

# Design and Characterization of a 28-nm Bulk-CMOS Cryogenic Quantum Controller Dissipating Less than 2 mW at 3 K

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**Abstract**—Implementation of an error corrected quantum computer is believed to require a quantum processor with on the order of a million or more physical qubits and, in order to run such a processor, a quantum control system of similar scale will be required. Such a controller will need to be integrated within the cryogenic system and in close proximity with the quantum processor in order to make such a system practical. Here, we present a prototype cryogenic CMOS quantum controller designed in a 28-nm bulk CMOS process and optimized to implement a 4-bit XY gate instruction set for transmon qubits. After introducing the transmon qubit, including a discussion of how it is controlled, design considerations are discussed, with an emphasis on error rates and scalability. The circuit design is then discussed. Cryogenic performance of the underlying technology is presented and the results of several quantum control experiments carried out using the integrated controller are described. The paper ends with a comparison to the state of the art. It has been shown that the quantum control IC achieves comparable performance with a conventional rack mount control system while dissipating less than 2 mW of total AC and DC power and requiring a digital data stream of less than 500 Mb/s.

**Index Terms**—Quantum computing, quantum control, pulse modulator, cryogenic electronics, radiofrequency integrated circuits

## I. INTRODUCTION

QUANTUM computers have the potential to solve currently intractable problems in cryptography [1], machine learning [2], computational chemistry [3], and database searching [4], to name a few. Over the past decade, significant progress has been made towards the implementation of such a computer and the field is now at the point where small quantum processors with on the order of 50-to-100 quantum bits, or qubits, are being demonstrated [5], [6], [7].

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However, qubits are error-prone devices and, even when cooled to 10 mK, today's best devices still suffer from error rates on the order of 0.1% per computational step. Performing error-free calculations using these noisy qubits will require the implementation of quantum error correction (QEC) codes and it is currently believed that approximately a million qubits will be required to implement an error protected quantum computer [8]. Scaling contemporary technology to these levels comes with many daunting challenges.

While intense research in the field has pushed the performance of small quantum processors beyond that required to achieve fault tolerance [9], significant work is still required if a system with on the order of a million qubits is to be realized. In order to operate a quantum processor at these levels, a high performance quantum control and measurement system is required [10]. Today's systems are realized using racks of room temperature electronics, connected to the quantum processor through meters of lossy coaxial cable, as shown conceptually in Fig. 1(a) [9]. If quantum computing systems are to be scaled to the million qubit level, these systems must be monolithically integrated and placed in close proximity to the quantum controller.

Multiple approaches to scale the quantum control and measurement system such that it can be integrated within the cryogenic system have been proposed. When operating at deep cryogenic temperatures, the use of mixed signal circuits based upon Josephson junctions becomes feasible. As such, authors have proposed mixed-signal control [11] and readout [12] architectures based on Josephson junction technology, with a large digital processor integrated at 4 K and drive/sensing circuitry co-located on the 10 mK stage of the system [13]. However, even for small-scale circuits, a significant impact on performance has been observed due to heating from the superconductive circuits heatsunk to the 10 mK stage of the system [11] and ongoing work seeks to overcome this limitation.

Other authors have proposed reducing the number of high speed interconnects from room temperature down to the quantum processor by introducing a semiconductor switch matrix at the 10 mK stage in order to multiplex RF control signals [14]. However, this approach also has the problem of introducing

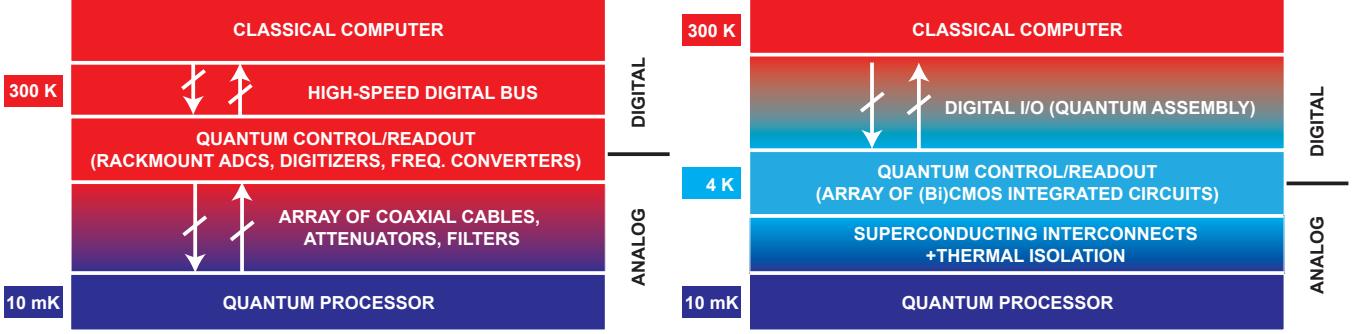


Fig. 1. High level picture of current and proposed approaches to interfacing a quantum processor to a classical computer.

dissipation at the base temperature.

Finally, significant work is currently underway towards implementation of the scheme shown conceptually in Fig. 1(b) (e.g., [15], [16]). In this approach, the quantum-to-classical interface is integrated in one or more (Bi)CMOS ICs and located on the 4-K stage of the system. The use of commercial (Bi)CMOS technologies provides a significant advantage due to the high manufacturing yields and mature design infrastructure. Moreover, 4 K is a particularly convenient temperature, since it is feasible to cool devices dissipating watts of power. Even so, this is a major challenge, as the cryo ICs must be high performance and very low power (eventually < 1 mW/qubit). Preliminary work in this area has focused on circuit blocks [17], [18], [19] and transistor modeling [17], [20], [21], both of which are important steps towards the implementation of integrated cryogenic quantum control and measurement systems.

In this paper, we present the design and implementation of one part of a cryogenic quantum control and measurement system: a CMOS IC that has been designed for operation at 3-K and optimized to perform XY gate operations on transmon qubits. The paper is organized as follows.

- 1) A brief introduction to qubits and quantum control is presented. The fundamentals of transmon qubits are described with an emphasis on microwave control of these devices.
- 2) Design considerations are described. Requirements associated with quantum error correction and scalability are emphasized.
- 3) The design of a cryogenic CMOS quantum control circuit is presented along with a discussion of particular challenges associated with design for operation at deep cryogenic temperatures.
- 4) Experimental results are presented. The temperature dependence the underlying transistor technology is evaluated. A series of quantum control experiments are carried out to validate the efficacy of the implemented quantum controller.
- 5) The results are compared to the state of the art and future steps are discussed.

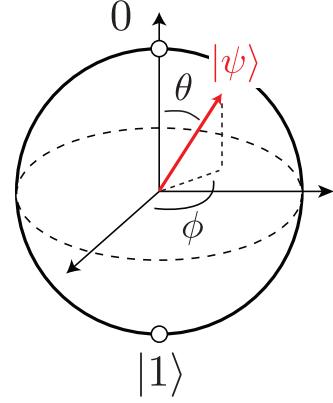


Fig. 2. Bloch sphere representation of a qubit.

## II. QUBITS AND QUANTUM CONTROL

The fundamental building block in a quantum computer is the quantum bit, or qubit. A qubit is a two-level quantum mechanical object whose instantaneous state can be described as a superposition of its two basis states<sup>1</sup>,

$$|\psi\rangle = \cos\left(\frac{\theta}{2}\right)|0\rangle + \exp\{j\phi\}\sin\left(\frac{\theta}{2}\right)|1\rangle. \quad (1)$$

The state of a qubit has a unique interpretation as a point on the surface of a unit sphere, which is referred to as the Bloch sphere. As shown in Fig. 2, the north and south poles of the Bloch sphere correspond to the |0> and |1> states respectively, whereas all other points on the surface of the Bloch sphere correspond to unique superposition states.

This geometric picture provides insight into the control and measurement of single qubits. The act of measuring the qubit will cause its state to collapse to either its |0> or |1> basis state and the probability of these two outcomes depends solely on the elevation angle,  $\theta$ :  $P\{|0\rangle\} = \cos^2(\theta/2)$  and  $P\{|1\rangle\} = \sin^2(\theta/2)$ . Single qubit gate operations are represented by  $2 \times 2$  unitary matrices and can be interpreted as deterministic rotations of the Bloch vector on the surface of the Bloch sphere. Thus, while  $\phi$  has no impact on measurement

<sup>1</sup>As is standard in quantum computing, we use Dirac notation as shorthand for state vectors. To prevent confusion:  $|0\rangle = [1 \ 0]^T$  and  $|1\rangle = [0 \ 1]^T$ , so  $|\psi\rangle = [\cos(\theta/2) \ \exp\{j\phi\}\sin(\theta/2)]^T$

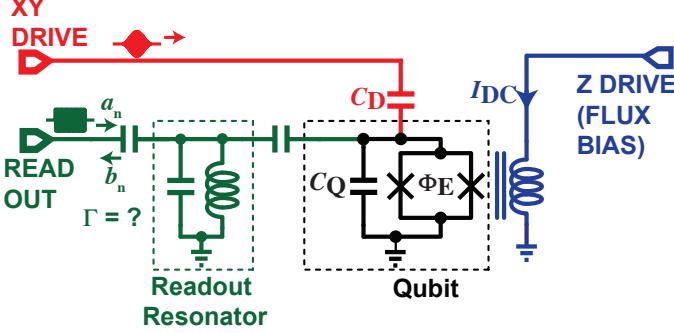


Fig. 3. Schematic diagram of transmon qubit including XY drive, Z drive, and readout ports. The “X” symbols represent Josephson junctions. The XY drive line is used to induce rotations of the qubit state about an axis in the XY plane of the Bloch sphere, the Z drive is used to control the qubit frequency (useful for two qubit gates, which are beyond the scope of this article), and the readout line is used to perform a projective measurement of the qubit state.

results, it does impact the effect of gate operations on the qubit.

To explain how single qubit gate operations are enabled by the physics of quantum mechanics, we begin by pointing out that a qubit is a quantum mechanical object and, as such, obeys the time dependent Schrödinger equation [22],

$$\frac{\partial}{\partial t}|\psi(t)\rangle = -\frac{j}{\hbar}\hat{H}|\psi(t)\rangle, \quad (2)$$

where  $\hbar$  is the reduced Planck’s constant and  $\hat{H}$  is the Hamiltonian (total energy) operator, which for a single qubit is a  $2 \times 2$  matrix. As such, the time evolution of the qubit state is completely determined by its Hamiltonian. Thus, deterministic control of the state of a quantum system requires the ability to systematically enable and disable components of the system’s Hamiltonian. In Section II-B, we will explain how this is carried out for transmon qubits. However, first we describe these devices.

#### A. The Flux-Tunable Transmon Qubit

A schematic diagram of a flux-tunable transmon qubit, complete with XY-drive, Z-drive, and readout ports is shown in Fig. 3. The intrinsic qubit consists of capacitor  $C_Q$  in parallel with a Josephson junction loop. A Josephson junction is a superconducting tunnel junction and can be thought of as a nonlinear inductance of the form  $L_J = L_{J0}/\cos(2\pi\Phi/\Phi_0)$ , where  $\Phi = \int v_{JJ}dt$  is the flux across the junction,  $\Phi_0 = h/2q$  is the flux quanta,  $h$  is Planck’s constant,  $q$  is the charge of an electron,  $L_{J0} = \Phi_0/2\pi I_C$ , and  $I_C$  is the critical current of the junction and is proportional to junction area [23]. A Josephson junction loop, or SQUID, can be thought of as a composite Josephson junction, with flux-tunable critical current,  $I_{C,SQUID} = 2I_{C0}|\cos(\pi\Phi_E/\Phi_0)|$ , where  $I_{C0}$  is the critical current of each of the (identical) junctions and  $\Phi_E$  is the external flux used to tune the effective critical current [24]. As such, the flux-tunable transmon qubit can be thought of as a frequency tunable non-linear LC resonator.

If cooled to temperatures such that thermal population of the non-linear resonator is suppressed, a transmon behaves

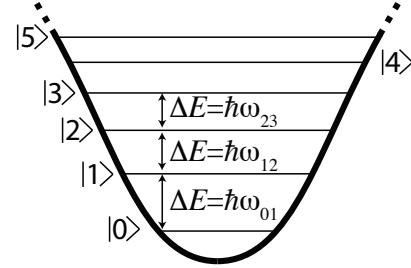


Fig. 4. Energy diagram for transmon qubit. The non-linearity of the Josephson junction creates anharmonicity.

quantum mechanically. For typical qubit frequencies in the vicinity of 5 GHz, the effective photon temperature ( $T_{\text{Photon}} = hf/k$ ) is approximately 250 mK. As such, these devices are typically cooled to the 10 mK range to ensure that thermal excitations are sufficiently suppressed<sup>2</sup>.

The eigenenergies of a transmon can be found from the Hamiltonian of the isolated qubit [25]:

$$E_n \approx \hbar\omega_0 \left( n + \frac{1}{2} \right) - \frac{E_C}{12} (6n^2 + 6n + 3). \quad (3)$$

Here, the index  $n$  is an integer greater than or equal to zero,  $\omega_0 = 1/\sqrt{L_{J0}C_Q}$ , and  $E_C = q^2/2C_Q$  is the energy required to add one electron to the charge on the capacitor. The corresponding energy diagram appears in Fig. 4. In contrast to the ideal qubit described above, the transmon has an infinite number of energy levels. As such, care must be taken to ensure that only the lowest two energy levels are occupied. Since it is only possible to populate higher levels if the  $|2\rangle$  state is already populated, we will constrain our control signals such that the  $|2\rangle$  state is not populated and neglect higher levels in the following discussion.

The XY drive port shown in Fig. 3 can be used to excite state transitions. The excitation frequencies corresponding to the first two transitions can be determined directly from Equation (3):

$$\omega_{01} = \frac{E_1 - E_0}{\hbar} = \omega_0 - E_C/\hbar \quad (4)$$

and

$$\omega_{12} = \frac{E_2 - E_1}{\hbar} = \omega_0 - 2E_C/\hbar \quad (5)$$

From this, we can determine the anharmonicity, or difference between the  $\omega_{12}$  and  $\omega_{01}$  transitions:

$$\eta = \omega_{12} - \omega_{01} = -E_C/\hbar = -\frac{q^2}{2\hbar C_Q}. \quad (6)$$

This metric is significant since it bounds the spectral width of microwave excitation pulses, and hence sets a minimum duration for XY gate operations. Ideally, the anharmonicity (or qubit nonlinearity) would be as large as possible in order

<sup>2</sup>This may make it seem advantageous to operate at much higher frequencies in hope of reducing the challenges associated with cryogenic cooling. However, there are other disadvantages to operating at higher frequency including decreased coherence time and more challenging specifications for the control electronics.

to enable fast gates. However, there is a trade-off as larger capacitances help to suppress decoherence due to  $1/f$  charge noise [25]. Typical values for the magnitude of  $\eta/2\pi$  are in the 150–350 MHz range, with the highest coherence time devices having values towards the lower end of this range.

A projective measurement of the transmon state can be accomplished through a reflection measurement of an ancillary linear resonator that is capacitively coupled to the qubit (see Fig. 3). Assuming the readout resonator frequency is below that of the qubit, the coupling between the resonator and the qubit will cause a dispersive frequency shift of the readout resonator up or down in frequency if the qubit collapses to the  $|0\rangle$  or  $|1\rangle$  states, respectively. If the readout resonator is interrogated at its bare frequency—that is, its resonant frequency if the coupling to the qubit were removed—the dispersive frequency shift will produce a state-dependent phase shift on the interrogation signal, which can be detected and used to determine the state of the qubit.

### B. XY Control of a Transmon

Assuming a voltage drive referenced to the input of  $C_D$  and of the form

$$v_D(t) = a(t) \sin(\omega_D t - \phi_D), \quad (7)$$

the Hamiltonian of the driven circuit in the rotating frame of the drive signal<sup>3</sup> can be written [26]

$$\hat{H}_D \approx g \frac{a(t)}{2} (\cos(\phi) \hat{\sigma}_X + \sin(\phi) \hat{\sigma}_Y) - \frac{\hbar \Delta \omega}{2} \hat{\sigma}_Z, \quad (8)$$

where  $g = (C_D/C_Q) \sqrt{\hbar/2Z_Q}$  is the drive coupling strength,  $Z_Q = \sqrt{L_{10}/C_Q}$  is the qubit impedance,  $\Delta\omega = \omega_D - \omega_0$  is the offset in drive frequency from the resonant frequency of the qubit, and

$$\hat{\sigma}_X = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}, \quad \hat{\sigma}_Y = \begin{bmatrix} 0 & -j \\ j & 0 \end{bmatrix}, \quad \hat{\sigma}_Z = \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix} \quad (9)$$

are the Pauli spin matrices.

It can be shown that this Hamiltonian produces a time evolution corresponding to a rotation of the qubit state about a vector

$$\begin{bmatrix} n_x \\ n_y \\ n_z \end{bmatrix} = \frac{1}{\sqrt{g^2 a^2(t) + \hbar^2 \Delta \omega^2}} \begin{bmatrix} g a(t) \cos(\phi_D) \\ g a(t) \sin(\phi_D) \\ -\hbar \Delta \omega \end{bmatrix}, \quad (10)$$

and at a frequency

$$\omega_r = \frac{\sqrt{g^2 a^2(t) + \hbar^2 \Delta \omega^2}}{\hbar}. \quad (11)$$

Referring to equations (10) and (11), we can identify three distinct control knobs,  $a(t)$ ,  $\phi_D$ , and  $\Delta\omega$ . Moreover, it is apparent that  $\Delta\omega$  affects the Z component of the rotation axis, whereas the other two degrees of freedom affect its XY projection.

<sup>3</sup>This is similar to a baseband analysis. Here, we have rotated the coordinate system at the carrier frequency to remove dynamics and have assumed that higher frequency components will average out through the integration that occurs when the Schrödinger equation is solved.

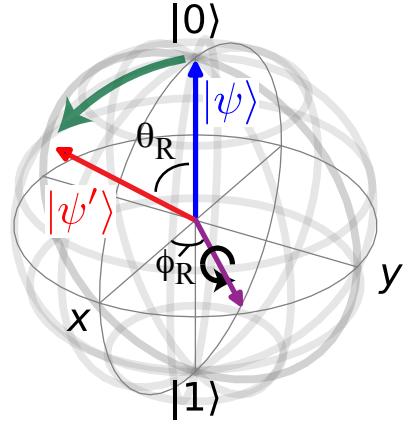


Fig. 5. Definition of rotation angles,  $\theta_R$  and  $\phi_R$

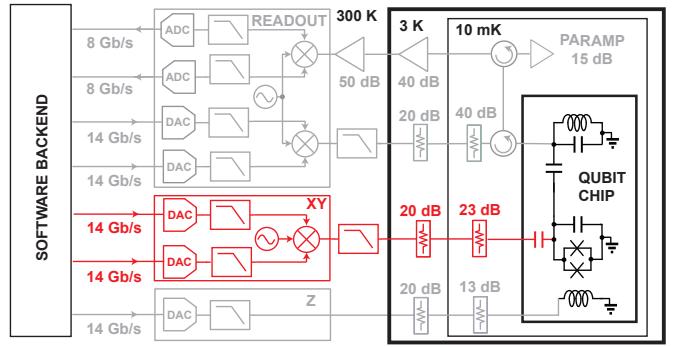


Fig. 6. Block diagram showing standard control and readout hardware, with XY control hardware highlighted.

Since it is desirable to only induce rotations about an axis in the XY plane of the Bloch sphere (Z rotations can be carried out in software [27]), the qubit should nominally be driven on resonance<sup>4</sup> ( $\Delta\omega = 0$ ). In this case, the axis of rotation is defined by the carrier phase,  $\phi_R = \phi_D$ , and the angle of rotation is proportional to the integrated envelope amplitude

$$\theta_R = \frac{g}{\hbar} \int_{t_0}^t a(t') dt', \quad (12)$$

as defined in Fig. 5.

A block diagram of a standard control and readout system appears in Fig. 6 with the XY control portion highlighted. The XY signals are generated using a pair of 1 Gb/s 14-bit DACs whose outputs drive the LO ports of an IQ mixer. Single sideband mixing is typically employed, with LO and RF signals in the 4–8 GHz frequency range. The upconverted output is heavily attenuated at both the 3-K and 10-mK stages of the cryogenic system. In the remainder of the paper, we consider simplifying and integrating this system in a manner such that it can be placed on the 3-K stage of the cryostat.

<sup>4</sup>It should be noted that the more complete description including  $\Delta\omega$  above allows describing the behavior that occurs if the drive signal is slightly detuned from the qubit frequency.

### III. XY CONTROLLER REQUIREMENTS

Techniques to accurately control and measure the state of a quantum processor with on the order of a million qubits will be required to enable fault tolerant quantum computing [8]. As a first step towards such a quantum control and measurement system, we consider the implementation of a cryogenic pulse modulator IC optimized to generate XY control signals. Here we summarize some of the key design specifications of this circuit.

#### A. Physical Temperature

We first consider the physical temperature at which to thermalize the quantum controller, as this is critical in driving other specifications. On the one hand, it is desirable to place the controller as close as possible to the quantum processor so as to minimize interconnects. In fact, if there were no other considerations, it would be appropriate to co-integrate the classical control with the quantum chip and researchers are currently exploring both 3D packaging approaches [28] and integrated control and readout architectures [11], [12], [13] as steps to make this a reality.

However, as discussed above, superconductive quantum processors must be thermalized to temperatures in the vicinity of 10 mK. Unfortunately, the efficiency of cryocoolers is fundamentally limited by the laws of thermodynamics to  $\eta \leq T_{\text{BASE}} / (T_A - T_{\text{BASE}})$ , where  $T_{\text{BASE}}$  and  $T_A$  are the base and room temperatures, respectively [29]. So, the efficiency in removing heat at 10 mK cannot be more than about 0.003%. In reality, the efficiency of the state-of-the-art dilution refrigerators employed for cooling to 10 mK is orders of magnitude lower than the theoretical Carnot efficiency. In fact, typical systems can handle less than 15  $\mu\text{W}$  at 10 mK despite drawing more than 10 kW of wall power [30], [31]. As such, thermalization of CMOS integrated control electronics to the same stage as the quantum IC is not viewed as a viable approach.

At the other extreme, we could consider placing the quantum controller at room temperature, as done today. The advantage here is that power consumption of the electronics is not critical and existing electronics could be miniaturized and scaled. However, scaling of the interconnects between the room temperature electronics and the 10 mK stage is very challenging, as these lines must be able to support microwave transmission with high isolation while presenting as low of a thermal load as possible. As such, it is not believed to be scalable to the levels required to control a quantum processor with a million or more qubits.

A more tractable solution is to thermalize the control electronics in the range of 3-to-4 K and use superconductive transmission lines to couple the control signals down to the 10 mK stage [14], [16]. By using superconducting interconnects, it is possible to achieve excellent electrical and thermal performance in a small cross sectional area [32]. Below, we will assume that the quantum control electronics are thermalized in the range of 3-to-4 K.

#### B. Power Consumption

While much higher than at 10 mK, the power handling capability of the 4 K stage of a typical closed-cycle refrigeration system is still limited. For near-term systems, which will employ standard pulse-tube cryocoolers, the total dissipation at 4 K will be limited to just 2 W at 4 K [33]. As this power budget must include any thermal load associated with cabling, the actual power available for electronic consumption is lower. As such, a reasonable near term power budget for the control and readout electronics is 1 W.

For a scaled system, one could envision building a much larger refrigerator and employing more advanced cooling techniques. For instance, helium liquifiers can be used to increase the capacity to around 1 kW [34], or about 1 mW/qubit at the million qubit level. As this power consumption must be shared between any incoming cabling (from 300 K), Z-control electronics, and the readout electronics (which can be multiplexed by 5-10x), a reasonable long term limit for the dissipation of the control electronics is 250  $\mu\text{W}$  per qubit. For this proof of concept work, which is being carried out without cryogenic simulation models, we relax this specification by a factor of ten to 2.5 mW, with the expectation that the power consumption can be further optimized in a future design.

#### C. Frequency Range

Typical transmon qubits have transition frequencies in the 4–8 GHz frequency range. As such, we seek to cover this full band with our initial prototype device. However, it may be desirable for a future device to only operate only over some sub-set of this frequency range.

#### D. Gate Fidelity and Error Rates

The remainder of the specifications are all performance related and, as such, a metric to benchmark performance is required. Fidelity and error rates provide such metrics. Gate fidelity is a measure of how close the effect of an applied gate is to that of the desired unitary and can be limited by a number of factors including control errors, noise, decoherence, etc. Formally, we can define the gate fidelity of a single qubit gate, averaged over all pure input states as [35]

$$\mathcal{F}_G \equiv \frac{\text{Tr} \left\{ U_{\text{Ideal}}^\dagger U U^\dagger U_{\text{Ideal}} \right\} + \left| \text{Tr} \left\{ U_{\text{Ideal}}^\dagger U \right\} \right|^2}{6}. \quad (13)$$

The first term,  $\text{Tr} \left\{ U_{\text{Ideal}}^\dagger U U^\dagger U_{\text{Ideal}} \right\}$  evaluates to two in the case that the realized operator is unitary, but is smaller in the case where the matrix is not unitary due to matrix truncation (e.g., if there is leakage to the  $|2\rangle$  state). In a computation, the average error per step is simply  $1 - \mathcal{F}_G$ .

The degree of redundancy required for fault tolerant quantum computing is strongly dependent up on error rates [8]. In order to reduce this to practical levels, the error rates should be reduced as far as possible. Here, we target an overall error rate of 0.01%, which is consistent with state of the art performance [9]. To achieve this, we will limit individual error contributors to an order of magnitude lower error rates.

### E. Noise on the Drive Line

Noise at the qubit transition frequency ( $\omega_{01} = 2\pi f_{01}$ ) causes decoherence. An available noise power spectral density of  $S_a(f_{01}) = kT_e$  at the drive port at frequency  $f_{01}$  leads to transitions between the  $|0\rangle$  and  $|1\rangle$  states at a rate [36]

$$R_{\uparrow\downarrow} = 2\pi \frac{T_e(f_{01})}{T_{\text{Photon}}} \Delta f, \quad (14)$$

where  $\Delta f = f_0/Q_D$ ,  $Q_D = (C_D/C_Q)^2 (Z_Q/Z_0)$  is the quality factor of the qubit due to the drive circuit,  $T_{\text{Photon}} = \hbar\omega_{01}/k$  is the effective temperature of a photon at the qubit frequency, and  $Z_0$  is impedance of the drive port. The noise spectral density  $S_a = kT_e$  must be kept low enough such that  $R_{\uparrow\downarrow}$  is less than other decoherence channels in the system, such as losses from materials imperfections. This usually means ensuring that the noise temperature seen looking back into the drive line is kept well below the effective temperature of a photon at the drive frequency. As such, it is important both to include attenuation at 10 mK on the drive line and also to minimize noise generated by the XY controller.

### F. Spectral Content

Also related to gate fidelity is the spectral content of the qubit drive signal. Due to the finite coherence time of a qubit (on the order of 10-to-100  $\mu\text{s}$  for transmon qubits) fast gates are desired. However, due to the finite separation between the  $\omega_{01}$  and  $\omega_{12}$  transition frequencies, it is important to ensure that the drive signal does not introduce leakage to higher order levels. In optimizing the control waveforms, one has to carefully balance the trade-off between speed and leakage. Typical pulse envelopes include Gaussian and raised cosine shapes and advanced techniques such as derivative removal by adiabatic gate (DRAG) are used regularly to further reduce the pulse duration beyond what can be achieved using envelope shaping alone [26], [37]. In this work, we limit our pulse generation capabilities to simple symmetric pulses without derivative compensation.

### G. Amplitude Control

The drive amplitude sets the range of rotations that can be carried out for a given pulse duration. As discussed in Section II-B, a drive pulse on resonance with the qubit produces a rotation proportional to the integrated envelope amplitude (see Equation (12)). The largest rotation required in a practical quantum algorithm is a  $\pi$ -pulse. For a raised cosine envelope, the peak amplitude required to achieve this rotation is

$$A_{\text{PK},\pi} = 2\pi \frac{\hbar}{g\tau_g}. \quad (15)$$

For typical values of  $g$ , the required peak amplitude for a 15 ns pulse is on the order of 100  $\mu\text{V}$  (peak available power of -76 dBm). In general, we want to be able to drive with pulses several times larger to allow both shorter  $\pi$ -pulses and also to carry out rotations well beyond  $180^\circ$ . As such, it is desirable that the XY controller be able to drive pulses on the order of 1 mV at the reference plane of the qubit drive port.

The signal at 4 K must be about an order of magnitude larger to account for the attenuation on the drive line that is required at 10 mK to reduce the thermal noise floor.

Amplitude resolution is also important, since any error in pulse amplitude will translate to an over or under rotation and contribute to gate error rates. An error in a rotation of  $\Delta\theta_R$  produces an average error rate of

$$\epsilon_{\Delta\theta_R} \approx \frac{\Delta\theta_R^2}{6}. \quad (16)$$

To keep error rates due to integrated envelope amplitude errors to below  $10^{-5}$ , it is necessary that XY rotation angles are controlled to better than  $0.5^\circ$ . This means that the integrated  $\pi$ -pulse amplitude must have an accuracy better than 0.15%. A resolution of 11 bits in the integrated envelope amplitude is required to provide the required dynamic range<sup>5</sup>.

### H. Carrier Phase Control

A carrier phase error of  $\Delta\phi_D$  on an XY gate will lead to a rotation around the wrong axis, resulting in an average gate error rate of

$$\epsilon_{\Delta\phi_D} = \frac{2}{3} \Delta\phi_D^2 \sin^2\left(\frac{\theta_R}{2}\right) \left(1 - \frac{\Delta\phi_D^2}{4} \sin^2\left(\frac{\theta_R}{2}\right)\right). \quad (17)$$

For small phase errors, it can be shown that the worst case average error rate will occur for  $\pi$ -pulses. To ensure the contribution of phase to the error rate is below  $1e^{-5}$  for all XY rotations, it is necessary that the carrier phase be controlled to better than  $0.25^\circ$ .

### I. ON/OFF Ratio

Carrier leakage causes initialization errors and reduces gate fidelity. This effect is most significant for direct conversion pulse modulation architectures, for which the leakage tone is on-resonance with the qubit. To understand the effect on initialization, we consider the case in which the qubit is reset to the ground state at  $t = 0$  and idles for a time  $\Delta t$  prior to being intentionally driven. Such a delay is typical to permit settling of the qubit after initialization. Under this scenario, a leakage tone with amplitude  $A_L$  produces a persistent XY rotation, resulting in a  $|1\rangle$  state population due to leakage of  $P_L\{|1\rangle\} = \sin^2(gA_L\Delta t/2\hbar)$ , which for small enough  $A_L\Delta t$  products simplifies to  $P_L\{|1\rangle\} \approx (gA_L\Delta t/2\hbar)^2$ . So, defining the specification for ON/OFF ratio in terms of the peak pulse amplitude required for a  $\pi$ -pulse ( $A_{\text{PK},\pi}$ ) and assuming raised cosine pulse shaping, we find

$$R_{\text{ON/OFF}} \equiv \frac{A_{\text{PK},\pi}}{A_L} \approx \pi \frac{\Delta t}{\tau_g} \frac{1}{\sqrt{P_L\{|1\rangle\}}}, \quad (18)$$

where  $\tau_g$  is the gate time and  $P_L\{|1\rangle\}$  is the initialization error due to leakage. As a numerical example, if  $T_g = 15$  ns, achieving an initialization error of 0.01% with a settling time of 500 ns requires an ON/OFF ratio of 80 dB.

<sup>5</sup>It should be noted that this is not the dynamic range that must be achieved on a pulse to pulse basis, but rather that that a design should be able to achieve over its entire configuration range. For typical operation, where the largest signal one would apply is a  $\pi$ -pulse, an order of magnitude dynamic range is acceptable.

Another important metric is the  $|1\rangle$  state population which is driven by carrier leakage over the course of a coherence time, an upper limit for which can be determined by substituting  $T_1$  for  $T_g$  in equation (18). A reasonable limit to this value is 5% for a typical  $T_1$  value of  $20\mu\text{s}$ . Reaching this value requires a slightly higher ON/OFF ratio of  $85\text{dB}$ . While this is a stringent specification, it should be feasible to meet this using modern cancellation techniques due to the narrowband nature of the carrier leakage.

### J. Summary

The performance specifications of the XY controller are summarized in Table I.

## IV. CIRCUIT DESIGN

A conceptual block diagram explaining the waveform generation approach appears in Fig. 7. A vector modulation based architecture has been chosen to enable simultaneous control of the envelope amplitude and carrier phase. Symmetric envelopes are generated using an array of current sources which are sequentially enabled and disabled with the appropriate timing to generate a symmetric staircase of current, as shown in Fig. 7. The current waveform is then lowpass-filtered to create a smooth envelope. By controlling the individual weights of each of the current-mode sub-DACs, a wide range of symmetric envelopes can be realized. After low-pass filtering, the envelope currents pass through a polarity switch, are up-converted to the carrier frequency, and the two quadratures are then combined to create the output pulse.

This architecture has been chosen as a trade-off between power consumption, performance, and robustness to the inherent uncertainty associated with designing for operation at 3-K, where foundry design models are currently unavailable. Several research groups are currently investigating the cryogenic performance of nanometer CMOS technology (e.g., [20], [21]) and it is known that threshold voltages, transconductances, and subthreshold slope all increase with cryogenic cooling. Unfortunately, so does mismatch, particularly in the sub-threshold regime [38]. A critical feature of the envelope generation approach is guaranteed monotonicity, even if the sub-DACs display non-linearity or non-monotonicity.

A block diagram of the implemented IC appears in Fig. 8. The circuit consists of a pair of baseband envelope DACs, which drive a vector modulator. The clock port of the DACs as well as the LO ports of the vector modulator are buffered to minimize the external RF power required to drive the chip. A small digital memory is incorporated to store configuration parameters and implement a rudimentary 4-bit XY instruction set. By integrating such an instruction set on-chip, the overall digital I/O rate required to operate the chip is greatly reduced, thereby resulting in a significant savings in power and system complexity. Finally, a trigger line is included to initialize a pulse.

A schematic diagram of one of the envelope DACs appears in Fig. 9. The circuit contains a bank of eleven 8-bit current-mode sub-DACs, whose outputs are combined in the current domain and lowpass filtered before being fed to the

modulator stage. Each DAC is constructed using a binary-weighted current mirror circuit, with the smallest unit cell being a minimum feature-size transistor. While linearity and monotonicity could be improved by using larger transistors and thermometer coding, respectively, these properties were sacrificed to reduce dynamic power consumption. The bank of DACs share a common reference current ( $I_N$ ), which has 8-bits of programmability. This reference current is biased from a constant current source ( $I_P$ ) which has an additional 6-bits of reconfigurability. The configuration bits for each of the sub-DACs as well as the master reference current for the sub-DACs ( $I_N$ ) are configured by the sixteen wavefrom configuration memory, with the desired waveform selected by the 4-bit instruction interface ( $\text{SEL} < 0 : 3 >$ ).

A current waveform of the form shown in Fig. 7 is generated by enabling each of the 11 current sources in the appropriate sequence. The enable signals for this operation are generated by the pulse controller shown in Fig. 9. The pulse controller is a shift-register based design in which the enable signal propagates through the shift register after a trigger pulse has been detected. In order to minimize the power consumption of this block, the clock signal is gated such that each flip-flop is only clocked if its output is to transition during a given clock cycle. The controller was designed to accept clock signals in excess of  $2\text{GHz}$  and produces pulses that are 21 clock cycles in duration.

A schematic diagram of the passive-mixer-based vector modulator appears in Fig. 10. A passive mixer has been selected to avoid introducing noise of a non-thermal nature during the mixing process and the circuit has been designed as a trade-off between power consumption and bandwidth. Each LO signal is transformer coupled to a fully differential gain block which helps to improve common-mode rejection. The differential output of this cell is further amplified by a standard cell based pseudo differential amplifier chain which is sized to drive the mixer. The LO paths were optimized to be driven with LO signals below  $50\mu\text{W}$ .

The IF currents from each envelope DAC are routed through one arm of a polarity switch—required to achieve a full  $360^\circ$  of carrier phase control—through the mixer, and back through the other arm of the polarity switch back to ground. The output of the mixer is transformer coupled to the output, where the two quadratures are combined in the voltage domain. Finally, all three transformers feature bondpad side capacitive tuning networks which can be used to optimize coupling over the full  $4\text{--}8\text{GHz}$  frequency range.

In combination, the number of configuration bits available to tailor the shape and amplitude of the control pulses exceeds that required to meet the specifications set out in Section III. However, the circuit was over-designed in order to ensure robustness against changes with cryogenic cooling. In the future the power could be reduced by lowering the resolution. In addition, for simplicity, no provision was made to null LO leakage, as it can be canceled off-chip and was not viewed as a fundamental limitation. This functionality could be added in a future design.

TABLE I  
KEY SPECIFICATIONS FOR CRYOGENIC XY CONTROLLER

	Phys. Temp.	RF Frequency	Envelope	Env. Amp	Pulse Duration	Amp. err.	Phase err	Inst. Set	AC+DC Power
Prototype Goal	3-to-4.2 K	4-to-8 GHz	Symmetric	>10 mV	10-to-30 ns	< 0.15%	< 0.5°	4-bit	<2.50 mW
Long-term Goal	3 K	TBD	DRAG	> 1 mV	<10 ns	< 0.15%	< 0.5°	TBD	<250 μW

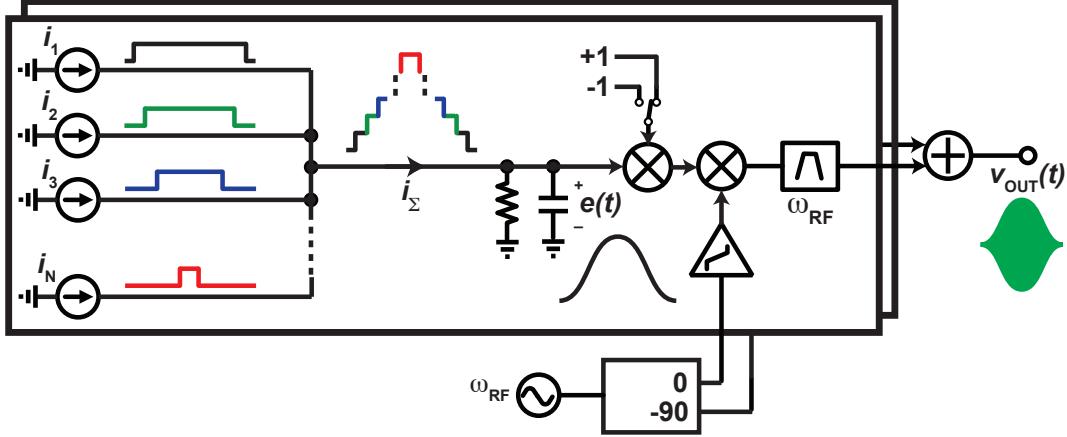


Fig. 7. Block diagram of the proposed pulse generation approach.

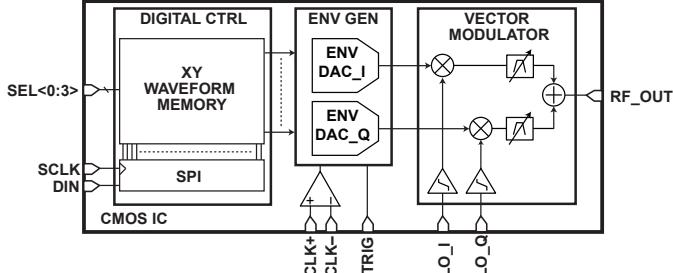


Fig. 8. Block diagram of the cryo-CMOS pulse generator.

## V. RESULTS

The pulse modulator was implemented in a 28-nm CMOS technology and a die photo appears in Fig. 11(a). The chip was packaged in a module for testing. As shown in Fig. 11(b), the die was mounted within a cutout in a printed circuit board so as to minimize bondwire lengths. A photograph of the module appears in Fig. 11(c).

Prior to characterizing the IC, we first performed baseline measurements of test structures for each of the different transistor flavors that are available in the 28-nm CMOS process. This process was carried out to ensure that the temperature dependence of devices with different doping profiles and polarities is similar to that previously reported for a single minimum-length 28-nm NMOS device [39]. These measurements were carried-out on wafer at 300 and 7-K and key parameters such as threshold voltage, sub-threshold slope, extrinsic transconductance ( $G_m$ ), and unity current gain cutoff frequency ( $f_t$ ) were extracted and display similar trends among the different device families. On average, the threshold voltages increased by a factor of 40% whereas the subthreshold

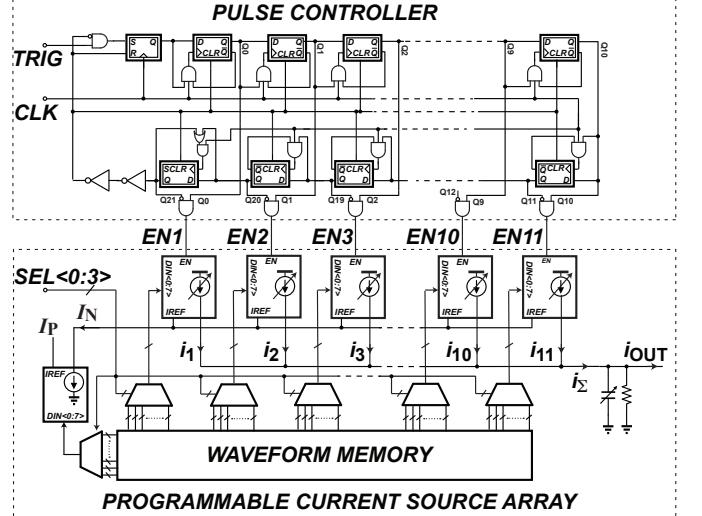


Fig. 9. Simplified schematic diagram of one of the envelope DACs.

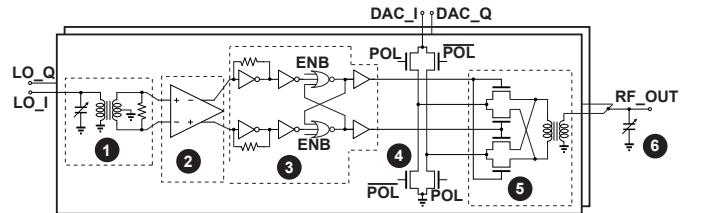


Fig. 10. Schematic diagram of the vector modulator.

slope, extrinsic transconductance, and unity current gain cutoff frequency improved by factors of 2.8, 2, and 1.8, respectively.

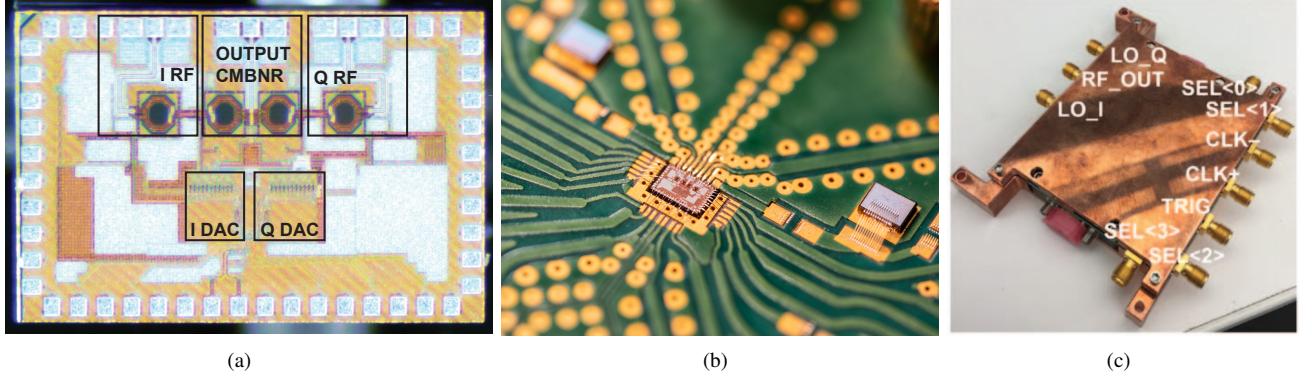


Fig. 11. (a) Die micrograph. The chip measures 1.1 mm by 1.6 mm. (b) Photograph of packaged integrated circuit. The chip was mounted within a pocket of a printed circuit board to minimize the RF bondwires. (c) Photograph of module used for testing.

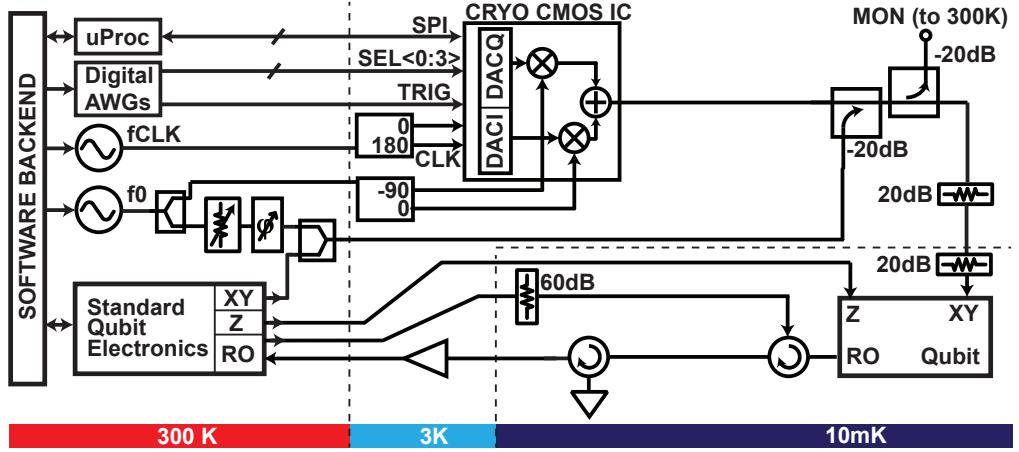


Fig. 12. Simplified block diagram of the test setup used for quantum control experiments.

It is interesting to note that these changes are consistent for both PMOS and NMOS devices. The full set of extracted parameters is provided in Table III.

After evaluating the transistor performance, the low-temperature operation of the chip was evaluated through a series of quantum control experiments. To facilitate these measurements, the packaged IC was mounted on the 3-K stage of a commercial dilution refrigerator and interfaced to a qubit mounted on the 10 mK stage of the system. The qubit employed for this experiment was a transmon that is part of a 5-qubit processor and is characterized by an anharmonicity parameter,  $\eta/2\pi \approx -330$  MHz. For all measurements, the other four qubits were tuned to be as far away in frequency as possible so as to make their presence inconsequential.

A detailed block diagram of the test setup appears in Fig. 12. The module containing the CMOS IC was mounted on the 3-K stage of the refrigerator, along with 90- and 180-degree hybrids, which were used to interface to the LO and clock ports of the chip, respectively. The LO and clock signals were generated at room temperature using commercial synthesizers.

The LO signal was split at room temperature to enable feedforward cancellation of LO leakage to the RF output port of the cryo-CMOS IC module. Vector modulation of the leakage cancellation tone was achieved using a digital step

attenuator followed by a digital phase shifter. The amplitude and phase shifted cancellation signal was then combined RF output using a 20-dB coupler, mounted on the 3-K stage of the cryostat. In concert with a power combiner added after the phase shifter, this coupler also provided a mechanism to inject a standard XY control signal, thereby enabling baseline measurements.

A second 20-dB coupler was employed at the 3-K stage to couple a small fraction of the RF output back to room temperature. This weak monitor signal was further amplified by approximately 50 dB (not shown), such that it could be viewed on an oscilloscope for debugging purposes.

Finally, the RF output was attenuated by 40 dB and connected to the XY port of the qubit. The Z and readout terminals of the qubit were connected to standard Z and readout electronics chains to complete the analog portion of the measurement setup.

The SPI port of the chip was interfaced to through a microprocessor, allowing for simple integration into a software stack. Finally, the trigger and word select lines of the CMOS IC were driven by a bank of AWGs, configured to operate with binary outputs. All instruments were under the control of a standard qubit software stack, with the necessary drivers added to incorporate the CMOS IC within a standard experimental

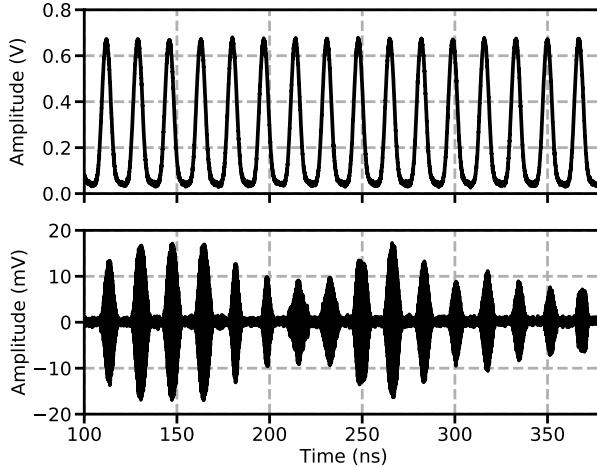


Fig. 13. Example time domain trigger (top) and pulse (bottom) waveforms, measured at 300 K. The chip was initialized with sixteen different waveforms and stepped through using the select lines. For these measurements, the chip was driven with a 2 GHz sample clock. A cable loss of approximately 5 dB has not been de-embedded from the measurement results.

flow.

Once the setup was complete, the system was cooled to base temperature. The qubit was calibrated using the standard room temperature control and readout electronics. Next a series of experiments were employed to evaluate the performance of the IC and compare it to that of conventional room temperature control electronics, as detailed below. The CMOS IC was powered down for all baseline measurements. Unless otherwise stated, all measurements were taken with the qubit tuned to 5.6 GHz.

#### A. Preliminary Room Temperature Measurements

Prior to cooling the system down, a set of measurements was carried-out to ensure that the CMOS IC was behaving as expected. For these measurements, a coaxial cable was connected directly to the output of the module and the performance was monitored both on an oscilloscope and a spectrum analyzer. The circuit was found to be operational for clock and LO signals in the range of 0.5-to-3 GHz and 4-to-8 GHz, respectively. The power required to drive the inputs of the clock and LO hybrids was less than  $-20$  dBm at 2 GHz and  $-10$  dBm at 5.6 GHz, respectively. Example time-domain waveforms appear in Fig. 13. For this measurement, the waveform memory was initialized with a set of sixteen different waveforms and the select lines were used to rotate between these different instructions. Clock and carrier frequencies of 2 GHz and 5.6 GHz were used.

#### B. LO Leakage Cancellation

Prior to performing quantum control experiments, we first nulled the LO leakage using the cancellation path shown in Fig. 12. The qubit was first initialized to the ground state and then allowed to idle for a period,  $\tau$ , before its state was

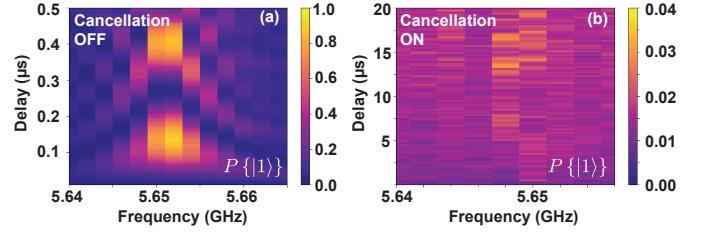


Fig. 14. Effect of local oscillator feedthrough. (a) When the LO cancellation circuit is off, the qubit is driven by the LO leakage. (b) With the LO cancellation circuit on, nearly all  $|1\rangle$  state population is suppressed.

measured<sup>6</sup>. The magnitude and phase of the cancellation tone were then varied to minimize the measured  $|1\rangle$  state population. The resolution employed for amplitude and phase control was 0.25 dB and  $1^\circ$ , respectively. We found that the nominal settings depended strongly on the impedances presented by the LO and RF ports of the IC (which could be varied through the transformer tuning capacitors). However, we also determined that these values were repeatable and stable on timescales of several days. As such, it appears feasible to implement leakage nulling in a future version of the chip.

Example results in which the cancellation is turned OFF and ON are shown in Fig. 14. For these measurements, the qubit was tuned to 5.65 GHz. With the cancellation disabled, Rabi oscillations were observed with a period of approximately 300 ns, indicating the presence of significant LO leakage. This is not surprising since the RF and LO bonds were in close proximity (see Fig. 11(b)). On the other hand, with the cancellation enabled, we found that the LO leakage was reduced to the level that a  $|1\rangle$  population of less than 4% was observed after 20  $\mu$ s of idling. This level of unintended drive is acceptable, as it corresponds to an error of less than 0.01% on the timescale of a gate operation.

#### C. Amplitude Control

Next, we performed a Rabi oscillation experiment in order to evaluate the feasibility of deterministically inducing an XY rotation using the CMOS IC. The protocol for this experiment, described in Fig. 15(a) and 15(b), was to initialize the qubit to the  $|0\rangle$  state, excite it with a raised cosine pulse of 21-ns in duration, and then measure its state. The experiment was repeated for a wide range of envelope amplitudes and 5,000 statistics were taken for each setting. While the measured statistics would nominally be plotted against the programmed envelope amplitude settings, we found that the DACs were both non-monotonic and nonlinear when operated at cryogenic temperatures. As such, we made an independent measurement of the pulse amplitude as a function of digital setting by using a spectrum analyzer to measure an amplified version of the signal at the monitor port (see Fig. 12).

<sup>6</sup>It may seem like a more direct approach one could take to null the LO feedthrough is to look at it on a spectrum analyzer, taking advantage of the monitor port that we have built into our test setup. However, we found that this was actually an ineffective method that did not produce nominal settings. We believe this is either due to the finite directivity of the directional coupler or secondary paths through which the LO signal leaked to the spectrum analyzer.

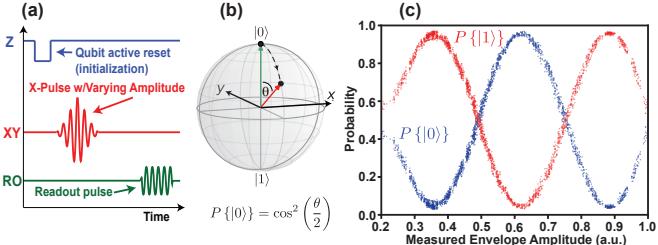


Fig. 15. Single-pulse Rabi amplitude experiment. (a) Experimental protocol. (b) Illustration of state trajectory on the Bloch sphere. (c) Experimental measurement results. High visibility Rabi oscillations were observed.

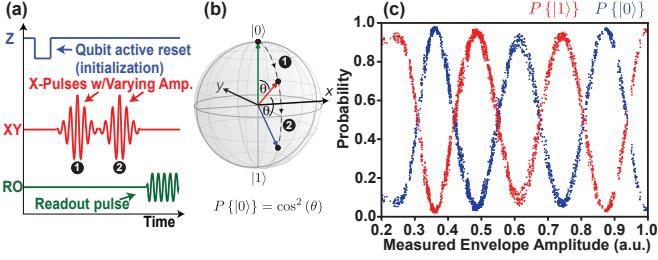


Fig. 16. Two-pulse Rabi amplitude experiment. (a) Experimental protocol. (b) Illustration of state trajectory on the Bloch sphere. (c) Experimental measurement results. High visibility Rabi oscillations were observed.

The measured state probabilities plotted as a function of measured envelope amplitude appear in Fig. 15(c). The data reported on this figure were acquired by sweeping the DAC reference current ( $I_N$ ) through its full range for eleven different values of  $I_P$ . Data is not shown for x-axis values below 0.22 since there was insufficient SNR to measure the envelope amplitude using the spectrum analyzer. The results in Fig. 15(c) show the expected behavior: the maxima of the  $|0\rangle$  and  $|1\rangle$  state probabilities are consistent with separately measured  $|0\rangle$  and  $|1\rangle$  state readout error rates of 2.4% and 6.8%, respectively.

A second Rabi experiment was conducted to further explore the ability to drive XY rotations. In this experiment, described in Fig. 16(a) and 16(b), the same protocol is employed except the qubit is excited with an extra pulse before being measured. As such, the qubit should experience a factor of two larger rotation. As expected, the Rabi oscillations in Fig. 16(c) display about a factor of two higher frequency of oscillation in comparison to the previous case in which the qubit was only excited by a single pulse.

#### D. Coherent Control and Fast Switching

The previous experiment showed that it is possible to accurately drive rotations using the cryo CMOS IC, but it did not probe the ability to control the axis of rotation. To test the coherent control and fast-switching capabilities of the chip, a three-pulse experiment was carried out. The experimental protocol is described in Figs. 17(a) and 17(b). The qubit was first initialized to the ground state and then excited by a series of three pulses. The first and third pulses were  $X$  pulses of varying amplitude,  $\theta_A$ , whereas the middle pulse was a  $\pi$ -pulse

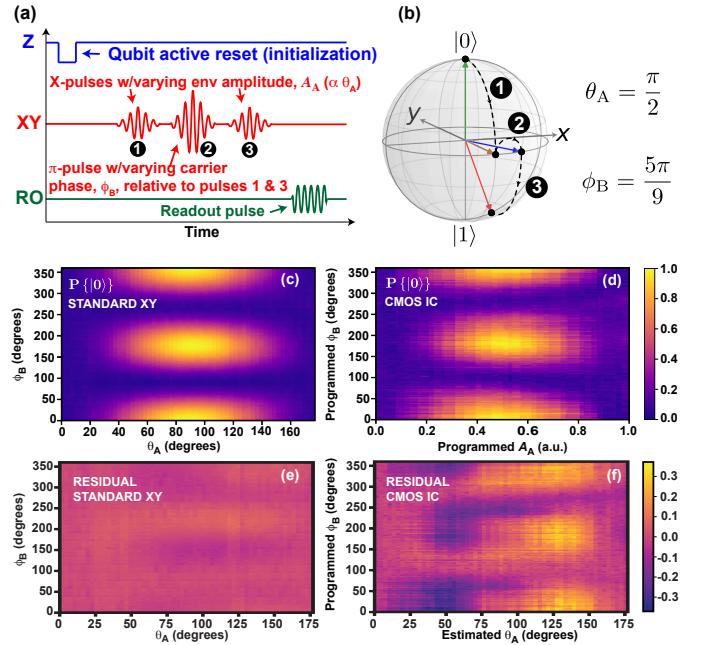


Fig. 17. Three pulse experiment used to evaluate fast switching and phase coherent features of the IC. (a) Experimental protocol. (b) Example qubit trajectory for  $\theta_A = \pi/2$  and  $\phi_B = 5\pi/9$ . (c) Measured  $P\{|0\rangle\}$  for standard XY control electronics. (d) Measured  $P\{|0\rangle\}$  for cryo-CMOS XY controller. (e) Residual error for standard XY controller. (f) Residual error for cryo-CMOS XY controller. No calibration was performed for the envelope amplitude or carrier phase generated by the cryo-CMOS controller and it is believed that the residual could be reduced significantly if a calibration were carried out.

with varying carrier phase,  $\phi_B$ . After the third pulse, the state of the qubit was measured.

It can be shown that the unitary evolution that results from this pulse sequence ideally leaves the qubit in a state such that if measured, the probability of being in the  $|0\rangle$  state depends upon both  $\theta_A$  and  $\phi_B$ :

$$P\{|0\rangle\} = 4 \cos^2(\phi_B) \sin^2\left(\frac{\theta_A}{2}\right) \cos^2\left(\frac{\theta_A}{2}\right). \quad (19)$$

As such, the experiment should produce a maximum probability of returning  $|0\rangle$  when  $\phi_B = 0, \pi$  and  $\theta_A = \pi/2, 3\pi/2$ .

The experiment was carried-out using both the standard control electronics and the CMOS IC and the results appear in Figs. 17(c) and 17(d), respectively. In both cases, the general structure is consistent with expectation, however the CMOS IC results appear noisier than those of the standard control electronics. However, this is explained by the fact that the envelope amplitude and carrier phase generated by the CMOS IC were not calibrated in this experiment. The residual error obtained by taking the difference between the measured and ideal results (i.e., equation (19)), is shown for the baseline measurement and the CMOS IC in Figs. 17(e) and 17(f), respectively. Referring to the residual error for the CMOS IC, it is clear that there is structure that could be calibrated out.

#### E. Qubit Relaxation Time ( $T_1$ )

The relaxation time,  $T_1$ , for the qubit was measured using the CMOS IC as well as the baseline system and the results

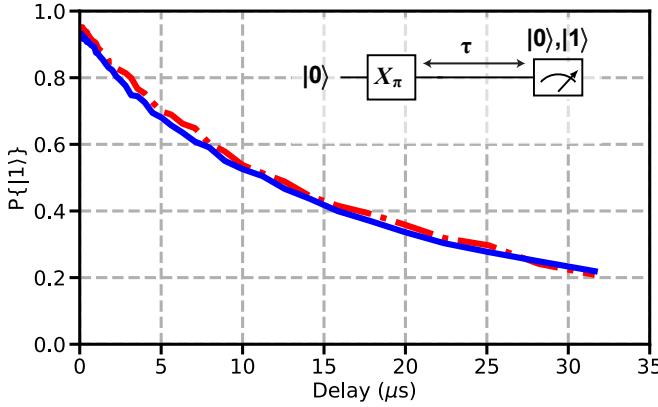


Fig. 18. Qubit relaxation time measurement. The relaxation time measured using the CMOS IC (blue line) and the standard control system (dashed red line) were found to be  $17.8 \mu\text{s}$  and  $18.3 \mu\text{s}$ , respectively. It is believed that these measurements are consistent to within the measurement repeatability.

were compared to ensure that the CMOS IC was not introducing additional noise that could drive  $\omega_{01}$ , thereby reducing  $T_1$ . For this experiment, the qubit was reset to the  $|0\rangle$  state, excited to the  $|1\rangle$  state with a  $\pi$ -pulse, and a state measurement was made after a delay,  $\tau$ . 5000 statistics were gathered for each value of  $\tau$ .

Results are plotted in Fig. 18. As expected, we observed that the qubit relaxed exponentially in both cases. The measured values of  $T_1$  were  $18.3 \mu\text{s}$  and  $17.8 \mu\text{s}$  when using the standard control electronics and the cryo-CMOS IC, respectively. It is believed that these numbers are within the measurement/fitting error, and thus that there was no evidence of any impact on qubit relaxation due to broadband noise.

#### F. Two-state population

The envelope quality (spectral width) was also evaluated. In this experiment, the qubit was first reset and then excited with a sequence of 200  $\pi$ -pulses. Since any energy at the  $\omega_{12}$  transition frequency will drive this undesired transition, the application 200  $\pi$ -pulses enables will result in substantial  $|2\rangle$  state population if the  $\omega_{12}$  transition is even weakly excited. After the final pulse, the state was measured using a readout scheme that permitted distinguishing the  $|0\rangle$ ,  $|1\rangle$  and  $|2\rangle$  states. The experiment was repeated for pulse durations ranging from 7.6–70 ns, corresponding to a clock frequencies in the range of 0.3–2.75 GHz and 5000 statistics were gathered at each point. A nominally raised cosine envelope shape was employed and the amplitude for a nominal  $\pi$ -pulse was determined independently at each clocking frequency.

The  $|2\rangle$ -state measurement results appear in Fig. 19 along with the measurement noise floor of 0.57%, which was limited by the separately measured readout infidelities. The  $|2\rangle$ -state population was found to be negligible for pulse durations of approximately 15 ns or longer. However, for faster pulses, excitation of the  $\omega_{12}$  transition was observed, with a maximum  $|2\rangle$  state population of just over 2.5%, or 0.0125% per pulse, for a pulse duration of 7.6 ns. The behavior is consistent with expectation, given the relatively large anharmonicity of

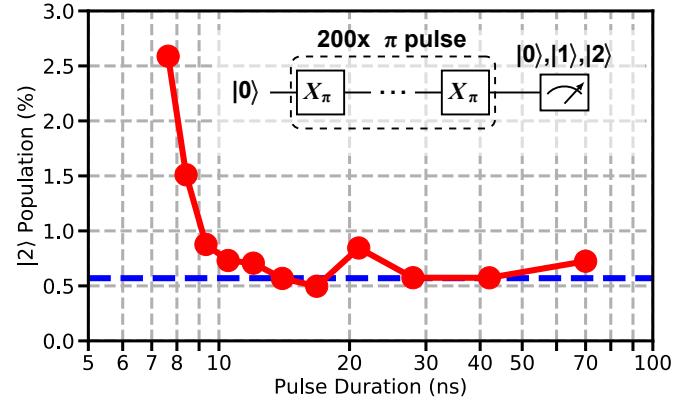


Fig. 19. Two-state population as a function of pulse duration (solid red line) and two-state measurement noise floor (dashed blue line). Negligible  $|2\rangle$  population was observed for gate times as short as 15 ns.

TABLE II  
COMPARISON OF CMOS IC TO STATE-OF-THE-ART QUANTUM CONTROL SYSTEM

	Conventional Control	Cryo-CMOS IC
Form Factor	Rack Mount	Integrated Circuit
Physical Temp	300 K	3 K
Update Rate	1 Gs/s	1 Gs/s
Instruction Set	N/A	4-bit
Digital Data Rate	28 Gb/s	<0.5 Gb/s
Measured $T_1$	$18.3 \mu\text{s}$	$17.8 \mu\text{s}$
$ 2\rangle$ population	Negligible	Negligible
$\pi$ -Rabi $P\{ 1\rangle\}$	$\approx 95\%$	$\approx 95\%$
3 Gate RMS Error	2.5%	11.7%
Total AC+DC Power	> 1 W	< 2 mW

the qubit, and would be worse for a qubit with smaller anharmonicity.

#### G. Comparison with state of the art

The integrated circuit is compared with a state-of-the-art quantum control system in Table II. The measured performance is comparable with the standard electronics in most regards. However, the size, digital data-rate, and power consumption required to operate the chip are all at least an order of magnitude lower than the standard readout electronics. Of particular importance is the total power consumption, which is below 2 mW. This number is equal to the total AC and DC power required to drive a continuous stream of  $\pi$ -pulses when clocked at 1 GHz and is viewed to be a conservative value as the chip is expected to operate at a lower activity factor in practice.

## VI. CONCLUSION

Future quantum computers will require low-power cryogenic control and readout electronics. Here, we have demonstrated a first generation quantum controller that dissipates under 2 mW while providing competitive performance. While this is an important step towards the implementation of a scalable quantum control and measurement system, considerable research is required before such a system can be realized. An important area of future work is to perform randomized

benchmarking on the XY controller such that gate error rates can be established. Other future work could include further reduction of power consumption, the demonstration of on-chip feedthrough cancellation and DRAG modulation, the development of multichannel XY controllers, as well as the demonstration of circuits for readout and Z-control.

## APPENDIX

Extracted parameters for each of the transistors appear for reference in Table III.

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TABLE III  
EXTRACTED TRANSISTOR PARAMETERS

	Temp.	uLVTn	LVTn	RVTn	HVTn	uLVTp	LVTp	RVTp	HVTp
$V_T$	300 K	0.18 V	0.22 V	0.26 V	0.34 V	0.21 V	0.24 V	0.29 V	0.37 V
	7 K	0.26 V	0.30 V	0.35 V	0.45 V	0.34 V	0.37 V	0.40 V	0.45 V
Subthreshold Slope	300 K	112 mV/dec	100 mV/dec	90 mV/dec	80 mV/dec	118 mV/dec	104 mV/dec	100 mV/dec	86 mV/dec
	7 K	36 mV/dec	34 mV/dec	33 mV/dec	32 mV/dec	65 mV/dec	52 mV/dec	28 mV/dec	23 mV/dec
$G_{m,pk}$	300 K	1.5 S/mm	1.4 S/mm	1.3 S/mm	1.2 S/mm	1.3 S/mm	1.3 S/mm	1.2 S/mm	1.1 S/mm
	7 K	2.0 S/mm	2.0 S/mm	1.8 S/mm	1.7 S/mm	1.8 S/mm	1.7 S/mm	1.7 S/mm	1.5 S/mm
$G_m$	300 K	14 mS/mm	15 mS/mm	16 mS/mm	16 mS/mm	13 mS/mm	14 mS/mm	15 mS/mm	17 mS/mm
$J_D = 10 \text{ mA/mm}$	7 K	33 mS/mm	32 mS/mm	32 mS/mm	31 mS/mm	23 mS/mm	27 mS/mm	30 mS/mm	28 mS/mm
$f_{t,pk}$	300 K	285 GHz	283 GHz	284 GHz	237 GHz	244 GHz	234 GHz	230 GHz	215 GHz
	7 K	360 GHz	365 GHz	347 GHz	313 GHz	349 GHz	335 GHz	327 GHz	291 GHz
$f_t$	300 K	52 GHz	53 GHz	46 GHz	53 GHz	49 GHz	49 GHz	49 GHz	49 GHz
$J_D = 10 \text{ mA/mm}$	7 K	92 GHz	93 GHz	89 GHz	86 GHz	93 GHz	94 GHz	89 GHz	85 GHz