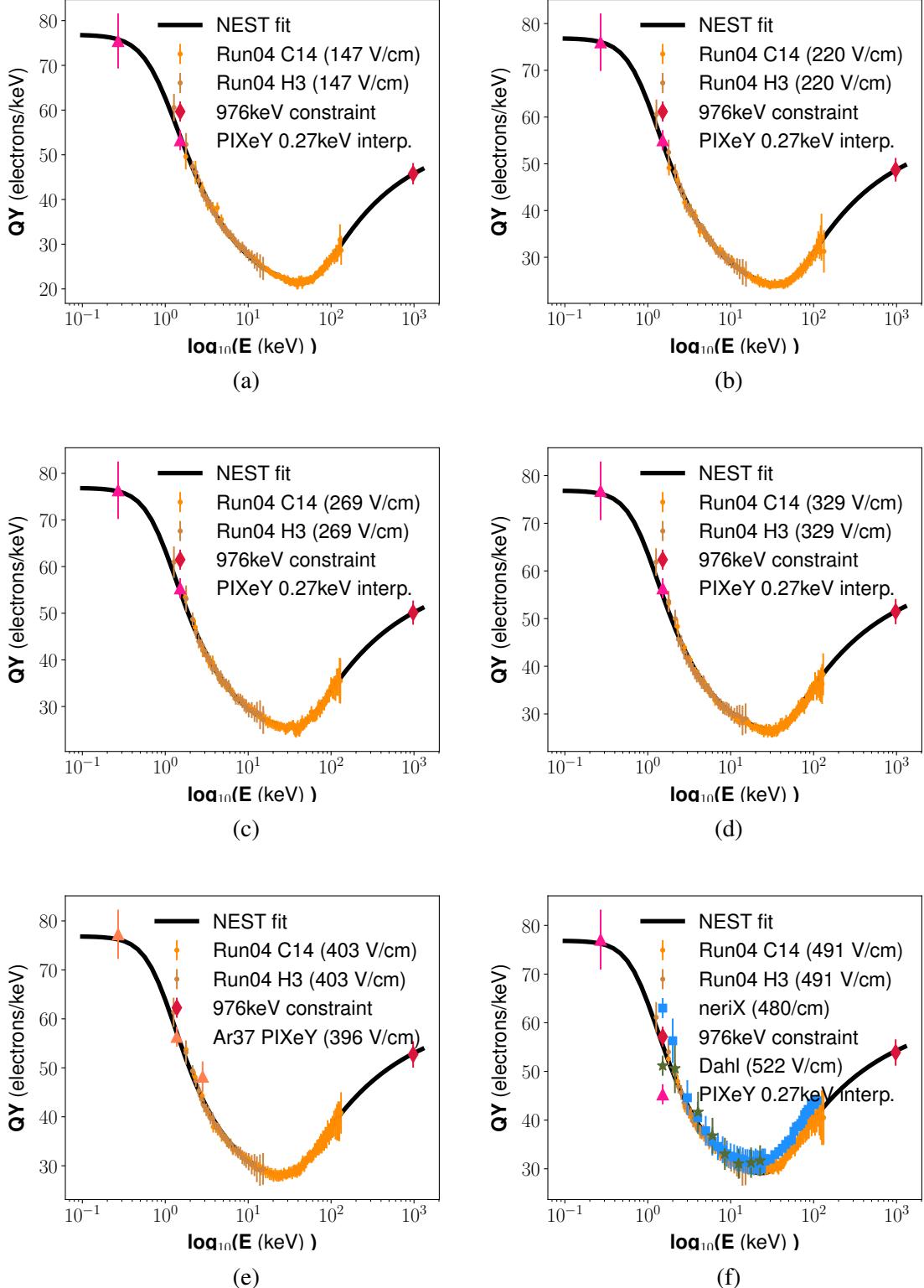


Figure 5.23: Best fit QY for “gfdcm” data in the 147, 220, 269, 329, 403, and 491 V/cm electric field bins. The orange points are the post-Run04 carbon-14 measurements, and the brown points are the post-Run04 tritium measurements. The other datasets are described in section 5.6.

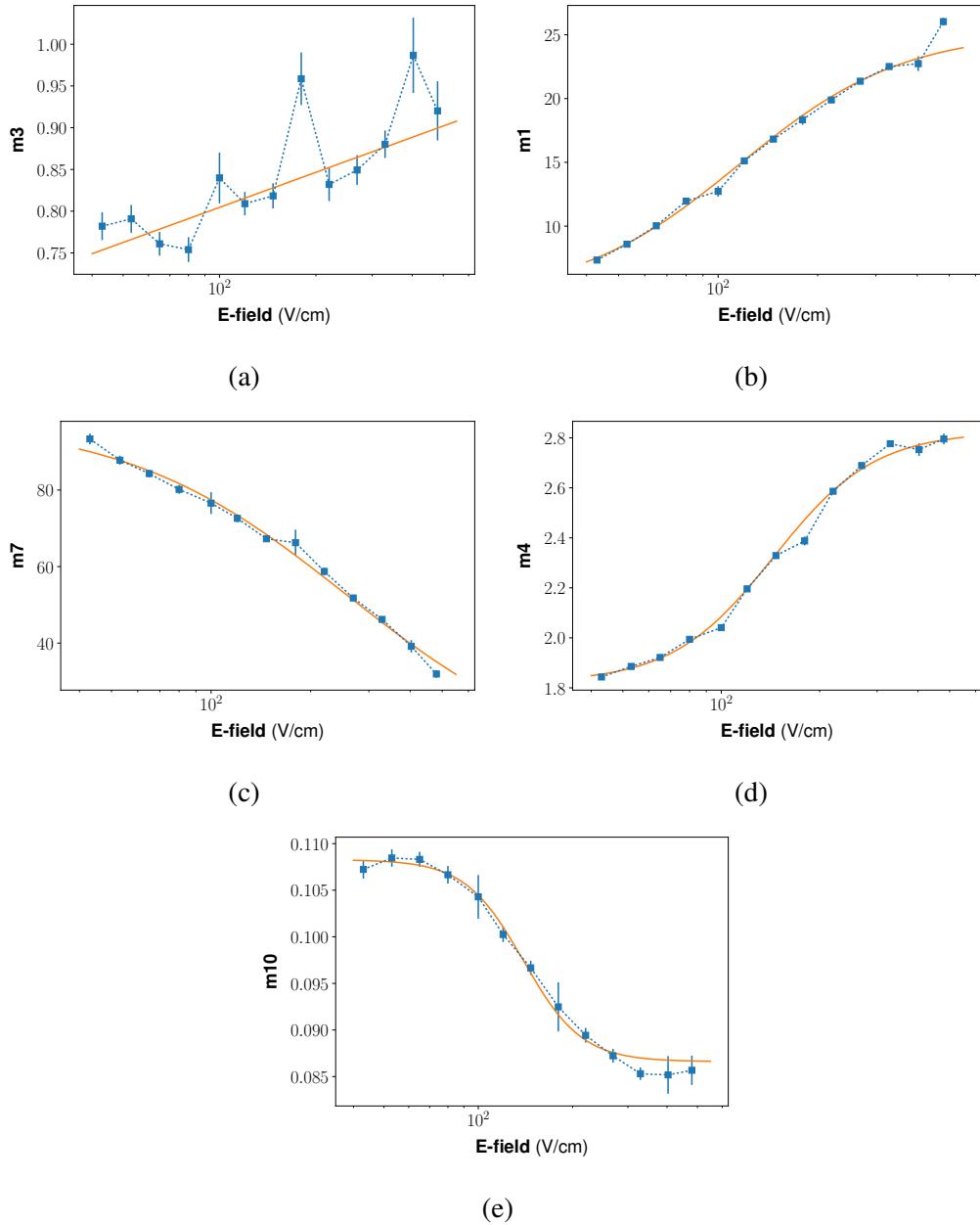


Figure 5.24: Best fit QY parameters as a function of electric field for the “dcm” style results. The parameters not shown in this figure are held constant in field at their error-weighted averages. The orange lines show sigmoid fits to the parameters as functions of electric field.

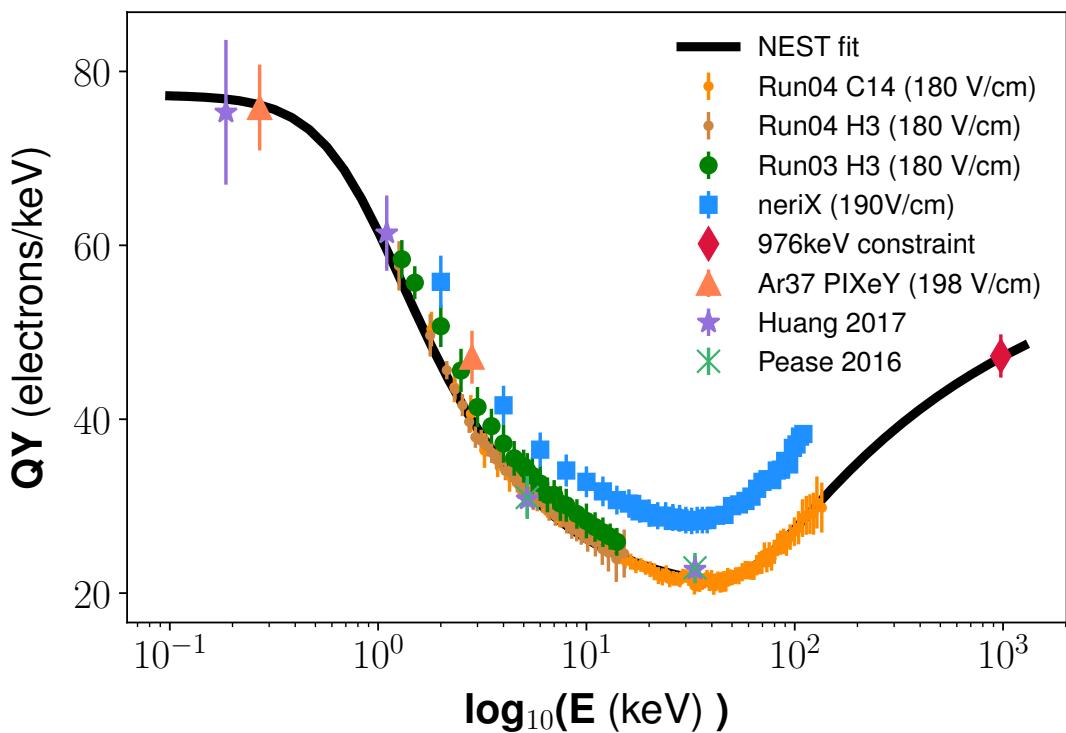


Figure 5.25: Best fit QY for “dcm” data in the 180 V/cm electric field bin. The orange points are the post-Run04 carbon-14 measurements, and the brown points are the post-Run04 tritium measurements. The datasets labeled “Run03 H3”, “Huang 2017”, and “Pease 2017” are all from LUX Run03 measurements. The blue squares are not included in the fit. The other datasets are described in section 5.6.

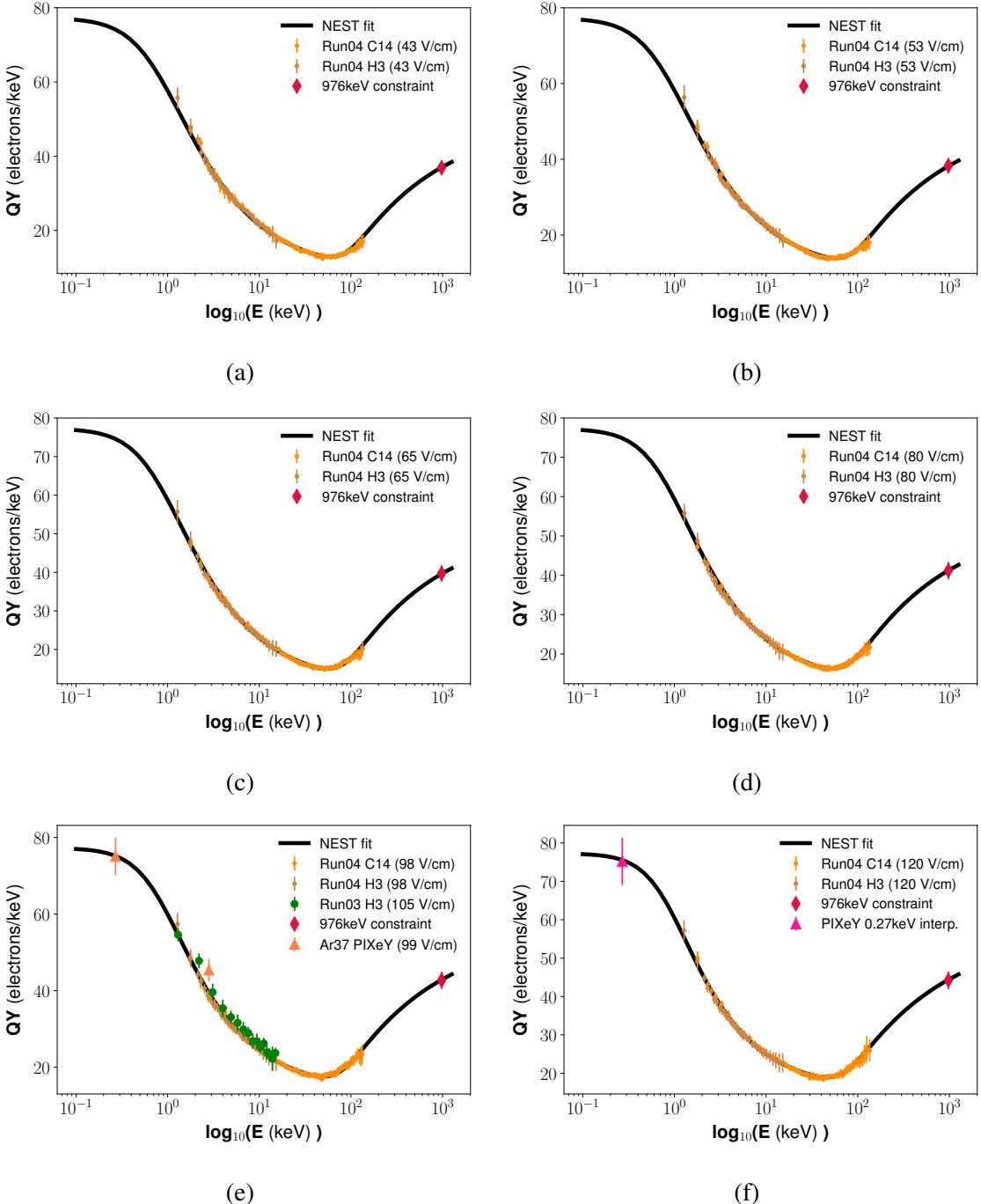


Figure 5.26: Best fit QY for “gfdcm” data in the 43, 53, 65, 80, 98, and 120 V/cm electric field bins. The orange points are the post-Run04 carbon-14 measurements, and the brown points are the post-Run04 tritium measurements. The other datasets are described in section 5.6.

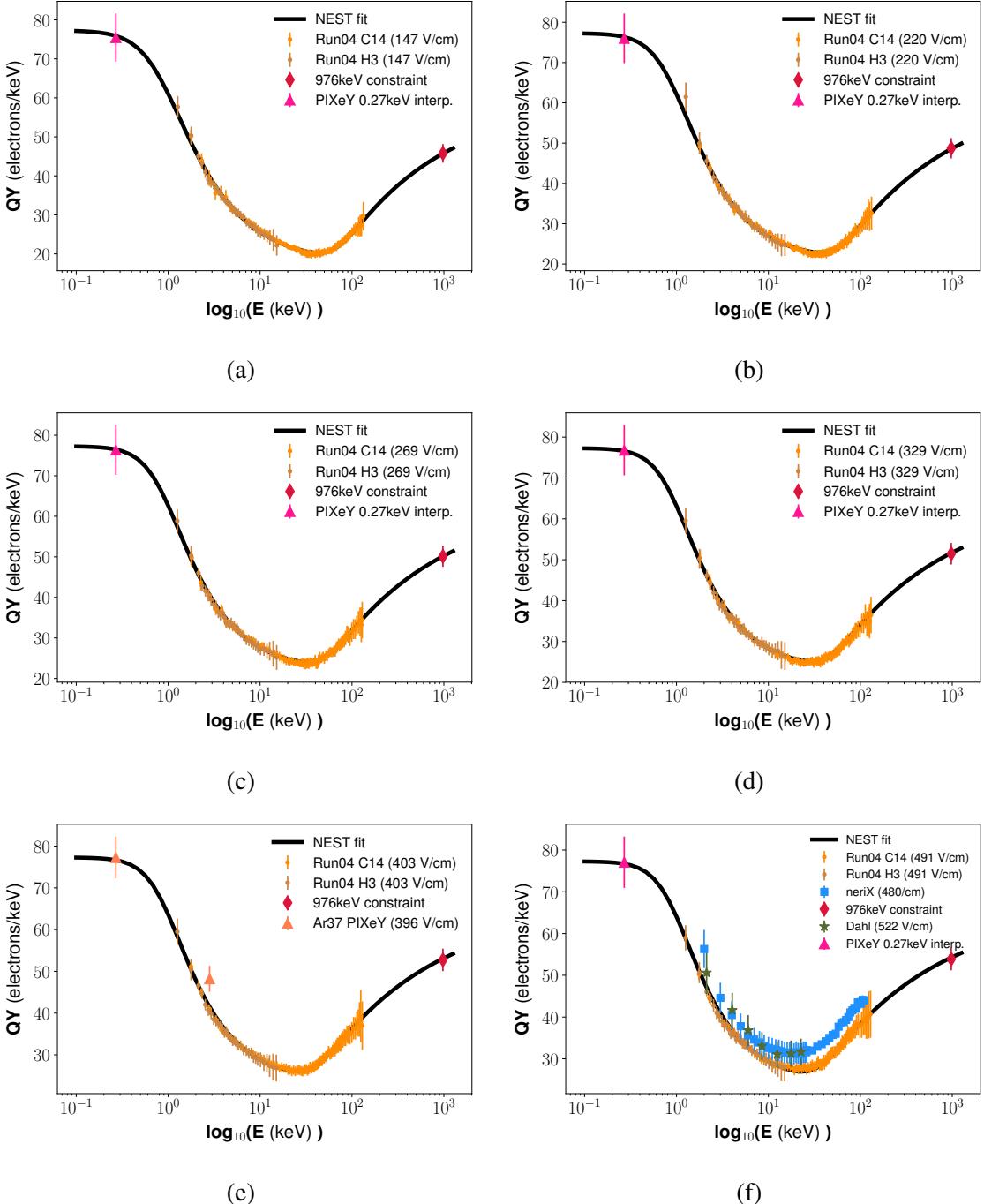


Figure 5.27: Best fit QY for “dcm” data in the 147, 220, 269, 329, 403, and 491 V/cm electric field bins. The orange points are the post-Run04 carbon-14 measurements, and the brown points are the post-Run04 tritium measurements. The other datasets are described in section 5.6.

5.4 Measurement of Recombination Fluctuations from ^{14}C

For an event with energy, E , and electric field, \mathcal{E} , is given by a certain number of electrons, N_R , will recombine with an ion. These electrons will be subtracted from the initial number of ions, N_i , and added to the number of excitons, resulting in the net number of electrons and photons produced by the event:

$$\begin{aligned} N_e &= N_i - N_R \\ N_\gamma &= \alpha N_e + N_R \end{aligned} \tag{5.36}$$

where the constant term α is the exciton to ion ratio. The expected value of N_R will be given by:

$$\langle N_R \rangle = N_i \cdot P(E, \mathcal{E}), \tag{5.37}$$

where $P(E, \mathcal{E})$ is the probability that an ionization electron will recombine. The expected charge yield for this event can then be written:

$$QY(E, \mathcal{E}) = \frac{1}{W} \cdot \frac{1}{1 + \alpha} \cdot \left(1 - P_R(E, \mathcal{E}) \right), \tag{5.38}$$

where we have taken:

$$\binom{N_i}{E} = \left(N_i \frac{1}{1 + \alpha} \right) \left(N_i \cdot W \right) = \frac{1}{W} \cdot \frac{1}{1 + \alpha} \tag{5.39}$$

Fluctuations in the recombination process, σ_R , will add to the fluctuations in detector resolution to give the total variance expected in the observed number of photons ($n_\gamma \equiv$

$S1c/G1$) and electrons ($n_e \equiv S2c/G2$):

$$\begin{aligned}\sigma_\gamma^2 &= \sigma_R^2 + \sigma_{\gamma,det}^2 \\ \sigma_e^2 &= \sigma_R^2 + \sigma_{e,det}^2\end{aligned}\tag{5.40}$$

In the simplest model, where every ionization electron from an event has the same probability of recombining, the recombination fluctuations would be expected to follow a binomial trend:

$$\sigma_{binom}^2 = nP(1 - P)\tag{5.41}$$

It has been observed, however, that σ_R grows much more quickly than the $\sqrt{N_i}$ dependence expected for a binomial process. In fact, LUX Run03 data shows that the recombination fluctuations have an approximately linear dependence on the number of ions[8]:

$$\sigma_R = (0.073) \cdot N_i\tag{5.42}$$

5.4.1 Separating σ_R from σ_{det} in a Continuous Spectrum

It is straightforward to calculate the recombination fluctuations from a mono-energetic line source without any prior knowledge of the detector resolution. In addition to equation 5.40 have also have:

$$\sigma_E^2 = W^2 \left(\sigma_{\gamma,det}^2 + \sigma_{e,det}^2 \right),\tag{5.43}$$

because the recombination process is orthogonal to energy. The recombination fluctuations can then be written in terms of the measurable quantities σ_{S1} , σ_{S2} , and σ_E :

$$\sigma_{R,line} = \frac{1}{2} \left(\sigma_\gamma + \sigma_{S2} - \frac{\sigma_E}{W} \right)\tag{5.44}$$

However, just as in the case of charge and light yields measurements, the measurement of σ_R by dividing a continuous spectrum into energy bins is significantly more complex than using all of the events from a mono-energetic source.

In a continuous spectrum such as tritium and carbon-14, we do not have immediate access to any of the measurables that go into the calculation of 5.44. The energy resolution is convolved with the spectral shape making a direct measurement nearly impossible. As we found in section 5.2, $\sigma_{\gamma,det}$, $\sigma_{e,det}$, and σ_R all smear the measured band of (n_e, n_γ) in nontrivial ways, making it difficult to reconstruct how a measurement in a reconstructed energy bin corresponds to the underlying physical process. We again turn to the method laid out in [30] for guidance, although the addition of the pathological S2 tails may again make this method largely ineffective for the post-Run04 data.

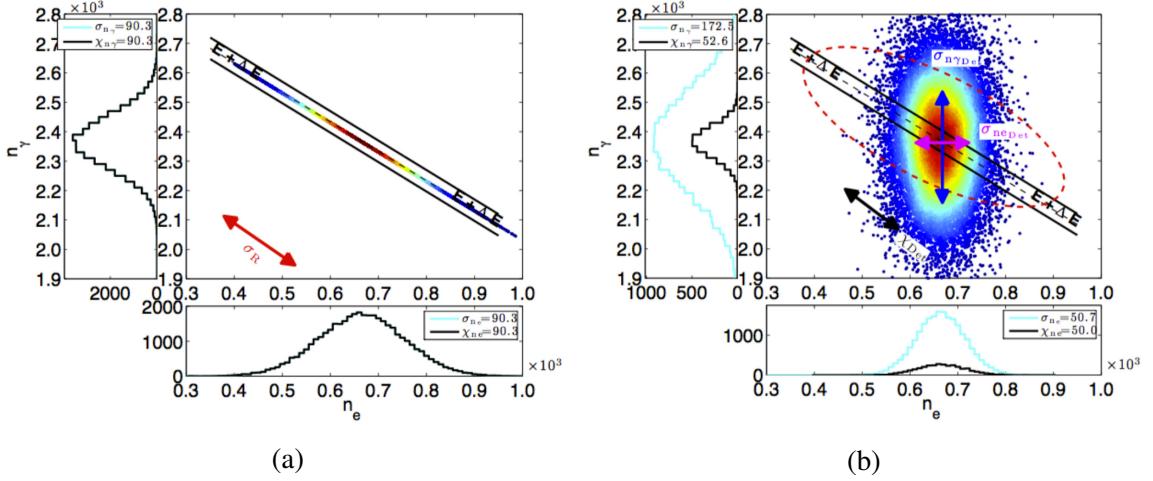


Figure 5.28: The left plot (a) shows the binning of a toy spectrum with recombination fluctuations, but no detector fluctuations. All of the events fall within the reconstructed energy bin, so the variance of events within the bin is equal to the total variance of the population. The right plot (b) shows the binning of a toy spectrum with no recombination fluctuations, but with detector fluctuations. In this case, the total photon width, $\sigma_\gamma = 172.5$ is much greater than the deviation within the energy bin, $\chi_\gamma = 52.6$. Meanwhile the total deviation in the electron spectrum $\sigma_e = 50.7$ is about equal to the deviation within the bin, $\chi_e = 50.0$. The discrepancy in χ_γ and χ_e is due to the finite width of the energy bin. Figures taken from [30].

We examine the behavior of the S1 and S2 spectra within an energy slice. We will

define the total variance of the S1 and S2 populations within this slice to be:

$$\chi_{tot}^2 \equiv \frac{\sigma_{S1,slice}^2}{G1^2} = \frac{\sigma_{S2,slice}^2}{G2^2} \quad (5.45)$$

The events in the bin will all have about the same reconstructed energy, so an event with $n_e = \langle n_e \rangle + N_R$ will have a corresponding $n_\gamma \approx \langle n_\gamma \rangle - N_R$. Therefore, the variance of the n_γ spectrum will be equal to that of the n_e spectrum within the bin.

The recombination fluctuations do not affect an event's reconstructed energy, so in a detector with infinite detector resolution, the variance of events within an energy bin will be equal to the recombination variance of events at that energy:

$$\chi_R = \sigma_R \quad (5.46)$$

In the case of a detector with finite detector resolution but no recombination fluctuations, the relation between χ_{det} , $\sigma_{e,det}$, and $\sigma_{\gamma,det}$ is significantly more complicated.

For example, consider figure 5.28 which shows a spectrum from a simulated krypton-83m source. The left plot has $\sigma_R = 90.3$ and $\sigma_{e,det} = \sigma_{\gamma,det} = 0$. In this case, all of the events fall within the reconstructed energy bin, so the variance of events within the bin is equal to the total variance of the population. In the right plot we have $\sigma_R = 0$, $\sigma_{e,det} = 50.7$, and $\sigma_{\gamma,det} = 172.5$. The width of the full photon population, $\sigma_\gamma = 172.5$ is much greater than the deviation within the energy bin, $\chi_\gamma = 52.6$. Meanwhile the total deviation in the electron spectrum $\sigma_e = 50.7$ is about equal to the deviation within the bin, $\chi_e = 50.0$. Conceptually, we see this is because the deviation of events within the energy slice is limited by the deviation in the number of electrons. An event with a larger upward fluctuation in n_γ must have an equally large fluctuation downward in n_e in order to pass the energy cut, but here we have $\sigma_{\gamma,det} \approx 3 \cdot \sigma_{e,det}$ so a 1-sigma fluctuation in n_γ requires a 3-sigma fluctuation in

n_e in order to be selected by the energy bin. Meanwhile, a 1-sigma fluctuation in n_e would require a 0.3-sigma fluctuation in n_γ to be selected, so $\chi_{e,det}$ is only slightly narrower than $\sigma_{e,det}$. We also note a small discrepancy in χ_γ and χ_e ; this is due to the finite width of the energy bin[30].

To obtain a better quantitative understanding of χ_{det} , Dobi analyzed small fluctuations along lines of constant energy using $E/W \equiv n_q = n_e + n_\gamma$; first holding n_γ and allowing for fluctuations in n_e , and then holding n_e constant, allowing for fluctuations in n_γ [30]:

$$\begin{aligned}\delta n_{q,\perp} &= \frac{\partial n_\gamma}{\partial n_q} \delta n_q \Big|_{n_\gamma} + \frac{\partial n_e}{\partial n_q} \delta n_q \Big|_{n_e} \\ &= \frac{\partial n_\gamma}{\partial n_q} \delta n_e + \frac{\partial n_e}{\partial n_q} \delta n_\gamma\end{aligned}\quad (5.47)$$

We square equation 5.47, dropping the cross-terms because $\sigma_{e,det}$ and $\sigma_{\gamma,det}$ are uncorrelated. This gives the following expression for χ_{det} :

$$\chi_{det}^2 = \left(\frac{\partial n_\gamma}{\partial n_q} \right)^2 \sigma_{e,det}^2 + \left(\frac{\partial n_e}{\partial n_q} \right)^2 \sigma_{\gamma,det}^2 \quad (5.48)$$

In the case of a line source with, $\frac{\partial n_\gamma}{\partial n_q}$ would be the slope of the major axis of the error ellipse in (n_q, n_γ) space:

$$\frac{\partial n_\gamma}{\partial n_q} = \frac{\sigma_{\gamma,det}^2}{\sigma_{\gamma,det}^2 + \sigma_{e,det}^2} \quad (5.49)$$

Similarly, the slope for electrons would be:

$$\frac{\partial n_e}{\partial n_q} = 1 - \frac{\partial n_\gamma}{\partial n_q} = \frac{\sigma_{e,det}^2}{\sigma_{\gamma,det}^2 + \sigma_{e,det}^2} \quad (5.50)$$

In the case of a continuous spectrum, the slopes $M_\gamma = \frac{\partial n_\gamma}{\partial n_q}$ and $M_e = \frac{\partial n_e}{\partial n_q}$ could be approximated by $LY \cdot W$ and $QY \cdot W$, respectively.

Equation 5.48 can also be derived by rotating the error ellipse by the angle of the central

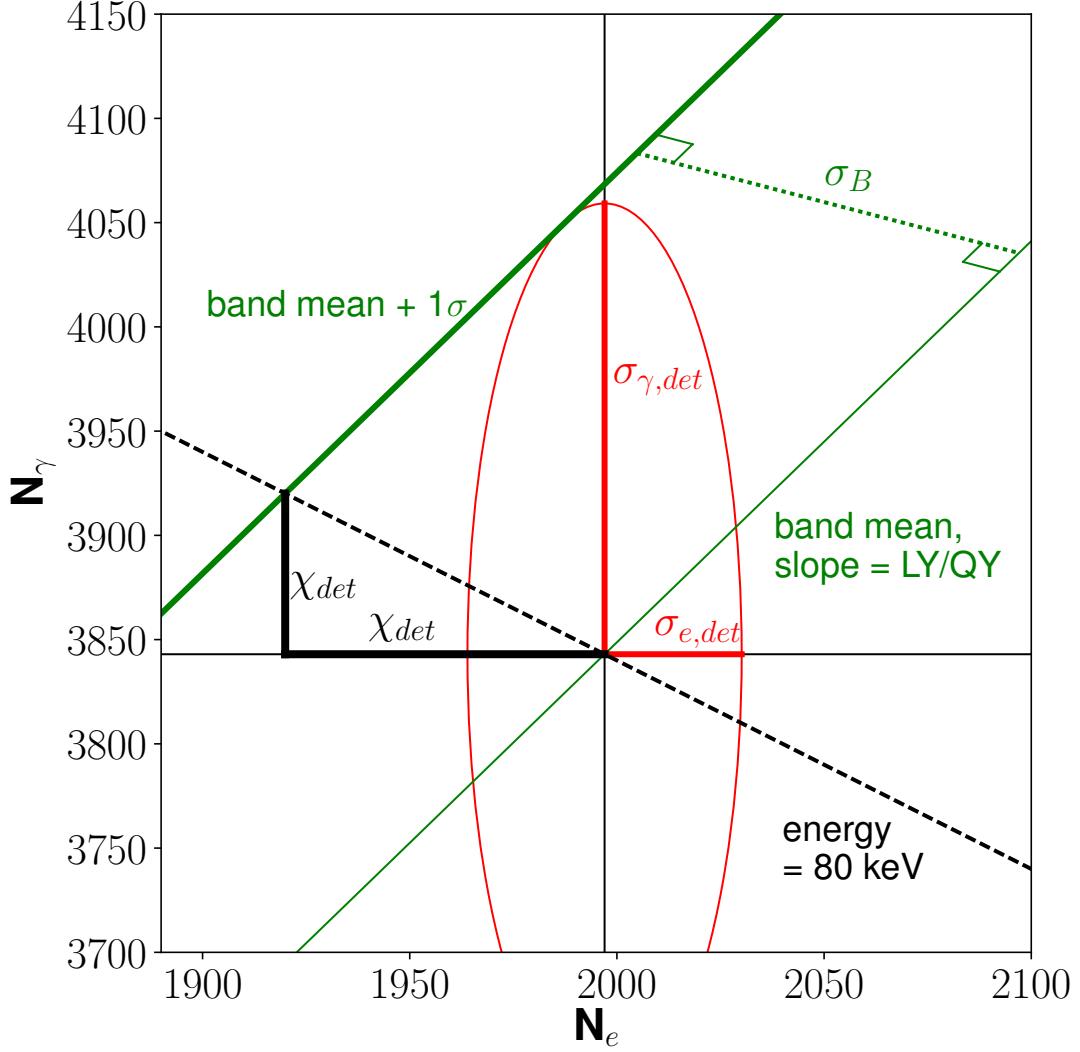


Figure 5.29: Calculation of χ_{det} using a rotated error ellipse. We used typical LUX parameters for an 80 keV decay. We set $QY = 25$ electrons per keV, $QY = 48$ photons per keV, $\sigma_{\gamma, det} = 216.2$ photons, and $\sigma_{e, det} = 33.1$ electrons. The light green line shows the trend-line of the (n_e, n_γ) band. The heavy green line shows the 1-sigma error band. The dashed black line is the 80 keV line of constant energy. The solid black lines indicate χ_{det} ; the size of the fluctuations of n_e and n_γ along the line of constant energy.

trend-line of the (n_e, n_γ) band, as shown in figure 5.29. For this figure, we used typical LUX parameters for an 80 keV decay. We set $QY = 25$ electrons per keV, $QY = 48$ photons per keV, $\sigma_{\gamma, det} = 216.2$ photons, and $\sigma_{e, det} = 33.1$ electrons. The orthogonal height of the error

ellipse rotated by $\theta = \arctan(M_\gamma/M_e)$, which is equivalent to the band width (σ_B), is given by:

$$\sigma_B = \sqrt{\left(\sigma_{e,det} \sin(\theta)\right)^2 + \left(\sigma_{\gamma,det} \cos(\theta)\right)^2} \quad (5.51)$$

We find χ_{det} by calculating the point at which the 80 keV constant energy line intersects the “band mean + 1 σ ” line and then project onto the x and y axes. This yields:

$$\begin{aligned} \chi_{det} &= \frac{\sigma_B}{\sin(\theta) + \cos(\theta)} \\ &= \frac{\sigma_B \cdot \sqrt{M_e^2 + M_\gamma^2}}{M_e + (1 - M_e)} \\ &= \sqrt{\sigma_{e,det}^2 M_\gamma^2 + \sigma_{\gamma,det}^2 M_e^2}, \end{aligned} \quad (5.52)$$

which reproduces the results from equation 5.48.

5.4.2 Recombination Fluctuations with S2 Tails

The procedure we have laid out for extracting recombination fluctuations from a continuous beta spectrum was used with success on the LUX Run03 tritium data[8]. However, we again must contend with the addition of the pathological S2 tails. To investigate how χ_{det} will be affected by the tails, we generate two toy carbon-14 spectra of (n_e, n_γ) ; one with tails and one without. We use the yields model measured in section 5.3.4 to determine the central values of n_e and n_γ for each event. We then apply recombination fluctuations based on the model in [8], $\sigma_R = 0.0734 \cdot N_i$. For the detector resolution, we take $\sigma_{e,det} = 0.74\sqrt{n_e}$ and $\sigma_{\gamma,det} = 3.5\sqrt{n_\gamma}$. For the pathological tails, we follow the model from section 4.4 where each S2 has a probability $R = 0.45$ of having tail area added to it, and the tail area is drawn from an exponential distribution with mean $\mu = S2 \cdot b = S2 \cdot 0.16$. The variance in the tail area will contain a contribution from the exponential distribution, as well as a contribution

from a binomial process with probability R . The variance of an exponential distribution is μ^2 , so we will model the variance in the tail area using:

$$\begin{aligned}\sigma_{tail}^2 &= R^2(S2 \cdot b)^2 + (S2 \cdot b)^2 \cdot R(1 - R) \\ &= R(S2 \cdot b)^2\end{aligned}\tag{5.53}$$

For each of the models, with tails and without tails, we generate an additional spectrum that does not include recombination fluctuations.

The results of these models are shown in figure 5.30. The left-hand plots show the model with no tails, while the right-hand plot shows the model with tails. In these plots, σ_R shows the expected recombination fluctuations for the average energy of events in each bin. χ_{det} shows the expected band width due to $\sigma_{\gamma,det}$ and $\sigma_{e,det}$; it is calculated using equation 5.48, with $\frac{\partial n_e}{\partial n_q} = QY/73$ and $\frac{\partial n_\gamma}{\partial n_q} = LY/73$. χ_{tail} is the expected added contribution due to the S2 tails. The two lines χ_{tot} and χ_{noR} are the measured band widths for the model with σ_R and without σ_R , respectively. Finally, we have defined $|\Delta\chi^2| = |\chi_{tot}^2 - (\chi_{noR}^2 + \sigma_R^2)|$ to test the assumptions that went into our method for extracting recombination fluctuations. This value will give us a hard limit as to how well we can measure recombination fluctuations using this method.

If our method is valid, the “ χ_{det}^2 ” and “ $\chi_{det}^2 + \chi_{tail}^2$ ” will lie on top of their respective “ χ_{noR}^2 ” lines and $|\Delta\chi^2|$ should be close to zero. We find that this is the case for the model with no S2 tails. The “ χ_{det}^2 ” line closely follows the measured “ χ_{noR} ” line across the entire energy range. Additionally, $|\Delta\chi^2|$ remains small at all energies; it is $< 10\%$ of χ_{tot} at all energies, and is $<$ about 1% of σ_R above keV 20.

As it was with the yields measurements, the Run03 method for extracting recombination fluctuations breaks down when S2 tails are added. Both of our tests for validity fail for our tailed model. The “ $\chi_{det}^2 + \chi_{tail}^2$ ” line is clearly not predicting the trend of the “ χ_{noR} ”

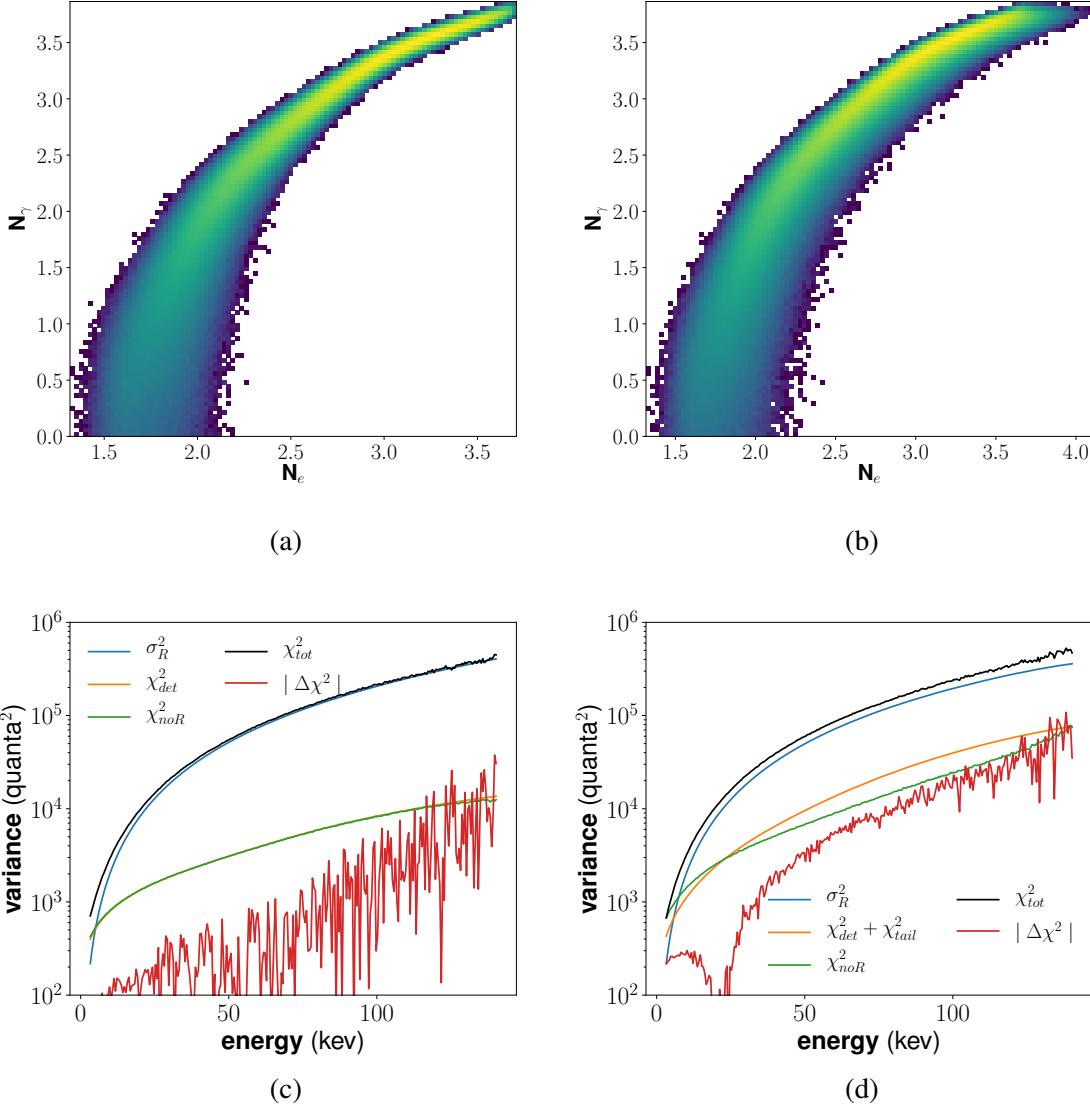


Figure 5.30: Models of recombination fluctuations. The left plots, (a) and (c), show a model which does not include S2 tails, while the model shown by (b) and (d) do include our S2 tail model. σ_R shows the expected recombination fluctuations for the average energy of events in each bin. χ_{det} shows the expected band width due to $\sigma_{\gamma,det}$ and $\sigma_{e,det}$; it is calculated using equation 5.48, with $\frac{\partial n_e}{\partial n_q} = QY/73$ and $\frac{\partial n_\gamma}{\partial n_q} = LY/73$. χ_{tail} is the expected added contribution due to the S2 tails. The two lines χ_{tot} and χ_{noR} are the measured band widths for the model with σ_R and without σ_R , respectively. Finally, we have defined $|\Delta\chi^2| = |\chi_{tot}^2 - (\chi_{noR}^2 + \sigma_R^2)|$.

line, and $|\Delta\chi^2|$ is on the order of 10% of σ_R across the entire energy range. The ability to account for detector resolution is even more important in the tailed model because the measured χ^2_{noR} has increased by about an order of magnitude over what it was for the untailed model. For these reasons, we will abandon this method of calculating recombination fluctuations and will again perform the measurement numerically.

5.4.3 Modelling ^{14}C Recombination Fluctuations in libNEST

The S2 tails interact with the recombination fluctuations and detector resolution in a non-trivial way, making our previous method of measuring recombination fluctuations from a beta spectrum invalid. We no longer have access to the value of σ_R in an individual energy bin. Instead we use results from prior experiments to motivate a functional form of $\sigma_R(E, \mathcal{E})$, inputting that model into the libNEST code, and optimizing its parameters.

As mentioned previously, it was found that the recombination fluctuations in the LUX Run03 tritium data is consistent with[8]:

$$\sigma_R = 0.0734 \cdot N_i \quad (5.54)$$

This model has been modified in several subsequent papers, but the underlying trend remains the same.

There is a set of measurements from the Xenon10 experiment which studied the fluctuations in a cobalt-57 deposit in liquid xenon at various electric fields. The results from this experiment, which are published in Eric Dahl's thesis [1], suggest that a pure linear trend in N_i is not sufficient to characterize all of the features of σ_R as a function of energy and electric-field. In the left panel of figure 5.31, we have displayed the results from this experiment, which were digitized from [1]. The blue markers indicate measurements of σ_R at various electric fields; ^{57}Co is a mono-energetic source, so N_i will be the same for each of

these measurements. The Run03 tritium model, displayed as the black line in figure 5.31, predicts that σ_R would be constant in field, but we see that the ^{57}Co measurements follow roughly quadratic shape when plotted as a function of $y \equiv n_e/n_q$ with a peak near $y = 0.5$. The prediction from Run03 tritium is in agreement with the peak value of σ_R as measured by ^{57}Co .

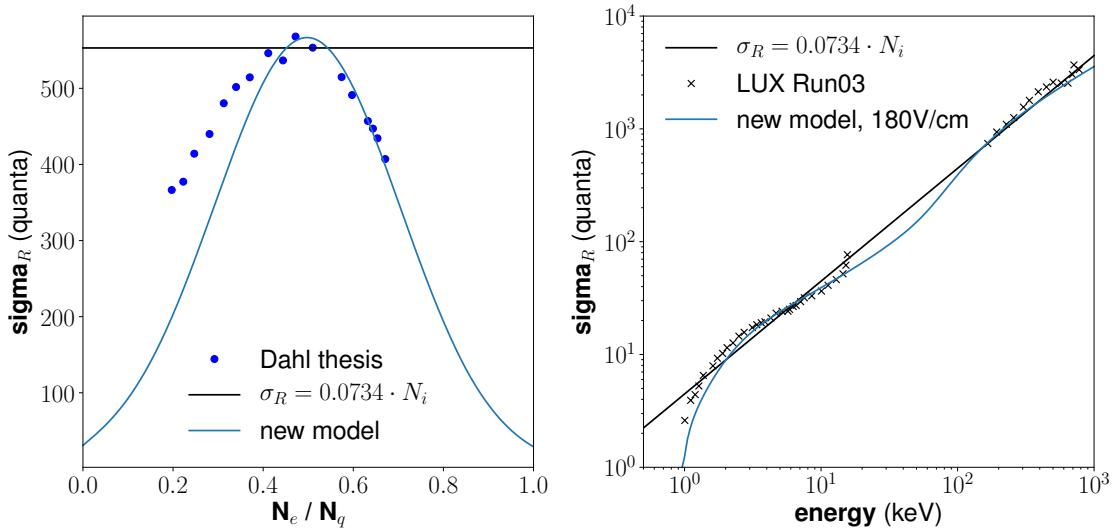


Figure 5.31: Comparison of the linear Run03 model of σ_R (black line) to the updated model (blue line). The points labeled “Dahl thesis” show measurements of ^{57}Co at varying fields, and are digitized from [1]. The black “x’s” show data from LUX Run03. The low energy points are from tritium, and the high energy points are primarily ^{137}Cs . These points were digitized from [8]. The new model does a significantly better job at reproducing the shape of both the cobalt-57 data and the LUX Run03 data.

With this in mind, we propose the following expression for σ_R :

$$\sigma_R(E, \mathcal{E})^2 = P_R(1 - P_R) \cdot N_i + F_R \left(\frac{n_e}{n_q} \right) N_i^2 \quad (5.55)$$

This is actually very similar to the Run03 tritium model, with the primary difference being that F_R here is a function of the electron-fraction, y , whereas in the Run03 model $F_R = 0.0734^2$ was a constant. We also force σ_R^2 to be no less than the variance of a binomial

process by explicitly adding the binomial term $P_R(1 - P_R) \cdot N_i$ to equation 5.55.

The question remains as to what the functional form of $F_R(\frac{n_e}{n_q})$ should be. We first tested a simple quadratic against the carbon-14 data, but found it fell too quickly toward low y and was not able model data from all of the electric field bins simultaneously. We instead switched to a Gaussian and found that this model did a fair job at capturing the band width of the carbon-14 data in all of the field bins. Equation 5.55 then becomes:

$$\sigma_R(E, \mathcal{E})^2 = P_R(1 - P_R) \cdot N_i + \left(F_0 \exp \left(\frac{-(n_e/n_q - F_1)^2}{2F_2^2} \right) \right)^2 N_i^2, \quad (5.56)$$

where F_0 , F_1 and F_2 will be constant fitting parameters.

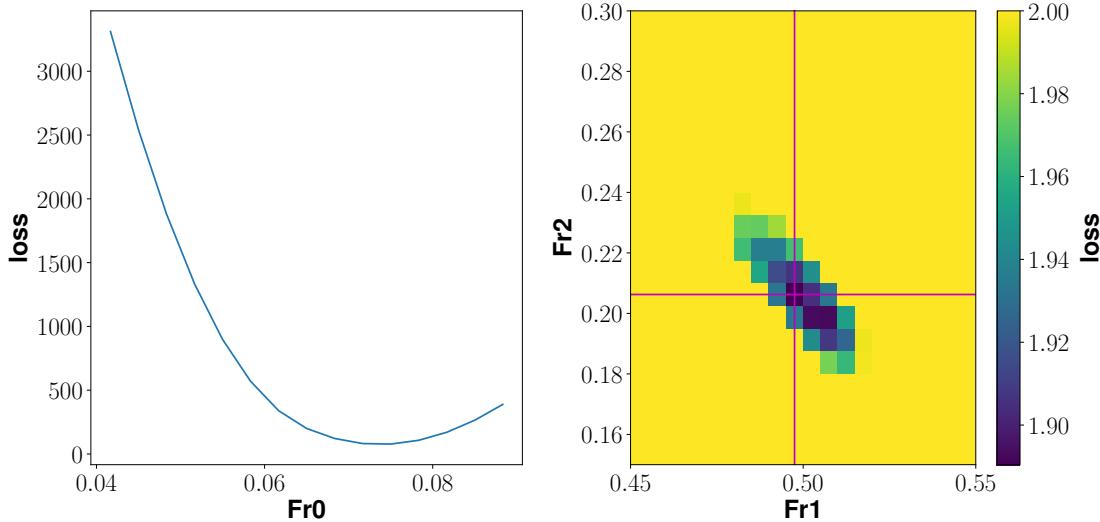


Figure 5.32: Fitting results for the updated model of the recombination fluctuations.

We find F_0 , F_1 , and F_2 by folding equation 5.56 into the libNEST code and generating a simulated carbon-14 spectrum. We then bin in energy and calculate the width of the S1 and S2 spectra in each bin. The width of the bands in a bin ($\chi_{S1(S2)}$) is calculated by fitting a Gaussian to its spectrum; we make a histogram of the binned data, apply a selection cut on the histogram centers, and then fit to selected histogram values. The selection

cut for S2 is -2 to 1 standard deviations from the mean, and for S1 is -1 to 2 standard deviations from the mean. In each energy bin, and for both data and simulation, we will then have a measurement of the width of the S1 and S2 bands along with values for the fitting uncertainty. We then take the average chi-squared difference between the data and simulation bands as the reduced chi-squared value for each band. We repeat this for all of the electric field bins, for both tritium and carbon-14 data. We sum the resulting set of reduced chi-squared values to give us a goodness-of-fit parameter (GoF_{Run04}) for a given set of (F_0, F_1, F_2) :

$$()_{S1} = \sum_{\mathcal{E}_i} \left\langle \frac{\left(S1 \text{ width})_{i,dat} - (S1 \text{ width})_{i,sim} \right)^2}{(S2 \text{ fitting error})_{i,dat}^2 + (S2 \text{ fitting error})_{i,dat}^2} \right\rangle \quad (5.57)$$

$$GoF_{Run04} = GoF_{S1,^{14}C} + GoF_{S2,^{14}C} + GoF_{S1,^{3}H} + GoF_{S2,^{3}H}$$

We also want to include results from the previous experiments in our fit, so we calculate a goodness of fit parameter (GoF_{Dahl}) for the data shown in figure 5.31. We define GoF_{Dahl} to be equal to the chi-squared error error between the ^{57}Co points and our test model. We find that our data is not in agreement with “Dahl Thesis” data at low values of y , so we only include points above $y = 0.4$ in our calculation of GoF_{Dahl} .

We then define a loss function:

$$loss = \log_{10}(GoF_{Run04} + w_{Dahl} \cdot GoF_{Dahl}) \quad (5.58)$$

The weight ($w - Dahl$) applied to GoF_{Dahl} was tuned until it is a heavy enough that the best fit model captures the high- y points in the cobalt-57 dataset but not so heavy that the Run04 data is overpowered in the low- y region. We selected a weight factor of 5, but the fitting result is insensitive to changes in w_{Dahl} of up to a factor of 2.

We will take the set of (F_0, F_1, F_2) which minimizes this loss function to be our best fit parameters. To find this minimum, we set up a 3-D grid in (F_0, F_1, F_2) and evaluate the loss function at the center of each box in the grid. We take the uncertainty on F_0 to be the width of a grid spacing, as is shown in figure 5.32. The uncertainties on F_1 and F_2 are taken to be 3 and 2 grid spacings, respectively, because the loss function is not as steep as it is for F_0 , so random fluctuations can beat the slope and the trend outward from the (F_1, F_2) optimum is not entirely monotonic. There is some subjectivity in our choice of w_{Dahl} . To characterize the uncertainty in our parameters added by this subjectivity, we vary w_{Dahl} up and down by a factor of 5 to see how the best fit values are affected. We find that when $w_{Dahl} = 1$ and when $w_{Dahl} = 25$, all of the best fit parameters deviate by exactly the previously stated error. We will therefore multiply these error by $\sqrt{2}$.

Using “gfdcm” data we find our best fit parameters are:

$$\begin{aligned} F_0 &= 0.075 \pm 0.005 \\ F_1 &= 0.4975 \pm 0.02 \\ F_2 &= 0.206 \pm 0.02 \end{aligned} \tag{5.59}$$

We find that the results for “z” and “dcm” data are identical. The best-fit model is shown in figures 5.33 and 5.34. We find that this model is much improved over the simple linear model, and that it does a decent job at characterizing the width of both the carbon-14 S1 and S2 bands in all of the field bins. The new libNEST model does tend to overestimate the width below about 30 keV, but it is not clear where the model is failing. It is possible, for instance, that our model of the S2 tails does not work in this region.

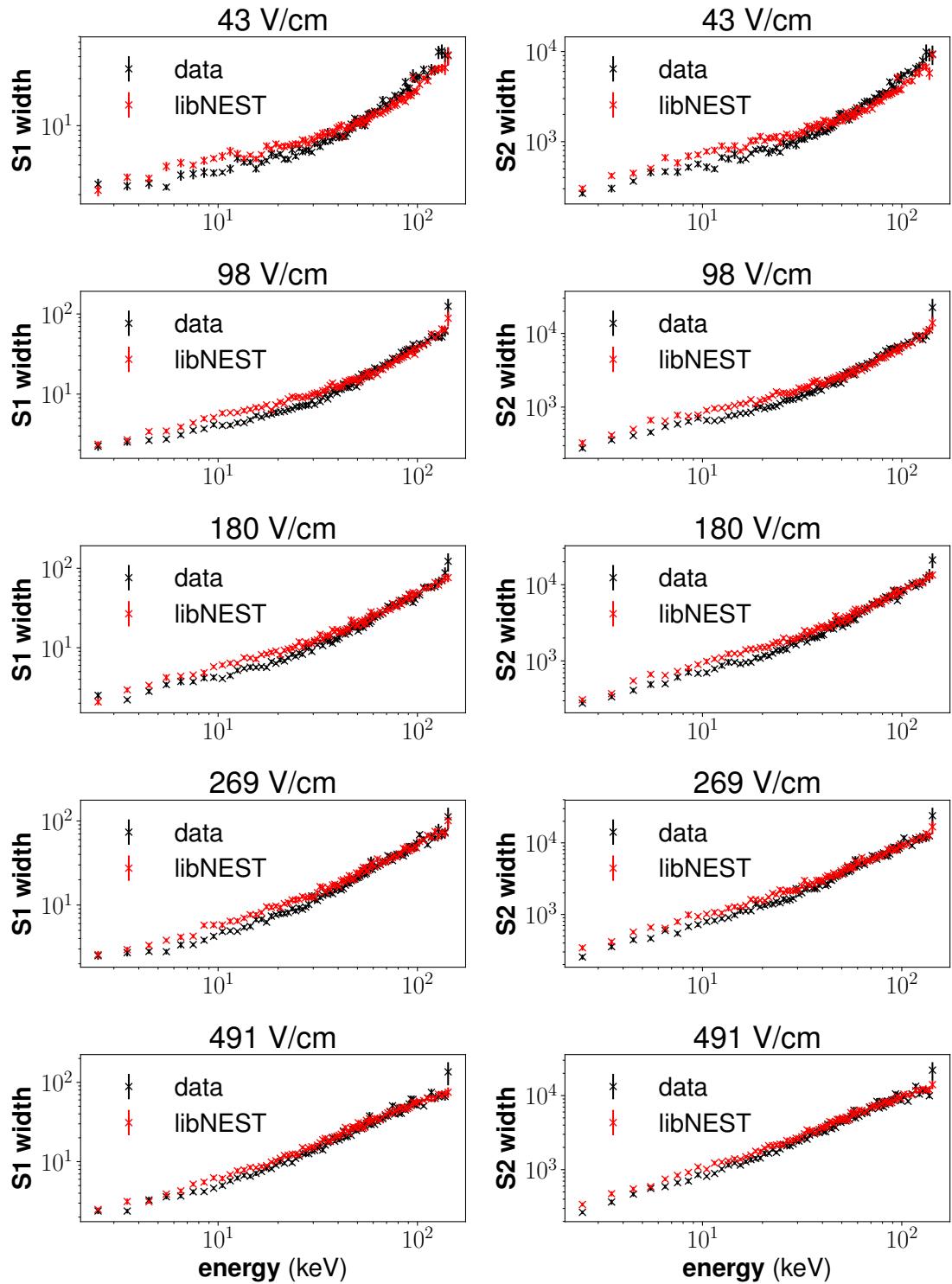


Figure 5.33: Comparison of the libNEST model of S1 and S2 widths, using the updated recombination model to the widths as measured in the “gfdcm” data.

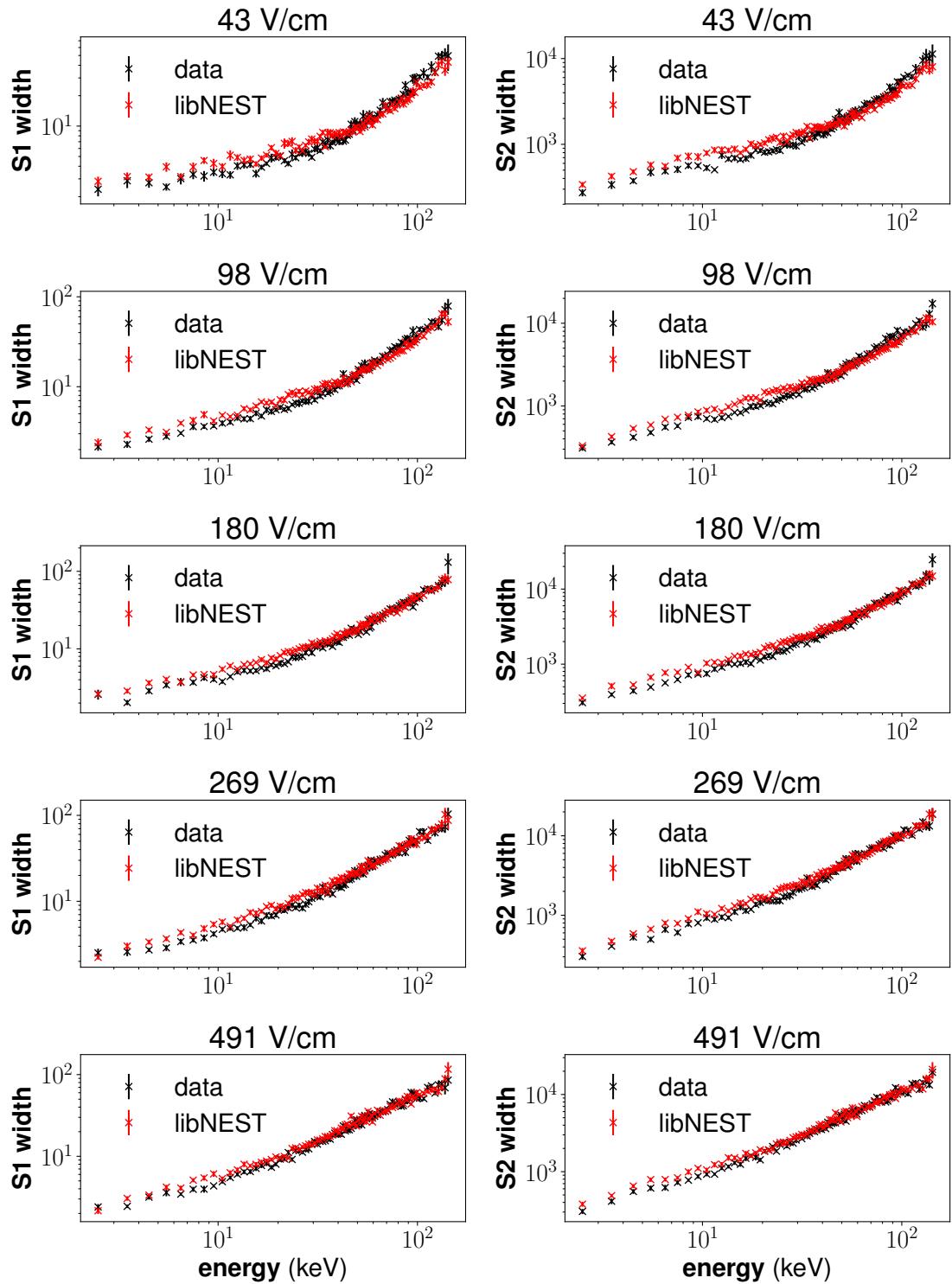


Figure 5.34: Comparison of the libNEST model of S1 and S2 widths, using the updated recombination model to the widths as measured in the “dcm” data.

5.5 Results from Post-Run04 ^{14}C and ^3H Calibrations

5.5.1 Yields and Recombination

We now have all of the ingredients we need to measure the charge and light yields using the post-Run4 carbon-14 and tritium data. The preliminary measurements of the charge yield obtained in section 5.3.4 are combined with the new model for recombination fluctuations derived in section 5.4.3, and both are input into the libNEST code. We then reapply the Metropolis fits for the S2 tail parameter fits from section 4.4 in order to account for any changes due to the updated parameters. The yields for gamma-type events are known to be different from beta-yields, so we use the existing set of yields when fitting the ^{131m}Xe peak. The results of these fits, which are shown in table 5.4, are consistent with those found previously.

Correction	b_{tail}	\pm	P_{tail}	\pm	$G2_{true}$	\pm
z	0.112	0.003	0.73	0.02	17.61	0.06
dcm	0.116	0.004	0.62	0.02	17.36	0.05
gfcdm	0.110	0.004	0.52	0.02	16.04	0.04

Table 5.4: Updated best fit results for the S2 tail model using the preliminary yields measurements and new σ_R model.

The addition of the newly fit tail parameters gives us a fully armed and operational model which we input into the libNEST infrastructure in order to recalculate the tritium and carbon-14 spectra. The newly simulated spectra are used to un-smear the E_{rec} , n_γ , and n_e using the method laid out in section 5.3.2. We thereby obtain final values for $\langle E_{true} \rangle_{ij}$, $\langle N_\gamma \rangle_{ij}$ and $\langle N_e \rangle_{ij}$. The “ i ” refers to the reconstructed energy bins described in section 5.3.2, and the “ j ” subscripts refer to the electric field bins laid out in section 4.1.3.

In order to calculate the light yield (LY), charge yield (QY), and recombination fraction

(r), we define a new parameter which will be equal to the ratio of photons to electrons:

$$\rho \equiv \frac{N_\gamma}{N_e} = \frac{LY}{QY} \quad (5.60)$$

Using $1/W = LY + QY$, the three parameters of interest can then be calculated:

$$LY = \frac{1}{W} \frac{1}{1 + \rho}$$

$$QY = \frac{1}{W} \frac{\rho}{1 + \rho} \quad (5.61)$$

$$r = \frac{\rho - \alpha}{1 + \rho}$$

The energy bins we used for carbon-14 are identical to those described in table ???. However, we found that the lowest energy binning was not fine enough for the tritium data. The systematic error due to binning was by far the dominant error in these bins. For the final measurements, we updated our binning as described in table 5.5.

Energy Range (keV)	1-6	6-10	10-14	14-18
Bin Width (keV)	0.2	0.5	1	2

Table 5.5: Tritium reconstructed energy bin widths and their associated energy ranges for the final measurements of $\langle \rho \rangle$.

For our set of electric field and energy bins, we use our measured $\langle N_\gamma \rangle_{ij}$ and $\langle N_\gamma \rangle_{ij}$ to calculate $\langle \rho \rangle_{ij}$. The measured values of $\langle E_{true} \rangle$ and $\langle \rho \rangle$ values are reported in appendix A. The systematic errors shown for $\langle \rho \rangle$ include the de-smearing error as well as the uncertainty in G1 and G2. The best-fit values for G1 and G2 have non-negligible correlation, so the cross-term is included in the error propagation. We also include a 4.3% systematic uncertainty on $\langle N_\gamma \rangle$, which comes from the rms offset from the Doke plot line shown in figure 4.17 and quantifies any remaining position dependence in G1 and G2 that our efficiency

corrections failed to remove. The uncertainties due to smearing and efficiency corrections are comparable in most of the energy bins and are the dominant systematic error. Near the endpoints of the spectra, the smearing error becomes dominant.

The uncertainties shown for $\langle E_{true} \rangle$ include the smearing error as well as the error due to finite bin width. We take the uncertainty due to a bin width of ΔE from the variance of a uniform distribution:

$$\sigma_{E,bin}^2 = \frac{\Delta E^2}{12} \quad (5.62)$$

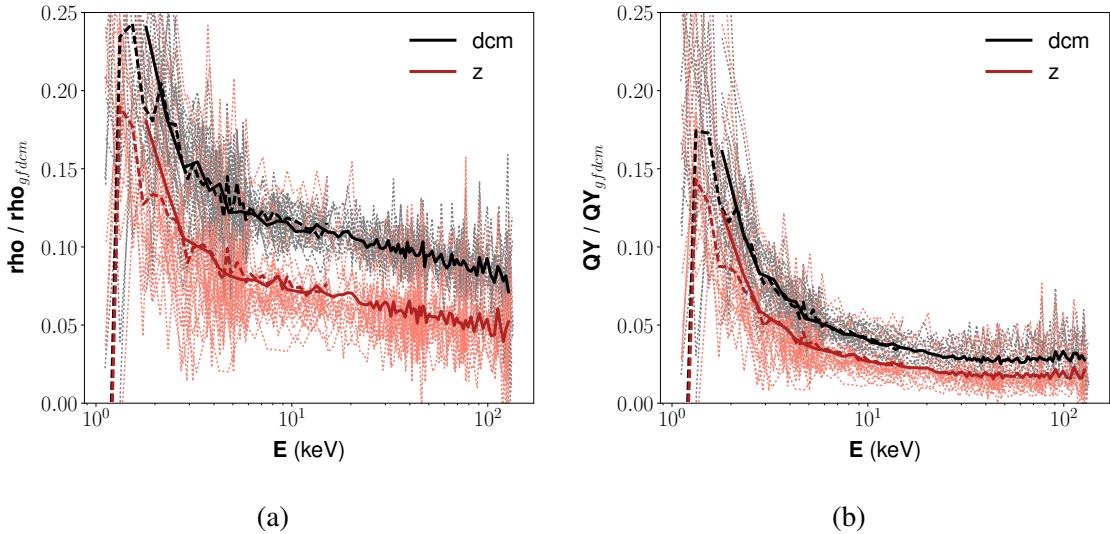


Figure 5.35: Ratio between the results for $\langle \rho \rangle$ (a) and QY (b) for the various corrections methods. The red lines indicate “z”/“gfdcm” data, and the black lines indicated “dcm”/“gfdcm” data. The light dotted lines indicate ratios in individual field-bins for both carbon-14 and tritium. The dark dashed lines show the average of tritium datasets over all of the field bins, and the solid lines show the average of carbon-14 datasets.

These measurements are also shown in figures 5.36 and 5.37. In these plots, the error-bars represent the systematic and statistical uncertainties are added together in quadrature. We can see here that there is some discrepancy between the various corrections-methods defined in section 4.3. The ratio of the “z” and “dcm” results to the “gfdcm” results are

shown in figure 5.35. On average, the “gfdcm” measurements of $\langle \rho \rangle$ are 7% lower than the “z” measurements and are 11% lower than the “dcm” measurements, with the discrepancy being higher toward low energy, and lower toward high energy. After translating to QY using equation 5.61, the mean offsets go down to 3.0% for “z” and 4.5% for “dcm”. The arguments we made in section 4.3.2 show that the “gfdcm” corrections provide the most physically sensible data, and as we show in the next section, it generates yield measurements that are consistent with world data. We will therefore continue to use the “gfdcm” data without accepting further systematic uncertainty due to the discrepancy between the correction types.

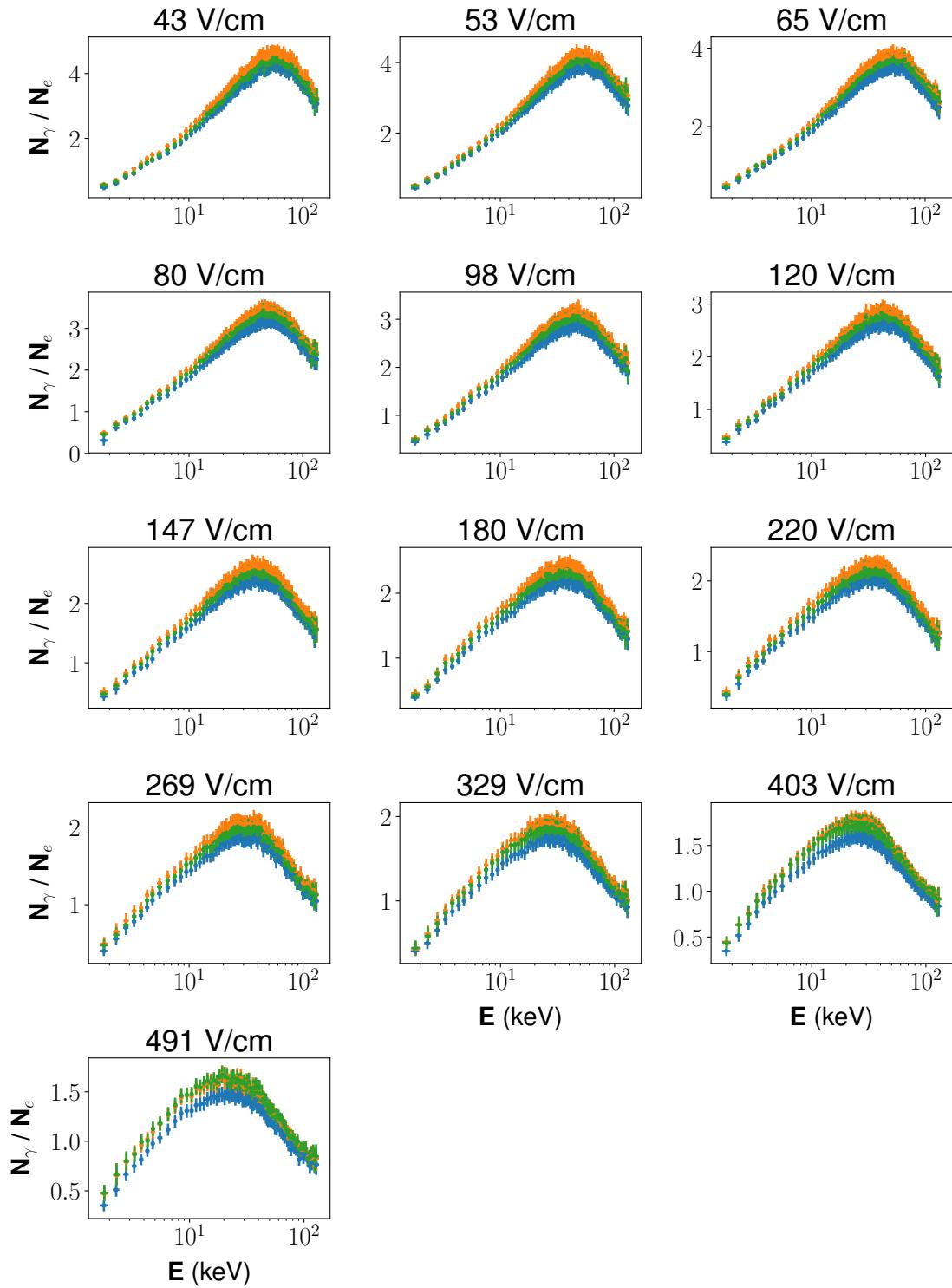


Figure 5.36: Measurements of $\langle \rho \rangle$ for post-Run04 carbon-14 data in the various electric field bins. The error-bars show a combination of statistical and systematic uncertainty. The blue points are for the “z” corrected data, the green points are for the “dcm” corrected data, and the orange points are for the “gfdcm” corrected data.

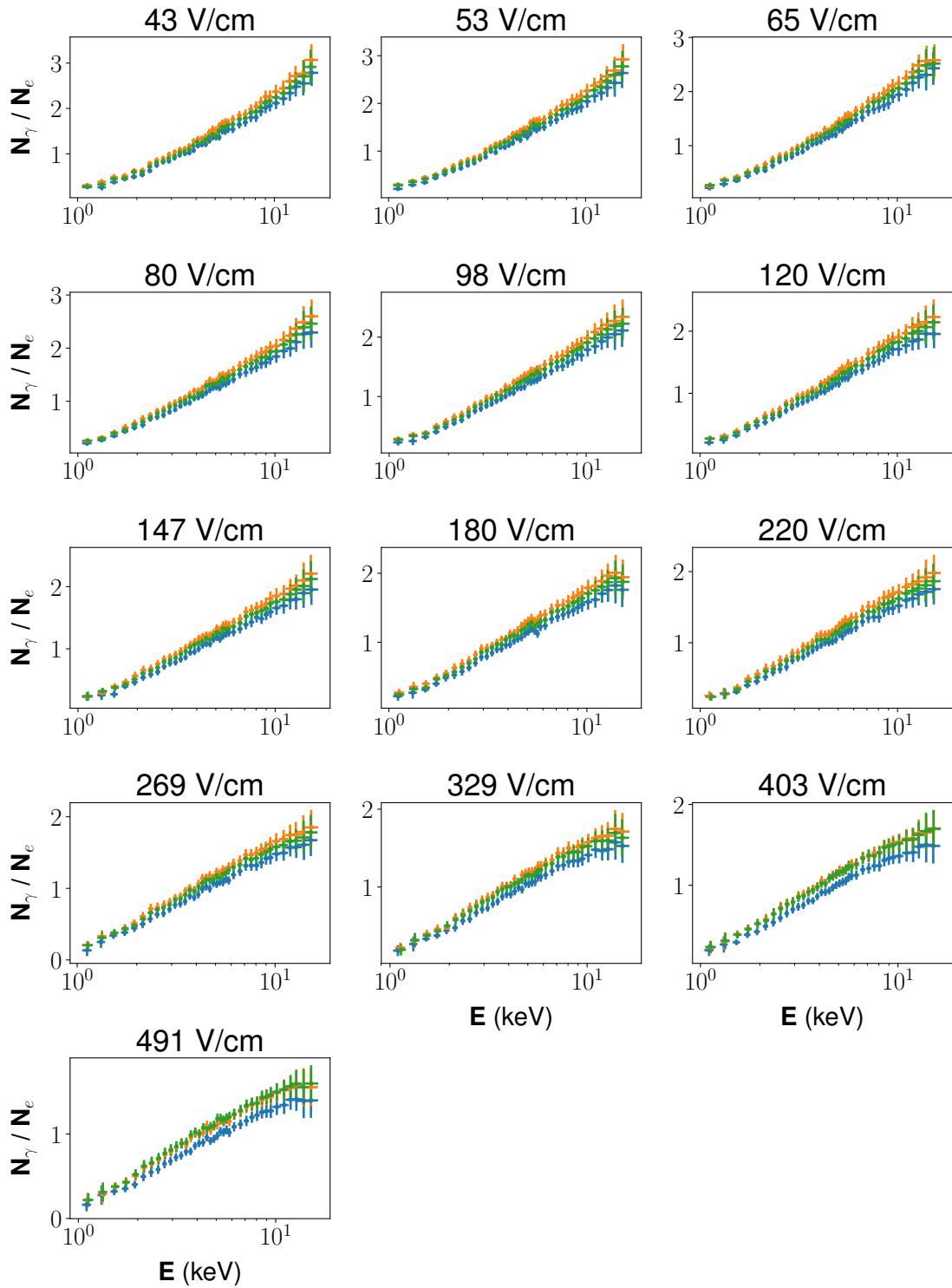


Figure 5.37: Measurements of $\langle \rho \rangle$ for post-Run04 tritium data in the various electric field bins. The error-bars show a combination of statistical and systematic uncertainty. The blue points are for the “z” corrected data, the green points are for the “dcm” corrected data, and the orange points are for the “gfdcm” corrected data.

5.5.2 Measurement of the Shape of the ^{14}C Beta-Spectrum

The updated libNEST model can also be used to test the measured carbo-14 beta spectrum for a non-statistical spectral shape. We assume a Kuzminoz-style shape factor[?] which was presented in section 5.1.3:

$$C(E_{true}) = 1 + \beta \cdot (Q - E_{true}) \quad (5.63)$$

We again apply a Metropolis-style fit, as was described for measuring the S2 tails in section 4.4. For each iteration, we select a shape factor slope, β from a normal distribution centered at the previous value, with a standard deviation of 0.1 MeV^{-1} . We apply the libNEST model to the new test spectrum, and then compute the chi-squared difference between the resulting libNEST spectrum and the observed spectrum. The transition probability is again taken to be:

$$P_{accept} = \min(1, \exp(-(\chi_i^2 - \chi_{i-1}^2)/2)) \quad (5.64)$$

Looking at all of the available data from 50 to 300 microseconds drift time we find that the most likely slope is $-0.24 \pm 3.7 \pm 1.7 \text{ MeV}^{-1}$, where the statistical error is 3.7 MeV^{-1} . The systematic error of 1.7 MeV^{-1} comes from the slope of the acceptance of our selection cut in section 4.1.1. We further analyze our systematics by dividing the data by drift time and event rate. We select five drift time slices ranging from 50 to 300 microseconds, and with width of 50 microseconds each. The best-fit slope for each of these bins is consistent with zero, and we find no significant variation between them. The results for the drift time slices are shown in table ??.

To divide the data by rate, we select two groups of events, one before the median event time and the other after the median event time. Since the radio-labeled methane is being purified away at a constant rate, the first group will have a maximum event rate that is

double that of the second group. We find that there is a small systematic effect due to event rate. The high event rate grouping had a best fit slope of $-0.07 \pm 3.8 \text{ MeV}^{-1}$, while the low event rate grouping had a best fit slope of $-0.51 \pm 3.8 \text{ MeV}^{-1}$. The most likely source of this systematic is a rate dependence of our acceptance cut. Regardless of its origin, we accept an additional systematic error of ± 0.29 on our measurement of β .

Combining statistical and systematic errors, our best fit shape factor is:

$$C(T) = 1 + (-0.07 \pm 0.50 \text{ MeV}^{-1}) \cdot (Q - T), \quad (5.65)$$

Where we have adjusted our measurement in the full dataset by the slope of the cut acceptance, as well as including it in the systematic error. This result is not in agreement with the Kuzminov result of $\beta = 1.24 \pm 0.04 \text{ MeV}^{-1}$.

We would like to check that this disagreement is not due to error in our S2 tail model. To do this, we refit the tail parameters using the carbon-14 spectrum itself. We assume a shape factor equal to the Kuzminov result when generating the libNEST spectrum. We include a simulation of the xenon-131m line, and accept only results for which the peak of the simulated spectrum is within 1 keV of the data. This puts a constraint on our fit to $G2_{true}$. The resulting best-fit spectrum does not match the data nearly as well as the spectrum generated assuming a purely statistical spectral shape. The reduced chi-squared for the Kuzminov carbon-14 spectrum is double that of the spectrum generated with no shape factor (4.4 and 2.2, respectively). This is despite the fact that the former was tuned specifically to the carbon-14 spectrum, while the latter was tuned using only argon-37 and xenon-131m data. Additionally, the xenon-131m line generated using the Kuzminov best-fit parameters is significantly wider than what is observed in the data.

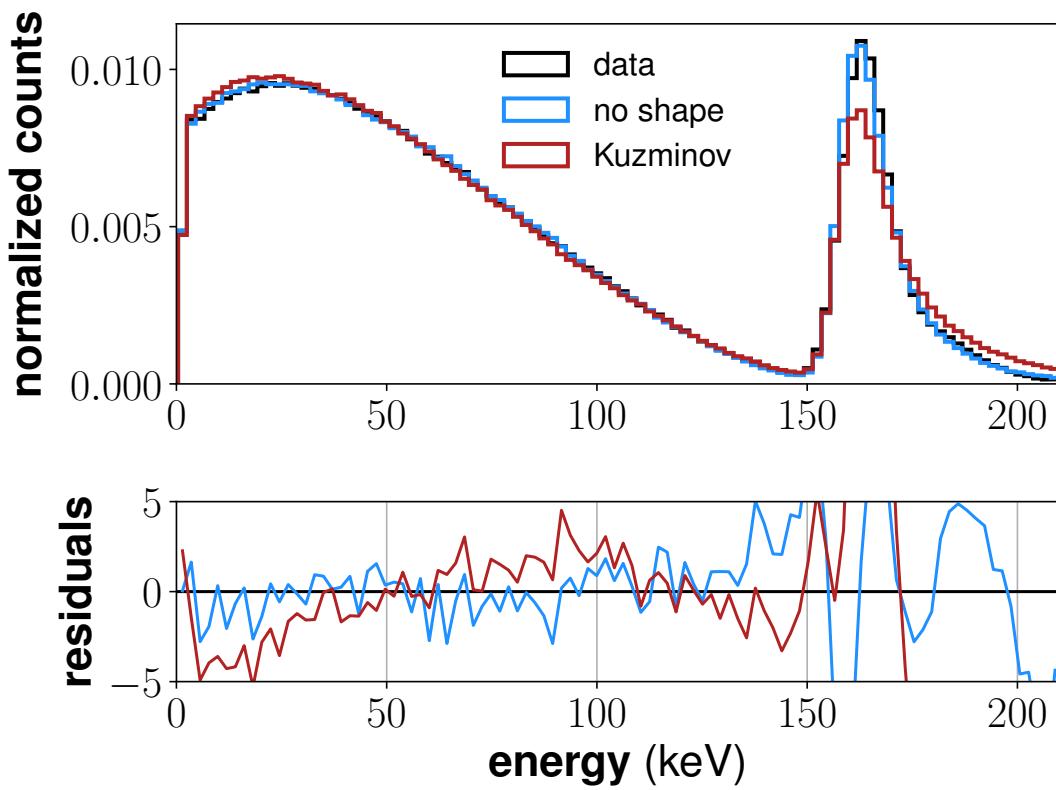


Figure 5.38: Comparison of simulated spectra to that measured by data. The Kuzminov spectrum uses a shape factor slope of $\beta = 1.24 \text{ MeV}^{-1}$, and tunes the S2 tail parameters to best fit the carbon-14 data spectrum. The “no shape” spectrum assumes $\beta = 0 \text{ MeV}^{-1}$, and uses the tail parameters obtained from argon-37 and xenon-131m.

5.6 Charge-Yield Model for Beta and Compton Interactions

These data represent an extremely comprehensive set of measurements for charge and light yield for beta- or Compton-like interactions in liquid xenon. We have probed 13 different electric-field values, from 43 to 491 V/cm, at energies ranging from 1 to 145 keV. By using existing world data to fill in the gaps, especially at high-field and high-energy, we should be able to develop a solid model of LY and QY as a function of field and energy.

5.6.1 World Data

Outside of LUX Run03 data [8, 10, 11], the first dataset we add to our fits is the argon-37 PIXeY data[22]. This data is extremely useful, in particular, because of the measurements of QY for the 0.27 keV L-capture peak. These measurements will form the low-energy constraint on our fits at most values of the electric field. The the measurements for the L-capture peak are taken at electric fields of 99, 198, 396, 693, 990, and 1980 V/cm. The trend in the L-capture QY is smaller than the stated errors, so it should be safe to interpolate between the PIXeY values for a low-energy constraint on datasets with intermediate electric fields. We take the uncertainty on these interpolations to be equal to the maximum error of the L-capture measurements plus their standard deviation. The PIXeY L-capture data, along with the interpolation is shown in figure 5.39

For the high energy constraint, we used data from a 2002 paper from Doke et. al., which measured scintillation yields of conversion electrons from ^{207}Bi [32]. We digitized the data for scintillation yield, LY, versus \mathcal{E} and calculated the charge yield using $QY = 73 - LY$. The measurements were taken at electric fields ranging from about 0 to 10 kV/cm, so to calculate values at intermediate fields, we fit the values of QY versus \mathcal{E} to a sigmoid. The error on these values is taken to be the 8% error cited in the paper plus the error due to the uncertainty in the electric field for the specified set of data.

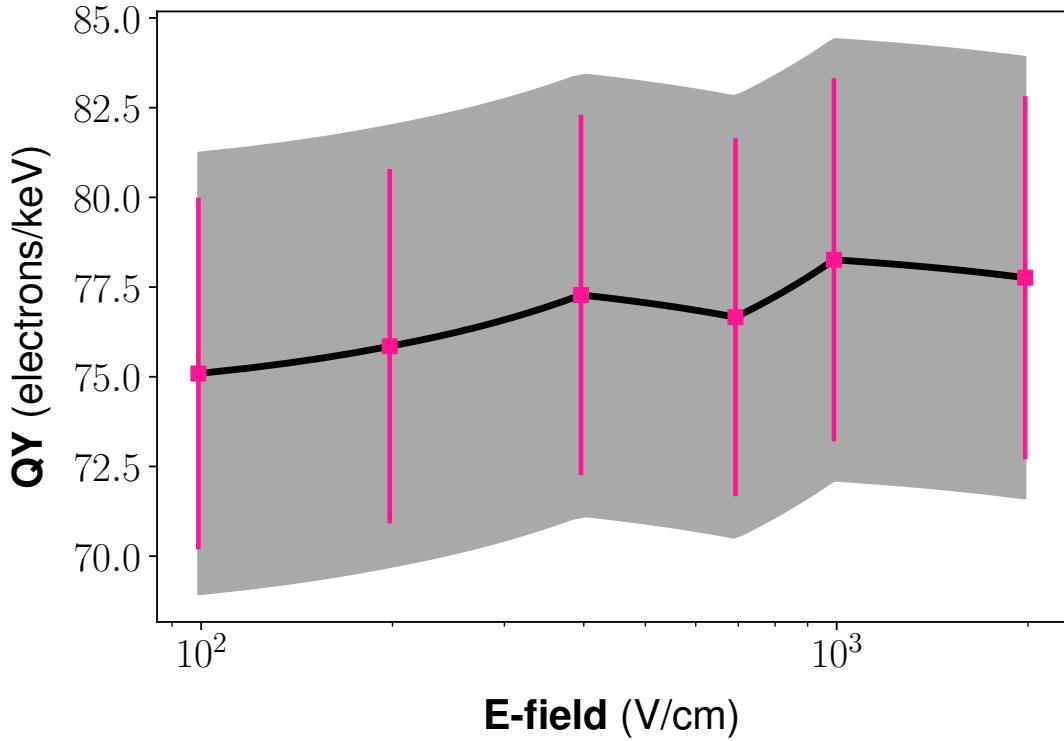


Figure 5.39: PIXeY L-capture measurements (pink) and the interpolation used to calculate the value at intermediate fields (black). The grey band indicates the size of the error accepted for the interpolated values.

In addition to the measurements of σ_R for ^{57}Co , Dahl also presents measurements of ρ for ^{133}Ba and ^{252}CF [1]. A recent study on the PIXeY experiment has shown that Dahl likely overestimates his extraction efficiency by about 13%[35]. We therefore adjust his measurements of QY by 1/0.883. The errors for this dataset are taken to be his maximum instrumental error.

The neriX experiment also has an extensive set of measurements of Compton scattering of photons from a ^{137}Cs source off of a liquid xenon target[43]. The experimenters use a HPGe scintillation detector to measure the scattering angle, and thereby reconstruct the energy deposited in the xenon. Using this method, they are able to create a set of data that spans from about 1-100 keV, at fields ranging from 100 to 2,000 V/cm.

We have also included a set of high-field measurements from Akimov et. al.[12]. This dataset includes a combination of beta and gamma events, but appears to fit with the rest of the beta data discussed. The data was taken at 3750 V/cm, and we will combine it with the 4050 V/cm dataset from Dahl.

We use three sets of data to create a collection of 0-field measurements. The paper from Doke et. al. quotes a 0-field value for LY, so we again use this measurement as our high-field constraint. Manalaysay et. al. and Aprile et. al. both made measurements of scintillation yield relative to the 32.1 keV gamma from the ^{83m}Kr decay at 0-field[14, 16]. Matthew Szadagis and Vetri Velan provided us with a formula for the absolute value of the ^{83m}Kr light yield, which was developed for the NEST v2.0 model,[74]. This dataset will not be used in the fits for QY, but will rather serve as a cross-check.

5.6.2 QY Model Fits

The procedure for this will be similar to what was introduced in section 5.3.4, where we derived a preliminary model of QY in order to improve our measurements of the smearing corrections. The primary difference here is that we will be including more data in our fits. We will again restrict our fits to QY only, allowing LY to be defined as equal to $1/W - QY$. The functional form for $QY(E, \mathcal{E})$, at a constant electric field, \mathcal{E}_1 will again be a double-asymmetric sigmoid:

$$QY(E, \mathcal{E})|_{\mathcal{E}_1} = m_1 + \frac{m_2 - m_1}{(1 + (E/m_3)^{m_4})^{m_9}} + m_5 + \frac{0 - m_5}{(1 + (E/m_7)^{m_8})^{m_{10}}}, \quad (5.66)$$

We have compiled the measurements from this work, along with the world data described in the previous section, into 18 collections, all at different electric field values. Each dataset that goes into a collection has its uncertainties multiplied by the square-root of its length to ensure that each of the datasets will have a roughly equal weight. This is impor-

tant because otherwise the argon-37 L-capture point and the ^{207}Bi conversion electron will be washed out by the datasets with measurements at many energies. The dominant error in all of the datasets is systematic so we would not necessarily expect the data-points within an individual dataset to fluctuate around the model, but rather should be offset from the model by it's true systematic error. Multiplying the individual uncertainties by \sqrt{N} allows a large number of data-points within a measurement to be systematically offset without completely throwing the fit off of the other measurements in the collection.

For the purposes of fitting we have combined the statistical errors shown in appendix A with systematic errors. In the formulas used for calculating the QY and its uncertainties are:

$$QY = \frac{1}{W} \frac{1}{1+\rho} \quad (5.67)$$

$$\sigma_{QY}^2 = \left(\frac{1}{W} \frac{\sigma_{\rho,tot}}{(1+\rho)^2} \right)^2 + \left(QY \frac{\sigma_{E,tot}}{E_{true}} \right)^2,$$

where $\sigma_{\rho,tot}$ and $\sigma_{E,tot}$ are the combined systematic uncertainties on the ρ and E_{true} measurements. Unless otherwise specified, we use only “gfdcm” corrected data.

Just as in section 5.3.4 we will to each collection individually, initially floating all of the parameters for all of the collections. We will iterate this process, selecting one parameter to hold constant after each iteration until we are left with only parameters which cannot be approximated as being constant in \mathcal{E} . At this point we will characterize the remaining parameters as functions of \mathcal{E} .

When calculating the constant value of a parameter, we use the error-weighted average of the best fit values from the various field collections. Figure 5.40 shows the results of these calculations. Especially in the first several iterations, there is degeneracy in the parameters leading to very large uncertainties in the best fit results. When calculating the error weighted average, we do no include the values with large error-bars. For the cal-

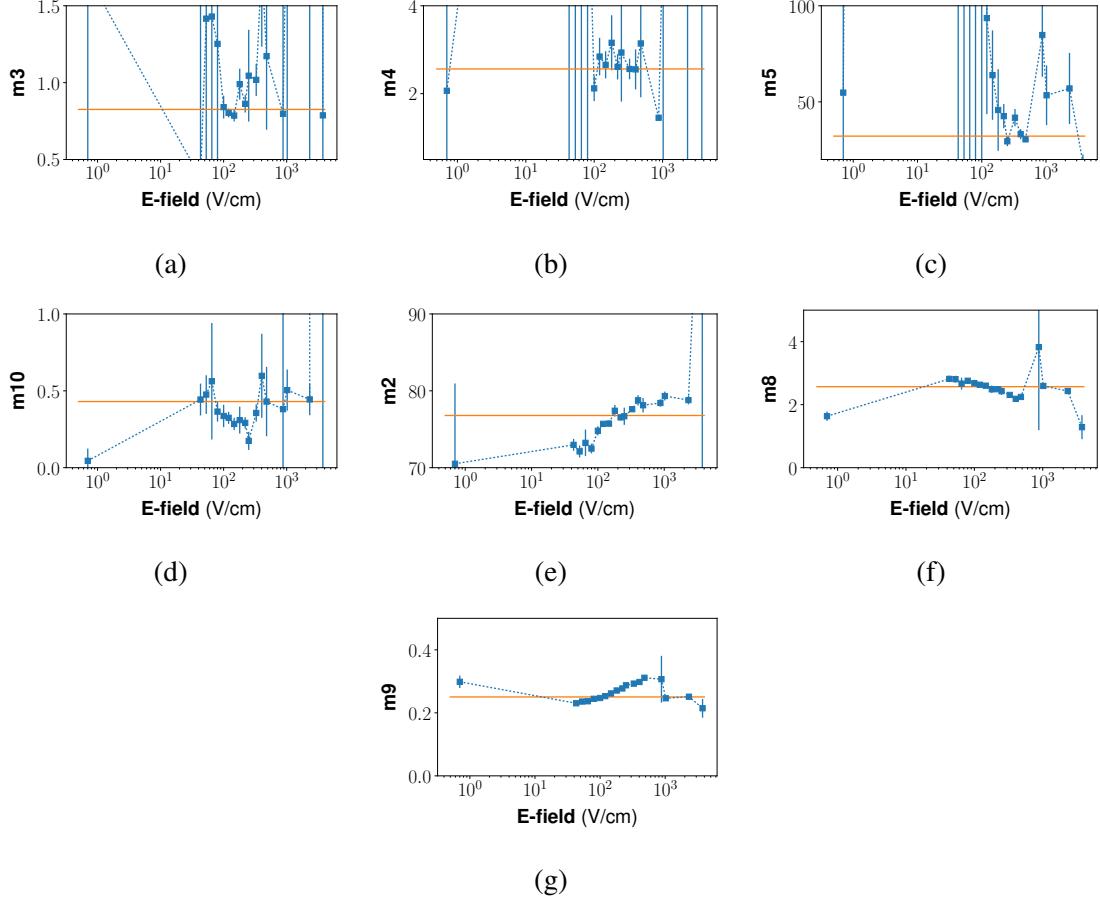


Figure 5.40: Parameters we have chosen to hold constant for the model of the beta/Compton charge yield. The blue markers show the best-fit values for the individual field collections, and the orange line shows the constant value to which we hold the parameter. The far left datapoint in these plots is the 0-field collection, which is shown but not included in the calculation of the constant value.

culations of m_4 and m_2 we also exclude field collections below our 100 V/cm collection, because there are not low-energy measurements in those collections, and these specific parameters are most sensitive at low-energy. An argument could be made that m_2 should be allowed to vary with electric field, but we found that the final model gives more sensible if it was held constant. The last two parameters we held constant, m_8 and m_9 , are clearly trend beyond the fitting error in collections that include LUX post-Run04 measurements. We hold these constant because the overall trend in world data between 0 to 4000 V/cm is roughly constant.

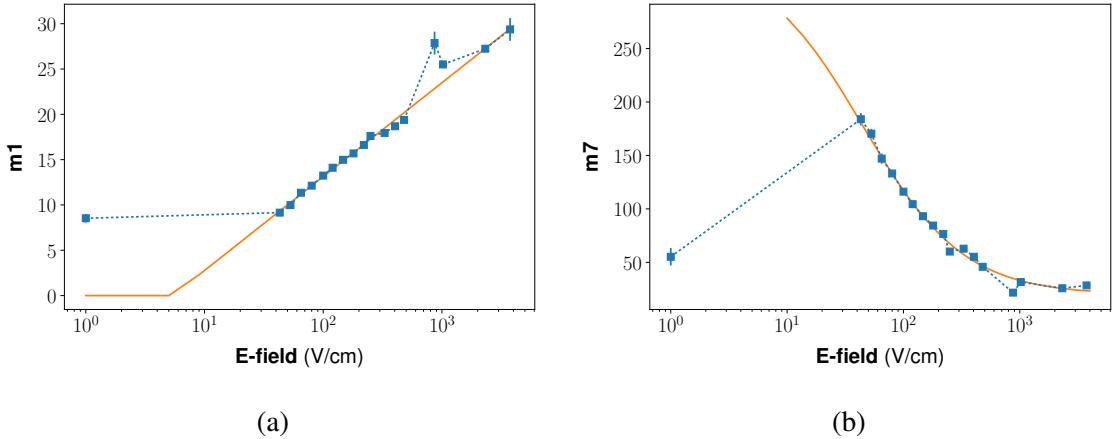


Figure 5.41: Fitting parameters for the beta/Compton model which we have selected to vary in electric field. In (a), we fit m_1 to a line in $\log_{10}(\mathcal{E})$ space, and in (b), we fit m_7 to a standard sigmoid in electric field. The lowest field data point is againd excluded from the fits.

The remaining parameters, m_1 and m_7 are successively fit to functions in \mathcal{E} . We found that m_1 can be sufficiently described by a line in $\log_{10}(\mathcal{E})$ space, while m_7 requires more free parameters to describe its shape. The parameter m_1 represents the minimum possible QY at a given field, so we also impose a physicality condition that $m_1 > 0$.

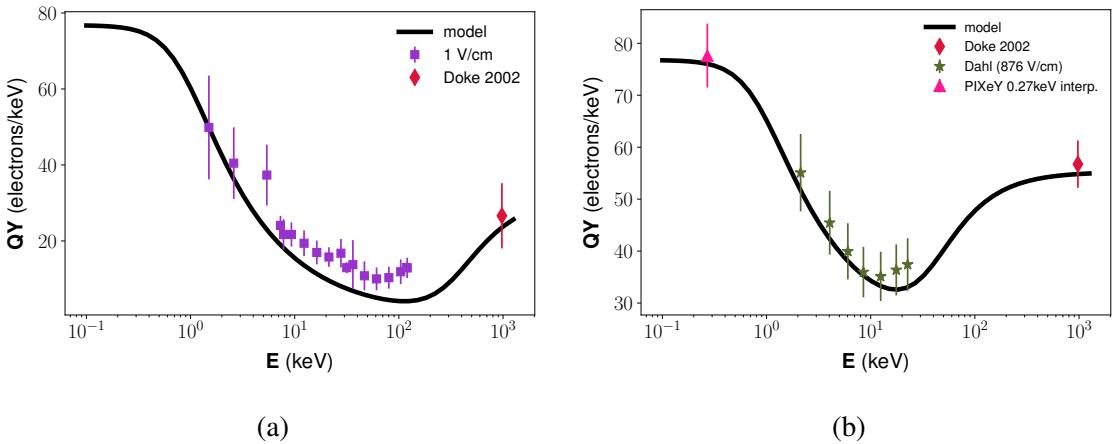


Figure 5.42: Comparison of model and data for the outliers shown in figure 5.41. The left plot (a) shows the 0-field collection, and the right plot (b) shows Eric Dahl's 876 V/cm measurements, along with interpolated values of the high and low energy constraints.

There are two clear outliers in these plots; the 876 V/cm point and the 0-V/cm point.

Outliers are not entirely unexpected because systematic effects can drive a dataset off of the model, thus changing the best-fit value this effect is clear in the 876 V/cm fit shown in figure 5.42 (b). The only dataset in this collection is the Dahl, 876 V/cm line. Dahl's measurements tend to turn over at lower energies than other measurements, and this drives the 876 V/cm dataset off of the model, thus altering the best-fit value. Even though the best fit values for m_1 and m_7 are several-sigma off of the trend-line, all the individual data-points in the 876 V/cm set are within error of the model. This again comes down to the nature of systematic uncertainty.

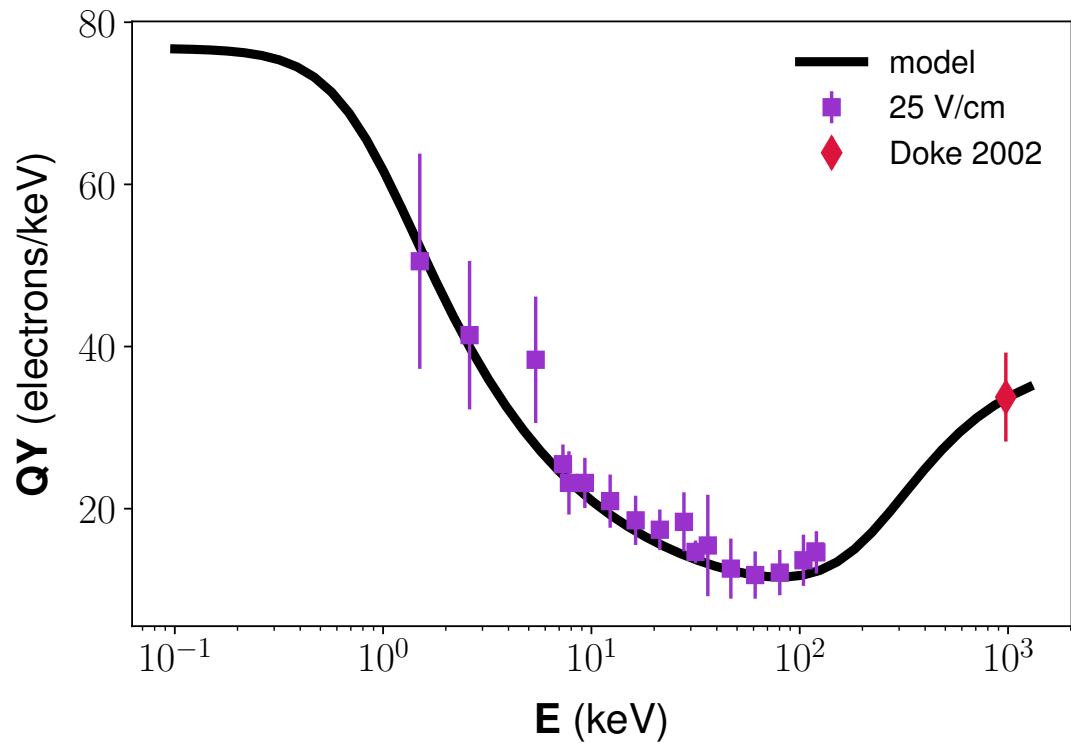


Figure 5.43: 0-field collection compared to our model evaluated at 25 V/cm.

The collection at 0-field is also an outlier as is shown in figure 5.42 (a). This collection disagrees with our model by close to 2-sigma. Our best guess is that this is due to non-zero electric field in the respective detectors. Electric fields in small detectors are notorious for

being hard to control and measure, so even with the voltage set to 0 it might be possible that residual electric fields persist. If we assume that the true value of the electric field for this collection is 25 V/cm, the points fall neatly into place with our model, as is shown in figure 5.43.

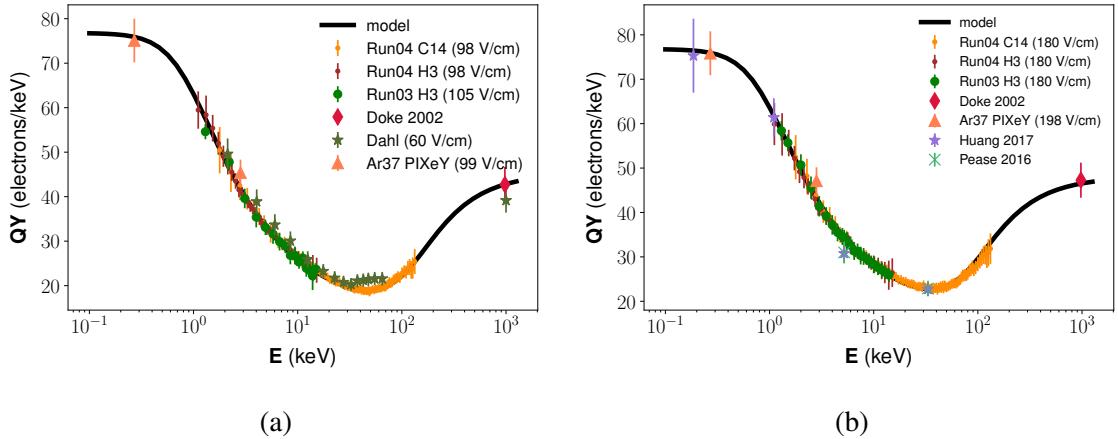


Figure 5.44: Model vs. data for collections including LUX Run03 measurements.

The LUX post-Run04 data holds together extremely well with previous measurements from LUX Run03, as we see in figure 5.44. There is one caveat; the Run03 measurements all use the standard summed pulse-finder area to measure S2 size, while the “gfdcm” measurements use the area under a Gaussian fit to the pulse-finder area. We have found that in post-Run04 data, this Gaussian best fit area is likely a better measure of the S2 size. If we compare Run03 data to the “dcm” measurements, which also use the summed pulse-finder area, we find that it is still in agreement with post-Run04 within about 1-sigma (see figure ??).

The neriX data and these data are extremely complimentary. The two experiments have overlap in electric from about 200 to 500 V/cm. Above that, neriX extends by about a factor of 5 up to 2,320 V/cm, and below that, LUX extends down by a factor of 5, to 43 V/cm. The neriX data has two subsets that can be directly compared to LUX data; one at 190 V/cm and the other at 480 V/cm. We compare the neriX 480 V/cm data to the our 491 V/cm

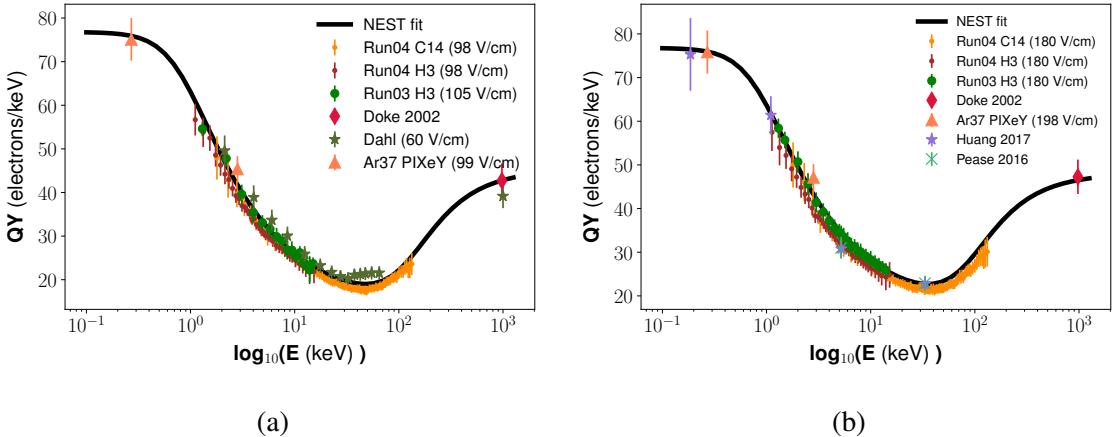


Figure 5.45: Model vs. data for collections including LUX Run03 measurements, where the “Run04” measurements are made using the “dcm” corrected data.

dataset. The two are in decent agreement, especially at low energy, with the high energy end being discrepant by just over 1-sigma. We would also like to compare the neriX 190 V/cm data with our 180 V/cm dataset, but the two disagree by several standard deviations. We instead combine the 190 V/cm neriX data with our 269 V/cm data into a collection we call 250 V/cm. This corresponds to a 2-sigma increase in the neriX field value and a 1-sigma decrease in the LUX value. We justify this increase in the neriX field because the authors show in [43] that their 190 V/cm light yield measurements are consistent with the 236 V/cm light yield data in [?].

Figures 5.48 and 5.49 show the remaining LUX post-Run04 datasets. We note that below 65 V/cm and above about 220 V/cm, there is some increased systematic disagreement between the model and the measured LUX yields at the high energy end of the carbon-14 spectrum. This tension can be resolved by allowing the m_3 parameter to vary, but that increases the number of free parameters in our fit by about 4. It would also likely worsen the agreement in the higher-field collections (shown in figure 5.50). The disagreement is never more than about 1-sigma, and the high energy end of the spectrum is the most sensitive to error in the tail model, so we opt to keep m_3 constant in field. We also note that Dahl’s 60

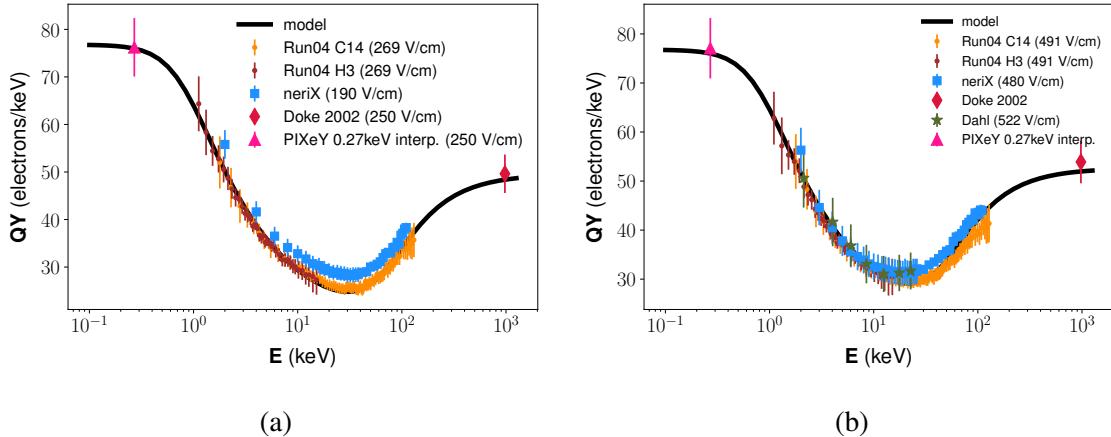


Figure 5.46: Model vs. data for collections including both LUX and neriX measurements.

V/cm measurement is more consistent with his quoted nominal value of 100 V/cm.

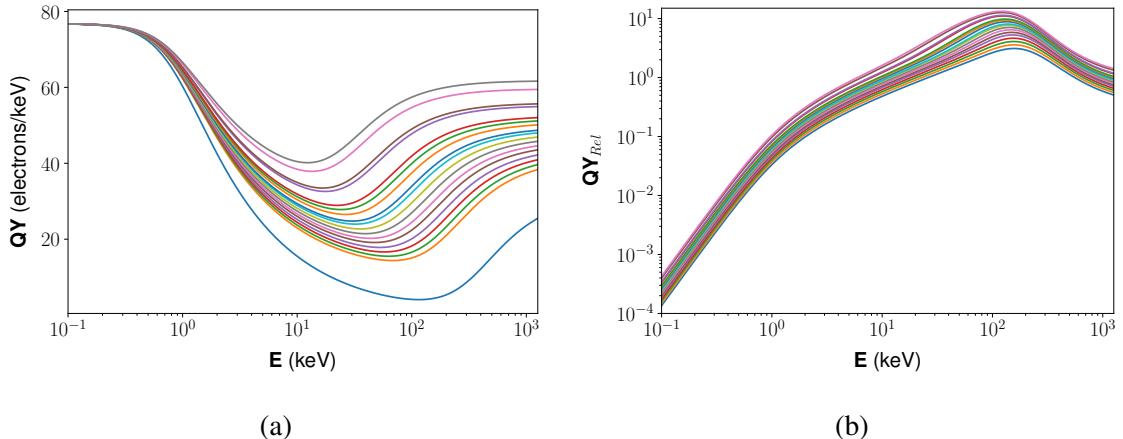


Figure 5.47: Model of QY for beta/Compton interactions at the various fields studied. The model is evaluated at 0, 43, 53, 65, 100, 120, 147, 180, 220, 250, 329, 403, 480, 876, 1020, 2320, and 3750 V/cm. The left plot (a) shows the absolute charge yield, while the right plot (b) shows the charge yield relative to the 0 V/cm value.

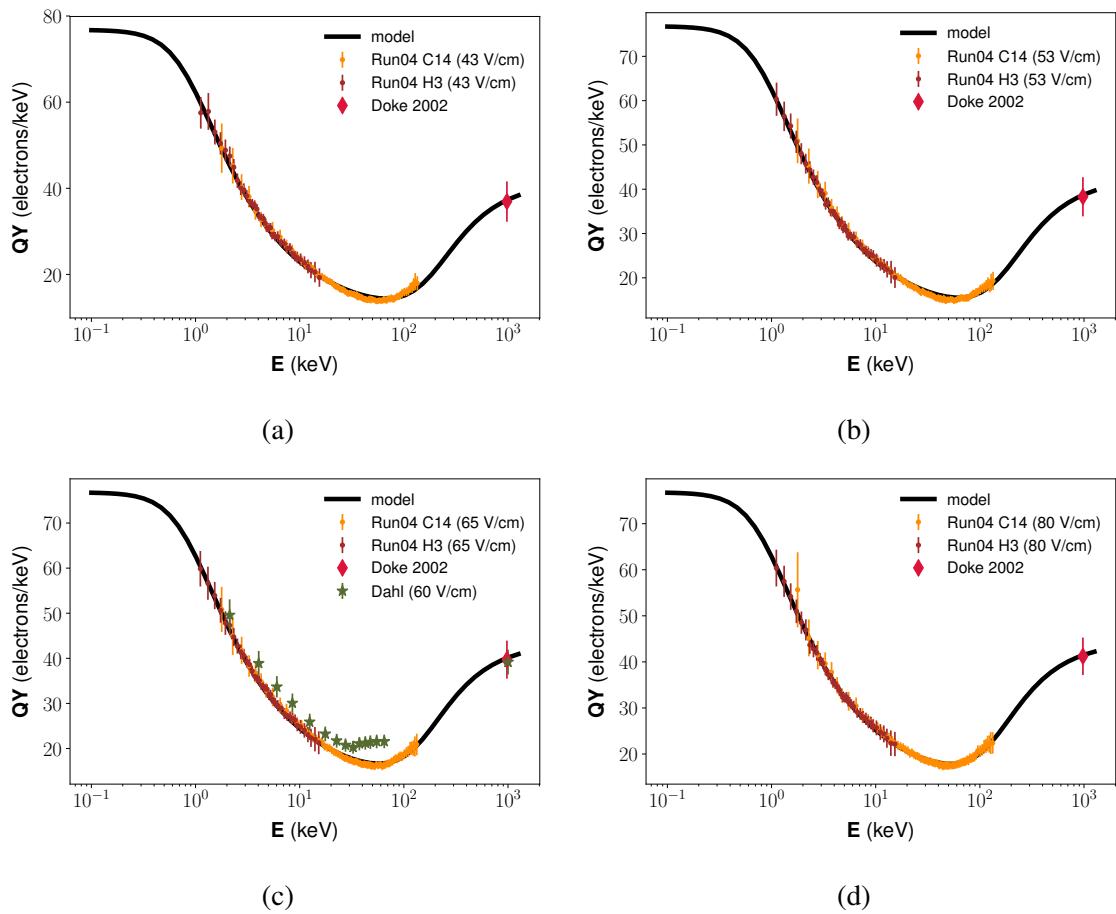


Figure 5.48: Model vs. data for low-field LUX post-Run04 measurements.

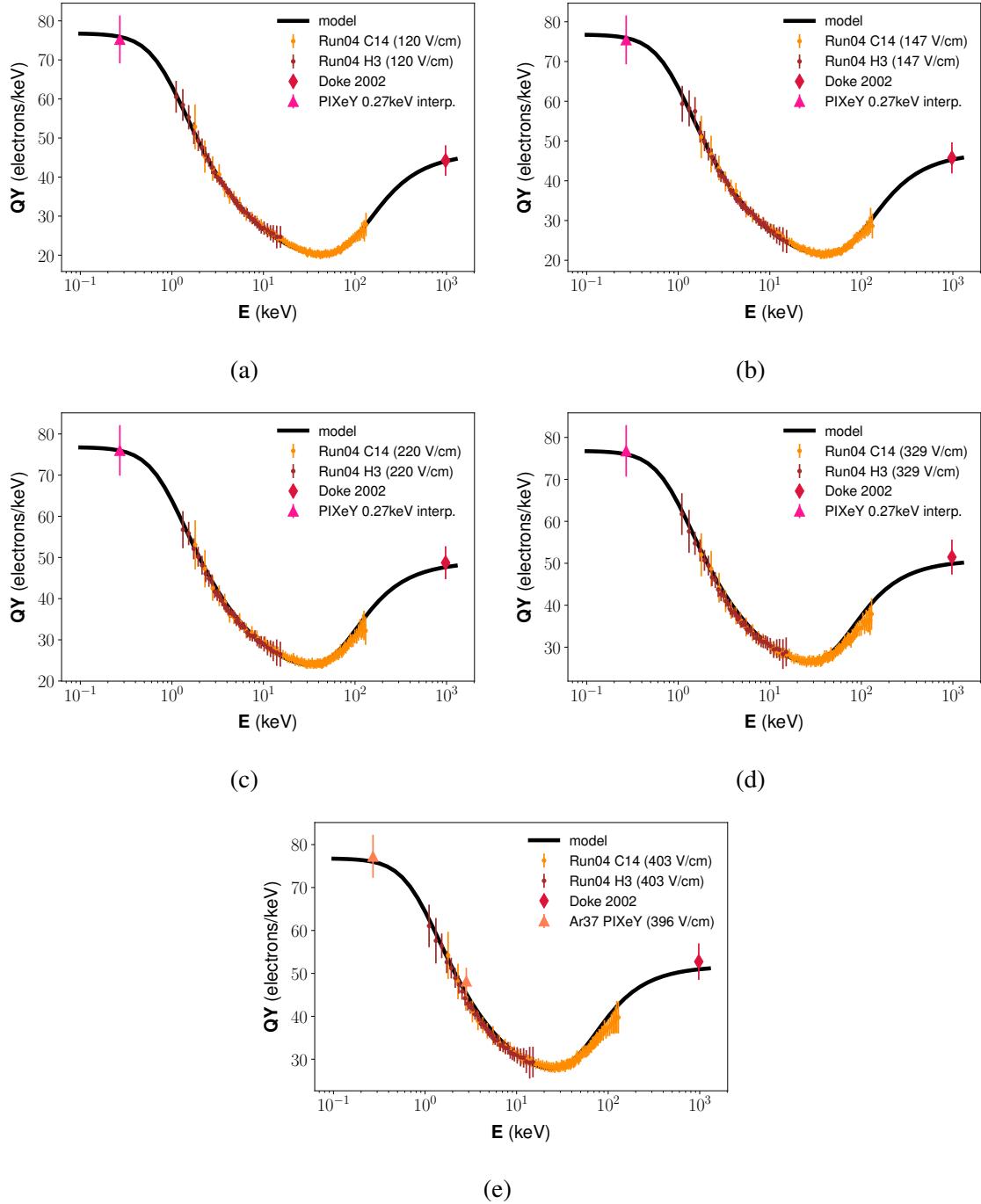


Figure 5.49: Model vs. data for intermediate-field LUX post-Run04 measurements.

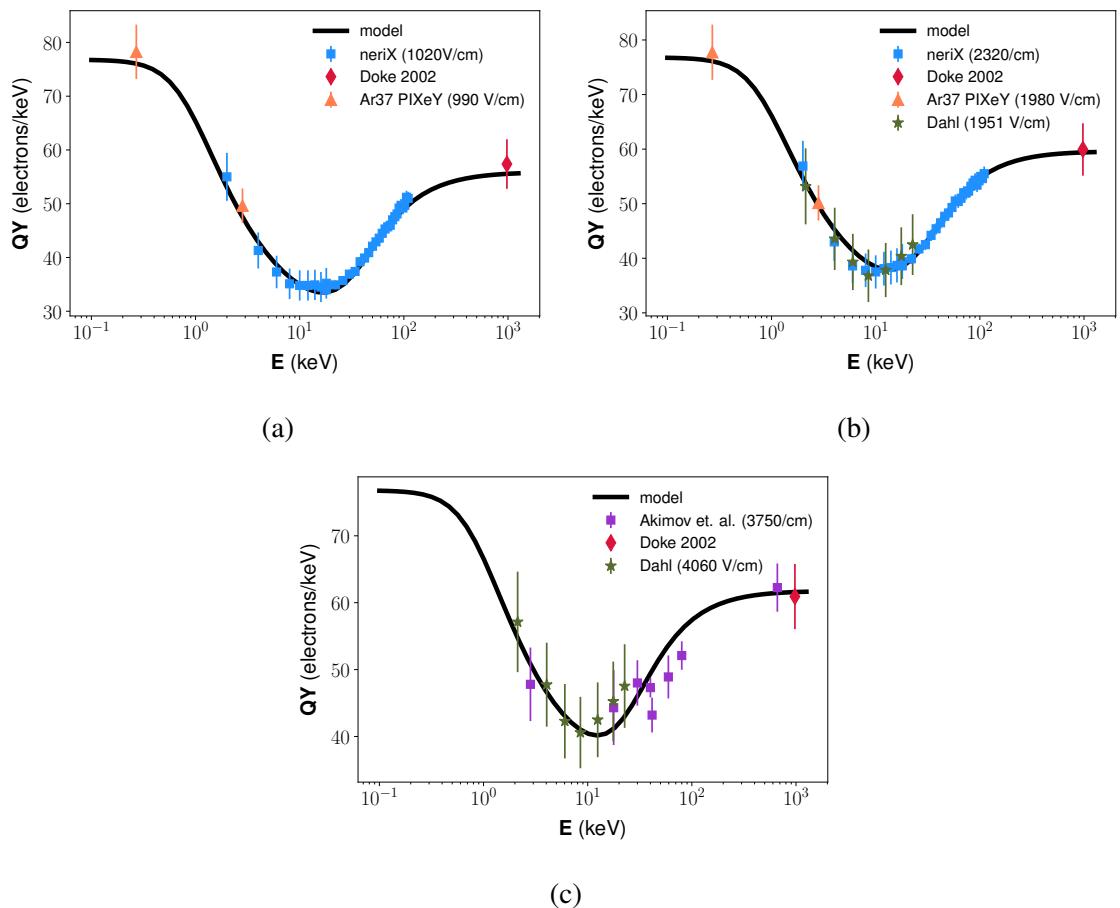


Figure 5.50: Model vs. data for collections with electric fields above those in LUX post-Run04.

Appendix A: Yields Results

A.1 Carbon-14 $\langle E_{true} \rangle$

E-field (V/cm)	43.2 ± 2.5	52.6 ± 2.9	64.8 ± 3.7	79.8 ± 4.6	97.8 ± 5.6	119.6 ± 6.9	146.7 ± 8.3	180 ± 10	219 ± 13	268 ± 15	329 ± 19	405 ± 22	484 ± 28	
energy bin #	$\langle E_{true} \rangle \pm$													
1	1.8	0.1	1.8	0.1	1.8	0.1	1.8	0.1	1.8	0.1	1.8	0.1	1.8	0.1
2	2.3	0.1	2.3	0.1	2.3	0.1	2.3	0.1	2.3	0.1	2.3	0.2	2.3	0.1
3	2.8	0.1	2.8	0.1	2.8	0.1	2.8	0.1	2.8	0.1	2.8	0.2	2.8	0.1
4	3.3	0.1	3.3	0.1	3.3	0.1	3.3	0.1	3.3	0.1	3.3	0.1	3.3	0.1
5	3.8	0.1	3.8	0.1	3.8	0.1	3.8	0.1	3.8	0.1	3.8	0.1	3.8	0.1
6	4.3	0.1	4.3	0.1	4.3	0.1	4.3	0.1	4.3	0.1	4.3	0.1	4.3	0.1
7	4.7	0.1	4.8	0.1	4.8	0.1	4.8	0.1	4.8	0.1	4.8	0.1	4.8	0.1
8	5.5	0.3	5.5	0.3	5.5	0.3	5.5	0.3	5.5	0.3	5.5	0.3	5.5	0.3
9	6.5	0.3	6.5	0.3	6.5	0.3	6.5	0.3	6.5	0.3	6.5	0.3	6.5	0.3
10	7.5	0.3	7.5	0.3	7.5	0.3	7.5	0.3	7.5	0.3	7.5	0.3	7.5	0.3
11	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3
12	9.5	0.3	9.4	0.3	9.4	0.3	9.5	0.3	9.4	0.3	9.4	0.3	9.4	0.3
13	10.4	0.3	10.4	0.3	10.4	0.3	10.4	0.3	10.4	0.3	10.4	0.3	10.4	0.3
14	11.4	0.3	11.4	0.3	11.4	0.3	11.4	0.3	11.4	0.3	11.4	0.3	11.4	0.3
15	12.4	0.3	12.4	0.3	12.4	0.3	12.4	0.3	12.4	0.3	12.4	0.3	12.4	0.3
16	13.4	0.3	13.4	0.3	13.4	0.3	13.4	0.3	13.4	0.3	13.4	0.3	13.4	0.3
17	14.4	0.3	14.4	0.3	14.4	0.3	14.4	0.3	14.4	0.3	14.4	0.3	14.4	0.3
18	15.4	0.3	15.4	0.3	15.4	0.3	15.4	0.3	15.4	0.3	15.4	0.3	15.3	0.3
19	16.4	0.3	16.4	0.3	16.4	0.3	16.4	0.3	16.4	0.3	16.3	0.3	16.3	0.3
20	17.4	0.3	17.4	0.3	17.4	0.3	17.3	0.3	17.3	0.3	17.3	0.3	17.3	0.4
21	18.4	0.3	18.4	0.3	18.3	0.3	18.3	0.3	18.3	0.3	18.3	0.4	18.3	0.4
22	19.4	0.3	19.3	0.3	19.3	0.3	19.3	0.3	19.3	0.4	19.3	0.4	19.3	0.4
23	20.3	0.3	20.3	0.3	20.3	0.4	20.3	0.4	20.3	0.4	20.3	0.4	20.3	0.4
24	21.3	0.3	21.3	0.3	21.3	0.4	21.3	0.4	21.3	0.4	21.3	0.4	21.2	0.4
25	22.3	0.3	22.3	0.4	22.3	0.4	22.3	0.4	22.3	0.4	22.2	0.4	22.2	0.4
26	23.3	0.4	23.3	0.4	23.3	0.4	23.3	0.4	23.3	0.4	23.2	0.4	23.2	0.4
27	24.3	0.4	24.3	0.4	24.3	0.4	24.3	0.4	24.2	0.4	24.2	0.4	24.2	0.4
28	25.3	0.4	25.3	0.4	25.3	0.4	25.2	0.4	25.2	0.4	25.2	0.4	25.2	0.5
29	26.3	0.4	26.3	0.4	26.3	0.4	26.2	0.4	26.2	0.4	26.2	0.4	26.1	0.5
30	27.3	0.4	27.3	0.4	27.2	0.4	27.2	0.4	27.2	0.4	27.2	0.5	27.1	0.5
31	28.3	0.4	28.2	0.4	28.2	0.4	28.2	0.4	28.2	0.4	28.1	0.5	28.1	0.5
32	29.2	0.4	29.2	0.4	29.2	0.4	29.2	0.4	29.2	0.5	29.1	0.5	29.1	0.5
33	30.2	0.4	30.2	0.4	30.2	0.4	30.2	0.4	30.2	0.5	30.1	0.5	30.1	0.5
34	31.2	0.4	31.2	0.4	31.2	0.5	31.2	0.5	31.1	0.5	31.1	0.5	31.1	0.5
35	32.2	0.4	32.2	0.4	32.2	0.5	32.1	0.5	32.1	0.5	32.1	0.5	32.0	0.6
36	33.2	0.4	33.2	0.4	33.2	0.5	33.1	0.5	33.1	0.5	33.1	0.5	33.0	0.6
37	34.2	0.4	34.2	0.5	34.2	0.5	34.1	0.5	34.1	0.5	34.1	0.5	34.0	0.6
38	35.2	0.5	35.2	0.5	35.1	0.5	35.1	0.5	35.1	0.5	35.0	0.6	35.0	0.6
39	36.1	0.5	36.1	0.5	36.1	0.5	36.1	0.5	36.1	0.6	36.0	0.6	36.0	0.7
40	37.1	0.5	37.1	0.5	37.1	0.5	37.1	0.5	37.0	0.6	37.0	0.6	36.9	0.7
41	38.1	0.5	38.1	0.5	38.1	0.5	38.1	0.5	38.0	0.6	38.0	0.6	37.9	0.7
42	39.1	0.5	39.1	0.5	39.1	0.5	39.0	0.5	39.0	0.6	38.9	0.6	38.9	0.7
43	40.1	0.5	40.1	0.5	40.1	0.5	40.0	0.6	40.0	0.6	39.9	0.6	39.9	0.7
44	41.1	0.5	41.1	0.5	41.0	0.5	41.0	0.6	41.0	0.6	40.9	0.6	40.8	0.7
45	42.1	0.5	42.1	0.5	42.0	0.6	42.0	0.6	42.0	0.6	41.9	0.7	41.8	0.8
46	43.1	0.5	43.1	0.5	43.0	0.6	43.0	0.6	42.9	0.6	42.9	0.7	42.8	0.8
47	44.0	0.5	44.0	0.5	44.0	0.6	44.0	0.6	43.9	0.7	43.9	0.7	43.8	0.8
48	45.0	0.6	45.0	0.6	45.0	0.6	44.9	0.6	44.9	0.7	44.8	0.7	44.8	0.8
49	46.0	0.6	46.0	0.6	46.0	0.6	45.9	0.6	45.9	0.7	45.8	0.7	45.7	0.8
50	47.0	0.6	47.0	0.6	46.9	0.6	46.9	0.7	46.9	0.7	46.8	0.8	46.7	0.9
51	48.0	0.6	48.0	0.6	48.0	0.6	47.9	0.7	47.9	0.7	47.8	0.8	47.7	0.9
52	49.0	0.6	49.0	0.6	48.9	0.7	48.9	0.7	48.8	0.8	48.8	0.8	48.7	0.9
53	50.5	0.8	50.5	0.8	50.4	0.8	50.4	0.9	50.3	0.9	50.2	1.0	50.1	1.1
54	52.4	0.8	52.4	0.8	52.4	0.9	52.3	0.9	52.3	1.0	52.2	1.0	52.1	1.1
55	54.4	0.8	54.4	0.8	54.4	0.9	54.3	0.9	54.3	1.0	54.2	1.0	54.1	1.1
56	56.4	0.9	56.4	0.8	56.3	0.9	56.3	1.0	56.2	1.0	56.1	1.1	56.0	1.2
57	58.4	0.9	58.4	0.9	58.3	0.9	58.2	1.0	58.2	1.0	58.1	1.1	58.0	1.2
58	60.3	0.9	60.3	0.9	60.3	1.0	60.2	1.0	60.1	1.1	60.1	1.2	59.9	1.3
59	62.3	0.9	62.3	0.9	62.2	1.0	62.1	1.1	62.1	1.2	62.0	1.2	61.9	1.3
60	64.3	0.9	64.3	0.9	64.2	1.0	64.1	1.1	64.0	1.2	64.0	1.2	63.8	1.3
61	66.2	1.0	66.2	1.0	66.1	1.0	66.0	1.2	66.0	1.2	65.9	1.3	65.8	1.4
62	68.2	1.0	68.2	1.0	68.1	1.1	68.0	1.2	67.9	1.2	67.9	1.3	67.7	1.4
63	70.2	1.0	70.1	1.1	70.1	1.1	70.0	1.2	69.9	1.2	69.8	1.3	69.7	1.4
64	72.1	1.1	72.1	1.1	72.0	1.2	71.9	1.3	71.8	1.3	71.8	1.4	71.7	1.5
65	74.1	1.1	74.0	1.1	74.0	1.2	73.9	1.3	73.8	1.4	73.7	1.4	73.5	1.5
66	76.0	1.1	76.0	1.2	75.9	1.2	75.8	1.4	75.7	1.4	75.6	1.5	75.5	1.6
67	78.0	1.2	77.9	1.3	77.8	1.3	77.7	1.4	77.7	1.5	77.5	1.5	77.4	1.6
68	80.4	1.4	80.4	1.5	80.3	1.5	80.3	1.6	80.1	1.7	80.0	1.8	79.8	1.9
69	83.4	1.5	83.3	1.6	83.2	1.6	83.1	1.7	83.0	1.8	82.9	1.8	82.8	2.0
70	86.3	1.5	86.2	1.6	86.1	1.7	86.0	1.7	85.9	1.9	85.9	1.9	85.7	2.1
71	89.2	1.6	89.1	1.7	89.0	1.7	88.9	1.8	88.8	1.9	88.7	2.0	88.6	2.1
72	92.1	1.7	92.0	1.8	91.9	1.9	91.8	1.9	91.7	2.1	91.6	2.3	91.4	2.5
73	96.0	2.1	95.9	2.2	95.9	2.4	95.7	2.4	95.6	2.5	95.4	2.6	95.3	2.8
74	100.9	2.3	100.8	2.3	100.7	2.4	100.5	2.6	100.3	2.7	100.2	2.9	99.9	3.1
75	105.7	2.4	105.6	2.4	105.5	2.5	105.2	2.8	105.1	2.9	105.0	3.0	104.8	3.2
76	110.5	2.6	110.4	2.7	110.3	2.8	109.9	3.2	109.6	3.4	109.4	3.6	109.1	3.8
77	115.2	2.9	115.1	2.9	114.9	3.1	114.4	3.6	114.3	3.6	113.8	4.0	113.5	4.4
78	119.8	3.3	119.6	3.3	119.3	3.6	118.8	4.0	118.7	4.1	118.7	4.5	117.9	4.8
79	124.2	3.7	124.0	3.9	123.6	4.2	123.1	4.6	123.					

E-field (V/cm)	43.2 ± 2.5	52.6 ± 2.9	64.8 ± 3.7	79.8 ± 4.6	97.8 ± 5.6	119.6 ± 6.9	146.7 ± 8.3	180 ± 10	219 ± 13	268 ± 15	329 ± 19	405 ± 22	484 ± 28
energy bin #	$\langle E_{true} \rangle \pm$												
1	1.8	0.1	1.8	0.1	1.8	0.1	1.8	0.2	1.8	0.2	1.8	0.2	1.8
2	2.3	0.1	2.3	0.1	2.3	0.1	2.3	0.2	2.3	0.2	2.3	0.2	2.3
3	2.8	0.1	2.8	0.1	2.8	0.1	2.8	0.2	2.8	0.2	2.8	0.2	2.8
4	3.3	0.1	3.3	0.1	3.3	0.1	3.3	0.1	3.3	0.2	3.3	0.2	3.3
5	3.8	0.1	3.8	0.1	3.8	0.1	3.8	0.1	3.8	0.1	3.8	0.2	3.8
6	4.3	0.1	4.3	0.1	4.3	0.1	4.3	0.1	4.3	0.1	4.3	0.1	4.3
7	4.8	0.1	4.8	0.1	4.8	0.1	4.8	0.1	4.8	0.1	4.8	0.1	4.8
8	5.5	0.3	5.5	0.3	5.5	0.3	5.5	0.3	5.5	0.3	5.5	0.3	5.5
9	6.5	0.3	6.5	0.3	6.5	0.3	6.5	0.3	6.5	0.3	6.5	0.3	6.5
10	7.5	0.3	7.5	0.3	7.5	0.3	7.5	0.3	7.5	0.3	7.5	0.3	7.5
11	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5
12	9.4	0.3	9.4	0.3	9.4	0.3	9.5	0.3	9.5	0.3	9.5	0.3	9.5
13	10.4	0.3	10.4	0.3	10.4	0.3	10.4	0.3	10.4	0.3	10.4	0.3	10.4
14	11.4	0.3	11.4	0.3	11.4	0.3	11.4	0.3	11.4	0.3	11.4	0.3	11.4
15	12.4	0.3	12.4	0.3	12.4	0.3	12.4	0.3	12.4	0.3	12.4	0.3	12.4
16	13.4	0.3	13.4	0.3	13.4	0.3	13.4	0.3	13.4	0.3	13.4	0.3	13.4
17	14.4	0.3	14.4	0.3	14.4	0.3	14.4	0.3	14.4	0.3	14.4	0.3	14.4
18	15.4	0.3	15.4	0.3	15.4	0.3	15.4	0.3	15.4	0.3	15.4	0.3	15.4
19	16.4	0.3	16.4	0.3	16.4	0.3	16.4	0.3	16.4	0.3	16.3	0.3	16.3
20	17.4	0.3	17.3	0.3	17.4	0.3	17.4	0.3	17.3	0.3	17.3	0.3	17.3
21	18.4	0.3	18.3	0.3	18.3	0.3	18.3	0.3	18.3	0.3	18.3	0.3	18.3
22	19.3	0.3	19.3	0.3	19.3	0.3	19.3	0.3	19.3	0.4	19.3	0.4	19.3
23	20.3	0.3	20.3	0.3	20.3	0.4	20.3	0.4	20.3	0.4	20.3	0.4	20.3
24	21.3	0.3	21.3	0.3	21.3	0.4	21.3	0.4	21.3	0.4	21.3	0.4	21.2
25	22.3	0.4	22.3	0.4	22.3	0.4	22.3	0.4	22.3	0.4	22.2	0.4	22.2
26	23.3	0.4	23.3	0.4	23.3	0.4	23.3	0.4	23.2	0.4	23.2	0.4	23.2
27	24.3	0.4	24.3	0.4	24.3	0.4	24.2	0.4	24.2	0.4	24.2	0.4	24.2
28	25.3	0.4	25.3	0.4	25.3	0.4	25.2	0.4	25.2	0.4	25.2	0.4	25.2
29	26.3	0.4	26.3	0.4	26.3	0.4	26.2	0.4	26.2	0.4	26.2	0.4	26.1
30	27.3	0.4	27.2	0.4	27.2	0.4	27.2	0.4	27.2	0.4	27.2	0.5	27.1
31	28.3	0.4	28.2	0.4	28.2	0.4	28.2	0.4	28.2	0.4	28.1	0.5	28.1
32	29.2	0.4	29.2	0.4	29.2	0.4	29.2	0.4	29.2	0.5	29.1	0.5	29.1
33	30.2	0.4	30.2	0.4	30.2	0.4	30.2	0.5	30.1	0.5	30.1	0.5	30.1
34	31.2	0.4	31.2	0.4	31.2	0.4	31.1	0.5	31.1	0.5	31.1	0.5	31.0
35	32.2	0.4	32.2	0.4	32.2	0.5	32.1	0.5	32.1	0.5	32.1	0.5	32.0
36	33.2	0.4	33.2	0.4	33.2	0.5	33.1	0.5	33.1	0.5	33.1	0.5	33.0
37	34.2	0.4	34.2	0.4	34.1	0.5	34.1	0.5	34.1	0.5	34.0	0.6	34.0
38	35.2	0.4	35.2	0.5	35.1	0.5	35.1	0.5	35.1	0.5	35.0	0.6	34.9
39	36.2	0.4	36.1	0.5	36.1	0.5	36.1	0.5	36.0	0.5	36.0	0.6	35.9
40	37.2	0.5	37.1	0.5	37.1	0.5	37.0	0.5	37.0	0.6	37.0	0.6	36.9
41	38.1	0.5	38.1	0.5	38.1	0.5	38.0	0.5	38.0	0.6	38.0	0.6	37.9
42	39.1	0.5	39.1	0.5	39.1	0.5	39.0	0.6	39.0	0.6	38.9	0.6	38.9
43	40.1	0.5	40.1	0.5	40.1	0.5	40.0	0.6	40.0	0.6	39.9	0.7	39.9
44	41.1	0.5	41.1	0.5	41.0	0.6	41.0	0.6	41.0	0.6	40.9	0.7	40.8
45	42.1	0.5	42.1	0.5	42.0	0.6	42.0	0.6	42.0	0.6	41.9	0.7	41.8
46	43.1	0.5	43.1	0.5	43.0	0.6	43.0	0.6	42.9	0.7	42.9	0.7	42.8
47	44.1	0.5	44.0	0.6	44.0	0.6	44.0	0.6	43.9	0.7	43.8	0.7	43.8
48	45.1	0.5	45.0	0.6	45.0	0.6	44.9	0.6	44.9	0.7	44.8	0.8	44.7
49	46.0	0.6	46.0	0.6	46.0	0.6	45.9	0.6	45.9	0.7	45.8	0.8	45.7
50	47.0	0.6	47.0	0.6	46.9	0.6	46.9	0.7	46.8	0.7	46.8	0.8	46.7
51	48.0	0.6	48.0	0.6	47.9	0.6	47.9	0.7	47.8	0.8	47.7	0.8	47.6
52	49.0	0.6	49.0	0.6	48.9	0.7	48.9	0.7	48.8	0.8	48.7	0.8	48.6
53	50.5	0.8	50.4	0.8	50.4	0.8	50.4	0.9	50.3	1.0	50.2	1.0	50.1
54	52.4	0.8	52.4	0.8	52.4	0.9	52.3	0.9	52.3	1.0	52.2	1.0	52.1
55	54.4	0.8	54.4	0.9	54.3	0.9	54.3	0.9	54.2	1.0	54.1	1.1	54.0
56	56.4	0.9	56.3	0.9	56.3	0.9	56.2	1.0	56.2	1.0	56.1	1.1	56.0
57	58.4	0.9	58.3	0.9	58.3	0.9	58.2	1.0	58.1	1.1	58.0	1.2	57.9
58	60.3	0.9	60.3	0.9	60.3	1.0	60.2	1.0	60.1	1.1	60.0	1.2	59.9
59	62.3	0.9	62.3	1.0	62.2	1.1	62.1	1.1	62.1	1.2	61.9	1.2	61.7
60	64.3	1.0	64.2	1.0	64.2	1.0	64.1	1.1	64.0	1.2	63.9	1.3	63.6
61	66.2	1.0	66.2	1.0	66.0	1.1	66.0	1.1	66.0	1.2	65.8	1.3	65.7
62	68.2	1.0	68.2	1.1	68.1	1.1	68.0	1.2	67.9	1.2	67.8	1.3	67.6
63	70.2	1.0	70.1	1.1	70.1	1.1	69.9	1.2	69.9	1.3	69.8	1.4	69.7
64	72.1	1.1	72.1	1.1	72.0	1.1	71.9	1.2	71.9	1.3	71.7	1.4	71.6
65	74.1	1.1	74.0	1.1	74.0	1.2	73.9	1.3	73.8	1.4	73.7	1.5	73.5
66	76.0	1.1	76.0	1.2	76.0	1.2	75.8	1.3	75.8	1.4	75.6	1.5	75.5
67	78.0	1.2	78.0	1.2	77.9	1.3	77.8	1.4	77.7	1.5	77.6	1.6	77.5
68	80.5	1.4	80.4	1.4	80.4	1.5	80.2	1.6	80.1	1.7	79.9	1.9	79.8
69	83.4	1.4	83.3	1.5	83.3	1.5	83.2	1.6	83.0	1.8	82.9	1.9	82.8
70	86.3	1.5	86.3	1.6	86.2	1.6	86.1	1.7	85.9	1.8	85.7	1.9	85.5
71	89.2	1.6	89.2	1.7	89.1	1.7	88.9	1.8	88.7	2.0	88.6	2.2	88.4
72	92.1	1.7	92.0	1.8	91.9	1.9	91.7	2.1	91.6	2.2	91.6	2.3	91.5
73	96.0	2.2	95.9	2.3	95.8	2.3	95.7	2.4	95.6	2.5	95.4	2.7	95.2
74	100.8	2.3	100.6	2.5	100.6	2.5	100.5	2.6	100.3	2.7	100.1	2.9	99.9
75	105.6	2.5	105.4	2.7	105.3	2.8	105.2	2.8	105.1	2.9	104.8	3.2	104.6
76	110.3	2.8	110.1	2.9	109.9	3.1	109.8	3.2	109.4	3.5	109.3	3.6	109.1
77	114.9	3.1	114.9	3.1	114.5	3.5	114.3	3.6	114.1	3.7	113.8	4.1	113.5
78	119.5	3.4	119.6	3.3	119.0	3.9	118.9	4.0	118.8	4.0	118.7	4.1	118.6
79	124.0	3.8	124.1	3.8	123.4	4.4	123.2	4.5	123.1	4.6	122.3	5.2	121.7
80	128.5	4.6	128.3	4.7	127.7	5.2	127.4	5.5	127.2	5.6	127.0	5.5	126.9
81	135.0	5.2	133.6	5.3	134.0	5.8	133.4	6.0	133.0	6.1	131.9	6.1	132.0

Table A.2: Results for $\langle E_{true} \rangle = \langle N_\gamma \rangle / \langle N_e \rangle$ using the carbon-14, “dcm” corrected data. The error column shows the combination of the uncertainty due to bin width and de-smearing. The first column shows the index of the reconstructed energy bin in which the measurement was made.

E-field (V/cm)	43.2 ± 2.5	52.6 ± 2.9	64.8 ± 3.7	79.8 ± 4.6	97.8 ± 5.6	119.6 ± 6.9	146.7 ± 8.3	180 ± 10	219 ± 13	268 ± 15	329 ± 19	405 ± 22	484 ± 28	
energy bin #	$\langle E_{true} \rangle \pm$													
1	1.8	0.1	1.8	0.1	1.8	0.1	1.8	0.2	1.8	0.1	1.8	0.2	1.8	0.2
2	2.3	0.1	2.3	0.1	2.3	0.1	2.3	0.2	2.3	0.1	2.3	0.2	2.3	0.2
3	2.8	0.1	2.8	0.1	2.8	0.1	2.8	0.1	2.8	0.1	2.8	0.2	2.8	0.2
4	3.3	0.1	3.3	0.1	3.3	0.1	3.3	0.1	3.3	0.2	3.3	0.2	3.3	0.2
5	3.8	0.1	3.8	0.1	3.8	0.1	3.8	0.1	3.8	0.1	3.8	0.2	3.8	0.2
6	4.3	0.1	4.3	0.1	4.3	0.1	4.3	0.1	4.3	0.1	4.3	0.1	4.3	0.1
7	4.7	0.1	4.7	0.1	4.8	0.1	4.8	0.1	4.8	0.1	4.8	0.1	4.8	0.1
8	5.5	0.3	5.5	0.3	5.5	0.3	5.5	0.3	5.5	0.3	5.5	0.3	5.5	0.3
9	6.5	0.3	6.5	0.3	6.5	0.3	6.5	0.3	6.5	0.3	6.5	0.3	6.5	0.3
10	7.5	0.3	7.5	0.3	7.5	0.3	7.5	0.3	7.5	0.3	7.5	0.3	7.5	0.3
11	8.5	0.3	8.4	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3
12	9.4	0.3	9.4	0.3	9.4	0.3	9.4	0.3	9.5	0.3	9.4	0.3	9.4	0.3
13	10.4	0.3	10.4	0.3	10.4	0.3	10.4	0.3	10.4	0.3	10.4	0.3	10.4	0.3
14	11.4	0.3	11.4	0.3	11.4	0.3	11.4	0.3	11.4	0.3	11.4	0.3	11.4	0.3
15	12.4	0.3	12.4	0.3	12.4	0.3	12.4	0.3	12.4	0.3	12.4	0.3	12.4	0.3
16	13.4	0.3	13.4	0.3	13.4	0.3	13.4	0.3	13.4	0.3	13.4	0.3	13.4	0.3
17	14.4	0.3	14.4	0.3	14.4	0.3	14.4	0.3	14.4	0.3	14.4	0.3	14.4	0.3
18	15.4	0.3	15.4	0.3	15.4	0.3	15.4	0.3	15.4	0.3	15.4	0.3	15.4	0.3
19	16.4	0.3	16.4	0.3	16.4	0.3	16.4	0.3	16.4	0.3	16.4	0.3	16.4	0.3
20	17.4	0.3	17.3	0.3	17.3	0.3	17.3	0.3	17.3	0.3	17.3	0.3	17.3	0.3
21	18.3	0.3	18.3	0.3	18.3	0.3	18.3	0.3	18.3	0.3	18.3	0.4	18.3	0.4
22	19.3	0.3	19.3	0.3	19.3	0.3	19.3	0.3	19.3	0.4	19.3	0.4	19.3	0.4
23	20.3	0.3	20.3	0.4	20.3	0.4	20.3	0.4	20.3	0.4	20.3	0.4	20.3	0.4
24	21.3	0.4	21.3	0.4	21.3	0.4	21.3	0.4	21.3	0.4	21.3	0.4	21.3	0.4
25	22.3	0.4	22.3	0.4	22.3	0.4	22.3	0.4	22.3	0.4	22.2	0.4	22.2	0.4
26	23.3	0.4	23.3	0.4	23.3	0.4	23.3	0.4	23.2	0.4	23.2	0.4	23.2	0.4
27	24.3	0.4	24.3	0.4	24.2	0.4	24.2	0.4	24.2	0.4	24.2	0.4	24.2	0.4
28	25.3	0.4	25.2	0.4	25.2	0.4	25.2	0.4	25.2	0.4	25.2	0.4	25.2	0.4
29	26.3	0.4	26.2	0.4	26.2	0.4	26.2	0.4	26.2	0.4	26.2	0.4	26.2	0.4
30	27.2	0.4	27.2	0.4	27.2	0.4	27.2	0.4	27.2	0.4	27.2	0.5	27.2	0.5
31	28.2	0.4	28.2	0.4	28.2	0.4	28.2	0.4	28.2	0.4	28.1	0.5	28.1	0.5
32	29.2	0.4	29.2	0.4	29.2	0.4	29.2	0.4	29.2	0.5	29.1	0.5	29.1	0.5
33	30.2	0.4	30.2	0.4	30.2	0.5	30.2	0.5	30.1	0.5	30.1	0.5	30.1	0.5
34	31.2	0.4	31.2	0.5	31.1	0.5	31.1	0.5	31.1	0.5	31.1	0.5	31.1	0.5
35	32.2	0.4	32.2	0.5	32.1	0.5	32.1	0.5	32.1	0.5	32.1	0.5	32.1	0.5
36	33.2	0.5	33.1	0.5	33.1	0.5	33.1	0.5	33.1	0.5	33.0	0.6	33.0	0.6
37	34.1	0.5	34.1	0.5	34.1	0.5	34.1	0.5	34.0	0.6	34.0	0.6	34.0	0.6
38	35.1	0.5	35.1	0.5	35.1	0.5	35.1	0.5	35.0	0.6	35.0	0.6	35.0	0.6
39	36.1	0.5	36.1	0.5	36.1	0.5	36.1	0.6	36.0	0.6	36.0	0.6	36.0	0.6
40	37.1	0.5	37.1	0.5	37.1	0.5	37.1	0.6	37.0	0.6	37.0	0.6	36.9	0.6
41	38.1	0.5	38.1	0.5	38.1	0.5	38.0	0.6	38.0	0.6	37.9	0.6	37.9	0.7
42	39.1	0.5	39.1	0.5	39.0	0.6	39.0	0.6	38.9	0.6	38.9	0.7	38.9	0.7
43	40.1	0.5	40.1	0.5	40.1	0.6	40.0	0.6	40.0	0.6	39.9	0.7	39.9	0.7
44	41.1	0.5	41.0	0.6	41.0	0.6	41.0	0.6	40.9	0.6	40.9	0.7	40.9	0.7
45	42.0	0.6	42.0	0.6	42.0	0.6	42.0	0.6	41.9	0.7	41.9	0.7	41.8	0.7
46	43.0	0.6	43.0	0.6	43.0	0.6	43.0	0.6	42.9	0.7	42.8	0.7	42.8	0.8
47	44.0	0.6	44.0	0.6	44.0	0.6	43.9	0.6	43.9	0.7	43.8	0.7	43.8	0.8
48	45.0	0.6	45.0	0.6	45.0	0.6	44.9	0.6	44.9	0.7	44.8	0.8	44.8	0.8
49	46.0	0.6	46.0	0.6	46.0	0.6	45.9	0.7	45.9	0.7	45.8	0.8	45.7	0.8
50	47.0	0.6	47.0	0.6	46.9	0.6	46.9	0.7	46.9	0.7	46.8	0.8	46.7	0.8
51	48.0	0.6	47.9	0.6	47.9	0.7	47.9	0.7	47.8	0.8	47.7	0.8	47.7	0.9
52	48.9	0.6	48.9	0.7	48.9	0.7	48.9	0.7	48.8	0.8	48.7	0.9	48.6	0.9
53	50.4	0.8	50.4	0.9	50.4	0.9	50.3	0.9	50.3	1.0	50.2	1.0	50.1	1.1
54	52.4	0.8	52.4	0.9	52.3	0.9	52.3	0.9	52.3	1.0	52.2	1.0	52.1	1.1
55	54.4	0.9	54.3	0.9	54.3	0.9	54.3	0.9	54.2	1.0	54.2	1.0	54.0	1.2
56	56.3	0.9	56.3	0.9	56.3	1.0	56.3	0.9	56.2	1.0	56.1	1.1	56.0	1.2
57	58.3	0.9	58.3	1.0	58.2	1.0	58.2	1.0	58.1	1.1	58.0	1.2	57.9	1.3
58	60.3	0.9	60.2	1.0	60.2	1.0	60.2	1.0	60.1	1.1	60.1	1.2	59.9	1.3
59	62.3	1.0	62.2	1.0	62.1	1.1	62.1	1.1	62.0	1.2	61.9	1.3	61.8	1.4
60	64.2	1.0	64.1	1.1	64.1	1.1	64.1	1.1	64.0	1.2	63.9	1.3	63.7	1.4
61	66.2	1.0	66.1	1.1	66.1	1.1	66.0	1.1	65.9	1.2	65.8	1.3	65.7	1.5
62	68.2	1.0	68.1	1.1	68.0	1.2	68.0	1.2	67.9	1.3	67.9	1.4	67.7	1.5
63	70.1	1.1	70.0	1.1	70.0	1.2	69.9	1.2	69.8	1.3	69.8	1.4	69.6	1.6
64	72.1	1.1	72.0	1.2	71.9	1.2	71.9	1.3	71.8	1.4	71.7	1.5	71.5	1.6
65	74.0	1.2	74.0	1.2	73.9	1.3	73.8	1.3	73.7	1.4	73.7	1.5	73.6	1.7
66	76.0	1.2	75.9	1.2	75.9	1.3	75.8	1.4	75.7	1.5	75.6	1.6	75.5	1.8
67	77.9	1.3	77.9	1.3	77.7	1.4	77.7	1.5	77.6	1.5	77.5	1.6	77.3	1.8
68	80.3	1.5	80.3	1.5	80.3	1.6	80.1	1.7	80.0	1.7	79.9	1.9	79.7	2.0
69	83.3	1.5	83.3	1.5	83.2	1.6	83.0	1.8	82.9	1.8	82.8	1.9	82.8	2.0
70	86.2	1.6	86.2	1.6	86.1	1.7	86.0	1.8	85.9	1.9	85.7	2.0	85.6	2.1
71	89.1	1.7	89.1	1.7	89.0	1.7	88.9	1.9	88.8	2.0	88.7	2.1	88.5	2.4
72	92.0	1.8	92.0	1.8	91.8	2.0	91.7	2.1	91.6	2.2	91.5	2.3	91.2	2.5
73	95.9	2.2	95.9	2.2	95.8	2.3	95.6	2.4	95.5	2.5	95.4	2.7	95.0	3.0
74	100.8	2.4	100.7	2.4	100.6	2.5	100.5	2.6	100.3	2.7	100.1	2.9	99.7	3.3
75	105.5	2.6	105.5	2.6	105.4	2.7	105.2	2.8	105.1	2.9	104.8	3.1	104.7	3.2
76	110.2	2.8	110.1	2.9	110.0	3.0	109.9	3.1	109.7	3.2	109.5	3.4	108.9	4.0
77	114.8	3.2	114.7	3.3	114.6	3.4	114.5	3.4	114.3	3.6	114.2	3.7	113.8	4.0
78	119.4	3.6	119.2	3.7	119.1	3.8	119.0	3.9	118.8	4.1	118.7	4.1	118.2	4.5
79	124.0	3.9	123.5	4.2	123.5	4.3	123.3	4.4	123.					

A.2 Carbon-14 $\langle \rho \rangle$

E-field (V/cm)	43.2 ± 2.5			52.6 ± 2.9			64.8 ± 3.7			79.8 ± 4.6			97.8 ± 5.6			119.6 ± 6.9			146.7 ± 8.3			180 ± 10			219 ± 13			268 ± 15			329 ± 19			405 ± 22			484 ± 28		
energy bin #	$\langle \rho \rangle$	stat.	syst.	$\langle \rho \rangle$	stat.	syst.	$\langle \rho \rangle$	stat.	syst.																														
1	0.48	0.06	0.06	0.43	0.02	0.05	0.44	0.02	0.06	0.3	0.1	0.0	0.45	0.01	0.07	0.38	0.04	0.06	0.43	0.02	0.07	0.39	0.02	0.05	0.38	0.04	0.06	0.40	0.03	0.06	0.40	0.02	0.05	0.35	0.03	0.05	0.35	0.04	0.05
2	0.61	0.02	0.08	0.61	0.02	0.08	0.62	0.03	0.08	0.61	0.02	0.08	0.60	0.02	0.10	0.61	0.01	0.09	0.56	0.02	0.09	0.52	0.01	0.06	0.54	0.02	0.09	0.56	0.01	0.08	0.50	0.02	0.07	0.52	0.02	0.07	0.51	0.02	0.07
3	0.81	0.02	0.08	0.78	0.02	0.07	0.75	0.02	0.07	0.76	0.02	0.07	0.72	0.02	0.07	0.73	0.01	0.08	0.69	0.02	0.06	0.67	0.02	0.07	0.72	0.02	0.07	0.70	0.01	0.09	0.65	0.03	0.07	0.64	0.01	0.06	0.67	0.02	0.07
4	0.92	0.02	0.07	0.87	0.03	0.07	0.91	0.02	0.06	0.84	0.01	0.06	0.85	0.02	0.06	0.79	0.02	0.06	0.83	0.02	0.06	0.82	0.02	0.06	0.79	0.02	0.06	0.78	0.02	0.07	0.78	0.01	0.06	0.77	0.01	0.06	0.75	0.02	0.06
5	1.10	0.03	0.07	1.04	0.02	0.07	0.99	0.03	0.06	0.93	0.02	0.06	0.96	0.01	0.06	0.97	0.02	0.06	0.91	0.02	0.06	0.87	0.02	0.06	0.87	0.02	0.06	0.86	0.02	0.06	0.88	0.01	0.06	0.88	0.01	0.06	0.82	0.02	0.06
6	1.23	0.02	0.07	1.13	0.02	0.07	1.09	0.02	0.06	1.09	0.02	0.06	1.05	0.03	0.06	1.09	0.02	0.06	0.95	0.03	0.06	0.96	0.02	0.06	1.02	0.02	0.06	0.96	0.02	0.06	0.95	0.03	0.06	0.92	0.01	0.06	0.90	0.02	0.06
7	1.32	0.02	0.07	1.26	0.02	0.07	1.22	0.02	0.07	1.23	0.02	0.07	1.14	0.02	0.06	1.11	0.02	0.06	1.06	0.03	0.06	1.09	0.02	0.06	1.06	0.01	0.06	1.05	0.02	0.06	1.00	0.02	0.06	0.99	0.02	0.06	0.98	0.02	0.06
8	1.42	0.02	0.07	1.39	0.02	0.07	1.32	0.02	0.07	1.32	0.02	0.07	1.30	0.01	0.07	1.23	0.02	0.07	1.22	0.01	0.07	1.17	0.02	0.07	1.13	0.02	0.06	1.14	0.01	0.06	1.10	0.01	0.07	1.055	0.010	0.060	1.03	0.01	0.06
9	1.55	0.02	0.08	1.54	0.02	0.08	1.47	0.02	0.08	1.40	0.02	0.07	1.42	0.01	0.07	1.39	0.02	0.07	1.33	0.02	0.07	1.32	0.02	0.07	1.27	0.02	0.07	1.22	0.02	0.07	1.18	0.02	0.07	1.16	0.01	0.06	1.12	0.01	0.06
10	1.75	0.03	0.09	1.69	0.02	0.08	1.57	0.02	0.08	1.57	0.02	0.08	1.48	0.01	0.08	1.47	0.02	0.08	1.41	0.01	0.07	1.40	0.02	0.07	1.31	0.02	0.07	1.30	0.01	0.07	1.27	0.02	0.07	1.21	0.01	0.06	1.20	0.01	0.06
11	1.86	0.02	0.09	1.83	0.02	0.09	1.72	0.02	0.09	1.67	0.02	0.08	1.60	0.02	0.08	1.55	0.02	0.08	1.48	0.02	0.07	1.44	0.02	0.07	1.37	0.02	0.07	1.36	0.02	0.07	1.31	0.02	0.07	1.25	0.02	0.06	1.28	0.01	0.07
12	2.02	0.02	0.10	1.96	0.02	0.10	1.84	0.02	0.09	1.78	0.02	0.09	1.69	0.02	0.08	1.62	0.02	0.08	1.57	0.02	0.08	1.53	0.02	0.08	1.48	0.02	0.07	1.42	0.02	0.07	1.37	0.02	0.07	1.31	0.01	0.07	1.31	0.02	0.07
13	2.14	0.02	0.11	2.04	0.02	0.10	1.91	0.02	0.09	1.84	0.02	0.09	1.79	0.02	0.09	1.75	0.01	0.09	1.63	0.02	0.08	1.60	0.01	0.08	1.48	0.03	0.07	1.44	0.02	0.07	1.44	0.02	0.08	1.36	0.01	0.07	1.31	0.01	0.07
14	2.28	0.02	0.11	2.15	0.02	0.11	2.05	0.02	0.10	1.94	0.01	0.10	1.87	0.01	0.09	1.80	0.02	0.09	1.71	0.02	0.09	1.63	0.02	0.08	1.58	0.02	0.08	1.50	0.01	0.08	1.48	0.02	0.08	1.42	0.01	0.07	1.36	0.01	0.07
15	2.33	0.03	0.12	2.26	0.02	0.11	2.14	0.02	0.10	2.07	0.02	0.10	1.95	0.02	0.10	1.85	0.02	0.09	1.73	0.02	0.09	1.70	0.02	0.08	1.63	0.01	0.08	1.54	0.01	0.08	1.52	0.02	0.08	1.43	0.01	0.07	1.37	0.01	0.07
16	2.45	0.03	0.12	2.37	0.02	0.12	2.25	0.02	0.11	2.10	0.02	0.10	1.99	0.02	0.10	1.90	0.02	0.10	1.80	0.01	0.09	1.70	0.02	0.08	1.67	0.02	0.08	1.60	0.01	0.08	1.55	0.02	0.08	1.45	0.01	0.07	1.38	0.02	0.07
17	2.60	0.04	0.13	2.46	0.02	0.12	2.30	0.02	0.11	2.19	0.01	0.11	2.05	0.02	0.10	2.00	0.02	0.10	1.89	0.02	0.09	1.79	0.02	0.09	1.69	0.02	0.08	1.63	0.02	0.08	1.55	0.01	0.08	1.48	0.01	0.07	1.42	0.01	0.07
18	2.72	0.03	0.13	2.56	0.01	0.12	2.36	0.02	0.12	2.26	0.02	0.11	2.10	0.02	0.10	2.01	0.01	0.10	1.93	0.02	0.10	1.85	0.02	0.09	1.76	0.02	0.09	1.63	0.02	0.08	1.59	0.02	0.08	1.49	0.01	0.08	1.44	0.01	0.07
19	2.74	0.02	0.13	2.61	0.02	0.13	2.40	0.02	0.12	2.34	0.02	0.11	2.18	0.01	0.11	2.05	0.02	0.10	1.96	0.01	0.10	1.86	0.01	0.09	1.77	0.02	0.09	1.64	0.02	0.08	1.57	0.02	0.08	1.53	0.01	0.08	1.45	0.01	0.07
20	2.83	0.02	0.14	2.66	0.02	0.13	2.57	0.01	0.13	2.38	0.02	0.12	2.24	0.01	0.11	2.11	0.02	0.11	1.98	0.02	0.10	1.94	0.02	0.10	1.80	0.02	0.09	1.71	0.02	0.09	1.64	0.02	0.08	1.51	0.01	0.08	1.44	0.02	0.07
21	2.92	0.03	0.14	2.80	0.02	0.14	2.61	0.02	0.13	2.41	0.02	0.12	2.26	0.02	0.11	2.17	0.02	0.11	2.06	0.02	0.10	1.94	0.02	0.10	1.85	0.02	0.09	1.73	0.02	0.09	1.69	0.02	0.09	1.552	0.010	0.080	1.46	0.01	0.08
22	2.97	0.02	0.14	2.82	0.02	0.14	2.63	0.02	0.13	2.49	0.02	0.12	2.33	0.02	0.11	2.23	0.02	0.11	2.09	0.01	0.10	1.98	0.02	0.10	1.87	0.01	0.09	1.78	0.01	0.09	1.67	0.02	0.09	1.55	0.01	0.08	1.47	0.01	0.08
23	3.03	0.03	0.15	2.94	0.02	0.14	2.71	0.02	0.13	2.52	0.03	0.12	2.42	0.02	0.12	2.24	0.02	0.11	2.12	0.02	0.11	1.99	0.02	0.10	1.87	0.02	0.09	1.78	0.02	0.09	1.68	0.01	0.09	1.58	0.01	0.08	1.44	0.02	0.07
24	3.15	0.03	0.15	2.98	0.02	0.15	2.79	0.02	0.14	2.63	0.02	0.13	2.44	0.02	0.12	2.27	0.02	0.11	2.17	0.02	0.11	2.04	0.02	0.10	1.85	0.02	0.09	1.81	0.01	0.09	1.72	0.02	0.09	1.56	0.01	0.08	1.49	0.01	0.08
25	3.25	0.03	0.16	3.02	0.03	0.15	2.83	0.02	0.14	2.59	0.02	0.13	2.48	0.02	0.12	2.31	0.03	0.11	2.19	0.02	0.11	2.06	0.02	0.10	1.95	0.02	0.10	1.80	0.02	0.09	1.73	0.02	0.09	1.59	0.01	0.08	1.46	0.01	0.08
26	3.25	0.03	0.16	3.11	0.02	0.15	2.88	0.02	0.14	2.68	0.02	0.13	2.52	0.02	0.12	2.33	0.02	0.12	2.17	0.01	0.11	2.05	0.02	0.10	1.90	0.02	0.10	1.82	0.02	0.09	1.73	0.02	0.09	1.60	0.01	0.08	1.48	0.01	0.08
27	3.40	0.02	0.17	3.11	0.02	0.15	2.93	0.02	0.14	2.72	0.02	0.13	2.53	0.02	0.12	2.39	0.02	0.12	2.21	0.02	0.11	2.07	0.02	0.10	1.97	0.02	0.10</												

E-field (V/cm)	43.2 ± 2.5			52.6 ± 2.9			64.8 ± 3.7			79.8 ± 4.6			97.8 ± 5.6			119.6 ± 6.9			146.7 ± 8.3			180 ± 10			219 ± 13			268 ± 15			329 ± 19			405 ± 22			484 ± 28		
energy bin #	$\langle \rho \rangle$	stat.	syst.																																				
31	3.62	0.03	0.18	3.28	0.02	0.16	3.08	0.03	0.15	2.86	0.02	0.14	2.67	0.02	0.13	2.43	0.02	0.12	2.36	0.02	0.12	2.13	0.02	0.11	1.99	0.02	0.10	1.89	0.02	0.10	1.77	0.02	0.09	1.59	0.01	0.08	1.47	0.01	0.08
32	3.70	0.05	0.18	3.38	0.02	0.17	3.16	0.02	0.16	2.91	0.02	0.14	2.66	0.03	0.13	2.47	0.02	0.13	2.34	0.02	0.12	2.17	0.02	0.11	2.03	0.02	0.10	1.85	0.03	0.10	1.72	0.02	0.09	1.60	0.01	0.09	1.42	0.02	0.08
33	3.67	0.04	0.18	3.42	0.02	0.17	3.19	0.03	0.16	2.91	0.02	0.14	2.72	0.02	0.14	2.61	0.01	0.13	2.28	0.02	0.12	2.09	0.02	0.11	2.04	0.02	0.11	1.83	0.02	0.10	1.72	0.02	0.09	1.59	0.01	0.08	1.42	0.02	0.08
34	3.68	0.03	0.18	3.47	0.02	0.17	3.19	0.03	0.16	2.93	0.02	0.15	2.68	0.03	0.13	2.52	0.02	0.13	2.34	0.02	0.12	2.15	0.02	0.11	1.99	0.02	0.10	1.83	0.02	0.10	1.76	0.02	0.09	1.55	0.02	0.08	1.42	0.01	0.08
35	3.74	0.03	0.18	3.47	0.04	0.17	3.25	0.02	0.16	2.99	0.02	0.15	2.75	0.02	0.14	2.47	0.03	0.13	2.37	0.02	0.12	2.18	0.02	0.11	2.03	0.02	0.10	1.85	0.02	0.10	1.76	0.02	0.09	1.57	0.02	0.08	1.44	0.02	0.08
36	3.74	0.05	0.18	3.53	0.03	0.17	3.28	0.04	0.16	2.95	0.03	0.15	2.74	0.02	0.14	2.57	0.03	0.13	2.36	0.02	0.12	2.21	0.01	0.11	2.03	0.02	0.10	1.86	0.02	0.10	1.72	0.02	0.09	1.55	0.01	0.08	1.44	0.01	0.08
37	3.82	0.03	0.18	3.52	0.03	0.17	3.26	0.02	0.16	2.99	0.02	0.15	2.78	0.02	0.14	2.57	0.03	0.13	2.35	0.02	0.12	2.20	0.03	0.11	1.97	0.02	0.10	1.84	0.02	0.10	1.73	0.02	0.09	1.59	0.01	0.09	1.40	0.02	0.08
38	3.76	0.05	0.18	3.60	0.02	0.18	3.28	0.03	0.16	3.02	0.03	0.15	2.83	0.02	0.14	2.61	0.02	0.13	2.34	0.02	0.12	2.19	0.02	0.11	2.04	0.02	0.11	1.82	0.02	0.10	1.69	0.02	0.09	1.53	0.01	0.08	1.35	0.02	0.07
39	3.98	0.03	0.19	3.60	0.03	0.18	3.30	0.03	0.16	3.04	0.02	0.15	2.78	0.02	0.14	2.59	0.03	0.13	2.44	0.02	0.13	2.18	0.03	0.11	2.03	0.02	0.11	1.88	0.02	0.10	1.75	0.02	0.09	1.52	0.02	0.08	1.38	0.01	0.08
40	3.88	0.04	0.19	3.69	0.03	0.18	3.36	0.03	0.17	3.07	0.02	0.15	2.80	0.02	0.14	2.61	0.03	0.13	2.40	0.03	0.12	2.23	0.02	0.12	2.03	0.02	0.11	1.89	0.02	0.10	1.74	0.02	0.09	1.53	0.01	0.08	1.39	0.02	0.08
41	3.95	0.05	0.19	3.74	0.03	0.19	3.35	0.03	0.16	3.05	0.02	0.15	2.82	0.02	0.14	2.63	0.03	0.14	2.38	0.02	0.12	2.17	0.02	0.11	2.03	0.02	0.11	1.90	0.02	0.10	1.70	0.02	0.09	1.510	0.010	0.083	1.42	0.02	0.08
42	3.96	0.05	0.19	3.73	0.03	0.19	3.43	0.02	0.17	3.05	0.02	0.15	2.81	0.02	0.14	2.55	0.02	0.13	2.43	0.02	0.13	2.19	0.02	0.12	1.99	0.02	0.11	1.85	0.02	0.10	1.67	0.02	0.09	1.54	0.02	0.08	1.36	0.02	0.08
43	4.01	0.04	0.20	3.69	0.03	0.18	3.42	0.03	0.17	3.13	0.02	0.16	2.75	0.03	0.14	2.58	0.02	0.13	2.41	0.03	0.12	2.15	0.02	0.11	2.01	0.02	0.11	1.81	0.02	0.10	1.62	0.04	0.09	1.51	0.01	0.08	1.36	0.02	0.08
44	4.13	0.03	0.20	3.83	0.03	0.19	3.43	0.03	0.17	3.18	0.02	0.16	2.88	0.02	0.15	2.61	0.03	0.13	2.32	0.02	0.12	2.24	0.02	0.12	2.00	0.02	0.11	1.88	0.02	0.10	1.65	0.02	0.09	1.47	0.01	0.08	1.36	0.02	0.08
45	4.13	0.03	0.20	3.74	0.03	0.19	3.40	0.03	0.17	3.08	0.03	0.16	2.81	0.03	0.14	2.67	0.03	0.14	2.42	0.02	0.13	2.17	0.03	0.11	2.00	0.02	0.11	1.90	0.02	0.10	1.60	0.02	0.09	1.50	0.01	0.08	1.33	0.02	0.07
46	4.13	0.05	0.21	3.83	0.03	0.19	3.45	0.03	0.17	3.14	0.03	0.16	2.90	0.02	0.15	2.60	0.02	0.13	2.36	0.02	0.12	2.17	0.03	0.11	2.03	0.02	0.11	1.86	0.02	0.10	1.66	0.02	0.09	1.49	0.01	0.08	1.34	0.01	0.08
47	4.17	0.04	0.21	3.85	0.05	0.19	3.45	0.04	0.17	3.23	0.02	0.16	2.87	0.02	0.15	2.64	0.03	0.14	2.32	0.03	0.12	2.14	0.03	0.11	2.03	0.02	0.11	1.78	0.02	0.10	1.66	0.02	0.09	1.46	0.02	0.08	1.32	0.01	0.08
48	4.20	0.04	0.21	3.75	0.05	0.19	3.48	0.04	0.18	3.17	0.04	0.16	2.87	0.02	0.15	2.61	0.02	0.13	2.40	0.03	0.12	2.18	0.02	0.12	2.00	0.03	0.11	1.71	0.02	0.09	1.63	0.02	0.09	1.42	0.02	0.08	1.29	0.02	0.07
49	4.14	0.06	0.21	3.83	0.04	0.19	3.45	0.03	0.18	3.18	0.03	0.16	2.88	0.03	0.15	2.59	0.02	0.13	2.37	0.02	0.12	2.11	0.03	0.11	1.97	0.02	0.11	1.80	0.02	0.10	1.62	0.02	0.09	1.38	0.02	0.08	1.29	0.01	0.07
50	4.09	0.04	0.20	3.94	0.03	0.20	3.47	0.03	0.18	3.15	0.03	0.16	2.90	0.02	0.15	2.60	0.03	0.13	2.36	0.03	0.12	2.19	0.03	0.12	1.95	0.02	0.11	1.77	0.02	0.10	1.55	0.03	0.09	1.40	0.02	0.08	1.25	0.02	0.07
51	4.20	0.07	0.21	3.87	0.04	0.19	3.49	0.04	0.18	3.16	0.04	0.16	2.84	0.02	0.15	2.54	0.03	0.13	2.38	0.02	0.12	2.10	0.03	0.11	1.95	0.02	0.11	1.78	0.02	0.10	1.61	0.02	0.09	1.43	0.01	0.08	1.23	0.02	0.07
52	4.13	0.06	0.21	3.85	0.04	0.19	3.52	0.04	0.18	3.18	0.03	0.16	2.95	0.03	0.15	2.61	0.02	0.14	2.34	0.02	0.12	2.13	0.04	0.11	1.97	0.02	0.11	1.74	0.02	0.10	1.61	0.03	0.09	1.39	0.02	0.08	1.21	0.02	0.07
53	4.15	0.04	0.21	3.86	0.03	0.19	3.51	0.03	0.18	3.18	0.03	0.16	2.85	0.02	0.15	2.57	0.02	0.13	2.31	0.02	0.12	2.16	0.01	0.12	1.92	0.02	0.11	1.77	0.02	0.10	1.58	0.01	0.09	1.37	0.01	0.08	1.22	0.01	0.07
54	4.20	0.03	0.21	3.81	0.03	0.19	3.56	0.03	0.18	3.16	0.02	0.16	2.80	0.02	0.15	2.62	0.02	0.14	2.32	0.02	0.13	2.12	0.02	0.11	1.90	0.02	0.10	1.68	0.02	0.09	1.54	0.02	0.09	1.32	0.01	0.08	1.203	0.010	0.070
55	4.29	0.05	0.22	3.83	0.03	0.19	3.44	0.02	0.17	3.17	0.02	0.16	2.84	0.02	0.15	2.55	0.02	0.14	2.31	0.02	0.13	2.09	0.01	0.11	1.89	0.02	0.10	1.70	0.01	0.10	1.51	0.02	0.09	1.30	0.01	0.08	1.19	0.01	0.07
56	4.26	0.04	0.21	3.93	0.03	0.20	3.51	0.02	0.18	3.16	0.02	0.16	2.79	0.03	0.15	2.55	0.02	0.14	2.27	0.02	0.12	2.05	0.01	0.11	1.84	0.01	0.10	1.65	0.02	0.09	1.48	0.02	0.09	1.29	0.01	0.07	1.13	0.01	0.07
57	4.22	0.04	0.21	3.88	0.03	0.20	3.47	0.02	0.18	3.14	0.03	0.16	2.79	0.02	0.15	2.54	0.02	0.14	2.28	0.02	0.13	2.04	0.02	0.11	1.83	0.01	0.10	1.56	0.03	0.09	1.46	0.01	0.08	1.30	0.01	0.08	1.13	0.01	0.07
58																																							

E-field (V/cm)	43.2 ± 2.5			52.6 ± 2.9			64.8 ± 3.7			79.8 ± 4.6			97.8 ± 5.6			119.6 ± 6.9			146.7 ± 8.3			180 ± 10			219 ± 13			268 ± 15			329 ± 19			405 ± 22			484 ± 28		
energy bin #	$\langle \rho \rangle$	stat.	syst.																																				
61	4.19	0.05	0.22	3.69	0.03	0.19	3.48	0.03	0.18	3.03	0.02	0.16	2.69	0.02	0.15	2.39	0.02	0.13	2.15	0.02	0.12	1.96	0.02	0.11	1.76	0.02	0.10	1.58	0.02	0.09	1.33	0.03	0.08	1.21	0.02	0.07	1.08	0.01	0.07
62	4.23	0.05	0.22	3.73	0.04	0.19	3.39	0.03	0.18	3.01	0.02	0.16	2.71	0.02	0.15	2.43	0.02	0.14	2.16	0.02	0.12	1.93	0.02	0.11	1.73	0.02	0.10	1.55	0.02	0.09	1.36	0.02	0.08	1.17	0.01	0.07	1.04	0.01	0.06
63	4.10	0.04	0.22	3.74	0.03	0.20	3.38	0.03	0.18	2.98	0.03	0.16	2.70	0.03	0.15	2.44	0.03	0.14	2.12	0.02	0.12	1.87	0.02	0.11	1.64	0.02	0.10	1.46	0.02	0.09	1.31	0.02	0.08	1.16	0.01	0.07	1.05	0.02	0.06
64	4.07	0.04	0.22	3.73	0.03	0.20	3.37	0.04	0.18	3.00	0.02	0.16	2.63	0.02	0.15	2.37	0.03	0.13	2.08	0.02	0.12	1.83	0.03	0.11	1.72	0.01	0.10	1.42	0.02	0.09	1.28	0.02	0.08	1.15	0.01	0.07	1.00	0.02	0.06
65	4.11	0.05	0.22	3.74	0.04	0.20	3.35	0.02	0.18	2.94	0.02	0.16	2.59	0.03	0.15	2.30	0.03	0.13	2.06	0.02	0.12	1.83	0.02	0.11	1.67	0.02	0.10	1.50	0.02	0.09	1.29	0.02	0.08	1.13	0.01	0.07	0.96	0.02	0.06
66	4.02	0.06	0.21	3.73	0.02	0.20	3.27	0.03	0.18	2.90	0.03	0.16	2.50	0.03	0.14	2.27	0.03	0.13	2.04	0.02	0.12	1.81	0.02	0.11	1.63	0.02	0.10	1.42	0.02	0.09	1.29	0.02	0.08	1.10	0.01	0.07	1.00	0.01	0.06
67	4.11	0.06	0.22	3.71	0.04	0.20	3.27	0.03	0.18	2.95	0.02	0.16	2.55	0.03	0.15	2.27	0.02	0.13	2.02	0.02	0.12	1.82	0.02	0.11	1.58	0.03	0.10	1.43	0.03	0.09	1.33	0.01	0.08	1.11	0.01	0.07	0.91	0.02	0.06
68	4.13	0.04	0.22	3.62	0.03	0.20	3.17	0.03	0.17	2.81	0.02	0.16	2.53	0.02	0.15	2.21	0.02	0.13	2.02	0.02	0.12	1.78	0.02	0.11	1.60	0.01	0.10	1.38	0.01	0.09	1.24	0.02	0.08	1.06	0.01	0.07	0.98	0.01	0.06
69	4.00	0.03	0.22	3.55	0.03	0.20	3.11	0.03	0.17	2.83	0.02	0.16	2.43	0.03	0.14	2.21	0.02	0.13	1.90	0.02	0.11	1.71	0.02	0.11	1.54	0.02	0.10	1.39	0.02	0.09	1.22	0.01	0.08	1.061	0.009	0.069	0.93	0.01	0.06
70	3.90	0.05	0.21	3.44	0.03	0.20	3.13	0.03	0.18	2.78	0.03	0.16	2.40	0.03	0.14	2.14	0.03	0.13	1.87	0.02	0.11	1.69	0.02	0.11	1.51	0.02	0.10	1.32	0.02	0.08	1.19	0.01	0.08	1.02	0.01	0.07	0.91	0.01	0.06
71	3.90	0.05	0.21	3.46	0.03	0.20	3.04	0.03	0.17	2.75	0.03	0.16	2.37	0.03	0.14	2.12	0.02	0.13	1.83	0.03	0.11	1.64	0.03	0.10	1.44	0.02	0.09	1.28	0.02	0.08	1.15	0.02	0.08	1.02	0.01	0.07	0.90	0.01	0.06
72	3.81	0.06	0.21	3.36	0.03	0.19	2.99	0.04	0.18	2.68	0.02	0.16	2.31	0.03	0.14	2.08	0.03	0.13	1.84	0.02	0.12	1.69	0.02	0.11	1.46	0.02	0.10	1.27	0.01	0.08	1.13	0.01	0.08	0.96	0.01	0.06	0.81	0.02	0.06
73	3.68	0.07	0.21	3.34	0.02	0.20	3.00	0.03	0.18	2.52	0.02	0.15	2.35	0.01	0.14	2.01	0.01	0.13	1.79	0.02	0.12	1.64	0.01	0.11	1.44	0.01	0.10	1.27	0.01	0.09	1.12	0.01	0.08	0.992	0.008	0.067	0.880	0.008	0.063
74	3.59	0.04	0.21	3.20	0.04	0.19	2.90	0.02	0.18	2.54	0.04	0.16	2.20	0.02	0.14	1.97	0.02	0.13	1.75	0.02	0.12	1.57	0.02	0.11	1.37	0.01	0.10	1.14	0.03	0.08	1.11	0.01	0.08	0.958	0.009	0.067	0.84	0.01	0.06
75	3.56	0.05	0.22	3.13	0.03	0.19	2.81	0.03	0.18	2.49	0.02	0.17	2.15	0.02	0.14	1.93	0.02	0.13	1.69	0.02	0.12	1.50	0.02	0.11	1.36	0.02	0.10	1.17	0.02	0.09	1.02	0.01	0.08	0.94	0.01	0.07	0.863	0.007	0.067
76	3.52	0.04	0.23	3.08	0.04	0.20	2.77	0.03	0.18	2.39	0.04	0.17	2.17	0.02	0.15	1.91	0.02	0.13	1.68	0.02	0.13	1.44	0.02	0.11	1.30	0.02	0.10	1.16	0.01	0.09	1.07	0.01	0.09	0.91	0.01	0.07	0.81	0.01	0.07
77	3.32	0.05	0.22	2.99	0.04	0.21	2.63	0.05	0.18	2.36	0.03	0.18	2.05	0.02	0.16	1.86	0.02	0.16	1.60	0.03	0.13	1.40	0.02	0.11	1.22	0.02	0.10	1.15	0.02	0.10	1.00	0.03	0.09	0.90	0.01	0.08	0.75	0.02	0.06
78	3.29	0.07	0.23	2.91	0.05	0.22	2.63	0.04	0.20	2.28	0.04	0.19	2.02	0.02	0.17	1.77	0.04	0.15	1.60	0.02	0.14	1.39	0.02	0.13	1.25	0.02	0.12	1.08	0.02	0.10	1.02	0.01	0.10	0.89	0.01	0.09	0.78	0.02	0.07
79	3.14	0.09	0.24	3.01	0.05	0.26	2.63	0.04	0.24	2.29	0.05	0.20	2.10	0.03	0.20	1.76	0.03	0.18	1.54	0.02	0.15	1.43	0.03	0.14	1.19	0.03	0.13	1.09	0.04	0.12	1.00	0.02	0.11	0.86	0.01	0.09	0.81	0.01	0.09
80	3.0	0.1	0.3	2.85	0.08	0.29	2.57	0.05	0.31	2.26	0.05	0.26	2.05	0.03	0.24	1.78	0.04	0.22	1.43	0.05	0.17	1.36	0.03	0.17	1.18	0.04	0.16	1.09	0.02	0.14	1.00	0.02	0.13	0.83	0.02	0.11	0.78	0.01	0.10
81	3.07	0.08	0.27	2.78	0.08	0.29	2.50	0.07	0.30	2.26	0.04	0.26	1.87	0.07	0.22	1.62	0.05	0.20	1.55	0.06	0.19	1.29	0.06	0.16	1.27	0.03	0.17	1.05	0.04	0.13	0.93	0.03	0.12	0.84	0.02	0.11	0.77	0.03	0.10

Table A.6: Continued results for $\langle \rho \rangle = \langle N_\gamma \rangle / \langle N_e \rangle$ using the carbon-14, “gfdcm” corrected data. The “stat.” and “syst.” columns are the statistical and systematic errors. The first column shows the index of the reconstructed energy bin in which the measurement was made.

Table A.7: Results for $\langle \rho \rangle = \langle N_\gamma \rangle / \langle N_e \rangle$ using the carbon-14, “dcm” corrected data. The “stat.” and “syst.” columns are the statistical and systematic errors. The first column shows the index of the reconstructed energy bin in which the measurement was made.

E-field (V/cm)	43.2 ± 2.5			52.6 ± 2.9			64.8 ± 3.7			79.8 ± 4.6			97.8 ± 5.6			119.6 ± 6.9			146.7 ± 8.3			180 ± 10			219 ± 13			268 ± 15			329 ± 19			405 ± 22			484 ± 28		
energy bin #	$\langle \rho \rangle$	stat.	syst.	$\langle \rho \rangle$	stat.	syst.	$\langle \rho \rangle$	stat.	syst.	$\langle \rho \rangle$	stat.	syst.																											
31	3.99	0.03	0.20	3.57	0.03	0.18	3.37	0.03	0.17	3.13	0.03	0.16	2.92	0.02	0.15	2.69	0.02	0.14	2.58	0.02	0.13	2.38	0.02	0.12	2.19	0.03	0.11	2.05	0.02	0.11	1.94	0.01	0.10	1.77	0.01	0.10	1.64	0.02	0.09
32	4.03	0.04	0.20	3.71	0.04	0.18	3.47	0.03	0.18	3.18	0.03	0.16	2.94	0.03	0.15	2.73	0.02	0.14	2.57	0.03	0.13	2.33	0.02	0.12	2.22	0.02	0.12	2.04	0.03	0.11	1.91	0.02	0.10	1.79	0.01	0.10	1.57	0.03	0.09
33	3.98	0.05	0.19	3.74	0.03	0.18	3.48	0.02	0.18	3.18	0.03	0.16	2.99	0.02	0.15	2.87	0.02	0.15	2.55	0.02	0.13	2.33	0.02	0.12	2.24	0.03	0.12	2.03	0.03	0.11	1.89	0.02	0.10	1.77	0.01	0.10	1.54	0.02	0.08
34	4.04	0.03	0.20	3.76	0.02	0.19	3.50	0.04	0.18	3.23	0.03	0.16	2.93	0.03	0.15	2.76	0.02	0.14	2.56	0.03	0.13	2.37	0.02	0.12	2.21	0.03	0.12	2.04	0.02	0.11	1.97	0.02	0.11	1.74	0.02	0.09	1.60	0.01	0.09
35	4.07	0.05	0.20	3.84	0.03	0.19	3.56	0.03	0.18	3.28	0.02	0.17	3.00	0.02	0.15	2.71	0.03	0.14	2.61	0.02	0.14	2.37	0.02	0.12	2.23	0.02	0.12	2.04	0.02	0.11	1.95	0.02	0.11	1.73	0.02	0.10	1.57	0.02	0.09
36	4.08	0.04	0.20	3.83	0.03	0.19	3.55	0.04	0.18	3.22	0.03	0.16	3.01	0.02	0.15	2.85	0.03	0.15	2.60	0.03	0.14	2.45	0.02	0.13	2.22	0.03	0.12	2.01	0.03	0.11	1.88	0.01	0.10	1.77	0.01	0.10	1.60	0.01	0.09
37	4.15	0.03	0.21	3.87	0.02	0.19	3.54	0.03	0.18	3.29	0.03	0.17	3.02	0.02	0.15	2.83	0.03	0.15	2.59	0.02	0.14	2.39	0.02	0.13	2.21	0.02	0.12	2.05	0.02	0.11	1.90	0.03	0.10	1.74	0.02	0.10	1.52	0.02	0.08
38	4.19	0.04	0.21	3.96	0.02	0.20	3.60	0.02	0.18	3.34	0.03	0.17	3.10	0.02	0.16	2.83	0.03	0.15	2.58	0.02	0.14	2.42	0.02	0.13	2.22	0.02	0.12	2.02	0.02	0.11	1.88	0.02	0.10	1.68	0.02	0.09	1.49	0.02	0.08
39	4.31	0.05	0.21	3.94	0.04	0.20	3.62	0.03	0.18	3.29	0.02	0.17	3.05	0.02	0.16	2.79	0.04	0.14	2.68	0.02	0.14	2.42	0.02	0.13	2.24	0.02	0.12	2.03	0.02	0.11	1.89	0.02	0.10	1.72	0.01	0.10	1.56	0.02	0.09
40	4.27	0.04	0.21	4.00	0.04	0.20	3.66	0.03	0.18	3.32	0.03	0.17	3.07	0.02	0.16	2.88	0.02	0.15	2.65	0.02	0.14	2.44	0.02	0.13	2.24	0.02	0.12	2.10	0.02	0.11	1.92	0.02	0.10	1.69	0.02	0.09	1.53	0.02	0.09
41	4.33	0.04	0.22	4.07	0.04	0.20	3.69	0.04	0.19	3.39	0.03	0.17	3.07	0.03	0.16	2.85	0.03	0.15	2.63	0.02	0.14	2.36	0.02	0.13	2.24	0.02	0.12	2.05	0.03	0.11	1.84	0.02	0.10	1.67	0.01	0.09	1.55	0.02	0.09
42	4.34	0.04	0.22	4.07	0.03	0.20	3.79	0.03	0.19	3.35	0.05	0.17	3.09	0.03	0.16	2.84	0.02	0.15	2.62	0.02	0.14	2.43	0.03	0.13	2.20	0.02	0.12	2.05	0.03	0.11	1.85	0.03	0.10	1.70	0.02	0.10	1.53	0.02	0.09
43	4.42	0.05	0.22	4.07	0.03	0.20	3.70	0.03	0.19	3.38	0.03	0.17	3.05	0.03	0.16	2.83	0.03	0.15	2.66	0.03	0.14	2.35	0.03	0.12	2.23	0.02	0.12	1.97	0.03	0.11	1.81	0.03	0.10	1.66	0.02	0.09	1.47	0.02	0.08
44	4.45	0.06	0.22	4.13	0.04	0.21	3.75	0.03	0.19	3.48	0.04	0.18	3.14	0.02	0.16	2.87	0.03	0.15	2.56	0.02	0.14	2.46	0.03	0.13	2.22	0.02	0.12	2.07	0.02	0.11	1.83	0.02	0.10	1.64	0.02	0.09	1.52	0.02	0.09
45	4.54	0.05	0.23	4.11	0.03	0.21	3.72	0.02	0.19	3.40	0.03	0.17	3.05	0.04	0.16	2.93	0.02	0.15	2.63	0.02	0.14	2.40	0.03	0.13	2.20	0.02	0.12	2.06	0.02	0.11	1.78	0.02	0.10	1.65	0.01	0.09	1.46	0.02	0.08
46	4.51	0.06	0.22	4.21	0.04	0.21	3.78	0.04	0.19	3.44	0.03	0.18	3.16	0.04	0.16	2.85	0.02	0.15	2.57	0.02	0.14	2.36	0.02	0.13	2.24	0.02	0.12	2.04	0.02	0.11	1.80	0.02	0.10	1.63	0.01	0.09	1.47	0.02	0.08
47	4.51	0.04	0.23	4.18	0.05	0.21	3.73	0.03	0.19	3.51	0.02	0.18	3.18	0.03	0.16	2.91	0.03	0.15	2.54	0.04	0.14	2.39	0.02	0.13	2.18	0.02	0.12	1.96	0.02	0.11	1.86	0.02	0.11	1.605	0.009	0.091	1.43	0.02	0.08
48	4.58	0.04	0.23	4.11	0.05	0.21	3.80	0.05	0.19	3.46	0.05	0.18	3.10	0.02	0.16	2.84	0.02	0.15	2.66	0.03	0.14	2.37	0.03	0.13	2.17	0.03	0.12	1.90	0.03	0.11	1.79	0.02	0.10	1.57	0.02	0.09	1.41	0.02	0.08
49	4.47	0.08	0.23	4.15	0.04	0.21	3.77	0.03	0.19	3.46	0.04	0.18	3.13	0.03	0.16	2.83	0.02	0.15	2.62	0.02	0.14	2.34	0.02	0.13	2.18	0.02	0.12	1.98	0.03	0.11	1.79	0.02	0.10	1.56	0.02	0.09	1.40	0.02	0.08
50	4.48	0.07	0.23	4.30	0.04	0.22	3.80	0.03	0.19	3.51	0.03	0.18	3.19	0.04	0.17	2.84	0.02	0.15	2.58	0.03	0.14	2.38	0.02	0.13	2.14	0.02	0.12	1.98	0.03	0.11	1.75	0.02	0.10	1.56	0.02	0.09	1.39	0.02	0.08
51	4.44	0.09	0.22	4.20	0.04	0.21	3.80	0.03	0.19	3.37	0.03	0.17	3.10	0.02	0.16	2.80	0.03	0.15	2.58	0.03	0.14	2.34	0.02	0.13	2.15	0.03	0.12	1.91	0.03	0.11	1.76	0.02	0.10	1.56	0.02	0.09	1.33	0.03	0.08
52	4.63	0.08	0.24	4.21	0.04	0.21	3.77	0.04	0.19	3.48	0.03	0.18	3.24	0.03	0.17	2.82	0.03	0.15	2.58	0.02	0.14	2.36	0.04	0.13	2.15	0.03	0.12	1.88	0.03	0.11	1.77	0.02	0.10	1.51	0.02	0.09	1.35	0.02	0.08
53	4.50	0.05	0.23	4.20	0.02	0.21	3.86	0.03	0.20	3.46	0.02	0.18	3.13	0.02	0.16	2.80	0.02	0.15	2.52	0.03	0.14	2.36	0.02	0.13	2.12	0.02	0.12	1.95	0.02	0.11	1.73	0.02	0.10	1.51	0.01	0.09	1.33	0.01	0.08
54	4.61	0.04	0.24	4.18	0.03	0.21	3.89	0.04	0.20	3.47	0.02	0.18	3.04	0.03	0.16	2.86	0.02	0.15	2.57	0.02	0.14	2.32	0.01	0.13	2.07	0.02	0.12	1.84	0.02	0.10	1.69	0.02	0.10	1.48	0.02	0.09	1.32	0.01	0.08
55	4.65	0.05	0.24	4.17	0.03	0.21	3.75	0.03	0.20	3.44	0.03	0.18	3.07	0.03	0.16	2.78	0.02	0.15	2.50	0.02	0.14	2.31	0.01	0.13	2.07	0.02	0.12	1.87	0.02	0.11	1.65	0.02	0.09	1.42	0.01	0.08	1.30	0.01	0.08
56	4.63	0.04	0.24	4.27	0.04	0.22	3.84	0.03	0.20	3.46	0.03	0.18	3.03	0.02	0.16	2.81	0.02	0.15	2.50	0.02	0.14	2.25	0.02	0.13	2.01	0.02	0.11	1.78	0.02	0.10	1.63	0.02	0.09	1.39	0.02	0.08	1.26	0.02	0.08
57	4.61	0.05	0.24	4.19	0.03	0.22	3.79	0.03	0.20	3.39	0.04	0.18	3.06	0.03	0.16	2.75	0.02	0.15	2.48	0.02	0.14	2.21	0.02	0.12	2.02	0.02</													

E-field (V/cm)	43.2 ± 2.5			52.6 ± 2.9			64.8 ± 3.7			79.8 ± 4.6			97.8 ± 5.6			119.6 ± 6.9			146.7 ± 8.3			180 ± 10			219 ± 13			268 ± 15			329 ± 19			405 ± 22			484 ± 28		
energy bin #	$\langle \rho \rangle$	stat.	syst.																																				
61	4.52	0.05	0.24	4.02	0.03	0.21	3.81	0.04	0.21	3.32	0.02	0.18	2.91	0.02	0.16	2.61	0.03	0.15	2.33	0.02	0.14	2.14	0.02	0.12	1.93	0.02	0.11	1.75	0.02	0.11	1.50	0.02	0.09	1.35	0.01	0.08	1.17	0.02	0.07
62	4.59	0.05	0.24	4.06	0.04	0.22	3.64	0.04	0.20	3.27	0.02	0.18	2.97	0.02	0.16	2.65	0.02	0.15	2.35	0.02	0.14	2.09	0.03	0.12	1.89	0.02	0.11	1.64	0.02	0.10	1.50	0.02	0.09	1.29	0.02	0.08	1.14	0.01	0.07
63	4.49	0.04	0.24	4.12	0.03	0.22	3.68	0.03	0.20	3.27	0.03	0.18	2.92	0.03	0.16	2.65	0.03	0.15	2.27	0.02	0.13	2.06	0.02	0.12	1.80	0.02	0.11	1.62	0.02	0.10	1.43	0.02	0.09	1.26	0.01	0.08	1.14	0.02	0.07
64	4.41	0.04	0.24	4.04	0.03	0.22	3.73	0.03	0.20	3.23	0.02	0.18	2.80	0.03	0.16	2.58	0.03	0.15	2.26	0.03	0.13	1.96	0.03	0.12	1.89	0.02	0.11	1.57	0.02	0.10	1.42	0.02	0.09	1.25	0.01	0.08	1.10	0.02	0.07
65	4.42	0.06	0.24	4.10	0.04	0.22	3.65	0.03	0.20	3.21	0.03	0.18	2.83	0.02	0.16	2.53	0.03	0.15	2.26	0.03	0.13	2.03	0.02	0.12	1.83	0.02	0.11	1.60	0.03	0.10	1.40	0.02	0.09	1.22	0.01	0.08	1.03	0.02	0.06
66	4.39	0.05	0.24	3.97	0.04	0.22	3.53	0.02	0.20	3.19	0.03	0.18	2.74	0.03	0.16	2.45	0.03	0.14	2.25	0.01	0.14	1.96	0.02	0.12	1.74	0.02	0.11	1.57	0.02	0.10	1.44	0.02	0.09	1.23	0.01	0.08	1.08	0.02	0.07
67	4.50	0.05	0.25	4.05	0.03	0.22	3.59	0.03	0.20	3.23	0.03	0.19	2.72	0.03	0.16	2.44	0.03	0.14	2.17	0.03	0.13	2.01	0.02	0.12	1.75	0.02	0.11	1.53	0.03	0.10	1.41	0.01	0.09	1.19	0.01	0.08	1.03	0.01	0.07
68	4.44	0.05	0.25	3.96	0.03	0.22	3.44	0.03	0.19	3.02	0.03	0.18	2.71	0.02	0.16	2.42	0.02	0.15	2.18	0.02	0.13	1.94	0.02	0.12	1.74	0.02	0.11	1.51	0.02	0.10	1.37	0.01	0.09	1.17	0.01	0.08	1.05	0.01	0.07
69	4.38	0.04	0.25	3.83	0.04	0.22	3.38	0.04	0.19	3.09	0.02	0.18	2.66	0.03	0.16	2.40	0.02	0.15	2.08	0.02	0.13	1.86	0.02	0.12	1.64	0.01	0.10	1.49	0.02	0.10	1.32	0.02	0.09	1.13	0.02	0.07	1.01	0.01	0.07
70	4.26	0.05	0.24	3.77	0.03	0.22	3.33	0.05	0.19	3.02	0.02	0.18	2.57	0.03	0.16	2.39	0.03	0.15	2.05	0.02	0.13	1.83	0.02	0.12	1.62	0.02	0.10	1.43	0.02	0.09	1.29	0.01	0.09	1.14	0.01	0.08	0.98	0.02	0.07
71	4.30	0.04	0.25	3.73	0.04	0.22	3.32	0.03	0.19	2.96	0.04	0.18	2.58	0.03	0.16	2.28	0.03	0.15	2.03	0.03	0.13	1.81	0.02	0.12	1.57	0.03	0.10	1.34	0.02	0.09	1.24	0.02	0.08	1.07	0.01	0.07	0.97	0.01	0.07
72	4.08	0.06	0.24	3.69	0.03	0.22	3.28	0.04	0.20	2.89	0.04	0.18	2.53	0.03	0.16	2.27	0.02	0.15	1.97	0.02	0.13	1.83	0.02	0.12	1.60	0.02	0.11	1.35	0.03	0.09	1.23	0.02	0.09	1.09	0.01	0.07	0.93	0.02	0.06
73	4.00	0.06	0.24	3.62	0.03	0.22	3.26	0.04	0.20	2.76	0.03	0.18	2.56	0.02	0.17	2.18	0.01	0.15	1.94	0.01	0.13	1.77	0.01	0.12	1.58	0.01	0.11	1.40	0.01	0.10	1.20	0.02	0.09	1.078	0.008	0.075	0.92	0.01	0.07
74	3.88	0.05	0.24	3.47	0.04	0.22	3.16	0.03	0.20	2.78	0.04	0.18	2.37	0.03	0.16	2.15	0.03	0.15	1.88	0.02	0.14	1.71	0.02	0.12	1.51	0.02	0.11	1.28	0.03	0.09	1.21	0.02	0.09	1.050	0.009	0.076	0.92	0.01	0.07
75	3.88	0.04	0.25	3.40	0.03	0.22	3.01	0.03	0.20	2.66	0.03	0.18	2.34	0.03	0.16	2.14	0.02	0.15	1.84	0.02	0.13	1.63	0.02	0.12	1.46	0.02	0.11	1.24	0.03	0.09	1.14	0.02	0.09	1.00	0.02	0.08	0.92	0.01	0.07
76	3.84	0.05	0.27	3.39	0.04	0.23	2.97	0.04	0.21	2.61	0.03	0.19	2.33	0.03	0.17	2.05	0.03	0.16	1.81	0.03	0.14	1.55	0.03	0.12	1.37	0.02	0.11	1.28	0.02	0.10	1.12	0.02	0.09	0.99	0.01	0.08	0.84	0.02	0.07
77	3.60	0.08	0.27	3.26	0.04	0.23	2.87	0.05	0.21	2.55	0.03	0.20	2.21	0.02	0.18	2.04	0.02	0.17	1.81	0.03	0.15	1.52	0.02	0.13	1.37	0.03	0.12	1.24	0.03	0.11	1.04	0.04	0.09	0.97	0.02	0.09	0.83	0.02	0.07
78	3.55	0.06	0.28	3.15	0.06	0.24	2.88	0.04	0.24	2.42	0.07	0.21	2.15	0.03	0.19	1.89	0.05	0.17	1.71	0.02	0.16	1.51	0.02	0.15	1.36	0.02	0.13	1.19	0.02	0.12	1.13	0.01	0.11	0.97	0.01	0.10	0.87	0.01	0.09
79	3.4	0.1	0.3	3.19	0.06	0.27	2.92	0.05	0.28	2.50	0.05	0.23	2.28	0.03	0.22	1.90	0.03	0.18	1.67	0.03	0.17	1.53	0.04	0.17	1.26	0.04	0.13	1.18	0.03	0.12	1.10	0.02	0.13	0.94	0.02	0.11	0.83	0.02	0.10
80	3.3	0.2	0.3	3.07	0.08	0.32	2.80	0.05	0.29	2.42	0.08	0.26	2.21	0.04	0.25	1.81	0.09	0.23	1.66	0.05	0.21	1.46	0.05	0.19	1.31	0.03	0.18	1.18	0.02	0.16	1.09	0.02	0.14	0.89	0.03	0.12	0.81	0.02	0.12
81	3.2	0.1	0.3	3.07	0.05	0.32	2.60	0.09	0.27	2.42	0.04	0.26	2.09	0.06	0.24	1.76	0.07	0.23	1.6	0.1	0.2	1.42	0.06	0.18	1.26	0.09	0.17	1.13	0.04	0.15	1.01	0.03	0.13	0.92	0.02	0.13	0.83	0.02	0.12

Table A.9: Continued results for $\langle \rho \rangle = \langle N_\gamma \rangle / \langle N_e \rangle$ using the carbon-14, “dcm” corrected data. The “stat.” and “syst.” columns are the statistical and systematic errors. The first column shows the index of the reconstructed energy bin in which the measurement was made.

E-field (V/cm)	43.2 ± 2.5			52.6 ± 2.9			64.8 ± 3.7			79.8 ± 4.6			97.8 ± 5.6			119.6 ± 6.9			146.7 ± 8.3			180 ± 10			219 ± 13			268 ± 15			329 ± 19			405 ± 22			484 ± 28		
energy bin #	$\langle \rho \rangle$	stat.	syst.																																				
1	0.55	0.03	0.07	0.50	0.02	0.06	0.48	0.03	0.06	0.46	0.04	0.06	0.50	0.01	0.07	0.45	0.02	0.06	0.47	0.02	0.06	0.43	0.02	0.07	0.40	0.05	0.06	0.48	0.02	0.07	0.44	0.03	0.08	0.44	0.03	0.06	0.48	0.02	0.08
2	0.68	0.02	0.08	0.67	0.02	0.09	0.68	0.02	0.08	0.69	0.02	0.08	0.68	0.02	0.09	0.69	0.01	0.09	0.61	0.03	0.08	0.56	0.02	0.09	0.63	0.02	0.09	0.61	0.02	0.09	0.58	0.02	0.11	0.63	0.02	0.09	0.67	0.02	0.11
3	0.86	0.02	0.07	0.80	0.02	0.06	0.84	0.02	0.08	0.82	0.02	0.08	0.80	0.02	0.08	0.78	0.02	0.08	0.78	0.02	0.08	0.76	0.02	0.09	0.79	0.02	0.08	0.74	0.02	0.07	0.73	0.02	0.09	0.75	0.01	0.10	0.80	0.02	0.10
4	0.94	0.03	0.06	0.94	0.03	0.07	1.00	0.02	0.08	0.93	0.02	0.07	0.89	0.03	0.07	0.88	0.02	0.07	0.92	0.02	0.08	0.92	0.02	0.08	0.88	0.02	0.07	0.85	0.02	0.07	0.86	0.02	0.07	0.89	0.02	0.08	0.87	0.02	0.08
5	1.16	0.03	0.07	1.10	0.02	0.07	1.04	0.03	0.07	1.04	0.03	0.07	1.04	0.02	0.06	1.08	0.02	0.07	0.98	0.02	0.07	0.97	0.02	0.07	0.97	0.02	0.07	0.91	0.02	0.06	0.98	0.01	0.07	0.96	0.02	0.07	0.99	0.02	0.07
6	1.25	0.02	0.07	1.19	0.03	0.07	1.20	0.02	0.07	1.20	0.02	0.07	1.10	0.05	0.06	1.15	0.02	0.07	1.08	0.02	0.07	1.06	0.02	0.07	1.09	0.02	0.07	1.06	0.02	0.07	1.03	0.03	0.07	1.04	0.01	0.07	1.01	0.02	0.07
7	1.35	0.03	0.07	1.33	0.02	0.08	1.29	0.03	0.07	1.30	0.02	0.07	1.25	0.02	0.07	1.19	0.02	0.07	1.19	0.03	0.07	1.16	0.03	0.07	1.13	0.02	0.07	1.13	0.02	0.06	1.11	0.02	0.07	1.13	0.02	0.07			
8	1.49	0.03	0.08	1.47	0.01	0.08	1.39	0.02	0.07	1.42	0.02	0.08	1.40	0.01	0.08	1.29	0.02	0.07	1.31	0.02	0.08	1.28	0.02	0.07	1.23	0.02	0.07	1.23	0.01	0.07	1.19	0.02	0.07	1.17	0.01	0.07	1.18	0.02	0.07
9	1.64	0.02	0.09	1.60	0.02	0.08	1.56	0.02	0.08	1.51	0.02	0.08	1.55	0.02	0.08	1.49	0.01	0.08	1.42	0.02	0.08	1.41	0.02	0.08	1.35	0.02	0.07	1.31	0.02	0.07	1.28	0.02	0.07	1.29	0.01	0.07	1.27	0.02	0.07
10	1.81	0.03	0.09	1.79	0.02	0.09	1.68	0.02	0.09	1.68	0.02	0.09	1.60	0.02	0.08	1.56	0.02	0.08	1.50	0.02	0.08	1.49	0.02	0.08	1.42	0.02	0.07	1.36	0.02	0.07	1.37	0.02	0.07	1.35	0.01	0.07	1.37	0.02	0.07
11	1.92	0.03	0.10	1.93	0.02	0.10	1.84	0.02	0.09	1.81	0.02	0.09	1.71	0.02	0.09	1.68	0.02	0.09	1.58	0.01	0.08	1.53	0.02	0.08	1.49	0.02	0.08	1.44	0.02	0.07	1.45	0.02	0.08	1.40	0.02	0.07	1.46	0.01	0.08
12	2.09	0.03	0.10	2.06	0.02	0.10	1.94	0.02	0.10	1.90	0.02	0.09	1.81	0.02	0.09	1.74	0.02	0.09	1.67	0.02	0.08	1.64	0.02	0.09	1.60	0.02	0.08	1.52	0.02	0.08	1.49	0.01	0.08	1.45	0.01	0.07	1.47	0.01	0.07
13	2.24	0.02	0.11	2.12	0.02	0.11	2.04	0.02	0.10	1.95	0.01	0.10	1.91	0.02	0.10	1.87	0.02	0.09	1.73	0.02	0.09	1.72	0.02	0.09	1.57	0.02	0.08	1.54	0.02	0.08	1.58	0.01	0.08	1.51	0.02	0.08	1.47	0.01	0.07
14	2.36	0.02	0.12	2.26	0.02	0.11	2.16	0.02	0.11	2.07	0.02	0.10	2.01	0.01	0.10	1.94	0.02	0.10	1.81	0.02	0.09	1.71	0.02	0.09	1.69	0.02	0.09	1.60	0.02	0.08	1.59	0.01	0.08	1.568	0.010	0.079	1.56	0.01	0.08
15	2.44	0.03	0.12	2.36	0.02	0.12	2.30	0.02	0.12	2.21	0.02	0.11	2.07	0.02	0.10	1.98	0.02	0.10	1.82	0.02	0.09	1.82	0.02	0.09	1.71	0.02	0.09	1.64	0.02	0.08	1.66	0.03	0.09	1.58	0.01	0.08	1.54	0.02	0.08
16	2.57	0.03	0.13	2.48	0.02	0.12	2.37	0.02	0.12	2.24	0.02	0.11	2.12	0.02	0.10	2.04	0.01	0.10	1.91	0.02	0.10	1.84	0.02	0.10	1.79	0.01	0.09	1.71	0.02	0.09	1.67	0.02	0.09	1.61	0.01	0.08	1.58	0.01	0.08
17	2.72	0.03	0.14	2.56	0.03	0.13	2.46	0.02	0.12	2.33	0.02	0.12	2.19	0.02	0.11	2.12	0.02	0.11	2.01	0.01	0.10	1.90	0.02	0.10	1.81	0.02	0.09	1.74	0.02	0.09	1.68	0.02	0.09	1.64	0.01	0.08	1.61	0.02	0.08
18	2.81	0.02	0.14	2.67	0.02	0.14	2.50	0.02	0.12	2.44	0.03	0.12	2.27	0.02	0.11	2.12	0.01	0.11	2.04	0.03	0.10	1.97	0.02	0.10	1.87	0.01	0.09	1.75	0.03	0.09	1.72	0.01	0.09	1.66	0.01	0.08	1.59	0.02	0.08
19	2.84	0.03	0.14	2.74	0.02	0.14	2.56	0.02	0.13	2.45	0.02	0.12	2.31	0.01	0.11	2.19	0.02	0.11	2.07	0.02	0.10	1.99	0.02	0.10	1.85	0.02	0.09	1.75	0.02	0.09	1.73	0.02	0.09	1.68	0.01	0.08	1.61	0.02	0.08
20	2.96	0.02	0.15	2.84	0.02	0.14	2.69	0.02	0.13	2.53	0.02	0.13	2.36	0.02	0.12	2.27	0.02	0.12	2.11	0.02	0.11	2.05	0.02	0.10	1.91	0.02	0.10	1.81	0.02	0.09	1.77	0.02	0.09	1.69	0.01	0.09	1.59	0.02	0.08
21	3.06	0.03	0.16	2.88	0.02	0.15	2.79	0.01	0.14	2.58	0.02	0.13	2.41	0.02	0.12	2.35	0.02	0.12	2.19	0.02	0.11	2.07	0.02	0.11	1.95	0.02	0.10	1.84	0.02	0.09	1.83	0.02	0.09	1.68	0.01	0.08	1.64	0.02	0.08
22	3.07	0.03	0.16	2.99	0.02	0.15	2.79	0.02	0.14	2.66	0.02	0.13	2.51	0.02	0.12	2.38	0.02	0.12	2.19	0.02	0.11	2.10	0.02	0.11	2.00	0.02	0.10	1.88	0.02	0.10	1.79	0.02	0.09	1.71	0.01	0.09	1.67	0.01	0.08
23	3.16	0.03	0.16	3.06	0.03	0.16	2.89	0.03	0.15	2.74	0.02	0.14	2.55	0.02	0.13	2.38	0.02	0.12	2.26	0.02	0.11	2.09	0.02	0.11	1.97	0.01	0.10	1.89	0.02	0.10	1.82	0.02	0.09	1.74	0.02	0.09	1.66	0.01	0.08
24	3.30	0.02	0.17	3.09	0.03	0.16	2.93	0.03	0.15	2.81	0.02	0.14	2.59	0.02	0.13	2.43	0.02	0.13	2.31	0.02	0.12	2.16	0.01	0.11	2.00	0.02	0.10	1.92	0.02	0.10	1.84	0.02	0.10	1.71	0.02	0.09	1.65	0.02	0.08
25	3.36	0.02	0.17	3.20	0.02	0.16	2.96	0.02	0.15	2.74	0.02	0.14	2.65	0.02	0.13	2.48	0.03	0.13	2.31	0.02	0.12	2.18	0.01	0.11	2.04	0.02	0.11	1.90	0.02	0.10	1.86	0.01	0.10	1.76	0.01	0.09	1.59	0.02	0.08
26	3.35	0.03	0.17	3.26	0.03	0.17	3.08	0.03	0.16	2.88	0.02	0.15	2.70	0.02	0.14	2.46	0.02	0.13	2.26	0.02	0.12	2.18	0.02	0.11	2.01	0.02	0.10	1.95	0.02	0.10	1.85	0.02	0.10	1.71	0.02	0.09	1.62	0.01	0.08
27	3.49	0.03	0.18	3.28	0.02	0.17	3.06	0.03	0.15	2.86	0.02	0.15	2.69	0.02	0.14	2.56	0.02	0.13	2.34	0.02	0.12	2.17	0.02	0.11	2.07	0.02	0.10	1.98	0.02	0.10	1.87	0.01	0.10	1.75	0.02	0.09	1.64	0.02	0.08
28	3.60	0.04	0.18	3.35																																			

E-field (V/cm)	43.2 ± 2.5			52.6 ± 2.9			64.8 ± 3.7			79.8 ± 4.6			97.8 ± 5.6			119.6 ± 6.9			146.7 ± 8.3			180 ± 10			219 ± 13			268 ± 15			329 ± 19			405 ± 22			484 ± 28		
energy bin #	$\langle \rho \rangle$	stat.	syst.																																				
31	3.76	0.03	0.19	3.44	0.03	0.17	3.29	0.03	0.17	3.02	0.02	0.15	2.84	0.02	0.15	2.59	0.02	0.13	2.45	0.02	0.13	2.23	0.02	0.12	2.07	0.02	0.11	1.99	0.02	0.11	1.87	0.02	0.10	1.75	0.01	0.09	1.61	0.02	0.08
32	3.77	0.03	0.19	3.52	0.04	0.18	3.31	0.03	0.17	3.08	0.02	0.16	2.84	0.02	0.15	2.65	0.02	0.14	2.44	0.03	0.13	2.26	0.02	0.12	2.18	0.02	0.11	1.97	0.02	0.11	1.87	0.02	0.10	1.74	0.02	0.09	1.58	0.02	0.08
33	3.81	0.04	0.20	3.59	0.03	0.18	3.31	0.04	0.17	3.10	0.03	0.16	2.91	0.02	0.15	2.75	0.02	0.14	2.42	0.02	0.13	2.24	0.02	0.12	2.15	0.02	0.11	1.96	0.02	0.10	1.81	0.02	0.10	1.75	0.01	0.09	1.59	0.02	0.08
34	3.85	0.03	0.20	3.61	0.02	0.18	3.38	0.02	0.17	3.11	0.02	0.16	2.85	0.02	0.15	2.64	0.02	0.14	2.44	0.02	0.13	2.29	0.03	0.12	2.05	0.03	0.11	1.95	0.02	0.10	1.93	0.02	0.10	1.70	0.01	0.09	1.56	0.02	0.08
35	3.82	0.04	0.20	3.61	0.03	0.18	3.42	0.03	0.17	3.16	0.02	0.16	2.93	0.01	0.15	2.65	0.03	0.14	2.49	0.02	0.13	2.23	0.02	0.12	2.16	0.02	0.11	1.93	0.02	0.10	1.83	0.02	0.10	1.71	0.02	0.09	1.59	0.02	0.09
36	3.83	0.05	0.20	3.69	0.03	0.19	3.42	0.03	0.17	3.16	0.03	0.16	2.90	0.02	0.15	2.71	0.02	0.14	2.52	0.02	0.13	2.35	0.02	0.13	2.11	0.03	0.11	2.00	0.02	0.11	1.85	0.02	0.10	1.73	0.01	0.09	1.60	0.01	0.09
37	4.01	0.03	0.20	3.67	0.03	0.18	3.43	0.02	0.17	3.15	0.03	0.16	2.91	0.03	0.15	2.71	0.02	0.14	2.48	0.02	0.13	2.27	0.03	0.12	2.11	0.02	0.11	1.93	0.02	0.10	1.84	0.02	0.10	1.73	0.01	0.09	1.53	0.02	0.08
38	3.90	0.05	0.20	3.70	0.03	0.19	3.44	0.04	0.17	3.24	0.02	0.17	2.97	0.02	0.15	2.73	0.03	0.14	2.49	0.02	0.13	2.29	0.02	0.12	2.14	0.02	0.11	1.92	0.03	0.10	1.83	0.02	0.10	1.65	0.02	0.09	1.49	0.02	0.08
39	4.09	0.04	0.21	3.74	0.03	0.19	3.52	0.03	0.18	3.20	0.02	0.16	2.94	0.02	0.15	2.69	0.04	0.14	2.54	0.03	0.13	2.33	0.02	0.13	2.14	0.02	0.12	1.98	0.01	0.11	1.83	0.02	0.10	1.70	0.01	0.09	1.54	0.02	0.08
40	4.07	0.04	0.20	3.86	0.03	0.19	3.47	0.03	0.18	3.22	0.02	0.17	2.98	0.03	0.15	2.78	0.02	0.15	2.54	0.03	0.13	2.33	0.02	0.13	2.14	0.02	0.12	2.00	0.02	0.11	1.83	0.02	0.10	1.65	0.02	0.09	1.54	0.02	0.08
41	4.03	0.03	0.20	3.87	0.03	0.19	3.56	0.03	0.18	3.27	0.02	0.17	2.96	0.03	0.15	2.76	0.02	0.15	2.55	0.02	0.13	2.25	0.02	0.12	2.14	0.02	0.12	1.96	0.02	0.11	1.80	0.02	0.10	1.65	0.01	0.09	1.56	0.02	0.09
42	4.12	0.04	0.21	3.89	0.02	0.20	3.59	0.02	0.18	3.27	0.03	0.17	2.99	0.02	0.15	2.70	0.02	0.14	2.51	0.03	0.13	2.31	0.02	0.13	2.09	0.02	0.11	1.98	0.02	0.11	1.77	0.02	0.10	1.67	0.02	0.09	1.53	0.02	0.08
43	4.18	0.03	0.21	3.91	0.03	0.20	3.62	0.03	0.18	3.30	0.03	0.17	2.96	0.02	0.15	2.74	0.02	0.15	2.53	0.02	0.13	2.27	0.02	0.12	2.14	0.03	0.12	1.90	0.03	0.11	1.79	0.02	0.10	1.64	0.02	0.09	1.49	0.02	0.08
44	4.23	0.04	0.22	3.88	0.04	0.20	3.61	0.03	0.18	3.32	0.02	0.17	2.95	0.03	0.15	2.83	0.02	0.15	2.46	0.02	0.13	2.35	0.02	0.13	2.11	0.02	0.12	1.95	0.02	0.11	1.76	0.02	0.10	1.63	0.01	0.09	1.53	0.02	0.09
45	4.26	0.05	0.22	4.04	0.02	0.21	3.60	0.03	0.18	3.30	0.05	0.17	2.99	0.04	0.15	2.77	0.02	0.15	2.52	0.02	0.13	2.29	0.03	0.12	2.09	0.02	0.11	1.99	0.02	0.11	1.72	0.02	0.10	1.61	0.01	0.09	1.48	0.02	0.08
46	4.33	0.05	0.23	3.93	0.03	0.20	3.60	0.03	0.19	3.36	0.02	0.17	3.02	0.04	0.16	2.79	0.02	0.15	2.49	0.03	0.13	2.30	0.02	0.12	2.15	0.02	0.12	1.95	0.02	0.11	1.75	0.02	0.10	1.61	0.01	0.09	1.49	0.02	0.08
47	4.29	0.05	0.22	4.01	0.03	0.21	3.62	0.03	0.19	3.37	0.03	0.17	3.07	0.02	0.16	2.75	0.03	0.15	2.43	0.02	0.13	2.26	0.03	0.12	2.08	0.03	0.12	1.82	0.02	0.10	1.78	0.01	0.10	1.58	0.01	0.09	1.43	0.02	0.08
48	4.32	0.04	0.23	4.00	0.04	0.21	3.61	0.04	0.19	3.43	0.03	0.18	3.03	0.02	0.16	2.78	0.03	0.15	2.55	0.03	0.14	2.24	0.03	0.12	2.11	0.03	0.12	1.87	0.02	0.11	1.74	0.02	0.10	1.49	0.02	0.08	1.42	0.01	0.08
49	4.11	0.08	0.21	4.00	0.03	0.21	3.67	0.03	0.19	3.29	0.04	0.17	2.99	0.04	0.16	2.74	0.02	0.14	2.47	0.02	0.13	2.28	0.03	0.12	2.07	0.02	0.11	1.89	0.03	0.11	1.71	0.02	0.10	1.55	0.02	0.09	1.40	0.02	0.08
50	4.32	0.05	0.22	4.09	0.05	0.21	3.68	0.02	0.19	3.34	0.03	0.17	3.06	0.03	0.16	2.72	0.03	0.14	2.46	0.03	0.13	2.24	0.03	0.12	2.06	0.02	0.11	1.86	0.02	0.10	1.68	0.02	0.10	1.56	0.02	0.09	1.40	0.02	0.08
51	4.26	0.06	0.22	4.07	0.04	0.21	3.67	0.04	0.19	3.36	0.03	0.17	3.06	0.03	0.16	2.68	0.03	0.14	2.47	0.02	0.13	2.25	0.03	0.13	2.05	0.02	0.11	1.87	0.02	0.10	1.76	0.01	0.10	1.51	0.02	0.08	1.36	0.03	0.08
52	4.30	0.05	0.22	4.01	0.03	0.21	3.64	0.04	0.19	3.32	0.03	0.17	3.06	0.03	0.16	2.75	0.03	0.15	2.47	0.02	0.13	2.23	0.03	0.13	2.07	0.03	0.12	1.80	0.03	0.10	1.71	0.02	0.10	1.51	0.03	0.09	1.32	0.02	0.07
53	4.28	0.04	0.22	4.01	0.02	0.21	3.69	0.03	0.20	3.34	0.02	0.17	3.00	0.03	0.16	2.71	0.02	0.15	2.44	0.02	0.13	2.26	0.01	0.13	2.00	0.01	0.11	1.85	0.03	0.11	1.68	0.01	0.10	1.50	0.01	0.08	1.35	0.01	0.08
54	4.29	0.05	0.23	3.96	0.03	0.21	3.73	0.03	0.20	3.37	0.02	0.18	2.96	0.02	0.16	2.73	0.02	0.15	2.43	0.02	0.13	2.22	0.01	0.12	1.99	0.02	0.11	1.81	0.01	0.10	1.61	0.01	0.09	1.45	0.01	0.08	1.30	0.02	0.07
55	4.40	0.04	0.23	4.07	0.03	0.22	3.67	0.03	0.20	3.33	0.02	0.18	2.98	0.02	0.16	2.73	0.03	0.15	2.40	0.02	0.13	2.20	0.01	0.12	2.00	0.01	0.11	1.77	0.02	0.10	1.59	0.02	0.09	1.38	0.01	0.08	1.30	0.02	0.08
56	4.44	0.04	0.24	4.03	0.04	0.21	3.66	0.03	0.20	3.35	0.03	0.18	2.94	0.03	0.16	2.69	0.02	0.15	2.40	0.02	0.13	2.15	0.02	0.12	1.92	0.02	0.11	1.72	0.01	0.10	1.56	0.02	0.09	1.39	0.02	0.08	1.25	0.02	0.07
57	4.35	0.04	0.23	4.06	0.03	0.22	3.66	0.03	0.20	3.32	0.02	0.18	2.93	0.03	0.16	2.65	0.02	0.15	2.39	0.02	0.13	2.10	0.02	0.12	1.91	0.02													

E-field (V/cm)	43.2 ± 2.5			52.6 ± 2.9			64.8 ± 3.7			79.8 ± 4.6			97.8 ± 5.6			119.6 ± 6.9			146.7 ± 8.3			180 ± 10			219 ± 13			268 ± 15			329 ± 19			405 ± 22			484 ± 28		
energy bin #	$\langle \rho \rangle$	stat.	syst.																																				
61	4.32	0.04	0.23	3.92	0.04	0.21	3.70	0.03	0.20	3.16	0.04	0.18	2.82	0.03	0.16	2.51	0.03	0.14	2.26	0.02	0.13	2.05	0.02	0.12	1.84	0.02	0.11	1.68	0.02	0.10	1.41	0.02	0.08	1.32	0.01	0.08	1.19	0.01	0.07
62	4.32	0.05	0.23	3.92	0.04	0.21	3.56	0.02	0.20	3.17	0.03	0.18	2.83	0.03	0.16	2.53	0.02	0.16	2.21	0.02	0.13	2.01	0.03	0.12	1.81	0.01	0.11	1.58	0.02	0.10	1.44	0.02	0.09	1.26	0.01	0.08	1.16	0.02	0.07
63	4.23	0.04	0.23	3.87	0.04	0.21	3.55	0.04	0.20	3.21	0.02	0.18	2.82	0.03	0.16	2.55	0.03	0.16	2.21	0.02	0.13	1.98	0.02	0.12	1.71	0.02	0.10	1.53	0.02	0.10	1.40	0.02	0.09	1.27	0.01	0.08	1.13	0.02	0.07
64	4.18	0.04	0.23	3.96	0.03	0.22	3.60	0.03	0.20	3.15	0.03	0.18	2.74	0.03	0.16	2.48	0.03	0.15	2.13	0.02	0.13	1.88	0.03	0.11	1.79	0.02	0.11	1.52	0.02	0.09	1.37	0.03	0.09	1.21	0.02	0.07	1.09	0.02	0.07
65	4.25	0.04	0.24	3.87	0.04	0.22	3.50	0.03	0.20	3.04	0.03	0.17	2.71	0.04	0.16	2.43	0.02	0.14	2.17	0.02	0.13	1.93	0.02	0.12	1.74	0.02	0.11	1.54	0.02	0.10	1.38	0.02	0.09	1.21	0.01	0.08	1.06	0.01	0.06
66	4.18	0.04	0.24	3.83	0.05	0.22	3.38	0.03	0.19	3.11	0.02	0.18	2.62	0.03	0.15	2.36	0.04	0.14	2.10	0.02	0.13	1.89	0.02	0.12	1.67	0.02	0.10	1.49	0.02	0.09	1.38	0.02	0.09	1.21	0.01	0.08	1.03	0.02	0.06
67	4.24	0.06	0.24	3.86	0.05	0.22	3.47	0.04	0.20	3.12	0.04	0.18	2.64	0.03	0.16	2.34	0.02	0.14	2.15	0.03	0.13	1.90	0.03	0.12	1.68	0.02	0.11	1.45	0.03	0.09	1.37	0.02	0.09	1.167	0.010	0.075	1.05	0.02	0.07
68	4.24	0.04	0.24	3.81	0.04	0.22	3.37	0.04	0.20	2.97	0.03	0.18	2.61	0.03	0.16	2.33	0.02	0.14	2.10	0.02	0.13	1.81	0.02	0.11	1.65	0.02	0.10	1.44	0.02	0.09	1.33	0.01	0.09	1.14	0.01	0.07	1.044	0.010	0.066
69	4.09	0.04	0.24	3.77	0.04	0.22	3.31	0.03	0.20	2.98	0.03	0.18	2.60	0.02	0.16	2.32	0.02	0.14	1.99	0.03	0.13	1.79	0.02	0.11	1.59	0.02	0.10	1.45	0.02	0.09	1.29	0.01	0.08	1.140	0.010	0.075	1.01	0.01	0.07
70	4.00	0.06	0.24	3.64	0.03	0.22	3.27	0.04	0.20	2.94	0.03	0.18	2.50	0.03	0.16	2.28	0.02	0.14	1.96	0.02	0.13	1.74	0.02	0.11	1.56	0.02	0.10	1.35	0.02	0.09	1.23	0.01	0.08	1.09	0.01	0.07	0.97	0.02	0.06
71	4.06	0.04	0.24	3.62	0.03	0.22	3.20	0.03	0.20	2.89	0.03	0.18	2.51	0.02	0.16	2.19	0.03	0.14	1.92	0.03	0.12	1.73	0.02	0.11	1.49	0.02	0.10	1.29	0.02	0.09	1.23	0.01	0.08	1.09	0.01	0.07	1.00	0.01	0.07
72	3.90	0.06	0.24	3.51	0.05	0.22	3.20	0.05	0.20	2.85	0.03	0.18	2.44	0.03	0.16	2.21	0.02	0.14	1.88	0.03	0.12	1.74	0.02	0.12	1.52	0.02	0.10	1.33	0.02	0.09	1.19	0.01	0.08	1.06	0.01	0.07	0.92	0.02	0.06
73	3.83	0.04	0.24	3.52	0.02	0.22	3.15	0.03	0.20	2.69	0.02	0.17	2.44	0.02	0.16	2.10	0.02	0.14	1.85	0.02	0.12	1.70	0.01	0.12	1.50	0.02	0.10	1.33	0.02	0.10	1.16	0.02	0.08	1.063	0.009	0.074	0.93	0.01	0.07
74	3.70	0.06	0.24	3.39	0.03	0.22	3.05	0.03	0.20	2.67	0.03	0.18	2.33	0.03	0.16	2.06	0.02	0.14	1.80	0.02	0.12	1.63	0.02	0.12	1.44	0.02	0.11	1.20	0.03	0.09	1.16	0.02	0.09	1.03	0.01	0.07	0.93	0.01	0.07
75	3.63	0.05	0.25	3.26	0.03	0.22	2.96	0.02	0.20	2.60	0.02	0.19	2.26	0.02	0.16	2.03	0.02	0.14	1.74	0.03	0.13	1.55	0.02	0.12	1.39	0.02	0.11	1.22	0.02	0.10	1.09	0.02	0.09	0.98	0.02	0.07	0.924	0.009	0.073
76	3.63	0.04	0.25	3.29	0.03	0.24	2.90	0.03	0.21	2.57	0.02	0.19	2.25	0.03	0.17	1.97	0.02	0.15	1.71	0.02	0.13	1.48	0.03	0.12	1.33	0.02	0.11	1.23	0.02	0.11	1.11	0.01	0.09	0.98	0.01	0.08	0.83	0.03	0.07
77	3.51	0.05	0.25	3.19	0.03	0.25	2.83	0.06	0.22	2.51	0.03	0.19	2.13	0.04	0.17	1.95	0.03	0.16	1.72	0.03	0.15	1.48	0.02	0.14	1.26	0.03	0.11	1.19	0.02	0.11	1.04	0.03	0.10	0.97	0.01	0.09	0.84	0.02	0.07
78	3.37	0.06	0.26	3.09	0.04	0.27	2.81	0.04	0.24	2.26	0.08	0.20	2.10	0.04	0.19	1.90	0.03	0.17	1.67	0.02	0.16	1.42	0.03	0.14	1.28	0.02	0.12	1.15	0.02	0.11	1.08	0.02	0.11	0.95	0.02	0.10	0.85	0.01	0.08
79	3.23	0.06	0.28	3.05	0.04	0.29	2.72	0.06	0.25	2.40	0.06	0.23	2.16	0.03	0.21	1.84	0.03	0.19	1.61	0.03	0.18	1.45	0.04	0.15	1.21	0.03	0.14	1.16	0.03	0.13	1.05	0.02	0.12	0.93	0.02	0.11	0.87	0.02	0.10
80	3.1	0.2	0.3	3.20	0.06	0.37	2.74	0.04	0.30	2.45	0.06	0.29	2.19	0.03	0.26	1.80	0.04	0.25	1.54	0.07	0.21	1.33	0.07	0.18	1.26	0.03	0.18	1.08	0.03	0.15	1.07	0.02	0.16	0.84	0.04	0.12	0.80	0.02	0.11
81	3.20	0.08	0.35	2.95	0.07	0.34	2.64	0.07	0.29	2.36	0.06	0.28	1.92	0.07	0.23	1.73	0.07	0.24	1.56	0.06	0.21	1.40	0.05	0.19	1.19	0.08	0.17	1.13	0.03	0.16	0.99	0.02	0.15	0.91	0.02	0.13	0.85	0.02	0.12

Table A.12: Continued results for $\langle \rho \rangle = \langle N_\gamma \rangle / \langle N_e \rangle$ using the carbon-14, “z” corrected data. The “stat.” and “syst.” columns are the statistical and systematic errors. The first column shows the index of the reconstructed energy bin in which the measurement was made.

A.3 Tritium $\langle E_{true} \rangle$

E-field (V/cm)	43.2 ± 2.5	52.6 ± 2.9	64.8 ± 3.7	79.8 ± 4.6	97.8 ± 5.6	119.6 ± 6.9	146.7 ± 8.3	180 ± 10	219 ± 13	268 ± 15	329 ± 19	405 ± 22	484 ± 28	
energy bin #	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm
1	1.12	0.06	1.12	0.06	1.11	0.06	1.11	0.06	1.11	0.06	1.11	0.06	1.12	0.06
2	1.33	0.07	1.32	0.06	1.32	0.07	1.32	0.06	1.32	0.06	1.32	0.06	1.32	0.06
3	1.53	0.07	1.53	0.06	1.53	0.07	1.53	0.07	1.53	0.07	1.53	0.07	1.52	0.07
4	1.74	0.07	1.73	0.07	1.74	0.07	1.73	0.07	1.74	0.07	1.73	0.07	1.73	0.07
5	1.93	0.07	1.93	0.07	1.93	0.07	1.94	0.07	1.93	0.07	1.94	0.07	1.94	0.07
6	2.13	0.07	2.13	0.07	2.13	0.07	2.13	0.07	2.14	0.07	2.14	0.07	2.14	0.07
7	2.33	0.07	2.33	0.06	2.33	0.07	2.33	0.07	2.34	0.07	2.34	0.07	2.34	0.07
8	2.52	0.06	2.52	0.06	2.52	0.07	2.53	0.07	2.53	0.07	2.54	0.07	2.54	0.07
9	2.72	0.06	2.72	0.06	2.72	0.06	2.73	0.06	2.73	0.07	2.73	0.07	2.74	0.07
10	2.91	0.06	2.92	0.06	2.91	0.06	2.92	0.06	2.92	0.06	2.93	0.07	2.93	0.07
11	3.10	0.06	3.11	0.06	3.11	0.06	3.12	0.06	3.12	0.06	3.12	0.06	3.13	0.07
12	3.30	0.06	3.30	0.06	3.30	0.06	3.31	0.06	3.31	0.06	3.32	0.06	3.32	0.06
13	3.51	0.06	3.50	0.06	3.50	0.06	3.51	0.06	3.51	0.06	3.52	0.06	3.52	0.06
14	3.70	0.06	3.69	0.06	3.70	0.06	3.70	0.06	3.70	0.06	3.70	0.06	3.71	0.06
15	3.89	0.06	3.89	0.06	3.89	0.06	3.90	0.06	3.90	0.06	3.90	0.06	3.90	0.06
16	4.08	0.06	4.08	0.06	4.09	0.06	4.09	0.06	4.09	0.06	4.09	0.06	4.10	0.06
17	4.28	0.06	4.28	0.06	4.28	0.06	4.28	0.06	4.29	0.06	4.29	0.06	4.29	0.06
18	4.48	0.06	4.47	0.07	4.48	0.06	4.48	0.06	4.47	0.07	4.48	0.06	4.48	0.06
19	4.67	0.07	4.67	0.07	4.67	0.07	4.67	0.07	4.67	0.07	4.68	0.06	4.68	0.07
20	4.86	0.07	4.86	0.07	4.86	0.07	4.86	0.08	4.87	0.07	4.87	0.07	4.87	0.07
21	5.05	0.08	5.05	0.08	5.06	0.08	5.05	0.08	5.06	0.07	5.06	0.07	5.06	0.07
22	5.24	0.09	5.25	0.08	5.25	0.08	5.24	0.08	5.25	0.08	5.25	0.08	5.25	0.08
23	5.43	0.09	5.44	0.09	5.44	0.08	5.44	0.09	5.44	0.08	5.45	0.08	5.44	0.09
24	5.6	0.1	5.63	0.09	5.63	0.09	5.64	0.09	5.64	0.09	5.63	0.09	5.64	0.09
25	5.8	0.1	5.8	0.1	5.8	0.1	5.83	0.10	5.8	0.1	5.8	0.1	5.83	0.10
26	6.1	0.2	6.2	0.2	6.2	0.2	6.2	0.2	6.2	0.2	6.2	0.2	6.2	0.2
27	6.6	0.2	6.6	0.2	6.6	0.2	6.7	0.2	6.6	0.2	6.6	0.2	6.6	0.2
28	7.1	0.2	7.1	0.2	7.1	0.2	7.1	0.2	7.1	0.2	7.1	0.2	7.1	0.2
29	7.6	0.2	7.6	0.2	7.6	0.2	7.6	0.2	7.6	0.2	7.6	0.2	7.6	0.2
30	8.1	0.2	8.1	0.2	8.1	0.2	8.1	0.2	8.1	0.2	8.1	0.2	8.1	0.3
31	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3
32	9.0	0.3	9.0	0.3	9.0	0.3	9.0	0.3	9.0	0.3	9.0	0.3	9.0	0.3
33	9.5	0.3	9.5	0.3	9.5	0.3	9.5	0.3	9.5	0.3	9.5	0.3	9.5	0.4
34	10.2	0.5	10.2	0.5	10.2	0.5	10.2	0.5	10.2	0.5	10.1	0.5	10.2	0.5
35	11.1	0.5	11.1	0.5	11.1	0.5	11.1	0.6	11.1	0.6	11.0	0.6	11.0	0.6
36	12.0	0.6	12.0	0.6	12.0	0.6	12.0	0.6	11.9	0.7	11.9	0.7	11.9	0.7
37	12.8	0.8	12.9	0.8	12.8	0.8	12.8	0.8	12.8	0.8	12.8	0.9	12.8	0.9
38	14.0	1.2	14.1	1.2	14.0	1.2	14.0	1.2	14.0	1.3	13.9	1.3	14.0	1.2
39	15.5	1.2	15.3	1.2	15.2	1.2	15.3	1.2	15.3	1.3	15.1	1.2	15.2	1.3

Table A.13: Results for $\langle E_{true} \rangle$ using the tritium, “gfdcm” corrected data. The error column shows the combination of the uncertainty due to bin width and de-smearing. The first column shows the index of the reconstructed energy bin in which the measurement was made. The dashed out values show where $\langle \rho \rangle$ was reconstructed to be < 0 .

E-field (V/cm)	43.2 ± 2.5	52.6 ± 2.9	64.8 ± 3.7	79.8 ± 4.6	97.8 ± 5.6	119.6 ± 6.9	146.7 ± 8.3	180 ± 10	219 ± 13	268 ± 15	329 ± 19	405 ± 22	484 ± 28	
energy bin #	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	
1	1.12	0.06	1.12	0.06	1.11	0.06	1.11	0.06	1.12	0.07	1.11	0.06	1.13	0.07
2	1.33	0.07	1.33	0.07	1.33	0.07	1.32	0.07	1.32	0.07	1.33	0.07	1.33	0.07
3	1.53	0.07	1.53	0.07	1.54	0.07	1.53	0.07	1.54	0.07	1.54	0.07	1.54	0.07
4	1.74	0.07	1.73	0.07	1.74	0.07	1.74	0.07	1.74	0.07	1.75	0.08	1.74	0.07
5	1.94	0.07	1.93	0.07	1.94	0.07	1.94	0.07	1.94	0.07	1.95	0.08	1.94	0.08
6	2.14	0.07	2.13	0.07	2.14	0.07	2.14	0.07	2.14	0.07	2.15	0.08	2.15	0.07
7	2.33	0.07	2.33	0.07	2.33	0.07	2.34	0.07	2.34	0.07	2.34	0.07	2.35	0.07
8	2.53	0.07	2.53	0.07	2.53	0.07	2.53	0.07	2.53	0.07	2.54	0.07	2.54	0.07
9	2.72	0.06	2.72	0.06	2.73	0.06	2.73	0.07	2.73	0.07	2.74	0.07	2.75	0.07
10	2.92	0.06	2.91	0.06	2.92	0.06	2.92	0.06	2.92	0.06	2.93	0.07	2.93	0.07
11	3.11	0.06	3.11	0.06	3.11	0.06	3.12	0.06	3.12	0.06	3.13	0.07	3.13	0.07
12	3.31	0.06	3.30	0.06	3.31	0.06	3.31	0.06	3.32	0.06	3.32	0.06	3.33	0.07
13	3.51	0.06	3.50	0.06	3.50	0.06	3.51	0.06	3.51	0.06	3.52	0.06	3.52	0.06
14	3.70	0.06	3.69	0.06	3.70	0.06	3.69	0.06	3.71	0.06	3.71	0.06	3.72	0.06
15	3.89	0.06	3.89	0.06	3.89	0.06	3.90	0.06	3.90	0.06	3.90	0.06	3.91	0.06
16	4.09	0.06	4.08	0.06	4.08	0.06	4.09	0.06	4.10	0.06	4.10	0.06	4.10	0.06
17	4.28	0.06	4.28	0.06	4.28	0.06	4.28	0.06	4.29	0.06	4.29	0.06	4.30	0.06
18	4.47	0.07	4.47	0.07	4.47	0.07	4.48	0.06	4.48	0.07	4.48	0.06	4.48	0.06
19	4.66	0.07	4.66	0.07	4.66	0.07	4.67	0.07	4.67	0.07	4.67	0.07	4.68	0.06
20	4.85	0.08	4.86	0.07	4.86	0.07	4.86	0.07	4.87	0.07	4.87	0.07	4.87	0.07
21	5.05	0.08	5.05	0.08	5.06	0.08	5.06	0.08	5.06	0.07	5.06	0.07	5.06	0.07
22	5.24	0.09	5.25	0.08	5.25	0.08	5.25	0.08	5.25	0.08	5.25	0.08	5.25	0.08
23	5.43	0.09	5.44	0.09	5.44	0.09	5.44	0.09	5.45	0.08	5.44	0.08	5.45	0.08
24	5.63	0.10	5.63	0.09	5.64	0.09	5.64	0.09	5.63	0.09	5.64	0.09	5.63	0.09
25	5.8	0.1	5.8	0.1	5.83	0.10	5.8	0.1	5.8	0.1	5.83	0.10	5.8	0.1
26	6.2	0.2	6.2	0.2	6.2	0.2	6.2	0.2	6.2	0.2	6.2	0.2	6.2	0.2
27	6.6	0.2	6.6	0.2	6.6	0.2	6.6	0.2	6.6	0.2	6.6	0.2	6.6	0.2
28	7.1	0.2	7.1	0.2	7.1	0.2	7.1	0.2	7.1	0.2	7.1	0.2	7.1	0.2
29	7.6	0.2	7.6	0.2	7.6	0.2	7.6	0.2	7.6	0.2	7.6	0.2	7.6	0.2
30	8.1	0.2	8.1	0.2	8.1	0.3	8.1	0.2	8.1	0.3	8.1	0.3	8.0	0.3
31	8.6	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3
32	9.0	0.3	9.0	0.3	9.0	0.3	9.0	0.3	9.0	0.3	9.0	0.3	9.0	0.3
33	9.5	0.3	9.5	0.3	9.5	0.3	9.5	0.3	9.5	0.3	9.5	0.4	9.4	0.4
34	10.2	0.5	10.2	0.5	10.2	0.5	10.2	0.5	10.2	0.5	10.1	0.5	10.1	0.5
35	11.1	0.6	11.1	0.6	11.1	0.5	11.1	0.6	11.1	0.6	11.0	0.6	11.0	0.6
36	12.0	0.6	12.0	0.6	12.0	0.6	11.9	0.7	11.9	0.7	11.9	0.7	11.9	0.7
37	12.8	0.8	12.8	0.8	12.8	0.8	12.8	0.9	12.8	0.9	12.8	0.8	12.7	0.9
38	14.0	1.2	14.0	1.2	14.1	1.2	14.0	1.2	13.9	1.3	13.9	1.2	14.0	1.2
39	15.4	1.2	15.5	1.2	15.4	1.2	15.3	1.2	15.3	1.3	15.2	1.2	15.3	1.3

Table A.14: Results for $\langle E_{true} \rangle$ using the tritium, “dcm” corrected data. The error column shows the combination of the uncertainty due to bin width and de-smearing. The first column shows the index of the reconstructed energy bin in which the measurement was made.

E-field (V/cm)	43.2 ± 2.5	52.6 ± 2.9	64.8 ± 3.7	79.8 ± 4.6	97.8 ± 5.6	119.6 ± 6.9	146.7 ± 8.3	180 ± 10	219 ± 13	268 ± 15	329 ± 19	405 ± 22	484 ± 28	
energy bin #	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	\pm	$\langle E_{true} \rangle$	
1	1.12	0.06	1.12	0.07	1.12	0.06	1.12	0.06	1.12	0.07	1.13	0.07	1.14	0.07
2	1.33	0.07	1.33	0.07	1.33	0.07	1.32	0.07	1.33	0.07	1.34	0.07	1.34	0.07
3	1.53	0.07	1.53	0.07	1.53	0.07	1.54	0.07	1.53	0.07	1.54	0.07	1.54	0.07
4	1.74	0.07	1.73	0.07	1.74	0.07	1.74	0.07	1.73	0.07	1.74	0.07	1.74	0.07
5	1.93	0.07	1.93	0.07	1.93	0.07	1.94	0.07	1.94	0.07	1.94	0.07	1.95	0.07
6	2.13	0.07	2.13	0.07	2.13	0.07	2.14	0.07	2.14	0.07	2.14	0.07	2.14	0.07
7	2.33	0.07	2.32	0.06	2.32	0.06	2.33	0.07	2.33	0.07	2.34	0.07	2.34	0.07
8	2.52	0.06	2.52	0.06	2.52	0.06	2.53	0.07	2.53	0.07	2.53	0.07	2.54	0.07
9	2.72	0.06	2.71	0.06	2.72	0.06	2.73	0.07	2.73	0.06	2.73	0.07	2.74	0.07
10	2.90	0.06	2.91	0.06	2.91	0.06	2.92	0.06	2.93	0.07	2.93	0.07	2.93	0.07
11	3.11	0.06	3.11	0.06	3.11	0.06	3.12	0.06	3.12	0.07	3.13	0.07	3.12	0.07
12	3.30	0.06	3.30	0.06	3.31	0.06	3.31	0.06	3.32	0.06	3.32	0.06	3.32	0.06
13	3.49	0.06	3.49	0.06	3.50	0.06	3.50	0.06	3.51	0.06	3.52	0.06	3.51	0.06
14	3.69	0.06	3.69	0.06	3.70	0.06	3.70	0.06	3.71	0.06	3.71	0.06	3.71	0.06
15	3.87	0.07	3.88	0.06	3.89	0.06	3.89	0.06	3.90	0.06	3.90	0.06	3.91	0.06
16	4.07	0.07	4.08	0.06	4.08	0.06	4.09	0.06	4.09	0.06	4.09	0.06	4.10	0.06
17	4.29	0.07	4.27	0.07	4.27	0.07	4.28	0.06	4.28	0.06	4.29	0.06	4.29	0.06
18	4.46	0.08	4.47	0.07	4.47	0.07	4.48	0.06	4.48	0.06	4.48	0.06	4.48	0.06
19	4.64	0.08	4.66	0.07	4.66	0.07	4.67	0.07	4.67	0.07	4.67	0.07	4.68	0.07
20	4.84	0.08	4.85	0.08	4.85	0.08	4.86	0.08	4.86	0.07	4.86	0.07	4.87	0.07
21	5.04	0.09	5.05	0.08	5.04	0.09	5.05	0.08	5.06	0.08	5.06	0.08	5.07	0.07
22	5.23	0.10	5.24	0.09	5.23	0.09	5.24	0.09	5.25	0.08	5.25	0.08	5.25	0.08
23	5.4	0.1	5.43	0.09	5.43	0.10	5.43	0.09	5.44	0.09	5.44	0.09	5.44	0.08
24	5.6	0.1	5.62	0.10	5.6	0.1	5.63	0.10	5.63	0.09	5.63	0.09	5.63	0.09
25	5.8	0.1	5.8	0.1	5.8	0.1	5.8	0.1	5.8	0.1	5.8	0.1	5.8	0.1
26	6.2	0.2	6.2	0.2	6.1	0.2	6.2	0.2	6.2	0.2	6.2	0.2	6.2	0.2
27	6.6	0.2	6.6	0.2	6.6	0.2	6.6	0.2	6.6	0.2	6.6	0.2	6.6	0.2
28	7.1	0.2	7.1	0.2	7.1	0.2	7.1	0.2	7.1	0.2	7.1	0.2	7.1	0.2
29	7.6	0.2	7.6	0.2	7.6	0.2	7.6	0.2	7.6	0.2	7.6	0.2	7.6	0.2
30	8.1	0.3	8.1	0.3	8.1	0.3	8.1	0.3	8.1	0.3	8.1	0.3	8.1	0.3
31	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3	8.5	0.3
32	9.0	0.3	9.0	0.3	9.0	0.3	9.0	0.3	9.0	0.3	9.0	0.3	9.0	0.3
33	9.5	0.3	9.5	0.3	9.5	0.3	9.5	0.3	9.5	0.4	9.5	0.4	9.4	0.4
34	10.2	0.4	10.2	0.5	10.2	0.5	10.1	0.5	10.1	0.5	10.1	0.5	10.1	0.5
35	11.1	0.5	11.1	0.6	11.1	0.6	11.1	0.6	11.0	0.6	11.0	0.6	11.0	0.6
36	12.0	0.6	12.0	0.7	12.0	0.6	11.9	0.7	11.9	0.7	11.9	0.7	11.9	0.7
37	12.8	0.8	12.8	0.8	12.8	0.8	12.8	0.9	12.8	0.9	12.8	0.9	12.7	0.9
38	14.1	1.1	14.0	1.2	14.0	1.2	14.0	1.3	13.9	1.3	13.9	1.3	13.9	1.3
39	15.3	1.1	15.4	1.2	15.3	1.2	15.2	1.2	15.3	1.3	15.2	1.3	15.1	1.3

Table A.15: Results for $\langle E_{true} \rangle$ using the tritium, “z” corrected data. The error column shows the combination of the uncertainty due to bin width and de-smearing. The first column shows the index of the reconstructed energy bin in which the measurement was made.

A.4 Tritium $\langle \rho \rangle$

E-field (V/cm)	43.2 ± 2.5			52.6 ± 2.9			64.8 ± 3.7			79.8 ± 4.6			97.8 ± 5.6			119.6 ± 6.9			146.7 ± 8.3			180 ± 10			219 ± 13			268 ± 15			329 ± 19			405 ± 22			484 ± 28		
energy bin #	$\langle \rho \rangle$	stat.	syst.																																				
1	0.269	0.009	0.034	0.21	0.02	0.03	0.22	0.02	0.04	0.21	0.03	0.03	0.23	0.03	0.05	0.205	0.008	0.048	0.23	0.01	0.06	0.219	0.007	0.069	-	-	-	0.13	0.07	0.04	0.18	0.03	0.06	0.196	0.007	0.072	0.16	0.04	0.07
2	0.26	0.06	0.03	0.29	0.02	0.04	0.29	0.02	0.05	0.27	0.01	0.04	0.25	0.05	0.05	0.25	0.02	0.06	0.25	0.03	0.07	0.27	0.01	0.08	0.29	0.02	0.08	0.25	0.02	0.08	0.27	0.01	0.09	0.27	0.01	0.10	0.277	0.009	0.114
3	0.38	0.02	0.04	0.35	0.02	0.04	0.35	0.01	0.04	0.35	0.02	0.04	0.32	0.03	0.03	0.32	0.02	0.04	0.27	0.05	0.03	0.31	0.02	0.03	0.31	0.02	0.03	0.34	0.02	0.04	0.33	0.01	0.03	0.29	0.02	0.03	0.32	0.01	0.04
4	0.45	0.02	0.04	0.440	0.009	0.045	0.44	0.01	0.05	0.432	0.009	0.044	0.40	0.01	0.04	0.42	0.01	0.05	0.40	0.01	0.04	0.40	0.02	0.04	0.40	0.01	0.04	0.38	0.01	0.05	0.38	0.01	0.04	0.387	0.009	0.041	0.35	0.02	0.04
5	0.49	0.03	0.05	0.52	0.01	0.05	0.527	0.010	0.062	0.50	0.01	0.05	0.487	0.008	0.050	0.48	0.01	0.06	0.46	0.01	0.05	0.48	0.01	0.05	0.45	0.01	0.05	0.44	0.01	0.05	0.44	0.01	0.05	0.425	0.007	0.044	0.40	0.02	0.04
6	0.54	0.02	0.05	0.60	0.01	0.06	0.54	0.02	0.05	0.56	0.01	0.06	0.55	0.01	0.05	0.53	0.01	0.05	0.54	0.02	0.05	0.53	0.01	0.06	0.52	0.01	0.05	0.50	0.01	0.05	0.492	0.007	0.051	0.49	0.01	0.05			
7	0.63	0.02	0.05	0.64	0.01	0.05	0.63	0.01	0.06	0.671	0.009	0.054	0.60	0.01	0.05	0.60	0.01	0.05	0.59	0.01	0.06	0.577	0.010	0.060	0.584	0.008	0.052	0.57	0.01	0.05	0.564	0.009	0.052	0.54	0.01	0.05	0.55	0.01	0.05
8	0.75	0.01	0.05	0.71	0.02	0.05	0.709	0.009	0.051	0.71	0.01	0.06	0.68	0.02	0.05	0.64	0.01	0.05	0.628	0.009	0.055	0.630	0.007	0.053	0.63	0.02	0.04	0.64	0.02	0.05	0.59	0.01	0.05	0.594	0.009	0.050	0.58	0.01	0.05
9	0.82	0.01	0.06	0.76	0.01	0.05	0.76	0.01	0.05	0.74	0.01	0.06	0.76	0.01	0.05	0.721	0.009	0.053	0.72	0.01	0.05	0.697	0.009	0.051	0.66	0.02	0.05	0.65	0.01	0.05	0.67	0.01	0.05	0.651	0.007	0.049	0.65	0.01	0.05
10	0.84	0.02	0.06	0.83	0.01	0.05	0.80	0.02	0.05	0.801	0.009	0.048	0.80	0.01	0.05	0.77	0.01	0.05	0.77	0.01	0.05	0.78	0.01	0.06	0.75	0.01	0.05	0.71	0.01	0.05	0.700	0.008	0.049	0.678	0.009	0.050			
11	0.91	0.01	0.06	0.88	0.01	0.05	0.86	0.01	0.05	0.841	0.009	0.045	0.84	0.01	0.05	0.82	0.01	0.05	0.78	0.01	0.05	0.792	0.010	0.050	0.78	0.02	0.05	0.77	0.02	0.05	0.728	0.009	0.045	0.734	0.008	0.048	0.723	0.010	0.049
12	0.98	0.01	0.06	0.997	0.009	0.053	0.89	0.01	0.05	0.909	0.008	0.049	0.88	0.01	0.05	0.86	0.02	0.05	0.83	0.01	0.05	0.84	0.01	0.05	0.80	0.01	0.05	0.79	0.01	0.05	0.78	0.01	0.05	0.752	0.009	0.047	0.74	0.01	0.05
13	1.01	0.02	0.05	0.97	0.01	0.05	0.96	0.02	0.05	0.96	0.01	0.05	0.93	0.02	0.05	0.89	0.01	0.05	0.86	0.01	0.05	0.89	0.01	0.05	0.85	0.01	0.05	0.82	0.01	0.05	0.81	0.01	0.05	0.805	0.007	0.046	0.789	0.009	0.046
14	1.03	0.02	0.05	1.08	0.01	0.06	1.03	0.01	0.05	0.97	0.02	0.05	0.96	0.01	0.05	0.93	0.02	0.05	0.94	0.01	0.05	0.90	0.01	0.05	0.89	0.01	0.05	0.88	0.01	0.05	0.809	0.009	0.043	0.79	0.02	0.04			
15	1.07	0.02	0.06	1.08	0.01	0.06	1.05	0.01	0.05	1.05	0.01	0.06	1.00	0.01	0.05	0.96	0.02	0.05	0.95	0.01	0.05	0.96	0.01	0.05	0.93	0.02	0.05	0.87	0.01	0.05	0.908	0.008	0.051	0.860	0.010	0.043	0.86	0.01	0.05
16	1.18	0.02	0.06	1.13	0.01	0.06	1.08	0.02	0.05	1.07	0.01	0.06	1.06	0.02	0.05	1.02	0.01	0.06	1.00	0.01	0.05	0.97	0.01	0.05	0.97	0.01	0.05	0.91	0.02	0.05	0.91	0.01	0.05	0.890	0.007	0.046	0.890	0.01	0.05
17	1.21	0.01	0.06	1.17	0.01	0.06	1.14	0.01	0.06	1.11	0.01	0.06	1.06	0.01	0.05	1.02	0.02	0.05	1.059	0.010	0.054	1.02	0.01	0.05	1.00	0.01	0.05	0.99	0.02	0.06	0.94	0.01	0.05	0.92	0.01	0.05	0.90	0.02	0.05
18	1.21	0.01	0.06	1.28	0.01	0.06	1.16	0.02	0.06	1.16	0.01	0.06	1.14	0.01	0.06	1.07	0.02	0.05	1.08	0.01	0.05	1.05	0.01	0.05	1.00	0.02	0.05	1.03	0.01	0.05	0.93	0.01	0.05	0.96	0.01	0.05			
19	1.29	0.01	0.06	1.24	0.01	0.06	1.20	0.01	0.06	1.21	0.01	0.06	1.15	0.02	0.06	1.11	0.02	0.06	1.08	0.01	0.05	1.07	0.02	0.05	1.02	0.02	0.05	1.00	0.02	0.05	0.97	0.01	0.05	0.94	0.02	0.04			
20	1.37	0.02	0.07	1.35	0.02	0.07	1.20	0.02	0.06	1.26	0.02	0.06	1.16	0.01	0.06	1.16	0.01	0.06	1.15	0.01	0.06	1.12	0.01	0.06	1.04	0.02	0.05	1.07	0.02	0.05	1.04	0.01	0.05	1.00	0.01	0.05	0.94	0.02	0.04
21	1.37	0.03	0.07	1.30	0.03	0.07	1.29	0.02	0.06	1.27	0.01	0.06	1.25	0.01	0.06	1.15	0.02	0.06	1.18	0.01	0.06	1.154	0.008	0.058	1.12	0.02	0.06	1.06	0.01	0.05	1.04	0.01	0.05	1.023	0.009	0.050	0.98	0.02	0.05
22	1.37	0.03	0.07	1.38	0.02	0.07	1.29	0.02	0.06	1.25	0.02	0.06	1.25	0.02	0.06	1.24	0.02	0.06	1.16	0.01	0.06	1.20	0.02	0.06	1.09	0.02	0.05	1.09	0.01	0.05	1.06	0.02	0.05	1.04	0.01	0.05	1.03	0.02	0.05
23	1.50	0.02	0.07	1.48	0.01	0.07	1.36	0.01	0.07	1.33	0.02	0.07	1.28	0.02	0.06	1.24	0.02	0.06	1.21	0.02	0.06	1.17	0.02	0.06	1.15	0.01	0.06	1.09	0.02	0.05	1.07	0.01	0.06	1.05	0.01	0.05	1.02	0.01	0.05
24	1.49	0.02	0.07	1.44	0.01	0.07	1.39	0.02	0.07	1.33	0.02	0.07	1.28	0.02	0.06	1.25	0.02	0.06	1.24	0.01	0.06	1.12	0.02	0.06	1.18	0.02	0.06	1.13	0.02	0.05	1.13	0.02	0.06	1.10	0.01	0.05	1.05	0.02	0.05
25	1.54	0.02	0.08	1.49	0.02	0.07	1.42	0.02	0.07	1.37	0.02	0.07	1.32	0.01	0.07	1.31	0.01	0.07	1.26	0.02	0.06	1.22	0.01	0.06	1.18	0.01	0.06	1.11	0.02	0.05	1.13	0.02	0.06	1.12	0.01	0.06	1.02	0.02	0.05
26	1.54	0.02	0.08	1.50	0.01	0.08	1.48	0.01	0.08	1.41	0.01	0.07	1.360	0.010	0.067	1.35	0.01	0.07	1.27	0.01	0.07	1.24	0.01	0.06	1.212	0.007	0.062	1.19	0.02	0.06	1.155	0.008	0.059	1.126	0.008	0.058	1.08	0.01	0.05
27	1.64	0.02	0.09	1.61	0.01	0.09	1.52	0.01	0.08	1.507	0.008	0.079	1.43	0.01	0.07	1.38	0.01	0.07	1.34	0.01	0.07	1.295	0.009	0.067	1.24	0.01	0.06	1.206	0.009	0.062	1.192	0.009	0.063	1.115	0.010	0.057			
28	1.69	0.02	0.09																																				

E-field (V/cm)	43.2 ± 2.5			52.6 ± 2.9			64.8 ± 3.7			79.8 ± 4.6			97.8 ± 5.6			119.6 ± 6.9			146.7 ± 8.3			180 ± 10			219 ± 13			268 ± 15			329 ± 19			405 ± 22			484 ± 28		
energy bin #	$\langle \rho \rangle$	stat.	syst.																																				
1	0.31	0.01	0.05	0.30	0.01	0.03	0.25	0.05	0.03	0.25	0.02	0.03	0.29	0.01	0.04	0.27	0.02	0.04	0.24	0.03	0.05	0.27	0.01	0.06	0.25	0.01	0.06	0.21	0.03	0.05	0.22	0.02	0.06	0.23	0.01	0.08	0.22	0.02	0.08
2	0.38	0.02	0.06	0.38	0.01	0.04	0.38	0.01	0.05	0.32	0.03	0.03	0.36	0.02	0.05	0.32	0.01	0.04	0.29	0.03	0.06	0.35	0.01	0.07	0.29	0.02	0.07	0.33	0.01	0.08	0.31	0.01	0.09	0.31	0.01	0.10	0.29	0.02	0.11
3	0.48	0.01	0.07	0.45	0.01	0.04	0.42	0.02	0.05	0.41	0.01	0.05	0.39	0.02	0.04	0.39	0.02	0.05	0.40	0.01	0.05	0.40	0.01	0.05	0.37	0.02	0.05	0.38	0.02	0.04	0.40	0.01	0.05	0.39	0.01	0.05	0.37	0.01	0.05
4	0.51	0.02	0.06	0.51	0.01	0.05	0.51	0.01	0.06	0.51	0.02	0.06	0.50	0.01	0.05	0.49	0.01	0.06	0.47	0.01	0.06	0.49	0.01	0.06	0.49	0.01	0.06	0.45	0.02	0.05	0.46	0.01	0.06	0.46	0.01	0.05	0.44	0.02	0.05
5	0.62	0.01	0.06	0.60	0.01	0.06	0.59	0.01	0.06	0.58	0.01	0.07	0.58	0.01	0.06	0.557	0.010	0.056	0.56	0.01	0.07	0.55	0.01	0.05	0.56	0.01	0.07	0.51	0.02	0.05	0.48	0.02	0.05	0.522	0.009	0.059	0.50	0.02	0.06
6	0.63	0.02	0.06	0.69	0.01	0.06	0.66	0.01	0.06	0.67	0.01	0.07	0.651	0.009	0.067	0.64	0.01	0.07	0.66	0.01	0.07	0.63	0.01	0.06	0.63	0.01	0.07	0.61	0.01	0.06	0.60	0.01	0.06	0.58	0.01	0.07	0.604	0.009	0.068
7	0.78	0.01	0.06	0.77	0.01	0.06	0.75	0.01	0.06	0.74	0.01	0.05	0.70	0.02	0.06	0.69	0.01	0.07	0.68	0.01	0.07	0.686	0.009	0.069	0.67	0.01	0.07	0.71	0.01	0.07	0.659	0.009	0.069	0.646	0.009	0.068	0.65	0.01	0.06
8	0.86	0.01	0.06	0.82	0.01	0.06	0.82	0.01	0.06	0.82	0.01	0.06	0.78	0.02	0.06	0.74	0.01	0.06	0.76	0.01	0.07	0.73	0.01	0.06	0.75	0.01	0.07	0.73	0.01	0.07	0.727	0.009	0.068	0.70	0.01	0.06			
9	0.90	0.02	0.06	0.86	0.01	0.06	0.84	0.01	0.06	0.86	0.01	0.06	0.84	0.01	0.06	0.83	0.01	0.06	0.82	0.01	0.06	0.77	0.01	0.06	0.77	0.01	0.07	0.771	0.008	0.065	0.76	0.01	0.06						
10	0.98	0.02	0.06	0.90	0.02	0.05	0.92	0.02	0.06	0.93	0.01	0.06	0.89	0.01	0.06	0.88	0.01	0.06	0.87	0.01	0.06	0.905	0.009	0.067	0.85	0.02	0.06	0.81	0.02	0.06	0.829	0.009	0.062	0.79	0.01	0.06	0.794	0.009	0.060
11	1.04	0.02	0.06	1.03	0.01	0.05	0.98	0.01	0.06	0.97	0.01	0.06	0.974	0.009	0.060	0.95	0.02	0.06	0.91	0.02	0.06	0.92	0.01	0.06	0.86	0.02	0.06	0.87	0.01	0.06	0.866	0.009	0.060	0.84	0.01	0.06			
12	1.09	0.02	0.06	1.09	0.01	0.06	1.02	0.02	0.06	1.03	0.01	0.06	0.99	0.01	0.06	0.98	0.01	0.06	0.96	0.01	0.06	0.95	0.01	0.05	0.95	0.01	0.06	0.89	0.01	0.05	0.888	0.008	0.058	0.89	0.01	0.06			
13	1.11	0.02	0.06	1.146	0.010	0.059	1.11	0.01	0.06	1.07	0.02	0.06	1.04	0.02	0.05	1.01	0.01	0.06	0.99	0.01	0.06	0.96	0.02	0.06	0.96	0.02	0.05	0.95	0.02	0.05	0.926	0.010	0.056	0.87	0.01	0.05			
14	1.17	0.01	0.06	1.17	0.01	0.06	1.16	0.01	0.06	1.13	0.02	0.06	1.08	0.01	0.06	1.06	0.02	0.06	1.07	0.01	0.06	1.04	0.02	0.06	1.01	0.02	0.06	1.005	0.009	0.053	1.01	0.01	0.06	0.952	0.009	0.055	0.96	0.01	0.06
15	1.28	0.02	0.07	1.21	0.02	0.06	1.19	0.02	0.06	1.19	0.02	0.06	1.16	0.01	0.06	1.05	0.03	0.06	1.11	0.01	0.06	1.05	0.02	0.05	1.08	0.01	0.06	0.98	0.02	0.05	1.01	0.01	0.05	1.01	0.01	0.06			
16	1.33	0.02	0.07	1.27	0.02	0.07	1.20	0.02	0.06	1.19	0.01	0.06	1.15	0.02	0.06	1.15	0.02	0.06	1.16	0.02	0.07	1.12	0.01	0.06	1.12	0.01	0.06	1.06	0.02	0.06	1.02	0.01	0.05	1.06	0.01	0.06	1.00	0.01	0.05
17	1.33	0.02	0.07	1.36	0.02	0.07	1.30	0.02	0.07	1.24	0.02	0.07	1.24	0.01	0.06	1.17	0.02	0.06	1.19	0.01	0.06	1.13	0.02	0.06	1.11	0.01	0.06	1.14	0.02	0.06	1.10	0.02	0.06	1.02	0.01	0.05	1.02	0.01	0.05
18	1.37	0.02	0.07	1.37	0.02	0.07	1.27	0.02	0.06	1.33	0.02	0.07	1.26	0.02	0.06	1.22	0.02	0.06	1.22	0.01	0.06	1.17	0.01	0.06	1.12	0.02	0.06	1.15	0.01	0.06	1.06	0.02	0.05	1.09	0.01	0.06	1.10	0.01	0.06
19	1.47	0.02	0.08	1.42	0.02	0.07	1.33	0.01	0.07	1.39	0.01	0.07	1.30	0.02	0.07	1.25	0.02	0.06	1.22	0.02	0.06	1.23	0.02	0.06	1.15	0.01	0.06	1.18	0.02	0.06	1.15	0.01	0.06	1.125	0.010	0.057	1.05	0.02	0.05
20	1.54	0.03	0.08	1.46	0.02	0.07	1.39	0.02	0.07	1.36	0.02	0.07	1.35	0.02	0.07	1.31	0.02	0.07	1.25	0.02	0.06	1.27	0.02	0.07	1.19	0.02	0.06	1.15	0.02	0.06	1.18	0.01	0.06	1.13	0.01	0.06	1.10	0.02	0.05
21	1.51	0.03	0.08	1.47	0.02	0.08	1.46	0.02	0.07	1.38	0.02	0.07	1.36	0.02	0.07	1.35	0.02	0.07	1.33	0.01	0.06	1.30	0.02	0.07	1.24	0.01	0.06	1.23	0.02	0.06	1.19	0.02	0.06	1.11	0.01	0.06	1.11	0.03	0.05
22	1.61	0.02	0.09	1.59	0.01	0.08	1.45	0.02	0.08	1.47	0.01	0.08	1.43	0.02	0.07	1.40	0.01	0.07	1.30	0.01	0.06	1.34	0.02	0.07	1.27	0.01	0.07	1.20	0.02	0.06	1.19	0.01	0.06	1.17	0.01	0.06	1.17	0.01	0.06
23	1.67	0.02	0.09	1.62	0.02	0.08	1.54	0.02	0.08	1.49	0.03	0.08	1.42	0.02	0.07	1.38	0.02	0.07	1.30	0.02	0.07	1.32	0.02	0.07	1.26	0.01	0.06	1.20	0.03	0.06	1.19	0.02	0.06	1.15	0.02	0.06	1.15	0.02	0.06
24	1.69	0.02	0.09	1.63	0.02	0.08	1.56	0.02	0.08	1.47	0.02	0.08	1.45	0.01	0.07	1.47	0.01	0.08	1.39	0.02	0.07	1.32	0.02	0.07	1.29	0.02	0.07	1.25	0.02	0.06	1.26	0.02	0.06	1.24	0.01	0.06	1.18	0.02	0.06
25	1.69	0.02	0.09	1.65	0.02	0.08	1.55	0.02	0.08	1.52	0.02	0.08	1.46	0.02	0.07	1.43	0.02	0.08	1.38	0.02	0.07	1.39	0.02	0.07	1.35	0.01	0.07	1.30	0.02	0.06	1.27	0.02	0.06	1.26	0.01	0.06	1.15	0.02	0.06
26	1.76	0.02	0.09	1.67	0.01	0.09	1.65	0.01	0.08	1.583	0.009	0.083	1.54	0.01	0.08	1.50	0.01	0.08	1.426	0.008	0.073	1.40	0.01	0.07	1.36	0.01	0.07	1.34	0.01	0.07	1.31	0.01	0.07	1.269	0.009	0.066	1.23	0.01	0.06
27	1.85	0.02	0.10	1.78	0.01	0.09	1.70	0.01	0.09	1.67	0.01	0.09	1.52	0.01	0.08	1.48	0.01	0.08	1.48	0.01	0.08	1.453	0.009	0.077	1.39	0.01	0.07	1.35	0.01	0.07	1.345	0.010	0.071	1.26	0.01	0.07			
28	1.87	0.02	0.10	1.86	0.02	0.10	1.82	0.01	0.10	1.73	0.01	0.10	1.67	0.01	0.09	1.64	0.01																						

E-field (V/cm)	43.2 ± 2.5			52.6 ± 2.9			64.8 ± 3.7			79.8 ± 4.6			97.8 ± 5.6			119.6 ± 6.9			146.7 ± 8.3			180 ± 10			219 ± 13			268 ± 15			329 ± 19			405 ± 22			484 ± 28		
energy bin #	$\langle \rho \rangle$	stat.	syst.																																				
1	0.28	0.02	0.03	0.28	0.02	0.04	0.27	0.03	0.03	0.26	0.02	0.03	0.27	0.02	0.04	0.27	0.02	0.04	0.24	0.06	0.04	0.24	0.02	0.04	0.24	0.02	0.05	0.21	0.01	0.05	0.19	0.05	0.06	0.236	0.010	0.074	0.22	0.02	0.08
2	0.33	0.03	0.04	0.36	0.01	0.05	0.36	0.01	0.05	0.30	0.03	0.04	0.34	0.02	0.04	0.28	0.01	0.04	0.32	0.02	0.05	0.32	0.02	0.06	0.28	0.03	0.06	0.31	0.01	0.08	0.32	0.01	0.09	0.31	0.01	0.10	0.31	0.02	0.11
3	0.45	0.01	0.05	0.41	0.01	0.05	0.39	0.01	0.05	0.40	0.01	0.04	0.37	0.02	0.04	0.36	0.02	0.04	0.37	0.02	0.05	0.34	0.02	0.04	0.34	0.02	0.04	0.38	0.01	0.05	0.38	0.01	0.04	0.38	0.01	0.04			
4	0.47	0.01	0.05	0.49	0.01	0.05	0.49	0.01	0.06	0.46	0.02	0.05	0.47	0.01	0.05	0.468	0.010	0.052	0.43	0.02	0.05	0.46	0.02	0.05	0.45	0.01	0.05	0.43	0.02	0.06	0.43	0.01	0.05	0.456	0.009	0.052	0.43	0.02	0.05
5	0.60	0.01	0.06	0.57	0.01	0.06	0.56	0.01	0.05	0.555	0.009	0.056	0.54	0.01	0.06	0.537	0.010	0.060	0.51	0.01	0.05	0.52	0.02	0.06	0.51	0.01	0.06	0.48	0.02	0.06	0.50	0.02	0.06	0.525	0.008	0.058	0.52	0.02	0.06
6	0.60	0.02	0.06	0.629	0.009	0.051	0.59	0.01	0.05	0.62	0.01	0.06	0.602	0.009	0.053	0.60	0.01	0.06	0.60	0.01	0.06	0.57	0.01	0.06	0.599	0.010	0.068	0.57	0.02	0.07	0.58	0.01	0.07	0.56	0.01	0.06	0.620	0.010	0.071
7	0.72	0.01	0.07	0.72	0.01	0.05	0.70	0.01	0.06	0.69	0.01	0.05	0.66	0.02	0.05	0.65	0.01	0.06	0.65	0.01	0.06	0.639	0.009	0.056	0.63	0.01	0.07	0.66	0.01	0.07	0.64	0.01	0.07	0.64	0.01	0.07	0.66	0.02	0.07
8	0.81	0.01	0.07	0.77	0.01	0.06	0.77	0.01	0.06	0.73	0.01	0.05	0.69	0.01	0.06	0.70	0.01	0.05	0.698	0.010	0.055	0.69	0.01	0.06	0.70	0.01	0.06	0.70	0.01	0.07	0.709	0.010	0.068	0.71	0.01	0.06			
9	0.84	0.02	0.05	0.81	0.01	0.05	0.80	0.01	0.05	0.82	0.01	0.06	0.82	0.01	0.06	0.815	0.010	0.059	0.79	0.01	0.06	0.76	0.01	0.05	0.75	0.01	0.06	0.73	0.01	0.06	0.75	0.01	0.07	0.765	0.007	0.062	0.77	0.01	0.06
10	0.90	0.02	0.06	0.84	0.02	0.05	0.85	0.01	0.05	0.89	0.01	0.06	0.861	0.009	0.058	0.81	0.01	0.05	0.82	0.01	0.06	0.85	0.01	0.06	0.80	0.01	0.05	0.77	0.01	0.05	0.80	0.01	0.06	0.79	0.01	0.06	0.811	0.009	0.068
11	0.95	0.01	0.06	0.96	0.01	0.05	0.93	0.01	0.06	0.92	0.01	0.05	0.917	0.009	0.059	0.91	0.01	0.06	0.85	0.02	0.06	0.87	0.01	0.06	0.80	0.01	0.05	0.84	0.01	0.06	0.831	0.009	0.057	0.852	0.009	0.059	0.85	0.01	0.06
12	1.03	0.02	0.06	1.04	0.01	0.06	0.99	0.01	0.06	0.99	0.01	0.05	0.95	0.02	0.06	0.93	0.01	0.06	0.92	0.01	0.06	0.92	0.01	0.06	0.89	0.01	0.05	0.86	0.01	0.06	0.866	0.009	0.055	0.89	0.01	0.06			
13	1.05	0.02	0.06	1.08	0.01	0.06	1.06	0.01	0.06	1.01	0.01	0.05	1.03	0.02	0.06	0.95	0.02	0.06	0.957	0.009	0.057	0.97	0.01	0.06	0.92	0.02	0.05	0.91	0.02	0.05	0.94	0.01	0.06	0.91	0.01	0.05	0.90	0.02	0.06
14	1.10	0.02	0.06	1.127	0.009	0.061	1.10	0.01	0.06	1.08	0.01	0.06	1.01	0.01	0.06	1.02	0.02	0.06	1.03	0.01	0.06	0.97	0.02	0.05	0.95	0.02	0.05	0.97	0.01	0.06	0.94	0.01	0.05	0.99	0.01	0.06			
15	1.18	0.02	0.07	1.19	0.01	0.06	1.12	0.02	0.06	1.08	0.02	0.05	1.10	0.01	0.06	1.00	0.02	0.05	1.06	0.01	0.06	1.04	0.01	0.06	1.04	0.02	0.06	0.96	0.02	0.06	1.01	0.01	0.06	0.98	0.01	0.05	1.02	0.01	0.06
16	1.26	0.02	0.07	1.19	0.01	0.06	1.16	0.02	0.06	1.14	0.01	0.06	1.12	0.02	0.06	1.12	0.02	0.06	1.08	0.02	0.06	1.12	0.02	0.06	1.05	0.02	0.05	1.08	0.01	0.07	1.05	0.01	0.06	1.02	0.01	0.05	1.00	0.01	0.05
17	1.24	0.02	0.07	1.28	0.02	0.07	1.22	0.02	0.07	1.17	0.01	0.06	1.14	0.02	0.06	1.08	0.02	0.06	1.12	0.02	0.06	1.10	0.02	0.06	1.05	0.02	0.05	1.08	0.01	0.07	1.05	0.01	0.06	1.02	0.01	0.05	1.07	0.01	0.05
18	1.31	0.02	0.07	1.32	0.02	0.07	1.24	0.01	0.07	1.29	0.01	0.07	1.21	0.02	0.06	1.16	0.02	0.06	1.17	0.01	0.06	1.09	0.02	0.06	1.05	0.02	0.05	1.12	0.01	0.06	1.06	0.01	0.05	1.087	0.009	0.055	1.06	0.02	0.05
19	1.37	0.02	0.07	1.32	0.02	0.07	1.28	0.02	0.07	1.31	0.01	0.07	1.25	0.01	0.06	1.22	0.02	0.06	1.15	0.02	0.06	1.17	0.01	0.06	1.11	0.01	0.05	1.12	0.02	0.06	1.09	0.01	0.05	1.11	0.01	0.06	1.09	0.02	0.05
20	1.43	0.03	0.07	1.40	0.01	0.07	1.33	0.02	0.07	1.33	0.02	0.07	1.29	0.01	0.07	1.23	0.02	0.06	1.21	0.02	0.06	1.20	0.01	0.06	1.15	0.02	0.06	1.13	0.02	0.06	1.14	0.01	0.06	1.14	0.01	0.06	1.10	0.01	0.05
21	1.40	0.03	0.07	1.40	0.02	0.07	1.41	0.02	0.07	1.33	0.02	0.07	1.30	0.02	0.07	1.25	0.02	0.06	1.27	0.01	0.07	1.25	0.02	0.07	1.15	0.02	0.06	1.18	0.01	0.06	1.16	0.02	0.06	1.16	0.01	0.06	1.18	0.02	0.06
22	1.50	0.02	0.08	1.48	0.02	0.08	1.38	0.02	0.07	1.37	0.02	0.07	1.36	0.02	0.07	1.33	0.02	0.07	1.25	0.02	0.07	1.29	0.02	0.07	1.21	0.02	0.06	1.14	0.02	0.06	1.17	0.01	0.06	1.18	0.02	0.06			
23	1.59	0.02	0.09	1.57	0.02	0.08	1.45	0.01	0.08	1.44	0.02	0.07	1.37	0.01	0.07	1.33	0.02	0.07	1.32	0.02	0.07	1.32	0.02	0.07	1.25	0.02	0.07	1.20	0.02	0.06	1.18	0.02	0.06	1.20	0.01	0.06	1.16	0.02	0.06
24	1.57	0.03	0.09	1.52	0.02	0.08	1.47	0.02	0.08	1.40	0.02	0.07	1.43	0.02	0.07	1.34	0.03	0.07	1.31	0.02	0.07	1.27	0.02	0.06	1.25	0.02	0.07	1.22	0.02	0.06	1.24	0.01	0.06	1.18	0.02	0.06			
25	1.63	0.03	0.09	1.55	0.02	0.08	1.48	0.02	0.08	1.47	0.02	0.08	1.38	0.02	0.07	1.39	0.02	0.08	1.32	0.02	0.07	1.30	0.02	0.07	1.27	0.02	0.07	1.26	0.02	0.07	1.22	0.02	0.06	1.23	0.01	0.06	1.20	0.02	0.06
26	1.65	0.01	0.09	1.59	0.01	0.09	1.57	0.02	0.09	1.501	0.009	0.079	1.46	0.01	0.08	1.45	0.01	0.08	1.36	0.01	0.07	1.32	0.01	0.07	1.30	0.01	0.07	1.29	0.01	0.07	1.28	0.01	0.07	1.260	0.010	0.066	1.23	0.01	0.06
27	1.76	0.02	0.10	1.703	0.009	0.094	1.63	0.02	0.09	1.59	0.01	0.09	1.55	0.02	0.08	1.45	0.01	0.08	1.415	0.009	0.076	1.44	0.02	0.08	1.38	0.01	0.07	1.33	0.01	0.07	1.30	0.01	0.07	1.334	0.009	0.0			

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