

The Innovatest Mobile Force Verification Kit

Group No. 02

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Executive Summary

The Innovatest Mobile Force Verification Kit project is focused on the design of a highly portable, robust, and user-friendly solution that allows technicians to verify and calibrate hardness testers directly in the field. The project's scope spans from the concept design to the project documentation and the design of an interactive brochure. The project spanned from October 5th, 2025, to January 13th, 2026. Five engineering students make up the interdisciplinary design team and the project was completed under the guidance of Hochschule Rhein-Waal professors and scientific staff.

Initial market analysis revealed that the market for hardness testers is growing and thus there is a need for such a portable verification kit. The proposed system enables fully integrated operation inside an IP67-rated Pelican case, ensuring resistance to dust, moisture, and mechanical shock. Internally, the device hosts a custom printed circuit board with high end components designed to handle the controls, power and signal processing of the device. The product's HMI was designed with ergonomics in mind, boasting a 10" liquid crystal display screen with intuitive touchscreen functionality. The final design is limited to a production budget of €4,000 per unit ensuring competitiveness on the market. The kit supports automatic identification of up to six Innovatest load cell models, enabling force verification from 10 gf to 3,000 kgf with clear numerical and graphical outputs. To support field operations, the device includes an integrated Li-Po battery designed for 8–10 hours of continuous use.

From a mechanical standpoint, the device uses an IP-67 rated rugged pelican case with an aluminium chassis mounted inside to house the electronics. Medium density foam inserts surround this chassis to provide shock absorption and padding. Load cells are stored in dedicated foam compartments on the opposite side of the case, allowing secure transport without damage or misalignment. A complete 3D model was constructed to demonstrate all mechanical connections, fasteners, sealants and other features to create a device that is suited for harsh factory environments.

On the electrical side of the design, a complete schematic diagram and preliminary PCB were designed to match all functionality requirements with the utmost precision and speed. An advanced measurement chain was designed to process the load cell signals and gives a noise free resolution of 17 bits, classifying as a Class A measuring device by OIML. The design also incorporates high performance components such as the ESP32-P4 which allows for incredible signal processing and input responsiveness. The control, power management and battery management circuits were designed to give a battery life of 8.77 hours and advanced features such as switching between 5V and 10V excitation and real-time graphing.

To manufacture and assemble the product, the team performed a Make or Buy analysis to identify which components must be custom made and which can be bought on the market. The custom components were then assigned the most suitable manufacturing techniques, and a detailed assembly guide was written. The parts that were chosen to be bought had all the key requirements outlined so that a purchasing team could identify and acquire all necessary components.

Keywords:

Mobile Force Verification · Innovatest/Innovatech · Hardness Tester Calibration · IP67 · Industrial Durability · Portability

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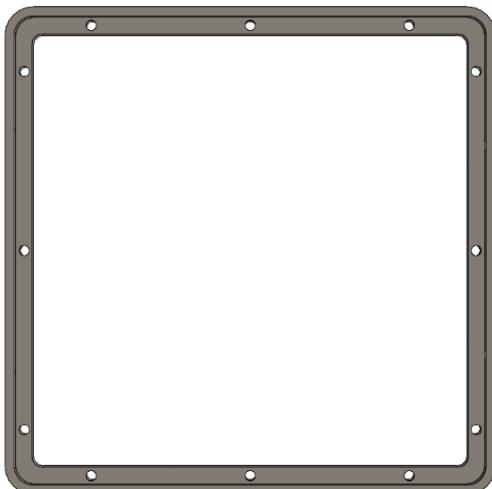


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1. Project Plan

1.1. Project Constraints

1.1.1. Project Scope

The overall scope of this project is the design of the Innovatest Mobile Force Verification Kit and relevant product documents. To achieve this, the following deliverables must be produced:

1. Concept Design
 - 1.1. Project Plan
 - 1.2. Market Analysis
 - 1.3. Overall Product Concept
 - 1.4. Functional Structure
 - 1.5. Human Machine Interface
 - 1.6. D-FMEA
 - 1.7. Concept Design Close-out
2. Product Design
 - 2.1. Complete 3D Model
 - 2.2. Measurement Chain
 - 2.3. Circuit Diagram
 - 2.4. Technology Selection for “Make” Parts
 - 2.5. Requirements Manual for “Buy” Parts
 - 2.6. Product Design Close-out
3. Project Documentation
 - 3.1. Technical Drawings for Main Assembly
 - 3.2. Program Flow Chart
 - 3.3. Bill of Material

- 3.4. Production Planning
- 3.5. Cost Calculation
- 3.6. Specification Sheet
- 3.7. User Manual
- 3.8. Interactive Brochure
- 3.9. Project Documentation Close-out
- 4. Project Close-out

It should be noted that some important aspects for the success of the Innovatest Mobile Force Verification Kit are outside of the scope of this project such as:

- Competitive Pricing Strategy
- Product Launch Schedule
- Development of Functioning Prototype

1.1.2. Project Schedule

The project will adhere to a schedule consisting of 3 milestones that coincide with the main deliverables of the project. These milestones are as follows:

1. Concept Design: 2025-10-28
2. Product Design: 2025-12-02
3. Project Documentation: 2026-01-13

1.1.3. Project Resources

The project team is comprised of five engineering students and responsibilities were distributed based on their degree program and experience as shown in Table 1.

Table 1: Responsibility Distribution Table

Name	Mat No.	Responsibilities	Degree Program
Abhinav Kothari	33349	<ul style="list-style-type: none"> • HMI • System Logic • Specification Sheet • Project Management (Process Verification and Coordination) 	Mechatronics Systems
Ahmad Zeaiter	33946	<ul style="list-style-type: none"> • Concept Design • Mechanical Design • Technical Drawings • Graphic Design of Brochure 	Mechanical
Justin Chin Cheong	34140	<ul style="list-style-type: none"> • Project Management (Planning and Framework setup) • System Design and Integration 	Mechatronics Systems

		<ul style="list-style-type: none"> • Signal Processing • Market and Industry Analysis • Financial Analysis • User Manual 	
Okan Can Meral	31684	<ul style="list-style-type: none"> • D-FMEA • Electrical Design • Manufacturing Technology Selection • Production Planning 	Industrial
Wasim Ahmed Mohammed Al Asbahi	31090	<ul style="list-style-type: none"> • D-FMEA • Electrical Design • Manufacturing Technology Selection • Production Planning 	Electrical

1.2. Responsibility Assignment Matrix

To distribute the work with greater precision, a responsibility assignment matrix was created to illustrate the responsibilities of all team members.

Key: X - responsible, + - support, * - approval

Table 2: Responsibility Assignment Matrix for Each Deliverable

ID	Deliverable	Wasim	Okan	Justin	Abhinav	Ahmad
1.1	Project Plan	+ *	+ *	X	+ *	+ *
1.2	Market Analysis		X	*		
1.3	Overall Product Concept	+ *		+	+	X
1.4	Functional Structure			X	*	
1.5	HMI				X	*
1.6	D-FMEA	X	*	+	+	+
1.7	Concept Design Close-out	X	X	X	X	X
2.1	Complete 3D Model	+ *				X
2.2	Measurement Chain	+		X	*	
2.3	Circuit Diagram	X		+ *	+	
2.4	Technology Selection for “Make” Parts	X	*	+		
2.5	Requirements Manual for “Buy” Parts		X	*		+
2.6	Product Design Close-out	X	X	X	X	X

3.1	Technical Drawings for Main Assembly	+ *			+	X
3.2	Program Flow Chart			+	X	*
3.3	Bill of Materials	+		X	*	+
3.4	Production Planning	X	*	*	+	
3.5	Cost Calculation		X	*		
3.6	Specification Sheet	+		*	X	+
3.7	User Manual		X	+	+	*
3.8	Interactive Brochure	*	*	+	+	X
3.9	Project Documentation Close-out	X	X	X	X	X
4.0	Project Close-out	X	X	X	X	X

1.3. Work Breakdown Structure

A complete work breakdown structure can be found in 19.1 Appendix A detailing each work package and its contributors, schedule, dependencies and type.

1.4. Gantt Chart

The following pages show the Gantt chart¹ for the project, highlighting each work package along with its resources, schedule, and dependencies. The Gantt chart is split across the three milestones. A complete Gantt chart with all three milestones at once can be found on [Sciebo](#)².

Key:



Abhinav Kothari



Ahmad Zeaiter

¹ The Gantt chart was created using trial version of the Gantt Pro Software <https://app.ganttpro.com/>

² The link to the file on Sciebo is <https://hochschule-rhein-waal.sciebo.de/f/197025147>



Justin Julius Chin Cheong



Okan Can Meral



Wasim Ahmed Mohammed Al Asbahi



Milestone

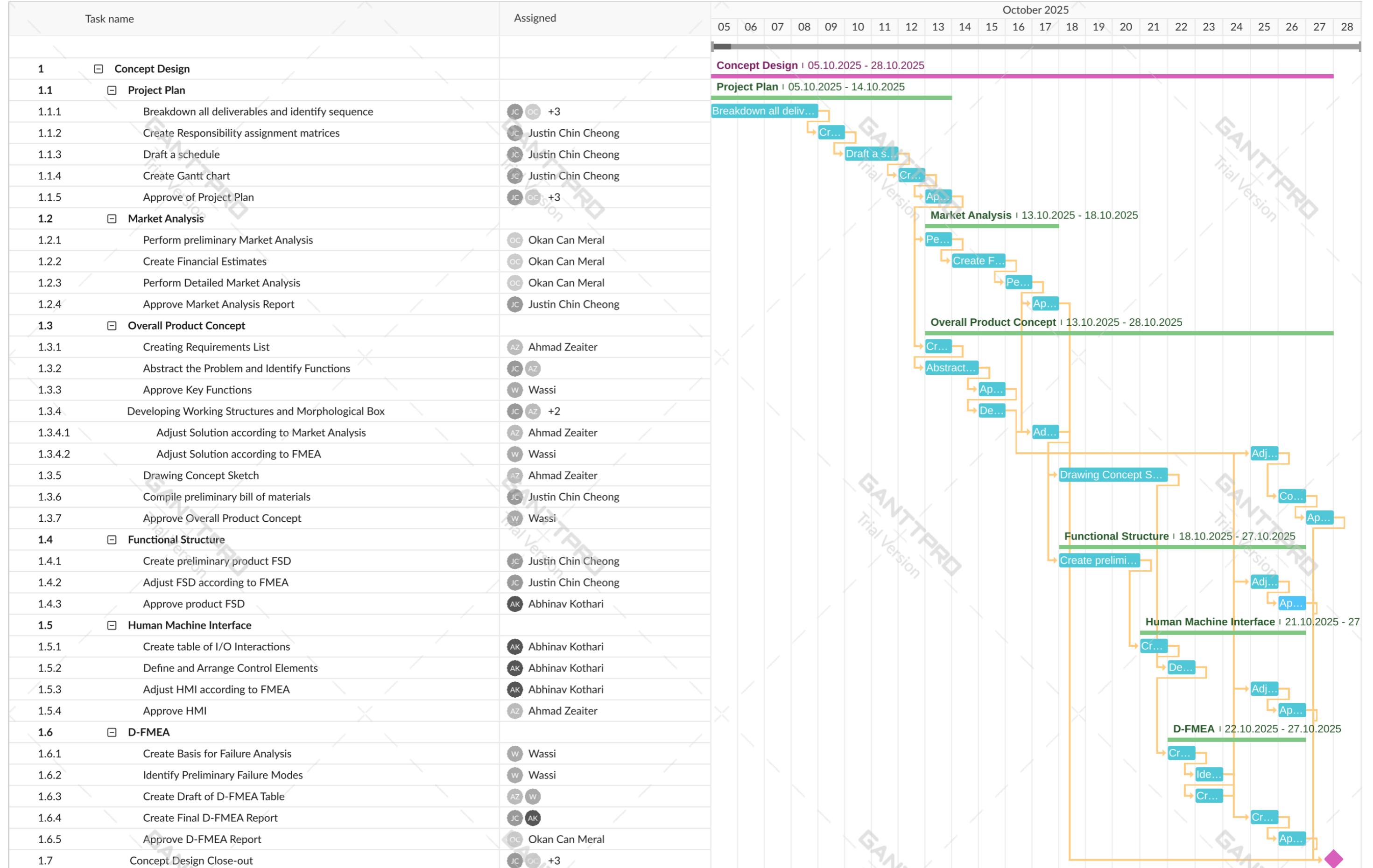


Figure 1: Gantt Chart for Milestone 1

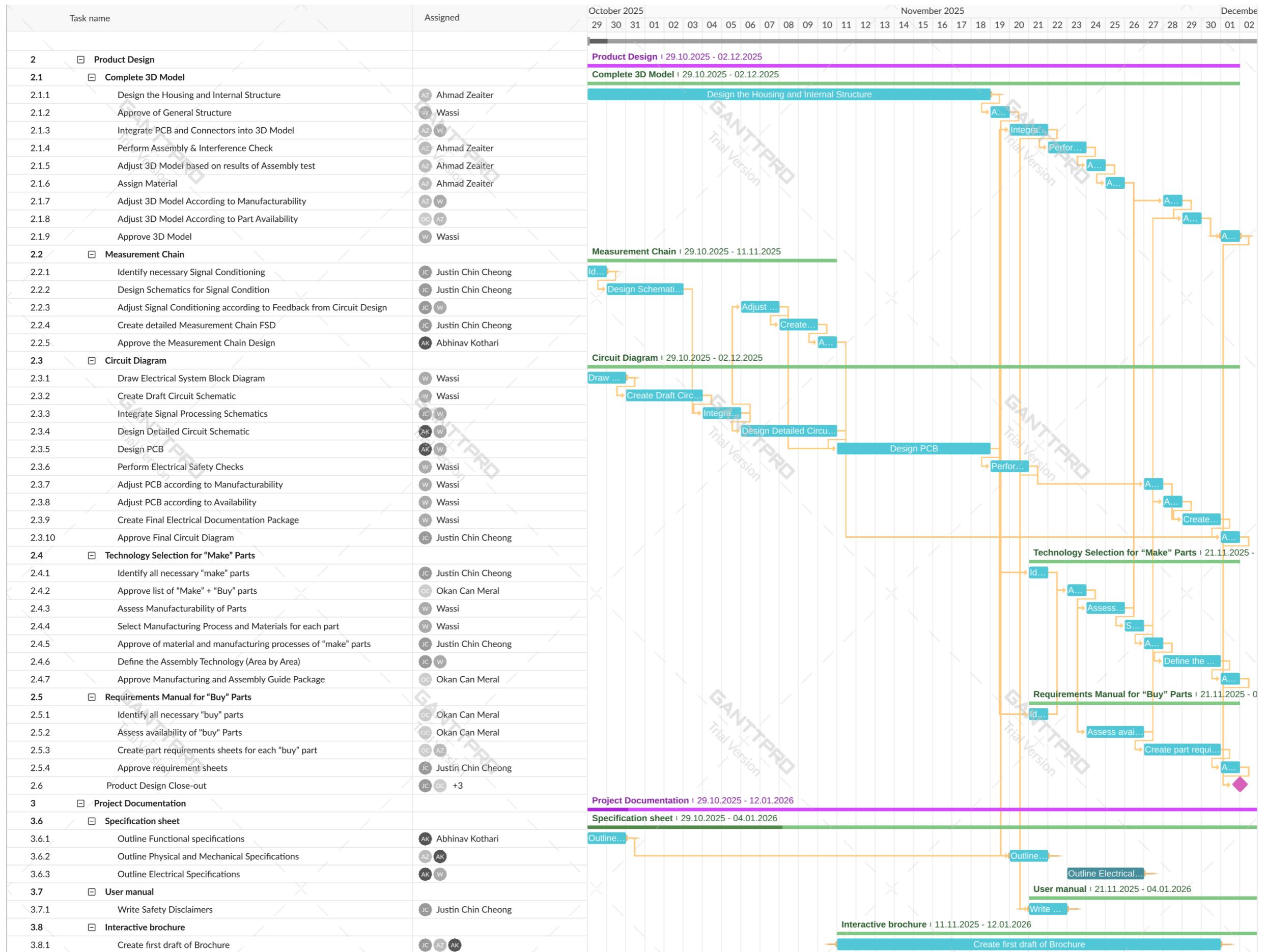


Figure 2: Gantt Chart for Milestone 2

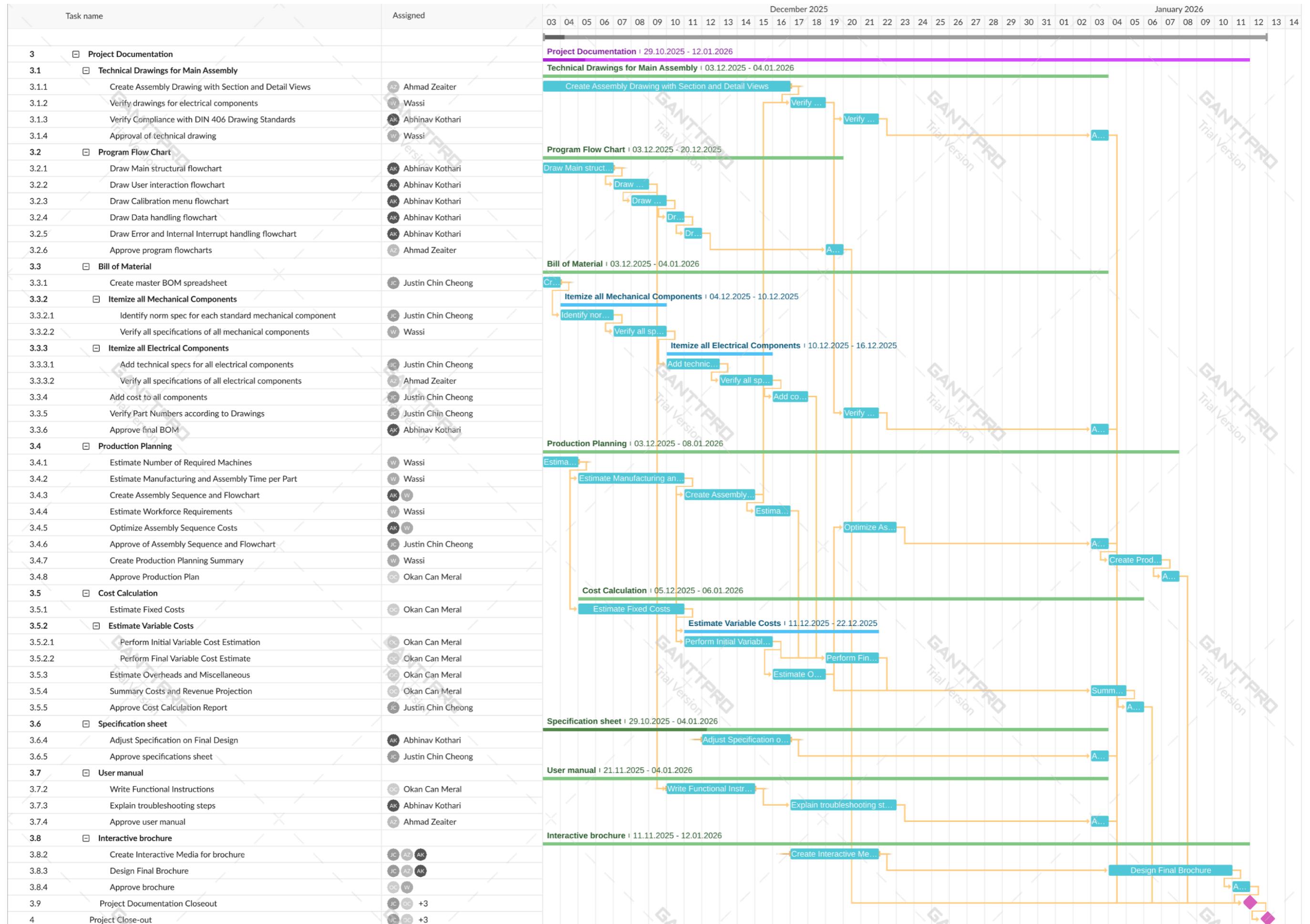


Figure 3: Gantt Chart for Milestone 3

2. Market Analysis

2.1. Industry Context

2.1.1. Market Overview

This analysis aims to determine the Innovatest Mobile Force Verification Kit's market potential, competitors, potential users, and emerging trends in force measurement and calibration systems. The basic marketing strategy and product placement will also be determined by the results.

Hardness testers and other mechanical measurement equipment are extremely pervasive in major sectors such as manufacturing, aerospace, automotive, and materials science. The global hardness testing market itself was valued at USD 274 million in 2025 according to Intel Market Research (2025) and by 2032, it is projected to reach USD 353 million. As the market grows, so does the need for precise calibration and verification equipment. Thus, there is a growing market for portable, reliable, and accurate verification kits that companies can use to evaluate and calibrate their equipment in the field. This is the exact market the Innovatest Mobile Force Verification Kit seeks to fill.

2.1.2. Competitor Analysis

The range of solutions for a mobile force verification kit currently on the market is quite sparse. However, there exists some products that can be used for force verification and calibration and could potentially be competition for the Innovatest Mobile Force Verification Unit. These products and their companies are outlined in Table 3: Comparison of Competitors in The Mobile Force Verification Kit Market.

Table 3: Comparison of Competitors in The Mobile Force Verification Kit Market

Competitor	Price Range [€]	Product Description	Region
Morehouse Instrument Company	6000 - 8000	A 5-in-1 force verification system is kit that includes a load cell, minicomputer with custom software for processing and a load cell cable stored inside of a custom.	USA
Sun-Tec Corporation	150 - 600	A set of standard hardness samples of known hardness which can be tested against the hardness tester's reading.	USA
Tovey Engineering Innovation	10000 - 60000	A portable calibration system comprised of load cells, dead weights, a laptop computer, and	USA

		load cell simulator. It can be in the form of a pushcart or carry case.	
Interfaceforce	20000 - 35000	An inspection kit with a force transducer, testing machine and measuring device which connects to a Windows computer.	Germany

Table 3: Comparison of Competitors in The Mobile Force Verification Kit Market shows that the other solutions on the market are portable, reliable and precise. However, there are some clear shortcomings. The Sun-Tec Hardness Samples requires incredibly careful handling and can only verify an extremely specific hardnesses per sample. On the other hand, the Morehouse, Tovey Engineering, and Interfaceforce products are sets of several different components that must be connected. The Interfaceforce even requires an additional computer for processing.

The Innovatest Mobile Force Verification Kit aims to overcome such faults by providing a verification system that is compact and completely integrated into the carrying case. This means all functionality is achieved with a single unit and not a series of components. By connecting to load cells of different ranges and precisions also allows the kit to verify the entire force range of the hardness testers with ease.

2.1.3. Market Drivers

The drivers of the Force Verification market are heavily tied to those of the Hardness Tester market. As precision hardness testers become more widespread, the need for accurate and convenient verification increases.

The main driver of these markets is the recent increase in quality assurance and control procedures in compliance with international standards. To ensure higher safety factors and durability hardness testers will be used more regularly and thus must be checked and monitored consistently. This is most prevalent in sectors such as manufacturing, aerospace, automotive, and material sciences.

Another driver in the market is the growth of the portable hardness tester market. It is projected to have a compound annual growth rate (CAGR) of 5.5% between 2023 and 2033. This coincides with demand for on-site testing which then requires on-site calibration and verification which the Innovatest Mobile Force Verification Kit will capitalise on.

2.1.4. Market Size

2.1.4.1. Total Addressable Market (TAM)

According to the Intel Market Research (IMR, 2025) report, the global hardness testing machine market is valued at USD 274 million in 2025 and is expected to reach approximately USD 353 million by 2032, with a CAGR of 3.8%. This growth will mainly occur in the automotive, aerospace, and heavy industry sectors, primarily due to the rising need for quality control and material verification. The ongoing automation and digitalization across industries are also significantly increasing the demand for hardness testing systems. This transformation greatly enhances the importance of both stationary laboratory equipment and portable testing devices.

The Future Market Insights (2024) report estimates the global market value at around USD 351 million for 2025, while Intel Market Research (2025) reports USD 274 million for the same year, indicating a consistent growth trend across the market.

2.1.4.2. Serviceable Available Market (SAM)

For the Innovatest Mobile Force Verification Kit, the initial commercialization area is Europe. The region's large number of industrial testing laboratories, quality control facilities, and advanced production sectors such as automotive and aerospace create a strong foundation for calibration systems.

According to Intel Market Research (2025), Europe accounts for about 30% of the global market, which corresponds to a market value between USD 100 M and 120 M as of 2025. This market includes stationary laboratory devices, as well as portable verification equipment and on-site calibration services.

MarketsandMarkets (2025) highlights that Germany, the Netherlands, Switzerland, and the Scandinavian countries are the regions where hardness testing activities are most concentrated within Europe.

2.1.4.3. Serviceable Obtainable Market (SOM)

When calculating the SOM, one of the most important factors is to fully understand the company's capacity and capabilities. In Europe, the Innovatest Mobile Force Verification Kit focuses on the portable, field-type calibration systems segment. Due to their ability to save time and increase mobility in quality control processes, there is a growing demand for these solutions.

Sharma (n.d.) states that the global market for such devices is valued at approximately USD 350 million, and it is expected to reach USD 580 million by 2032. This calculation

is based on target countries such as Germany, the Netherlands, Switzerland, and the Scandinavian region.

Capturing even 1% of this market would mean about 100–200 units sold during the launch period of 6 months. This demonstrates that the Innovatest Mobile Force Verification Kit effectively addresses the high-quality standards and on-site verification needs of the European market.

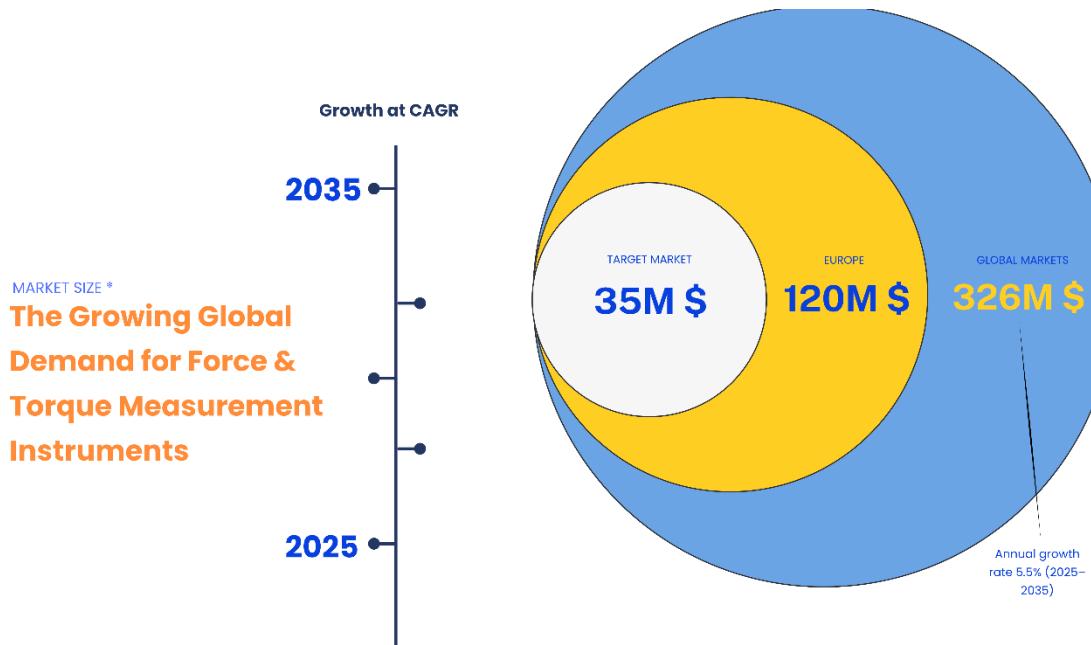


Figure 4: Market Size Chat

2.2. Target Buyer Analysis

2.2.1. Overview

The Innovatest Mobile Force Verification Kit is intended to be sold in a business to business (B2B) capacity. It is especially designed for organizations and institutions engaged in quality assurance, metrology, and mechanical testing.

The product addresses a critical gap between laboratory-based calibration systems and practical field verification tools, offering laboratory-level precision in a compact, mobile design.

2.2.2. Primary Target Buyer

The primary target buyers for the Innovatest Mobile Force Verification Kit are institutions and companies that have already purchased Innovatest Hardness Testers and/or other products. This would include:

- Industrial Quality Assurance Departments
- Research and Development Institutions

2.2.2.1. Industrial Quality Assurance (QA) & Metrology Departments

These departments of larger industrial companies (e.g., automotive, aerospace, and precision manufacturing) require a convenient and reliable way to perform routine checks and internal calibrations.

Some of the key needs met by the product include:

- Compact and rugged design that can be used in the field in harsh conditions.
- Reducing external calibration by enabling in-house functional checks
- Compatibility with multiple Innovatest load cell models
- Integrated data logging for USB export
- Intuitive graphical user interface

2.2.2.2. Research & Development (R&D) and Academic Institutions

Technical universities and research centres need force verification tools to inspect the machines they use to investigate materials, develop prototypes, and train engineers.

They are primarily interested in the research and learning opportunities. Similarly to the QA departments they are required to do checks of their hardness testers. Besides the needs highlighted in 2.2.2.1, the ease of use of the product can make it an excellent educational tool.

2.2.3. Secondary Target Buyer

2.2.3.1. Machine Manufacturers' & OEM Partners

There is also potential to sell to other manufacturers of hardness testers for preliminary testing after assembly. This provides a quick and easy alternative to lab testing and can reveal issues before more complicated testing methods are used.

2.2.3.2. Geographical Focus

The initial commercialization phase focuses on Europe, where force calibration activities and standards are well established.

Some key markets include:

- Germany, Netherlands, Switzerland, Scandinavia - High industrial density and quality infrastructure
- France, Belgium, UK - Strong aerospace and research institutions
- Eastern Europe - Emerging demand from cost-sensitive manufacturers

Following successful European deployment, expansion will target North America and Asia-Pacific, driven by industrial modernization and increasing quality regulation.

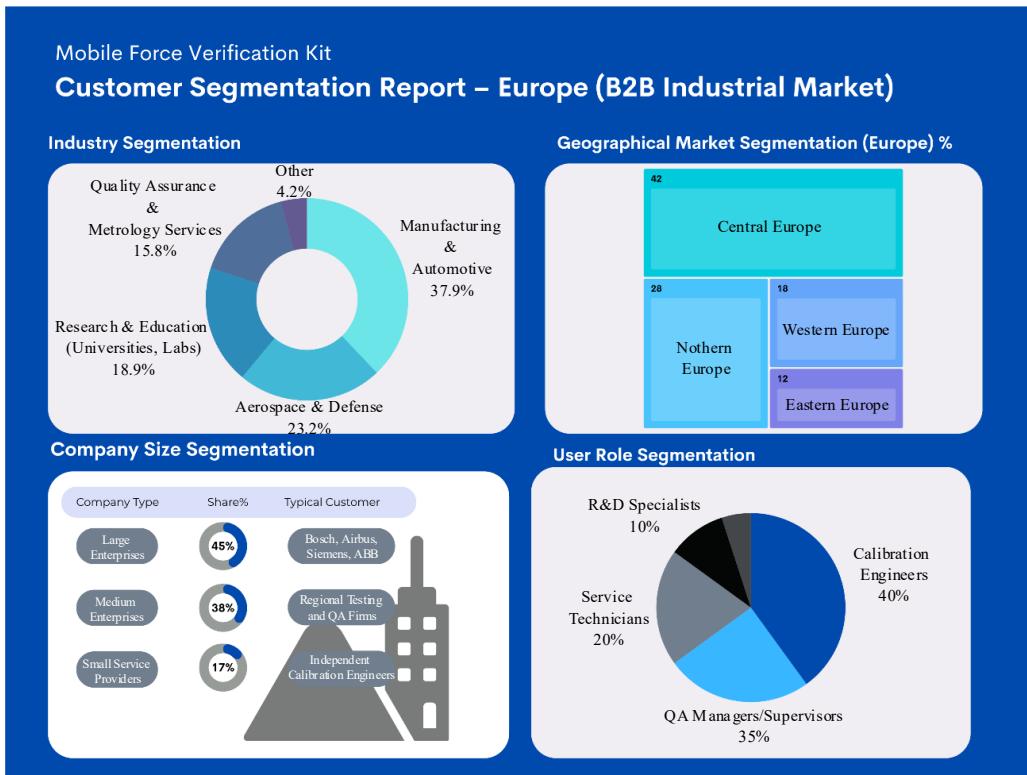


Figure 5: Customer Segmentation Report

2.3. Basic Marketing Approach (4P Analysis)

2.3.1. Product

The Innovatest Mobile Force Verification Kit is a compact, portable, and precise measurement device designed to verify the applied forces of hardness testers in both laboratory and field environments.

Developed for Innovatest Europe BV, the product integrates existing Innovatest load cells with a portable digital control unit capable of automatically identifying up to six different load cells, all together covering a force range from 10 gf to 3,000 kgf. Allowing engineers to perform on-site calibration and verification across a wide spectrum of hardness testing machines.

The verification kit is housed in an IP-67 rated Pelican 1500 case, ensuring full protection against dust, water, and shock. The case has a modular interior separating the electronics from a dedicated load cell storage compartment. This modular design simplifies assembly, maintenance, and future upgrades.

With 8-10 hours of battery life, USB-C charging, and a graphical user interface that supports data logging, USB export, and calibration functions, the device ensures efficient and user-friendly operation.

The primary needs that the product aims to meet is portability and ease of use for field engineers. Being encased in rugged and compact carrying case makes it easier to travel with and having everything contained and integrated into the case allows engineers to quickly setup and start measurements.



Figure 6: Product Preview Image

2.3.2. Price

Typical products in this market, as seen from Section 2.1.2, range from €6,000-€60,000. The Innovatest Mobile Force Verification Kit, aims to be produced at a maximum cost price of €4,000. So even after a profit margin of 50%, makes it €6,000, keeping it very competitively priced.

The competitive price comes without compromise on precision and reliability, while also being highly portable.

During the introduction and growth stage, a combination of value-based pricing and cost-plus pricing strategy may be implemented to quickly establish a market presence while ensuring no loss is borne by the company itself.

Example:

Innovatest could look at the competitors from Section 2.1.2 and set the pricing based on what the value the product bares in mind of the customer compared to the already existing customers. This can be done through primary research of the customers perception of the product as well. Special prices can also be offered to already existing customers, to encourage them to stay in the Innovatest ecosystem.

Providing services on top of the product, such as extended warranties, training sessions, can also increase the value of the product in the customers mind, leading to a higher price which the company can charge and justify.

This pricing model combination ensures both market entry and sustainable revenue, as no losses will be borne by the company.

Moreover, as the product life cycle goes forward towards decline stage, prices can be reduced to keep the product relevant and competitive.

2.3.3. Place (Distribution)

Distribution will primarily follow a B2B model, focusing on direct sales to industrial clients, calibration service providers, and research institutions.

Initial market entry will target Europe, particularly Germany, the Netherlands,

Switzerland, and Scandinavia, due to their established industrial and testing infrastructure.

Distribution channels include:

- Direct sales through Innovatest's existing dealer network.
- Online sales platform for product demonstration, quotation, and customer support.
- Participation in industrial trade fairs such as *Control Expo Germany* and *Sensor+Test Nürnberg*.
- Partnerships with calibration service providers and testing laboratories for joint demonstrations and pilot installations.

As market demand grows, Innovatest may expand into North American and Asia-Pacific markets through authorized distributors.

2.3.4. Promotion

Promotion activities will aim to position The Innovatest Mobile Force Verification Kit as a professional, reliable, and portable solution for force verification while maintaining high precision and accuracy.

The marketing department shall highlight:

- IP67 Rating: for incredible durability even in industrial environments
- All day battery life: 8 hours' worth of uninterrupted usage
- Automatic load cell identification: hassle free cell detection and naming
- HMI: Intuitive UI design and easy to use touch screen display
- Ergonomic + Stylish shape: Pelican case provides ergonomic handles for carrying while maintaining a sleek look
- Portability: The small size and nominal weight design makes it easy to travel with

Much more benefits can also be highlighted in marketing.

Planned promotional strategies may include:

- Technical presentations and webinars for calibration engineers and quality managers.
- E-Newsletters to existing Innovatest customers
- LinkedIn campaigns targeting industrial testing professionals.
- Collaborations with universities and research labs for academic demonstrations.
- After growth rate case studies and customer testimonials can be used to showcase field performance.
- Trade show exhibitions and product brochures emphasizing features and ROI.

During the maturity stage, Innovatest can strengthen its brand visibility through certifications and global reseller partnerships, ensuring long-term market presence and trust.

3. Overall Product Concept

3.1. Requirements List

3.1.1. Functional Requirements

- System can recognize at least six Innovatest load cell models automatically.
- Each load cell is displayed with an intuitive name that can be modified by user.
- System uses a universal port compatible with all supported load cells.
- Device can measure forces from 10gf – 3,000 kgf.
- Measurement results displayed numerically (in gf, kgf, N, kN) and graphically in real-time.
- User can configure numerical formats on digital display.
- Interface includes standard functions such as Tare, Zero, and Peak & Hold.
- Device supports data logging and export via USB, manually triggered by the user.
- System can delete old data with confirmation when storage is full.
- System includes 1 channel for the load measurement signals and 1 channel for cell recognition.
- System can perform basic calibration of load cells using 1 to 5 data points per cell.
- Sampling rate is adjustable.

3.1.2. User Interface (UI) & Display Requirements

- Display is a 10-inch touchscreen.
- UI is intuitive and responsive, suitable for field operation.
- Display can show real-time force curves.
- Display includes status indicators for battery, connection, and data logging.

3.1.3. Mechanical Requirements

- Compact, ruggedized housing integrated into a portable protective case.
- Minimum IP65 protection rating with shock absorbing padding.
- Protective compartments for load cells.
- Minimum operating temperature range: 0-60°C.
- Minimum humidity tolerance: 10-90% non-condensing.

- Weight: ~5-6 kg.
- Aesthetically refined and ergonomic form factor.

3.1.4. Electrical Requirements

- Rechargeable power source with a battery life of 8-10 hours.
- Battery voltage range 3.2 V – 4.2 V.
- 3.3 V regulator for microcontroller.
- 5V/10V boost converter for selectable load cell excitation.
- 24-bit ADC for precision measurement.
- Input sensitivity: 4mV/V.
- Low pass and noise filtering on input signals.
- Non-volatile internal storage for measured data.
- USB-A port for data export.
- USB-C port for charging.

3.1.5. Software Requirements

- Integrated signal to force conversion algorithm.
- Sufficient sampling rate to prevent aliasing.
- Software supports real-time graph plotting of force measurements.
- Calibration data and user preferences are stored persistently.
- Basic troubleshooting instructions/functions.

3.1.6. Reliability & Lifecycle Requirements

- Expected service life: 8 years.
- System designed for field robustness and electrical protection.
- Firmware supports future software updates.

3.1.7. Economic Requirements

- Target production cost: ≤ 4000 EUR per unit.

3.2. Abstraction to Identify the Essential Problems

Table 4: Abstraction of essential problems

Requirements	Functional Abstraction	Generalized Problem	Essential Problem Definition
Measurement range: 10 gf – 3000kgf	Ability to detect and quantify force signals of varying magnitudes	Transform electrical signal from load cell into a force measurement	Accurately measure mechanical forces across a wide range
Recognize 6 Innovatest load cell models	Interface compatible with multiple sensor types	Establish adaptable communication between sensor and processor	Enable automatic identification and integration of various load cells
Numeric and graphical output on display	Visualise real-time data and user parameters	Translate measurement data into interpretable information	Present measurement data clearly
Calibration using 1 to 5 points per cell	Adjust system response to known reference loads	Ensure traceable and repeatable force measurements	Maintain measurement accuracy through user calibration
Data logging, USB export, deletion function	Store, manage, and transfer data	Maintain organized, retrievable measurement records	Provide reliable data handling
Minimum IP65, shock protected, and portable housing	Protect internal components from environment	Maintain functionality under field conditions	Ensure durability and usability in rough environments
Programmable sample rate, low-pass, and noise filtering	Adapt signal to different measurement needs	Minimize signal distortion and noise	Deliver accurate and stable readings across different measurement conditions
Cost ≤ 5000 EUR	Economically feasible design	Optimize material manufacturing, and components cost	Achieve a balance between performance, manufacturability, and cost

The crux of the problem: to develop a portable and robust system capable of accurately acquiring, processing, and presenting force measurements from multiple load cell types under different field conditions.

3.3. Working Structure

3.3.1. Morphological Box

Table 5: Morphological Box for Selection of Solutions

Function	Sub-function	Option 1	Option 2	Option 3
Sensor Interface	Load Cell Interface	5-pin header Connector	M12 5-pin connector	MIL-Circular Connector
	Load Cell Identification	Resistor-based recognition in connector	1-wire ID chip embedded in connector	Software-based AI Detection
	Load Cell Excitation Voltage	Fixed 5V output	Selectable 5V/10V output	Software-adjustable voltage
Signal Processing	Analog Signal Conversion	Delta-Sigma 24-bit ADC	24-bit SAR ADC	Integrated bridge front-end ICs
	Signal Conditioning	Passive low-pass filter	Instrumentation Amplifier	Programmable gain amplifier (PGA)
User Interface	Processing Unit	Micro-controller	Micro-processor	ASIC
	Data Display	TFT LCD	OLED	IPS TFT LCD
	HMI	Analogue Buttons	Capacitive Touch Screen	Resistive Touch Screen
Structure	Data Logging Export	USB flash drive storage	MicroSD card slot	Wireless data transfer via Wi-Fi
	Power Source	Rechargeable Li-Po Battery	Rechargeable NiMH Battery	Replaceable Li-Po Battery
	Housing Size and Form	Tablet-style Hand-held	Compact, rugged brief case size	Laptop-Style and Size
	Housing Protection Class	IP65	IP66	IP67

3.3.2. Solution Evaluation

Table 6: Solution Evaluation Table

Solution	Reasoning
M12 5 pin connector	<ul style="list-style-type: none"> • Standard connector with IP67-IP68 rating • Locking mechanism • Support five pins, 4 for signal transmission and 1 for load cell recognition • Compact footprint ³
Resistor based recognition	<ul style="list-style-type: none"> • Reasonable • Can do many variations of load cells
Selectable 5V/10V output	<ul style="list-style-type: none"> • Allows for flexibility • Can increase sensitivity or reduce power consumption
Delta-Sigma 24-bit ADC	<ul style="list-style-type: none"> • Good speed • High accuracy
Passive low pass filter and instrumentation amplifier	<ul style="list-style-type: none"> • Blocks high noise • More reliable
Microcontroller	<ul style="list-style-type: none"> • Less heat dissipation • Flexible enough, compared to ASIC
TFT LCD	<ul style="list-style-type: none"> • Less power consumption • No burn-in
Resistive touch screen	<ul style="list-style-type: none"> • Less power consumption • More durable in harsh environments⁴ • Can be used with gloves
USB Flash Drive Storage	<ul style="list-style-type: none"> • More common than Micro USB • Faster than most Wi-Fi networks
Rechargeable Li-Po batteries	<ul style="list-style-type: none"> • Higher energy density • Lighter weight • More charge-discharge cycles⁵
Compact rugged brief case size	<ul style="list-style-type: none"> • Can carry load cells as well • Easy to carry
IP67	<ul style="list-style-type: none"> • Can withstand harsh environments

³ (Dlesauvage, 2023)

⁴ (TouchWo, 2025)

⁵ (EcoFlow, n.d.)

3.4. Preliminary Bill of Materials

Table 7: Preliminary Bill of Materials

Component	Description	Quantity	Approx. Total Cost [EUR]
Electrical			
Microcontroller (MCU)	Main control unit and processor	1	4
Printed Circuit Board (PCB)	Circuit board upon which all electrical components are mounted and connected via	1	10
Load Cell Connector	Wire that connects the load cell to the verification kit	1	40
Load Cell Interface Port	Port for the load cell connector to interface with verification kit	1	5
Noise and Low-pass Filter	Module that eliminates noise from load cell signal	1	2
Amplifier	Module that amplifies load cell signal for better reading	1	4
Analog to Digital Converter (ADC) Module	Module that converts load cell signal into digital signal that the microcontroller can process	1	10
Cell Excitation Regulator	Power regulator to regulate the excitation voltage of the load cells	1	8
Touchscreen Display	Screen that displays graphical output and allows user input	1	100
Push Button	Reliable button for controlling power to the Kit	2	40
LED light	Light to indicate warnings such as low battery or measurement ongoing	1	0.1
Internal Memory Module	Module that stores measured data within the verification kit	1	3
USB-A Port	Connector for standard USB stick for exporting measured data	1	1
Power Regulator	General power regulator to provide regulated power to components on the PCB	1	4
USB-C Port	Connector for charging cable	1	2
Battery Charging Circuit	Module to regulate incoming power to safely charge battery	1	5

Battery	Storage of electrical energy which provides power to entire verification kit	1	20
Misc	Passives, Wires, Insulation, Pin headers	n./a.	15
Mechanical			
Protective Carrying Case	Housing for the verification kit that provides IP67 level protection of the exterior	1	200
Foam	Soft foam that provides padding for internal electronics	1	50
1-Panel Frame	Frame that outlines the HMI of the kit secures it to the protective case and seals it for IP67	1	30
Internal Aluminium Frame	Aluminium frame inside which electronics and battery are secured and then placed into the protective case	1	150
Misc	Screws, Fasteners, O-rings, Mounting brackets	n./a.	50
Estimated Total of control unit			753.1
Load cells	The instruments that send signals to the kit when force is applied	6	2.884
Estimated Total of full Verification Kit			3,637.1

3.5. Concept Design Sketch

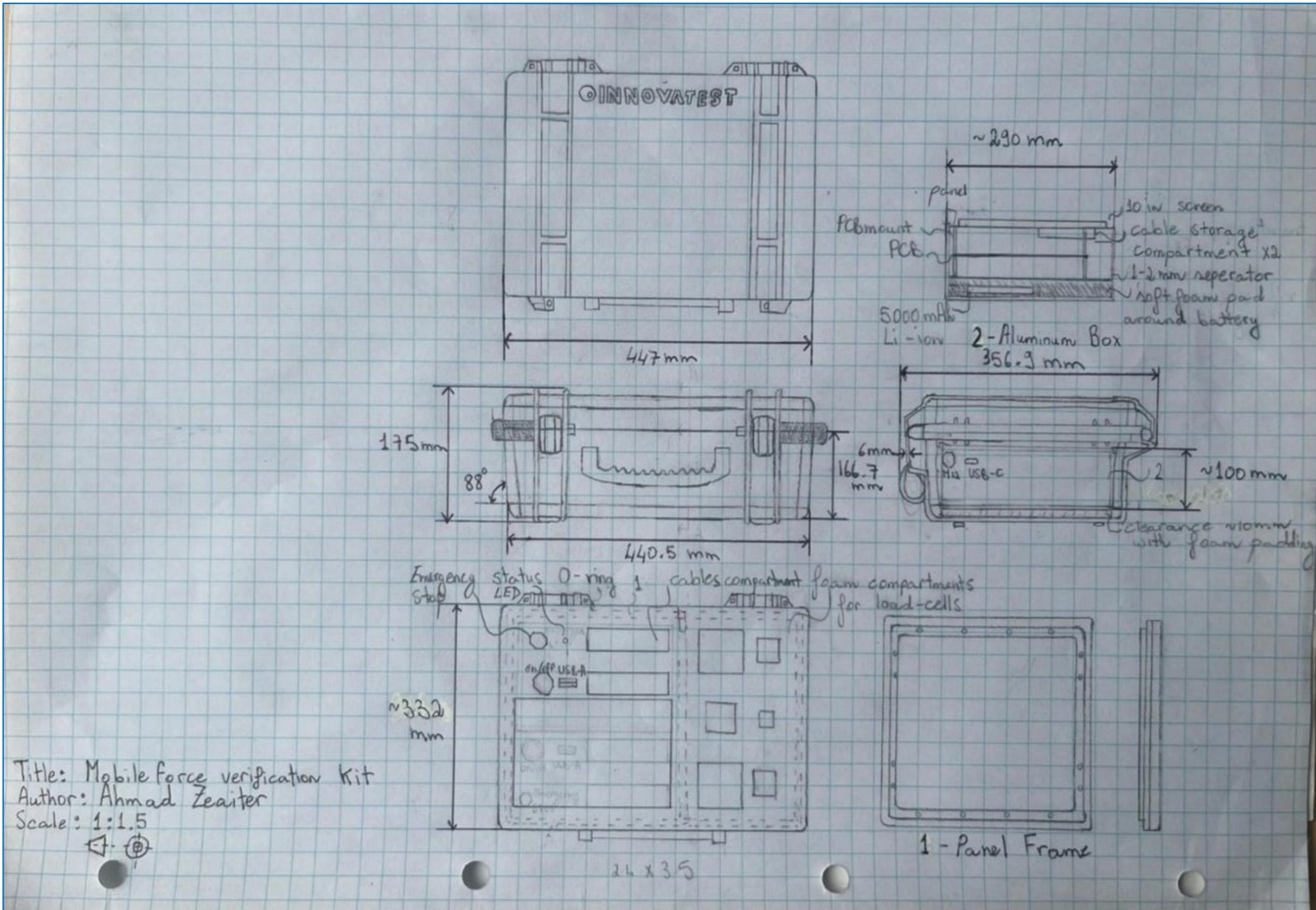


Figure 7: Freehand Sketch according to ISO 129 using First Angle Projection

3.6. Overall Product Concept Description

The Innovatest Mobile Force Verification Kit is designed to be a compact, and rugged system stored inside a Pelican 1500 protective case. The case provides IP67 level protection, is portable and robust for field operations. The interior is modularly with two separate sections one for load cell storage and another containing the verification kit.

3.6.1. Structure

The electronics panel is mounted in a metal frame with O-ring sealing. The frame is supported by the case ribs and reinforced with two L-brackets on the suspended side. Foam compartments store load cells securely on the opposite side. Inside the aluminium electronics box, the PCB is mounted above Li-Po battery. Foam padding and a separator plate provide shock absorption and thermal isolation. The box sits slightly above the case bottom with foam padding under it to further protect components.

3.6.2. Power

A rechargeable 5000 mAh Li-Po battery will run the system for 8-10 hours. See 19.2 Appendix B for the battery life estimation calculations. Cutouts in the case for USB-C port is used to charge the battery to full health in approximately 1-2 hours.

3.6.3. Sensor Interface

The kit connects to Innovatest load cells via an M12 5-pin connector. The load cell model is automatically recognized via a specific resistor placed inside of the connector cable. The system can provide excitation voltage of 5V or 10V depending on the load cell model.

3.6.4. Signal Processing

Signals from the load cells are filtered by the passive low-pass filter and then amplified by the instrumentation amplifier. These two together reduce noise and amplify before conversion using a dedicated 24-bit ADC. The microcontroller handles real-time processing of the signal into force measurements.

3.6.5. User Interface

A 10-inch TFT touchscreen displays numerical and graphical measurements in real time. Standard functions like Tare, Zero, and Peak & Hold are built in. Data logging is supported via USB-A. A LED indicates the status of the kit and an emergency shut off button is included. Cable and accessory storage are integrated around the touchscreen.

3.6.6. Cell Detection Concept

The 5-pin M12 connector allows for identification of individual load cells while simultaneously carrying the power and signal lines for the load cell.

There are 4 cables from the load cells which must be connected for successfully reading of the required data. This includes the V_{CC}, GND, + Signal and – Signal, as shown in the figure below.

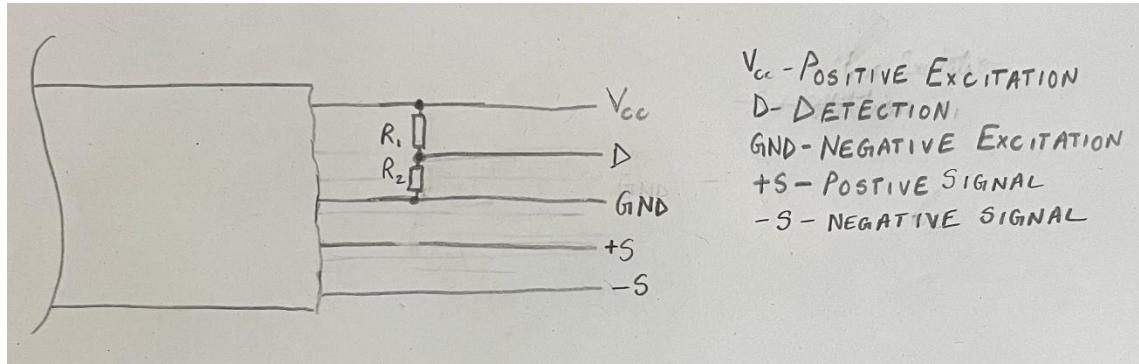


Figure 8: Load cell identification concept

For the identification of the load cell, a voltage divider can be placed between the V_{CC} and GND, and a 5th cable can be connected to read the voltage and hence identify each load cell. When first identified, it will give it an intuitive name, based on the existing data, however the user will be given the possibility to rename it, and when the same resistance is identified in future use, that name will be displayed from the saved storage.

$$D = \frac{R_1}{R_1 + R_2} \times V_{CC}$$

Through the formula above the D can be calculated for each load cell, so this can be saved and used to compare for load cell voltages measured in the future, allowing us to easily identify load cell if the value matches within a tolerance.

Whenever a new load cell, other than predefined one is connected and added, a random name will be given and the voltage value will be saved, this same load cell can then be identified by using the saved value.

This mechanism will be placed entirely within the M12 connector.

4. Functional Structure

4.1. Key Functions

As determined in Section 3.2, the key function of the Innovatest Mobile Force Verification Kit is acquiring, processing, and displaying force data from connected sensors. Achieving this overall function requires the following system functionalities:

- Startup: User powers on system and battery supplies power.
- User Control: User can select commands to start measurement or export measured data.
- Interface Sensor: Load cell is recognised and then interface is ready to receive raw measurement signal when force is exerted on the load cell and user initiates measurement.
- Process Sensor Signal: Internal components filter, amplify and convert signal into force measurement readings.
- Display Force Curve: Screen displays force measurements in real-time, plotting a curve.
- Log and Export Data: Data is stored internally and exported to USB when prompted by the user.
- Alert Status and Battery Level: LED alerts user of measuring status or low battery level.
- Shutdown: User switches off kit after measurement is complete, and data is exported.
- Emergency Shutdown: User can kill power to kit in case of an emergency.

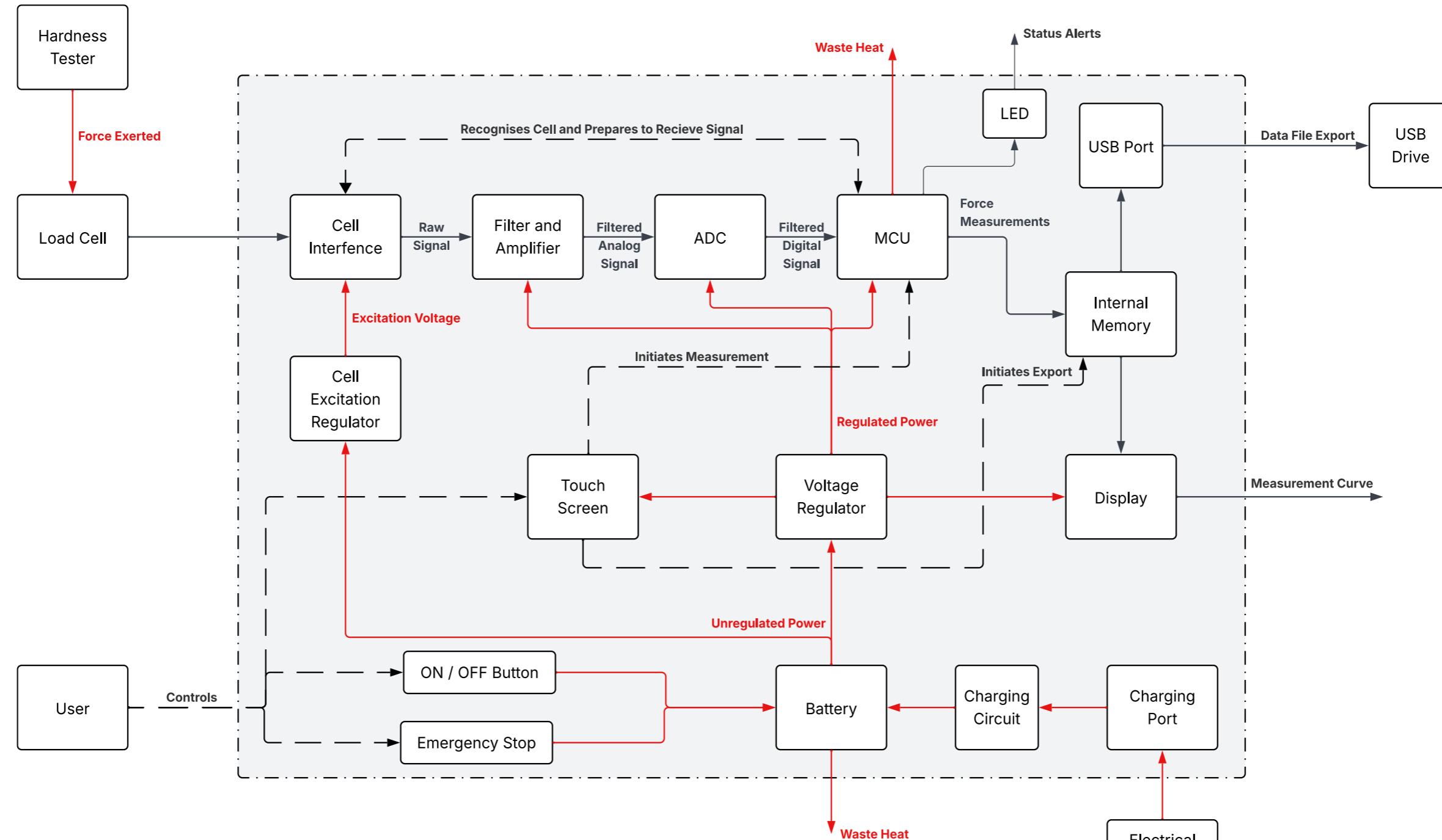
4.2. System Boundaries and Interactions

To create a structure of the system functionalities, the exact boundary of the system and its interactions with the environment must be outlined.

- System Boundary:
 - Internal electrical components that make up the filter, amplifier, ADC, microcontroller, and internal memory
 - HMI including the touchscreen, push buttons, LED, and USB A port
 - Power management system including the battery, charging circuit and USB C port
 - Interior of the carrying case housing
 - The interface port for the load cell
- External Environment:
 - User

- Load cell
- Hardness tester
- USB drive
- Source of electrical power
- Interactions:
 - User inputs commands
 - Load cell signals are sent for processing
 - Display shows measurement curve to the user
 - LED alerts the user of the system status
 - Measured data is exported to USB drive
 - External power source charges internal battery

4.3. Functional Structure Diagram (FSD)



Key:



Component → Flow of Data and Information

—→ Flow of Control Signal



System Boundary → Flow of Energy

5. Human Machine Interface

5.1. Human Machine Interface Overview

The Human Machine Interface section is a crucial part of the design process, as it converts the conceptual design of the product and functional structure into a tangible method of interaction for the end user. This must be done keeping three things in mind: clarity, simplicity, and safety.

The objective behind developing a good Human Machine Interface system is a satisfied customer, as it is the primary interaction an end user has with a system and is the basis of their opinion about the product. A good HMI system could lead to a user being able to do the same tasks successfully in a much more time efficient manner and have more focus towards the task rather than getting the system to work.

To make this a successful system, the product must fulfil all the functional requirements and functions mentioned in the sections above which specifically include managing the display operation, facilitating basic calibration of the cell, and handling data logging and export functionality. This also must be done while keeping in mind ergonomics and safety aspects of products.

5.2. Inputs and Outputs

Based on the functions discussed in Section 4, here is a list of all the inputs and outputs interactions between the system and the user.⁶

Table 8: Input/Output Interactions of Product with User

Interaction	Purpose	Input/Output	Character
Power on/off	To turn on/off the system	Input	Digital control signal
Battery/Power level	Display battery percentage	Output	Text
Critical Battery/Power alert	Alert user if battery too low, or in case of power fault	Output	Text / LED
Battery charging indicator	Indicate if battery is charging or full	Output	Text / LED
Menu navigation	Move between the different functions of the device	Input	Digital control signal
System status indicator	Alert user if system busy for interaction	Output	Text / LED

⁶ Some I/O interaction ideas taken from ChatGPT

Load cell detection	Inform user if load cell detected or not	Output	Text
Load cell disconnection	If load cell is disconnected alert the user	Output	Text / LED
Load cell naming	Allow user to name individual load cell	Input	Digital control signal / Text
Start calibration	To get system ready for calibration/reading data	Input	Digital control signal
Calibration begins	Let users know calibration process is starting	Output	Text
Calibration status	Let user know if calibration was completed successfully or not	Output	Text
Start/Stop logging	Start/Stop recording data	Input	Digital control signal
Force signal onto load cell	Receive raw analogue signal from load cell, converted via 24-bit ADC for processing	Input	Analog variable
Store processed data	Confirms data is stored to the user	Output	Text
Display current data	Process and show data visually currently being read	Output	Text / Graph
Emergency cancel calibration	Cancel calibration at any point	Input	Tactile button (External interrupt)
Tare command	Set current force reading to zero	Input	Digital control signal
Storage full alert	Inform user if internal storage is full on device	Output	Text
Old data deletion confirmation	Ask users if older data can be deleted	Input	Digital control signal
USB Drive plugged in confirmation	Confirm a device being connected	Output	Text
Data export trigger	Get data in state to export onto a USB drive	Input	Digital control signal
Data export confirmation	Let user know if data was exported successfully	Output	Text
Error detection	Let user know in case of error with troubleshooting steps	Output	Text

Error reset	User clears error message	Input	Digital control signal
Data display format change	Allow users to customize data display format	Input	Digital control signal / Text / Numeric
Data display unit change	Allow user to change the unit of displaying	Input	Digital control signal / Text / Numeric
Current unit display	Display the currently used unit (N, kgf etc.)	Output	Text
USB Ejection trigger	End all tasks using USB drive	Input	Digital control signal
USB Ejection confirmation	Ensure no tasks are using USB drive	Output	Text
Peak and hold value function trigger	Record measurements and keeping only the highest measured value	Input	Digital control signal
Emergency peak and hold value function stop	Stop peak and hold value	Input	Tactile button (External interrupt)
Peak and hold value display	Show the maximum force value captured by the peak and hold function	Output	Text
Interaction	Purpose	Input/Output	Character

5.3. Control Elements

Table 9: Selection of control elements

Control Element	Function	Type	Further consideration
ON/OFF button	Power on/off the device	Tactile button	
Emergency Stop button	Button to cancel an operation in case of emergency	Tactile button	This button should be harder to press
Touch screen display	Show data, help user navigate, take inputs	LCD Resistive Touch screen	Should be usable with gloves
LED Status Indicator	Indicate in case of critical alert	RGB LED	Should not extrude out of the device for durability reasons

LED Charging indicator	Indicate if battery is charging or full	RGB LED	Should not extrude out of the device for durability reasons
USB A Port	Data export	USB Type A 2.0 female port	
USB C port	Power supply	USB C Female port	
Load cell connector port	To connect any Innovatest load cell	5-pin M12 Circular Connector	Should not disconnect too easily

5.4. Safety Aspects

5.4.1. Data Safety

For such devices data is crucial and losing it can mean hours of work to be repeated. So, for data safety these things are to be considered and followed:

- USB Ejection Protocol: prevent data corruption when USB Drive is removed.
- Battery/Power alert: alert user in case of low/unstable power
- Automatic data backup: periodically save data to minimize problems in case of unexpected interruptions.

5.4.2. Operational Safety

This aspect of safety is necessary to be looked at to ensure user interaction with system is only under safe and valid conditions.

- System status indicator: inform user when system is busy/unsafe for interaction.
- Lockout for critical operations: reduce/remove interactions with system in case of certain critical operations such as file transfers.
- Emergency cancellation: allow user to abort both calibration and peak and hold function in case required, for instance in case of the screen hanging.

5.4.3. Hardware and Environmental Safety

These measures must be taken to protect the load cells and the hardware itself from damage/misuse.

1. Overload protection: alert user as well as stop taking readings in case force exceeds load cell's safe range.

2. Port disconnection detection: alert user and stop process in case the load cell port is disconnected or unexpected readings are read.
3. Temperature warning: alert user in case device is nearing or out of its recommended temperature range for readings.

5.4.4. User Safety

Measures must be taken to protect the user within the environment as well, these include:

- Permit use with gloves: resistive touch screen has been chosen to permit use of screen with gloves, which will be required in the environment these devices are used in.
- Emergency cancel/stop button: a tactile button to cancel any process immediately in case of emergency such as evacuation of the working area. An external button permits user to cancel process even if screen freezes.

5.5. Control Elements Arrangement

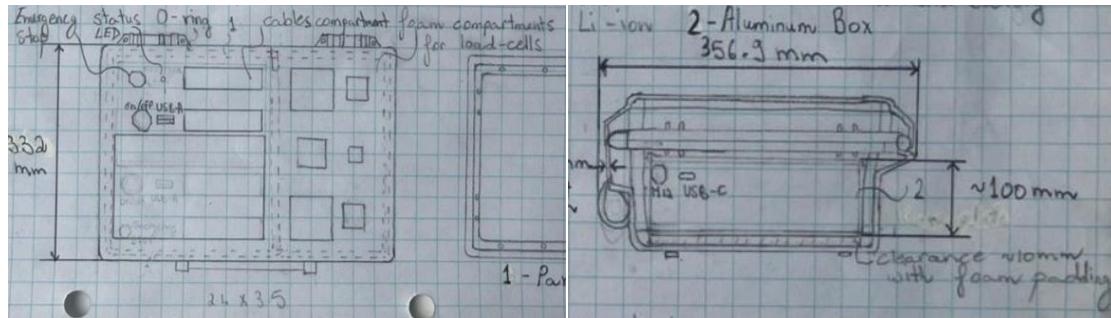


Figure 10:Arrangement of control elements (extracted from Freehand Sketch in Section 3.5)

The device has been made keeping the convenience and ergonomics of the user in mind. The power button has been placed right above the screen for easy access and has the led for telling the status of the battery on it for easy visibility. The emergency button has been placed away from all other used devices, to prevent accidental presses, but close enough for pressing in case of an emergency. The status indicator has been placed beside it to see if the device is busy or not. Keeping the similar function I/O together makes the design more intuitive for the user.

The screen has been kept closer to the opening of the case, for easy access for the user. Even in case of a USB-stick plugged into the device, it will not interrupt the user or make it uncomfortable because it is above the screen.

The charging port and M12 connector for load cells have been kept outside, so that no cables are sticking out from the inside of the case which could have also been damaged in case of the case being closed. Charging port being available while case is closed also makes it easier to charge.

5.6. User Interface Design Description

Upon start up, the user will be met with a login screen to access the device only with valid credentials. All buttons will be big and clearly visible with high contrast.

Upon logging in, the main menu will be shown, allowing the user to go between different functions: calibration, settings, peak and hold value, data read/export, etc. At the top left of the screen, there will be permanently placed navigation buttons for back-and-forth navigation between the menus. The placement is also keeping in mind the familiarity of users with today's software. On the top right there will be a battery percentage indicator also permanently visible again for similar reasons.

Upon going into calibration menu, the user will be asked to connect the load cell, if not already connected. Upon connection the UI will also let the user know which load cell has been connected. After confirmation from user for starting calibration, if load cell connected, the system will start the calibration process. While calibration takes place, the readings will be shown while also plotting a graph of force vs time, with units visible as well. After calibration, the data will be saved with a name by default, according to time, with an option to be modified by user.

The settings menu will allow the user to change units, adjust brightness, reset/restart device, and some other settings. Furthermore, peak-hold function will allow user to see the maximum value being displayed with its units.

Lastly, the data menu will allow user to access older saved recordings, as well an option to export the data to the USB-stick, considering one is connected and detected. Upon pressing the power button, the UI will ask user for confirmation for shutdown and close all processes before powering off.

5.7. Ergonomics Aspects Considered

For a device to be used for hours at a stretch, its ergonomics must be considered. The device is designed keeping in mind that the user will travel with it and therefore an inbuilt handle has been provided. The handle of pelican cases is also ergonomically shaped (Mostafawi Group, 2024). The latches are made to be secure and easy to close for a secure closure of the case. The foam inside the case also prevents movement of equipment inside, which would hamper the weight distribution while carrying and affect the comfort of carrying the case.

Placing related items together, makes the experience better for the user, for example the power button right next to the main screen, as well as the USB-A port used to extract data from the device.

The system's user interface will also be designed keeping ergonomics in mind. For easy understanding of data being read, analogue values will be read whilst also plotting a graph to visualize the data. The UI will also not be violating any stereotypes of traditional and already familiar user interface designs. This, for instance, includes placing the navigation

icons on top left, and graphs being growing from left to right on x-axis and bottom to top on y-axis (European Commission, 2010).

6. Design-Failure Mode and Effect Analysis (D-FMEA)

6.1. D-FMEA Rating Scheme

FMEA is a formalised analytical method for the systematic identification of possible failures and the estimation of the related risks (Pahl, Beitz, Feldhusen & Grote, 2007). It helps quantitatively illustrate the potential failures of the product.

Three Factors must be considered:

- Severity (S) – An estimation of the effects of the failure on the customer
- Occurrence (O) – An estimation of the probability of occurrence
- Detection (D) – An estimation of the probability that the failure can be detected before delivery.

With these factors, the Risk Probability Number (*RPN*) can be calculated using Equation (1):

$$RPN = S \cdot O \cdot D^7 \quad (1)$$

Any *RPN* greater than 125 is considered critical and requires action.

The rating schemes for these factors and the calculated Risk Number are as follows:

Table 10: Rating Scheme for Severity (S)

Rating	Effect on Customers
1	Effects hardly noticeable
2-3	Failures not important (little trouble to the user)
4-6	Reasonably serious failure (difficult to use)
7-8	Serious failure (annoying for the user)
9-10	Failure with large negative effects (almost unusable)

Table 11: Rating Scheme for Occurrence (O)

Rating	Probability of Occurrence
1	Very low
2-3	Medium low
4-6	Medium (occasional)
7-8	Medium high

⁷ (Juran, 2024)

9-10	High likelihood (almost inevitable)
------	-------------------------------------

Table 12: Rating Scheme for Detection (D) Probability

Rating	Probability of Detection
1	High (obvious)
2-5	Medium high
6-8	Medium (detectable in quality control)
9	Medium low
10	Low (almost undetectable)

6.2. D-FMEA Table

Table 13: Design Failure Mode and Effect Analysis of the Product

Component	Function	Failure Mode	Potential Effect	Potential Cause	S	O	D	RPN	Recommended Actions
Load Cell Interface	Connect sensor to electronics	No function	Device reads zero, cannot measure	Broken wiring, open bridge	10	2	4	80	Check wiring, add diagnostics
		Underfunction	Low readings, poor precision	Connector corrosion, broken wires	6	4	5	120	Check wiring, scheduled calibration and maintenance
		Overfunction	Overstated readings	Shorted bridge, wrong polarity	9	3	5	135	Add diagnostics, plausibility checks
		Intermittent	Glitches or dropouts	Loose crimp, connector mismatch	6	6	7	252	Securing connectors, strain relief
Load Cell Excitation Regulator	Supply regulated voltage to sensor	Underfunction	Gain error, low readings	Regulator drift, battery sag	8	4	5	160	Use high precision regulator, monitor Vcc
		Overfunction	Pegged output, sensor damage	Transient surge	9	2	5	90	TVS diodes, input protection
		Intermittent	Temporary gain shifts	Loose connector	7	3	6	126	Monitor Vcc, secure connectors
		Malfunction	Sensor damaged, erratic readings	Voltage spike or regulator failure	9	2	5	90	Surge protection
Signal Conditioning Chain	Filter & compensate signal	Underfunction	Biased readings	Missing compensation	8	4	5	160	Add temperature sensor, compensation
		Overfunction	Slow response	Low cutoff	6	4	4	96	Tuning filters
		Malfunction	Permanent biased readings	Faulty filter components	8	3	4	96	Add diagnostics checks
ADC	Convert analog to digital	Underfunction	Small loads unreadable	Wrong gain	7	4	5	140	Precise calibration
		Overfunction	Maxed readings	Amplifier saturation	8	3	5	120	Clamping diodes
		Malfunction	Readings always incorrect or pegged	ADC/amplifier damage	9	2	5	90	Clamping diodes and current limiting resistors
Microcontroller	Process & manage data	No function	Device unresponsive	Memory corruption	9	3	4	108	Watchdog, regression tests
		Underfunction	Non-linear readings	Wrong coefficients	7	4	5	140	Validate algorithm, calibration
		Intermittent	Missed samples	RTOS issue	7	3	4	84	Priority config, watchdog
		Malfunction	Device unresponsive, no measurement	Firmware crash or hang	10	3	5	150	Watchdog, firmware rollback
Display	Show measurement	No function	No visible readings	Display driver failure	9	3	4	108	Driver check, display replacement
		Underfunction	Truncated readings	UI bug	5	4	4	80	Check formatting, raw view
		Overfunction	Displayed values incorrect	Unit mapping bug	8	3	5	120	End-to-end checks

		Intermittent	Blank/flickering display	Race condition	6	5	5	150	Decouple refresh
Buttons	User interaction tactile buttons	No function	Buttons stuck in pressed state	Broken spring	9	5	1	45	Use good quality springs
		Underfunction	Buttons require excessive force	Button contacts damaged	4	4	4	64	Increase buffer rating
		Overfunction	Repeated operation for single press	Contact bouncing	5	6	6	180	Implement software debouncing
		Intermittent	Occasionally presses unregistered	Contact contamination	5	6	5	150	Ensure a clean environment near button soldering
Touch Screen	User interaction with screen	No function	Unresponsive touch screen	Touch controller failure	9	4	3	108	Test screen functionality, replace controller if required
		Underfunction	Harder press for click registering	Spacer dots are too large / too few	5	6	5	150	Ensure precision application of spacer dots
		Overfunction	Multiple touches for same touch	Contact bouncing	6	4	4	96	Increase debounce time
		Intermittent	Occasional touches unregistered	Presence of conductive debris	6	7	4	168	Ensure a clean environment near panel assembly
		Malfunction	Ghost interactions	Layers stick together due to adhesive failure	9	5	4	180	Ensure a clean environment near panel assembly
Internal Memory and USB Port	Record & export data	Overfunction	Data overwritten	Too frequent logs	6	3	6	108	Limit data rate, alarms
		Intermittent	Partial file transfer	Voltage fluctuation disrupts write process	6	6	6	216	Brown-out detector
		Malfunction	Cannot retrieve data	Flash memory corruption	9	2	4	72	CRC Checks, periodic memory dumps
Battery	Provide power to device	No function	Device does not power on	Battery failure	10	2	4	80	Battery test/replacement
		Underfunction	Short operating time	Parasitic drain	9	4	5	180	Monitor battery drain
		Overfunction	Battery damage	Faulty charger	10	2	4	80	Certified IC, thermal cutout
		Intermittent	Unexpected resets	Loose connector	9	4	4	144	Secure connectors, brown-out
		Malfunction	Battery swelling or fire	Overcharge or short	10	2	2	40	Overcharge alerts
Housing Fasteners	Provide mechanical structure	Overfunction	Overstressing the housing	Fasteners too tight	5	3	4	60	Determine precise fastening torque for material
		Intermittent	Occasional misalignment	Loose fasteners	6	4	6	144	Retention clips, torque specification
Housing Protection	Protect electronics	No function	System stops working	Water ingress	10	1	2	20	Regular QA inspection
		Underfunction	Moisture ingress, corrosion	Gasket wear	8	2	6	96	Purchasing high durability gaskets
		Intermittent	Short, transient faults	Poor assembly	9	5	4	180	IP connectors, QA

7. 3D Model

7.1. Protective Case

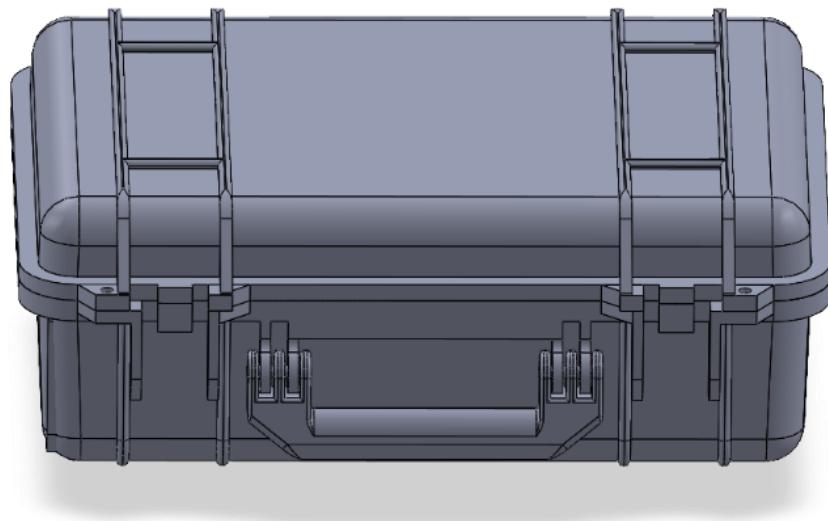


Figure 11: Protective Carrying Case Model



Figure 12: Isometric View of Complete 3D Model

7.2. HMI

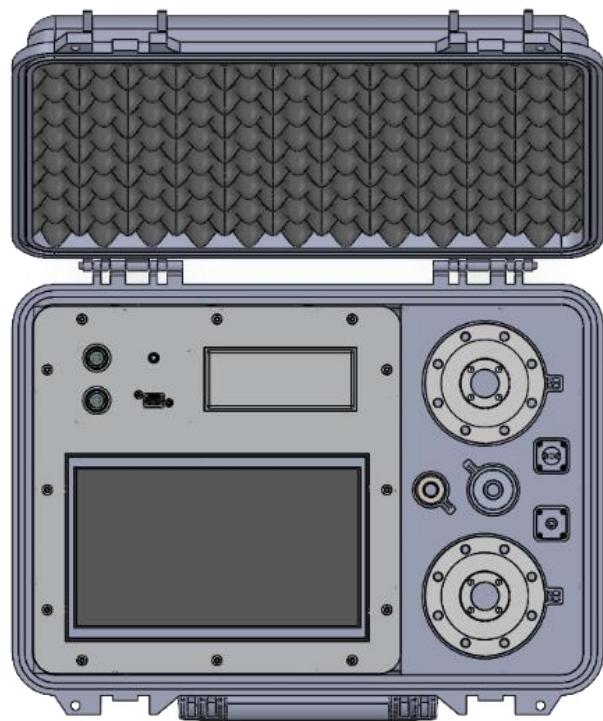


Figure 13: Top View of Complete 3D Model showing HMI

7.3. Interior

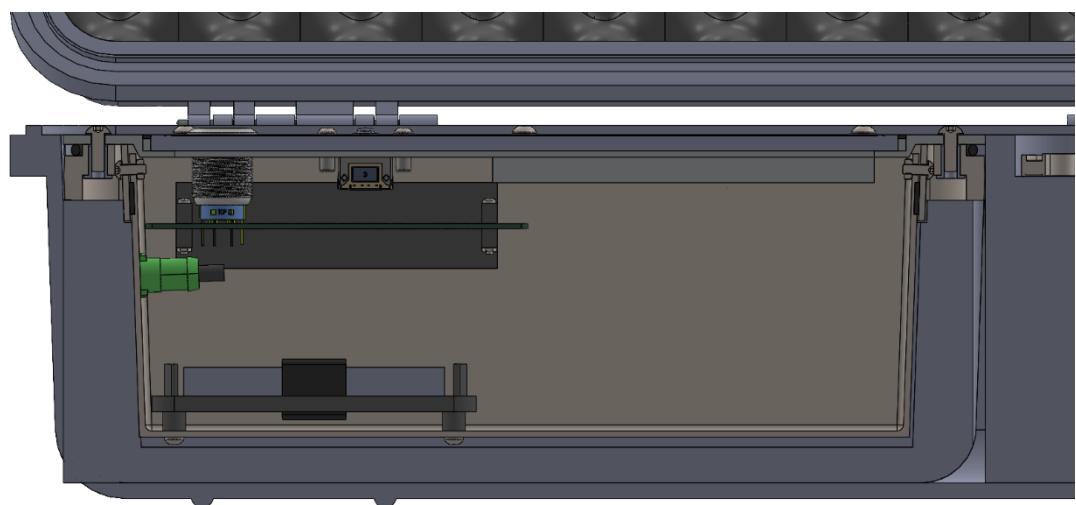


Figure 14: Interior of Complete 3D Model showing PCB, Battery and Aluminium Frame

7.4. Load Cell Connector

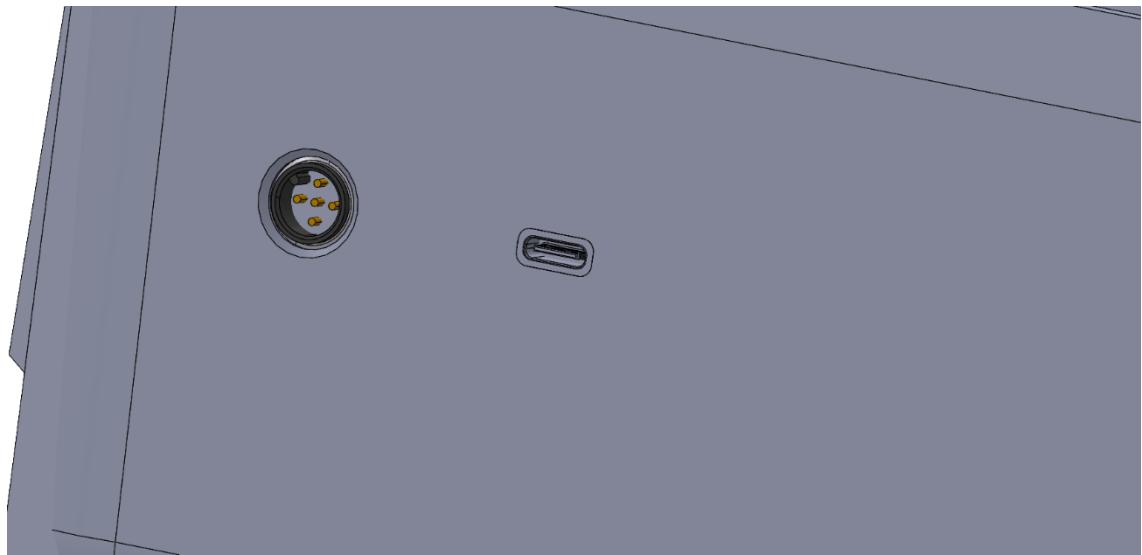


Figure 15: Connectors on the Complete 3D Model for Load Cells and Charing

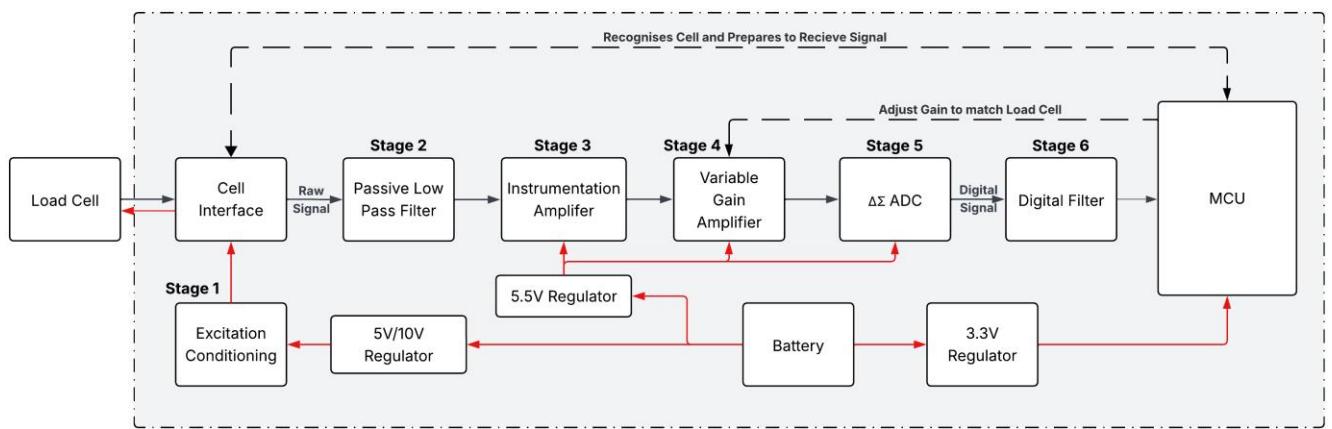
8. Technical Drawing of Main Assembly

9. Measurement Chain

9.1. Architecture

For the signal to be processed by the microcontroller, the raw signal needs to undergo the following stages of signal conditioning:

1. Excitation Conditioning
2. Passive Low Pass Filtering
3. Instrumentation Amplification
4. Precision Variable Gain Amplification
5. Analogue to Digital Conversion (ADC)
6. Digital Filtering



Key:

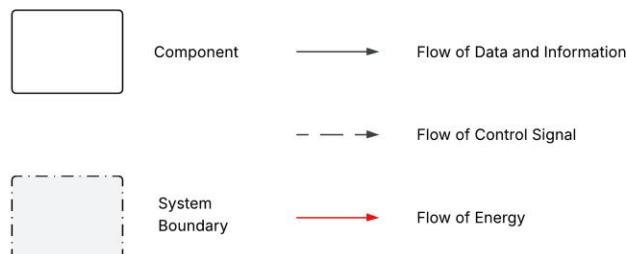


Figure 16: Functional Structure Diagram of Measurement Chain

In order to implement the measurement chain such that it can meet all the reliability and performance requirements; each stage uses dedicated integrated circuits (ICs) and passives instead of using a complete analogue front end chip like the HX711 or AD7794, as they do not allow for the functionality, precision and accuracy that is necessary for this product.

9.2. Schematic

9.3. Design of Signal Conditioning Stages

9.3.1. Excitation Conditioning

To minimise the power fluctuation noise, the power supply for the load cells must be conditioned with low-noise boost converters and decoupling.

One of the leading noise components in many instrumentation applications is the fluctuations in the power supply. To reduce the noise introduced by battery fluctuations, low noise boost converters are used. Three of these devices are used to create three power rails: 5V, 5.5V and 10V. The 5V and 10V rails are switchable via a power MOSFET switching network and provide excitation to the load cells. The 5.5V supply powers the devices in the measurement chain. These devices ensure the mean voltage level remains relatively constant with a low voltage ripple. For the load cell excitation rails, this is incredibly important as it ensures that the measurements are consistent and application of the same force yields the same voltage response. Additionally, the switching network was configured such that one supply rail is active the other is completely cut off. This ensures that there is no overcurrent and that noise in one rail does not affect the other.

Another important process in mitigating noise is using decoupling capacitors. $10\mu F$ and $0.1\mu F$ capacitors (or a parallel combination) are used to on the supplies of each IC to ensure that they are decoupled from the ground plane. This helps to reduce interference between the ICs, especially between the analogue and digital devices.

9.3.2. Passive Low Pass Filtering

To reject high frequency noise while also reducing the chances of aliasing, a series of passive low pass RC filters are to be implemented between the other stages.

Since the device is measuring only a series of static forces, the frequency of the relevant signal is effectively zero. These filters thus remove all noise components with a frequency higher than 4.98Hz. This includes noise caused by electromagnetic interference and power supply fluctuations. Additionally, for the input of the instrumentation amplifier, a differential RC filter was used with matched resistors to preserve the Common Mode Rejection Ratio (CMRR). To ensure noise is reduced across the entire measurement chain, a series of filters are used between each stage up to the ADC. These stages also have their own noise filtering properties, so, to reduce settling times, the filters get “looser” with each stage, that is the specified corner frequency increases to 7.2Hz between stages 3 and 4 and 19.86Hz between stages 4 and 5.

To dimension the RC filters, the corner frequency formula as shown in Equation (2) is used.

$$f_c = \frac{1}{2\pi RC} \quad (2)$$

Detailed calculations for the relevant resistor and capacitor values as well as the corner frequencies and settling times of each filter can be found in Appendix C (19.3.1).

9.3.3. Instrumentation Amplification

To amplify the signal for readability while also providing common mode rejection, an Instrumentation Amplifier (INA) is to be implemented. The two signal lines from the load cell enter the INA and the amplified differential output is sent to the next stage.

The load cells output a very small differential signal of around 14mV⁸ when excited with 5V and 28mV when excited at 10V. As such, they need to be amplified with minimal noise. The INA allows for high gains with very low noise and high CMRR. This means that it can amplify the signal and reject common noise from both signal lines all while adding very little device noise. However, the different load cell models have different sensitivities and thus require different gains for full utilisation. To solve this issue, the INA is used as pre-amplifier to provide most of the required gain with low noise injections and a Precision Variable Gain Amplifier is used in the following stage for the remaining gain. The INA provides a gain of 100, which is less than the minimum gain of 307.69 required any of the load cells.

9.3.4. Precision Variable Gain Amplification

To compensate for the remaining gain, a precision variable gain amplifier (VGA) is to be implemented as a second stage amplifier.

After pre-amplification by the INA, the VGA provides the small remaining gain and is programmed to match the specific gain required by each load cell. To implement this precision VGA, a simple non-inverting operational amplifier (op-amp) is set up with a digital potentiometer acting as the feedback resistor.

To calculate the gain required by a load cell, the Equation (3) is used.

$$G = \frac{5000mV}{SEN \cdot V_E} \quad (3)$$

Where SEN is the sensitivity of the load cell [mV/V], V_E is the excitation voltage.

The remaining gain is then calculated by dividing the required gain by 100 from the INA. The gain values for 5V and 10V excitation are shown in Table 14 and Table 15 respectively.

The gain of a non-inverting amplifier can be calculated using Equation (4) and hence the resistance of the potentiometer is calculated using Equation (5).

⁸ This saturated voltage output of all six load cells averaged and rounded to the nearest mV

$$G = 1 + \frac{R_F}{R_N} \quad (4)$$

$$R_F = R_N(G - 1) \quad (5)$$

Where G is gain, R_F is the resistance of the feedback resistor and R_N is the resistance of the resistor at the negative input of the op-amp.

Using an OPA188 op-amp, a MCP41U83 digital potentiometer and a fixed $4.99\text{k}\Omega$ resistor (at the negative input), the required gains are achievable with a maximum gain error of 0.162%. Table 14 shows all the gains required for each load cell, the dimensioned R_F values and the resulting gain error for 5V excitation. Table 15 shows the same for 10V excitation. The gain has an inherent error since the MCP41U83 has a precision of 1024 positions over the $20\text{k}\Omega$ range and cannot match the gain exactly. So, to estimate the gain error, the position was first estimated by mapping the required resistance over the $20\text{k}\Omega$ range using Equation (6) to a position and rounded down to the nearest integer. The position value was then used to find the exact resistance using Equation (7) and thus the actual gain using Equation (4). The gain error is simply the difference between the actual and remaining gain divided by the remaining gain.

$$D = \left\lfloor 1024 \cdot \frac{R_F}{20\text{k}\Omega} \right\rfloor \quad (6)$$

$$R_F^{actual} = 20\text{k}\Omega \cdot \frac{D}{1024} \quad (7)$$

Table 14: Required Gains and Gain Error for Each Load Cell for 5V Excitation (Using OPA188 and MCP41U83)

Load Cell Model [kgf]	Sensitivity [mV]	Required Gain	Remaining Gain	R_F [kΩ]	Gain Error
0.15	3	333.33	3.33	11.64	0.016%
2	2.35	425.53	4.26	16.24	0.064%
20	2.7	370.37	3.70	13.49	0.081%
45	3	333.33	3.33	11.64	0.016%
250	3.25	307.69	3.08	10.36	0.080%
3000	2.8	357.14	3.57	12.83	0.106%

Table 15: Required Gains and Gain Error for Each Load Cell for 10V Excitation (Using OPA188 and MCP41U83)

Load Cell Model [kgf]	Sensitivity [mV]	Required Gain	Remaining Gain	R_F [kΩ]	Gain Error
0.15	3	166.67	1.67	3.33	0.076%
2	2.35	212.77	2.13	5.63	0.019%
20	2.7	185.19	1.85	4.25	0.135%
45	3	166.67	1.67	3.33	0.076%
250	3.25	153.85	1.54	2.69	0.145%
3000	2.8	178.57	1.79	3.92	0.162%

9.3.5. Analogue to Digital Conversion

To convert the analogue voltage into a digital signal that the microcontroller can process, a 24-bit delta-sigma ADC was used because of its high precision and low noise output.

The load cells output very small analogue voltages of at most 32.5mV. For the microcontroller to process them, the signals need to be sampled and converted into digital values with enough precision that measurement and calibration are possible at an industry standard level. A 24-bit ADC has a theoretical resolution of 298nV which means there are 16, 777, 216 possible voltage levels and thus force values that can be read. This of course doesn't account for noise which is discussed in Section 10.6 Noise Performance. However, the 24-bit ADC is more than sufficient to meet precision requirements. The delta-sigma architecture also employs over-sampling through the modulator which allows for a simplified anti-aliasing filter while still following the Shannon-Nyquist Theorem. This over-sampling process also spreads the quantisation noise over a much higher bandwidth than that of the signal. The oversampling ratio (OSR) can also be modified to effectively change the sampling rate. Most delta-sigma ADC chips also have an on-board digital filter which further helps to reduce noise and aliasing. This is discussed in further detail in Section 9.3.6 Digital Filtering.

For the ADC to operate with the best accuracy, a voltage reference IC is also required. This IC must be able to reliably provide 5V to the ADC reference pins. Thus, it must have low noise and a low drop-out voltage. It should also be noted that the ADC will only use 5V as a reference voltage despite the load cell excitation voltages being switchable between 5V and 10V. This is primarily a technical limitation since there are no reliable ADC ICs on the market that can handle both 5V and 10V references. The 10V excitation does still provide a higher signal-to-noise ratio however since the load cell and excitation noise do not change much between 5V and 10V while the applied voltage is doubled.

9.3.6. Digital Filtering

To reduce random in-band noise and quantisation noise, a programmable finite impulse response (FIR) and infinite impulse response (IIR) filters are to be applied to the signal as substages within the ADC IC.

Even after the previous filtering stages, the signal still has some quantisation noise introduced by the ADC process and random in-band noise from environmental conditions. Digital filtering allows for removal of these random noise components as well as the flexibility to shape the noise profile. Most delta-sigma ADC ICs have built-in FIR and IIR filters which reduces the required processing load on the microcontroller.

The FIR filter performs weighted averaging across many samples where each sample is multiplied by a corresponding filter coefficient. This allows the FIR filter to effectively act as a digital low-pass filter which helps to reduce the out-of-band quantisation noise.

This noise is spread across a very large bandwidth due to the oversampling of the ADC. The averaging also helps to remove some random noise. After this substage, the signal undergoes decimation whereby it is downsampled to the desired data transfer speed. It is imperative that the FIR substage occurs before the decimation because otherwise the signal may experience aliasing.

The IIR filter use a feedback structure which allows it to suppress specific frequencies. This is especially effective against 50/60Hz “Hum Noise” and other known noise components. IIR filters also require less coefficients than an equivalent FIR filter so using it as a second substage to the FIR filter allows for overall lower computation for the same performance.

9.4. Component Specifications

Table 16: List of Components and Specifications for Measurement Chain

Stage	Component	Specifications	Potential Candidate
1	5V Regulator	<ul style="list-style-type: none"> • 5V output • > 80 % efficiency to keep power losses low • ≤ 0.1 mV noise at output 	TPS61099
1	10V Regulator	<ul style="list-style-type: none"> • 10V output • > 80 % efficiency to keep power losses low • ≤ 0.1 mV noise at output 	TPS61170
1	5.5V Regulator	<ul style="list-style-type: none"> • 5.5V output • > 80 % efficiency to keep power losses low • ≤ 0.1 mV noise at output 	TPS61089
2	RC Filter	<ul style="list-style-type: none"> • Passive components to ensure reliability and lower power consumption • Around 5 to 8 to 20 Hz successively increasing corner frequency • < 5Hz Bandwidth to block all higher frequency noise 	-
2	Resistors	<ul style="list-style-type: none"> • 0.1% tolerance for accurate corner frequency dimensioning • Thin film resistor for best precision 	-
2	Capacitors	<ul style="list-style-type: none"> • 1% tolerance for accurate corner frequency dimensioning 	-

		<ul style="list-style-type: none"> • 3216⁹ package size for capacitors $\geq 10 \mu\text{F}$ for better bulk decoupling • 2012 package size for capacitors $< 10 \mu\text{F}$ to reduce inductance of components • X7R ceramic capacitors for stable capacitance values 	
3	INA	<ul style="list-style-type: none"> • 100 Gain set precision resistor (0.1% tolerance) • $> 124\text{dB}$ CMRR at Gain of 100 • $> 35 \text{ V}/\mu\text{s}$ slew rate for quick measurement times • $> 10 \text{ Hz}$ bandwidth at 100 gain to ensure it operates within system bandwidth. • $< 0.1 \mu\text{V}$ peak-to-peak noise (input) at gain of 100 to stay within noise budget • $> 5\text{V}$ single supply operation for compatibility with rest of measurement chain • 2–3 mA supply current to stay within power budget • 40V overvoltage protection • $< 0.3 \mu\text{V}/^\circ\text{C}$ offset drift to minimize effects of high temperature environments • $< 3 \text{ ppm}/^\circ\text{C}$ gain drift to minimize effects of high temperature environments 	AD8421
4	Operational Amplifier	<ul style="list-style-type: none"> • 1 – 5 gain range • $< 0.4 \mu\text{V}$ peak-to-peak noise to stay within noise budget • $> 5\text{V}$ single supply operation for compatibility with rest of measurement chain • 0.3 – 0.6 mA supply current to stay within power budget • Zero drift 	OPA188
4	Digital Potentiometer	<ul style="list-style-type: none"> • 1024 steps (or 10-bit resolution) to ensure precise gain selection • $20\text{k}\Omega$ range for easier dimensioning • Serial communication for programming of resistance • $< 5 \mu\text{A}$ supply current during normal operation to stay within power budget 	MCP41U83
5, 6	$\Delta\Sigma$ ADC	<ul style="list-style-type: none"> • 24-bit resolution to ensure precision requirements are met 	ADS127L21

⁹ Package sizes provided in metric (mm)

		<ul style="list-style-type: none"> • Programmable OSR to adjust sampling rate • On-board digital filter • Serial Peripheral Interface (SPI) for very fast data transfer speeds • 5V reference mode • Buffered inputs to reduce current draw and increase accuracy • $< 7\mu\text{V}$ peak-to-peak noise at input to stay within noise budget • 1 – 3 mA supply current to stay within power budget • > 5V single analogue supply operation for compatibility with rest of measurement chain • 3.3V isolated digital supply so that level shifting is not needed • $< 0.1 \mu\text{V}/^\circ\text{C}$ offset drift to minimize effects of high temperature environments • $< 1 \text{ ppm}/^\circ\text{C}$ gain drift to minimize effects of high temperature environments 	
5	Voltage Reference	<ul style="list-style-type: none"> • 5V reference output • $\pm 0.02\%$ accuracy for reliable ADC operation • $< 3\mu\text{V}$ peak-to-peak noise at input to stay within noise budget • < 1mA supply current to stay within power budget • < 0.5V voltage dropout • $< 1 \text{ ppm}/^\circ\text{C}$ voltage temperature coefficient of to minimize effects of high temperature environments 	MAX6126
6	Digital Filter	<ul style="list-style-type: none"> • Finite Impulse Response filter for removing quantisation and random noise • Infinite Impulse Response filter for removing specific noise components and reducing computational load • Integrated into ADC to reduce computational load of MCU • Decimation to downsample to desired data rate 	ADS127L21

10. Circuit Design

The circuit diagram was designed using specific components that were found to match the specifications required to operate and meet the requirements outlined in 3.1 Requirements List. These components are subject to change as the design is further developed, and all critical specifications are outlined in 14.1 Requirements for Electrical Parts. Note that all calculations and dimension was done using the datasheets and specifications of the chosen components.

10.1. Simplified Schematic Diagram

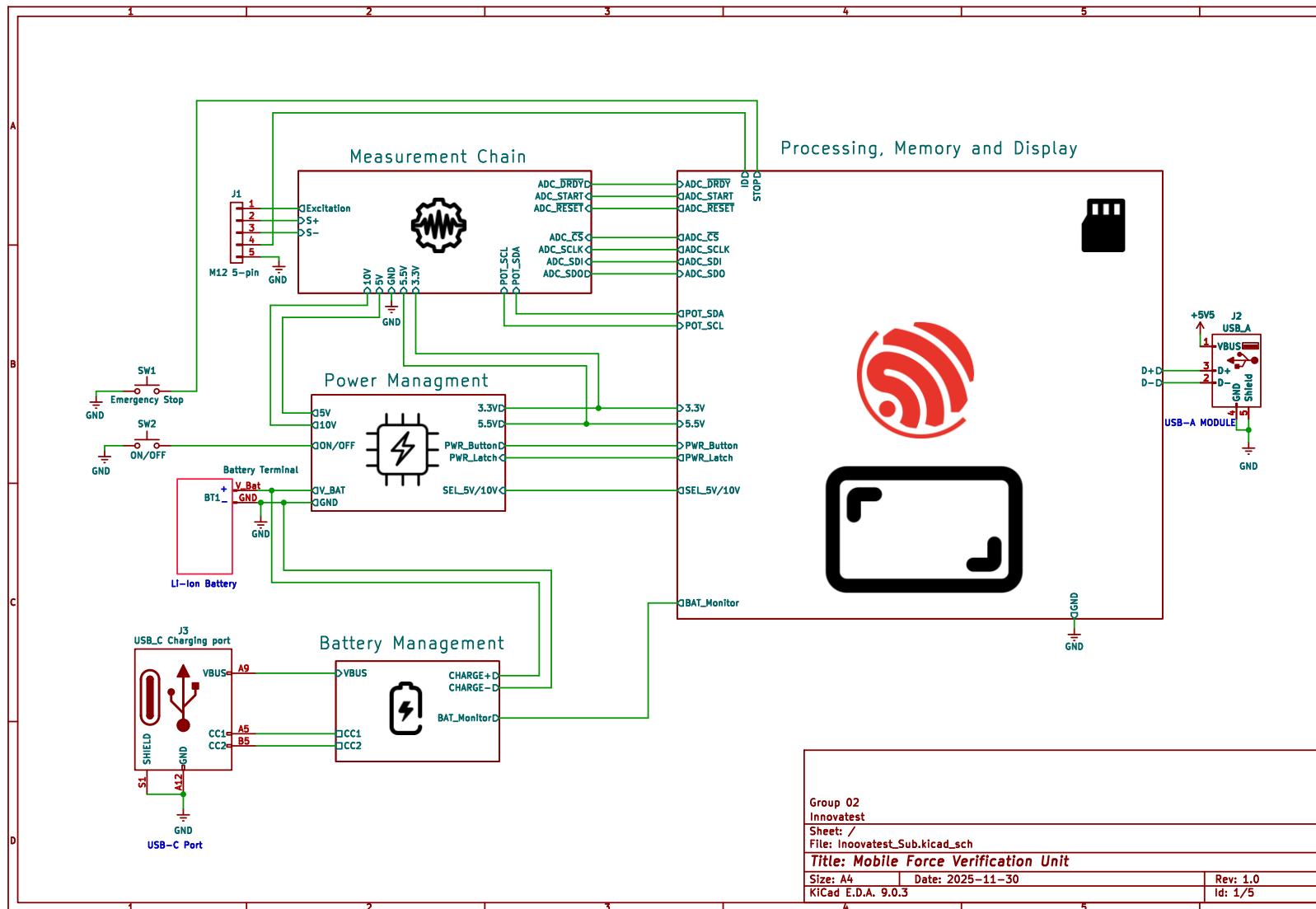


Figure 17: Simplified Schematic Diagram

10.2. Full Schematic Diagram

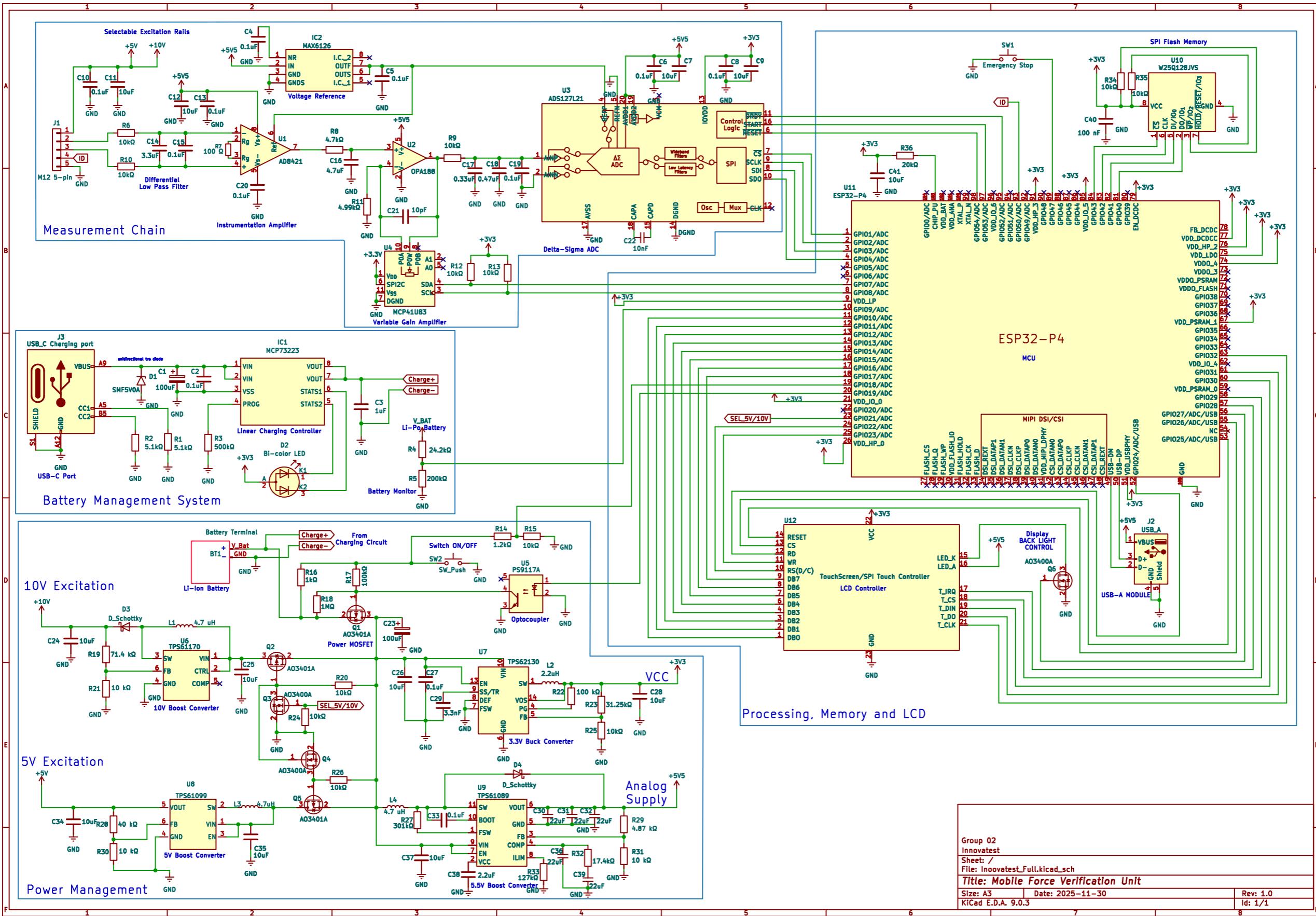


Figure 18: Full Detailed Schematic Diagram

10.3. Schematics of Subsystems

10.3.1. Main Controller

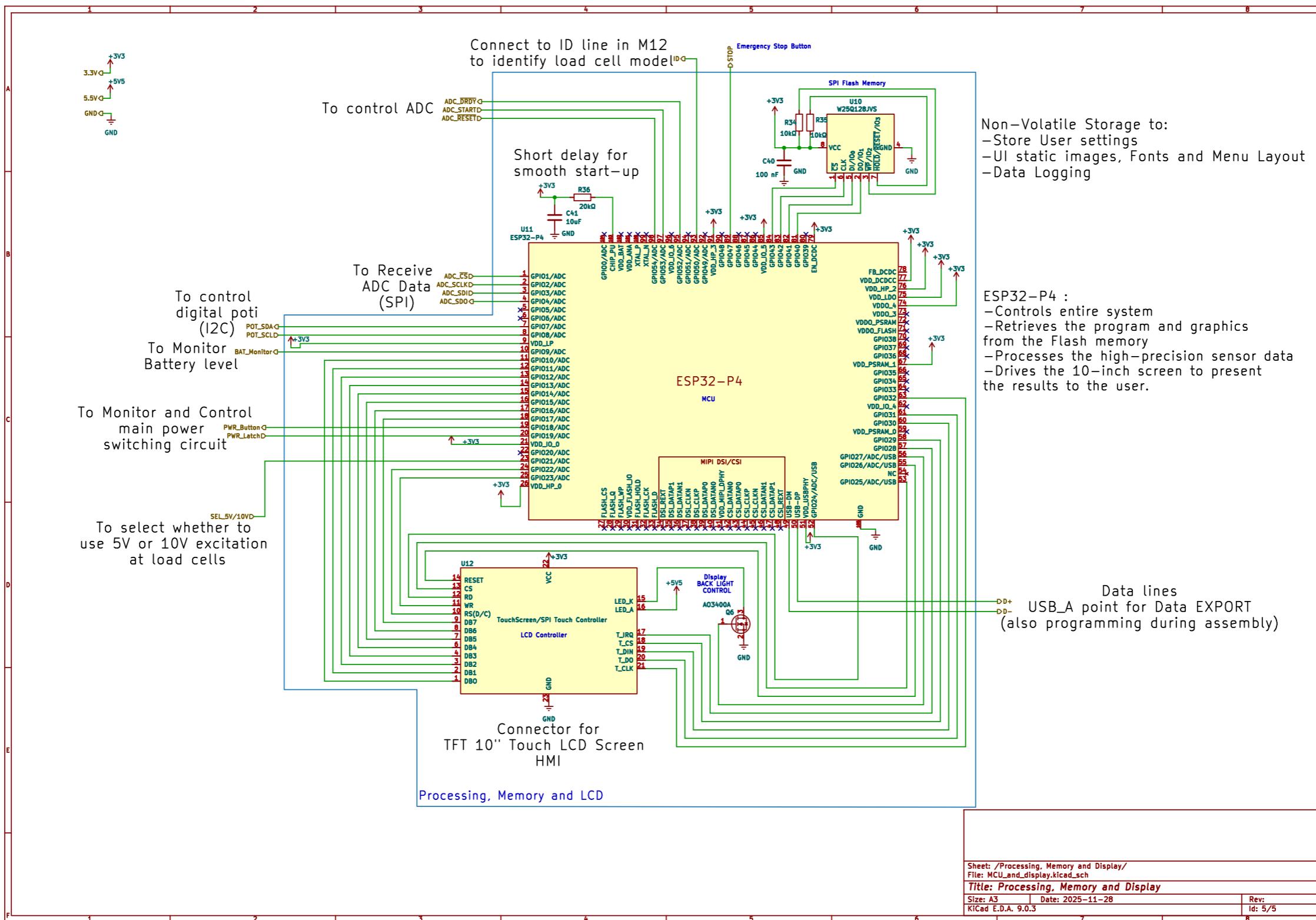


Figure 19: Processing, Memory and Display System Schematic Diagram

10.3.2. Power Regulation

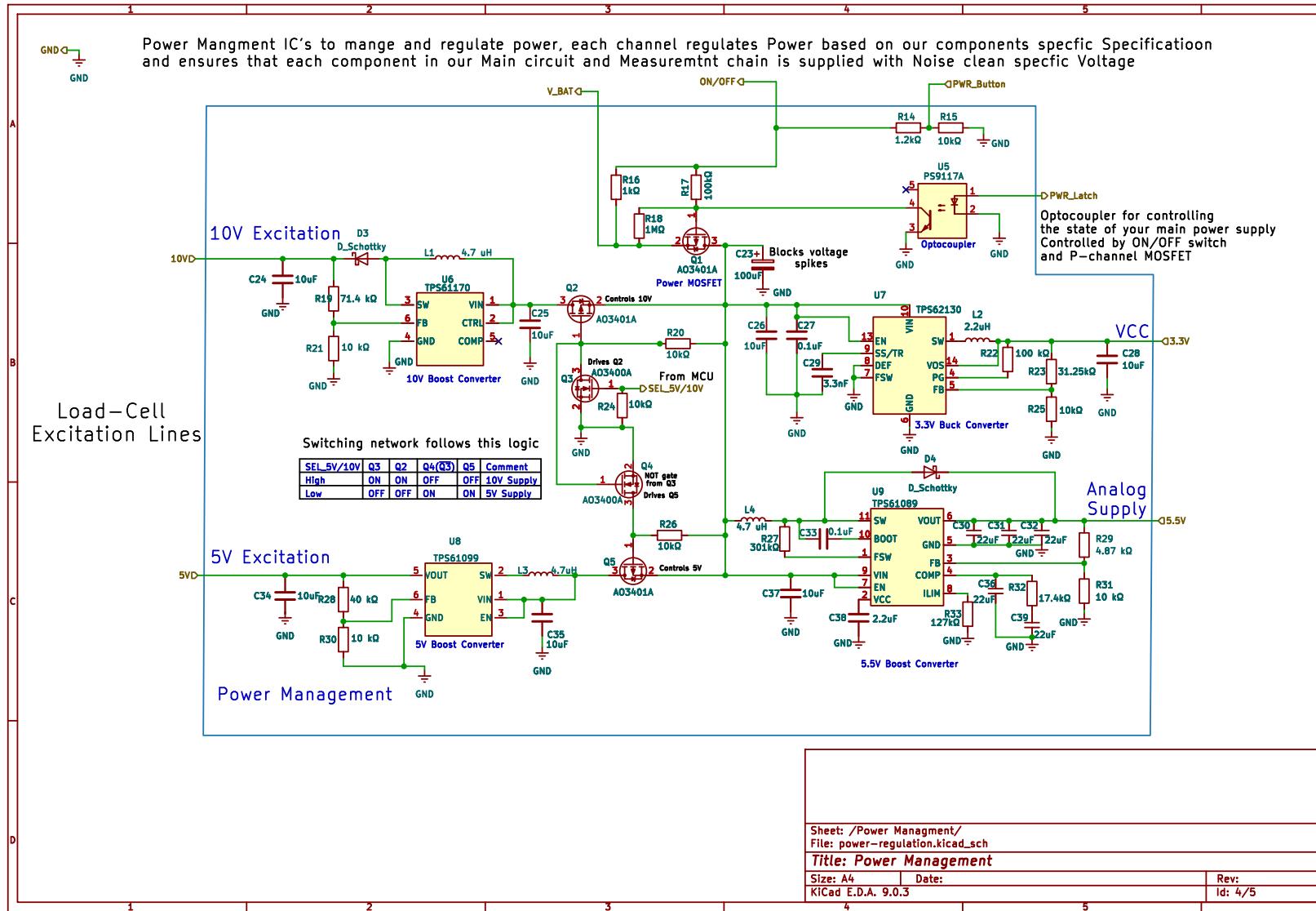


Figure 20: Power Regulation System Schematic Diagram

10.3.3. Measurement Chain

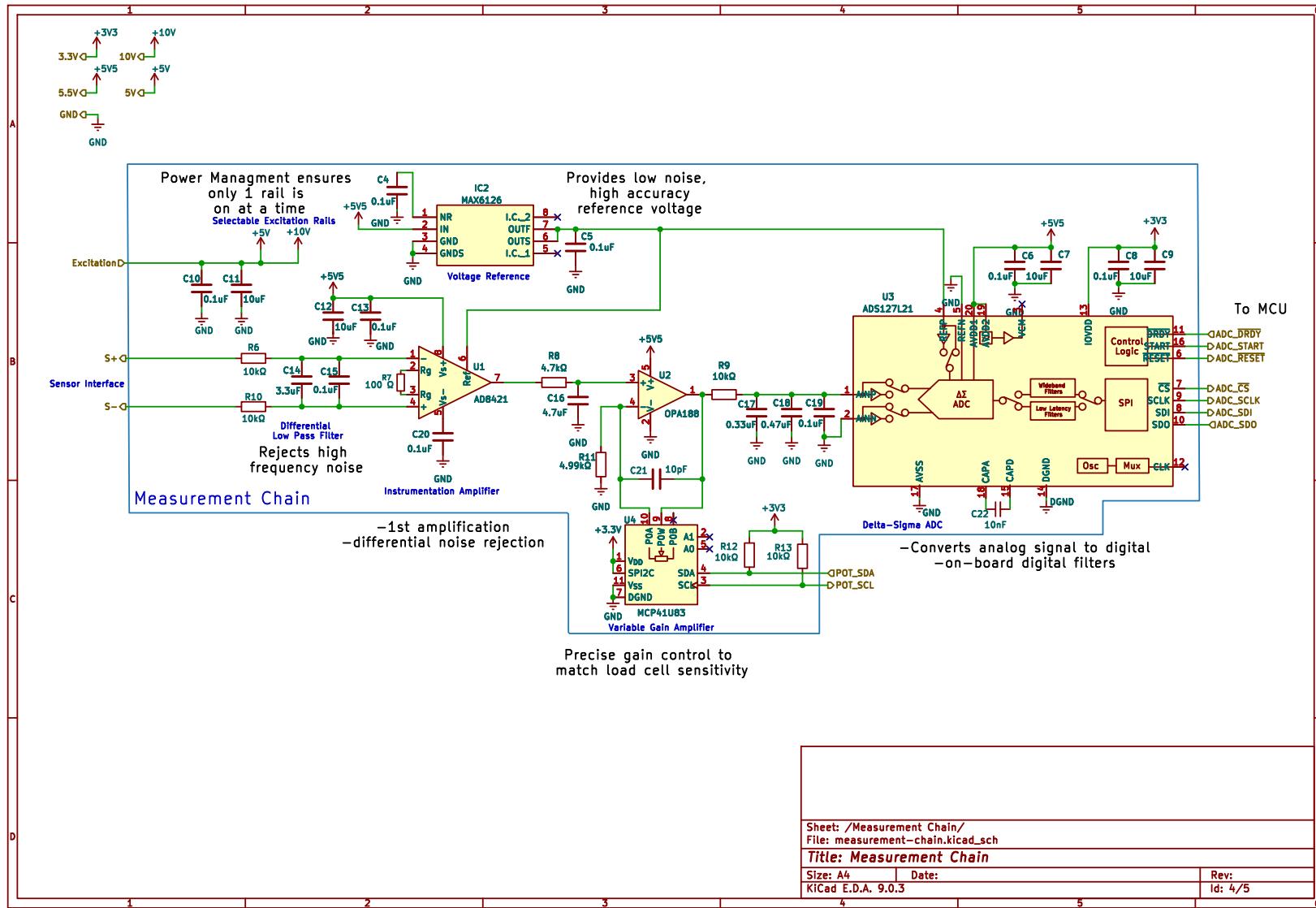


Figure 21: Measurement Chain System Schematic Diagram

10.3.4. Battery Management

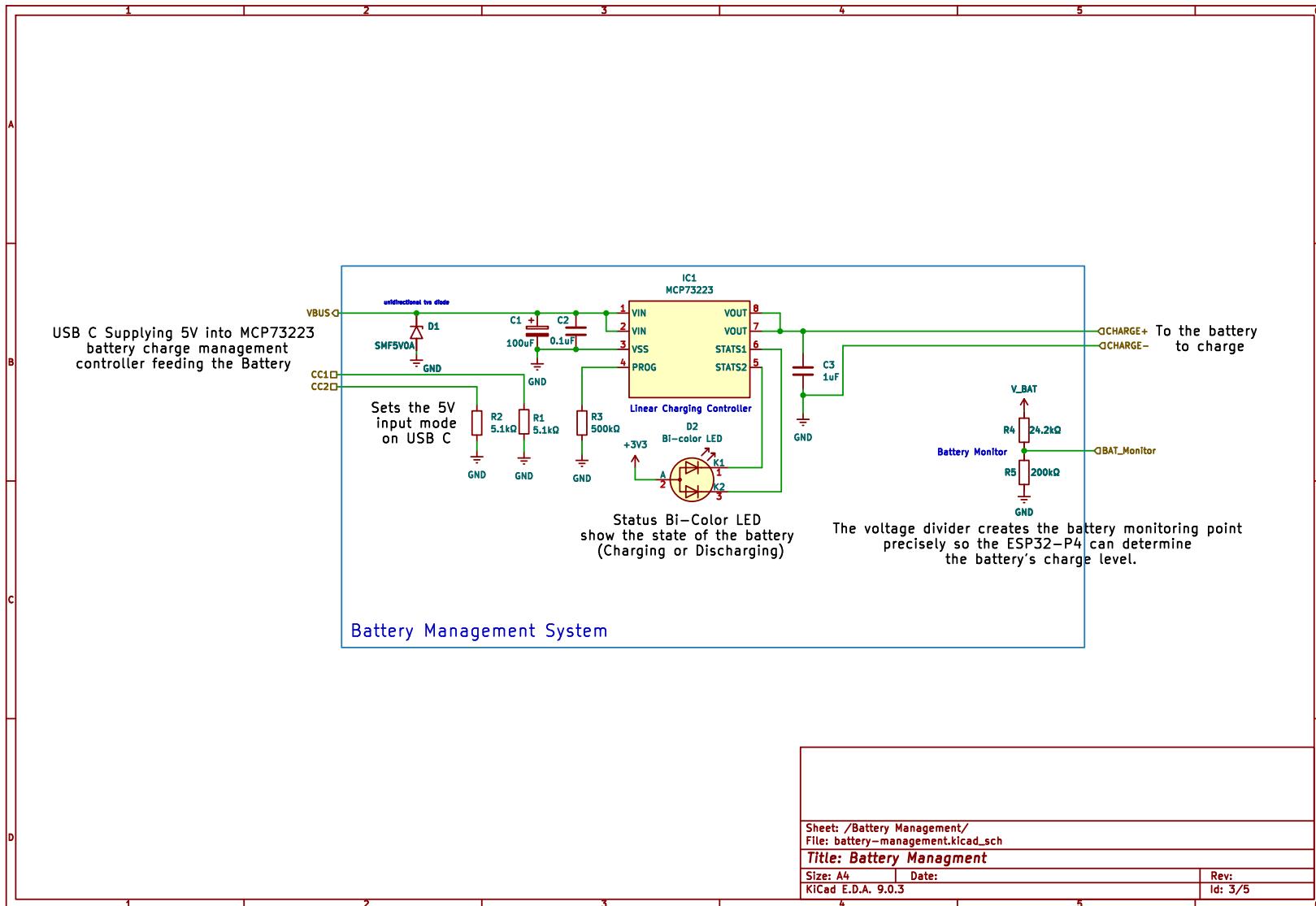


Figure 22: Schematic diagram of battery management

10.4. Load Cell Identification

To make each load cell uniquely identifiable, a simple voltage divider is to be implemented into the connector cables of each load cell as shown in Figure 23. The assembly of this system is shown in Table row 13.

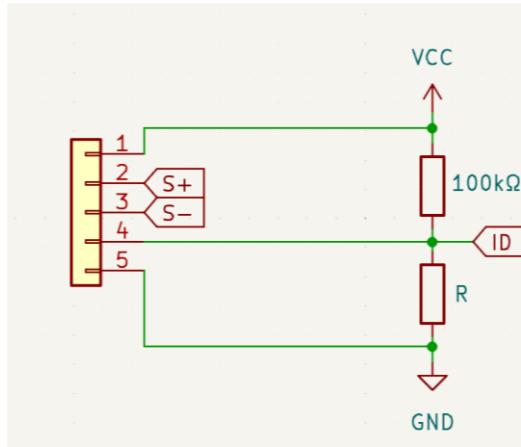


Figure 23: Schematic Diagram of Voltage Divider inside M12 Load Cell Connector

The upper resistor is chosen to be $100\text{k}\Omega$ while the lower resistor is changed for each load cell as shown in Table 17. The resultant voltage is calibrated and stored in the MCU memory for fast identification of the load cell. Once identified, it the MCU adjusts the settings of the VGA from 9.3.4.

Table 17: Resistor Values for Each Load Cell for Identification

Load Cell Model [kgf]	Resistor Value (R) [kΩ]
0.15	10
2	2
20	20
45	45
250	200
3000	300

These resistor values were chosen so that there is sufficient distance between load cells to make them easily identifiable and with sufficient room for future load cell models to be integrated for compatibility.

10.5. Battery Life Estimate

To update the battery life estimate in 19.2 Appendix B, the typical supply current values from the components listed in Table 20 we used to calculate a new estimate.

Table 18: Typical and Specified Supply Current Values for Electronic Components

Component	I_{typ} [mA]	I_{max} [mA]	I_{spec} [mA]
Load Cell	14.28	28.57	21.425 ¹⁰
INA	2	2.3	3
OPAMP	0.45	0.51	1
Digi Poti	0.001	0.002	0.005
DS ADC	1.24	1.43	3
VREF	0.38	0.58	1
MCU	500	600	500
10 V Excitation Regulator	2.3	2.8	2.5
5V Excitation Regulator	0.001	0.0027	0.002
5.5 V ADC Channel	0.101	0.183	0.15
3.3V Regulator	0.017	0.03	0.02
Optocoupler	10	10	10
Display Back light	120	120	120
USB	2.5	500	2.9 ¹¹
Total			655.002

The typical and maximum values were considered in choosing the specified current value and this value was used to calculate the battery life using Equation (8)

$$T_{dur} = \frac{\text{Capacity}}{I_{spec}^{total} \cdot 1.2}$$

(8) Where Capacity is the full capacity of the battery, T_{dur} is the duration in hours, I_{spec}^{total} is the sum of the specified currents and 1.2 is the safety factor.

When using the original 5000mAh battery, the estimate battery life is only 6.26 hours. The main proponent to this is the ESP32-P4 which draws an immense 500mA. So either another controller matching the requirements in Table 25 must be found, or the battery can be upgraded to 7000mAh which yields a specified battery life of 8.77 hours which matches the requirements outlined in 3.1.4 Electrical Requirements.

¹⁰ An average of the two load cell currents

¹¹ See 19.1 for estimate considering data transfer rate as well

10.6. Noise Performance

10.6.1. Noise Components

The main contributors to the noise in the system are:

- Load cell noise caused by vibrations, hysteresis, creep and temperature fluctuations
- Electromagnetic Interference (EMI) or 50/60 Hz “Hum Noise” caused by nearby electrical equipment
- Power noise caused by fluctuations in the power supply
- Device noise caused by internal non-ideal processes of the ICs (including flicker noise)
- Quantisation noise from the ADC

The stages of the Technical Drawing of Main Assembly

Measurement Chain have been designed to minimise and reject these noise components, however these processes are non-ideal and thus there will always be some noise in the system which limits the precision and accuracy of the measurements.

10.6.2. Peak-to-Peak Noise

To estimate the noise of the system, we cannot approximate the load cell noise or the EMI noise as they are heavily dependent on the environment. So, they are assumed to be Sufficiently attenuated by the filters and estimate the peak-to-peak noise accounting for the other noise components. This estimate will also be done using the potential candidate components listed in Table 16.

The excitation conditioning outlined in 9.3.1 results in a 0.1mV voltage ripple with a frequency of approximately 1MHz that propagates into both signal lines. However, the differential RC filter at the inputs of the INA help to attenuate it.

Firstly, considering the bandwidth of 4.97Hz, the frequency gap can be found through Equation (9) to be around 5.3 dec.

$$f_{\text{GAP}} = \frac{f_{\text{noise}}}{B} = \frac{1\text{MHz}}{4.97\text{Hz}} = 201207 \approx 5.3 \text{ dec} \quad (9)$$

Since passive RC filters have a roll-off of -20dB/dec, we get an attenuation of approximately 106dB as shown in Equation (10).

$$A = -20 \frac{dB}{dec} \cdot 5.3 \text{ dec} \approx -106dB \quad (10)$$

Thus, the attenuated peak-to-peak voltage noise from the power supply ripple is 501.187pV as shown in Equation (11).

$$100\mu\text{V} \cdot 10^{-\frac{106}{20}} = 501.187\text{pV} \quad (11)$$

The AD8421 INA also has an intrinsic peak-to-peak noise at its input of 0.07μV when the gain is 100. Thus, the total noise at the output of the INA after amplification is approximately 7.050μV as shown in Equation (12).

$$(0.000501187\mu\text{V} + 0.07\mu\text{V}) \cdot 100 \approx 7.050 \mu\text{V} \quad (12)$$

The OPA188 as a typical intrinsic input noise of 0.25 μV. Hence, considering the noise from the INA and the maximum gain of 4.26 from Table 14, the peak-to-peak voltage noise at the output would be 31.098 μV as shown in Equation (13).

$$(7.050\mu\text{V} + 0.25\mu\text{V}) \cdot 4.26 \approx 31.098 \mu\text{V} \quad (13)$$

The ADS127L21 has a typical input RMS voltage noise of around 0.969 μV¹². To convert the RMS noise into the peak-to-peak noise, we can use the statistical factor of 6.6 to approximate it as shown in Equation (14) (Analog Devices, 2012)

$$0.969\mu\text{V} \cdot 6.6 = 6.395\mu\text{V} \quad (14)$$

¹² This is when using the FIR filter with an OSR of 2048 and low speed data transfer

The MAX6126 has a noise of $2.85 \mu V$ when the output voltage is set to $5V$. This can be considered as noise at the input of the ADC.

Hence, the total noise at the input of the ADC $40.344 \mu V$ peak-to-peak as shown in Equation (15).

$$31.098\mu V + 6.395\mu V + 2.85\mu V = 40.344\mu V \quad (15)$$

10.6.3. Noise Free Resolution

With a peak-to-peak voltage noise of $40.344 \mu V$, there are 123,934 noise free counts according to Equation (16).

$$\frac{U_{\text{full scale}}}{U_{\text{noise}}} = \frac{5V}{40.344\mu V} \approx 123934 \quad (16)$$

Thus, the noise-free resolution is around 17 bits according to Equation (17).

$$\log_2(123934) = 16.92\text{bits} \approx 17\text{bits} \quad (17)$$

This essentially means that the ADC can accurately measure with 17-bit precision instead of the theoretical 24 bits. Table 19 shows the resulting measurement resolutions for each load cell.

Table 19: Noise Free Measurement Resolution of the Each Load Cell

Load Cell [kgf]	Measurement Resolution [gf]
0.15	0.0012
2	0.016
20	0.16
45	0.36
250	2.02
3000	24.21

According to The International Organization of Legal Metrology (2000, November), having over 100,000 measurable intervals classifies the load cell with accuracy class A. Additionally, it should be noted that complete analogue front-end chips such as the HX711 and the AD7794 have much lower noise-free resolutions of 14 ad 16 bit respectively.

10.7. Component Specifications

Table 20: List of Electronic Components in the Electronic System

Reference	Qty.	Value / Model Number	Description
BT1	1	XT90PW	Battery connector designed for secure connection

C1, C23	2	100µF	Electrolytic capacitors to block voltage spikes
C2, C4, C5, C6, C8, C10, C13, C15, C19, C20, C27, C33, C40	13	0.1µF	X7R ceramic capacitors for decoupling ICs
C3	1	1µF	X7R ceramic capacitors to smoothen output of charging circuit MCP73223
C7, C9, C11, C12, C24, C25, C26, C28, C34, C35, C37, C41	12	10µF	X7R ceramic capacitors for decoupling ICs
C14	1	3.3µF	X7R ceramic capacitor for low pass filtering
C16	1	4.7µF	X7R ceramic capacitor for low pass filtering
C17	1	0.33µF	X7R ceramic capacitor for low pass filtering
C18	1	0.47µF	X7R ceramic capacitor for low pass filtering
C21	1	10pF	multilayered ceramic capacitor for counteracting parasitic elements of digital potentiometer
C22	1	10nF	X7R ceramic bypass capacitor of ADS127L21 ADC
C29	1	3.3nF	X7R ceramic capacitor to set the internal voltage reference rise time of TPS62130 buck convert
C30, C31, C32, C36, C39	5	22µF	X7R ceramic capacitor for smoothing output of TPS61089 boost convert and acting as loop compensation
C38	1	2.2µF	X7R ceramic capacitor for decoupling TPS61089 boost converter
D1	1	SMF5V0A	TVS Diode for overvoltage and discharge protection of the MCP73223 charging circuit
D2	1	Bi-colour LED	Bi-colour LED to indicate charging status of battery
D3, D4	2	Schottky	Diodes required by the TPS61170 and TPS61089 boost converters to direct the high voltage pulse during the release phase of the converter each cycle

IC1	1	MCP73223	Linear charge management controller used to safely charge the Li-Po battery of the device
IC2	1	MAX6126	Ultra-High-Precision, Ultra-Low-Noise, Voltage reference IC to ensure the ADS127L21 ADC has an accurate 5V reference for conversion
J1	1	M12 5-pin	IP67 connector for the load cells
J2	1	USB A	IP67 USB 2.0 port for output of measurement data
J3	1	USB C	IP67 USB C port for charging the battery of the device
L1, L4	2	4.7 μ H	Inductors used by the switching voltage regulators for storage and release of energy
L2	1	2.2 μ H	Inductor used by the switching voltage regulators for storage and release of energy
L3	1	4.7 μ H	Inductor used by the switching voltage regulators for storage and release of energy
Q1	1	AO3401A	P-channel Power MOSFET used to control the main supply line from the battery
Q2, Q5	2	AO3401A	P-channel Power MOSFETs used to control the switch the excitation line between 5V and 10V
Q3, Q4	2	AO3400A	N-channel Power MOSFETs used to drive Q2 and Q5 in switching between 5V and 10V excitation
Q6	1	AO3400A	N-channel Power MOSFET used to drive the back light of the LCD
R1, R2	2	5.1k Ω	Metal oxide resistors to pull-down the Configuration Channel pins of the USB C port for 5V input.
R3	1	500k Ω	Metal oxide resistors to set the charging speed of the MCP73123 charging circuit
R4	1	24.2k Ω	Metal oxide resistor for the voltage divider to monitor the battery charge
R5	1	200k Ω	Metal oxide resistor for the voltage divider to monitor the battery charge

R6, R9, R10	3	10kΩ	Thin film low tolerance resistors for the low pass filters in the measurement chain
R12, R13, R20, R24, R26, R34, R35	7	10kΩ	Metal oxide pull-up resistors to set default state of various pins
R7	1	100 Ω	Thin film low tolerance resistor to set the gain of the AD8421 instrumentation amplifier
R8	1	4.7kΩ	Thin film low tolerance resistor for the low pass filters in the measurement chain
R11	1	4.99kΩ	Thin film low tolerance resistor to set the gain of the AD8421 instrumentation amplifier
R14	1	1.2kΩ	Metal oxide resistor for the voltage divider to monitor power button state
R15	1	10kΩ	Metal oxide resistor for the voltage divider to monitor power button state
R16	1	1kΩ	Metal oxide pull-up resistor to set default state of SW1 power switch
R17	1	100kΩ	Metal oxide resistor to separate the SW1 and Q1 nodes
R18	1	1MΩ	Metal oxide pull-up resistor to set default state of Q1 power MOSFET
R19	1	71.4 kΩ	Metal oxide resistor for the voltage divider to set voltage output for TPS61170 boost converter
R21	1	10 kΩ	Metal oxide resistor for the voltage divider to set voltage output for TPS61170 boost converter
R22	1	100kΩ	Metal oxide pull-up resistor to set default state of PG pin on TPS62130
R23	1	31.25kΩ	Metal oxide resistor for the voltage divider to set voltage output for TPS62130 buck converter
R25	1	10kΩ	Metal oxide resistor for the voltage divider to set voltage output for TPS62130 buck converter

R27	1	301kΩ	Metal oxide resistor for programming the switching frequency of the TPS61089 boost converter
R28	1	40 kΩ	Metal oxide resistor for the voltage divider to set voltage output for TPS61099 boost converter
R29	1	4.87 kΩ	Metal oxide resistor for the voltage divider to set voltage output for TPS61089 boost converter
R30	1	10kΩ	Metal oxide resistor for the voltage divider to set voltage output for TPS61099 boost converter
R31	1	10kΩ	Metal oxide resistor for the voltage divider to set voltage output for TPS61089 boost converter
R32	1	17.4kΩ	Metal oxide resistor for loop compensation of the TPS61089 boost converter
R33	1	127kΩ	Metal oxide resistor for programming the switching peak current of the TPS61089 boost converter
R36	1	20kΩ	Metal oxide resistor to create short delay on the enabling pin of the MCU. This ensures supply lines are energised before start up
SW1	1	Emergency Stop	IP67 button to interrupt program in case of emergency
SW2	1	ON/OFF	IP67 button to power device on and off
U1	1	AD8421	Low-noise instrumentation amplifier to perform first stage amplification and noise rejection of the load cell signals
U2	1	OPA188	Zero-drift operational amplifier to perform second stage amplification of load cell signals
U3	1	ADS127L21	Delta-sigma ADC to convert analog signal into digital for processing in the microcontroller
U4	1	MCP41U83	1024 position digital potentiometer for adjusting the gain of the OPA188 amplifier

U5	1	PS9117A	Optocoupler to isolate the main power line from controlling MCU pin for latching the supply switching network
U6	1	TPS61170	Low noise boost converter for 10V excitation line
U7	1	TPS62130	Low noise buck converter for 3.3V supply line
U8	1	TPS61099	Low noise boost converter for 5V excitation line
U9	1	TPS61089	Low noise boost converter for 5.5V supply line
U10	1	W25Q128JVS	SPI Flash memory IC to store measurement data
U11	1	ESP32-P4	High performance MCU to control device and perform data processing
U12	1	TouchScreen/SPI Touch Controller	Connection to control the resistive touch screen LCD

10.8. Preliminary PCB Design

A PCB design was drafted as an illustration of the parts for Table 22: List of Make Parts and Manufacturing Technology. This design is not complete and is only for illustration purposes.

11. Programming Flow Chart

12. Make or Buy Decision

12.1. Criteria for Make or Buy Decision

A Make or Buy Decision was made for each component to determine whether it is more viable and economical to have the component custom manufactured or purchased from a vendor as a standard part or a Commercial off-the-shelf (COTS) solution. These decisions are documented in Table 21.

The details about the manufacturing process of the make parts are documented in Table 22. The requirements manuals for the buy parts are documented in Table 25 and Table 26. Some COTS parts may also need some simple modifications after purchasing and are thus classified as Buy & Modify and documented in Table 23.

This process was based on the following factors:

- Product Design Requirements
- Cost Efficiency
- Production Volume
- Design Complexity
- Project Schedule and Risk
- Quality Control
- Availability of standard parts on the market

12.2. List of Make and Buy Parts

Table 21: Make and Buy Decisions for Each Component

Component	Decision	Justification
Electrical		
Microcontroller (MCU)	Buy	Many COTS solutions meet the required specifications and complexity in designing an MCU is very high leading to delays.
Printed Circuit Board (PCB)	Make	To ensure all the design specifications are met, a PCB must be designed and manufactured. It will be based off the designs in 8. Measurement Chain and 10. Circuit Diagram.
Load Cell Connector	Buy & modify	To include the necessary load cell identification channel, the connector will need to be developed in house.
Load Cell Interface Port	Buy	There are many available COTS M12 connector ports which meet the IP67 requirements and can be attached to the PCB.
Noise and Low-pass Filter	Buy	All the components for the filters are available as COTS parts. Given the precision required for these components, developing such ICs in-house would add too much

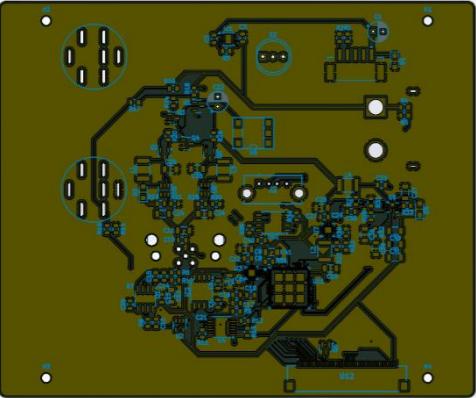
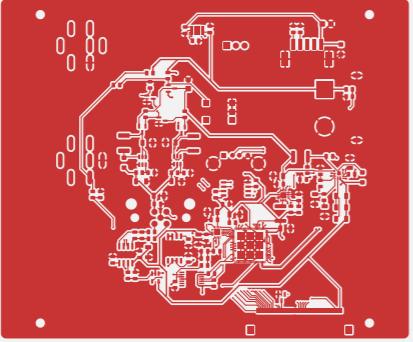
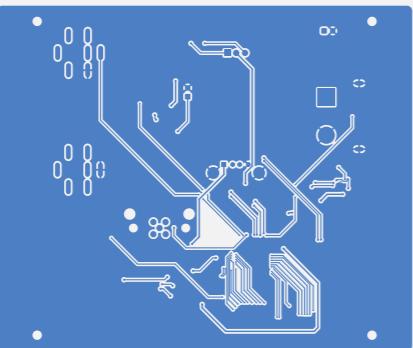
		design complexity and require robust quality control.
Amplifier	Buy	COTS amplifier ICs meet requirements and are incredibly reliable, precise and cost effective. The design complexity and quality control necessary to ensure zero-drift and accurate gain are too high to justify in-house development.
Analog to Digital Converter (ADC)	Buy	It is more cost effective to purchase a COTS delta-sigma than develop one as they are very complex ICs. COTS ICs are also very feature rich including digital filtering and buffers.
Cell Excitation Regulator	Buy	COTS power regulation ICs are precise and low noise. Developing such devices in house would be too complex and time-consuming.
Touchscreen Display	Buy	Many COTS resistive touch screens are sufficiently robust to be used in factory and worksite conditions. Developing a custom display and touch screen layer is highly complex and unnecessary.
Push Button	Buy	Developing a button that meets IP67 requirements while being mechanically robust and durable is too complex and time-consuming. It is much more cost effective to purchase a COTS button.
LED light	Buy	COTS LED lights are incredibly cheap and reliable.
Internal Memory Module	Buy	COTS memory modules both on-board in the MCU and external chips are reliable and fast.
USB-A Port	Buy	USB-A ports are standard parts that are readily and widely available. They are compatible with USB drives that most people already have.
Power Regulator	Buy	COTS regulators which are low-noise and efficient are widely available. Designing such devices in-house would require too much quality control and testing.
USB-C Port	Buy	USB-C ports are standard parts that are readily and widely available. They are compatible with charging cables that most people already have.
Battery Charging Circuit	Buy	Many Li-Po charging circuits exist on the market as COTS ICs. These ICs are reliable, safe and fast.
Battery	Buy	Li-po battery development is highly complex and requires intricate manufacturing processes. While high-capacity batteries are readily available as COTS products.

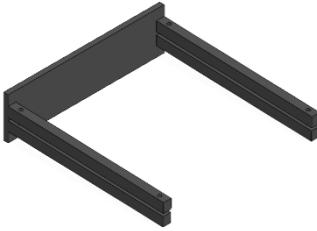
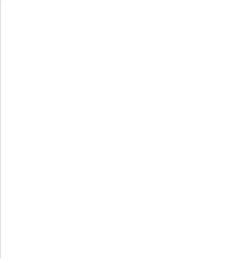
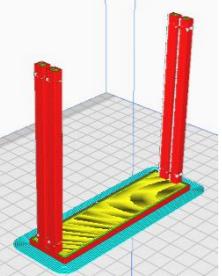
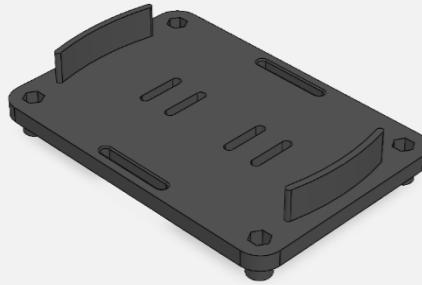
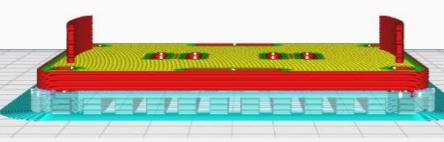
Misc	Buy	Resistors, capacitors, inductors, transistors, connection terminals, wires are all widely available at Sufficient quality as COTS products.
Mechanical		
Protective Carrying Case	Buy & modify	There are several COTS cases with IP67 ratings and shock absorption that can be used to house the product. Developing a custom case require extensive mechanical testing and is not cost effective.
Foam	Buy	The soft foam padding is a crucial for Components holding. It's an available COTS material, providing the benefits of low cost and rapid availability.
1-Panel Frame	Make	To make sure that the design meets its requirements a Panel Frame is holding the HMI interface and sealed by applying precise compression to a highly resilient gasket material.....
Internal Aluminium Frame	Make	Essential because aluminium's high strength-to weight ratio provides a rigid structure to secure all internal components, including the battery and delicate electronics, protecting them from internal movement and external shock.
Misc	Buy	They are selected because the DIN standard ensures that every fastener and bracket is made with precise, repeatable dimensions and strength, guaranteeing consistent assembly quality across all units.
Load cells	Given	The Innovatest line of load cell products are already existing and their design and manufacturing are outside the scope of this project.

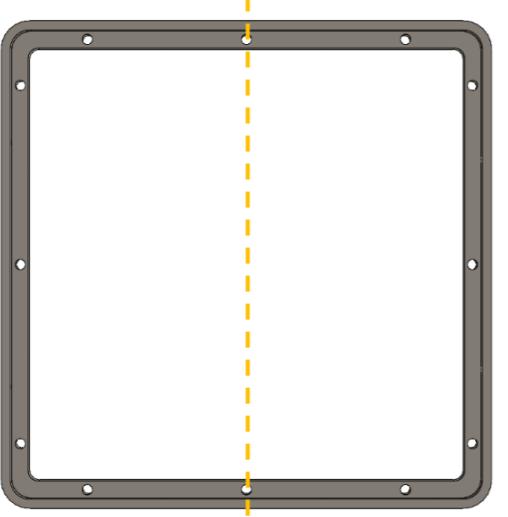
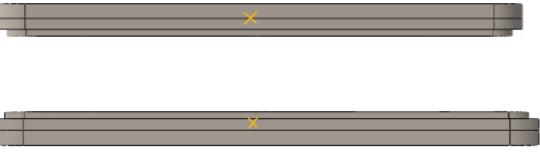
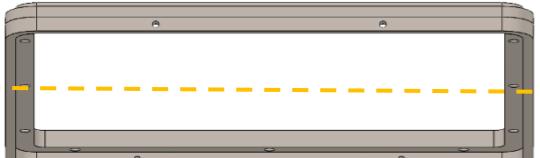
13. Technology Selection for Make Parts

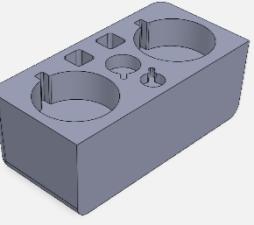
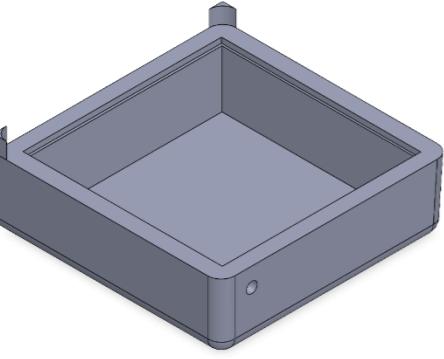
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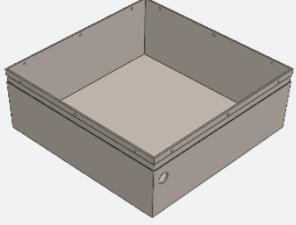
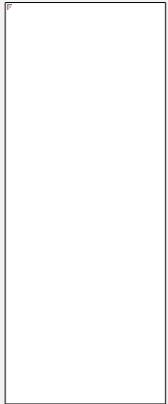
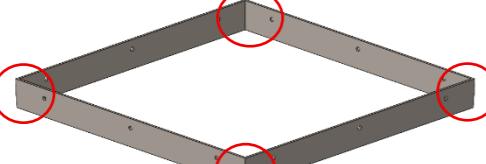
Table 22: List of Make Parts and Manufacturing Technology

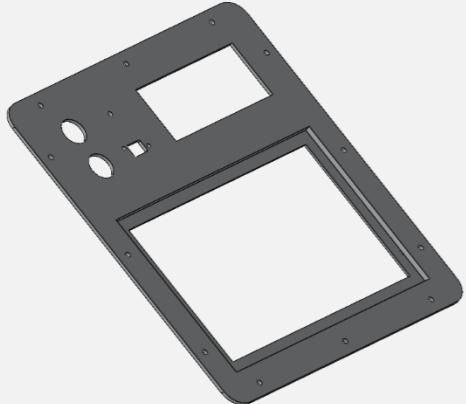
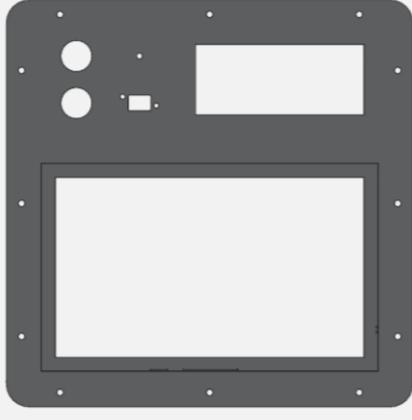
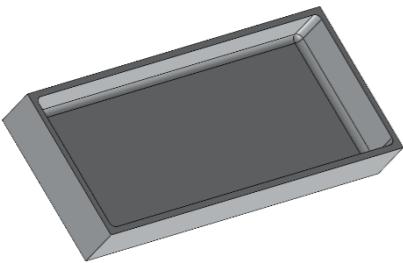
Identification Number	Part	Material Details	Manufacturing Technology	Justification
1	 <i>Figure 24: Printed Circuit Board (PCB)</i>  <i>Figure 25: Routing on Front Side of PCB</i>  <i>Figure 26: Routing on Back Side of PCB</i>	<p><u>Material:</u></p> <ul style="list-style-type: none"> • Fibreglass substrate insulating dielectric • Copper foil for conductive layer • Gold pads for component footprint <p><u>Grade:</u></p> <ul style="list-style-type: none"> • FR-4 fibreglass • Electrodeposited copper for copper foil • Electroplated gold on component pads <p><u>Standard:</u> IPC-2221</p> <p><u>Reason:</u></p> <ul style="list-style-type: none"> • FR-4 has higher strength and durability than epoxy-based boards. It is also more cost effective than high strength Polymimide boards. • Copper has higher electrical and thermal conductivity than aluminium allowing for efficient signal transmission and heat dissipation. It is also less expensive than gold or silver and thus better for the foil which covers large surface area. • Plated gold is better for component connectors since it does not corrode or oxidize. This allows for reliable and long-lasting connections. 	<p><u>Blank Preparation:</u></p> <p>The blank is a FR-4 board with deposited copper foil on both sides as well as an ultraviolet sensitive laminate. The blank is cut to size (100mmx90mm) before processing. The design only has components and tracks on the top and bottom layers of the board.</p> <p><u>Chemical PCB Fabrication:</u></p> <p>The blank is to undergo the following chemical processes according to IPC-2221 in this order:</p> <ol style="list-style-type: none"> 1. Ultraviolet Treatment 2. Chemical Development 3. Acid Etching 4. CNC Drilling for holes 5. Electroless & Electrolytic Copper Deposition 6. Soldermask Application 7. Electroless Nickle Immersion Gold (ENIG) Surface Finish 8. Silkscreen Screen printing <p>The track sizes of the PCB are made to be a thickness $\geq 0.2\text{mm}$ to allow for the etching process to run smoothly while still not being cumbersome in routing connections.</p> <p>All holes (screw holes, vias, plated through-holes) are made $\geq 0.2\text{ mm}$ to ensure sufficient surface area for the copper deposition process.</p>	<p>FR-4 blanks with dual side copper foil and laminate are an industry standard and are available at any PCB manufacturing firm.</p> <p>Chemical fabrication is chosen over traditional milling as it is faster for the given size, and it widely adopted by most PCB manufacturing firms.</p> <p>Soldermask application is required to ensure the PCB to prevent oxidization of the copper tracks and prevent soldering from bridging the gaps between tracks. This is preferred over no solder mask as it will produce PCB that is longer lasting and easier to solder.</p> <p>Using an ENIG surface finish over Hot Air Soldering Levelling (HASL) and Organic Solderability Preservative (OSP) allows for a more planar pads, higher performance and longevity. This justifies its use despite higher costs.</p> <p>A silkscreen with component designators should be printed on so that each component can be placed in the correct footprint during assembly.</p>

2	 <p><i>Figure 27: PCB Mount – hold the PCB in place</i></p>  <p><i>Figure 28: PCB Mount top view</i></p>  <p><i>Figure 29: PCB Mount 3D printer view with supports and bridging</i></p>	<p>Material: Polycarbonate Grade: General Purpose Polycarbonate ISO: 21305-1:2019</p> <p>Reason: Higher glass transition temperature than ABS, more impact resistant than ABS, higher heat resistance, non-conductive unlike steel, lighter weight than metal counterparts. These properties are vital as this will support the PCB/Motherboard.</p>	<p>Additive Manufacturing: FDM 3D Printing. For this the part must be oriented as shown in Figure 28, with the flat rectangular parallel to the surface. No supports are required, considering the small size of the part. Because of the use of polycarbonate, The minimum wall thickness in the part is 3 mm (The thickness of the clamp for the PCB), hence a maximum nozzle size of 1.5 mm must be used. An extrusion temperature of 260°C - 310°C is required. As no bridging, no supports are used however the brim is still there to prevent warping.</p>	<p>This technology has been preferred over injection moulding, as considering for the projected 500 units over the 3 years, the speed is not a larger priority than the price which must be borne, which will be much higher for the mould.</p>
3	 <p><i>Figure 30: Battery Cradle – To house the battery</i></p>  <p><i>Figure 31: Battery Cradle with Support for Manufacturing</i></p>	<p>Material: ABS Grade: Heat Resistant ABS ISO: 2580-1 ABS</p> <p>Reason: Does not reach glass transition temperature till 105°C. Has higher thermal shock resistance than aluminium. Much lighter than steel. Easier to print compared to Polycarbonate, or metals.</p>	<p>Additive Manufacturing: FDM 3D Printing. For this the part must be oriented as shown in Figure 31, with the flat rectangular base parallel to the surface. Because of the use of ABS, to prevent warping (corner of a print lift off the build plate) we must enclose the 3D printing chamber, to maintain a consistent temperature. Extruder temperature must be within 220°C and 250°C. The minimum wall thickness in the part is 1.6mm (The thickness of the hollow cylindrical legs), hence a maximum nozzle size of 0.8mm must be used. Due to the long flat base, normal supports are required, which can be seen in Figure 31. The flat area around is a brim to prevent warping. The details regarding screws</p>	<p>This technology has been preferred over injection moulding, as considering for the projected 500 units over the 3 years, the speed is not a larger priority than the price which must be borne, which will be much higher for the mould.</p>

		<p>Material: Aluminium Grade: 5052 ISO: Al-Mg2,5</p> <p>Lighter weight than steel, better corrosion resistance than 6061, more durable than plastic counterparts, more economical than 6061, good strengths to weight ratio.</p> <p>Another motivation for using Aluminium 5052, for this part is because the “waste” cut out of this part is being used in the cable tray, which are being welded to other Aluminium 5052 parts.</p>	<p>CNC Milling:</p> <p>The shape can be manufactured with index 4-axis milling from an aluminium box of minimum dimensions (295mmx295mmx18mm(h)). The milling will start with orientation showed in the top image in Figure 34, with the side with side holes (Figure 35) parallel to axis of rotation (yellow).</p> <p>First a square box of size 250mmx250mm, will be cut out from the centre. After this the features of the parts will be milled. After milling is completed in that orientation, the material will be rotated by 180° around the x-axis to machine the other side as shown in the top image in Figure 34. The part will also be rotated 90° and 270° to machine the holes on the sides.</p>	<p>4-axis has been used over 3-axis milling, as for the 500 units the human labour cost for flipping the part manually will be higher, also because the part must be milled on 4 sides, if manual method is used it will take much longer and is also more likely to lead to errors/misalignment which will not be tolerable for the frame to maintain IP rating.</p> <p>The cutout of the part has been done to reduce material wastage, and this block will be used for manufacturing 5.</p> <p>The 500 units is also to less to justify the mould costs, and hence no moulding method is used.</p>
			<i>Figure 32: Panel frame</i>	
	4		<i>Figure 33: Top view of panel frame</i>	
			<i>Figure 34: Orientations for 4-axis milling</i>	
			<i>Figure 35: Angled side view of side with holes</i>	

5	 <p><i>Figure 36: Load Cell Compartment – to house the load cells</i></p>  <p><i>Figure 37: Orientation for CNC Router (Start with orientation image on left and change to the right image orientation afterwards)</i></p>	<p><u>Material:</u> EVA Foam <u>Grade:</u> Medium Density EVA <u>Shore hardness:</u> 40-60 Shore C</p> <p>Good balance of compressibility with durability, in between soft and hard foams, to remain more durable than soft foams, but more compressible than hard foams to keep the load cells safe. Lightweight. Better shock absorption than plastics.</p>	<p><u>CNC Contour cutting:</u></p> <p>A simple 3-(primary)-axis CNC router cutting machine can be used to accurately make the cutouts for the load cells as well as the fillet corners on one side of the part from an initial foam box of dimensions minimum (95mm(w)x110mm(h)x293mm(l)) by placing it in the orientation shown in Figure 37 on the left.</p> <p>For the fillets at the bottom and the draft angle the part must rotated 180° along its x-axis and placed as shown in Figure 37 on the right.</p>	<p>The 500 units are not enough to justify the use die cutting, which will fall to expensive. 3-axis milling with manual intervention will fall more economical.</p>
6	 <p><i>Figure 38: Aluminium Box Foam - To keep it stable inside the case</i></p>  <p><i>Figure 39: Aluminium Box Foam Front view</i></p>  <p><i>Figure 40: Aluminium box Side view</i></p>	<p><u>Material:</u> EVA Foam <u>Grade:</u> Medium Density EVA <u>Shore hardness:</u> 40-60 Shore C</p> <p>Good balance of compressibility with durability, in between soft and hard foams, to remain more durable than soft foams, but more compressible than hard foams to keep the electronics safe. Lightweight. Better shock absorption than plastics.</p>	<p><u>CNC Contour cutting:</u></p> <p>A simple 3-(primary)-axis CNC router cutting machine can be used to accurately make the cutouts for the load cells as well as the fillet corners on one side of the part from an initial foam box of dimensions minimum (295mm(w)x105mm(h)x295mm(l)) by placing it in the orientation shown in Figure 38.</p> <p>For the fillets at the bottom and the draft angle the part must rotated 180° along its x-axis and placed as shown in Figure 39.</p> <p>Finally, the foam should be placed flat with the hole seen in Figure 38 facing upwards, to remove material from the hole.</p>	<p>The 500 units are not enough to justify the use die cutting, which will fall to expensive. 3-axis milling with manual intervention will fall more economical.</p>

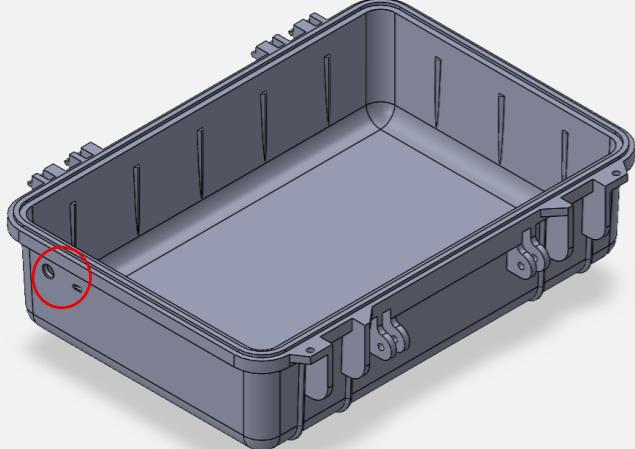
7	 <p><i>Figure 41: Basin - to house all the electronics</i></p>  <p><i>Figure 42: Starting clamping orientation for 4-axis CNC Milling</i></p>	<p><u>Material:</u> Aluminium <u>Grade:</u> 5052 <u>ISO:</u> Al-Mg2,5</p> <p>Lighter weight than steel, good workability for cold forming, better corrosion resistance and weldability than 6061 while remaining more economical, better durability than plastics.</p> <p>The primary motivation behind using all parts with Aluminium 5052 is to have better welding between all parts.</p>	<p><u>Cold forming followed by CNC:</u></p> <p>Backward cold forming extrusion will be used to create the open box like shape from billet of volume above the part volume of 276151.54 mm^3. This may lead to minor fillets on the internal edges, which are tolerable.</p> <p>4-axis index CNC milling will then be used for material removal near for the groove near the top, this with the screw through holes will be done per outside face by placing it as shown in Figure 42 and then rotating it 90 degrees to do the next, till all 4 sides are machined. For each side the right side of basin must also be finished for better accuracy for better assembly.</p> <p>The fillets on the lower external edges, if any can also be tolerated as component will be placed inside foam.</p>	<p>Backward cold forming has been chosen over only CNC milling, to minimize material wastage. 4-axis index CNC milling is required for the sharp groove depth and holes. The 2mm wall thickness will hard/impossible with sand casting, and 500 units is to less to justify initial costs of die casting. 4-axis is necessary over 3-axis, as the part must be machined on 4-sides. 5-axis is not necessary for the part, hence has been avoided to save costs. The tolerance of lower external edges has been made to save on cost for milling operation, as are not critical to the functionality of the product.</p>
8	 <p><i>Figure 43: Aluminium Frame</i></p>  <p><i>Figure 44: Side view for manual cutting</i></p>	<p><u>Material:</u> Aluminium <u>Grade:</u> 5052 <u>ISO:</u> Al-Mg2,5</p> <p>Better weldability and formability than 6061, more durable than plastic, lighter than steel.</p> <p>The primary motivation behind using all parts with Aluminium 5052 is to have better welding between all parts.</p>	<p><u>Laser cutting, Welding:</u></p> <p>2mm thick sheet of aluminium 5052, will be laser cut into 4 identical parts as shown in Figure 44. The draft angle of 2 degree must be made. The laser will also make the holes for screws.</p> <p>The 4 parts will then be welded using tig welding at the corners to make the frame as seen in Figure 43. The areas to weld have been circled in red. Welding will be on the exterior.</p> <p>The welds will then be with ER5356, and after welding they will have manual finishing (grinding, sanding, etc) for a better surface finish.</p>	<p>CNC has been avoided, as too much material wastage, and the costs with laser cutting method will be much cheaper than CNC or even water jet cutting. 500 units is not enough to justify costs for a mould. TIG Welding is superior for thin sheets. Manual finishing is more economical.</p>

9	 <p><i>Figure 45: Panel</i></p>  <p><i>Figure 46: Front view of Panel</i></p>  <p><i>Figure 47: Top View (Above) and Bottom view (Below)</i></p>	<p><u>Material:</u> Aluminium <u>Grade:</u> 5052 <u>ISO:</u> Al-Mg2,5</p> <p>More corrosion resistant than and economical than 6061, better machinability than 3003. More durable than ABS, lighter weight than steel.</p> <p>The primary motivation behind using all parts with Aluminium 5052 is to have better welding between all parts.</p>	<p><u>CNC Milling:</u></p> <p>3-axis CNC milling will be used on some aluminium sheet of minimum dimensions 290mm(l)x290mm(w)x7mm(h). This will be first milled clamped in the orientation in Figure 47 (image on top). After completion of this face, it will be rotated 180 degrees along its longitudinal axis and milled clamped in orientation shown in same figure on the bottom.</p>	<p>CNC Milling was preferred over casting, as 500 units are not enough to justify cost of a die, and laser cutting has been avoided due to the presence of 3D cuts. CNC Milling will also give us high quality, for the part which is going to be exposed to the user.</p>
10	 <p><i>Figure 48: Cable tray</i></p>  <p><i>Figure 49: Cable tray side view</i></p>	<p><u>Material:</u> Aluminium <u>Grade:</u> 5052 <u>ISO:</u> Al-Mg2,5</p> <p>Better weldability than 6061, more economical than 6061, better machinability than 3003, more durable than plastic, lighter than steel.</p> <p>The primary motivation behind using all parts with Aluminium 5052 is to have better weldability between all parts.</p>	<p><u>CNC Milling:</u></p> <p>The block used here will be the block removed in 4. Out of that one block, 8 cable trays can be made by cutting that into half through, and each half into 4 equal length blocks. This will give us an aluminium block of 125mm(l)x62.5mm(w)x18mm(depth minimum) which is larger than this part (120mm(l)x50mm(w)x15mm(d)).</p> <p>3-axis CNC milling will be used for this part, keeping the part vertically flat as shown in Figure 49 with the hollowing done from the top.</p>	<p>CNC Milling has been chosen, as the existing aluminium block removed from 4 can be shaped easily and precisely.</p>

11		<p><u>Material:</u> EVA Foam <u>Grade:</u> Medium Density EVA <u>Shore hardness:</u> 40-60 Shore C</p> <p>Good balance of compressibility with durability, in between soft and hard foams, to remain more durable than soft foams, but more compressible than hard foams to keep the load cells safe and screen. Lightweight.</p> <p>Better shock absorption than plastics.</p>	<p><u>CNC Contour cutting:</u></p> <p>A simple 3-(primary)-axis CNC router cutting machine can be used to accurately make the cutouts for the load cells as well as the fillet corners on one side of the part from an initial foam box of dimensions minimum. (295mm(w)x40mm(h)x295mm(l)).</p> <p>A blank of convoluted foam should be used.</p>	<p>The 500 units are not enough to justify the use die cutting, which will fall to expensive. 3-axis milling with manual intervention will fall more economical.</p> <p>Using convoluted foam allows for pressure distribution on the sensitive load cells and HMI components inside of the case.</p>
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13.2. Modifications to Buy Parts

Table 23: Modifications to Buy Parts

Identification No.	Part	Modification technology	Justification
12	 <i>Figure 51: Lower Pelican Case modifications</i>  <i>Figure 52: Side view of modifications</i>	<p>First mark both the ports precisely. M12 Pin connector - Drilling and reaming:</p> <p>The hole will be drilled using a drill bit of maximum diameter of 11.75 mm. (Closer to 11.75 mm will save costs, but standard bit available can be used). This will be followed by reaming with reamer of 12mm diameter.</p> <p>Slower drilling and reaming speeds should be used to avoid melting of Polypropylene.</p> <p>USB-C Port – Drilling and filing Drill small holes in the corners of the USB-C port. Use hand nibbler tool to remove the excessive material between the holes. Needle files will be used to get the shape precisely, by needling and testing the part fit to see if dimension is correct.</p>	<p>Drilling followed by reaming, allows us to have very precise holes for maintaining the IP ratings sound. Laser cutting has been avoided, as polypropylene (the material of the case) tends to melt and fuse during laser cutting, causes residues to overheat and smoke. Filing is required after material removal to maintain the IP rating sound. Filing allows us with more control while also remaining economical.</p>

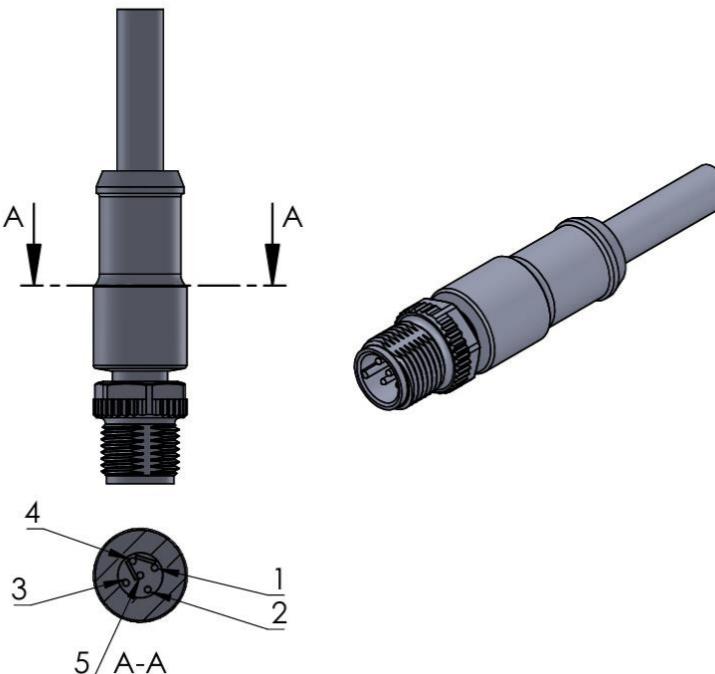
<p>13</p> 	<p>Soldering: The SMD resistors will be soldered between the pins. One between 1 and 4, then another between 4-5. To get access to the pins the M12 connector will be opened.</p>	<p>Provides a strong mechanical and reliable electrical connection.</p>
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Figure 53: Drawing shown modification of M12

13.3. Assembling Individual Parts

Table 24: Assembly of Individual Parts

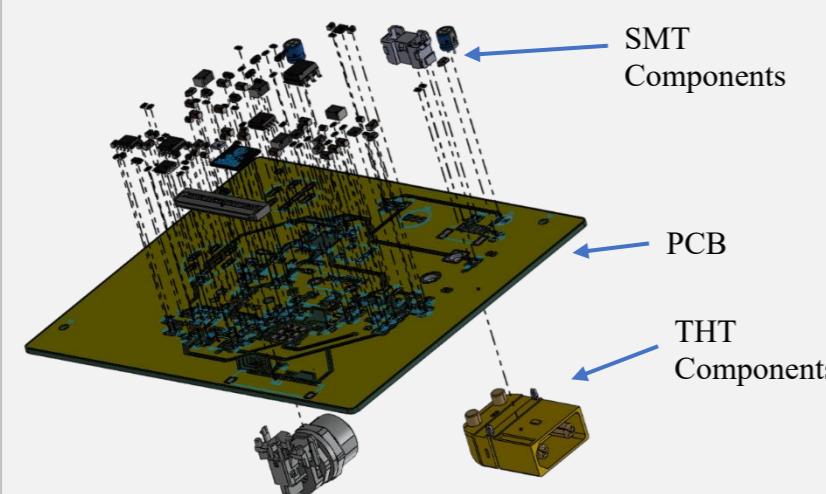
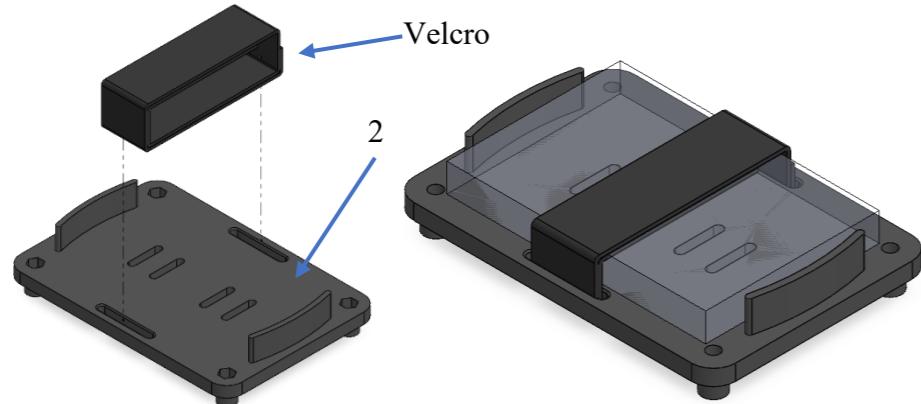
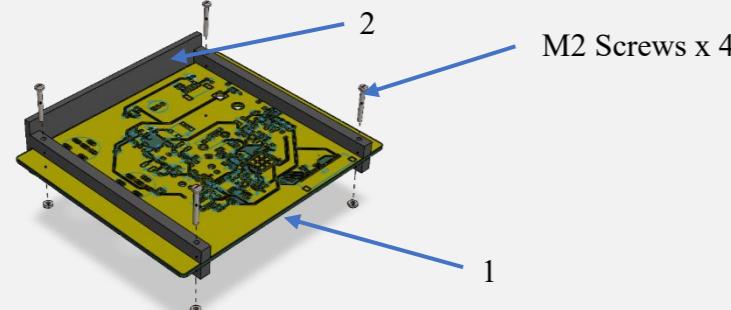
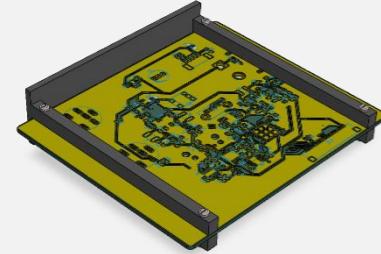
Identification Number	Image	Parts	Assembling Procedure
A1	<p>PCB Assembly</p> 	<ul style="list-style-type: none"> • PCB (1) • Electronic Components (See Table 20) 	<p>Steps:</p> <ol style="list-style-type: none"> 1. Place the PCB (1) into a secured frame. 2. Using a stencil from the PCB manufacturing firm, spread solder paste across all of the pads on the PCB. (Using Sn96.5Ag3Cu0.5 solder paste) 3. Place the SMT electronic components on the top plane of the carefully using the designators and the silkscreen as a guide. 4. Place the PCB and its components into a reflow oven. 5. Heating phase 1: preheating up to 150°C at around 3°C/s 6. Heating phase 2: holding 150°C for around 100 seconds 7. Heating phase 3: heating to above the liquidus line at 217°C for around 60 seconds 8. Heating phase 4: cooling at around 3°C/s 9. Remove the PCB from the oven. 10. Hand solder the through-hole components (J3, BT1, C1 and C23 from Table 20)

Figure 54: PCB and Components Exploded View

A2	<p>Battery Cradle Assembly</p>  <p>Figure 55: Battery Cradle Assembly Exploded View (left), assembled with Battery Ghost View(right)</p>	<ul style="list-style-type: none"> • Battery Cradle (3) • Velcrow 	<p><u>Steps:</u></p> <ol style="list-style-type: none"> 1. Insert the Velcro underneath the cradle through the longitudinal holes (parallel to long side of battery) 2. Wrap the Velcro around the cradle through the holes for it shown in Figure 55 on the left. <p>Battery will be placed afterwards as shown in Figure 55 on the right, with battery in ghost view to visualize. The battery will be stuck to the base with minimal glue.</p> <p><u>Reasons:</u></p> <p>The idea behind combination of glue and Velcro comes to prevent the battery from experiencing too much mechanical stress and while also so that it does not wobble causing stress from side panels if collided with the walls and noise.</p> <p>The motivation behind the minimal glue is also so that replacement is easy in case of degradation.</p>
A3	<p>PCB Mount Assembly</p>  <p>Figure 56: Screwing PCB in PCB Mount</p>  <p>Figure 57: PCB Mount Assembly - Completed</p>	<ul style="list-style-type: none"> • Assembled PCB (A1) • PCB Mount (2) • 4 x ISO 1580 M2 x 16 – 16 N Screws • 4 x ISO 4035 M2 – N Nuts 	<p><u>Steps:</u></p> <ol style="list-style-type: none"> 1. Slide PCB into the frame, with the components side facing upwards. 2. Screw the PCB through the 4 holes into the mount <p><u>Reasons:</u></p> <p>Easy replace if PCB faces issue, 4 x screw restrict movements of PCB within frame, else could lead to wear of the components faster. The open frame keeps ventilation, hence helping keep the components cooler.</p>
A4	<p>Top panel and Tray Assembly</p>	<ul style="list-style-type: none"> • Top panel (9) • Cable tray (10) 	<p><u>Steps:</u></p> <ol style="list-style-type: none"> 1. Clean all surfaces to be welded thoroughly before beginning. In case of heavy contaminants use sanding paper. Else use only acetone. 2. 9 will be placed upside down as shown in Figure 58 (left) 3. 10 shall be placed within its designated area upside down as shown in Figure 58 (left). 4. TIG welding will be used to filet weld (radius 2mm) the 2 parts together 5. Manual grinding method, abrasive grinding to remove excess material. <p><u>Reasons:</u></p>

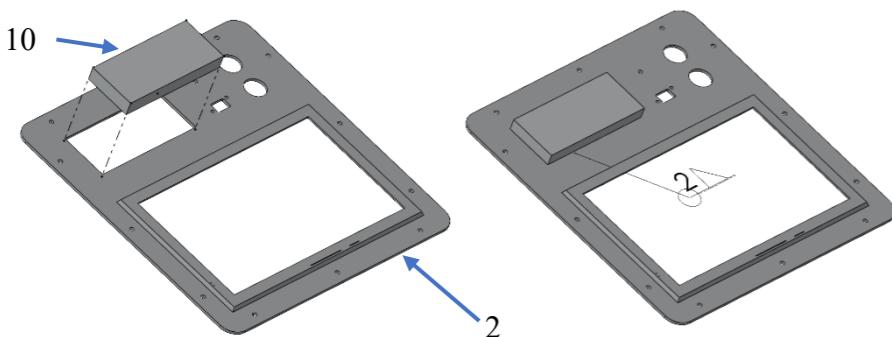


Figure 58: Welding assembly (Left), Welded Assembly (Right)

TIG Welding is used instead of MIG, as it is better for thinner parts, reduces risk of porosity which is essential to keep the IP rating sound.

Top Panel Assembly

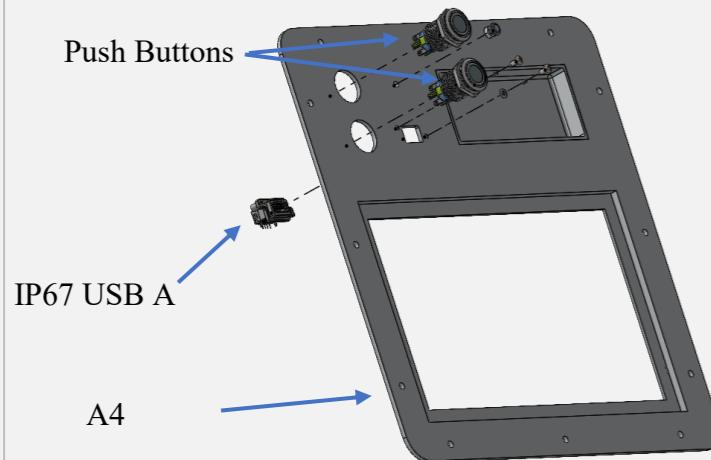


Figure 59: Insertion of Buttons, LED and USB-A Port

- Top panel and Tray Assembly (A4)
- 2 x Buttons Threaded (with bolt)
- USB-A port
- 2 x M3x6 Screws
- 2 x ISO 7092 Washer
- LED threaded (with bolt)

Steps:

1. 2 x buttons, the LED and the USB A port will be screwed onto the board as seen in Figure 59.

Final assembly top and bottom view are visible in Figure 60 for a better understanding.

A5

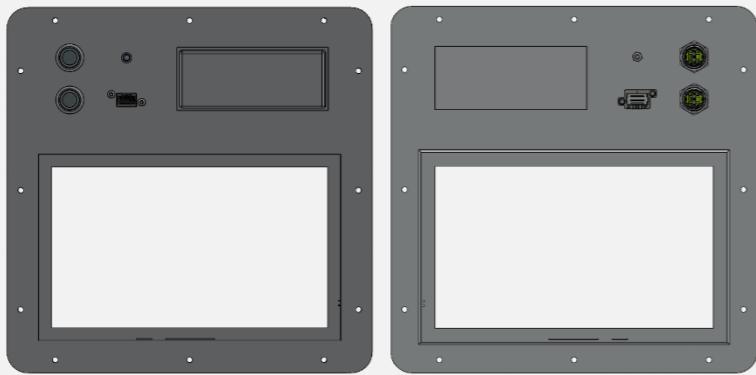
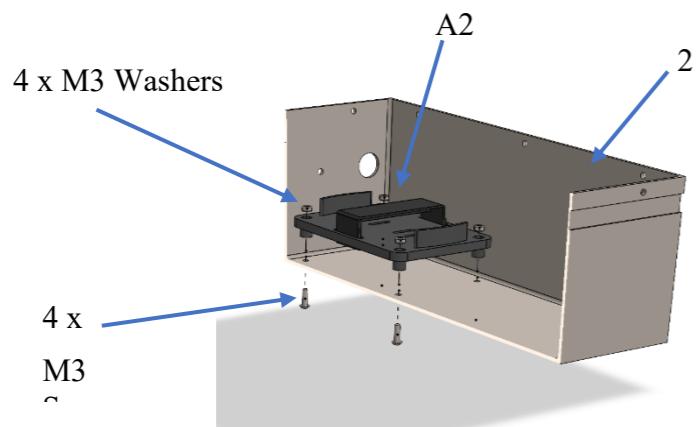
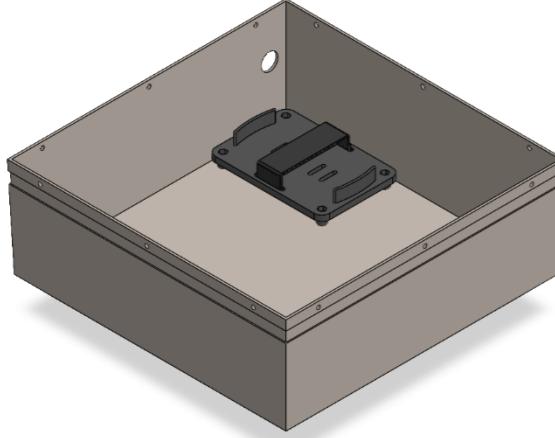
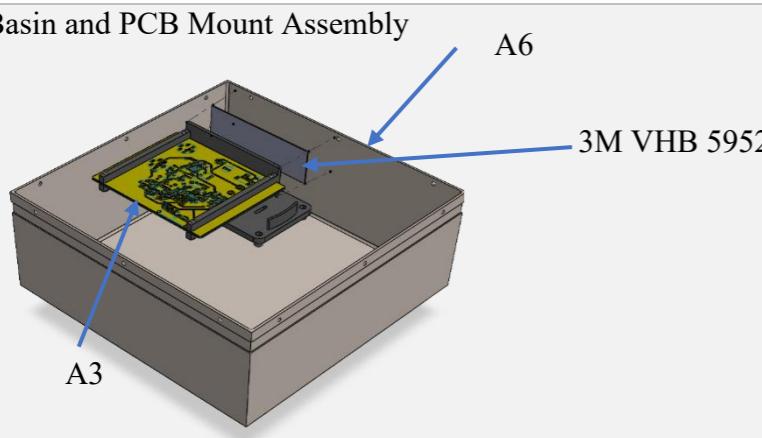
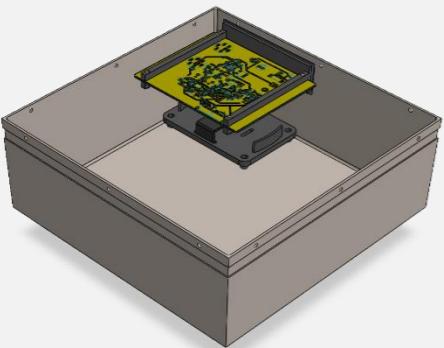
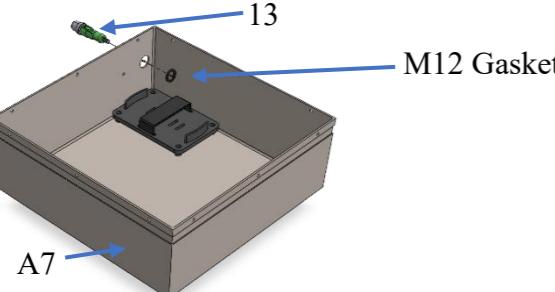
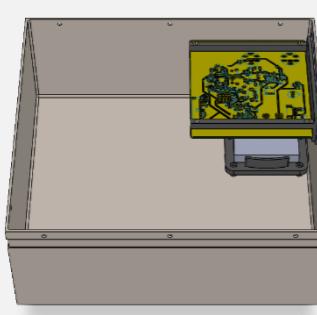
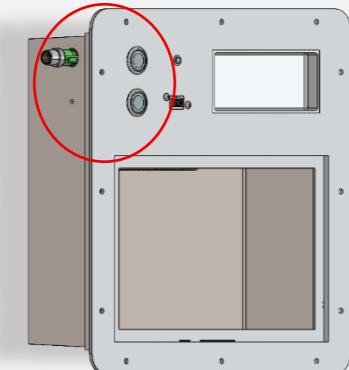
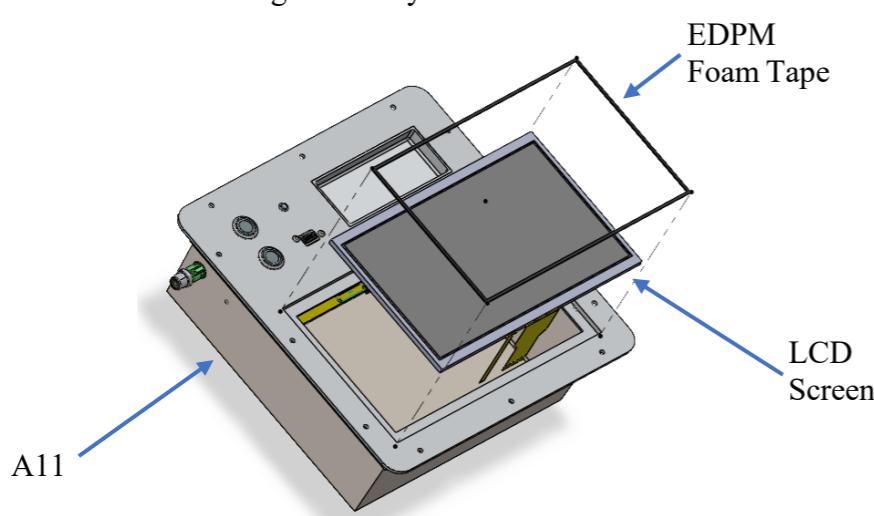
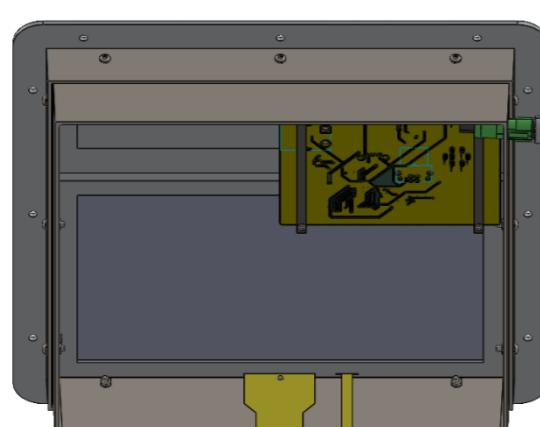


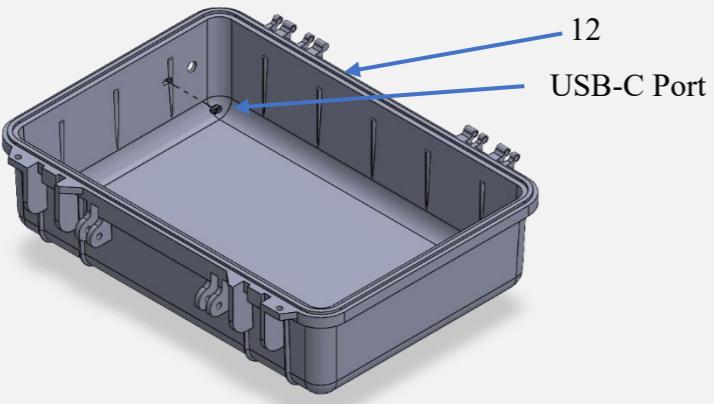
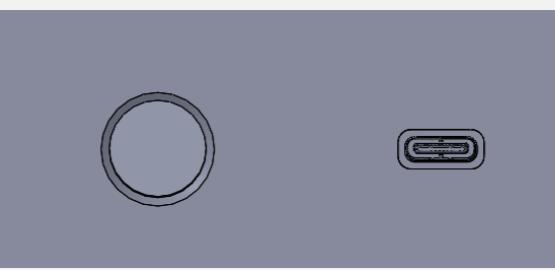
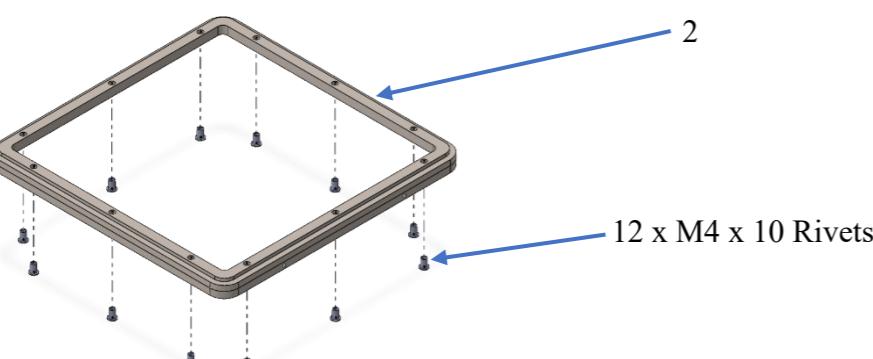
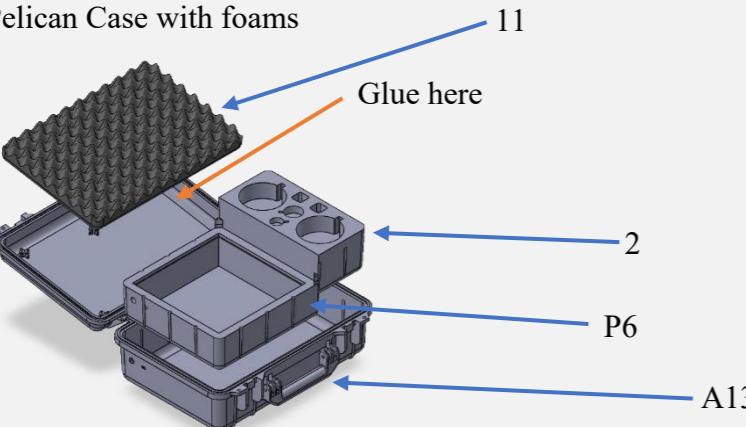
Figure 60: Completed Top Panel Assembly top view (left) and bottom view (right)

<p>A6</p> <p>Basin and Battery Cradle Assembly</p>  <p>Figure 61: Section Isometric View for Battery Cradle Assembly (Cradle made translucent for visibility)</p>	<ul style="list-style-type: none"> • Basin (7) • Battery Cradle Assembly (A2) • 4 x ISO 7380 – M3 x 10 – 10N • 4 x ISO 4032 – M3 – W - N <p>Steps:</p> <ol style="list-style-type: none"> 1. Place A2 on to the basin, 2. Put the M3 – W – N Nuts from the top into the respective holes and screw from underneath as shown in Figure 61. <p>Reasons: For battery no movement is tolerable hence screws are used.</p>
<p>A7</p> <p>Basin and PCB Mount Assembly</p>  <p>Figure 62: Battery cradle assembled</p>	 <p>Figure 63: PCB Mount Assembly, Isometric</p> <ul style="list-style-type: none"> • PCB Mount (A3) • Basin and battery cradle assembly (A6) • 3M VHB 5952 <p>Steps:</p> <ol style="list-style-type: none"> 1. Place the 3M VHB 5952 on the basin side panel as shown in Figure after cleaning it with acetone 2. Place A3 on the 3M VHB 5952, press firmly and hold for a few seconds for the adhesive to properly stick as shown in Figure. Again, the contact surface PCB assembly must also be cleaned before placing. <p>Reasons: As the PCB is very light weight, tape can be used instead of screws to save on weight.</p>

	 <p>Figure 64: Full Basin Assembled</p>		
A8	<p>Basin and Port assembly</p>  <p>Figure 65: Assembly of M12 port into the Basin (PCB Mount hidden for clarity)</p> <p>Figure 66: Assembled port - Basin made translucent for better view (PCB Mount hidden for clarity)</p>	<ul style="list-style-type: none"> • Basin and PCB mount Assembly (A7) • Modified M12 Port (13) • M12 Gasket 	<p><u>Steps:</u></p> <p>Place in the Gasket for the M12 port, followed by the M12 port as shown in to get an interference fit.</p> <p><u>Reasons:</u></p> <p>The gasket is required for an interference fit to remain an IP rating.</p>
A9	<p>Basin and Gasket Assembly</p>  <p>Figure 67: Battery into the cradle</p>	<ul style="list-style-type: none"> • Basin and Port Assembly (A8) • Battery • PVC Foam tape (Gasket) 	<p><u>Steps:</u></p> <ol style="list-style-type: none"> 1. A7 will be placed flat with opening facing upwards and the battery will now be placed inside the battery cradle into the A2 (Battery Cradle) with some drops of glue placed onto the cradle surface, this final appearance can be seen in Figure 67. 2. PVC Foam tape will be placed around the basin exterior inside the grooves as shown in Figure 68. <p><u>Reasons:</u></p> <p>The PVC Foam tape acts as an interference fit, helping maintain IP rating,</p>

	<p>Figure 68: Gasket assembly</p>		
A10	<p>Basin and Frame Assembly</p> <p>Figure 69: Exploded view of assembling 8 and A8 together</p>	<ul style="list-style-type: none"> • Aluminium frame (8) • Basin and Gasket Assembly (10) • 12 x ISO 7380 – M3 x 10 – 10N • 12 x ISO 7092 – M3 • 12 x ISO 4032 – M3 – W – N 	<p><u>Step:</u> 8 will now be screwed into A9 as shown in Figure 69.</p>
A11	<p>Assembled basin and panel</p> <p>Figure 70: Assembling A10 onto A5 – Through TIG welding</p>	<ul style="list-style-type: none"> • Top panel Assembly (A5) • Basin and Frame Assembly (A10) 	<p><u>Step:</u> A5 will be placed flat upside down, and A10 will be welded onto its upside with a fillet weld of 2mm as shown in Error! Reference source not found.. The buttons should be in the corner with M12, the orientation can be seen in Error! Reference source not found.. You must align the things in the red circle.</p> <p><u>Reasons:</u> TIG Welding is preferred over MIG, as better for thin-walled parts such as here.</p>

	 <p>Figure 71: Correct Orientation of A5 to be welded onto A10</p>		
A12	<p>Final Electronics Housing Assembly</p>  <p>Figure 72: Assembly the Screen and Seal onto Basin and Panel</p>	<ul style="list-style-type: none"> Assembled basin and panel (A11) EDPM Foam Tape LCD Screen 	<p><u>Steps:</u></p> <ol style="list-style-type: none"> Plug the cables through the designated holes, as shown in Figure 73, onto the PCB Place the LCD screen in its designated indent, as shown in Error! Reference source not found. and Error! Reference source not found.. EDPM Foam tape will be added all around the screen as shown in Error! Reference source not found.. <p><u>Reasons:</u> THE EDPM Foam tape allows for an interference fit to help maintain the IP rating.</p>
A13	<p>Pelican case ports assembly</p>  <p>Figure 73: Section view to show LCD Screen Orientation for assembl from bottom view</p>	<ul style="list-style-type: none"> Pelican case lower modified (12) 	<p><u>Steps:</u></p>

	 <p>Figure 74: Assembly of USB C port into Pelican Case (Hidden top panel and handle for simplicity)</p>  <p>Figure 75: Zoomed Front View USB-C Port</p>	<ul style="list-style-type: none"> • USB-C Port 	
A14	<p>Panel Frame with Rivets</p>  <p>Figure 76: Panel frame and Rivets assembly</p>	<ul style="list-style-type: none"> • Panel frame (4) • 12 x – M4 x 10 Rivet 	<p><u>Steps:</u></p> <p>Place the rivets into the panel frame from below in the orientation shown in Figure 76. The inner cavity should face downwards.</p>
A15	<p>Pelican Case with foams</p>  <p>Figure 77: Foam Assembly into Pelican case ports assembly</p>	<ul style="list-style-type: none"> • Load Cell Compartment (5) • Aluminium Box Foam (6) • Pelican Case Ports Assembly (A13) • Foam for Top (11) 	<p><u>Steps:</u></p> <ol style="list-style-type: none"> 1. Place 5 and 6 into the bottom of pelican case. The hole on 2 must align with hole in A13 2. Place 11 in the orientation as shown Figure 77 and glue it to the sealing of the box.

	<p>Panel frame and rivets into Pelican Case</p> <p>A16</p>	<ul style="list-style-type: none"> • Panel Frame with Rivets (A14) • Pelican case with foam (A15) • 4 x ISO 14585 ST2.9 x 9.5 – C – N 	<p><u>Steps:</u></p> <ol style="list-style-type: none"> 1. Place A14 into A15 as shown in Figure 78. 2. Use ST2.9 to screw the A14 into A15 as shown in Figure 79.
A17	<p>Final electronics housing into the Pelican Case</p> <p>A17</p>	<ul style="list-style-type: none"> • Lower pelican case assembly (A16) • O-ring • 12 x ISO 7380 M4 x 12 – 12 N 	<p><u>Steps:</u></p> <ol style="list-style-type: none"> 1. Place the O-ring and A12 into the panel frame as shown in Figure 80.

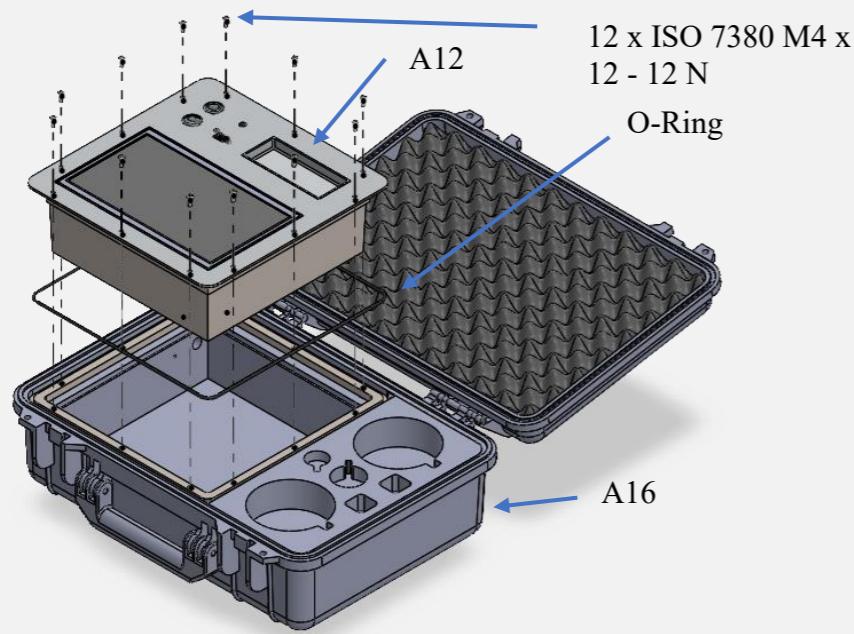


Figure 80: Exploded view of final electronics assembly into pelican case

A18	Final Assembly	<ul style="list-style-type: none"> • Final electronics housing in pelican case (A17) • Load cells 	<p><u>Steps:</u></p> <p>Place the load cells into the designated spots in the case.</p>



Figure 81: Final assembly with load cells

13.4. Assembly of Entire Product

Here is a sequence chart for assembling the product. When two arrows are pointing in one box, both predecessors must be completed to start the next assembling stage.

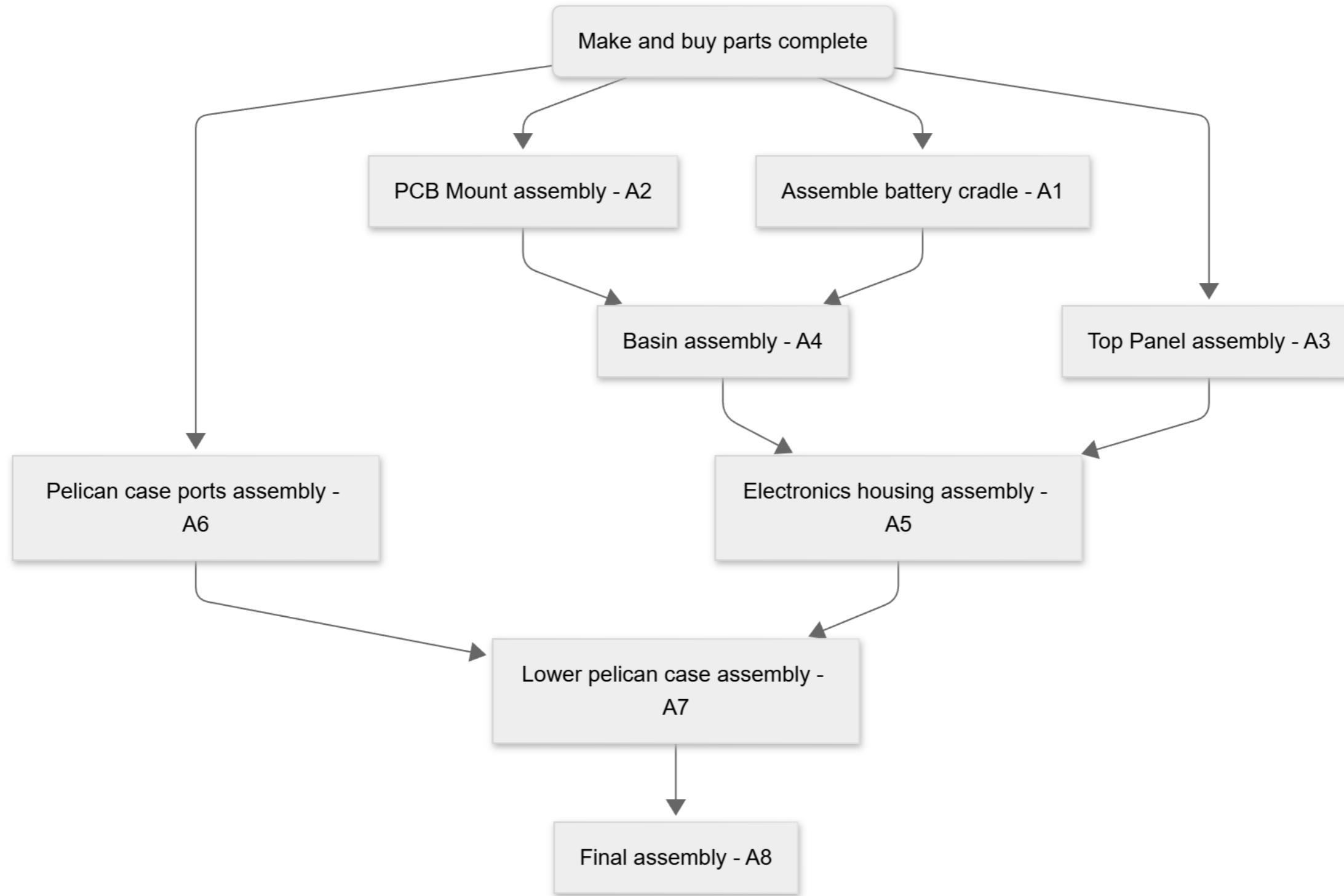


Figure 82: Sequence chart to assembly process

Here we can see how the entire product will be assembled.

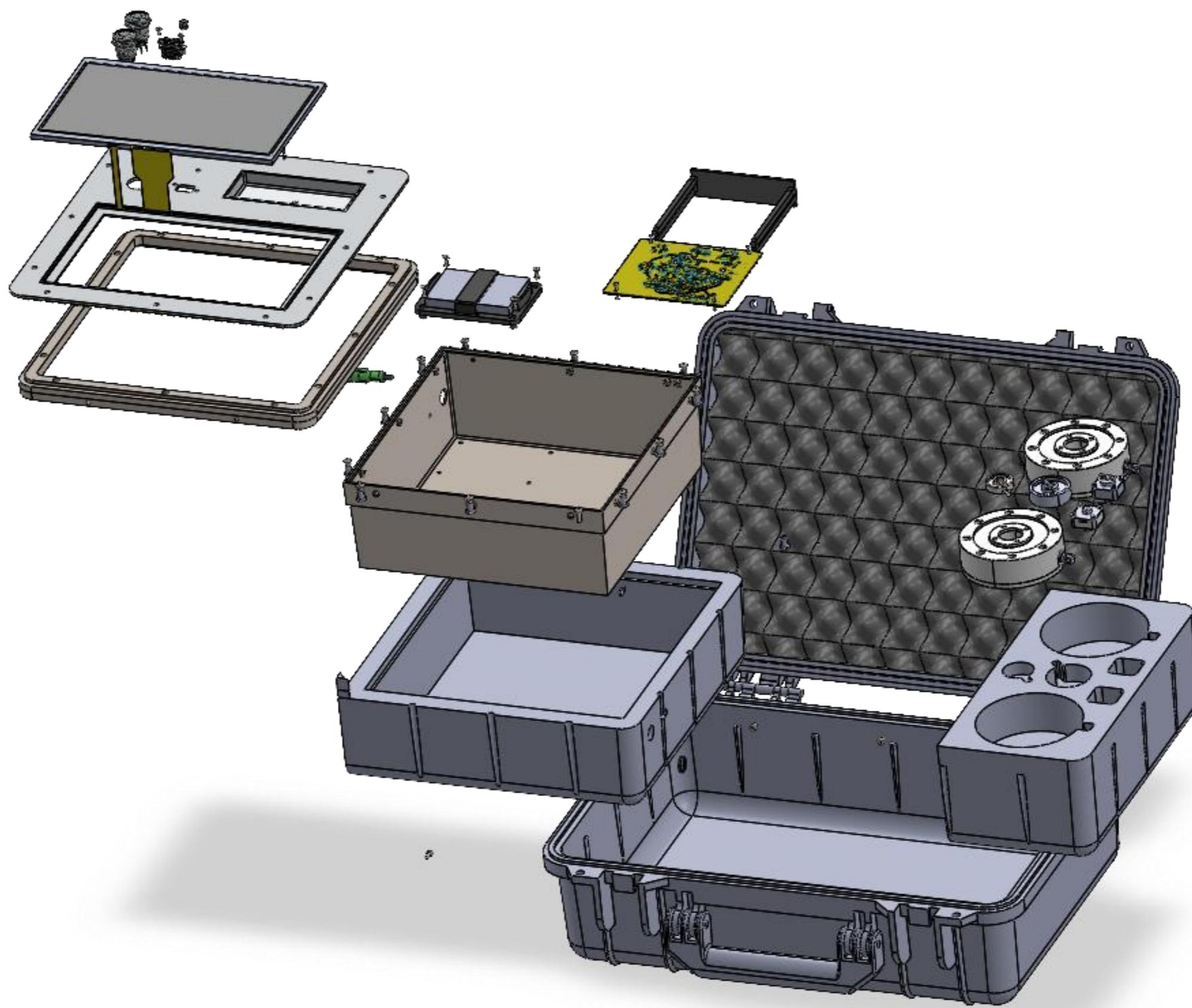


Figure 83: Exploded View of Entire Assembly

14. Requirements Manuals for Buy Parts

14.1. Requirements Manual for Electrical Parts

Table 25: Requirements Manual for Electrical Parts

Part	Qty.	Requirements	Justification
Microcontroller (MCU)	1	<ol style="list-style-type: none"> 1. ≥ 28 GPIOs 2. ≥ 160 MHz clock speed 3. ≥ 1 ADC GPIOs and ≥ 1 ADC controller 4. 3.3 V operation 5. ≥ 32 kB SRAM 6. SPI interface 7. I²C interface 8. \geq two 54-bit general purpose timers 9. USB 2.0 peripheral and USB boot mode 10. $-40\ldots 85$ °C operating temperature 	<ol style="list-style-type: none"> 1. Enough interfaces to control all components (see 10) 2. Sufficient speed to process data, control systems, drive LCD in real-time. 3. To handle battery monitoring 4. To match digital power supply (see 10.3.1) 5. To run program with Sufficient speed 6. To communication with ADC, SPI flash memory and LCD 7. To communication with digital potentiometer 8. To handle timing operations in program 9. To be programmable via USB and ease in interface with USB A for data export 10. To operate in industrial factory conditions
Load Cell Connector	1	<ol style="list-style-type: none"> 1. 5-pins 2. M-12 A-coded 3. Shielded cable. 4. compatible with Innovatest load-cell wiring. 5. PVC/PUR jacket. 6. $-25\ldots 80$ °C temperature rating. 7. low-resistance copper conductors 	<ol style="list-style-type: none"> 1. Sufficient for all load cell lines 2. IP67 rating and standardized 3. To reduce EMI noise 4. For product to be useable with Innovatest load cells 5. Suitable for harsh environments 6. To operate in industrial factory conditions 7. To reduce power loss and signal attenuation
Load Cell Interface Port	1	<ol style="list-style-type: none"> 1. Panel-mount 5-contact connector 2. IP67 rating 3. Rated current ≥ 1 A 4. screw-lock interface. 	<ol style="list-style-type: none"> 1. Compatibility with load cell connector 2. To operate in industrial factory conditions 3. Safe margin for operating with load cells (10 - 30mA) 4. Secure mechanical connection

Noise and Low-pass Filter	3	<ol style="list-style-type: none"> 1. RC/passive low-pass filter. 2. Cutoff frequency 5–20 Hz. 3. 0.1% tolerance resistors and 1% tolerance capacitors 	<ol style="list-style-type: none"> 1. Passive to ensure reliability and low power consumption 2. Aggressive filtering since signal is static 3. Accurate dimensioning of corner frequency
Amplifier (Pre-amplifier + noise filtering)	1	<ol style="list-style-type: none"> 1. Resistor set gain (100) 2. > 124dB CMRR at Gain of 100 3. > 35 V/μs slew rate 4. > 10 Hz bandwidth at 100 gain 5. < 0.1 μV peak-to-peak noise (input) at gain of 100 6. > 5V single supply operation 7. 0.3 – 0.6 mA supply current 8. < 0.3 μV/°C offset drift 9. < 3 ppm/°C gain drift 	<ol style="list-style-type: none"> 1. For pre-amplification (see 9.3.3) 2. To Sufficiently attenuate common noise from the load cell signals 3. Ensures quick measurement times 4. To ensure it operates within system bandwidth. 5. To stay within noise budget (see 10.6) 6. For compatibility with rest of measurement chain 7. To stay within power budget (see 10.4) 8. To minimize effects of high temperature environments 9. To minimize effects of high temperature environments
Amplifier (Variable Gain)	1	<ol style="list-style-type: none"> 1. 1 – 5 gain range 2. < 0.4 μV peak-to-peak noise 3. >5V single supply operation 4. 0.3 – 0.6 mA supply current 5. Zero-drift 6. 1024 step digital potentiometer 	<ol style="list-style-type: none"> 1. To match load cell sensitivity 2. To stay within noise budget (see 10.6) 3. For compatibility with rest of measurement chain 4. To stay within power budget (see 10.4) 5. Sufficient precision to vary gain to match load cells with minimal error
Analog to Digital Converter (ADC) Chip	1	<ol style="list-style-type: none"> 1. 24-bit resolution 2. Programmable OSR 3. On-board digital filter 4. SPI 5. 5V reference mode 6. Buffered inputs 7. < 7μV peak-to-peak noise 8. 1 – 3 mA supply current 9. > 5V single analogue supply operation 10. 3.3V isolated digital supply 11. < 0.1 μV/°C offset drift 12. < 1 ppm/°C gain drift 	<ol style="list-style-type: none"> 1. To ensure precision requirements are met 2. To adjust sampling rate (see 3.1.5) 3. To reject in-band noise and remove quantization noise (see 9.3.6) 4. For very fast data transfer speeds 5. To have Sufficient reading resolution 6. To reduce current draw and increase accuracy 7. To stay within noise budget (see 10.6) 8. To stay within power budget (see 10.4) 9. For compatibility with rest of measurement chain

			<ul style="list-style-type: none"> 10. So that level shifting the output is not needed 11. To minimize effects of high temperature environments 12. To minimize effects of high temperature environments
Cell Excitation Regulator	2	<ul style="list-style-type: none"> 1. One with 5V output and one with 10V output 2. > 80 % efficiency to keep power losses low 3. ≤ 0.1 mV noise at output 4. ≥ 30mA output current 	<ul style="list-style-type: none"> 1. To be able to switch between 5V and 10V excitation 2. To keep power losses low 3. To stay within noise budget (see 9.5) 4. Sufficient current to excite load cells at both excitation voltages
Touchscreen Display	1	<ul style="list-style-type: none"> 1. 10.1" TFT; 1024×600 resolution; ≥ 100 cd/m² brightness 2. 4-wire resistive touch. 3. ≥ 3.3 V supply 4. SPI/parallel interface. 	<ul style="list-style-type: none"> 1. Guarantees visibility in different lighting conditions during field use 2. Allows for precise control even with gloves 3. Compatibility with digital supply 4. High speed communication with MCU for good reactivity on display
Push Button	2	<ul style="list-style-type: none"> 1. Panel-mount 2. IP67 3. ≥ 1 A @ 5 VDC. 4. ≥ 30 000 electrical cycles 5. ≥ 30 000 mechanical cycles 6. RGB ring LED 	<ul style="list-style-type: none"> 1. To ensure it is secure in panel (see A4 in Table 24) 2. Suitable for harsh factory environments and to not compromise IP rating of the rest of the product 3. To handle complete battery load 4. To last 8-year service life 5. To last 8-year service life 6. To indicate power status to user
Non-volatile Memory Module	1	<ul style="list-style-type: none"> 1. ≥ 8 MB SPI Flash. 2. 3.3 V operation 3. $\geq 100k$ P/E cycles 4. ≥ 8 years data retention 	<ul style="list-style-type: none"> 1. Sufficient storage and speed for data logging and export 2. For compatibility with digital supply 3. To last 8-year service life 4. To last 8-year service life
USB-A Port	1	<ul style="list-style-type: none"> 1. USB-A female 2. Panel mount 3. USB 2.0 compliant. 4. Insertion life ≥ 1500 cycles. 5. IP67 	<ul style="list-style-type: none"> 1. Standard and common connector for USB drives 2. To ensure it is secure in panel (see A4 in Table 24) 3. To allow for faster data transfer rate 4. To last 8-year service life 5. To operate in factory environment and not compromise IP rating of the rest of the product

Power Regulator	2	<ol style="list-style-type: none"> 1. 5.5 V and 3.3 V outputs. 2. ≤ 0.1 mV ripple for 5.5V 3. < 20 mV ripple for 3.3V 4. ≥ 500 mA continuous output 	<ol style="list-style-type: none"> 1. Dedicated regulators maintain stable 5.5 V and 3.3 V rails for analog and digital devices (respectively) 2. Low noise injection into sensitive measurement chain components (see 10.6) 3. Low noise, but less sensitive than analogue components 4. To ensure sufficient power output to drive all devices (see 10.4)
USB-C Port	1	<ol style="list-style-type: none"> 1. USB-C receptacle. 2. 5 V input. 3. mechanical retention ≥ 8 N. 4. IP67 housing and coating 	<ol style="list-style-type: none"> 1. Compatibility with modern charging cables 2. Sufficient voltage to charge the Li-Ion battery 3. To ensure charging cable does not disconnect accidentally 4. To operate in factory environment and not compromise IP rating of the rest of the product
Battery Charging Controller	1	<ol style="list-style-type: none"> 1. 3.7V charging option designed for Li-Po 2. Charge current up to 1 A 3. Integrated OV/OC/OT protection 	<ol style="list-style-type: none"> 1. Compatible with 3.7V Li-Po battery 2. For faster charging 3. To handle fluctuations and spikes from external power source
Battery	1	<ol style="list-style-type: none"> 1. Li-Po battery ≥ 7000 mAh. 2. Discharge capability ≥ 2 A. 3. IEC-compliant cell pack. 	<ol style="list-style-type: none"> 1. High energy cell with Sufficient capacity to operate for 8 hours of measurements (see 10.4) 2. To ensure Sufficient output of power to supply entire circuit 3. For safety and regulatory concerns
Battery Terminal	1	<ol style="list-style-type: none"> 1. ≥ 2 A current rating 2. $\geq 10 \text{ mm}^2$ wire size 3. $\geq 60\text{N}$ separation force 	<ol style="list-style-type: none"> 1. To handle required output current 2. Low resistance and thus low power loss 3. To ensure connector does not come loose after assembly
LED	1	<ol style="list-style-type: none"> 1. Bi-colour 2. $\geq 50,000$ hours life span 3. IP67 4. 4 mm diameter 	<ol style="list-style-type: none"> 1. To indicate 2 states; charging and discharging (see 10.3.4) 2. To last 8-year service life 3. To operate in factory environment and not compromise IP rating of the rest of the product 4. For compatibility with product top panel (see A4 in Table 24)
Transistors (MOSFETs)	6	<ol style="list-style-type: none"> 1. 3 N-Channel and 3 P-Channel 2. ≥ 5 V maximum drain-source voltage 3. ≥ 2 A maximum current 	<ol style="list-style-type: none"> 1. To ensure switching network is configured correctly (see 10.3.1) 2. To ensure MOSFETs can block the battery voltage effectively

		4. $\leq 10\text{ns}$ on-delay	3. To ensure MOSFET does not burn out from battery current 4. To ensure switching happens quickly and does not delay the circuit operations
Diodes	3	1. $\geq 2\text{ A}$ maximum forward current 2. $\geq 5\text{V}$ peak inverse voltage 3. $< 1.0\text{V}$ voltage drop	1. To ensure power can flow without burning out the diode 2. To ensure the diode can block main supply lines from reverse polarity 3. To ensure there is fewer potential losses
Optocoupler	1	1. $\geq 10\text{V}$ isolation voltage 2. $\geq 5\text{Mbps}$ speed	1. Sufficient isolation between MCU pin and power line 2. Sufficient speed for the circuit to power up quickly
Capacitors	41	1. X7R ceramic capacitors 2. 3216 ¹³ package size for capacitors $\geq 10\ \mu\text{F}$ 3. 2012 package size for capacitors $< 10\ \mu\text{F}$ 4. Various values (see 10.7) for values	1. Greater stability of nominal capacitance 2. Larger package size is better for bulk decoupling 3. Smaller package size is better for low inductance 4. Capacitance values chosen for specific purposes as described in 10. Circuit Design and 10.7 Component Specifications
Resistors	30	1. Metal oxide resistors (or bet 2. Various values (see 10.7) for values	<ul style="list-style-type: none"> • Better for higher current and voltage but lower precision • Resistor values chosen for specific purposes as described in 10. Circuit Design and 10.7 Component Specifications
Precision Resistors	6	1. Thin film 2. $\leq 0.1\%$ tolerance 3. Various values (see 9.7) for values	1. Have more precision than metal oxide resistors 2. Sufficiently precise for measurement chain 3. Resistor values chosen for specific purposes as described in 10. Circuit Design and 10.7 Component Specifications
Inductors	4	1. $\geq 2\text{ A}$ current rating 2. $\leq 10\ %$ tolerance 3. Various values (see 9.7) for values	3. Sufficient current to handle power delivery 4. Inductances values is not required to be as precise as capacitors and resistors 5. Inductance values chosen for specific purposes as described in

¹³ All package sizes are referred to in metric units (mm)

			10. Circuit Design and 10.7 Component Specifications
Wires	-	1. ≥ 2 A current rating 2. $\geq 10 \text{ mm}^2$ wire size	1. Sufficient current to handle power and signal for connections of M12, USB A, USB C and LED to the PCB. 2. Low resistance and thus low power loss

14.2. Requirements Manual for Mechanical Parts

Table 26: Requirements Manual for Mechanical Parts

Part	Qty.	Requirements	Justification
Protective Carrying Case	1	<ul style="list-style-type: none"> Polypropylene copolymer case. IP67 rating. pressure equalization valve. internal dimensions $\geq 420 \times 280 \times 150$ mm. impact-resistant hinges and latches. 	A rugged IP67 case protects the entire system from dust, water, shock, and transport damage during field deployment.
Foam	1	<ul style="list-style-type: none"> EVA/PU foam inserts; density $\geq 30 \text{ kg/m}^3$. CNC/laser-cut cavities. compression-set resistant. thickness matched to internal case profile. 	Custom-cut EVA/PU foam provides precise support for each load cell and electronic component, minimizing vibration and mechanical stress.
1-Panel Frame	1	<ul style="list-style-type: none"> Aluminium/steel front panel. 2–3 mm thickness. anodized or powder coated. cut-outs for display, button, LED. mounting pattern aligned with internal frame. 	A rigid front panel provides secure mounting for the display and controls, preventing misalignment and improving long-term usability.
Button Head Screws	12	<ul style="list-style-type: none"> M4 x 0.7 x 12 ISO 7380 	Button head screws were selected because they provide sufficient clamping force to securely fasten components while also applying uniform pressure to gaskets and O-rings, improving the overall IP sealing performance. M4 screws were used on the panel plate interface because this region has greater aluminium thickness and requires higher structural rigidity,
	4	<ul style="list-style-type: none"> M2 x 0.4 x 16 ISO 1485 	
	12	<ul style="list-style-type: none"> M3 x 0.5 x 8 ISO 7380 	
	2	<ul style="list-style-type: none"> M3 x 0.5 x 6 ISO 7380 	

			making the larger fastener size more appropriate
Tapping Screws	4	<ul style="list-style-type: none"> • ST2.9 x 9.5 • ISO 14585 	Tapping screws were used to connect the panel frame to the case, as they can create threads directly in the plastic.
Rivet Nuts	12	<ul style="list-style-type: none"> • M4 x 10 • Length 9-10 mm 	Rivet nuts were used to allow the head screws to clamp the panel plate securely, without having to tap the threads into the aluminium frame, this has the advantage of keeping the joints serviceable for longer.
Hex Nuts	16	<ul style="list-style-type: none"> • M3 x 0.5 • ISO 4032 	Hex nuts were used as they provide reliable, removable fastening where aluminium is too thin to be threaded.
	4	<ul style="list-style-type: none"> • M2 x 0.4 • ISO 4035 	
Washers	12	<ul style="list-style-type: none"> • M4 • ISO 7092 	Washers were used to distribute the load from the screws, preventing local deformations. They also help maintain the IP rating by ensuring even compression.
	16	<ul style="list-style-type: none"> • M3 • ISO 7092 	
Velcro Roll	1	<ul style="list-style-type: none"> • 20mm Wide 	A Velcro strap will be used to secure the battery to the cradle while still allowing for it to expand without over constraining it.
PVC Foam Tape	1	<ul style="list-style-type: none"> • 10mm Wide • 2mm thick 	PVC foam tape was used to seal small gaps around the screen because it compresses well, and provides good water and dust resistance.
3M Scotch-Weld Epoxy DP420	1	<ul style="list-style-type: none"> • 1 mm Thickness 	A 1 mm layer of DP420 was used as it bonds well to aluminium and ABS, and provides great shear and peel strength.

15. Bill of Materials

15.1. Electrical Bill of Materials

Table 27: Electrical Bill of Materials

Reference	Part Name (Model No.)	Brand	Qty.	Specifications
BT1	Battery Terminal (XT90PW)	AMASS	1	<ul style="list-style-type: none"> • 3.7V charging option designed for Li-Po • Charge current up to 1 A • Integrated OV/OC/OT protection
C1, C23	Voltage Blocking Capacitor (ECA-1HM101B)	Panasonic	2	<ul style="list-style-type: none"> • 100µF • Aluminium electrolytic capacitors
C2, C4, C5, C6, C8, C10, C13, C15, C19, C20, C27, C33, C40	Decoupling Capacitor (GRT21BR71H104KE01L)	Murata	13	<ul style="list-style-type: none"> • 0.1µF • X7R ceramic capacitors • 2012 package size
C3	Filter Capacitor (GRM21BR71C105KA01K)	Murata	1	<ul style="list-style-type: none"> • 1µF • X7R ceramic capacitors • 2012 package size
C7, C9, C11, C12, C24, C25, C26, C28, C34, C35, C37, C41	Decoupling Capacitor (GCJ31CR71C106KA15K)	Murata	12	<ul style="list-style-type: none"> • 10µF • X7R ceramic capacitors • 3216 package size
C14	Filter Capacitor (GCM21BR71C335KA73L)	Murata	1	<ul style="list-style-type: none"> • 3.3µF • X7R ceramic capacitors • 2012 package size
C16	Filter Capacitor (GRM21BR71C475KE51L)	Murata	1	<ul style="list-style-type: none"> • 4.7µF • X7R ceramic capacitors • 2012 package size
C17	Filter Capacitor (GRM21BR71C334JA01L)	Murata	1	<ul style="list-style-type: none"> • 0.33µF • X7R ceramic capacitors • 2012 package size
C18	Filter Capacitor (GRM219R71C474JA01D)	Murata	1	<ul style="list-style-type: none"> • 0.47µF • X7R ceramic capacitors • 2012 package size
C21	Capacitor (GCQ0335C1H100JB01D)	Murata	1	<ul style="list-style-type: none"> • 10pF • MLCC

				<ul style="list-style-type: none"> • 0603 package size
C22	Capacitor (GRJ21AR72E102KWJ1D)	Murata	1	<ul style="list-style-type: none"> • 10nF • X7R ceramic capacitors • 2012 package size
C29	Capacitor (GRM21AR7LU332KW01D)	Murata	1	<ul style="list-style-type: none"> • 3.3nF • X7R ceramic capacitors • 2012 package size
C30, C31, C32, C36, C39	Capacitor (GRM31CZ71C226ME15K)	Murata	5	<ul style="list-style-type: none"> • 22µF • X7R ceramic capacitors • 3216 package size
C38	Capacitor (GRT21BR71C225KE01L)	Murata	1	<ul style="list-style-type: none"> • 2.2µF • X7R ceramic capacitors • 2012 package size
D1	ESD Diode (SMF5V0A)	Vishay	1	<ul style="list-style-type: none"> • 50 A maximum forward current • 7.1V peak inverse voltage • 0.7V voltage drop
D2	Bi-colour LED Light Pipe (PLTR5-8MM-PR1)	Bivar	1	<ul style="list-style-type: none"> • Bi-colour LED • IP67
D3, D4	Schottky Diode (STPS340S)	STMicro-electronics	2	<ul style="list-style-type: none"> • 3A maximum forward current • 40V peak inverse voltage • 0.52V voltage drop
IC1	Charging Controller (MCP73223)	Microchip	1	<ul style="list-style-type: none"> • 3.7V charging option designed for Li-Po • Charge 0.130 to 1.1 A • Integrated OV/OC/OT protection
IC2	Voltage Reference (MAX6126)	Maxim Integrated	1	<ul style="list-style-type: none"> • 5V reference output • ±0.02% accuracy • 1.3µV peak-to-peak noise • 380 µA supply current • 0.4V voltage dropout at 5V reference • 3ppm/°C voltage temperature coefficient
J1	M12 5-pin (ABQEHI)	Phoenix Contact	1	<ul style="list-style-type: none"> • 5-pins • M-12 A-coded • Shielded terminal • -25...80 °C temperature rating. • low-resistance copper conductors

J2	USB A (SS-52200-001)	Stewart Connector	1	<ul style="list-style-type: none"> • USB-A female • Panel mount • USB 2.0 compliant. • Insertion life 1500 cycles. • IP67
J3	USB C (SS-52400-012)	Stewart Connector	1	<ul style="list-style-type: none"> • USB-C receptacle. • 5 V input. • mechanical retention 9 N. • IP67 housing and coating
L1, L3, L4	Inductor (8532R-09K)	Delevan	3	<ul style="list-style-type: none"> • 4.7µH • 4.01 A current rating • 10 % tolerance
L2	Inductor (RLB0913-2R2K)	Bourns	1	<ul style="list-style-type: none"> • 2.2µH • 5.6 A current rating • 10 % tolerance
Q1, Q2, Q5	P-Channel MOSFET (AO3401A)	Alpha & Omega	3	<ul style="list-style-type: none"> • P-channel • 30V maximum drain-source voltage • 4A maximum current • 6.5ns on-delay
Q3, Q4, Q6	N-Channel MOSFET (AO3400A)	Alpha & Omega	3	<ul style="list-style-type: none"> • N -channel • 30 V maximum drain-source voltage • 5.7 A maximum current • 3ns on-delay
R1, R2	Resistor (TNPW08055K10FETA)	Vishay	2	<ul style="list-style-type: none"> • 5.1kΩ • Thin film resistors
R3	Resistor (ROX050500KFKLB)	Vishay	1	<ul style="list-style-type: none"> • 500kΩ • Metal oxide resistors
R4	Resistor (271-24.3K-AP-RC)	Xicon	1	<ul style="list-style-type: none"> • 24.3kΩ • Metal film resistors
R5	Resistor (RSF200JR-52-200K)	YAGEO	1	<ul style="list-style-type: none"> • 200kΩ • Metal oxide resistors
R6, R9, R10	Precision Resistor (ERA-3AEB103V)	Panasonic	3	<ul style="list-style-type: none"> • 10kΩ • Thin film resistors • 0.1% Tolerance
R12, R13, R15, R20, R21, R24, R25, R26, R30, R31, R34, R35	Resistor (RSF50SJT-52-10K)	YAGEO	11	<ul style="list-style-type: none"> • 10kΩ • Metal oxide resistors
R7	Precision Resistor (ERA-3AEB101V)	Panasonic	1	<ul style="list-style-type: none"> • 100Ω • Thin film resistors

				<ul style="list-style-type: none"> • 0.1% Tolerance
R8	Precision Resistor (ERA-3ARB472V)	Panasonic	1	<ul style="list-style-type: none"> • 4.7kΩ • Thin film resistors • 0.1% Tolerance
R11	Precision Resistor (ERA-3AEB4991V)	Panasonic	1	<ul style="list-style-type: none"> • 4.99kΩ • Thin film resistors • 0.1% Tolerance
R14	Resistor (RSPF12JT1K20)	SEI Stackpole	1	<ul style="list-style-type: none"> • 1.2kΩ • Metal oxide resistors
R16	Resistor (RSF100JT-73-1K)	YAGEO	1	<ul style="list-style-type: none"> • 1kΩ • Metal oxide resistors
R17, R22	Resistor (RNF14BBE100K)	SEI Stackpole	2	<ul style="list-style-type: none"> • 100kΩ • Metal film resistors
R18	Resistor (RSF100JB-73-1M)	YAGEO	1	<ul style="list-style-type: none"> • 1MΩ • Metal oxide resistors
R19	Resistor (MFR-25FBF52-71K5)	YAGEO	1	<ul style="list-style-type: none"> • 71.5kΩ • Metal film resistors
R23	Resistor (PTF6531K250BZWF)	Vishay	1	<ul style="list-style-type: none"> • 31.25kΩ • Metal film resistors
R27	Resistor (MFR-25FBF52-301K)	YAGEO	1	<ul style="list-style-type: none"> • 301kΩ • Metal oxide resistors
R28	Resistor (PTF6540K000FZBF)	Vishay	1	<ul style="list-style-type: none"> • 40kΩ • Metal film resistors
R29	Resistor (MFR-25FBF52-4K87)	YAGEO	1	<ul style="list-style-type: none"> • 4.87kΩ • Metal film resistors
R32	Resistor (MF1/4DC1742F)	KOA Speer	1	<ul style="list-style-type: none"> • 17.4kΩ • Metal film resistors
R33	Resistor (MFR-25FRF52-127K)	YAGEO	1	<ul style="list-style-type: none"> • 127kΩ • Metal film resistors
R36	Resistor (RSF-50JT-52-20K)	YAGEO	1	<ul style="list-style-type: none"> • 20kΩ • Metal oxide resistors
SW1, SW2	Push Buttons (P19TFRGBPOWER)	Metzler	2	<ul style="list-style-type: none"> • Panel-mount • IP67 • Up to 3A @ 250 V • >100,000 electrical cycles • >1,000,000 mechanical cycles • RGB ring LED
U1	Instrumentation Amplifier (AD8421)	Analog Devices	1	<ul style="list-style-type: none"> • Resistor set gain (100) • 124dB CMRR at Gain of 100 • 35 V/µs slew rate • 10 Hz bandwidth at 100 gain

				<ul style="list-style-type: none"> • 0.07 μV peak-to-peak input noise at gain of 100 • 5V single supply operation • 2 – 2.3 mA supply current • 0.2 μV/$^{\circ}$C offset drift • 1 ppm/$^{\circ}$C gain drift
U2	Operational Amplifier (OPA188)	Texas Instruments	1	<ul style="list-style-type: none"> • 1 – 5 gain range • 0.25 μV peak-to-peak noise • 2V to 18V single supply operation • 0.51 mA supply current • Zero-drift (0.03 μV/$^{\circ}$C)
U3	Delta-Sigma Analogue to Digital Converter (ADS127L21)	Texas Instruments	1	<ul style="list-style-type: none"> • 24-bit resolution • Programmable OSR • On-board digital filter (sinc, FIR and IIR chain) • SPI • 5V reference mode • Buffered inputs • ~6.395μV peak-to-peak noise • 1.24 – 1.43 mA supply current • 5V single analogue supply operation • 3.3V isolated digital supply • 0.05 μV/$^{\circ}$C offset drift • 0.5 ppm/$^{\circ}$C gain drift
U4	Digital Potentiometer (MCP41U83)	Microchip	1	<ul style="list-style-type: none"> • 1024 steps • 20kΩ range • SPI communication • 2 μA supply current in standby • 15 mA supply current when being programmed
U5	Optocoupler (PS9117A)	Renesas	1	<ul style="list-style-type: none"> • 3750V insulation voltage • 10 Mbps
U6	10V Voltage Regulator (TPS61170)	Texas Instruments	1	<ul style="list-style-type: none"> • 10 V output

				<ul style="list-style-type: none"> • ~0.1 mV ripple • Up to 300 mA continuous output • 90% efficiency at 10V output
U7	3.3V Voltage Regulator (TPS62130)	Texas Instruments	1	<ul style="list-style-type: none"> • 3.3 V output • 18 mV ripple at 3.3V and 0.7A • Up to 3A continuous output • 94% efficiency at 3.3V and 0.7A
U8	5V Voltage Regulator (TPS61099)	Texas Instruments	1	<ul style="list-style-type: none"> • 5V output • ~0.1mV ripple • Up to 300mA continuous output • 95% efficiency at 3.3V and 30mA output
U9	5.5V Voltage Regulator (TPS61089)	Texas Instruments	1	<ul style="list-style-type: none"> • 5.5 V output • ~0.1 mV • Up to 10A continuous output • 94% efficiency at 5.5V and 0.7A output
U10	Non-volatile Memory (W25Q128JVS)	Winbond	1	<ul style="list-style-type: none"> • 16 MB SPI Flash. • 2.7 to 3.6 V operation • >100k P/E cycles • > 20 years data retention
U11	Microcontroller (ESP32-P4)	Espress-if	1	<ul style="list-style-type: none"> • 55 GPIOs • 360 MHz clock speed • 25 ADC GPIOs and 2 ADC controller • 3.3 V operation • 32 kB SRAM • SPI interface • I²C interface • Four 54-bit general purpose timers • USB 2.0 peripheral and USB boot mode • -40...85 °C operating temperature
U12	TouchScreen/SPI Touch Controller (ER-TFT101-1)	EastRising	1	<ul style="list-style-type: none"> • 10.1" TFT; 1024×600 resolution • 150 cd/m² brightness • 4-wire resistive touch. • 3.3 V supply

				<ul style="list-style-type: none"> • SPI/parallel interface. • 120mA backlight current
1	Printed Circuit Board	Würth Elektronik	1	<ul style="list-style-type: none"> • FR-4 substrate • Copper foil • ENIG finish • Solder mask and silkscreen lamination
13	M12 Load Cell Cable (77 2529 0000 50705-0200)	Binder	1	<ul style="list-style-type: none"> • 5-pins • M-12 A-coded • Shielded cable • Four wires available to connect to Innovatest load cells • PVC/PUR jacket. • -25...80 °C temperature rating. • low-resistance copper conductors • 28 AWG
15	Battery (YDL866898)	YDL	1	<ul style="list-style-type: none"> • Lithium Polymer • 3.7V • 7200mAh • Up to 2.5A discharge current • IEC-compliant
16	150 gf Load Cell (A151)	Innovatest	1	<ul style="list-style-type: none"> • 3.0 mV/V @ 150gf • 350Ω bridge resistance • ≥500MΩ insulation resistance
17	2 kgf Load Cell (C202)	Innovatest	1	<ul style="list-style-type: none"> • 2.35 mV/V @ 2kgf • 350Ω bridge resistance • ≥500MΩ insulation resistance
18	20 kgf Load Cell (E20K)	Innovatest	1	<ul style="list-style-type: none"> • 2.7 mV/V @ 20kgf • 175Ω bridge resistance • ≥500MΩ insulation resistance
19	45 kgf Load Cell (D45K)	Innovatest	1	<ul style="list-style-type: none"> • 3.0 mV/V @ 45kgf • 350Ω bridge resistance • ≥500MΩ insulation resistance
20	250 kgf Load Cell (F250K)	Innovatest	1	<ul style="list-style-type: none"> • 3.25 mV/V @ 250kgf • 175Ω bridge resistance • ≥500MΩ insulation resistance

21	3000 kgf Load Cell (F3000K)	Innovatest	1	<ul style="list-style-type: none"> • 2.8 mV/V @ 3000kgf • 175Ω bridge resistance • ≥500MΩ insulation resistance
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15.2. Mechanical Bill of Materials

Table 28: Mechanical Bill of Materials

Position Number	Part Name	Material	Qty	Standard¹⁴
2	PCB Mount	General Purpose Polycarbonate	1	ISO 21305-1:2019
3	Battery Cradle	Heat resistant ABS	1	ISO 2580-1 ABS
4	Panel Frame	5052 Aluminium	1	ISO: Al-Mg2,5
5	Load Cell Compartment	Medium Density EVA Foam	1	Make
6	Aluminium Box Foam	Medium Density EVA Foam	1	Make
7	Electronics Basin	5052 Aluminium	1	ISO: Al-Mg2,5
8	Aluminium Frame	5052 Aluminium	1	ISO: Al-Mg2,5
9	Panel	5052 Aluminium	1	ISO: Al-Mg2,5
10	Cable Tray	5052 Aluminium	1	ISO: Al-Mg2,5
11	Top Foam	Medium Density EVA Foam		Make
12	Lower Pelican Case			Modify
14	Upper Pelican Case			

¹⁴ For custom “Make” parts, the ISO standard refers to the material while for “Buy” parts it is the design of the machine element itself

	M4 x 0.7 x 12 Butten Head Screws		12	ISO 7380
	M2 x 0.4 x 16 Butten Head Screws		4	ISO 1485
	M3 x 0.5 x 8 Butten Head Screws		12	ISO 7380
	M3 x 0.5 x 6 Butten Head Screws		2	ISO 7380
	ST2.9 x 9.5 Tapping Screws		4	ISO 14585
	M4 x 0.7 Rivet Nuts		12	
	M3 x 0.5 Hex Nuts		16	ISO 4032
	M2 x 0.4 Hex Nuts		4	ISO 4035
	M4 Washers		12	ISO 7092
	M3 Washers		16	ISO 7092
	Velcro Roll		1	
	PVC Foam Tape		1	
	3M Scotch- Weld Epoxy DP420		1	

16. Production Planning

16.1. Production Inputs

16.1.1. Production Assumptions

Some assumptions have been made regarding the calculations in this section, these include:

1. No technical failure, with machines or powers (which can cease production for some time) in the manufacturing and assembly process
2. No human failure, such as failed production (e.g. incorrectly welded, breakage)
3. 100% human resource availability (no employee holiday etc.)

4. 100% production yield rate – no make parts are incorrectly manufactured
5. No shipment time – shipment is instantly available
6. All machines are ideally available for the same time as employees minus a 30-minute break.
7. A single worker can only work one shift per day

16.1.2. Production Target

The production target for the first 3 years is set as 500, this distribution will not be even, and will be as such:

Table 29: Production targets for three years

Year	Production Target	Accumulated Units	Reasoning
1	150	150	
2	150	300	For the first two years, production has been kept relatively low, so in case of problems with manufacturing the process can be improved, or in case of poor response from market, production halted to minimize losses.
3	200	500	By year three, the company has a better picture of the product so can start ramping up production.

16.1.3. Working days

Naturally, each year has holidays, which should be accounted for production planning, to estimate how many units must be produced per time unit, here is an overview of how many working days there are in a year where production can continue and how many products must be produced per week.

In Germany three general working structures can be considered, 2-day weekends, 1-day weekends or continuous production with no holidays, however that is only permitted legally for products which technically require uninterrupted production, which is not the case for the product hence calculations omitted.

Numbers of days in a year (assuming non-leap year): 365 days

Table 30: Target production per unit time calculations

Field	Considering 2-day weekends	Considering 1-day weekend
Weekend holidays	52 weeks x 2 days/weeks = 104 days	52 weeks x 1 day/weeks = 52 days

Public holidays¹⁵	9 days	9 days
Working days (D_{year})	365 days – (104 days+9 days) = 252 days	365 days – (52 days+9 days) = 304 days
Target production per day (years 1 and 2)	150 units / 252 days = 0.5952 units/day	150 units / 304 days = 0.4934 units/day
Target production per week (years 1 and 2)	0.5952 units/day x 5 days/weeks = 2.976 units/week ≈ 3 units/week	0.4934 units/day x 6 days/weeks = 2.96 units/week ≈ 3 units/week
Target production per day (year 3)	200 units / 252 days = 0.7937 units/day	200 units / 304 days = 0.6579 units/day
Target production per week (year 3)	0.7937 units/day x 5 days/weeks = 3.968 units/week ≈ 4 units/week	0.6579 units/day x 6 days/weeks = 3.947 units/week ≈ 4 units/week

Considering the minimal change in units produced per day or week in 5 or 6 working days, it is best to go for 5 days working, to save on costs of another day on employees and machinery (variable costs). Thus, we will use a 5-day work week.

16.1.4. Takt Time

Considering the working shifts and production target, the Takt Time can now be calculated using the Equation (18):

$$T_{takt} = \frac{D_{year} \cdot N_{shift} \cdot t_{shift}}{U_{year}^{total}} \quad (18)$$

Where T_{takt} is the takt time [seconds], D_{year} working days in a year [days/year], N_{shift} is the number of shifts in a working day [shifts/day], t_{shift} is the shift working time [seconds/shift] and U_{year}^{total} is the production volume target [units/year]

Together, the working days, shifts and time per shift make the yearly working time (t_w).

For the 5-day work week, we get $D_{year} = 252 \frac{\text{days}}{\text{year}}$. We also assume there to be 1 shift in a day ($N_{shift} = 3 \frac{\text{shifts}}{\text{day}}$) of around 7.5 hours each ($t_{shift} = 27000 \frac{\text{s}}{\text{shifts}}$) accounting for 30-minute break.

Hence, we get the following takt times for each production year:

¹⁵ These vary state-by-state (usually 10-13), however 9 are nationwide hence assumed for the calculations

1. Year 1: $45360 \frac{s}{unit}$ or $756 \frac{min}{unit}$
2. Year 2: $45360 \frac{s}{unit}$ or $756 \frac{min}{unit}$
3. Year 3: $34020 \frac{s}{unit}$ or $567 \frac{min}{unit}$

For more details on the calculations, see Appendix D: Production Planning Calculations.

16.1.5. Outsourcing

Given the limited manufacturing capabilities of Innovatest and the tight budget constraints, a number of the custom “Make” parts should be outsourced to manufacturing firms. For the 500 unit over three years target, purchasing machines to manufacture the parts is not economically justifiable.

16.2. Equipment Outline

16.2.1. List of Machinery

Table 31: Machine Selection for Production

Machine	Technical Requirements	Cost per Unit (Euros)	Selected Machine
3D Printer	Printing Technology FDM Build Volume $250 \times 210 \times 220$ mm Layer Resolution 0.05–0.3 mm adjustable Nozzle Diameter 0.4 mm (standard) Materials ABS Heated Bed 100–120°C bed Tolerances ± 0.2 –0.4 mm Filament Diameter 1.75 mm (standard) Slicing Software Must support rafts, supports and custom infill	800	Prusa i3 MK4
4-Axis CNC Milling Machine	Axes 4-axis simultaneous interpolation (X/Y/Z + rotary A) Work Envelope $\geq 300 \times 300 \times 200$ mm Spindle Speed 10,000–24,000 rpm	70000	Haas Automation 4-Axis CNC

	Spindle Power	2–7 kW		
	Tool Changer	6–12 ATC minimum		
	Accuracy	Positioning: ±0.01 mm, Repeatability: ±0.005 mm		
	Materials	Aluminium 5052		
	Table	T-slot or vacuum		
	Coolant	Flood or minimum-quantity lubrication (MQL)		
3-Axis CNC Contour Machine	Axes	X/Y/Z with contouring capability		
	Work Envelope	≥ 400 × 400 × 100 mm		
	Cutting Speed	Suitable for foam cutting at 5,000–20,000 mm/min		
	Spindle Speed	10,000–20,000 rpm	50000	Datron neo
	Tooling	Ball-end mills, foam cutters, V-bits		
	Accuracy	±0.1 mm (foam tolerances are low)		
	Dust Management	Vacuum extraction required		
3-Axis CNC Milling Machine	Axes	X/Y/Z		
	Spindle Speed	8,000–15,000 rpm		
	Spindle Power	1.5–5 kW		
	Tool Capacity	6–10 tool turret		
	Work Envelope	≥ 250 × 250 × 150 mm	9000	Tormach PCNC 440
	Accuracy	Positioning ±0.02 mm, repeatability ±0.01 mm		
	Materials	Aluminium 5052		
	Coolant	Flood coolant or MQL		
	Fixturing	Vise, clamps, soft jaws		
Extrusion Press	Press Tonnage	300–1,000 tons for aluminium 5052 profiles		
	Die Compatibility	Standard extrusion dies, up to 150 mm diameter		
	Output Speed	1–5 m/min		
	Heating	Billet heater: 400–500°C		
	Puller	Automatic profile puller		
				Outsourced to SMS Group

	Cooling	air-cooled table		
Drill	Drill Type	Hand drill		Bosch UniversalImpact 18V
	Diameter Range	2mm and 11.75mm	150	
	Material	Polypropylene		
Reamer	Reamer Type	Hand reamer		Gühring H7
	Diameter Range	12mm	30	
	Material	Polypropylene		
	Tolerance	H7 hole finishes		
Laser Cutter	Laser Type	Fiber Laser (1064nm wavelength)		HPC Minim PRO Fibre Metal Cutter
	Bed Size	$\geq 600 \times 400$ mm		
	Supported Materials	Aluminum 5052	40000	
	Cutting Speed	10–50 mm/s (2mm thickness)		
	Cooling	Integrated water cooling		
	Ventilation	Fume extractor		
	Precision	± 0.1 mm		
Welding Plant	Welding Process	TIG		Stahlwerk AC/DC TIG 200 Puls ST
	Current Range	80–200 A		
	Current Type	AC/DC		
	Torch	Air-cooled torch	500	
	Gas	Argon 99.99%		
	High Frequency Start	Required (clean arc start)		
	Foot Pedal	Recommendation for precision		
	Filler Material	ER5356		
Automated Pick-and-Place Machine	Placement Rate	> 5,000 CPH		NEODEN YY1
	Feeder Count	≥ 30 feeders		
	Component Types	Min 0603 components	3500	
	Vision System	Bottom camera + fiducial alignment		
	Board Size	$\geq 120 \times 150$ mm		
	Accuracy	± 0.05 –0.1 mm		
Reflow Oven	Zones	2–3 heating zones		iTECH RF-A350
	Throughput	> 2 boards/hour	360	
	Max Temp	225–260°C		

	Profile Control	PID-controlled multi-zone ramp/soak/spike		
	Conveyor Type	Mesh or edge-rail		
Hand Soldering Station	Power	60–120 W	200	Weller WE 1010 Löstation
	Temp Range	150–450°C		
	Tips	Variety: conical, chisel, knife		
	ESD Safe	Required		
	Stand & Cleaning	Brass wool + sponge		
	Hot Air Tool	Option for rework		
	Magnifier	3–5× inspection lens or microscope		

16.2.2. Machinery Calculations

Table 32: Machine Efficiencies and Available Time

Machine	OEE	Ideal Machine Availability [minutes/day]	Real Machine availability [minutes/day]	Real Machine availability [minutes/year]
3D Printer	55%	450	247.5	62370
4-Axis CNC Milling Machine	70%	450	315	79380
3-Axis CNC Contour Machine	65%	450	292.5	73710
3-Axis CNC Milling Machine	70%	450	315	79380
Extrusion Press	90%	450	405	102060
Drill	60%	450	270	68040
Reamer	50%	450	225	56700
Laser Cutter	70%	450	315	79380
Welding Plant	50%	450	225	56700
Automated Pick-and-Place Machine	75%	450	337.5	85050
Reflow Oven	85%	450	382.5	96390
Hand Soldering Station	35%	450	157.5	39690

The values of the Overall Equipment Efficiencies (OEE) were selected based on factors such as set-up time and complexity, reliability, performance and operation. The largest factor causing low OEE is manual processes such as drilling, reaming welding and hand soldering.

16.3. Part Production Time

Table 33 shows the estimate production times for each part accounting for both processing time as well as setup. The total production time for each piece was then expanded to get the total production time for the first year.

This table also shows that all parts have a production time much smaller than the calculated Takt Time. However, the sum of all production times (assuming parts manufactured in series) is 1032 min/unit which is larger than the 756 min/unit takt time. This means that parts should be manufactured in parallel.

All calculations can be found in Appendix D: Production Planning Calculations.

Table 33: Production Times per Part

Part	Process(s)	Processing Time [min/unit]	Setup Time [min/unit]	Production Time Per Unit [min/unit]	Production Volume [units/year]	Total Production Time [min/year]
Printed Circuit Board	Etching, Screen printing	102	15	117	150	17550
PCB Mount	3D Printing	193	2	195	150	29250
Battery Cradle	3D Printing	202	5	207	150	31050
Panel Frame	4-axis CNC Milling	30	16	46	150	6900
Load Cell Compartment	3-axis CNC Contour	35	10	45	150	6750
Aluminium Box Foam	3-axis CNC Contour	60	15	75	150	11250
Electronics Basin	Backward Extrusion and 4-axis CNC Milling	74	60	134	150	20100
Aluminium Frame	Fiber Glass Laser cutting and Manual Welding	40	30	70	150	10500
Panel	3-axis CNC Milling	40	25	65	150	9750
Cable Tray	3-axis CNC Milling	20	10	30	150	4500
Top Foam	3-axis CNC Contour	8	5	13	150	1950
Lower Pelican Case	Manual Drilling and Reaming	10	10	20	150	3000
M12 Load Cell Cable	Soldering	10	5	15	150	2250

16.4. Machine Allocation

The number of machines necessary to meet the Production Target can be calculated using Equation (20).

$$No. \text{ of } Machines = \frac{\text{Required Production Time}}{\text{Machine Availability}} \quad (19)$$

To determine the required production time, the production times for relevant parts were summed up. Special care was taken when estimating the required production time for the welding plant, automated pick-and-place machine, reflow oven and hand soldering station as they are used during the assembly process and hence assembly times from Table 35 were included. The results are shown in Table 34.

Table 34: Machine Number Estimation

Machine	Required Production Time [min/year]	Machine Availability [min/year]	No. of Machines
3D Printer	60300	62370	1
4-Axis CNC Milling Machine	24450	79380	1
3-Axis CNC Contour Machine	19950	73710	1
3-Axis CNC Milling Machine	14250	79380	1
Extrusion Press	2550	102060	1
Drill	2100	68040	1
Reamer	2400	56700	1
Laser Cutter	3750	79380	1
Welding Plant	11550	56700	1
Automated Pick-and-Place Machine	1650	85050	1
Reflow Oven	3075	96390	1
Hand Soldering Station	3750	39690	1

16.5. Assembly

16.5.1. Assembly Stations

The product consists of 13 individual make/modify parts and various buy parts. All these must be assembled step by step, in an efficient procedure to keep the cost at a minimum, thus process has been split up into these assembly stations. The assemblies can be seen in more detail in Section 13.3. The timings must be kept underneath the takt time calculated in Section 16.1.4. Some assemblies are interdependent; these dependencies are seen in Figure 84.

Table 35: List of Assembly Stations

Assembly Station	Sub assembly station	Parts assembly	Assembly Process	No. of Machines	Total Time (mins)	Expected Worker
Line 1 – Basin Assembly	Line 1.1 – PCB Assembly (A1)	Part 1 and all electrical components (Table 27, except USB C and M12 port)	Place solder paste using stencil Place all components (Automated pick and place machine) Solder (Reflow oven)	1	50	1
	Line 1.2 – PCB mount assembly (A3)	1, 2, 16 and 22	Screw PCB into Mount	-	1	
	Line 1.3 – Battery Cradle Assembly (A2)	3 and 25	Strap Velcro onto cradle	-	1	
	Line 1.4 – Battery cradle into basin (A6)	2, 7, 17 and 21	Screw the battery cradle in	-	1	
	Line 1.5 – M12 port into basin (A8)	7, 13 and M12 gasket	Insert M12 port into the basin	-	1	
	Line 1.6 – PCB Mount	2, 7 and 27	Tape the PCB mount onto the wall	-	2	

	into basin (A7)					
	Line 1.7 – Frame and gasket onto basin (A9 & A10)	7, 8, Battery, 17, 21, 24 and 26	Place in the battery, then place gasket and screw frame on to the basin	-	2	
Line 2 – Top Panel Assembly	Line 2.1 – Top Panel welding (A4)	9 and 10	Weld cable tray onto top panel	1	14	1
	Line 2.2 – Buttons and ports insertion	SW1, SW2, J2, D2, 9, 18 and 24	Screw the buttons, LEDs and USB A port into the top panel	-	4	
Line 3 – Electronics interior assembly	Line 3.1 – Top panel and basin assembly (A11)	7 and 9	Weld top panel and basin together	1	18	1
	Line 3.2 – Screen insertion (A12)	7, EDPM Foam tape and U12	Insert screen and tape for sealing	-	1	
Line 4 – Panel frame assembly	(A14)	4 and 20	Insert rivets into panel frame	-	3	1
Line 5 – Pelican case assembly	Line 5.1 – USB C port insertion (A13)	J3 and 12	Insert USB – C port	-	1	2
	Line 5.2 – screw in panel frame (A15 & A16)	4, 5, 6, 11, 12 and 19 and glue	Insert foam into case, then screw in panel frame	-	4	
	Line 5.3 – electronics insertion (A17)	7, 12 and O-ring	Screw in electronics with O-ring	-	2	

Line 6 – Final assembly	A18	12 and load cells and cables	Keep the load cells and cables in and close the box	-	2	1
Total time (T_{tot})				107 minutes	-	

Total time is 107 minutes which is much less than the takt time for any year calculated in Section 16.1.4 of minimum 567 minutes/unit. The number of lines required for assembly can also be calculated using formula (20)

$$n_{lines} = \frac{T_{tot}}{T_{takt}} \quad (20)$$

1. Year 1: $0.141 \approx 1$ (rounded up to nearest integer)
2. Year 2: $0.141 \approx 1$ (rounded up to nearest integer)
3. Year 3: $0.189 \approx 1$ (rounded up to nearest integer)

Hence only 1 line is required to meet the target production quantity for all years.

16.5.2. Assembly Line

Below is a flow chart showing the assembly sequence. This flow chart assumes all make, modified and bought parts are available and ready for usage.

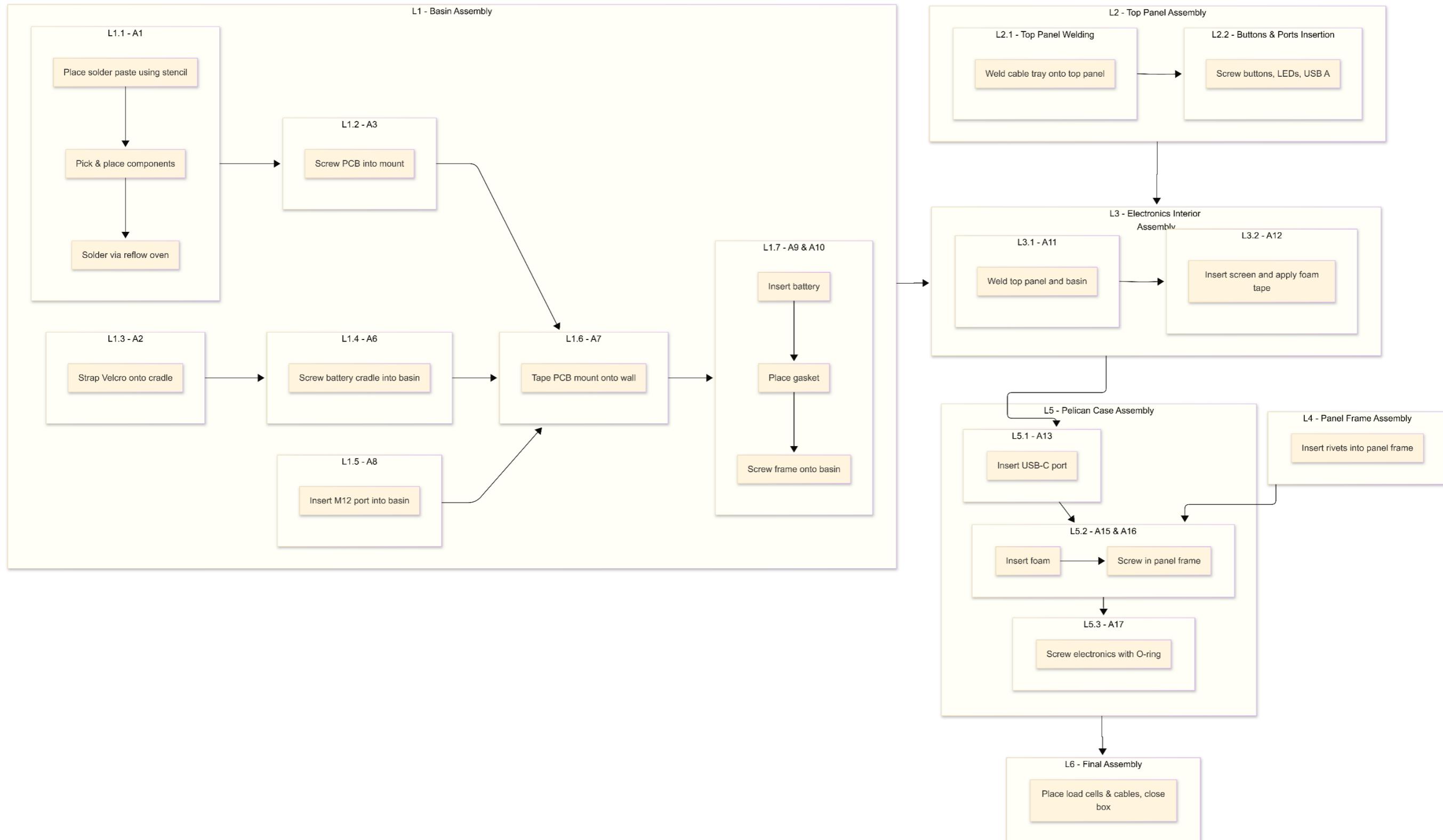


Figure 84: Assembly sequence flowchartThe

16.6. Workforce Requirements

To calculate the number of workers required, the required production times for each machine in the production processes were considered for each day by dividing the values in Table 34 by the number of working days (252). The required number of 7.5hr shifts per day was then estimated by dividing the production time by $7.5h \cdot 60 \frac{min}{h}$. Since each worker can only work one shift a day, a suitable number of workers based on the required shifts was chosen. The results are shown in Table 36. Note that the automated pick-and-place machine and reflow oven are excluded since they are part of the assembly process.

Table 36: Workforce Requirements for Production Processes

Machine	No. of Machines	Required Production Time [min/day]	Required Shifts [shifts/day]	Required Workers
3D Printer	1	239.3	0.532	0.5
4-Axis CNC Milling Machine	1	97.0	0.216	1
3-Axis CNC Contour Machine	1	79.2	0.176	0.5
3-Axis CNC Milling Machine	1	56.5	0.126	0.5
Extrusion Press	1	10.1	0.022	1
Drill	1	8.3	0.019	0.5
Reamer	1	9.5	0.021	0.5
Laser Cutter	1	14.9	0.033	1
Welding Plant	1	45.8	0.102	1
Hand Soldering Station	1	6.5	0.015	0.5

To account for the assembly process, the estimated number of workers from Table 35 were considered. Given the short assembly times and low daily production target, it can be assumed that a single worker can operate the hand soldering station in both production and assembly as well as the automated pick-and-place machine and reflow oven in assembly.

Thus, the total number of workers required is 13.

The number of paid working hours can be calculated using Equation (21).

$$T_{wf} = N_w \cdot D_{year} \cdot N_{shift} \cdot t_{shift} \quad (21)$$

Where T_{wf} is the paid work force time [hours/year], N_w is the number of workers, D_{year} working days in a year [days/year], N_{shift} is the number of shifts in a working day [shifts/day] and t_{shift} is the shift working time [hours/shift]

Therefore, in a given year, there are 24570 paid hours per year.

17. Cost Calculations

17.1. Material Costs

17.2. Labour Costs

17.3. Production Costs

17.4. Overhead

17.4.1. Material

17.4.2. Administrative

17.4.3. Marketing and Sales

17.5. Potential Selling Price

17.5.1. Sales Projection

17.5.2. Profit Projection

17.6. Offer Price

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19. Appendices

19.1. Appendix A: Work Breakdown Structure

WBS Number	Task name	Assigned to	Start	End	Predecessor	Type
1	Concept Design		10/5/2025	10/28/2025		phase
1.1	Project Plan		10/5/2025	10/14/2025		deliverable
1.1.1	Breakdown all deliverables and identify sequence	Justin, Okan, Ahmad, Abhinav, Wasim	10/5/2025	10/9/2025		task
1.1.2	Create Responsibility assignment matrices	Justin	10/9/2025	10/10/2025	1.1.1	task
1.1.3	Draft a schedule	Justin	10/10/2025	10/12/2025	1.1.2	task
1.1.4	Create Gantt chart	Justin	10/12/2025	10/13/2025	1.1.3	task
1.1.5	Approve of Project Plan	Justin, Okan, Ahmad, Abhinav, Wasim	10/13/2025	10/14/2025	1.1.4	task
1.2	Market Analysis		10/13/2025	10/18/2025		deliverable
1.2.1	Perform preliminary Market Analysis	Okan	10/13/2025	10/14/2025	1.1.5	task
1.2.2	Create Financial Estimates	Okan	10/14/2025	10/16/2025	1.2.1	task
1.2.3	Perform Detailed Market Analysis	Okan	10/16/2025	10/17/2025	1.2.2	task
1.2.4	Approve Market Analysis Report	Justin	10/17/2025	10/18/2025	1.2.3	task
1.3	Overall Product Concept		10/13/2025	10/28/2025		deliverable
1.3.1	Creating Requirements List	Ahmad	10/13/2025	10/14/2025	1.1.5	task
1.3.2	Abstract the Problem and Identify Functions	Justin, Ahmad	10/13/2025	10/15/2025	1.3.1	task
1.3.3	Approve Key Functions	Wasim	10/15/2025	10/16/2025	1.3.2	task

1.3.4	Developing Working Structures and Morphological Box	Justin, Ahmad, Abhinav, Wasim	10/15/2025	10/16/2025	1.3.3	task
1.3.4.1	Adjust Solution according to Market Analysis	Ahmad	10/17/2025	10/18/2025	1.2.3, 1.3.4	task
1.3.4.2	Adjust Solution according to FMEA	Wasim	10/25/2025	10/26/2025	1.6.3, 1.3.4	task
1.3.5	Drawing Concept Sketch	Ahmad	10/18/2025	10/22/2025	1.3.4.1	task
1.3.6	Compile preliminary bill of materials	Justin	10/26/2025	10/27/2025	1.3.4.2	task
1.3.7	Approve Overall Product Concept	Wasim	10/27/2025	10/28/2025	1.3.6	task
1.4	Functional Structure		10/18/2025	10/27/2025		deliverable
1.4.1	Create preliminary product FSD	Justin	10/18/2025	10/21/2025	1.3.4.1	task
1.4.2	Adjust FSD according to FMEA	Justin	10/25/2025	10/26/2025	1.6.3	task
1.4.3	Approve product FSD	Abhinav	10/26/2025	10/27/2025	1.4.2	task
1.5	Human Machine Interface		10/21/2025	10/27/2025		deliverable
1.5.1	Create table of I/O Interactions	Abhinav	10/21/2025	10/22/2025	1.4.1	task
1.5.2	Define and Arrange Control Elements	Abhinav	10/22/2025	10/23/2025	1.5.1, 1.3.5	task
1.5.3	Adjust HMI according to FMEA	Abhinav	10/25/2025	10/26/2025	1.6.3	task
1.5.4	Approve HMI	Ahmad	10/26/2025	10/27/2025	1.5.3	task
1.6	D-FMEA		10/22/2025	10/27/2025		deliverable
1.6.1	Create Basis for Failure Analysis	Wasim	10/22/2025	10/23/2025	1.5.2	task
1.6.2	Identify Preliminary Failure Modes	Wasim	10/23/2025	10/24/2025	1.6.1	task
1.6.3	Create Draft of D-FMEA Table	Ahmad, Wasim	10/23/2025	10/24/2025	1.6.2	task
1.6.4	Create Final D-FMEA Report	Justin, Abhinav	10/25/2025	10/26/2025	1.6.3	task

1.6.5	Approve D-FMEA Report	Okan	10/26/2025	10/27/2025	1.6.4	task
1.7	Concept Design Close-out	Justin, Okan, Ahmad, Abhinav, Wasim	10/28/2025	10/28/2025	1.6.5, 1.2.4, 1.5.4, 1.4.3, 1.3.7	milestone
2	Product Design		10/29/2025	12/2/2025		phase
2.1	Complete 3D Model		10/29/2025	12/2/2025		deliverable
2.1.1	Design the Housing and Internal Structure	Ahmad	10/29/2025	11/19/2025	1.7	task
2.1.2	Approve of General Structure	Wasim	11/19/2025	11/20/2025	2.1.1	task
2.1.3	Integrate PCB and Connectors into 3D Model	Ahmad, Wasim	11/20/2025	11/22/2025	2.3.5, 2.1.2	task
2.1.4	Perform Assembly & Interference Check	Ahmad	11/22/2025	11/24/2025	2.1.3	task
2.1.5	Adjust 3D Model based on results of Assembly test	Ahmad	11/24/2025	11/25/2025	2.1.4	task
2.1.6	Assign Material	Ahmad	11/25/2025	11/26/2025	2.1.5	task
2.1.7	Adjust 3D Model According to Manufacturability	Ahmad, Wasim	11/28/2025	11/27/2025	2.1.6, 2.4.3	task
2.1.8	Adjust 3D Model According to Part Availability	Okan, Ahmad	11/29/2025	11/28/2025	2.1.7, 2.5.2	task
2.1.9	Approve 3D Model	Wasim	12/1/2025	12/2/2025	2.1.8	task
2.2	Measurement Chain		10/29/2025	11/11/2025		deliverable
2.2.1	Identify necessary Signal Conditioning	Justin	10/29/2025	10/30/2025	1.7	task
2.2.2	Design Schematics for Signal Condition	Justin	10/30/2025	11/3/2025	2.2.1	task
2.2.3	Adjust Signal Conditioning according to Feedback from Circuit Design	Justin, Wasim	11/6/2025	11/8/2025	2.3.3	task
2.2.4	Create detailed Measurement Chain FSD	Justin	11/8/2025	11/10/2025	2.2.3	task

2.2.5	Approve the Measurement Chain Design	Abhinav	11/10/2025	11/11/2025	2.2.4	task
2.3	Circuit Diagram		10/29/2025	12/2/2025		deliverable
2.3.1	Draw Electrical System Block Diagram	Wasim	10/29/2025	10/31/2025	1.7	task
2.3.2	Create Draft Circuit Schematic	Wasim	10/31/2025	11/4/2025	2.3.1	task
2.3.3	Integrate Signal Processing Schematics	Justin, Wasim	11/4/2025	11/6/2025	2.3.2, 2.2.2	task
2.3.4	Design Detailed Circuit Schematic	Abhinav, Wasim	11/6/2025	11/11/2025	2.3.3	task
2.3.5	Design PCB	Abhinav, Wasim	11/11/2025	11/19/2025	2.3.4, 2.2.3	task
2.3.6	Perform Electrical Safety Checks	Wasim	11/19/2025	11/21/2025	2.3.5	task
2.3.7	Adjust PCB according to Manufacturability	Wasim	11/27/2025	11/28/2025	2.4.3, 2.3.6	task
2.3.8	Adjust PCB according to Availability	Wasim	11/28/2025	11/29/2025	2.5.2	task
2.3.9	Create Final Electrical Documentation Package	Wasim	11/29/2025	12/1/2025	2.3.7, 2.3.8	task
2.3.10	Approve Final Circuit Diagram	Justin	12/1/2025	12/2/2025	2.3.9, 2.2.5	task
2.4	Technology Selection for “Make” Parts		11/21/2025	12/2/2025		deliverable
2.4.1	Identify all necessary “make” parts	Justin	11/21/2025	11/22/2025	2.3.5, 2.1.3	task
2.4.2	Approve list of “Make” + “Buy” parts	Okan	11/23/2025	11/24/2025	2.4.1, 2.5.1	task
2.4.3	Assess Manufacturability of Parts	Wasim	11/24/2025	11/27/2025	2.4.2	task
2.4.4	Select Manufacturing Process and Materials for each part	Wasim	11/26/2025	11/27/2025	2.4.3	task
2.4.5	Approve of material and manufacturing	Justin	11/27/2025	11/28/2025	2.4.4	task

	processes of “make” parts					
2.4.6	Define the Assembly Technology (Area by Area)	Justin, Wasim	11/28/2025	12/1/2025	2.4.5	task
2.4.7	Approve Manufacturing and Assembly Guide Package	Okan	12/1/2025	12/2/2025	2.4.6	task
2.5	Requirements Manual for “Buy” Parts		11/21/2025	12/2/2025		deliverable
2.5.1	Identify all necessary “buy” parts	Okan	11/21/2025	11/22/2025	2.1.3, 2.3.5	task
2.5.2	Assess availability of "buy" Parts	Okan	11/24/2025	11/27/2025	2.4.2	task
2.5.3	Create part requirements sheets for each “buy” part	Okan, Ahmad	11/27/2025	12/1/2025	2.5.2	task
2.5.4	Approve requirement sheets	Justin	12/1/2025	12/2/2025	2.5.3	task
2.6	Product Design Close-out	Justin, Okan, Ahmad, Abhinav, Wasim	12/2/2025	12/2/2025	2.5.4, 2.4.7, 2.3.10, 2.1.9	milestone
3	Project Documentation		10/29/2025	1/12/2026		phase
3.1	Technical Drawings for Main Assembly		12/3/2025	1/4/2026		deliverable
3.1.1	Create Assembly Drawing with Section and Detail Views	Ahmad	12/3/2025	12/17/2025	2.6	task
3.1.2	Verify drawings for electrical components	Wasim	12/17/2025	12/19/2025	3.1.1, 3.4.3	task
3.1.3	Verify Compliance with DIN 406 Drawing Standards	Abhinav	12/20/2025	12/22/2025	3.1.2	task
3.1.4	Approval of technical drawing	Wasim	1/3/2026	1/4/2026	3.1.3	task
3.2	Program Flow Chart		12/3/2025	12/18/2025		deliverable
3.2.1	Draw Main structural flowchart	Abhinav	12/3/2025	12/7/2025	2.6	task

3.2.2	Draw User interaction flowchart	Abhinav	12/7/2025	12/9/2025	3.2.1	task
3.2.3	Draw Calibration menu flowchart	Abhinav	12/8/2025	12/10/2025	3.2.2	task
3.2.4	Draw Data handling flowchart	Abhinav	12/10/2025	12/11/2025	3.2.3	task
3.2.5	Draw Error and Internal Interrupt handling flowchart	Abhinav	12/11/2025	12/12/2025	3.2.4	task
3.2.6	Approve program flowcharts	Ahmad	12/19/2025	12/18/2025	3.2.5	task
3.3	Bill of Material		12/3/2025	1/4/2026		deliverable
3.3.1	Create master BOM spreadsheet	Justin	12/3/2025	12/4/2025	2.6	task
3.3.2	Itemize all Mechanical Components		12/4/2025	12/10/2025		tasks group
3.3.2.1	Identify norm spec for each standard mechanical component	Justin	12/4/2025	12/7/2025	3.3.1	task
3.3.2.2	Verify all specifications of all mechanical components	Wasim	12/7/2025	12/10/2025	3.3.2.1	task
3.3.3	Itemize all Electrical Components		12/10/2025	12/16/2025		tasks group
3.3.3.1	Add technical specs for all electrical components	Justin	12/10/2025	12/13/2025	3.3.2.2	task
3.3.3.2	Verify all specifications of all electrical components	Ahmad	12/13/2025	12/16/2025	3.3.3.1	task
3.3.4	Add cost to all components	Justin	12/16/2025	12/19/2025	3.3.3.2	task
3.3.5	Verify Part Numbers according to Drawings	Justin	12/20/2025	12/22/2025	3.1.2	task
3.3.6	Approve final BOM	Abhinav	1/3/2026	1/4/2026	3.3.5	task
3.4	Production Planning		12/3/2025	1/8/2026		deliverable
3.4.1	Estimate Number of Required Machines	Wasim	12/3/2025	12/5/2025	2.6	task

3.4.2	Estimate Manufacturing and Assembly Time per Part	Wasim	12/5/2025	12/11/2025	3.4.1	task
3.4.3	Create Assembly Sequence and Flowchart	Abhinav, Wasim	12/11/2025	12/15/2025	3.4.2	task
3.4.4	Estimate Workforce Requirements	Wasim	12/15/2025	12/17/2025	3.4.3	task
3.4.5	Optimize Assembly Sequence Costs	Abhinav, Wasim	12/20/2025	12/23/2025	3.5.3	task
3.4.6	Approve of Assembly Sequence and Flowchart	Justin	1/3/2026	1/4/2026	3.4.5	task
3.4.7	Create Production Planning Summary	Wasim	1/4/2026	1/7/2026	3.4.6	task
3.4.8	Approve Production Plan	Okan	1/7/2026	1/8/2026	3.4.7	task
3.5	Cost Calculation		12/5/2025	1/6/2026		deliverable
3.5.1	Estimate Fixed Costs	Okan	12/5/2025	12/11/2025	3.4.1	task
3.5.2	Estimate Variable Costs		12/11/2025	12/16/2025	3.5.1	tasks group
3.5.2.1	Perform Initial Variable Cost Estimation	Okan	12/11/2025	12/16/2025	3.4.2	task
3.5.2.2	Perform Final Variable Cost Estimate	Okan	12/19/2025	12/22/2025	3.5.2.1, 3.4.4, 3.3.4	task
3.5.3	Estimate Overheads and Miscellaneous	Okan	12/16/2025	12/19/2025	3.5.2.1	task
3.5.4	Summary Costs and Revenue Projection	Okan	1/3/2026	1/5/2026	3.5.2.2, 3.5.3	task
3.5.5	Approve Cost Calculation Report	Justin	1/5/2026	1/6/2026	3.5.4	task
3.6	Specification sheet		10/29/2025	1/4/2026		deliverable
3.6.1	Outline Functional specifications	Abhinav	10/29/2025	10/31/2025	1.7	task
3.6.2	Outline Physical and Mechanical Specifications	Ahmad, Abhinav	11/20/2025	11/22/2025	2.1.2, 3.6.1	task

3.6.3	Outline Electrical Specifications	Abhinav, Wasim	11/23/2025	11/27/2025		task
3.6.4	Adjust Specification on Final Design	Abhinav	12/12/2025	12/17/2025	3.6.3, 3.6.2, 2.6	task
3.6.5	Approve specifications sheet	Justin	1/3/2026	1/4/2026	3.6.4	task
3.7	User manual		11/21/2025	1/4/2026		deliverable
3.7.1	Write Safety Disclaimers	Justin	11/21/2025	11/23/2025	2.3.6	task
3.7.2	Write Functional Instructions	Okan	12/10/2025	12/15/2025	3.2.2, 3.7.1	task
3.7.3	Explain troubleshooting steps	Abhinav	12/17/2025	12/23/2025	3.7.2	task
3.7.4	Approve user manual	Ahmad	1/3/2026	1/4/2026	3.7.3	task
3.8	Interactive brochure		11/11/2025	1/12/2026		deliverable
3.8.1	Create first draft of Brochure	Justin, Ahmad, Abhinav	11/11/2025	12/1/2025	1.7	task
3.8.2	Create Interactive Media for brochure	Justin, Ahmad, Abhinav	12/17/2025	12/22/2025	3.8.1, 2.1.9	task
3.8.3	Design Final Brochure	Justin, Ahmad, Abhinav	1/4/2026	1/11/2026	3.8.2	task
3.8.4	Approve brochure	Okan, Wasim	1/11/2026	1/12/2026	3.8.3	task
3.9	Project Documentation Closeout	Justin, Okan, Ahmad, Abhinav, Wasim	1/12/2026	1/12/2026	3.1.4, 3.5.5, 3.4.8, 3.3.6, 3.6.5, 3.7.4, 3.8.4, 3.2.6	milestone
4	Project Close-out	Justin, Okan, Ahmad, Abhinav, Wasim	1/13/2026	1/13/2026	3.9	milestone

19.2. Appendix B: Preliminary Battery Life Calculations

Assumed current draw rates:

- Microcontroller: 200 mA
- Signal Conditioning Circuit: 10 mA
- ADC: 5 mA
- Display: 150 mA
- Peripherals: 5 mA
- USB: 2.5 mA (suspended) or 500 mA (data transfer)

Assumed operating times:

- USB Data Transfer: 5s
- Working Period: 8h

Additional assumptions:

- Safety Factor: 1.2
- Number of USB Transfers in a Working Period: 4

Within a single working period, the average USB data transfer current:

$$I_{USB}^{avg} = 500mA \cdot \frac{5s}{8h \cdot 3600 \frac{s}{h}} \cdot 4 = 0.347mA$$

The total average current in a working period:

$$\begin{aligned} I^{avg} &= 200mA + 10mA + 5mA + 150mA + 5mA + 2.5mA + 0.347mA \\ &= 372.847mA \end{aligned}$$

Hence, the expected battery life:

$$T_{dur} = \frac{5000mAh}{372.847mA \cdot 1.2} = 11.175h$$

19.3. Appendix C: Dimensioning of Measurement Chain

19.3.1. Low Pass RC Filters

Firstly, we consider the filter at the inputs of the INA. Using AD8421, we dimension the resistors first based on the bias error at the inputs. The AD8421 has maximum bias current of 500pA. So, designing for a maximum error of 0.1mV.

$$R \leq \frac{V_{bias}}{I_{bias}} = \frac{0.1 \cdot 10^{-3}V}{500 \cdot 10^{-9}mA} = 200k\Omega$$

This gives a large range for R, but to keep thermal noise low we use $R = 10k\Omega$.

Designing for $f = 5Hz$:

$$C = \frac{1}{2\pi \cdot (2R) \cdot f_c} = \frac{1}{2\pi \cdot 20k\Omega \cdot 5Hz} \approx 1.59\mu F$$

We must use $2R$ since the filter is symmetric.

We select a standard capacitor such that $C = 1.5\mu F$ with $0.1\mu F$ for decoupling.

With this set up we get the following results:

- Corner frequency: $f_c = 4.97Hz$
- Bias Error: $V_{bias} = 0.005 mV$
- Settling Time: $\tau = 32ms$

Next, the filter between the INA and VGA. The OPA188 has a max bias current of 18nA.

$$R \leq \frac{V_{bias}}{I_{bias}} = \frac{0.1 \cdot 10^{-3}V}{18 \cdot 10^{-9}mA} = 5.55k\Omega$$

Hence, using $R = 4.7k\Omega$ and designing for $f_c = 8Hz$,

$$C = \frac{1}{2\pi \cdot R \cdot f_c} = \frac{1}{2\pi \cdot 4.7k\Omega \cdot 8Hz} \approx 4.233\mu F$$

Hence, we select $C = 4.7\mu F$.

With this set up we get the following results:

- Corner frequency: $f_c = 7.20Hz$
- Bias Error: $V_{bias} = 0.0846 mV$
- Settling Time: $\tau = 22ms$

Finally, the filter before the ADC. For this filter, we primarily aim to reduce the device noise, so a corner frequency of 20Hz is chosen and since the bias error is a minor component here, we just choose a $10k\Omega$ resistor.

$$C = \frac{1}{2\pi \cdot R \cdot f_c} = \frac{1}{2\pi \cdot 10k\Omega \cdot 20Hz} \approx 0.796\mu F$$

So, we can use $0.33\mu F$ and $0.47\mu F$ in parallel.

With this set up we get the following results:

- Corner frequency: $f_c = 19.89Hz$
- Settling Time: $\tau = 8ms$

19.3.2. Amplification Gain

Ensuring each load cell could be amplified to meet its specific sensitivity was a bit of a challenge. At first, just the INA was used, and the gain set resistor was dimensioned to the average of the required gains. But this yielded large gain errors of up to 17.5%. So, an approach was taken from Analog Devices (2017, February) where a VGA could be designed with an Op-Amp and a digital potentiometer to allow for continuous gain control.

Firstly, the INA was dimensioned to have gain of 100 so that it provides most of the amplification. Using the AD8421, the gain resistor is calculated using the formula:

$$R_G = \frac{9.9k\Omega}{G - 1}$$

Hence for a gain of 100, we get $R_G = 100\Omega$.

Then to dimension the resistance for each load cell, an excel spreadsheet was used to calculate the required gain, remaining gain after pre-amplification, the required VGA resistance (R_F), the required step on the digital potentiometer (D), the rounded step, the actual VGA gain and the gain error. The VGA setup uses a $4.99k\Omega$ resistor and the equations as described in 9.3.4 were used. The excel spreadsheet can be found here:

These calculations are in the sheet titled “Gain INA + VGA”.

19.4. Appendix D: Production Planning Calculations

All calculations for 16. Production Planning were done in the attached spreadsheet titled ‘Group 02_WS_25-26 M3 Production Planning’.

Statement of Originality

We hereby declare that this report and its contents were written, created and designed by the members of Group Project WS25/26 Group 02 as listed below. All sources of information utilised in the making of this report are referenced in Section 7. Bibliography. Any special tools used in the making of this report are referenced in the footnotes in the section in which they have been used.

Kleve, 28.10.25

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