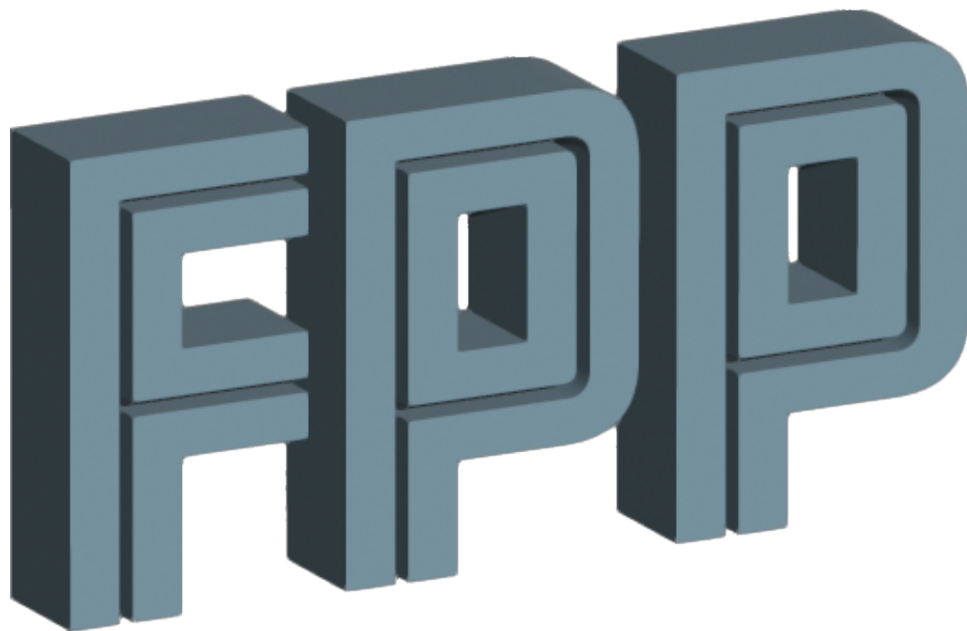


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# Fully Polymorphic Package Manual

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# 1 Introduction to packages within FPP/PTC

The name PTC is commonly used to designate a code written by Etienne Forest with the help of Frank Schmidt and later David Sagan. PTC is an object oriented, open source, subroutine library for

- The manipulation and analysis of Taylor series and Taylor maps.
- Modeling of charged particle beams in accelerators using Taylor maps.

The popularity of PTC can be attested to by its use with the Bmad[16] toolkit for accelerator and X-ray simulations as well as its use within the MAD[11] simulation program.

PTC is linked with the overloaded Truncated Power Series Algebra (TPSA) package of Martin Berz. Berz's package is called **Polymorphic Package** (PP). By virtue of using the polymorphic package and by virtue of being able to do tracking, PTC stands for "Polymorphic Tracking Code". PTC can be decomposed into two parts:

1. The Fully Polymorphic Package (FPP) part handles Taylor series. FPP is pure mathematics detached from any "physics".
2. The Tracking Code (TC) part is where the physics of PTC is located. It is simply an integrator pushing the phase space and spin of particles through magnets. TC relies on FPP for handling Taylor series. In particular, via the magic of FPP (specifically the magic of PP), a Taylor map can be produced if wanted when tracking with TC.

FPP is the subject of this manual. FPP itself can be subdivided into two parts:

1. The "Polymorphic Package" (the PP of FPP) deals with the production of Taylor series.
2. The Analysis Package (AP) analyses physically sensible Taylor maps: Taylor maps that approximate the tracking of the code. Spin and magnet modulation can also be analyzed.

To appreciate the role of PP, we can show a tiny piece of code TC representing a drift.

```
      .  
      .  
      .  
      TYPE (REAL_8), INTENT (INOUT):: X (6)  
      TYPE (REAL_8), INTENT (IN):: L  
      .  
      .  
      .  
      PZ=SQRT (1.0_dp+2.0_dp*X (5) /b+x (5)**2 - X (2)**2 - X (4)**2)  
      X (1)=X (1)+L*X (2) /PZ  
      X (3)=X (3)+L*X (4) /PZ
```

For completeness, here is type **real\_8**:

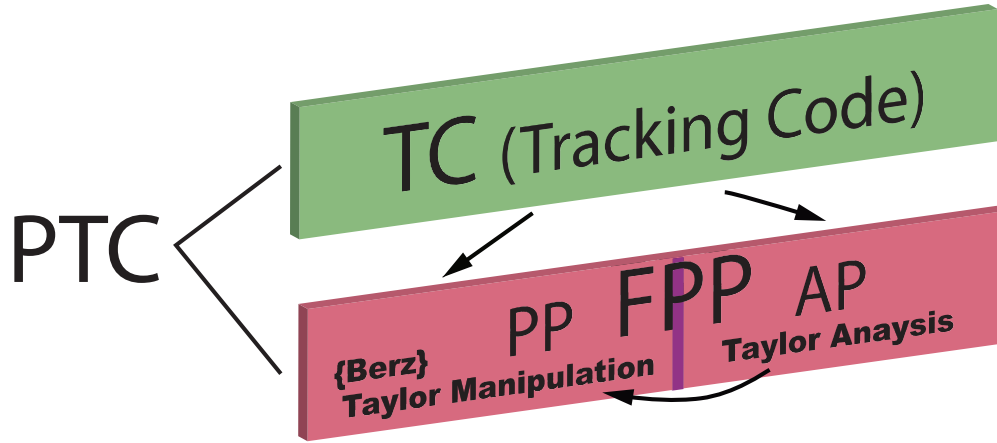


Figure 1: The Fully Polymorphic Package (FPP) part of the FPP/PTC library provides manipulation and analysis of Taylor series and maps and the Tracking Code (TC) part contains the physics of the accelerators. Arrows indicate code dependencies. The Taylor analysis code uses the Taylor manipulation code but not vice versa. FPP does not use PTC but PTC code uses both FPP's Taylor manipulation and potentially analysis as the red arrow indicates.

```

TYPE REAL_8
  TYPE (TAYLOR) T      ! USED IF TAYLOR
  REAL(DP) R           ! USED IF REAL
  INTEGER KIND ! 0,1,2,3 (1=REAL,2=TAYLOR,3=TAYLOR KNOB, 0=SPECIAL)
  INTEGER I ! USED FOR KNOBS AND SPECIAL KIND=0
  REAL(DP) S ! SCALING FOR KNOBS AND SPECIAL KIND=0
  LOGICAL(lp) :: ALLOC ! IF TAYLOR IS ALLOCATED IN DA-PACKAGE
END TYPE REAL_8

```

In the above definition, we see **real\_8%t** and **real\_8%r**. They are respectively the Taylor and double precision entries of the polymorph. If the polymorph must for some reason become a Taylor series, then its value is stored in **%t**, otherwise it is stored in **%r**. A **real\_8** can also be a “knob”: this is described in section (§12.2).

If type **REAL\_8** was simply **real(8)**, then this code fragment would simply be the exact formula for a drift in canonical variables. However **REAL\_8** can become a Taylor series in certain chosen variables at execution time and thus Taylor series can be produced. The actual package that does the Taylor calculation is the package of Martin Berz[2], namely the old version from LBNL properly modified by Johan Bengtson and overloaded by Etienne Forest using Fortran90.

This manual is focused on how to use FPP. Since FPP is designed to serve PTC or a code like PTC, there will be some mention of PTC but only so far as how PTC relates to FPP. In particular, tracking through lattices is not discussed and the reader is referred to the PTC documentation for this.

The red arrow in Figure 1 refers to a potential dependency. PTC can dump on files Taylor series which can be analyzed or tracked by another code. Conversely, PTC (via FPP), can read maps

---

produced by other codes and track them. For example, a person might have a COSY-INFINITY version of a damping ring and the subsequent injection line. The Taylor map describing this structure can be an input to PTC in the absence of a PTC lattice for this structure: this is equivalent to inputting linear uncoupled lattice functions in a regular code but much more general.

In fact most analysis in PTC is done by people (including the authors) who write independent modules for generalized Twiss calculations. This will be illustrated later and is the main topic of reference [7].

The FPP package can be used with any tracking code including TC. Indeed one can write an integrator in Fortran90 using the polymorphic types of FPP for the production and analysis of Taylor maps: Forest has written many such examples in lectures.

## 2 Where to Obtain FPP/PTC

FPP/PTC can be downloaded from the web via the Bmad web site[16] or at

```
https://github.com/jceepf/fpp\_book
```

Taylor manipulation routines are contained in the following code files:

```
a_scratch_size.f90      j_tpsalie.f90
b_da_arrays_all.f90     k_tpsalie_analysis.f90
b_da_arrays_all_pancake.f90 l_complex_taylor.f90
c_dabnew.f90            m_real_polymorph.f90
c_dabnew_pancake.f90    n_complex_polymorph.f90
d_lielib.f90            o_tree_element.f90
h_definition.f90        Sa_extend_poly.f90
i_tpsa.f90
```

Taylor analysis routines are contained in the following code files

```
cb_da_arrays_all.f90    Ci_tpsa.f90
cc_dabnew.f90           Su_duan_zhe_map.f90
```

The library

```
Su_duan_zhe_map.f90
```

can actually be used separately. It allows for tracking using Taylor maps: remember that PTC proper (TC) does not use Taylor maps for tracking, it is a “kick code” or integrator.

## 3 Concepts: why we need TPSA?

The purpose of this section is to explain why we would like to write an integrator equipped with polymorphism. Of course the purpose exists before the code and, for the most part, is not the result of “Darwinian evolution”.

---

It is true from a goal driven point of view (teleological) that PTC was created with the production of Taylor maps of phase space in mind. This is simply because Forest is convinced, see references [6] and [7], that an analytical theory primarily based on finite “s” maps is superior than a theory primarily based on the s-dependent Hamiltonian of the Courant-Snyder theory in the context of accelerators. This s-dependent Hamiltonian is far from the code and thus not adequate as the primary theory for most applications.

But can we guess from TC’s structure, the tracking part, that PTC prioritizes a map-based theory for analysis? The answer as we will see is :no.

There are two options if we have Taylor maps in mind:

1. We can write a beam line code whose goal is the production of Taylor series approximate maps around some chosen orbit and whose internal structure reflects this goal. The prime representative of such codes is COSY-INFINITY[14, 13]. This is also true of MARYLIE, TRANSPORT[4] and the Twiss modules part of MAD8 ported into MAD-X. All these codes choose a “design” orbit and then compute Taylor maps around this orbit. If a user examine these codes, especially TRANSPORT, Taylor series maps will jump in their faces: arrays of monomial coefficients for each phase space variables are defined and they contain increasingly complex formulae as the degree increases. The TRANSPORT approach reached a grotesque end point with the code COSY 5.0<sup>1</sup> of Berz : Fortran formulae at the fifth order Taylor coefficients covered pages of computer generated algebra.
2. Forest, following mainly the philosophy of Talman, prefers the usage of integrators, in particular, symplectic integrator in the simulations of LINACs, recirculators and rings. (See Forest’s review article [8] for a comprehensive opinionated description of this topic.) As a result, and irrespective of teleological consideration i.e., wanting Taylor maps for analysis–Twiss, etc. . . , TC is a (mostly symplectic) integrator whose main purpose is the tracking of rays. It is only via polymorphism that this integrator can, under some very specific conditions, produce a Taylor map which approximates the phase space maps produced by the likes of COSY-INFINITY or MARYLIE.

In fact Forest produced a “kick code”. Imagine if the type **real\_8** was a Fortran90 intrinsic. Anyone could write a kick code using the floating point **real(8)**. The fact that same person could recompile the code using **real\_8** would not automatically elevate the code to a code which produces sensible phase space maps. COSY-INFINITY, MARYLIE or TRANSPORT on the other hand always produce sensible maps when applied to magnets: this is their end purpose and their internal structure can be guessed from their purpose.

Looking internally at TC, it is not possible to see any maps<sup>2</sup>: only tracking of **real\_8** completely mimicking the tracking of **real(8)**.

Therefore it is not mathematically true that PTC produces “Taylor maps” despite Forest’s motives. Sometimes PTC produces Taylor series and it is not clear to the author of PTC (Forest)

---

<sup>1</sup>This is not to be confused with COSY-INFINITY which uses Berz’s TPSA package. COSY 5.0[3] was really the end of the dinosaur line of TRANSPORT like codes. It is mercifully extinct.

<sup>2</sup>A now retired CERN scientist exclaimed upon looking in the guts of PTC: “where are the beta functions?” The reader should understand upon reading this manual that this question is ridiculous: they are nowhere. PTC is unaware of them even when it tracks them! This is the central topic of reference [7].

---

what kind of maps should be created. An example of this is provided in sections (§7.2) and (§7.3): from the Taylors series produced by PTC we construct a contracting map to be used in a Newton search. In that case, the user must write the interface since no one can guess *a priori* what the user has in mind.

We will see that PTC provides an interface between TC and AP which privileges the production of phase space maps so that the users can *de facto* state that for the most part PTC facilitates the production of Taylor maps related to phase space via the derived type **real\_8**. But this is not visible in TC proper and is only true because Forest has programmed a very specific interface between polymorphs and Taylor maps. He could have left that task to the user (Bmad and MAD-X programmers) but they would have complained. Forest himself as the prime user would have complained schizophrenically to himself.

In the rest of this section we explain TC's interaction with FPP. It is thus necessary to introduce certain concepts in very broad terms. Since PTC is an existing code, we can use its existing structures to describe the general approach. Someone else, writing in a different language would most likely be tempted to use similar concepts and perhaps do a better job.

After general considerations to set the tone and provide some context, we will examine 3 cases in section (§5.3):

1. In section (§7.1), we extract a phase space map. We use special constructs and routines that facilitates this for the user. Namely they connect TC to AP. In AP, normal forms for example have very special assumptions : they deal with linearly stable spin-orbit maps for example.
2. In sections (§7.2) and (§7.3), we create a contraction map that fits the output of TC that has no connection with accelerator theory proper. FPP is used directly without the interface to AP. This program can be understood without the slightest understanding of TC and what it allegedly computes.
3. In section (§7.4), we fit the orbit (as in item 2) and the tunes/phase-slip. This is a typical accelerator physics case. We create the usual one-turn maps as well as the Langrangian contraction maps of item 2.

### 3.1 Conventions

FPP/PTC is written in Fortran90. It is assumed that the reader has some familiarity with this language. In particular, it is assumed that the reader knows what a **structure** is (roughly corresponding to a **class** in Python or C++) which is also called a **derived type**. Additionally it is assumed that the reader knows about operator overloading.

FPP/PTC uses double precision numbers. The kind type parameter “**dp**” is defined in FPP/PTC to correspond to double precision numbers. For example:

```
real(dp) abc, xyz      ! Declare double precision vars abc and xyz.
xyz = 3.4_dp * abc / 1e9_dp ! 3.4_dp and 1e9_dp are double precision.
```

In this manual, **real(dp)** is often written as **real(8)** in case the meaning of **dp** is forgotten. However **dp** could be **16** if quadruple precision is used.



## 4 Tables with examples

### 4.1 Some useful operators on Taylor series

This section contains simple operations which are useful mainly to programmers using FPP.

It must be remarked that the integral operator `.i.` loses one order in the Taylor series. It is better to use the `c_universal_taylor` if integrals are needed to obtain Poisson bracket operators.

	Description (t: c_taylor)	Fortran Operator
1	Real and imaginary part of c_taylor	t=real(t) and t=aimag(t)
2	Extract the coefficient of $x_i$ (constructing matrices)	r=t.index.i
3	$\frac{dt}{dx_i}$ and $\int t dx_i$	t=t.d.i and t=t.i.i
4	Extract order "i"	t=t.sub.i
5	Truncates above "i"	m=m.cut.i
6	Extracts coefficient $r$ of monomials $x_1^{j_1} \dots x_1^{j_{nv}}$	r=t.sub.j or r=t.sub.'j1...jn'
7	$t=a + b x_i$ where $a$ and $b$ are real or complex	t=a+b dz_c(i)
8	Create Monomials $r x_1^{j_1} \dots x_1^{j_{nv}}$ $r x_1^{j_1} \dots x_1^{j_{nv}}$ $r x_i$	t = r.cmono.j(1 : nv) t = r.cmono.'j1...jnv' t = r.cmono.i
9	Peek coefficient $t$ , as a c_taylor, of monomial $x_1^{j_1} \dots x_n^{j_n}$	t = r.par.j(1 : nv) t = r.par.'j1...jn'
10	Generalization of .par. using a type called sub_taylor (inf)	t=r.par.inf or t=r.part.inf
11	Shift exponents downwards by k	t=t<=k
12	Peek and shift (operators 9 and 11 combined)	t=t<=k
13	Pseudo derivative : $d(x_i^n) = x_i^{n-1}$	t=t.k.i
14	Poisson Bracket	t=t.pb.t'

## 4.2 Table of useful operators on **c\_damap** and **c\_vector\_field**

	Description (M,A: <b>c_damap</b> and F,F': <b>c_vector_field</b> $F \cdot \nabla$ )	Fortran Operator
1	Extract order "i"	<b>M=M.sub.i</b>
2	Truncates above "i"	<b>M=M.cut.i</b>
3	Extracts order "i"	<b>F=F.sub.i</b>
4	Truncates above "i"	<b>F=F.cut.i</b>
5	Exponenting a vector field	<b>M=exp(F,M)</b> or <b>M=exp(F)</b>
6	Logarithm of a map (look at link for optional variables)	<b>F=ln(M)</b>
7	$\mathcal{A} \left( F \cdot \nabla + \hat{f} \right) \mathcal{A}^{-1} = \tilde{F} \cdot \nabla + \hat{\tilde{f}}$ $\mathcal{A} = \exp (F_a \cdot \nabla + q_a)$ $\tilde{F}_k = \left( F_i \partial_i a_k^{-1} \right) \circ a$ $\tilde{f} = \left( \tilde{F}_k \partial_k \alpha^{-1} \right) \alpha + \alpha^{-1} f \circ a \alpha$ $a \text{ is the orbital map and } \alpha \text{ is the quaternion}$	<b>F=A*F</b>
8	If $\mathcal{A} = \exp(F' \cdot \nabla)$ in item 7	<b>F=exp_ad( F',F)</b>
9	Lie Bracket: exp_ad reprogrammed with .lb.	<b>F=F.lb.F</b>
10	Tpsa and DA concatenation of <b>c_damap</b> 's and powers (see §6)	$M = A.o.M, M = M.o.o.(n)$ $M = A.*.M, M = M.*.*(n)$
11	$M+M', M-M', r*M$ (r is real or complex)	<b>M=A*M</b> and <b>M=M**(n)</b>

## 4.3 Table on the permanent storage type **c\_universal\_taylor**

A taylor series produced by TC or a map analysed by FPP depends on the two versions of the TPSA package of Berz. One version deals intrinsically with real Taylor: this is **c\_dabnew.f90**. It is the package on which the polymorphs are used and therefore used by the code TC. A complex taylor does exist but simply made of two real taylor

```

type complextaylor
  type (taylor) r ! Real part
  type (taylor) i ! Imaginary part
end type complextaylor

```

and similarly a complex polymorph exists and it is used in TC and it uses the above **complextaylor**:

```

type complex_8
  type (complextaylor) t
  complex(dp) r
  logical(lp) alloc
  integer kind
  integer i,j
  complex(dp) s
end type complex_8

```

The other package, **cc\_dabnew.f90** is a version of Berz package which is intrisically complex. It is used in the analysis part of FPP namely **Ci\_tpsa.f90**. During a run of PTC or worse BMAD, we would like to store permanently some Taylor series. This is not possible via Berz's package since they function with a given order and number of variables. For that purpose BMAD uses a type **universal\_taylor** and AP uses the complex equivalent **c\_universal\_taylor**. Since this manual is about analysis — not BMAD— we describe the **c\_universal\_taylor** via examples in a table.

	(t,f: c_taylor, M,A: c_damap and F,F': c_vector_field, uf,uf1: c_universal_taylor )	Fortran Operator
1	Simple operations illustrated via a one-resoance normal form	<b>.sub.</b> and <b>.par. .d.</b>
2	Multiplicity of logarithms of maps and universal taylors for Poisson brackets	<b>get_field_c_universal_taylor(vf,uf1)</b>
3	Evaluation via <b>.o.</b> on <b>c_universal_taylor(:)</b>	<b>uf.o.c_ray</b> and <b>uf(:).o.c_ray</b>

In item **2**, we compute the logarithm of map two different ways: via **ln(c\_damap)** and normal form. The logarithm can only be used on map near the identity. Via the normal form, it is easy to generate an infinite number of logarithms for maps far from the identity by simply adding integer units of tune to the linear tune.

In item **3**, we substitute a type **c\_ray** into a inversal taylor or an array. An array can represent a map for example: not fast by very convenient. The type **c\_ray** is:

```

type c_ray
  complex(dp) x(lnv)           ! orbital and/or PTC magnet modulation clocks
  type(complex_quaternion) q   ! quaternion
  integer n                     ! of dimensions used in x(lnv)
!  Obsolescent
  complex(dp) s1(3),s2(3),s3(3) !# 3 spin directions
end type c_ray

```

If a **c\_ray** is used with a **c\_damap**, the quaternion array will be filled with the resulting quaternion.

## 4.4 Table of important routines related to Normal Forms (Twiss)

---

```

type c_factored_lie
integer :: n = 0
integer :: dir= 0
type (c_vector_field), pointer :: f(:)=>null()
end type c_factored_lie

```

This type is used in normal forms since the (reverse)-Dragt-Finn representation is natural and this useful. This is not found in the early papers of Hori[10, 9] or Deprit[5].

	(t,f: c_taylor, M,A: c_damap and F,F': c_vector_field, df :Dragt-Finn )	Fortran Operator
1	Factored Lie from a Normal Form	<code>a=exp(normal%g)</code>
2	Factorization: canonizing and factoring: averages as example	<code>c_full_factorise</code> and <code>c_full_canonise</code>
3	Linear twiss and nonlinear twiss	<code>c_fast_canonise</code> and <code>c_full_canonise</code>
4	Linear twiss and nonlinear twiss : coasting beam example	<code>c_fast_canonise</code> and <code>c_canonise/c_full_canonise</code>
5	Teng-Edwards via de Moivre	<code>call teng_edwards_a1(a1,R,C,COSLIKE,t_e)</code>

In item 1, we use the example of a normal form:

$$\mathcal{R} = \underbrace{C^{-1} \overbrace{\exp(q)}^{\text{Spin}} \overbrace{\exp(\hat{F}^{No}) \cdots \exp(\hat{F}^2)}^{\text{Factored } n\%g}}_A \mathcal{C} \mathcal{A}_1 \mathcal{A}_0 M \mathcal{A}^{-1} \quad (1)$$

where

$$\hat{F}^i = F^i \cdot \nabla \quad (2)$$

$\mathcal{A}_0$  is the transformation to the fixed point and  $\mathcal{A}_1$  is the linear transformation. Notice that the vector fields of the factored product do not contain any quaternion operator. This is because the orbital normalization is done first. The spin transformation is done later and here it is represented by  $\exp(q)$ .

In item 2, we simply factorized the map  $A$ . In the case of `c_full_factorise`, we have :

$$A = A_0(k) \circ A_1(k) \circ A_{>2}(k) \quad (3)$$

where  $k$  are the parameters and the index is the orbital order. If we use `c_full_factorise`, then we have

$$A = A_0(k) \circ A_1(k) \circ A_{>2}(k) \circ \rho(k) \quad (4)$$

---

In Eq. (4), the  $A_0(k) \circ A_1(k) \circ A_{>2}(k)$  as a special form. In particular,  $A_1(k)$  has a Courant-Snyder-Teng-Edwards form:  $A_{12} = A_{34} \dots = 0$ . The map  $\rho(k)$  is a (nonlinear) rotation in the symplectic case.

In item 3, we use the canonization routines to compute (nonlinear) phase advances. In the linear case, damping is also included. In item 4, the same routines are used for the coasting beam example. In that case, in BMAD, the sixth variable is a constant. The normalization is a Jordan<sup>3</sup> normal form in the linear case and, in the nonlinear case, an extension where the time variable depends only on the sixth variable (the invariant energy) and the transverse actions. Turning on damping, in this case, is unphysical.

Symplectic stable matrices can be represented using a de Moivre representation where the matrices  $H^i$  and  $B^i$  form 3 independent representations of the complex numbers:  $(B^i)^2 = -H^i$ :

$$T^N = \sum_i \left\{ \cos(N\mu_i) H^i + \sin(N\mu_i) B^i \right\} \quad (5)$$

Item 5 refers to the Teng-Edwards factorization. The 4 by 4 matrix which diagonalizes the one-turn matrix in 2-d-f can be factorized as:

$$\text{If } M = BRB^{-1} \rightarrow B = VA \text{ where } V = \begin{pmatrix} \gamma I & C \\ -C^+ & \gamma I \end{pmatrix} \quad (6)$$

$$\text{where } A \text{ is block diagonal} \quad (7)$$

For example,  $H^1$  and  $H^2$  can be expressed in terms of the Teng-Edwards matrices and vice versa.

$$H^1 = \begin{pmatrix} \gamma^2 I & -\gamma C \\ -\gamma C^+ & (1 - \gamma^2) I \end{pmatrix} \text{ and } H^2 = \begin{pmatrix} (1 - \gamma^2) I & \gamma C \\ \gamma C^+ & \gamma^2 I \end{pmatrix} \quad (8)$$

In Eq. (6), the matrix  $V$  has a divergence for large coupling. This happens eventhough the one-turn matrix  $M$  is well behaved. The constant  $\gamma$  goes to zero while the 2 by 2 matrix goes to infinity. Also  $\gamma^2 < 0$  is not a problem for  $H^1$ . In any event, the computation of the Teng-Edwards matrices, with parameter depedence, is explained in item 5.

## 4.5 Symplectific restauration and symplectification

In reference [8], Forest distinguishes two processes. One process he dubs “symplectic restauration” and the other one is the more traditional “symplectification”.

Symplectic restauration is not about tracking. It is a process which only involves the truncated map, i.e., the jet algebra  $_{no}D_{nv}$  described in (§5.4). Usually a Taylor map, truncated at order  $no$  is not symplectic simply because the Taylor series is truncated. However it is also possible that

---

<sup>3</sup>Strictly speaking it is not, but it could be at the expense of making a non-symplectic transformation which is a stupid thing to do.

---

the Taylor series at order  $\leq no$  is incompatible with a symplectic map. This can happen if the integrator used to extract the Taylor coefficients was not symplectic.

Finally, given a proper Taylor series, we may want to add an “infinite” number of monomials to make it symplectic to machine precision during tracking. This is extremely useful if a map is used for tracking. If the map contains radiation, the non-symplectic effects due to numerics can easily overcome the physical effects due to radiation and care must be taken.

	(t:c_taylor, M,A: c_damap and F,F': c_vector_field )	Fortran Routines
1	Symplectic restauration and symplectification	<code>symplectify_general(M,L_r , N_r , L_s, N_s,Q_s )</code>
2	Symplectic restauration and symplectification	<code>fill_tree_element_line_zhe_outside_map</code>
3	Check symplectic or orthogonal condition	<code>call checksymp(M,normt,orthogonal=.false.)</code>

The map  $M$ , midly in item 1 is factorized as

$$M = L_r \circ N_r \circ L_s \circ N_s \circ Q_s \quad (9)$$

where  $L_s$  is a symplectic matrix and  $N_s$  is a symplectic jet near the identity.  $L_r$  is a linear non-symplectic matrix and  $N_r$  is near the identity and non-symplectic.

$L_s$  is computed from the linear part of  $M$  using a contraction map due to Furman.  $L_s$  is computed via a procedure using an integral of a vector field . These are described in [8] sections 2, 3 and 4.

In item 2 we show a routine which factorizes a map into a radiative part and symplectic is a variable called `sagan_gen` is false. This follows pretty much the factorization explained in Eq. (9).

If `sagan_gen` is true, then the nonlinear map is described by a partially inverted map whose implicit solution is symplectic if there is no radiation, otherwise it contains radiation. This is the preferred method.

In item 3, we can check the symplectic condition of a linear map, i.e., the matrix part of  $M$ . `normt` is closed to zero if the map is orthogonal or symplectic.

For a nonlinear map, the symplectic condition can be checked by looking at  $L_r \circ N_r$  in Eq. (9).

## 4.6 Linear matrices and type `c_linear_map`

Matrices can be extracted and linear vector fields as well. They can also be exponentiated.

More importantly there is also a type `c_linear_map` which can be used for linear twiss with spin. The invariant of the linear map (Ripken style) as well as the invariant spin field can be computed.

---

	(mat(:, :), M, A: c_damap and F, F': c_vector_field )	Fortran Routines
1	Matrices and <b>c_damap</b>	<b>Mat(n,n) = M</b> where n=nd2+np : Mat is complex(8) or real(8)
2	Matrices and <b>c_vector_field</b>	<b>H(:, :)=F</b>
3	Exponentiation of matrices	<b>call exp(H(:, :), M(:, :))</b> means <b>M=exp(H)</b>
4	Phase advance with <b>c_linear_map</b>	<b>c_fast_canonise</b> and <b>compute_lattice_functions</b>

Very often we want to do linear calculations of the so-called Twiss type. These calculations in general can compute all orbital lattice functions (as defined by Ripken-Nishikawa-Wolski) and also include the triad of spin vectors  $(l, n, m)$ . Also, we may compute phase advances as well as phase slip and damping “advances.”

## 5 TPSA Algebra

TPSA stands for “Truncated Power Series Algebra” and DA stands for “Differential Algebra.” What does it mean when applied to a typical accelerator ring? Once we cut the mathematical jargon, we will see that

- TPSA operations take into account the constant part and the results change as a function of the order (see below).
- DA operations are equivalent to normal TPSA operations used around the closed orbit and thus the constant part of the map is ignored. All the coefficients of the Taylor series stay the same independently of the order invoked. It so happens that the computation of nonlinear differential operators (Lie vector fields for example), are self-consistent because they form a differential algebra. But it is much simpler in our field to state that they are self-consistent because there are no feed down terms.

It is important to understand why a non-zero constant part of a Taylor series can be problematical. To see this, consider two TPSA maps of order  $N$ . One maps  $x$  to  $y$  and the second maps  $y$  to  $z$ :

$$y = \sum_{j=0}^N a_j x^j \quad (10)$$

$$z = \sum_{j=0}^N b_j y^j + \mathcal{O}(y^{N+1}) \quad (11)$$

In Eq. (11) it is made explicit that there are terms of order  $N + 1$  or higher that are being neglected.

---

The two maps can be concatenated to form a map of  $w$  as a function of  $x$ :

$$w(x) = \sum_{j=0}^N c_j x^j \equiv z(y(x)) \quad (12)$$

If there is a neglected term in Eq. (11) that looks, for example, like  $b_m y^m$  with  $m > N$ , substituting Eq. (10) into this term will result in modification of all lower order terms in Eq. (12) if, and only if,  $a_0$  is non-zero. This is called “feed-down”. That is, terms of higher order will affect the coefficients of lower order terms when TPSA maps are combined. To avoid this, maps with zero constant term (DA maps) should be used. With simulations, this generally means computing maps with respect to the orbit. For lattices with a closed geometry, this generally means computing maps with respect to the **actual period-one closed** orbit. For lattices with an open geometry (EG: Linacs), the reference orbit can be some orbit defined by tracking a beam from some **wisely** user-specified initial position.

## 5.1 Polymorphism

In computer programming “**polymorphism**” is the property that a given variable, object, or function can act in different ways depending upon the context. With FPP/PTC, polymorphism is used to define types that can act as if the structure components were real valued numbers or Taylor series. See the documentation of the **real\_8** type (§??) as an example.

Note: Many **PTC** tracking code routines come in pairs. One routine of the pair, typically having a “r” suffix in its name, will use real variables while the other routine, typically having a “p” suffix in its name. **One could track real numbers with the polymorphic routines but this with entail a substantial speed decrease and therefore we opted for a duplication of the routines.**

Polymorphic types always have structure names that have a **\_8** suffix.

## 5.2 Operator Overloading

FPP/PTC heavily uses operator overloading for the manipulation of Taylor series and polymorphs. Not only are the standard arithmetical operators (+, −, \*, /, \*\*) overloaded as well as the equal sign (=), but there are a number of custom operators that are defined as well. Below is a partial list.<sup>4</sup>

**+, -**

Standard addition and subtraction of Taylor series.

**\***

$M1 * M2$  is used with two maps for **a DA concatenation while  $M1.o.M2$  is a TPSA concatenation with constant part retained.**

---

<sup>4</sup>Note: Fortran mandates that custom operator names begin and end with a dot “.”. These operators have the lowest priority and therefore require parentheses. The usual Fortran operators, if overloaded, inherit the priorities of the intrinsic operators.



---

**.o.**

**\*\***

Powers of Taylor maps

**.oo.**

Powers of Taylor maps using .o. for concatenation.

The difference between **.o.** and **\*** was explained in section (§6) using a one-dimensional example for simplicity.

### 5.3 Tracking Versus Analysis

An important distinction here is the difference between **tracking** and **analysis**. By “tracking” it is meant the propagation through a lattice of a single particle which typically involves six **real\_8** numbers for the orbital motion and four **real\_8** for spin represented via a quaternion.

However, with objects ending in **\_8**, the orbital part and the quaternion can internally become Taylor series in some variables via polymorphism. *De facto*, if these polymorphs are properly initialized, then we can end up tracking Taylor series which can be turned into *bona fide* Taylor maps which approximate the beam line as they do in COSY-INFINITY or MARYLIE. Typically this is used to either compute a one-turn Taylor map or propagate a canonical transformation such as the Courant-Snyder transformation. However it could also produce a map unrelated to the usual one-turn map, for example, the closed orbit as a Taylor series in dipole strengths or anything ... <sup>5</sup> This is opposed to “analysis” which is the study of a **Taylor** transport map to extract such things as tunes, lattice functions, resonance driving terms, etc. With **FPP**, analysis is always done on **Taylor** maps.

### 5.4 TC tracks elements of the algebra $_{no}D_{nv}$

The purpose of this section is to unpack clearly the statement that PTC can track Taylor maps while TC tracks polymorphs which are members of an algebraic extensions of the real numbers. We do this with examples because in the end, all of this is very trivial if we focus on applications rather than theory. For the theory, the reader can look at Berz’s book [1] and in particular the section on Levi-Civita fields<sup>6</sup> which provide inverses to the infinitesimals.

Since any function is a map, we usually reserve the word map to a function of phase space which, in TC, is of dimension 2 at a minimum. Therefore when PTC invokes TPSA it will always track Taylor “maps” but they can be nonsensical as a beam line map. We do allow PTC to track without any TPSA monomials reserved for the orbital motion, but this is only permitted if the

---

<sup>5</sup>Mathematically, single particle tracking is just tracking using Taylor series truncated at zeroth order. From the code perspective, due to the speed reduction with dealing with Taylor series, the two are distinct: the routines with suffixes **\_r** and **\_p**.

<sup>6</sup>We think that it is better for most readers to get a practical view of Berz’s idea before reading his exposition of such fields.

---

TPSA package is initialized with a subroutine proper to FPP: it forces the programmer to view TC as just an “unknown” black box subroutine. We will see what it implies in section (§7.2).

Mathematically what does TC track?

A normal “kick” code tracks a subset of the field  $(\mathbb{R}, +, \times)$ , namely floating point numbers. When embedded in the code Bmad, the TC subroutine “**propagate**”, which we will encounter in the examples, is a function (or map in the usual mathematical sense) from :

$$\mathbb{R}^6 \xrightarrow{TC} \mathbb{R}^6 \quad (13)$$

$$z \longrightarrow z^f = TC(z) \quad (14)$$

$$\text{where in BMAD } z = (x, P_x/p_0, y, P_y/p_0, \beta ct, \delta P/p_0) \in \mathbb{R}^6 \quad (15)$$

PTC or **propagate** is a map of  $\mathbb{R}^6$  in PTC at a minimum. (Spin and other goodies can be included).

Polymorphism extends  $(\mathbb{R}, +, \times)$  to an algebra called by Berz[1]  ${}_{no}D_{nv}$ , i.e., to  $({}_{no}D_{nv}, +, \times)$ . This is the TPSA algebra described in §5. This algebra is a ring, not a field, i.e., not all elements have inverses. In fact all the so-called infinitesimals have no inverses. Colloquially, we might say that we deal with Taylor series not Laurent series. Thus we can say very clearly that

$${}_{no}D_{nv}^6 \xrightarrow{TC} {}_{no}D_{nv}^6 \quad (16)$$

$$z \longrightarrow z^f = TC(z) \quad (17)$$

$$\text{where } z = (x, p_x/p_0, y, p_y/p_0, \beta ct, \delta p/p_0) \in {}_{no}D_{nv}^6 \quad (18)$$

As an example, we can use a 1-d example as in Eq. (49). Consider two second order polynomials in one-variable, i.e., elements of  ${}_2D_1$ :

$$\begin{aligned} \text{if } m &= m_0 + m_1\Delta + m_2\Delta^2 \\ \text{and } n &= n_0 + n_1\Delta + n_2\Delta^2 \end{aligned} \quad (19)$$

then we can write

$$\begin{aligned} \text{if } m &\equiv (m_0, m_1, m_2) \in {}_2D_1 \\ \text{and } n &\equiv (n_0, n_1, n_2) \in {}_2D_1 \end{aligned} \quad (20)$$

In Eq. (20), we use the array notation for elements of the ring  ${}_2D_1$  which is more in line with the actual Fortran90 code. Then we have:

$$m \pm n = (m_0 \pm n_0, m_1 \pm n_1, m_2 \pm n_2) \quad (21)$$

and for multiplication,

$$m \times n = (m_0n_0, m_0n_1 + m_1n_0, m_2n_0 + m_1n_1 + m_0n_2) \quad (22)$$

and finally for division we have,

$$m \div n = \left( \frac{m_0}{n_0}, -\frac{m_0n_1 - m_1n_0}{n_0^2}, -\frac{m_0n_0n_2 - m_0n_1^2 + m_1n_0n_1 - m_2n_0^2}{n_0^3} \right) \quad (23)$$

---

It should be clear from this example that we regain the field of real (or complex) numbers if only the entry of the element of  ${}_2D_1$  is used. Secondly, if  $n_0 = 0$ , then the division of Eq. (23) is not defined: we have a ring, not a scalar field (See Berz[1]).

When TC tracks elements of  ${}_{no}D_{nv}$ , it is totally “unaware” that these objects can be turned into *bona fide* phase space Taylor maps: this was shown in the drift code fragment of section (§1) where no “Taylor maps” are to be seen. In order to explain this dichotomy between tracking and analysis, between polymorphs and Taylors maps, we need to define different structures of FPP/PTC that are optimized to handle one or the other. Structures that have been designed to handle tracking are

```
TC structures

real_8
complex_8      (only used internally in TC)
probe_8
probe          (this is the real version of probe_8)
```

and for analysis here is an important subset

```
AP structures

c_taylor
c_damap
c_normal_form
c_vector_field
```

Finally we have structures which allow us to save Taylor series outside the TPSA package(s) of Berz. This is a permanent kind of storage that does not depend on the order and number of variables used by the TPSA of Berz which underpins FPP. They are totally independent.

```
Storage structures

universal_taylor
c_universal_taylor
```

While the structures that PTC uses for tracking are discussed here, the details of how to track through a lattice are deferred to the PTC documentation. Here the primary concern is FPP and analysis as well as the interaction between analysis and tracking, between AP and TC.

The interaction between the world of polymorphs **\_8**, which are elements of  ${}_{no}D_{nv}$  and Taylor maps, we will illustrate below in section (§7.1). In summary, the code TC produces the usual orbital and spin but, via polymorphism, it can be fed into a structure **c\_damap**, which is a Taylor map and thus can be analyzed if sensible. The result of this analysis, for example a Courant-Snyder transformation, in the form of a **c\_damap**, can then be fed into a polymorphic ray (**probe\_8**, and tracked again. This is how one does any type of Twiss calculation, i.e., propagates canonical transformations including spin and nonlinearities. This is the topic of reference [7].

**Nota Bene:**

---

In summary, there are 3 ways to look at a TPSA variable. They are all isomorphic mathematically but they serve very different purposes in the human brain.

1. As a polynomial in some variable, say  $\Delta$  of Eq. (19), with automatic truncation at order  $no + 1$ . Our brains are in physics mode when doing this.
2. As a polynomial in some abstract object, say  $\Delta$  of Eq. (19), where  $\Delta^{no+1} = 0$ . In that case we are dealing with an abstract representation of  ${}_{no}D_{nv}$ . This is useful when thinking about  $({}_{no}D_{nv}, +, \times)$ . Our brains are in mathematical mode.
3. Finally, the algebra  $({}_{no}D_{nv}, +, \times)$  can be represented as an n-tuple as in Eq. (20). Here we are in a computer science mode since ultimately the computer stores all the TPSA variables in arrays with specific rules under addition and multiplication.

Item 3 is fully demonstrated if one downloads from the git site the following folder:

```
https://github.com/jceepf/fpp\_book/my\_demo\_package
```

This folder contains a mini-TPSA and analysis package as well as a nonlinear Twiss example.

Indeed, the TSPA package of that site (no polymorph but only Taylor) contains the following definition of a Taylor derived type:

```
TYPE my_taylor
  complex(dp) a(0:n_mono)
END TYPE my_taylor
```

This package can represent  $({}_0D_3, +, \times)$ ,  $({}_1D_3, +, \times)$ ,  $({}_2D_3, +, \times)$ ,  $({}_3D_3, +, \times)$  and  $({}_4D_3, +, \times)$ . Obviously  $({}_0D_3, +, \times)$  is just the field of complex numbers  $(\mathbb{C}, +, \times)$  where each number is stored **my\_taylor%a(0)**.

Moreover addition and subtraction are defined respectively by overloading the Fortran90 intrinsic operators via the following functions:

```
FUNCTION add( S1, S2 )
  implicit none
  TYPE (my_taylor) add
  TYPE (my_taylor), INTENT (IN) :: S1, S2

  add%a=S1%a + S2%a

  call clean(add)
END FUNCTION add

FUNCTION subs( S1, S2 )
  implicit none
  TYPE (my_taylor) subs
  TYPE (my_taylor), INTENT (IN) :: S1, S2

  subs%a=S1%a - S2%a
```

---

```

    call clean(subs)
END FUNCTION subs

```

This is exactly Eq. (21). We encourage the reader to compile the files and run the main program.

## 6 DA and TPSA maps

The code for this section is located at `z_track_da_tpsa.f90`.

A code like TC always produces TPSA objects by default. To make the explanations simple, we will assume here that TC is tracking for one turn in a ring. The closed orbit in that case is a natural special orbit demanded by theory. For example, all textbooks assume some version of Hill's equation **around the ideal closed orbit** when discussing Courant-Snyder theory.

Calling this orbit  $f$  — for fixed point — we have:

$$f = TC(f) \quad (24)$$

We now, via polymorphism, track the following ray  $z_0$ :

$$z_0 = f + \Delta \quad (25)$$

$\Delta$  is an array of infinitesimals:

$$\Delta = (\Delta_1, \dots, \Delta_{nv}) \quad \text{where} \quad \Delta_k^{no+1} = 0 \quad (26)$$

If we substitute Eq. (25) in  $TC(z)$ , we get:

$$TC(f + \Delta) = TC(f) + t_f(\Delta) = f + t_f(\Delta) \quad (27)$$

$t_f(\Delta)$  is a (vector) polynomial in  $\Delta$  of maximum degree  $no$  and such that  $t_f(0) = 0$

We can evaluate  $TC$  at a different ray not involving the closed orbit  $f$ , for example, we can use some arbitrary input in the units of TC:

$$TC(z + \Delta) = TC(z) + t_z(\Delta) = z_1 + t_z(\Delta) \quad (28)$$

In Eq. (27) and Eq. (28), the variable  $\Delta$  represents a different expansion. If we want  $\Delta$  to represent the same variable, we need to translate these expressions:

$$m_f(\Delta) = f + t_f(\Delta - f) \quad \text{and} \quad m_z(\Delta) = z_1 + t_z(\Delta - z) \quad (29)$$

In Eq. (29), the maps  $m_f$  and  $m_z$  are the same if and only if  $no = \infty$ . For example, we have:

$$m_f(f) = f = m_z(f) + O(|z - f|^{no+1}) \quad (30)$$

Eq. (30) is again exposing a symptom to TPSA maps: inconstant in the order  $no$  is finite.

Next we see how to such maps can be concatenated.

---

## 6.1 Concatenating two TPSA maps

Consider two TPSA maps:

$$m_{w_0}(z) = w_1 + M_{w_0}(z - w_0) \quad \text{and} \quad n_{z_0}(z) = z_1 + N_{z_0}(z - z_0) \quad (31)$$

For the record here, in FPP, the map  $m_{w_0}$  of Eq. (31) is stored as follows:

$$\begin{aligned} &\text{type(c\_damap) m} \quad | \text{ Here } nv = nd2 + \# \text{ of parameters} \\ &\cdot \\ &m \% \times 0(1:nd2) = w_0 \quad | \text{ these are } \mathbf{complex(dp)}, nd2 \text{ is the size of phase space} \\ &m \% v(1:nd2) = w_1(1:nd2) + M_{w_0}(\Delta(1:nv)) \quad | \text{ these are complex Taylor, i.e., in Berz's } {}_{no}D_{nv} \end{aligned} \quad (32)$$

We compute now the map  $t = m \circ n$ :

$$\begin{aligned} t(x) &= (m_{w_0} \circ n_{z_0})(x) \\ &= w_1 + M_{w_0}(n_{z_0}(x) - w_0) \\ &= w_1 + M_{w_0}(N_{z_0}(x - z_0) + z_1 - w_0) \end{aligned} \quad (33)$$

This operation is done in FPP between two **c\_damap**'s using the operator **.o**.

## 6.2 Inverse of a TPSA map in terms of a DA map

The inverse of a DA map is well known. First one inverts the linear part, a matrix, and then one inverts the nonlinear part by an iterative method that has a finite number of steps, namely  $no$  at most. This routine was programmed by Berz and is in **c\_dabnew.f90**. In FPP is called as follows:

```
type(c_damap) m, m_inverse
.
.
m_inverse = m**(-1)
.
.
```

We work out the TPSA inverse of  $m_{w_0}$  of Eq. (31). To do so we solve the following equation for  $y$  in terms of  $x$ :

$$\begin{aligned} m_{w_0}(x) &= w_1 + M_{w_0}(x - w_0) = y \\ \Rightarrow x &= M_{w_0}^{-1}(y - w_1) + w_0 \\ \text{or } m_{w_0}^{-1}(x) &= M_{w_0}^{-1}(x - w_1) + w_0 \end{aligned} \quad (34)$$

In FPP, the TPSA inverse is invoked by the following call:

---

```

type(c_damap) m, m_tpsa_inverse
.
.
m_tpsa_inverse= m.oo.(-1)
.
.

```

### 6.3 Concatenating two DA maps using their TPSA representation

In a “DA” situation, the exit value of the first map must be the entrance value of the second map, i.e., they must be evaluated on the same orbit. Therefore we must have  $z_1 = w_0$ :

$$m_{w_0}(\Delta) = w_1 + M_{w_0}(\Delta - w_0) \quad \text{and} \quad n_{z_0}(\Delta) = w_0 + N_{z_0}(\Delta - z_0) \quad (35)$$

For example the first map could be from the entrance of a wiggler to its center followed by the second half of the wiggler. Obviously, the exit value of  $n_{z_0}$  must be the entrance value of the ray of map  $m_{w_0}$ . Here we verified, that in this case, we can ignore completely these constant values. In an integrator, this happens completely naturally since we do not deal with **c\_damap** but with the rays themselves in polymorphic form, i.e., type **probe\_8**.

$$\begin{aligned}
(m_{w_0} \circ n_{z_0})(\Delta) &= w_1 + M_{w_0}(n_{z_0}(\Delta) - w_0) \\
&= w_1 + M_{w_0}(N_{z_0}(\Delta - z_0)) \\
&= w_1 + (M_{w_0} \circ N_{z_0} \circ (I - z_0))(\Delta) \\
&= w_1 + \underbrace{(M_{w_0} \circ N_{z_0})}_{DA \circ}(\Delta - z_0)
\end{aligned} \quad (36)$$

We see in Eq. (36), where  $I - z_0$  represents a translation, that only the concatenation of the map around the orbit is necessary, i.e.,  $M_{w_0} \circ N_{z_0}$ . This is why, in FPP, the DA concatenation does not keep track of the constant parts at all. This is the case, for example, during all the normal form operations: in the linear case for example, all the matrices are around the closed orbit, no feed-down effects are present and thus constant parts can be ignored in diagonalizing the matrix.

This DA operation is done in FPP between two **c\_damap**’s using the operator **\***.

#### 6.3.1 Where are TPSA map and DA stored: one Fortran type but two operations

A code like TC naturally produces TPSA maps of the form

$$TC(z) = m_{w_0}(z) = w_1 + M_{w_0}(z - w_0) \quad (37)$$

This map is produced by tracking a particle starting at  $w_0$  and using TPSA to extract the Taylor representation denoted by  $M_{w_0}$ . However there is an infinite number of choices for  $w_0$ :

$$TPSA = \left\{ w_0 \in \mathbb{R}^6 \mid TC(z) = m_{w_0}(z) = w_1 + M_{w_0}(z - w_0) \right\}_{No=\infty} \quad (38)$$

---

If the order  $No$  is infinite, then all these maps are identical and anyone could be used to represent the map of the code, namely  $TC(z)$ . You are simply expanding the same function around a different point.

In fact their Taylor representations form a natural equivalent class. Things start to degenerate if  $No$  is finite, as it is in all realistic applications:

$$TPSA_{No} = \left\{ w_0 \in \mathbb{R}^6 \mid TC(z) \approx m_{w_0}(z) = w_1 + M_{w_0}(z - w_0) \right\}_{No < \infty} \quad (39)$$

With a finite  $No$ , there is a need to be close to the design orbit (LINAC) or closed orbit (ring). This is to avoid feed down issues. This is achieved, in a ring, by choosing the map expressed around the actual closed orbit of the code TC.

It is clear that any member of that set can be stored to order  $No$  in the type **c\_damap**. Therefore we use this type for both DA and TPSA maps.

The difference is in the operator used: both are types **c\_damap**. If **M** and **N** are DA maps, then the resulting DA map **K** will be:

$$K = M * N$$

If we intend **M** and **N** to be TPSA maps, then the code is

$$K = M . o . N$$

The code for **M\*N** completely ignore the constant parts when performing the required substitutions. For example, in a linear map, we are just multiplying matrices.

As we will see in section (§6.7),  $w_0$  is stored in **c\_damap%w0(:)**. It is ignored by the DA concatenation “.”.

## 6.4 Finding the closed orbit of a one-turn TPSA map

In an integrator such as Bmad or PTC, we normally find the exact closed orbit  $f$ . However what if we have a TPSA map  $m_{w_0}$  which is **not** around the closed orbit? We need to solve the following equation:

$$m_{w_0}(f) = w_1 + M_{w_0}(f - w_0) = f \quad (40)$$

Eq. (40) into an equation involving a map:

$$\begin{aligned} m_{w_0}(f) &= f \\ w_1 + M_{w_0}(f - w_0) - f &= 0 \end{aligned} \quad (41a)$$

$$\begin{aligned} w_1 + M_{w_0}(f - w_0) - (f - w_0) - w_0 &= 0 \\ w_1 - w_0 + M_{w_0}(f - w_0) - (f - w_0) &= 0 \\ w_1 - w_0 + (M_{w_0} - I)(f - w_0) &= 0 \end{aligned} \quad (41b)$$

$$c_{w_0}(f) = 0 \quad (41c)$$



---

Eq. (41b) is exactly in the TPSA form of our **c\_damap**, i.e., the right hand term of Eq. (29). We can solve for the fixed point  $f$ :

$$f = c_{w_0}^{-1}(0) \quad (42)$$

Once again, the value of  $f$  will depend on the order of truncation  $no$  while the fixed point of the integrator is “exact”.

## 6.5 Computing the DA map from the TPSA map: inconsistent

Consider the map of Eq. (40)

$$m_{w_0}(z) = w_1 + M_{w_0}(z - w_0) \quad (43)$$

and its fixed point given by Eq. (42). We can re-expressed around the fixed point  $f$ . It is done by a strange similarity transformation. Consider this representation of the identity map:

$$a_f(z) = f + I(z - f) \quad (44)$$

Eq. (44) is the identity “expressed” around  $f$ . The two  $f$ ’s obviously cancel. We also notice, not too surprisingly, following Eq. (34), we have

$$a_f^{-1}(z) = a_f(z) \quad (45)$$

We are now ready to make the following similarity transformation on  $m_{w_0}$ . To do so, we keep the identity explicitly in Eq. (44) and apply twice the concatenation formula of Eq. (33). It is just a matter of substituting carefully variables:

$$(a_f \circ m_{w_0} \circ a_f)(\Delta) = w_1 + M_{w_0}(I(\Delta - f) - w_0 + f) \quad (46a)$$

$$= \left\{ \underbrace{(w_1 + M_{w_0} \circ (I - w_0 + f))}_{\text{DA map around } f} \circ \underbrace{(I - f)}_{\text{shift}} \right\}(\Delta) \quad (46b)$$

In Eq. (46a)<sup>7</sup>, if we use the definition of  $I$ , clearly all  $f$ ’s disappear and we are back where we started. However we use the definition of a **c\_damap** and extract  $-f$  from the map and use a shift. This is consistent with the definition shown in blue in Eq. (32).

This last formula allows for normal form on TPSA maps. Of course, if  $no = \infty$  inconsistencies will appear. For example otherwise symplectic maps will become non-symplectic or, worse, radiation effects will be wiped out. This is why we love integrators with DA maps around the true closed orbit.

We now illustrates all of this in a one dimensional example and also with a real map from a ring.

---

<sup>7</sup>We avoided abuses of notation in Eq. (46a). Some people may want to confuse the identity  $I$  with the dummy variable  $\Delta$  if that helps.

---

Finally we substitute  $\Delta = 0$  is the left factor (DA map) of Eq. (46b) and get

$$w_1 + M_{w_0}(-w_0 + f)$$

which is, according to Eq. (41a), precisely the fixed orbit if  $f$  is selected according to Eq. (41c).

## 6.6 Concatenating two “DA” maps from the “code” of Eq. (47)

We provide an actual one-dimensional example using AP. This is a map in one dimension which is the result of the concatenation of two maps. It imitates a ring made of two parts.

$$\begin{aligned} m_1(x) &= 0.05 + \sin(0.5x) + 0.3 \sin^2(x) \\ m_2(x) &= 0.03 + \sin(0.3x) + 0.2 \sin^2(x) \\ m_{12} &= m_2 \circ m_1 \end{aligned} \tag{47}$$

As we can see,  $m(0) \neq 0$ : therefore the numbers 0.05 and 0.03 represent a deliberate weird placement of a magnet or the inevitable misalignments found in every beam line. Suppose we want the linear properties of this map, in a code like PTC, it is recommended to first solve for the closed orbit,

$$m_{12}(x_0) = x_0 \rightarrow x_0 = 0.05469119581164052 \dots \tag{48}$$

and then we expand the one-turn map around this closed orbit:

$$m_{12}(x_0 + \Delta) = x_0 + m_{12;1}\Delta + m_{12;2}\Delta^2 + \dots \tag{49}$$

The actual “DA” map is made of the coefficients  $m_{12;i}$  of Eq. (49). We can compute this map to second order which is very common in ring dynamics: the linear part gives the usual lattice functions and the second order part gives us the sextupoles distortions and/or chromaticities in a real ring. Here is the code fragment:

```
type(c_taylor) x    ! In PTC, x would be a probe_8

write(6,*) "Imitating PTC: tracking through  "

x=x_closed+(1.d0*cmono.1)
x=sin(x/2.d0)+0.3d0*sin(x)**2+0.05d0
x_closed1=x        ! recording orbit for future use
x=sin(0.3d0*x)+0.2d0*sin(x)**2+0.03d0

call print(x)
```

The result, for  $x$ , is:

---

```
Imitating PTC: tracking through
```

```

      1, NO =      2, NV =      1, INA =      9
*****

```

I	COEFFICIENT	ORDER	EXPONENTS
	NO = 2 NV = 1		
0	0.5469119581164052E-01	0.0000000000000000	0
1	0.1763235586477631	0.0000000000000000	1
2	0.1533323662801814	0.0000000000000000	2
-3	0.0000000000000000	0.0000000000000000	0

We see that the real part of the Taylor series is the closed orbit indeed.

The code fragment is:

```

! computing map1
x=x_closed+(1.d0.cmono.1)
x=sin(x/2.d0)+0.3d0*sin(x)**2+0.05d0
map1%v(1)=x
! computing map2
x=x_closed1+(1.d0.cmono.1)
x=sin(0.3d0*x)+0.2d0*sin(x)**2+0.03d0
map2%v(1)=x
one_turn_map_AP = map2*map1
Write(6,*) " This is map1 "
call print(map1)
Write(6,*) " This is map2 "
call print(map2)
write(6,*) "one_turn_map_AP = map2*map1 "
call print(one_turn_map_AP)
!!! Saving DA coefficients to imitate a TRANSPORT-like code
m(1,1)=map1%v(1).sub.'1'
m(1,2)=map1%v(1).sub.'2'
m(2,1)=map2%v(1).sub.'1'
m(2,2)=map2%v(1).sub.'2'
write(6,*) "Coefficients using Taylor Map Multiplication "
write(6,*) m(1,1)*m(2,1), m(2,1)*m(1,2)+m(2,2)*m(1,1)**2

```

and the result is

```

Creating two DA maps : map1 and map2
This is map1
tpsa status for tracking type(c_ray) F
      1 Dimensional DA map (around chosen orbit in map%x0)

      1, NO =      2, NV =      1, INA =     10
*****

      I  COEFFICIENT          ORDER  EXPONENTS
      NO =      2      NV =      1

```

---

```

0 0.7823863368603357E-01 0.000000000000000 0
1 0.5325623875161611 0.000000000000000 1
2 0.2947893387720240 0.000000000000000 2
-3 0.000000000000000 0.000000000000000 0
No Spin Matrix
No c_quaternion
No Stochastic Radiation
This is map2
tpsa status for tracking type(c_ray) F
1 Dimensional DA map (around chosen orbit in map%x0)

1, NO = 2, NV = 1, INA = 24
*****

I COEFFICIENT ORDER EXPONENTS
NO = 2 NV = 1
0 0.5469119581164052E-01 0.000000000000000 0
1 0.3310852639633932 0.000000000000000 1
2 0.1965003538431843 0.000000000000000 2
-3 0.000000000000000 0.000000000000000 0
No Spin Matrix
No c_quaternion
No Stochastic Radiation
one_turn_map_AP = map2*map1
tpsa status for tracking type(c_ray) F
1 Dimensional DA map (around chosen orbit in map%x0)

1, NO = 2, NV = 1, INA = 66
*****

I COEFFICIENT ORDER EXPONENTS
NO = 2 NV = 1
0 0.5469119581164052E-01 0.000000000000000 0
1 0.1763235586477631 0.000000000000000 1
2 0.1533323662801814 0.000000000000000 2
-3 0.000000000000000 0.000000000000000 0
No Spin Matrix
No c_quaternion
No Stochastic Radiation
Coefficients using Taylor Map Multiplication
0.176323558647763 0.153332366280181

```

Since the maps **map1** and **map2** are around the closed orbit, we expect them to obey the usual

---

rules of DA concatenation which ignore the constant parts. Thus, given  $m_{12} = m_2 \circ m_1$ ,

$$\text{if } m_1(x_0 + \Delta) = x_1 + m_{1;1}\Delta + m_{1;2}\Delta^2 + \dots \quad (50a)$$

$$\text{and } m_2(x_0 + \Delta) = x_2 + m_{2;1}\Delta + m_{2;2}\Delta^2 + \dots \quad (50b)$$

$$\text{then } m_{12}(x_0 + \Delta) = x_0 + m_{12;1}\Delta + m_{12;2}\Delta^2 + \dots \quad (50c)$$

$$\text{where } m_{12;1} = m_{1;1}m_{2;1} \text{ and } m_{12;2} = m_{2;1}m_{1;2} + m_{2;2}m_{1;1}^2 \quad (50d)$$

We see perfect agreements in the numerical results. Now we will turn this into a TPSA concatenation problem.

## 6.7 Concatenating the two “TPSA” maps from the “code” of Eq. (47)

Let us compute the one-turn map by concatenating the two maps map1 and map2 around, respectively, the weird orbits  $x_1 = 0.015$  and  $x_2 = 0.02$ . As we explained before these are the same as the DA maps of section (§6.6) is  $no = \infty$  but here  $no = 2$ .

The map is computed using the code fragment

```
! Creating TPSA maps around the design orbit

x1= 0.015d0
map1%x0(1)=x1
x=map1%x0(1)+(1.d0.cmono.1)
map1%v(1)=sin(x/2.d0)+0.3d0*sin(x)**2+0.05d0

x2=.02d0
map2%x0(1)=x2
x=map2%x0(1)+(1.d0.cmono.1)
map2%v(1)=sin(0.3d0*x)+0.2d0*sin(x)**2+0.03d0

!!! multiplying the TPSA maps
map12=map2.o.map1

x=map12%v(1)+i.*one_turn_map_AP%v(1)
write(6,*) " The map map12 for one turn"
call print(map12)
write(6,*) " Comparing the TPSA one-turn map with the DA one-turn map"
write(6,*) " TPSA coefficients DA coefficient ",k
call print(x)
```

The results are:

```
      The map map12 for one turn
      tpsa status for tracking type(c_ray) F
      1 Dimensional DA map (around chosen orbit in map%x0)
Initial orbit for TPSA calculations
(1.5000000000000000E-002,0.0000000000000000E+000)

      1, NO =      2, NV =      1, INA =      38
*****
```

---

```

      I  COEFFICIENT          ORDER  EXPONENTS
      NO =      2      NV =      1
0  0.4793209256475234E-01  0.0000000000000000  0
1  0.1643954713972499    0.0000000000000000  1
2  0.1482514114953167    0.0000000000000000  2
-3  0.0000000000000000    0.0000000000000000  0
No Spin Matrix
No c_quaternion
No Stochastic Radiation
Comparing the TPSA one-turn map with the DA one-turn map
TPSA coefficients      DA coefficient      0

      1, NO =      2, NV =      1, INA =      9
*****

      I  COEFFICIENT          ORDER  EXPONENTS
      NO =      2      NV =      1
0  0.4793209256475234E-01  0.5469119581164052E-01  0
1  0.1643954713972499    0.1763235586477631  1
2  0.1482514114953167    0.1533323662801814  2
-3  0.0000000000000000    0.0000000000000000  0

```

The two maps, map12 and one\_turn\_map\_AP, are identical but expressed around different orbits. The map one\_turn\_map\_AP is expressed around the closed orbit. We will use the results of section (§6.4) to move map12 to its fixed point. This is done with the code fragment:

```

type(c_ray) rayon
.
.
.
! TPSA maps re-expressed around the closed orbit !

write(6,*) " closed orbit computation "
write(6,*) map12%x0(1)
c_w0%x0=map12%x0
c_w0%v(1)=map12%v(1)-(1.d0.cmono.1)-map12%x0(1)
c_w0_inv=c_w0.oo.(-1)

f_map%x0=0
f_map%v(1)=0.d0
f_map=c_w0_inv.o.f_map
f_ray=0
f_ray=c_w0_inv.o.f_ray
call print(c_w0_inv)
call print(f_map)
write(6,*) "exact ", x_closed
x_closed_tpsa=map1%v(1)
write(6,*) "TPSA  ", x_closed_tpsa
write(6,*) "f_ray ", f_ray%x(1)

```

---

```

go_to_orbit%v(1)= (1.d0.cmono.1)+x_closed_tpsa
go_to_orbit%x0=x_closed_tpsa

map12=(go_to_orbit.o.map12).o.(go_to_orbit.oo.(-1))

call print(map12)

x=map12%v(1)+i*one_turn_map_AP%v(1)
write(6,*) "      Maps around the TPSA closed orbit "
write(6,*) "      Comparing TPSA one-turn map around the TPSA fixed point "
write(6,*) "      with the DA one-turn map"
write(6,*) "      TPSA coefficients          DA coefficient "

call print(x)

```

The answer for the TPSA map around the approximately computed closed orbit is:

```

      Maps around the TPSA closed orbit
      Comparing TPSA one-turn map around the TPSA fixed point
      with the DA one-turn map
      TPSA coefficients          DA coefficient

      1, NO =      2, NV =      1, INA =      9
      *****

      I  COEFFICIENT          ORDER  EXPONENTS
      NO =      2          NV =      1
0  0.5469069935363461E-01  0.5469119581164052E-01  0
1  0.1761640230032753      0.1763235586477631      1
2  0.1482514114953167      0.1533323662801814      2
-3  0.0000000000000000      0.0000000000000000      0

```

We see that the agreement has improved. Indeed if  $no = \infty$ , the agreement would be perfect. This is why a code like COSY-INFINITY usually runs at a high order. If we rerun this example with  $no = 10$ , we get:

```

      Maps around the TPSA closed orbit
      Comparing TPSA one-turn map around the TPSA fixed point
      with the DA one-turn map
      TPSA coefficients          DA coefficient

      1, NO =     10, NV =      1, INA =     17
      *****

      I  COEFFICIENT          ORDER  EXPONENTS
      NO =     10          NV =      1
0  0.5469119581164050E-01  0.5469119581164052E-01  0
1  0.1763235586477634      0.1763235586477631      1
2  0.1533323662802094      0.1533323662801814      2
3  0.4375700106665827E-01  0.4375700106455089E-01  3

```

---

4	-0.3637622533509953E-01	-0.3637622544112402E-01	4
5	-0.3834044616082886E-01	-0.3834044989384196E-01	5
6	-0.1063392477923387E-01	-0.1063401860744071E-01	6
7	0.1162532131698485E-01	0.1162363855314815E-01	7
8	0.1090970864911106E-01	0.1088862478020678E-01	8
9	0.2833241323816774E-03	0.1079668683861611E-03	9
10	-0.3309462539739653E-02	-0.4174183972224262E-02	10

We can see that we are closing on the DA map section (§6.6).

In a kick code or integrator, we can compute maps at a low order while preserving perfect self-consistency provided all the maps are computed around the closed orbit in a ring. Therefore, in an integrator, if you like your model, you are assured of self-consistency.

One additional issue is “symplecticity” which cannot be analyzed with a fake map like that of Eq. (47). This can become a severe issue especially if radiation is turned on: the TPSA maps lack of consistency can be greater than radiation damping, thus erasing a very important effect. This does not happen in a (symplectic) integrator since the maps are always self-consistent.

## 7 PTC examples of DA vs TPSA maps

The code for this section is located at `z_track_map_code.f90`. If you run the code, you can select case 1,2,3 or 4 which correspond respectively to sections (§7.1), (§7.2), (§7.3) and (§7.4).

### 7.1 Extracting Taylor orbital maps around the closed orbit: case 1

Now we look at a “PTC” piece of code which mixes, in a trivial but very fundamental way, the analysis part (AP) with the tracking part (TC) of PTC with the specific intent of creating a *bona fide* Taylor series map which approximates the beam line in PTC, i.e., the output of the subroutine **propagate**.

Consider:

```
p=>ring%start
closed_orbit=0
call find_orbit_x(closed_orbit,bmad_state, 1.0e-7_dp, fibre1=p)
write(6,*) " closed orbit "
write(6,"(6(1x,g11.4))") closed_orbit
```

The above code is pure tracking of real numbers. The closed orbit is computed at the start of the ring. The **find\_orbit\_x** routines finds the closed orbit and returns :

```
closed orbit
-0.1788E-03 -0.9790E-05 -0.1328E-04 -0.6548E-04 -0.1866E-05 -0.5154E-01
```

The object **Bmad\_state**, of type **internal\_state**, is a PTC structure where the particulars of Bmad are fed for compatibility : units of Bmad, phase space dimension of 6 for **c\_damap**’s, etc. . .



---

**internal\_state**'s are objects which control the initialization interface between TC and AP when *bona fide* Taylor maps are needed for analysis. They do not need to exist and could be left to the user if the interaction between TC and AP was a once-in-a-blue-moon event.

The new code fragment is interesting:

```
select case(case_section)
case(1)
p=>ring%start
call move_to(ring,p,"QF1")    ! Locating QF1 in TC
call make_it_knob(p%magp%bn(1),1) ! PP : making a Polymorph into a knob
call move_to(ring,p,"QF2")    ! Locating QF2 in TC
call make_it_knob(p%magp%an(1),2) ! PP : making a Polymorph into a knob

p=>ring%start
closed_orbit=0
call find_orbit_x(closed_orbit,bmad_state, 1.0e-7_dp, fibre1=p)
write(6,*) " closed orbit "
write(6,"(6(1x,g11.4))") closed_orbit

no=1 ; np=2 ; ! nv=6+2=8
call init(bmad_state,no,np) ! Berz's TPSA package is initialized
```

The TPSA variables will be of order no=1 and the phase space dimension will be six via **Bmad\_state**. Additionally, via np=2, the polynomials will have two extra variables—knob 1 and 2. Therefore the total number of variables will be 8. Then it is decided that the dipole components of the first QF1 and QF2 will be the 7th (6+1) and 8th (6+2) variables representing respectively the normal dipole component of QF1 and the skew component of QF2. These things are called knobs and can be turned off at will. If they are active, then the dipole components of these quadrupoles are TPSA variables otherwise they stay **real(8)** variables.

Now we mix TC and AP:

```
type(probe) ray_TC
type(probe_8) ray_8_TC
type(c_damap) one_turn_map_AP, identity_AP, two_turn_map_AP
real(dp) closed_orbit(6)
type(internal_state),target :: Bmad_state
.
.
.

ray_TC=closed_orbit ! For TC

identity_AP=1 ! For AP

ray_8_TC=ray_TC+identity_AP ! Connect AP with TC
write(6,*) " The initial x "
call print(ray_8_TC%x(1))
call propagate(ray_8_TC,+bmad_state,fibre1=p) ! TC of PTC proper
```

---

```

one_turn_map_AP=ray_8_TC ! TC into AP : makes a map out of ray_8_TC

write(6,*) "x_final for one turn "
call print(one_turn_map_AP%v(1))

two_turn_map_AP=one_turn_map_AP*one_turn_map_AP
write(6,*) "x_final for two turns : squaring the map "
call print(two_turn_map_AP%v(1))

! Tracking two turns using TC
ray_8_TC=ray_TC+identity_AP ! Connect AP with TC
call propagate(ray_8_TC,+bmad_state,fibre1=p) ! TC of PTC proper
call propagate(ray_8_TC,+bmad_state,fibre1=p) ! TC of PTC proper
two_turn_map_AP=ray_8_TC ! TC into AP : makes a map out of ray_8_TC
write(6,*) "x_final for two turns : tracking two turns "
call print(two_turn_map_AP%v(1))

```

**identity\_AP** is an AP object of type **c\_damap**. It is set to a phase space identity by equating it to 1. Indeed in any code which tracks Taylor maps (COSY-INFINITY, TRANSPORT, MARYLIE, etc...) the initial value of a map must be the identity in 6 dimensions. In the linear case, it amounts to the identity matrix in the 6 orbital variables of Bmad. The first variable is the monomial  $z_1$  representing  $x$ , the second variable is  $z_2$  will represent  $p_x$  and so on, i.e., the variables of the Bmad phase space. (See Bmad manual)

The next line is crucial: it mixes AP and TC. **ray\_8\_TC** is a **probe\_8**: we feed in it the closed orbit buried in **ray\_TC** which is made of **real(8)** and add to this the identity map. This operation reveals Forest intent: generally make useful Taylor series phase space maps from TC. It could have been left to the user. Indeed if a user links TC to a library which finds the linear eigenvalues of a matrix, neither Forest nor the authors of that library would provide the interface: it must be written by the user based on the nature of these matrices. Here the object **Bmad\_state**, of type **internal\_state**, contains all that is needed to make of TC and AP consistent packages.

So now the polymorphic probe **ray\_8\_TC** contains a polymorph consistent with the identity map expressed around the closed orbit. The code prints this polynomial:

```

The initial x

etall      1, NO =      1, NV =      8, INA =      29
*****

```

I	COEFFICIENT	ORDER	EXPONENTS
	NO = 1 NV = 8		
0	-0.1787724612820044E-03	0	0 0 0 0 0 0 0 0
1	1.0000000000000000	1	0 0 0 0 0 0 0 0
-2	0.0000000000000000	0	0 0 0 0 0 0 0 0

We recognize the closed orbit value of  $x$  and the monomial  $1.0 * z_1^1$ .

Therefore the tracking will take place correctly around the closed orbit and the feed down effects will be correctly computed. This is to be contrasted with *bona fide* Taylor codes (COSY-INFINITY, TRANSPORT, MARYLIE, etc...) where feed-down effects are not self-consistent<sup>8</sup>. Here they are

---

<sup>8</sup>COSY-INFINITY is often more accurate than PTC but is not self-consistent with its own model. In rings, this can be

totally self-consistent with the code.

The next is TC proper: **propagate(ray\_8\_TC,+Bmad\_state,fibre1=p)** tracks through the total beam line— actually one turn in this example. The + sign in front of **Bmad\_state** activates the “knobs” connected to QF1 and QF2. In TC, knobs are deactivated by default. This is not true of PP proper.

The next line **one\_turn\_map\_AP=ray\_8\_TC** sends the final TC structure **ray\_8\_TC** into a **c\_damap**: it connects TC to AP. Finally, we attempt a pure AP operation

```
two_turn_map_AP=one_turn_map_AP*one_turn_map_AP
```

This operation is the concatenation of two “differential algebraic” maps: the constant part is ignored.

This is followed by a two turns tracking of TC. The results are identical to machine precision. This is the virtue of using “DA” maps around the closed orbit in an “kick code” or integrator like TC. We print the results for the skeptics: notice machine precision agreement—only the last two digits are different.

```
x_final for one turn
1, NO = 1, NV = 8, INA = 230
*****

I COEFFICIENT ORDER EXPONENTS
NO = 1 NV = 8
0 -0.1787724612819064E-03 0.0000000000000000 0 0 0 0 0 0 0 0
1 -0.3889828486539758 0.0000000000000000 1 0 0 0 0 0 0 0
1 11.40736328972829 0.0000000000000000 0 1 0 0 0 0 0 0
1 -0.3464662557908923E-02 0.0000000000000000 0 0 1 0 0 0 0 0
1 -0.4171271427570414E-01 0.0000000000000000 0 0 0 1 0 0 0 0
1 0.6963086125527715E-10 0.0000000000000000 0 0 0 0 1 0 0 0
1 0.8036598951947091E-01 0.0000000000000000 0 0 0 0 0 1 0 0
1 -4.224142793166476 0.0000000000000000 0 0 0 0 0 0 1 0
1 -0.3125492004102120E-05 0.0000000000000000 0 0 0 0 0 0 0 1
-9 0.0000000000000000 0.0000000000000000 0 0 0 0 0 0 0 0
x_final for two turns : squaring the map

1, NO = 1, NV = 8, INA = 179
*****

I COEFFICIENT ORDER EXPONENTS
NO = 1 NV = 8
0 -0.1787724612819064E-03 0.0000000000000000 0 0 0 0 0 0 0 0
1 -0.7056565190107400 0.0000000000000000 1 0 0 0 0 0 0 0
1 -8.751690962380659 0.0000000000000000 0 1 0 0 0 0 0 0
1 -0.3542316696944531E-01 0.0000000000000000 0 0 1 0 0 0 0 0
1 0.2562552716914303E-02 0.0000000000000000 0 0 0 1 0 0 0 0
1 0.5610356685840276 0.0000000000000000 0 0 0 0 1 0 0 0
1 0.8726398593300869E-01 0.0000000000000000 0 0 0 0 0 1 0 0
1 -2.218998803166924 0.0000000000000000 0 0 0 0 0 0 1 0
1 -0.1965421389017537E-01 0.0000000000000000 0 0 0 0 0 0 0 1
-9 0.0000000000000000 0.0000000000000000 0 0 0 0 0 0 0 0
x_final for two turns : tracking two turns
```

a problem. In a single pass system, it might be better to have accurate inconsistent models with complex fringe effects, then simplistic integrators like TC.

```

1, NO = 1, NV = 8, INA = 179
*****
I   COEFFICIENT          ORDER  EXPONENTS
NO = 1      NV = 8
0 -0.1787724612818773E-03  0.0000000000000000  0 0 0 0 0 0 0 0
1 -0.7056565190107397     0.0000000000000000  1 0 0 0 0 0 0 0
1 -8.751690962380632      0.0000000000000000  0 1 0 0 0 0 0 0
1 -0.3542316696944601E-01  0.0000000000000000  0 0 1 0 0 0 0 0
1 0.2562552716913452E-02   0.0000000000000000  0 0 0 1 0 0 0 0
1 0.5610356685840368      0.0000000000000000  0 0 0 0 1 0 0 0
1 0.8726398593301046E-01   0.0000000000000000  0 0 0 0 0 1 0 0
1 -2.218998803166917      0.0000000000000000  0 0 0 0 0 0 1 0
1 -0.1965421389017552E-01  0.0000000000000000  0 0 0 0 0 0 0 1
-9 0.0000000000000000     0.0000000000000000  0 0 0 0 0 0 0 0

```

## 7.2 Extracting Taylor Series which are not orbital maps: case 2

*Nota Bene* : In this section, we call FPP outside the constructs of PTC, namely without the use of **bmad\_state**. Of course, we could still use **bmad\_state** and thus produce a phase space map with null transverse entry. In this case we waste, in Bmad, 6 TPSA variables. This might be a memory/speed issue if a large number of variables or a higher order are required. Otherwise it is perfectly fine. See section (§7.4) to see how the equivalent calculation is done when running with Bmad variables as Taylor series.

The function **propagate** of TC computes a final position  $z^f = (z_1^f, z_2^f, z_3^f, z_4^f)$  in terms of an initial position  $z^0 = (z_1^0, z_2^0, z_3^0, z_4^0)$ .

Furthermore, we can choose 6 magnets to have TPSA parameters. Namely 3 of them will be normal dipole kicks and 3 of them will be skew dipole kicks.

```

p=>ring%start
call move_to(ring,p,"QF1")    ! Locating QF1 in TC
call make_it_knob(p%magp%bn(1),1) ! PP : making a Polymorph into a knob
call move_to(ring,p,"QF2")    ! Locating QF2 in TC
call make_it_knob(p%magp%an(1),2) ! PP : making a Polymorph into a knob
call move_to(ring,p,"QD1")    ! Locating QD1 in TC
call make_it_knob(p%magp%bn(1),3) ! PP : making a Polymorph into a knob
call move_to(ring,p,"QD2")    ! Locating QD2 in TC
call make_it_knob(p%magp%an(1),4) ! PP : making a Polymorph into a knob
call move_to(ring,p,"BEND")    ! Locating BEND in TC
call make_it_knob(p%magp%bn(1),5) ! PP : making a Polymorph into a knob
call move_to(ring,p,"BEND1")   ! Locating BEND1 in TC
call make_it_knob(p%magp%an(1),6) ! PP : making a Polymorph into a knob

```

Even if  $z^0$  starts as **real(8)**, by virtue of polymorphism, it will become a vector of Taylor series if **propagate** visits any of the above magnets..

Here is the code computing  $z^f$ . Notice that in this example we start with the entrance orbit  $z^0 = 0$ . We will try to fit the output  $z^f$  also to 0. None of this will depend on the meaning of TC. It could compute the values of stocks for all that we know.

---

```

bmad_state=bmad_state+nocavity0 ! turns cavities into drifts

p=>ring%start
closed_orbit=0
call find_orbit_x(closed_orbit,bmad_state, 1.0e-7_dp, fibre1=p)
write(6,*) " closed orbit "
write(6,"(6(1x,g11.4))") closed_orbit

np=6      ! number of free parameters to solve these equations
no=1; nV=NP ; ! nv=6
call c_init_all(no,nv) ! FPP command to initialize the TPSA

call alloc(ct);call alloc(ray_8_TC);

ray_TC=entrance_orbit ! For TC
ray_8_TC=ray_TC ! Connect AP with TC: no identity added
write(6,*) "The variable x = z_1^0 "
call print(ray_8_TC%x(1))
p=>ring%start
call propagate(ray_8_TC,+bmad_state,fibre1=p) ! TC of PTC proper
call print(ray_8_TC%x(1))

```

The important difference is the line **ray\_8\_TC=ray\_TC**: the initial orbit made of 6 **real(8)** numbers is simply put into the polymorphic **probe\_8** structure **ray\_8\_TC**. At this stage, there are no Taylor series in sight. Indeed the code print the initial value of  $x$  and it is the simply a **real(8)** unlike the example of section (§7.1):

```

The variable x = z_1^0
0.0000000000000000E+000

```

However, TC will encounters some Taylor series during the tracking, namely the dipole components of the magnets QF1, QF2, QD1, QD2, BEND and BEND1. Thus, via polymorphism, a Taylor series in these components will appear as the 1st to 6th variables of the TPSA package.

Additionally, the command to initialize TPSA, **call c\_init\_all(no,nv)**, is pure FPP and is unaware of the analysis package (symplectic maps) or of the code PTC. Indeed while **propagate** is a PTC command, we could have used any code computing anything for the example of this section and section (§7.3).

The output for the variable  $x = z_1$  is

```

The variable x = z_1^f

etall      1, NO =      1, NV =      10, INA =      44
*****

      I   COEFFICIENT                ORDER   EXPONENTS
      NO =      1          NV =      10
0  0.6109701219350949E-02    0  0  0  0  0  0  0  0  0  0  0  0
1  -4.962724533009230        1  0  0  0  0  0  0  0  0  0  0

```

---

```

1 -0.2968892804328157E-05  0  1  0  0  0  0  0  0  0  0
1 -1.421420498227908      0  0  1  0  0  0  0  0  0  0
1 -0.1231462510798852E-05  0  0  0  1  0  0  0  0  0  0
1 -1.116448300584394      0  0  0  0  1  0  0  0  0  0
1 -0.4314330647295780E-04  0  0  0  0  0  1  0  0  0  0
-7  0.0000000000000000    0  0  0  0  0  0  0  0  0  0

```

Naive attempts to create a Taylor map using the standard interface between TC and AP, in this example, will lead to nonsense. Instead we will use the resulting polymorphic **probe\_8** to create a kind of closed orbit bump by fitting the final  $z^f$  to  $z^0$ :

This is the topic of the next section using the example of this section.

### 7.3 Fitting the output of section (§7.2): case 3

In section (§7.2), the Taylor series of the output **probe\_8** called **ray\_8\_TC** have 6 variables for the dipole strengths. Consider the following functions

$$G = \frac{1}{2} \sum_{i=1,6} k_i^2 + \sum_{i=1,4} \lambda_i \left( z_i^f(\mathbf{k}) - \mathbf{g}_i \right) \quad (51)$$

The vector  $\mathbf{v} = (k_1, k_2, k_3, k_4, k_5, k_6, \lambda_1, \lambda_2, \lambda_3, \lambda_4)$  contains the 6 dipole strengths and 4 Lagrange multipliers. The first term in Eq. (51) is the function we will minimize namely the norm of the total dipole strengths. The second term represents the equations we want to set equal to a goal function namely  $\mathbf{g}$ . In our example, they are the values of  $x$ ,  $p_x$ ,  $y$ , and  $p_y$ .

The solutions are found by solving the following set of equations:

$$\text{lagrange\_map\_ap}(\mathbf{v}) = \nabla_v G = 0 \quad (52)$$

*lagrange\_map\_ap* is a map in 10 TPSA variables. We can solve with by TPSA inversion since the constant part is significant:

$$\mathbf{v} = \text{lagrange\_map\_ap}^{-1}(0) \quad (53)$$

If the order of the TPSA was infinite, then we would get an exact solution. Otherwise this is simply the first step of a Newton search. We show the actual algorithm and the results:

```

bmad_state=bmad_state+nocavity0 ! turns cavities into drifts

p=>ring%start
closed_orbit=0
call find_orbit_x(closed_orbit,bmad_state, 1.0e-7_dp, fibre1=p)
write(6,*) " closed orbit "
write(6,"(6(1x,g11.4))") closed_orbit

goal=0.d0

```

---

```

entrance_orbit=0
goal(1:6)=entrance_orbit

do k=1,4      ! performing 4 iterations

    !!!!!!! Part 1 : calling TC !!!!!!!
    neq=4      ! number of equations to solve
    np=6      ! number of free parameters to solve these equations
    no=1; nV=NP ; ! nv=6
    call c_init_all(no,nv) ! FPP command to initialize the TPSA

    call alloc(ct);call alloc(ray_8_TC);

    ray_TC=entrance_orbit ! For TC
    ray_8_TC=ray_TC ! Connect AP with TC: no identity added
    !write(6,*) "The variable x = z_1^0 "
    !call print(ray_8_TC%x(1))
    p=>ring%start
    call propagate(ray_8_TC,+bmad_state,fibre1=p) ! TC of PTC proper
    !call print(ray_8_TC%x(1))

    !!!!!!! Part 2 : saving the relevant Taylor series !!!!!!!

    call ALLOC(tpos,1,NV,0) ! c_universal_taylor
    do i=1,4
        ct=ray_8_TC%x(i)%t ! saving final transverse positions and momenta
        tpos(i)=ct
    enddo
    call kill(ct);call kill(ray_8_TC);

    !!!!!!! Part 3 : creating a map of some sort and using it !!!!!!!

    nV=NP+neq ; ! nv=6+4=10
    call c_init_all(no,nv) ! FPP command to initialize the TPSA
    call alloc(ct);call alloc(eq);

    lagrange_map_ap%n=nv
    call alloc(lagrange_map_ap)

    do i=1,4
        eq(i)=tpos(i) ! putting the c_universal_taylor into c_taylor
    enddo

    !!! Construction of Lagrange function
    do i=1,np
        lagrange_map_ap%v(i)=1.d0.cmono.i
        do j=np+1,np+neq

            ct=((eq(j-np).d.i)*(1.d0.cmono.j))

```

---

---

```

    lagrange_map_ap%v(i)=lagrange_map_ap%v(i)+ct
  enddo
enddo

do i=np+1,np+neq
  lagrange_map_ap%v(i)=eq(i-np)-goal(i-np)
enddo

lagrange_map_ap=lagrange_map_ap.oo.(-1)

f_ray=0
f_ray=lagrange_map_ap.o.f_ray

p=>ring%start
call move_to(ring,p,"QF1")    ! Locating QF1 in TC
  k1=f_ray%x(1)
  call add(p,1,1,k1)
call move_to(ring,p,"QF2")
  k1=f_ray%x(2)
  call add(p,-1,1,k1)
call move_to(ring,p,"QD1")    ! Locating QF1 in TC
  k1=f_ray%x(3)
  call add(p,1,1,k1)
call move_to(ring,p,"QD2")    ! Locating QF2 in TC
  k1=f_ray%x(4)
  call add(p,-1,1,k1)
call move_to(ring,p,"BEND")    ! Locating QF2 in TC
  k1=f_ray%x(5)
  call add(p,1,1,k1)
call move_to(ring,p,"BEND1")  ! Locating QF2 in TC
  k1=f_ray%x(6)
  call add(p,-1,1,k1)

p=>ring%start

ray_TC=entrance_orbit    ! For TC

call propagate(ray_TC,bmad_state,fibre1=p) ! TC of PTC proper

write(6,*) " exit orbit "
write(6,"(4(1x,g11.4))") ray_TC%x(1:4)
call kill(lagrange_map_ap);call kill(ct);call kill(eq);call kill(tpos);

enddo

```

This code fragment has two parts:

1. In the first part, TC is called with the FPP initialization `call c_init_all(no,nv)` with `nv=6`.
2. In the second part, some Taylor series are saved for future used in 4 `c_universal_taylor`'s.



---

These are the Taylor series for the transverse phase space as a function of 6 dipole strengths.

3. A map is created to fit the final positions and momenta reconstructed from the 4 **c\_universal\_taylor**'s. FPP is initialized with **nv=10**.

First we are taking the derivative of the output of the orbital ray. Secondly we multiply is by **(1.d0.mono.j)** which represents the variables  $v_{7,8,9,10}$ , i.e., the Lagrange multipliers. There is no chance in hell that this could have been guessed by the programmers of either PTC or Bmad. This map is truly a construction of the user and is not the output of PTC. It is created from the output of PTC the same way a matrix can be computed from the output of an ordinary **real(8)** code via numerical differentiation. What for? Up to the user.

Here is the result of 4 iterations with no=1:

```
exit orbit
0.5673E-03  0.4982E-04 -0.1294E-06  0.4597E-08
exit orbit
0.1903E-04 -0.2253E-07 -0.1233E-09  0.1115E-08
exit orbit
0.6044E-09  0.5405E-09 -0.1040E-11 -0.1279E-12
exit orbit
0.1130E-14 -0.3989E-16  0.1440E-19  0.5051E-19
```

With no=5, the convergence takes two iterations:

```
exit orbit
-0.1216E-06  0.9864E-08  0.1979E-09  0.6521E-10
exit orbit
-0.1139E-15  0.1102E-16 -0.2711E-19 -0.1347E-19
```

In conclusion, the subroutine **propagate** returns Taylor series which have no apparent special meaning. The user creates in this case a map which the author of PTC, Etienne Forest, could never have anticipated. For this reason, the creation of this Lagrangian-Newton map is entirely the responsibility of the user.

On the other hand, in section (§7.1), the code TC was initialized with the construct

```
identity_AP=1 ! For AP
ray_8_TC=ray_TC+identity_AP ! Connect AP with TC
```

This construction is provided by PTC under the assumption that Taylor maps produced by PTC are the usual phase space maps. The **probe\_8** is constructed by adding phase space identity to the closed orbit or entrance orbit. In that sense, PTC tracks phase space maps because of the default interface between TC and FPP.

In fact, as we pointed out, not only the identity can be added but any canonical transformation which represent the shape of a beam or lattice functions— linear, nonlinear, spin, etc. . .

But it is important to remember that any change of variables within PTC involves elements of Berz's TPSA algebra  $_{no}D_{nv}$  and manipulations which are identical to the manipulations of **real(8)**. There are no Taylor maps, no **c\_damap**.

---

## 7.4 Fitting the orbital ray and the tunes: case 4

This example is a more in tune (pun intended) with the usual usage of PTC. Suppose we want to fit the final position of the ray, as in section (§7.3), as well as the transverse tunes and the phase slip. Then, as in Eq. (51), a contracting map can be constructed from a Lagrange function:

$$G = \frac{1}{2} \sum_{i=1,12} k_i^2 + \sum_{i=1,3} \mu_i (v_i(\mathbf{k}) - v_{0i}) + \sum_{i=1,4} \lambda_i \left( z_i^f(\mathbf{k}) - \mathbf{g}_i \right) \quad (54)$$

This time the vector  $\mathbf{v} = (k_1, \dots, k_{12}, \mu_1, \mu_2, \mu_3, \lambda_1, \lambda_2, \lambda_3, \lambda_4)$  contains the 12 dipole strengths, 3 Lagrange multipliers for the tunes and phase slip and finally 4 Lagrange multipliers for the orbit.

The code is similar to the code of section (§7.3). However this time a “real map” is computed with 6 phase space variables (Bmad) and 12 parameters for a total of 18 variables. This map is normalized and the transverse tunes in **phase(1:2)** and the phase slip in **phase(3)** are extracted.

In part 2, the equations to solve are saved via the **c\_universal\_taylor**’s **tpos(:)**. Finally the Lagrange map with the 19 variables of  $\mathbf{v}$  is computed and inverted as part of the Newton search.

Here is the code. This concludes our discussion on “Taylor maps” coming out of TC.

```
p=>ring%start
call move_to(ring,p,"QF1")      ! Locating QF1 in TC
call make_it_knob(p%magp%bn(2),1) ! PP : making a Polymorph into a knob
call move_to(ring,p,"QF2")      ! Locating QF2 in TC
call make_it_knob(p%magp%an(2),2) ! PP : making a Polymorph into a knob
call move_to(ring,p,"QD1")      ! Locating QD1 in TC
call make_it_knob(p%magp%bn(2),3) ! PP : making a Polymorph into a knob
call move_to(ring,p,"QD2")      ! Locating QD2 in TC
call make_it_knob(p%magp%an(2),4) ! PP : making a Polymorph into a knob
call move_to(ring,p,"BEND")      ! Locating BEND in TC
call make_it_knob(p%magp%bn(2),5) ! PP : making a Polymorph into a knob
call move_to(ring,p,"BEND1")     ! Locating BEND1 in TC
call make_it_knob(p%magp%an(2),6) ! PP : making a Polymorph into a knob

p=>ring%start
call move_to(ring,p,"QF1")      ! Locating QF1 in TC
call make_it_knob(p%magp%bn(1),7) ! PP : making a Polymorph into a knob
call move_to(ring,p,"QF2")      ! Locating QF2 in TC
call make_it_knob(p%magp%an(1),8) ! PP : making a Polymorph into a knob
call move_to(ring,p,"QD1")      ! Locating QD1 in TC
call make_it_knob(p%magp%bn(1),9) ! PP : making a Polymorph into a knob
call move_to(ring,p,"QD2")      ! Locating QD2 in TC
call make_it_knob(p%magp%an(1),10) ! PP : making a Polymorph into a knob
call move_to(ring,p,"BEND")      ! Locating BEND in TC
call make_it_knob(p%magp%bn(1),11) ! PP : making a Polymorph into a knob
call move_to(ring,p,"BEND1")     ! Locating BEND1 in TC
call make_it_knob(p%magp%an(1),12) ! PP : making a Polymorph into a knob

write(6,*) " %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%"

bmad_state=bmad_state+nocavity0

p=>ring%start
closed_orbit=0
call find_orbit_x(closed_orbit,bmad_state, 1.0e-7_dp, fibre1=p)
write(6,*) " closed orbit "
write(6,"(6(1x,g11.4))") closed_orbit
```

---

```

goal=0.d0
entrance_orbit=closed_orbit
goal(1)=0.28d0
goal(2)=0.79d0
goal(3)=(-1)**ndpt_bmad*2.5d-2
goal(4:7)=entrance_orbit(1:4)

do k=1,8

!!!!!! Part 1 : calling TC !!!!!
neq=7      ! number of equations to solve
np=12      ! number of free parameters to solve these equations
no=2 ;      ! nv=6+12=18
call init(bmad_state,no,np) ! Berz's TPSA package is initialized
nv=c_%nv    !
call alloc(ct)
call alloc(identity_AP,one_turn_map_AP);call alloc(normal_form);
call alloc(ray_8_TC);call alloc(phase);call alloc(eq)
p=>ring%start

ray_TC=entrance_orbit ! For TC
identity_AP=1
ray_8_TC=ray_TC + identity_AP ! Connect AP with TC: identity added

p=>ring%start
call propagate(ray_8_TC,+bmad_state,fibre1=p) ! TC of PTC proper

one_turn_map_AP=ray_8_TC

! compute 2 tunes and the phase slip
call c_normal(one_turn_map_AP,normal_form,phase=phase)
ray_TC=ray_8_TC
write(6,"(3(1x,g17.10,1x))" ) normal_form%tune(1:3)
write(6,"(6(1x,g17.10,1x))" ) ray_TC%x(1:6)
identity_AP=0

phase(3)=phase(3).d.(5+ndpt_bmad) ! compute phase slip dbeta*t/ddelta

phase(1)=(phase(1).o.identity_AP)<=6 ! removing delta dependence
phase(2)=(phase(2).o.identity_AP)<=6 ! removing delta dependence
phase(3)=(phase(3).o.identity_AP)<=6 ! removing delta dependence

eq(1)=phase(1)-goal(1) ! tune x
eq(2)=phase(2)-goal(2) ! tune y
eq(3)=phase(3)-goal(3) ! pahse slip

do i=1,4
ct=ray_8_TC%x(i)%t
eq(3+i)=((ct.o.identity_AP)<=6)-goal(3+i)
enddo

!!!!!! Part 2 : saving the relevant Taylor series !!!!!
call ALLOC(tpos,1,NV,0)
do i=1,7
tpos(i)=eq(i)
enddo

call kill(identity_AP,one_turn_map_AP);call kill(normal_form);
call kill(ray_8_TC);call kill(phase);call kill(eq);call kill(ct) ;
!!!!!! Part 3 : creating a map of some sort and using it !!!!!

neq=7      ! number of equations to solve
np=12      ! number of free parameters to solve these equations
no=no-1; nv=NP+neq ; ! nv=7+12=19
call c_init_all(no,nv) ! FPP command to initialize the TPSA
lagrange_map_ap%n=nV ! size of the c_damap must be explicitely stated

```

---

---

```

call alloc(ct);call alloc(eq);call alloc(lagrange_map_ap);
do i=1,7
  eq(i)=tpos(i)
enddo
!!! Construction of Lagrange function
do i=1,np
  lagrange_map_ap%v(i)=1.d0.cmono.i
  do j=np+1,np+neq
    ct=(eq(j-np).d.i)*(1.d0.cmono.j)
    lagrange_map_ap%v(i)=lagrange_map_ap%v(i)+ct
  enddo
enddo

do i=np+1,np+neq
  lagrange_map_ap%v(i)=eq(i-np)
enddo

lagrange_map_ap=lagrange_map_ap.oo.(-1)

f_ray=0
f_ray=lagrange_map_ap.o.f_ray

p=>ring%start
call move_to(ring,p,"QF1")      ! Locating QF1 in TC
k1=f_ray%x(1)
call add(p,2,1,k1)
call move_to(ring,p,"QF2")
k1=f_ray%x(2)
call add(p,-2,1,k1)
call move_to(ring,p,"QD1")      ! Locating QF1 in TC
k1=f_ray%x(3)
call add(p,2,1,k1)
call move_to(ring,p,"QD2")      ! Locating QF2 in TC
k1=f_ray%x(4)
call add(p,-2,1,k1)
call move_to(ring,p,"BEND")      ! Locating QF2 in TC
k1=f_ray%x(5)
call add(p,2,1,k1)
call move_to(ring,p,"BEND1")     ! Locating QF2 in TC
k1=f_ray%x(6)
call add(p,-2,1,k1)

p=>ring%start
call move_to(ring,p,"QF1")      ! Locating QF1 in TC
k1=f_ray%x(7)
call add(p,1,1,k1)
call move_to(ring,p,"QF2")      ! Locating QF2 in TC
k1=f_ray%x(8)
call add(p,-1,1,k1)
call move_to(ring,p,"QD1")      ! Locating QD1 in TC
k1=f_ray%x(9)
call add(p,1,1,k1)
call move_to(ring,p,"QD2")      ! Locating QD2 in TC
k1=f_ray%x(10)
call add(p,-1,1,k1)
call move_to(ring,p,"BEND")      ! Locating BEND in TC
k1=f_ray%x(11)
call add(p,1,1,k1)
call move_to(ring,p,"BEND1")     ! Locating BEND1 in TC
k1=f_ray%x(12)
call add(p,-1,1,k1)

call kill(ct) ;call kill(eq);call kill(lagrange_map_ap);
enddo

```

In this code we fit the orbit to the original closed orbit.

---

The results are for the tunes, phase slip and the orbit:

0.2828310304	0.7875313802	-0.2508933816E-01	
0.4575879602E-02	-0.8650459066E-05	-0.1701393632E-04	-0.4623033694E-04
-0.1176909853E-02	0.000000000		
0.2799916973	0.7900014703	-0.2499706314E-01	
0.4581594167E-02	-0.8590151609E-05	-0.1700070068E-04	-0.4623484201E-04
-0.1214079405E-02	0.000000000		
0.2799981589	0.7900002081	-0.2500013027E-01	
0.4575879632E-02	-0.8650379343E-05	-0.1701358606E-04	-0.4623024223E-04
-0.1212988306E-02	0.000000000		
0.2799999976	0.7899999994	-0.2500000017E-01	
0.4575879600E-02	-0.8650459057E-05	-0.1701393633E-04	-0.4623033694E-04
-0.1213016115E-02	0.000000000		
0.2800000000	0.7900000000	-0.2500000000E-01	
0.4575879602E-02	-0.8650459066E-05	-0.1701393632E-04	-0.4623033694E-04
-0.1213016151E-02	0.000000000		
0.2800000000	0.7900000000	-0.2500000000E-01	
0.4575879602E-02	-0.8650459067E-05	-0.1701393632E-04	-0.4623033694E-04
-0.1213016151E-02	0.000000000		
0.2800000000	0.7900000000	-0.2500000000E-01	
0.4575879602E-02	-0.8650459066E-05	-0.1701393632E-04	-0.4623033694E-04
-0.1213016151E-02	0.000000000		
0.2800000000	0.7900000000	-0.2500000000E-01	
0.4575879602E-02	-0.8650459066E-05	-0.1701393632E-04	-0.4623033694E-04
-0.1213016151E-02	0.000000000		

## 8 Normalizing a TPSA map

The code for this section is located at [z\\_track\\_normal\\_tpsa.f90](#).

### 8.1 Normalizing as a DA map around the closed orbit

Here we run a code where we can choose to get a one-turn map around the closed orbit (DA map) or around the orbit  $x = 0$  which in this ring would correspond to the so-called “design orbit”. As in section (§7.1) we used to knobs corresponding to quadrupole components:

```
p=>ring%start
call move_to(ring,p,"QF1")    ! Locating QF1 in TC
call make_it_knob(p%magp%bn(2),1) ! PP : making a Polymorph into a knob
call move_to(ring,p,"QF2")    ! Locating QF2 in TC
call make_it_knob(p%magp%an(2),2) ! PP : making a Polymorph into a knob
```

The next step is to decide whether we want a DA map or a TPSA map around the so-called “design orbit” **x0=0** here:

```
bmad_state=only_4d
```

```

.
.
.
p=>ring%start
closed_orbit=0
call find_orbit_x(closed_orbit,bmad_state, 1.0e-7_dp, fibre1=p)
write(6,*) " closed orbit "
write(6, "(6(1x,g11.4))") closed_orbit
x0=closed_orbit

write(6,*) " For TPSA map around f=(0,...,0) type 1 "
write(6,*) " For DA map around closed orbit type 0 "
read(5,*) ignore_closed_orbit
write(6,*) " Give order no "
read(5,*) no
if(ignore_closed_orbit==1) then
  closed_orbit=0
endif

```

We first show the results for the DA map:

```

closed orbit
0.4576E-02 -0.8650E-05 -0.1701E-04 -0.4623E-04 0.000 0.000
For TPSA map around f=(0,...,0) type 1
For DA map around closed orbit type 0
0
Give order no
2
Transverse tunes
0.2828310304 0.7875313802
Dampings (numerical noise)
-0.4329869796E-14 0.1332267630E-14

z_1-component of the Linear Vector Field in Phasors Variables

1, NO = 3, NV = 6, INA = 358
*****
I COEFFICIENT ORDER EXPONENTS
NO = 3 NV = 6
1 0.0000000000000000 -1.777079774508286 1 0 0 0 0 0
-1 0.0000000000000000 0.0000000000000000 0 0 0 0 0 0

z_1-component of the Non-Linear Vector Field in Phasors Variables (2nd order)

1, NO = 3, NV = 6, INA = 659
*****
I COEFFICIENT ORDER EXPONENTS
NO = 3 NV = 6
2 0.0000000000000000 -2.580306677113468 1 0 0 0 1 0
2 0.0000000000000000 0.3425829877097634E-01 1 0 0 0 0 1
3 0.0000000000000000 -2900.949436382287 2 1 0 0 0 0
3 0.0000000000000000 6556.211092278534 1 0 1 1 0 0
3 0.0000000000000000 -0.2020888563626094 1 0 0 0 2 0

```

---

3	0.0000000000000000	-0.2080839310516064	1	0	0	0	1	1
3	0.0000000000000000	5.902822986039759	1	0	0	0	0	2
-7	0.0000000000000000	0.0000000000000000	0	0	0	0	0	0

In the above example, the vector field is given by:

$$F \cdot \nabla = i \left\{ -1.777 - 2.580dk_1^n - 0.034dk_2^s - 2900.949 \underbrace{z_1 z_2}_{I_1} + \dots \right\} z_1 \partial_{z_1} + \text{other planes} \quad (55)$$

In fact, it is a purely imaginary vector field: it represents a tune. In fact  $1.777079774508286/2/\pi = 0.2828310304 \dots$  which is just the tune in the first plane.

There is no real part in this vector field since this would represent damping. The state of PTC, **bmad\_state=only\_4d**, is a cavity-less radiation-less, state which restricts Taylor maps to the transverse orbital dimensions as the **4d** in **only\_4d** indicates.

## 8.2 Normalizing as a TPSA map around the (0,0,0,0,0,0)

Because the map is not around the closed orbit, we must first move the TPSA map around the closed orbit using the algorithm of section (§6.4) and the same code as in page 31. This is given by the code:

```
if(ignore_closed_orbit==1) then
!   Compute TPSA closed orbit
one_turn_map_AP%x0(1:c_%nd2)=x0(1:c_%nd2)
c_w0%x0(1:c_%nd2)=x0(1:c_%nd2)

!!! inversion only need in the transverse plane in this example
do i=1,c_%nd2
  c_w0%v(i)=one_turn_map_AP%v(i)-(1.d0.cmono.i)-one_turn_map_AP%x0(i)
enddo

  c_w0_inv=c_w0.oo.(-1)

f_map%x0=0
do i=1,c_%nd2
  f_map%v(i)=0.d0
f_map=c_w0_inv.o.f_map
enddo

f_ray=0
f_ray=c_w0_inv.o.f_ray

! Similarity transformation to the closed orbit

go_to_orbit= 1
go_to_orbit%x0(1:c_%nd2)=f_ray%x(1:c_%nd2)
do i=1,c_%nd2
  go_to_orbit%v(i)= go_to_orbit%v(i)+f_ray%x(i)
enddo
```

---

```

one_turn_map_AP=(go_to_orbit.o.one_turn_map_AP).o.(go_to_orbit.o.(-1))

write(6,"(a18,6(1x,g11.4))") "Exact  closed orbit",closed_orbit(1:c_%nd2)
write(6,"(a18,6(1x,g11.4))") "TPSA  closed orbit",real(f_ray%x(1:c_%nd2))

endif

```

The result of this normalization is to second order:

```

Exact  closed orbit  0.4576E-02 -0.8650E-05 -0.1701E-04 -0.4623E-04
TPSA  closed orbit  0.4575E-02 -0.8523E-05 -0.1716E-04 -0.4624E-04
EIG6: Eigenvalues off the unit circle!
1.00159643192902
EIG6: Eigenvalues off the unit circle!
1.00159643192902
EIG6: Eigenvalues off the unit circle!
1.00056073888672
EIG6: Eigenvalues off the unit circle!
1.00056073888672
Transverse tunes
0.2826834097      0.7872786253
Dampings (numerical noise)
-0.1595158986E-02 -0.5605817314E-03

z_1-component of the Linear Vector Field in Phasors Variables

      1, NO =      3, NV =      6, INA = 358
*****

      I  COEFFICIENT          ORDER  EXPONENTS
      NO =      3      NV =      6
1  0.1595158986163770E-02  -1.776152246232164      1  0  0  0  0  0
-1  0.0000000000000000      0.000000000000000      0  0  0  0  0  0

z_1-component of the Non-Linear Vector Field in Phasors Variables (2nd order)

      1, NO =      3, NV =      6, INA = 667
*****

      I  COEFFICIENT          ORDER  EXPONENTS
      NO =      3      NV =      6
2  -0.1819669443106595      -2.657937823855120      1  0  0  0  1  0
2  0.1187338977469338E-02  0.3373570996746057E-01      1  0  0  0  0  1
3  1707.209464520280      -2338.602046283265      2  1  0  0  0  0
3  782.8781372860180      6922.042189398233      1  0  1  1  0  0
3  3.114213005812829      -0.5998691420874549      1  0  0  0  2  0
3  -0.2927537938038314E-01  -0.1634680876623557      1  0  0  0  1  1
3  0.7397499373591118E-01  5.985271299438016      1  0  0  0  0  2
-7  0.0000000000000000      0.000000000000000      0  0  0  0  0  0

```

One notices the problems: apparitions of damping, i.e., non-symplectic terms. For example, the (anti)-damping in the first plane is **-0.1595158986E-02**. This is an unacceptable artifact of the feed-down being completely wrong. We see also non-linear anti-damping. This is also a phenomenon of non-symplectic integrators.

Of course we can run at a higher order, for example  $no = 11$ , printing only numbers greater than  $10^{-10}$ :



---

```

Exact closed orbit 0.4576E-02 -0.8650E-05 -0.1701E-04 -0.4623E-04
TPSA closed orbit 0.4576E-02 -0.8650E-05 -0.1701E-04 -0.4623E-04
Transverse tunes
0.2828310304      0.7875313802
Dampings (numerical noise)
-0.1043609643E-13 0.2309263891E-13

z_1-component of the Linear Vector Field in Phasors Variables

      1, NO = 11, NV = 6, INA = 494
*****

      I COEFFICIENT      ORDER EXPONENTS
      NO = 11 NV = 6
      1 0.0000000000000000 -1.777079774507927 1 0 0 0 0 0
      -1 0.0000000000000000 0.000000000000000 0 0 0 0 0 0

z_1-component of the Non-Linear Vector Field in Phasors Variables (2nd order)

      1, NO = 11, NV = 6, INA = 605
*****

      I COEFFICIENT      ORDER EXPONENTS
      NO = 11 NV = 6
      2 0.0000000000000000 -2.580306677112761 1 0 0 0 1 0
      2 0.0000000000000000 0.3425829877673507E-01 1 0 0 0 0 1
      3 0.7402969486021055E-08 -2900.949436547272 2 1 0 0 0 0
      3 0.5652109279438409E-06 6556.211092675170 1 0 1 1 0 0
      3 -0.2248561335679724E-08 -0.2020888596108968 1 0 0 0 2 0
      3 0.6870246124991154E-09 -0.2080839306933067 1 0 0 0 1 1
      3 0.0000000000000000 5.902822986046178 1 0 0 0 0 2
      -7 0.0000000000000000 0.000000000000000 0 0 0 0 0 0

```

We see that the situation as improved and approaches the DA result. It is not surprising that users of COSY-INFINITY must run at very higher order in rings. This is not necessary with a symplectic integrator provided all the maps are around the closed orbit, i.e., DA maps.

## 9 Skeletal description of `c_normal_new`: normal form routine

This routine `c_normal_new`, normally, is used with a DA map presumably computed around the closed orbit of a tracking code. It is made of 3 essential parts and some incidental parts:

1. Go to the parameter dependent fix point
2. Normalizing exactly the linear map using complex eigenvectors and the constant quaternion.
3. Normalizing the nonlinear map spin included

**N.B.** In the presence of radiation, the tune shifts are left in. They act like a resonance for the damping. This is controlled by a global variable called `remove_tune_shift` which is set to false by default. See reference [7], section 5.5 for an example.

---

## 9.1 New formulae: changing a vector field and the Lie bracket

A vector field operates on a quaternion as follows:

$$\hat{F}q = \{\vec{F} \cdot \vec{\nabla} + \hat{f}\} q = \vec{F} \cdot \vec{\nabla} q + qf \quad (56)$$

Consider the Lie map  $\mathcal{A}$  operator associated with the phase space map  $A = (a, \alpha)$ . It acts on a phase space map  $M = (m, q)$  following, the formula:

$$\mathcal{A}(m, q) = (m, q) \circ (a, \alpha) = (m \circ a, \{q \circ a\} \alpha) \quad (57)$$

How does a vector field  $\hat{F}$  transform by the map of Eq. (57)? This has to be done by a similarity transformation:

$$\mathcal{A}(F \cdot \nabla + \hat{f}) \mathcal{A}^{-1} = \tilde{F} \cdot \nabla + \hat{\tilde{f}} \quad (58)$$

The answer for  $\tilde{F}$  and  $\tilde{f}$  is:

$$\begin{aligned} \tilde{F}_k &= (F_i \partial_i a_k^{-1}) \circ a \\ \tilde{f} &= (\tilde{F}_k \partial_k \alpha^{-1}) \alpha + \alpha^{-1} f \circ a \alpha \end{aligned} \quad (59)$$

As for the Lie bracket, we first evaluate the commutator of two operators  $\hat{F}$  and  $\hat{H}$ :

$$\begin{aligned} [\hat{F}, \hat{H}] &= [F \cdot \nabla + \hat{f}, H \cdot \nabla + \hat{h}] \\ &= G \cdot \nabla + \hat{g} \end{aligned} \quad (60)$$

The answer for  $\hat{G}$  is:

$$\begin{aligned} G &= \langle F, H \rangle = F \cdot \nabla H - H \cdot \nabla F \\ g &= hf - fh + F \cdot \nabla h - H \cdot \nabla f \end{aligned} \quad (61)$$

Where the orbital part of the Lie bracket is defined by

$$\langle F, G \rangle = F_b \frac{\partial G}{\partial z_b} - G_b \frac{\partial F}{\partial z_b} \quad (62)$$

## 9.2 Going to the fixed point: transformation $A_0$

This routines is called at position !#1 in **Ci\_tpsa.f90**.

---

This routine is only “complicated” if the 3rd plane is coasting (energy  $z_6$  is constant). In that case,  $z_6$  is added to the list of parameters.

$$\sum_{1,4, k=6,1:np} N_{ij} f_j + \Delta_k v_{kj} = f_i \quad (63)$$

The array  $\Delta$  contains  $z_6$  and **np** system parameters. The fixed point  $f$  is computed via a DA inversion. This is done at location `!##3` in the code.

The presence of  $z_6$  implies a modification of the time of flight if the canonical transformation is to be symplectic. Therefore the following Lie map is constructed:

$$\mathcal{A}_0 = \exp \left( : \sum_{i,j=1,4} f_i S_{ij} z_j : \right) \quad (64)$$

The change in the time variable  $z_5$  is done using:

$$z_5^{new} = z_5 - \sum_{i,j=1,4} \frac{\partial f_i}{\partial z_6} S_{ij} x_j \quad (65)$$

This is done after line `!##5` in the code using a **c\_universal\_taylor** called **uf1**, this is needed in Berz’s package.

N.B. This calculation must be done to order 1 at least in a standard normal form.

### 9.3 Linear normal form: $A_1$

#### 9.3.1 Linear orbital map in normal form: **c\_linear\_a(m1,a1)**

This transformation, at line `!#2`, requires access to a package capable of finding the complex eigenvectors and eigenvalues. Parameters are not (never) included in this stage: they are always handled by the nonlinear part of the normal form.

In FPP, this is done via a routine by Filippo Neri. It is located at `!###1`. Prior to this, the coasting plane, if it exists, is relegated to the last plane. This is necessary if some magnets are modulated via an harmonic oscillation and thus part of the normal form.

The rest of the routine, `!###4`, insures that the Poisson bracket is 1 between planes. If the original map is symplectic, this is enough to insure that the linear transformation is symplectic. For nonsymplectic maps, this does not hurt.

The theory behind this is described in section (2.4.1) of the yellow book[6].

---

### 9.3.2 Linear spin normal form:

Assuming the spin part of the one-turn map has the form:

$$q = \cos\left(\frac{\theta}{2}\right) + \sin\left(\frac{\theta}{2}\right) (\omega_1 i + \omega_2 j + \omega_3 k) \quad (66)$$

then we can diagonalize it:

$$q_r = \cos\left(\frac{\theta}{2}\right) + \sin\left(\frac{\theta}{2}\right) j \quad (67)$$

using the following transformation

$$a = \cos(\alpha) + \sin(\alpha) (\alpha_1 i + \alpha_3 k) \quad (68)$$

In other words we have:

$$q = a q_r a^{-1} \quad (69)$$

This calculation is performed in `c_normal_spin_linear_quaternion(m1,m1,n%AS,alpha)`.

In FPP, as displayed in Eq. (67), the normal axis of the normal form is  $j$ , i.e., the vertical axis. This makes sense to the extent that most rings are planar.

## 9.4 The nonlinear algorithm

This is usually the most scary thing for neophytes. In reality, the nonlinear algorithm is a turn-the-crank algorithm that monotonically repeats itself order by order until the map is in normal form. It is easiest to describe in terms of Lie operators, i.e., vector fields. The type `c_vector_field` is made of an orbital operator and a quaternion.

$$\hat{F} = \vec{F} \cdot \vec{\nabla} + \hat{f} \quad (70)$$

It operates on a quaternion  $q$  as follows:

$$\hat{F}q = \vec{F} \cdot \vec{\nabla} q + q\hat{f} \quad (71)$$

The reverse order on the quaternion is necessary for consistency with the orbital Lie operator.

At line !#3, the orbital dependence is transformed into phasors. This is important to identify the resonances from the tune shifts. At line !#10, a similar thing is done for the quaternion: we go into “eigenquaternions” under rotation around the  $y$ -axis. This is done inside the normalization loop.

In the normalization, the Lie map version of the map, always looks as follows:

$$\mathcal{M}_i = \mathcal{R} \exp\left(\hat{K}_1\right) \cdots \exp\left(\hat{K}_{i-1}\right) \exp\left(\hat{F}_i\right) \quad (72)$$

---

Here  $\hat{F}_i$  contains terms which ought to be removed. The normalization iteration ends when  $\hat{F}_i = 0$  and  $\hat{K}_i$  contains only tune shifts, dampings and perhaps a set of resonances chosen by the user (one-resonance normal form).

This is done via the computation of a canonical transformation

$$\begin{aligned}
\mathcal{M}_{i+1} &= \exp(\hat{G}_i) \mathcal{M}_i \exp(-\hat{G}_i) \\
&= \exp(\hat{G}_i) \mathcal{R} \exp(\hat{K}_1) \cdots \exp(\hat{K}_{i-1}) \exp(\hat{F}_i) \exp(-\hat{G}_i) \\
&= \mathcal{R} \exp(\hat{K}_1) \cdots \exp(\hat{K}_i) \exp(\hat{F}_{i+1})
\end{aligned} \tag{73}$$

In the normal form algorithm,  $\hat{F}_i$  are computed via a logarithm at line !#7 and put in a spin eigenbasis at line !#8.

$\hat{G}_i$  and  $\hat{K}_i$  are computed iteratively in lines !#9, !#10, !#11 and !#12.

The final form of the normalized map after the iterative loop is:

$$\mathcal{M}_{no+1} = \exp(\hat{G}_{no}) \cdots \exp(\hat{G}_1) \mathcal{A}_2 \mathcal{A}_1 \mathcal{M} \mathcal{A}_1^{-1} \mathcal{A}_2^{-2} \exp(-\hat{G}_1) \cdots \exp(-\hat{G}_{no}) \tag{74}$$

$$\mathcal{M}_{no+1} = \mathcal{R} \exp(\hat{K}_1) \cdots \exp(\hat{K}_{no}) \tag{75}$$

This is shown at line !#14. When performing perturbation theory, it is natural for the canonical transformation to be in the reverse Dragt-Finn order. As for the kernel part  $\hat{K}_i$ , the order is more arbitrary.

## 10 Stochastic map

This is done at line !#17 and is most useful on linear maps. It computes the equilibrium beam sizes when there are stochastic fluctuations.

## 11 Final result

Eq. (75) can be rewritten as

$$\begin{aligned}
\mathcal{M}_{no+1} &= \mathcal{R} \exp(\hat{K}_1) \cdots \exp(\hat{K}_{no}) \\
&= \exp(\hat{H}_l) \exp(\hat{H}_{nl})
\end{aligned} \tag{76}$$

This is done at line !#18.

---

In the symplectic case, in the absence of resonances in the normal form, the full map can be represented by  $\widehat{H} = \widehat{H}_l + \widehat{H}_{nl}$ .

When resonances dominate the phase space, the one-turn map cannot be represented as a single Lie operator but a certain co-moving map sometimes can. This is important in orbital or spin resonance calculations.

## 12 Taylors and Polymorphs

The PP of FPP defines two fundamental structures that are the building blocks of many other structures: **taylor** and **complextaylor**. The **direct** use of either **taylor** or **complextaylor** in a tracking program ( in a simulation code like TC) is highly discouraged. Polymorphic types like **real\_8** and **complex\_8** should be used.

**taylor** and **complextaylor** are used via the polymorphic types **real\_8** and **complex\_8** in the tracking code TC. They are no longer used in AP. Indeed the analysis used in FPP uses the package **c\_dabnew.f90** which is a “complexification” of Berz’s **dabnew.f90**: it uses the complex Taylor **c\_taylor**. The glue between these two world is described in section (S7). These types delay the usage of a Taylor and this save memory: the program can decide during execution if a quantity is real or Taylor.

They are defined as follows:

```
type real_8
  type (taylor) t ! used if taylor
  real(dp) r ! used if real
!
  integer kind ! 1,2,3 (1=real,2=taylor,3=taylor knob )
  integer i ! used for knobs and special kind=0
  real(dp) s ! scaling for knobs and special kind=0
  logical(lp) :: alloc ! true if taylor is allocated in c_dabnew.f90 of Berz
end type real_8

type complex_8
  type (complextaylor) t -> t= t%r +i t%i are 2 real taylor
  complex(dp) r
  logical(lp) alloc
  integer kind
  integer i,j
  complex(dp) s
end type complex_8
```

### 12.1 The various Taylor types of the analysis package

We describe below the taylor (**taylor**) and complex Taylor (**complextaylor**) used in the polymorphs. They are all based on the real package of Berz: **dabnew.f90**.

---

### 12.1.1 Taylor Type

The **taylor** structure stores an integer which points to a stored Taylor (or element of  ${}_{no}D_{nv}$ ) in Berz's original package.

The structure is:

```
type taylor
  type (taylor) r      ! Real part of complex Taylor series.
  type (taylor) i      ! Imaginary part of complex Taylor series.
end type complextaylor
```

We can look at the function **add**, from **i\_tpsa.f90**, which overloads addition:

```
function add( s1, s2 )
  implicit none
  type (taylor) add
  type (taylor), intent (in) :: s1, s2
  integer localmaster
  if(.not.c_%stable_da) then
    add%i=0
    return
  endif
  localmaster=master

  call ass(add)

  ! Old Fortran77 called on the integer pointers of
  ! s1, s2 and add, all type taylor

  call daadd(s1%i,s2%i,add%i)

  master=localmaster
end function add
```

### 12.1.2 ComplexTaylor Type

The **complextaylor** structure stores two Taylor series which represent the real and imaginary parts. The structure is:

```
type complextaylor
  type (taylor) r      ! Real part of complex Taylor series.
  type (taylor) i      ! Imaginary part of complex Taylor series.
end type complextaylor
```

Again, showing the function **add**, from **l\_complex\_taylor.f90**, which overloads addition, is self-explanatory:

```
function add( s1, s2 )
```

---

```

implicit none
type (complextaylor) add
type (complextaylor), intent (in) :: s1, s2
integer localmaster
localmaster=master
call ass(add)

add%r=s1%r+s2%r ! adds using overloading
add%i=s1%i+s2%i

master=localmaster
end function add

```

### 12.1.3 C\_taylor Type

The **c\_taylor** structure stores Taylor series in the complexified version of Berz's TPSA package: **c\_dabnew.f90**. This type is used only in AP and in the glue between AP and TC. (See section §7.1)

The structure is:

```

type c_taylor
  integer i ! integer i is a pointer to the complexified berz package
end type c_taylor

```

Everything that was said about **taylor** in section (§12.1.1) applies to **c\_taylor** if one substitutes **c\_dabnew.f90** for Berz's package. In this new package, all the coefficients are **complex(dp)**.

## 12.2 Examples of the polymorphs **real\_8** and **complex\_8**

The Taylor series embedded in types **real\_8** and **complex\_8**, types **taylor** and **complextaylor** respectively, are all coming from the real package **dabnew.f90** of Berz.

A polymorph can be an ordinary floating point number, a Taylor series from **c\_dabnew.f90** or a knob which we will now describe. A knob is a latent simple Taylor:

$$t = t\%r + t\%s \Delta_{t\%i+nd2} \quad (77)$$

To understand these three instantiations of the **real8/complex\_8** types, we propose the code **z\_track\_real\_8.f90**. Consider these fragments from the program **z\_track\_real\_8.f90**:

#### 1. Creation of knobs

```

p=>ring%start
call move_to(ring,p,"QF1") ! Locating QF1 in TC
! PP : making a Polymorph into a knob
call make_it_knob(p%magp%bn(2),1)
p_QF1=>p

```



---

```

call move_to(ring,p,"QF2")      ! Locating QF2 in TC
call make_it_knob(p%magp%bn(2),2)
p_QF2=>p

write(6,*) ; write(6,*) "Printing knob 1  "
call print(p_QF1%magp%bn(2))
write(6,*) ; write(6,*) "Printing knob 2  "
call print(p_QF2%magp%bn(2))

```

## 2. Using knobs with no phase space

```

write(6,*) "A polyphorm powered by a knob : FPP no phase space maps "
x1=p_QF2%magp%bn(2)
write(6,*) " x1 "
call print(x1)
x2=p_QF2%magp%bn(2)+i_*p_QF1%magp%bn(2)
write(6,*) " x2"
call print(x2,6)
call kill(x1); call kill(x2);

```

## 3. Using knobs with phase space

```

no=2
nd=3
np=2
ndpt=0
knob=.true.
call c_init_all(no,nd,np,ndpt)
write(6,*) " Jordan Normal Form ", c_%ndpt

call alloc(x1); call alloc(x2);

write(6,*) "Taylors powered by a knob : FPP with phase space maps "
x1=p_QF2%magp%bn(2)
call print(x1)
x2=p_QF2%magp%bn(2)+i_*p_QF1%magp%bn(2)
call print(x2)
call kill(x1); call kill(x2);

```

## 4. Using knobs with phase space via PTC

```

call in_bmad_units()
bmad_state=default+time0      !+nocavity0

call init_all(bmad_state,no,np)
write(6,*) " Jordan Normal Form ", c_%ndpt

```

---

```

call alloc(x1);call alloc(x2);

call print(bmad_state)

write(6,*) "Taylors created by a knob : PTC with phase space maps "
x1=p_QF2%magp%bn(2)
call print(x1)
x2=p_QF2%magp%bn(2)+i_*p_QF1%magp%bn(2)
call print(x2)

```

## 5. Ignoring knobs PTC

```

knob=.false.
write(6,*) "Knobs are ignored "

x1=p_QF2%magp%bn(2)
call print(x1)
x2=p_QF2%magp%bn(2)+i_*p_QF1%magp%bn(2)
call print(x2)

call kill(x1);call kill(x2);

```

## 6. Removing knobs permanently

```

write(6,*) "Knobs are eliminated "
knob=.true.
if(p_QF1%magp%bn(2)%kind==3) p_QF1%magp%bn(2)%kind=1
if(p_QF2%magp%bn(2)%kind==3) p_QF2%magp%bn(2)%kind=1
x1=p_QF2%magp%bn(2)
call print(x1)
x2=p_QF2%magp%bn(2)+i_*p_QF1%magp%bn(2)
call print(x2)

```

### 12.2.1 Initializing a polymorph: fragment 1

All polymorphs must be initialized prior to their usage: this done with the call

```
call alloc(x1)
```

or in the depth of PTC by

```

subroutine zero_anbn_p(el,n)
  implicit none
  type(elementp), intent(inout) ::el
  integer, intent(in) ::n

  if(n<=0) return

```

---

```

    if(associated(el%an)) deallocate(el%an)
    if(associated(el%bn)) deallocate(el%bn)
    el%p%nmul=n
    allocate(el%an(el%p%nmul),el%bn(el%p%nmul))
    call alloc(el%an,el%p%nmul);      ! polymorphic an constructed
    call alloc(el%bn,el%p%nmul);      ! polymorphic bn constructed

end subroutine zero_anbn_p

```

This allocation is done, in the case of **an,bn**, prior to any call to the TPSA package. Polymorphs can be allocated as soon as the space in memory exists.

Next we create two knobs, for example,

```

p=>ring%start
call move_to(ring,p,"QF1")      ! Locating QF1 in TC
! PP : making a Polymorph into a knob
call make_it_knob(p%magp%bn(2),1)
p_QF1=>p

```

This implies that the quadrupole component **bn(2)** of the magnet QF1 can become the  $nd2 + 1$  variable of a Taylor series. If we run the code of item 1, we get:

```

Printing knob 1
  printing a real polymorph (real_8)
2.25384743526091+1.000000000000000(x_1)

Printing knob 2
  printing a real polymorph (real_8)
2.247400000000000+1.000000000000000(x_2)

```

This shows that the two polymorphs are latent Taylor series consistent with Eq. (77). Now we see how that is actualized in a real code.

### 12.2.2 Knobs with no phase space: item 2

Also the TPSA package must be initialized otherwise the code will not know the values  $no$  and  $nv$ : remember that the code tracks an element of the algebra  ${}_{no}D_{nv}$  (see section §5.4).

In fragment of item 2, as in section (§7.2), the call **c\_init\_all(no,nv)** creates polynomials in **nv** variables but **no** phase space, i.e.,  $nd2 = 0$ , therefore the parameters for **QF1** and **QF2** are respectively 1 and 2. The output from item 2 is:

```

A polyphorm powered by a knob : FPP no phase space maps
x1

etall      1, NO =      2, NV =      7, INA =      28
*****

      I  COEFFICIENT          ORDER  EXPONENTS
      NO =      2          NV =      7
0      2.247400000000000      0  0  0  0  0  0  0

```

```

1 1.0000000000000000 0 1 0 0 0 0 0
-2 0.0000000000000000 0 0 0 0 0 0 0
x2
Real Part

etall 1, NO = 2, NV = 7, INA = 35
*****
I COEFFICIENT ORDER EXPONENTS
NO = 2 NV = 7
0 2.2474000000000000 0 0 0 0 0 0 0
1 1.0000000000000000 0 1 0 0 0 0 0
-2 0.0000000000000000 0 0 0 0 0 0 0
Imaginary Part

etall 1, NO = 2, NV = 7, INA = 36
*****
I COEFFICIENT ORDER EXPONENTS
NO = 2 NV = 7
0 2.253847435260914 0 0 0 0 0 0 0
1 1.0000000000000000 1 0 0 0 0 0 0
-2 0.0000000000000000 0 0 0 0 0 0 0

```

We see that the knobs are the first and second variable of the Taylor series.

### 12.2.3 Knobs with phase space: item 3

In fragment of item 3, as in section (§7.2), the call `c_init_all(no,nd,np,ndpt=0)` creates polynomials in  $\mathbf{nv}=2*\mathbf{nd}+\mathbf{np}$  variables. The huge difference with the call from the previous section (§12.2.2) is the creation of a phase space of  $\mathbf{nd2}=2*\mathbf{nd}$  dimension,  $\mathbf{nd}$  degrees of freedom. According to Eq. (77), the position of knob 1 and 2 will be respectively 7 and 8.

The variable `ndpt` can be give the values 0, 5 or 6. It affects on the normal form. If `ndpt` is 0 (`ndpt` is optional, default=0), the 3 planes execute pseudo-harmonic oscillations and the normal form is 3 rotations. If the `ndpt` is 5 or 6, than the normal form is a drift-like matrix in the longitudinal plane. In that case, `ndpt` is the position of the energy-like variable. It is 6 in Bmad and that variable is  $\frac{\delta p}{p_0}$ . In this section, since there are no normal form displayed, this is completely irrelevant.

Here is the result of running item 3:

```

Taylors powered by a knob : FPP with phase space maps

etall 1, NO = 2, NV = 8, INA = 30
*****
I COEFFICIENT ORDER EXPONENTS
NO = 2 NV = 8
0 2.2474000000000000 0 0 0 0 0 0 0 0
1 1.0000000000000000 0 0 0 0 0 0 0 1
-2 0.0000000000000000 0 0 0 0 0 0 0 0
Real Part

```

```

etall 1, NO = 2, NV = 8, INA = 37
*****

I COEFFICIENT ORDER EXPONENTS
NO = 2 NV = 8
0 2.2474000000000000 0 0 0 0 0 0 0 0
1 1.0000000000000000 0 0 0 0 0 0 0 1
-2 0.0000000000000000 0 0 0 0 0 0 0 0
Imaginary Part

etall 1, NO = 2, NV = 8, INA = 38
*****

I COEFFICIENT ORDER EXPONENTS
NO = 2 NV = 8
0 2.253847435260914 0 0 0 0 0 0 0 0
1 1.0000000000000000 0 0 0 0 0 0 1 0
-2 0.0000000000000000 0 0 0 0 0 0 0 0

```

#### 12.2.4 Knobs with phase space via PTC: item 4

The result below is identical to that of section (§12.2.3). The difference lies in the way the FPP is activated. Here we pass a so-called **internal\_state**. First, in item 4, we see that main program invoked Bmad units: therefore energy will be the sixth variable. Secondly, by default, the cavity is turned on. This corresponds to the FPP call **c\_init\_all(no,nd,np,ndpt=0)**. If the **internal\_state** invokes **nocavity0**, then cavities are generally turned into drifts and this is equivalent to **c\_init\_all(no,nd,np,ndpt=6)** in Bmad units.

```

Jordan Normal Form 0
***** State Summary *****
MADTHICK=>KIND = 32 DRIFT-KICK-DRIFT
Rectangular Bend: input arc length (rho alpha)
Default integration method 2
Default integration steps 8
This is an electron (positron actually if charge=1)
EXACT_MODEL = TRUE
TOTALPATH = 0
RADIATION = FALSE
STOCHASTIC = FALSE
ENVELOPE = FALSE
NOCAVITY = FALSE
TIME = TRUE
FRINGE = FALSE
PARA_IN = FALSE
ONLY_2D = FALSE
ONLY_4D = FALSE
DELTA = FALSE
SPIN = FALSE
MODULATION = FALSE
RAMPING = FALSE
ACCELERATE = FALSE

```

---

Taylor's created by a knob : PTC with phase space maps

etall 1, NO = 2, NV = 8, INA = 30

\*\*\*\*\*

I	COEFFICIENT	ORDER	EXPONENTS
	NO = 2	NV = 8	
0	2.2474000000000000	0 0 0 0 0 0 0 0	0
1	1.0000000000000000	0 0 0 0 0 0 0 0	1
-2	0.0000000000000000	0 0 0 0 0 0 0 0	0

Real Part

etall 1, NO = 2, NV = 8, INA = 37

\*\*\*\*\*

I	COEFFICIENT	ORDER	EXPONENTS
	NO = 2	NV = 8	
0	2.2474000000000000	0 0 0 0 0 0 0 0	0
1	1.0000000000000000	0 0 0 0 0 0 0 0	1
-2	0.0000000000000000	0 0 0 0 0 0 0 0	0

Imaginary Part

etall 1, NO = 2, NV = 8, INA = 38

\*\*\*\*\*

I	COEFFICIENT	ORDER	EXPONENTS
	NO = 2	NV = 8	
0	2.253847435260914	0 0 0 0 0 0 0 0	0
1	1.0000000000000000	0 0 0 0 0 0 0 0	1
-2	0.0000000000000000	0 0 0 0 0 0 0 0	0

## 13 The `c_damap` type: fundamental to analysis

The `c_damap` type is given by:

```
type c_damap
! Orbital part
type (c_taylor) v(lnv) !@1 orbital part of the map
type(c_quaternion) q
! Stochastic part
complex(dp) e_ij(6,6) !@1 stochastic fluctuation in radiation theory
! Number of planes allocated
integer :: n=0 !@1 number of planes allocated
! Initial orbit if tpsa = true
complex(dp) x0(lnv)
logical :: tpsa=.false.
! Lie map matrix (Yu's square matrix)
complex(dp), pointer :: cm(:, :)=> null()
```

---

```

! Moment matrix (transpose of Yu Matrix)
real(dpn),pointer :: m(:,:)=> null()
! S0(3) is deprecated in FPP
! and computed from quaternion if needed
type(c_spinmatrix) s !@1 spin matrix
end type c_damap

```

### 13.1 The `c_` type: storing global data for AP

Before discussing the `c_damap`, we need to understand a few parameters that are crucial to that map and are global in AP. We can show a code fragment that prints them in particularly complex cases. This is from the main program `z_track_c_.f90`.

There are two basic ways to track in TC: the RF-cavity is on or the RF-cavity is off. Even when RF cavity are absolutely necessary, it is useful to compute a 6-d map with the RF cavity off, i.e., with  $\delta p = \text{constant}$ . Why?

`state=nocavity` In that case, it is possible, via simple normal form, to compute things like the chromaticities, the dispersions, the phase slip, etc... Strictly speaking these concepts are ill-defined in the presence of longitudinal oscillations. However they are approximately defined for a small synchrotron (longitudinal) tune which is the case in normal rings.

`state=default` In that case, the cavities are turned on. This is usually the “physical” case. It is necessary when extracting from the map the longitudinal tunes and the damping decrements due to radiation. PTC also computes the quadratic fluctuations  $\langle z_i z_j \rangle$ , 21 of them, from which beam sizes can be extracted. We can also extract the so-called “equilibrium” emittances which are also approximate concepts, i.e., valid in the limit of small damping.

Consider the following call:

```

p=>ring%start
call move_to(ring,p,"QF1")    ! Locating QF1 in TC
! PP : making a Polymorph into a knob
call make_it_knob(p%magp%bn(2),1,s=1.0_dp)
p_QF1=>p
call move_to(ring,p,"QF2")    ! Locating QF2 in TC
call make_it_knob(p%magp%bn(2),2,s=1.0_dp)
p_QF2=>p
.
.
no=2
nd=3
np=2
.
.
call in_bmad_units()
bmad_state=default+time      !+nocavity

```

---

```
call init_all(bmad_state,no,np)
```

This initializes FPP and AP in particular to track with cavities. The basic phase space will be 6 dimensional with 3 tunes. We print the relevant parts of **c\_**:

```
Taylor's created with two knobs : PTC with phase space maps
Cavities turned on
      c_%no = 2      ! Order of TPSA
      c_%nv = 8      ! Total number of variables
      c_%nd = 3      ! Orbital degrees of freedom
      c_%nd2 = 6     ! c_%nd2=2*c_%nd
      c_%nd2harm = 6  ! All oscillating planes including magnet modulation
      c_%ndpt = 0     ! Energy is not constant
      c_%ndpt_bmad = 1 ! Bmad units used
      c_%np = 2      ! Number of parameters
      c_%npara_fpp= 6  ! Position of parameters minus 1
      c_%nd2t= 6     ! Oscillating orbital planes
      c_%ndc2t= 0
      c_%pos_of_delta 6
      c_%rf= 0
      c_%setknob= T
      c_%knob= T
```

These numbers are all encoded in **bmad\_state=default+time**. Bmad by default using 3 degrees of freedom. Moreover, these 3 planes are oscillating with a cavity. This is encoded in **c\_%nd2t=6**. Notice that there are 8 variables total: 2 quadrupole strengths at location **c\_%npara\_fpp+1** and **c\_%npara\_fpp+2**.

Before we go into a detailed explanations of type **c\_damap**, we show a more complex call to **init\_all**. We run PTC with the **internal\_state**

```
.
.
call in_bmad_units()
!call in_ptc_units()
bmad_state=default+time0+nocavity0
bmad_state=bmad_state+modulation0+spin0
.
.
```

and then we get:

```
Taylor's created with 2 knobs : PTC with phase space maps
without a cavity and modulation on a magnet
      c_%no = 2
      c_%nv = 10
      c_%nd = 4
      c_%nd2 = 8
      c_%nd2harm = 6
      c_%ndpt = 6
```



---

```

c_%ndpt_bmad = 1
c_%np = 2
c_%npara_fpp= 8
c_%nd2t= 4
c_%ndc2t= 2
c_%pos_of_delta 6
c_%rf= 1
c_%setknob= T
c_%knob= T

```

The first thing we notice is that **c\_%ndpt=6**. This means that the sixth variable is the energy variable and is a constant. The orbital phase space has 6 dimensions. However we notice that the number of oscillating dimensions is 4, i.e., **c\_%nd2t=4** that is the two transverse orbital planes.

The total phase space is eight since **c\_%nd2=8** and thus the maps have 8 entries. This is because of the presence of a modulating magnet. Additional parameters, the two quadrupoles, must occupy the 9<sup>th</sup> and 10<sup>th</sup> variables. The total number of TPSA variables and indeed we have **c\_%nv=10**.

These numbers are necessary for AP. However this is automatically set up by the call to **init\_all(bmad\_state,no,np)**.

FPP does not attempt to do a forensic analysis of a map and then determine the right settings. Indeed if a map is created outside PTC, the user must either call **init\_all(state,no,np)** with the proper state or directly call **c\_init\_all**. For example, the above case can be reproduced by the pure AP call:

```

no=2
nd=4
np=2
ndpt=6
knob=.true.
ac_modulation=1
call c_init_all(no,nd,np,ndpt,ac_modulation)

```

Even if you do not use PTC, calls to initialize FPP via a PTC **internal\_state** like **bmad\_state** are far less cryptic.

## 13.2 The c\_damap in detail

The Taylor maps can be used for all sorts of purposes (see §7). But its main function, in TC proper, is analysis and **not** tracking. This is not true of “matrix” codes like COSY-INFINITY or MARYLIE where the ultimate object of the code is a one-turn Taylor map. In TC, the tracking is achieved normally by pushing through individual magnets using a variety of integrators. This is also true in the case of Bmad which not only includes PTC, but also also a collection of tracking methods which for the most part are integrators. For example, Bmad has a variable step Runge-Kutta method which handles complex magnets without the paraxial approximation, i.e., does not assume Hills equations.

---

It is true that most users of PTC seek it for its ability to produce Taylor maps, but it is fundamentally an integrator whose algebra is extended from  $(\mathbb{R}, +, \times)$  to  $({}_{no}D_{nv}, +, \times)$  via polymorphism. What it is and what it is used for — often confused by users — are two different things.

Here we concentrate on the DA map, i.e., a map around the closed orbit. All constant parts are ignored and that includes **c\_damap%*x0*** whose functions is described in section (§6.1) and Eq. (31): it is the  $w_0$  of map  $m_{w_0}$ .

The **c\_damap** contains primarily phase space and a quaternion:

```
type c_damap
! Orbital part
type (c_taylor) v(lnv) !@1 orbital part of the map
type(c_quaternion) q
.
.
```

The array **%*(lnv)*** contains the phase space variables. For example, in a normal Bmad run, it will contain the six polynomials for  $(x, p_x, y, p_y, -\beta ct, \delta)$ , the usual Bmad variables. If a “clock” is present for sinusoidal magnet modulation, then it will contain eight polynomials  $(x, p_x, y, p_y, -\beta ct, \delta, q_c, p_c)$ .

The type **c\_quaternion** is made of four **c\_taylor**:

```
type c_quaternion
type(c_taylor) x(0:3)
end type c_quaternion
```

Two DA **c\_damap**’s **S1** and **S2** are concatenated by the following code fragment:

```
function c_concat(s1,s2)
implicit none
type (c_damap) c_concat
type (c_damap), intent (in) :: s1, s2
t1=s1;t2=s2;

! code for s1 o s2
! removes the constant part since these are da maps
do i=1,t1%n
t1%v(i)=t1%v(i)-(t1%v(i).sub.'0')
enddo
do i=1,t2%n
t2%v(i)=t2%v(i)-(t2%v(i).sub.'0')
enddo

! calls to the concatenator in c_dabnew.f90
call c_etcct(t1%v%i,t1%n,t2%v%i,t2%n,tempnew%v%i)
! the constant part at the end of the orbit (not necessary)
if(add_constant_part_concat) then
do i=1,t1%n
tempnew%v(i)=tempnew%v(i)+(s1%v(i).sub.'0')
enddo
endif
```

---

```
t1%q = t1%q*t2 !!! substituting s2 into quaternion of s1
tempnew%q=t1%q*t2%q !!! multiplying quaternions
```

Symbolically, we can write the above code fragment as:

$$\begin{aligned}
c\_concat\%x &= S1\%x \circ S2\%x \\
c\_concat\%q &= \underbrace{\{S1\%q \circ S2\%x\}}_{\text{transformed quaternion}} \times S2\%q
\end{aligned} \tag{78}$$

The  $\times$  in Eq. (78) represents quaternion multiplication.

We know that the motion can also include radiation. The classical radiation, which is deterministic, is stored in the orbital map. However, the stochastic part, the quadratic fluctuation of the moments, is stored in `c_damap%e_ij(1:6,1:6)`. Denoting the linear part of **S1** and **S2** by the matrices **M1** and **S2**, we have:

$$c\_concat\%E_{ij} = M2 S1\%E_{ij} M2^\top + S2\%E_{ij} \tag{79}$$

Eq. (79) is realized by the code:

```
.
.
t1=t1.sub.1
m2=t1
m2t=transpose(m2)
tempnew%e_ij=t1%e_ij + matmul(matmul(m2,t2%e_ij),m2t)
```

Other parts of the `c_damap` are experimental. For example, in `c_damap%cm(:,:)` one can compute and store the matrix representation of the Lie map associated to the orbital map: this is a huge matrix acting on space of polynomials of order **no** and dimension **nv**. The huge matrix `c_damap%m(:,:)` is the matrix acting on moment. In a deterministic case, it is the transposed of `c_damap%cm(:,:)`.

These matrices are not used in AP for analysis. It is possible in theory to compute a normal form directly using the matrix `c_damap%cm(:,:)`, see [17] for example.

## 14 The normal form and the vector field

It is in the normal form where a lot of perturbation theory is embedded. This type can permit the extraction of any lattice function, linear and nonlinear. For example, it can **trivially** extract the dependence of the coupled Courant-Snyder invariants in terms of parameters including  $\delta p$  if energy is a constant. It can compute all quantities related to spin with equal ease using quaternions. Obviously it follows that phase advances for both the orbital and the spin are trivially constructed once these tools exist. This is the topic of Forest's new book [7] which unfortunately uses  $SO(3)$  instead of quaternions.

---

Normal forms can also leave a “single resonance” in the map. This is topologically equivalent to the one-resonance Hamiltonian theory. It can be done with either an orbital resonance or a spin resonance.

Here is the normal form structure. We skip variables of the structure which are obsolescent.

```

type c_normal_form
!!! full transformation with spin
  type(c_damap) atot ! for spin (m = atot n atot^-1)
  type(c_vector_field) h,h_l,h_nl
!!!envelope radiation stuff to normalize radiation (sand's like theory)
  complex(dp) s_ij0(6,6) ! equilibrium beam sizes
  complex(dp) s_ijr(6,6) ! equilibrium beam sizes in resonance basis
  complex(dp) b_ijr(6,6) ! stochastic kick in resonance basis
! equilibrium emittances as defined by chao
! (computed from s_ijr(2*i-1,2*i) i=1,2,3 )
  real(dp) emittance(3)
!! controls resonances left in normal form
! stores resonances to be left in the map, including spin (ms)
  integer nres,m(ndim2t/2,nreso),ms(nreso)
!! redundant stuff
! stores simple information
  real(dp) tune(ndim2t/2),damping(ndim2t/2),spin_tune,quaternion_angle
  logical positive ! forces positive tunes (close to 1 if <0)
  .
  .
  .
end type c_normal_form

```

## 14.1 The normal form type

See program [z\\_track\\_normal\\_tpsa.f90](#) for a simple call to the normal form.

The normal form rewrites a **c\_damap** as follows:

$$n = a^{-1} \circ m \circ a \quad (80)$$

where  $n$  is called a normal form. In the simplest case, in the presence of a cavity, the orbital map is an amplitude dependent rotation. If classical radiation is present, it is an amplitude dependent dilation (rotation and damping akin to a circular drain). The simplest call to achieve this is

```

type(c_normal_form) normal_form
type(c_damap) one_turn_map_AP
.
.
.
call c_normal(one_turn_map_AP,normal_form)

```

We deduce that in Fortran90, the equivalent of Eq. (80) is

---

```

type(c_normal_form) normal_form
type(c_damap) n , one_turn_map_AP
.
.
.
call c_normal(one_turn_map_AP,normal_form)
n=normal_form%a**(-1)*one_turn_map_AP*normal_form%a

```

The analysis AP has two global parameters of importance:

```

logical :: remove_tune_shift=.false.
complex(dp) :: n_cai=-2*i_

```

If the parameter **remove\_tune\_shift** is true, then in the case of a damped map, the code will attempt to remove all nonlinearities and create a linear sink. This is generally not recommended in accelerator physics since damping decrements are often very small. On a map without radiation, this will create a crash since division by zero will occur: it is impossible to remove tune shifts with amplitude by similarity transformations in the symplectic case.

The parameter **n\_cai** can be  $-i = -\sqrt{-1}$  or  $-2i$ . This parameter selects the phasors' definition which is the complex transformation which diagonalizes the linear part of  $n$  which is rotation. That is to say that matrix part of  $n$ , denoted  $N$ , obeys, in 1-d-f:

$$\Lambda = C^{-1}NC \quad \text{where} \quad R = \begin{pmatrix} e^{-i\mu} & 0 \\ 0 & e^{i\mu} \end{pmatrix} \quad (81)$$

If **n\_cai** =  $-2i$ , then

$$\begin{aligned} \text{map } c^{-1} : x^{new} &= x + ip \\ p^{new} &= x - ip \end{aligned} \quad (82)$$

Notice that the Poisson bracket  $[x^{new}, p^{new}] = n_{cai} = -2i$ . More importantly, we have for Eq. (82):

$$x^{new} p^{new} = x^2 + p^2 = 2J \quad (83)$$

If on the other hand **n\_cai** =  $-i$ , then we have:

$$\begin{aligned} \text{map } c^{-1} : x^{new} &= \frac{1}{\sqrt{2}}(x + ip) \\ p^{new} &= \frac{1}{\sqrt{2}}(x - ip) \end{aligned} \quad (84)$$

$$\text{and } [x^{new}, p^{new}] = -i \quad (85)$$

with

$$x^{new} p^{new} = x^2 + p^2 = J \quad (86)$$

It can be argued that the choice **n\_cai** =  $-i$  is the best since the action is simply the product of the phase space variables.

---

In phasors, the full normalized map is:

$$d = c^{-1} \circ n \circ c = c^{-1} \circ a^{-1} \circ m \circ a \circ c \quad (87)$$

The maps  $c$  and  $c^{-1}$  are obtained using the function **c\_phasor()** and **ci\_phasor()** respectively.

## 14.2 The type **c\_vector\_field** type and Lie maps

The normal form is defined, in FPP, via vector fields:

```
type c_vector_field
! n dimension used v(1:n) (nd2 by default) ;
! nrmax some big limiting integer to use for exponentiation
integer :: n=0,nrmax
! if eps=-integer then |eps| # of lie brackets are taken
! otherwise eps=eps_tpsalie=10^-9
real(dp) eps
! orbital part
type (c_taylor) v(lnv)
! quaternion part
type(c_quaternion) q
end type c_vector_field
```

The type **c\_quaternion** is defined as

```
type c_quaternion
type(c_taylor) x(0:3)
end type c_quaternion
```

A general quaternion is defined from type **c\_quaternion** as

$$q = q\%x(0) + q\%x(1)b_1 + q\%x(2)b_2 + q\%x(3)b_3 \quad (88)$$

$$\text{where } b = (i, j, k) \quad (89)$$

$i, j$  and  $k$  are the 3 usual quaternions which define the quaternion algebra.

In FPP, the action of a **c\_vector\_field** on a

$$F = F\%\vec{v} \cdot \vec{\nabla} + F\%q = F\%v(i)\partial_i + F\%q \quad (90)$$

where in Eq. (90) it is summed over the index  $i$ .

A general vector field as in Eq. (90), acts on a map  $m$  as follows:

$$\begin{aligned} (Fm)\%x(k) &= F\%v(i)\partial_i m\%x(k) \\ (Fm)\%q &= F\%v(i)\partial_i m\%q + m\%q \times F\%q \end{aligned} \quad (91)$$

---

A map near the identity always have a vector field representation. So if  $m$  is near the identity

$$\exists F \quad m = \exp(F) I \quad \text{where } I \text{ is the identity map} \quad (92)$$

If we have a function  $f$  of phase space, then the Lie maps have the following “virtue”:

$$\text{if } m = \exp(F) I \implies f \circ m = \exp(F) f \quad (93)$$

Eq. (93) implies that transforming a function by a map  $m$  can be done with a Lie operator. It also implies that a Lie operator is a “compositional” map.

Here is a list of operation using the vector field.

Now we define the normal form in terms of Lie operators.

### 14.3 The Lie operator of the normal form

The map  $d$  of Eq. (87) is, in the simplest symplectic case, an amplitude dependent rotation. Using Dragt’s notation for Lie maps (calligraphic font), we can write the Lie map associated to  $d$ , i.e.,  $\mathcal{D}$  as :

$$\mathcal{D} = \exp(H \cdot \nabla + q) \quad (94)$$

where

$$\begin{aligned} q &= \cos(\theta/2) + \sin(\theta/2) \\ \theta &= \theta(J_1, \dots, J_{nd}) \text{ and } J_i = z_{2i-1} z_{2i} \text{ per Eq. (86)} \end{aligned} \quad (95)$$

and

$$H_1 \partial_1 = -iz_1 \mu_1(J_1, \dots, J_{nd}) \partial_1 \quad \text{and} \quad H_2 \partial_2 = iz_1 \mu_1(J_1, \dots, J_{nd}) \partial_2 \quad (96)$$

In the case of damping, a real piece is added to Eq. (96):

$$\text{real part} = -z_1 \alpha_1(J_1, \dots, J_{nd}) \partial_1 \quad \text{and} \quad H_2 \partial_2 = -z_1 \alpha_1(J_1, \dots, J_{nd}) \partial_2 \quad (97)$$

Finally in the absence of a cavity, the longitudinal normal form, in the Bmad units, have the form:

$$H_5 \frac{\partial}{\partial z_5} = z_6 \phi(J_1, J_2; z_6) \partial_1 \quad \text{and} \quad H_6 = 0 \quad (98)$$

In Eq. (98),  $\phi$  is the phase/time slip.  $z_5$  is the time in the units of Bmad and  $z_6$  is  $\frac{\delta p}{p_0}$  — a conserved quantity.

The **c\_vector\_field** of Eq. (94) is stored in the field **c\_normal\_form%H**.

It is also possible to leave a resonance in the map via a normal form: please look into reference[7]. If the normal form  $\mathcal{D}$  is not a rotation then in FPP it can be written as

$$\mathcal{D} = \exp(H_{nl} \cdot \nabla + q_{nl}) \exp(H_l \cdot \nabla + q_l) \quad (99)$$

These vector fields are stored in **c\_normal\_form%h\_nl** and **c\_normal\_form%h\_l**.

---

## 14.4 Call to the normal form

```
subroutine c_normal(xyso3,n,dospin,no_used,rot,phase,nu_spin,canonize)

type(c_damap) , intent(inout) :: xyso3      ! map to be normalized
type(c_normal_form), intent(inout) :: n
type(c_damap), optional :: rot ! normal form rot=n%Atot**(-1)*xy*n%Atot
type(c_taylor), optional :: phase(:),nu_spin
logical(lp), optional :: dospin,canonize
integer,optional :: no_used
```

**dospin** is false by default: spin is ignored. In the symplectic case, **phase(1:nd)** will contain the tunes. If the last plane, 3 in Bmad, is not oscillating, this contains the time slip. If **canonize** is true, the map **n%atot** is put in a special form, i.e., the Courant-Snyder-Teng-Edwards form in the linear case (see [7]).

The normalization is done to order **no** of the algebra  $_{no}D_{nv}$ . But we can perform the normalization to lower order: this is specified by **no\_used**. To perform a normalization to higher order than **no** is possible but it is very unusual: for that the map has to be stored in a “**c\_universal\_taylor**” and then the TPSA package has to be re-initialized to higher order.

Finally the type **c\_normal\_form** has structures which can be modified in order to change the calculation. Here is the list assuming that **n** is a **c\_normal\_form**:

- If **n%nres=0**, the maps are turns into rotations and perhaps a time slip if no cavity are present.
- If **n%nres/ = 0**, then **n%nres** resonances, labelled by  $k$ , are left in the map:

$$n\%m(1,k)v_1 + \dots + n\%m(ndharm,k)v_{ndharm} + n\%ms(k)v_{spin} = \text{integer} \quad (100)$$

**ndharm** is the number of oscillating plane, typically 2 or 3 in Bmad. If a magnet is modulated, then **ndharm** is increased by 1, the tune of the modulation enters in the modulation.

- If **n%positive=.false.**, the fractional part of the tune stored in **n%tune** is between  $-1/2, 1/2$ . This does not apply to the time/phase slip. This is useful in “one-resonance” normal form.
- **force\_spin\_input\_normal** is a global which is normally false. If true, it makes the optional parameter **dospin** obligatory.
- As pointed out above, the parameter **remove\_tune\_shift** is false by default. On a very damped map, one can set this parameter to true. The normal form is a linear sink around the origin. It is not recommended in accelerators.

## 14.5 Factorizing the map **n%atot**

Any Taylor map  $a$  can be factorized as follows:

$$a = a_0 \circ a_1 \circ a_2 \circ a_s \text{ if } \text{dir} = 1 \quad (101)$$

using the command



---

```
!# at = a_0 o a_1 o a_2 o a_s for dir=1
call c_full_factorise(at,as,a0,a1,a2,dir=1)
```

If **dir=-1**, the order is reverse.

This factorization is general. However we can explain it in the context of a normal form where it is useful for finding the lattice functions around the parameter dependent closed orbit.

$$\begin{aligned}
n &= a^{-1} \circ m \circ a \\
&= a_s^{-1} \circ a_2^{-1} \circ a_1^{-1} \circ \underbrace{a_0^{-1} \circ m \circ a_0}_{m_c} \circ a_1 \circ a_2 \circ a_s \\
&= a_s^{-1} \circ a_2^{-1} \circ \underbrace{a_1^{-1} \circ m_c \circ a_1}_{n_c} \circ a_2 \circ a_s
\end{aligned} \tag{102}$$

1. The map  $a_0$  is the identity in the harmonically oscillating parts of phase space, either 4 (no cavity) or 6 (with RF cavity). It brings the map to the parameter dependent fixed point where  $\delta$ , if constant, is included.
2. The map  $a_1$  turns the linear part of the map around the fixed , to all orders in the parameters, into a rotation.
3. The map  $a_2$  is purely nonlinear.

An example of this useful call is in program **z\_track\_normal\_fact.f90** . This example computes the so-called beta function in two different ways using  $a_1$ , First it defines  $a_1$  as the coefficient of  $p_x^2$  in the quadratic invariant. Secondly it defines it has the coefficient of  $J_1$  in the computation of  $\langle x^2 \rangle$ . In the Ripken formalism, these are the same functions.

```
!# normal_form%atot = a_0 o a_1 o a_2 o a_s for dir=1
call c_full_factorise(normal_form%atot,as,a0,a1,a2,dir=1)

! computing the "beta function" two different ways
! x^2+p^2 is invariant of normal form n
ct=(1.d0.cmono.'2')+(1.d0.cmono.'02')
! (x^2+p^2) o a^-1 is invariant around the fixed point
ct=ct*a1**(-1)
allocate(jindex(c_%nd2harm))
call clean(ct,ct,prec=prec)
jindex=0
jindex(2)=2
ct=ct.par.jindex
Write(6,*) "Beta via Coefficient of p^2 in invariant"
call print(ct)
! function x^2 is constructed
ct=(1.d0.cmono.'2')
! function x^2 is averaged using a_1
call C_AVERAGE(ct,a1,ct)
jindex=0
```

```

jindex(1)=1
jindex(2)=1
! coefficient of J_1 extracted
ct=ct.par.jindex
call clean(ct,ct,prec=prec)
write(6,*) " Beta via average "
call print(ct)

```

The result if **no=3** is:

```

Beta via Coefficient of p^2 in invariant

      1, NO =      3, NV =      7, INA = 209
*****

      I  COEFFICIENT          ORDER  EXPONENTS
      NO =      3      NV =      7
0    13.57348336645041      0.0000000000000000      0 0 0 0 0 0 0
1    25.47460380089213      0.0000000000000000      0 0 0 0 1 0 0
1   -7.011940286158579      0.0000000000000000      0 0 0 0 0 1 0
1    0.9489986322495689      0.0000000000000000      0 0 0 0 0 0 1
-4    0.0000000000000000      0.0000000000000000      0 0 0 0 0 0 0
Beta via average

      1, NO =      3, NV =      7, INA = 209
*****

      I  COEFFICIENT          ORDER  EXPONENTS
      NO =      3      NV =      7
0    13.57348336645041      0.0000000000000000      0 0 0 0 0 0 0
1    25.47460380089214      0.0000000000000000      0 0 0 0 1 0 0
1   -7.011940286158588      0.0000000000000000      0 0 0 0 0 1 0
1    0.9489986322495378      0.0000000000000000      0 0 0 0 0 0 1
-4    0.0000000000000000      0.0000000000000000      0 0 0 0 0 0 0

```

## 14.6 Putting a transformation in “canonical” form

If the normal form  $n$  is free of resonance driving terms, then it commutes with any similar normal forms. This means that we can multiply  $a$  by a rotation (phase slip and/or damping depending on the case).

$$n = a^{-1} \circ m \circ a \Rightarrow n = r^{-1} \circ a^{-1} \circ m \circ \underbrace{a \circ r}_{a_c} \quad (103)$$

In accelerator physics, we often desire a special form for the canonical transformation  $a$ . This special form is of special significance in the linear case, i.e., the map  $a_1$  of (§14.5). Namely, we require that the matrix of  $a_c$ , denoted by  $A$ , obeys:

$$A_{12} = A_{34} = 0 \text{ and } A_{11}, A_{33} > 0 \quad (104)$$

If we select the transformation  $a_c$  according to Eq. (104), then the phase difference of two position

---

monitors will be the Hamiltonian phase advance. There is no known extension of this property<sup>9</sup> to the nonlinear problem: FPP, for the nonlinear part, selects  $a$  using an arbitrary construction explained in reference [7].

Obviously if the longitudinal plane is oscillating, the same condition can be applied :  $A_{56} = 0$ . In the case of a phase slip, we do something else (See routine . **extract\_a0** in **Ci\_tpsa.f90** or section 7.3 of reference [7]).

We refer to Eq. (104) as the Courant-Snyder(-Teng-Edwards)'s condition. As for the other planes, spin and nonlinear effects, our choice is, at present, arbitrary (see reference [7]).

There are two calls to “canonize”: a nonlinear routine and a faster linear routine for standard usage.

### 14.6.1 Nonlinear Call

The full call is given by:

```

type(c_damap) a0,as,a1,a2,a_cs,rot,a_tracked
type(c_taylor) phase(3),phase_spin
.
.
.

! Usual computation of a Taylor maps within TC
ray_TC=x0 ! For TC
identity_AP=1
ray_8_TC=ray_TC + identity_AP ! Connect AP with TC: identity added

p=>ring%start
call propagate(ray_8_TC,bmad_state,fibre1=p) ! TC of PTC proper

one_turn_map_AP=ray_8_TC

! compute 2 tunes and the phase slip
call c_normal(one_turn_map_AP,normal_form,phase=phase,dospin=bmad_state%spin) ! #1

write(6,*) "Transverse tunes "
write(6,"(3(1x,g17.10,1x))") normal_form%tune(1:c_%nd)

!!!! Canonize !!!!!
phase(1)=0.d0
phase(2)=0.d0
phase(3)=0.d0
phase_spin=0.d0

call c_full_canonise(normal_form%atot,a_cs) ! initial A ! #2
! Usual computation of a Taylor maps within TC
ray_TC=x0 ! For TC

```

---

<sup>9</sup>It should be possible to investigate this in 1-d-f without too much trouble.

---

```

ray_8_TC=ray_TC + a_cs ! Connect AP with TC: identity added

p=>ring%start
call propagate(ray_8_TC,+bmad_state,fibre1=p,fibre2=p2) ! TC of PTC proper ! #3a
a_tracked=ray_8_TC

.
.
.
call c_full_canonise(a_tracked,a_cs,as=as,a0=a0,a1=a1,a2=a2,rotation=rot & ! #3b
,phase=phase,nu_spin=phase_spin)

```

The map **a\_tracked** is now:

```
a_tracked=as*a0*a1*a2*rot=a_cs*rot
```

In the above code fragment, which is in **z\_track\_normal\_fact.f90**, there three important steps.

1. At # 1, the one-turn map is normalized. In FPP, the normalization map is **normal\_form%atot**. No special attention is given to that map except that it produces a normal form.
2. At # 2, the map is put in a special form denoted **a\_cs**. In the linear case, it is given by Eq. (104).
3. At # 3a, the canonical transformation **a\_cs** is tracked by the code PTC from **fibre1** to **fibre2**. It is extremely important to realize that what PTC is in detail, what a fibre is in detail is irrelevant. The code PTC could be full of bugs, full of errors of physics, etc... This particular call works for any tracking code— in fact people reading this manual should try writing a little code and convince themselves.
4. At # 3b, the object tracked by the code PTC, after having been converted into a **c\_damap**, is now rotated into the form of Eq. (104). The angles of that rotation, here **rot**, are the phase advances (or time slip) between the positions represented by **fibre1** and **fibre2**. They are stored in **phase(1:3)** and **phase\_spin**.

#### 14.6.2 Linear fast call phase\_spin and type c\_linear\_map

For a typical calculation, we want to be fast. For this purpose we have a type **c\_linear\_map**.

```

type c_linear_map
  complex(dp) mat(6,6)      ! orbital
  complex(dp)  q(0:3,0:6)   ! spin
end type c_linear_map

```

The field **c\_linear\_map%q** contains the four quaternions components in **q(0:3,0)**. The orbital dependence is in **q(0:3,1:6)**.

```
call c_fast_canonise(normal_form%atot,a_cs,dospin=bmad_state%spin)
```

---

```

p2=>ring%start
call move_to(ring,p2,"SF",reset=.true.)    ! Locating SF in TC

! Usual computation of a Taylor maps within TC
ray_TC=x0    ! For TC
ray_8_TC=ray_TC + a_cs ! Connect AP with TC: identity added

p=>ring%start

call propagate(ray_8_TC,bmad_state,fibre1=p,fibre2=p2) ! TC of PTC proper

a_tracked=ray_8_TC

call c_fast_canonise(a_tracked,a_cs,phase=pha,damping=damp,q_cs=q_cs, &
q_as=q_as,q_orb=q_orb,q_rot=q_rot,spin_tune=spin_tune ,dospin=bmad_state%spin)

end type c_linear_map

```

## 15 Normalizing a Hamiltonian representing a ring

**N.B.** The general theory is in sections 8.4, 8.6 and 8.7 of reference [7]. This theory was developed for orbital motion but is formally identical thanks to our use of vector field operators.

It is possible using the logarithm described in §4.2 to create a Hamiltonian operator for the ring. The first step is to normalize the linear part. This is the starting point in standard text books.

$$\begin{aligned}
\widehat{H}_\theta &= -i \underbrace{\sum_{a=1,3} \nu_a \{z_{2a-1} \partial_{2a-1} - z_{2a} \partial_{2a}\}}_{\text{transverse tunes}} + \underbrace{\sum_{a=1,3} \frac{-\alpha_a}{2\pi} \{z_{2a-1} \partial_{2a-1} + z_{2a} \partial_{2a}\}}_{\text{damping}} + \frac{1}{2} \nu_{\text{spin}} \widehat{j} + \widehat{V}_\theta \\
&\quad \text{Linear Part } \widehat{H}_0 \\
&= - \underbrace{\sum_{a=1,3} \nu_a : J_a :}_{\text{transverse tunes}} + \underbrace{\sum_{a=1,3} \frac{-\alpha_a}{2\pi} \{z_{2a-1} \partial_{2a-1} + z_{2a} \partial_{2a}\}}_{\text{damping}} + \frac{1}{2} \nu_{\text{spin}} \widehat{j} + \widehat{V}_\theta \tag{105}
\end{aligned}$$

The Hamiltonian in Eq. (105) can be obtained via a Twiss loop as described in the blue book [7]. Here is a list of important point:

1. The Hamiltonian of Eq. (105) is in term of an angle  $\theta$  running from 0 to  $2\pi$ . In textbooks, there is always an assumption that  $\theta$  must be related to some continuous  $s$  and/or the Courant-Snyder phase advance. This is not necessary. There is an infinite number of ways to relate  $\theta$  to an actual position in the ring.

- 
2. In conjunction with the above comment, special care<sup>10</sup> must be exercised if zero-length transformations are used. This can be the case for fringe fields or misalignments represented by operators at the ends of magnets. It is also the case if one uses thin lens multi-poles.
  3. It also follows that the total tunes  $\nu_i$  can have an absolutely arbitrary integer part. In the example of this manual, we demonstrate this. In general, one has to be careful in selecting the integer part.

## 15.1 Computation of $\widehat{H}_0$ and $\widehat{H}_\theta$

We start with the fundamental Twiss loop explained in [7]. Here  $i$  and  $i + 1$  are positions in the ring, normally successive integration steps. But this is arbitrary. If there are  $n$  such steps around the ring, the phase advance per step will be  $1/n^{th}$  of the total tune.

$$A_{i+1} = \underbrace{L_{i+1} \circ A_i}_{\text{from tracking}} \circ R_{i+1}^{-1} \quad (106)$$

In a standard Twiss, we know that  $A_{i+1}$  should be in a standard form, say Courant-Snyder, we then rotate the result of tracking the initial  $A_i$  until  $A_{i+1}$  has the Courant-Snyder form. Here  $L_{i+1}$  is the linear part of the tracked map.

Here, we do the opposite: we assume that the rotation is  $1/n^{th}$  of the total tune and we then determine  $A_{i+1}$  which is certainly not in a Courant-Snyder form. This is explained in chapter 8 of the blue book[7]. In standard textbooks, like that of S.Y. Lee[12], it is done via generating functions: this completely fails if we need to introduce quaternions and/or radiation damping. In the present of damping, the map  $R_{i+1}$  is a rotating sink.

Now let us apply Eq. (106) to the full nonlinear map. If we track with order higher than one, then Eq. (106) becomes:

$$U = R_{i+1} \circ N_{i+1} = A_{i+1}^{-1} \circ \underbrace{M_{i+1} \circ A_i}_{\text{from tracking}} \quad (107)$$

Here is the code snippet. Notice that lines 16a and 16b computes Eq. (106) using the Lie operator of the linear part and hence the reverse order. The second line cuts from the result terms higher than linear in orbital and higher than zeroth order in quaternion. The rest, 16c, computes Eq. (107).

```
U=ray !copying the tracking result {M}_{i+1} o {A}_{i} into a map U (15):

U_c=exp(-dtheta*H0_hat,U)      ! (16a)
U_c=U_c.cut.(-2)              ! (16b)
```

---

<sup>10</sup>Forest forgot about this and spent a long time looking for an unexisting bug in the example code of this manual.

---


$$U = U_c^{**(-1)} * U \quad ! \quad (16c)$$

$$H_{\theta} = \ln(U) \quad ! \quad (17)$$

The Lie map associated to  $U$ ,  $\mathcal{U}$  is given by

$$\mathcal{U} = \exp(\widehat{H}_{\theta}) = \exp(H_{\theta} \cdot \nabla + \widehat{h}_{\theta}) \quad (108)$$

which is the missing part of Eq. (105). Notice that the logarithm is almost guaranteed to converge since the map  $U$  must be near the identity since it represents no more than a full magnet.

## 15.2 Fourier transformation of $\widehat{H}_{\theta}$

$$\text{if } \widehat{V}_{\theta} = \sum_{k=-n_{mode}, n_{mode}} \exp(ik\theta) \widehat{V}_k \quad (109a)$$

$$\text{then } \widehat{V}_k = \frac{1}{2\pi} \sum_{j=1, n_s} \exp(-ik\theta) \widehat{V}_{\theta} \quad \text{where } \theta = j \frac{2\pi}{n_s} \quad (109b)$$

Below is code fragment for the Fourier transform of  $\widehat{H}_{\theta}$  which is the sum of the linear part  $\widehat{H}_0$  and the Fourier transform of  $\widehat{V}_{\theta}$ :

```
theta=theta+dtheta;
do n=-n_mode, n_mode
  H%f(n)=H%f(n)+(exp(-i_*n*theta)/twopi)*H_theta ! (19)
enddo

ray=ray_closed+U_c
```

As pointed out before, if there are thin lens objects or entire objects that can be “skipped” like arcs with near integer phase advance, then the relationship between  $\theta$  and the actual position in the ring can be tricky. In the example of this section, the relationship is essentially an ideal distance proportional to  $\theta$ . This is more or less the textbook case as in reference [12].

## 15.3 Useful formulae for evaluating the effect of a vector field via the Lie bracket

### 15.3.1 Using a phase space map

Consider the Lie map  $\mathcal{A}$  operator associated with the phase space map  $A = (a, \alpha)$ . It acts on a phase space map  $M = (m, q)$  following the formula:

$$\mathcal{A}(m, q) \& = (m, q) \circ (a, \alpha) = (m \circ a, \{q \circ a\} \alpha) \quad (110)$$

---

This is the type of map produced by PTC and created via FPP (type **c\_damap**).

How does a vector field  $\widehat{H}$  transforms under the map  $\mathcal{A}$ ? This has to be done by a similarity transformation:

$$\mathcal{A} \left( H \cdot \nabla + \hat{h} \right) \mathcal{A}^{-1} = G \cdot \nabla + \hat{g} \quad (111)$$

The answer for  $G$  and  $g$  is:

$$\begin{aligned} G_k &= \left( H_i \partial_i a_k^{-1} \right) \circ a \\ g &= \left( G_k \partial_k \alpha^{-1} \right) \alpha + \alpha^{-1} h \circ a \alpha \end{aligned} \quad (112)$$

This is not proven anywhere in the literature. The orbital part can be found in accelerator texts books, Michelotti and Forest for example. It is a standard result of mathematical physics. Eq. (112) is fully implemented in FPP.

### 15.3.2 Using a Lie map

We first assume that  $\mathcal{A}$  of Eq. (111) is given by:

$$\mathcal{A} = \exp \left( \widehat{F} \right) = \exp \left( F \cdot \nabla + \hat{f} \right) \quad (113)$$

Then by standard operator theory, we have:

$$G \cdot \nabla + \hat{g} = \exp \left( \widehat{F} \right) \widehat{H} = \sum_{n=0}^{\infty} \frac{\widehat{F}^{\#n}}{n!} \widehat{H} \quad \text{where } \widehat{F}^{\#} \widehat{H} = \left[ \widehat{F}, \widehat{H} \right] = \widehat{\langle F, H \rangle} \quad (114)$$

We must evaluate the commutator of the Lie operators  $\widehat{F}$  and  $\widehat{H}$  in terms of their Lie bracket  $\langle F, H \rangle$ :

$$\begin{aligned} \left[ \widehat{F}, \widehat{H} \right] &= \left[ F \cdot \nabla + \hat{f}, H \cdot \nabla + \hat{h} \right] \\ &= K \cdot \nabla + \hat{k} \end{aligned} \quad (115)$$

The answer for  $\widehat{K}$  is:

$$\begin{aligned} K &= \langle F, H \rangle = F \cdot \nabla H - H \cdot \nabla F \\ k &= hf - fh + F \cdot \nabla h - H \cdot \nabla f \end{aligned} \quad (116)$$

Where the orbital part of the Lie bracket can be written as:

$$K = \langle F, H \rangle = F_b \frac{\partial H}{\partial z_b} - H_b \frac{\partial F}{\partial z_b} \quad (117)$$



---

In FPP, we define a generalized Lie bracket between the vectors and the quaternions defining the Lie operators:

$$\underbrace{(K, k) = \langle (F, f), (H, h) \rangle}_{\text{FPP's c\_vector\_field}} \quad (118)$$

## 15.4 Transforming $\widehat{H}_\theta$ by a Lie map $\exp(\widehat{F}_\theta)$

We need to transform the  $\theta$  dependent operator  $\widehat{H}_\theta$  by a  $\theta$  dependent periodic transformation where  $\theta$  measures a position around a ring typically. If we use Lie operators, the answer does not depend on the actual form of the Lie operator. So the results of equations 8.28 and 8.29 of section 8.7.1 of reference [7] are correct as is.

Therefore if

$$\mathcal{A}_\theta = \exp(\widehat{F}_\theta) \quad \text{where} \quad \widehat{F}_\theta = \vec{F}_\theta \cdot \nabla + \widehat{f}_\theta \quad (119)$$

then

$$\widehat{K}_\theta = \exp\left(\widehat{F}_\theta\right) \widehat{H}_\theta - \sum_{n=1}^{\infty} \frac{\widehat{F}_\theta^{\#n-1}}{n!} \frac{\partial \widehat{F}_\theta}{\partial \theta} \quad (120a)$$

$$= \exp\left(\widehat{F}_\theta\right) \widehat{H}_0 + \exp\left(\widehat{F}_\theta\right) \widehat{V}_\theta - \sum_{n=1}^{\infty} \frac{\widehat{F}_\theta^{\#n-1}}{n!} \frac{\partial \widehat{F}_\theta}{\partial \theta} \quad (120b)$$

where

$$\underbrace{\widehat{F}_\theta^{\#} \widehat{H}_\theta}_{\text{Dragt's notation}} = ad_{\widehat{F}_\theta} \widehat{H}_\theta = \widehat{F}_\theta \widehat{H}_\theta - \widehat{H}_\theta \widehat{F}_\theta$$

$$= \langle (F_\theta, f_\theta), (H_\theta, h_\theta) \rangle \quad \leftarrow \text{Eq. (118) implemented in FPP} \quad (121)$$

In Eq. (120b), the Lie bracket must be the Lie bracket including the quaternion operator. The normal form proceeds order by order as in any perturbative scheme— spin or no spin.

In FPP, Eq. (120b) is performed by a call to a subroutine:

```
call exp_vector_field_fourier(F_theta, H_theta, H_theta)
```

It makes sense to call the entire operation of Eq. (120b) an “exponential” since this equation is derived by “extending state space” to include  $\theta$  as a state variable. In that case, the normal exponential of a Lie map applies.

---

## 15.5 The actual iterative step of the normal form

For simplicity we do the calculations of this section in one degree of freedom (1-d-f) and later extend the results to a higher number of dimensions.

We expand Eq. (120b) and retain the leading order terms in  $F_\theta$  and  $V_\theta$ . Here  $H_0$  is the orbital vector field and  $h_0$  is the quaternion part:

$$(\Delta_\theta, \delta_\theta) = \langle (F_\theta, f_\theta), (H_0, h_0) \rangle + (V_\theta, v_\theta) + \left( \frac{\partial F_\theta}{\partial \theta}, \frac{\partial f_\theta}{\partial \theta} \right) \quad (122)$$

These operators can be Fourier expanded:

$$F_\theta = (F_\theta^1, F_\theta^2) \quad F_\theta^{1,2} = \sum_{m,n,k} F_{m,n,k}^{1,2} z_1^m z_2^n \exp(ik\theta) \quad (123a)$$

$$f_\theta = \sum_{m,n,k,\ell=-1,0,1} f_{m,n,k}^\ell z_1^m z_2^n e^{ik\theta} e_\ell \quad (123b)$$

and, of course, a similar expansion for the potential operator  $\widehat{V}_\theta$ .

The  $e_i$ 's are eigen-quaternions of the operators made from the original quaternions  $q_i$ 's:

$$\begin{aligned} \text{if } q_i &= \varepsilon_{ijk} q_j q_k \\ &\text{then we define } e_i' \text{ as} \\ e_1 &= \frac{1}{2} (q_1 + iq_3) \\ e_0 &= q_2 (= j) \\ e_{-1} &= \frac{1}{2} (q_1 - iq_3) \\ \text{then } \widehat{je}_1 &= e_1 q_2 - q_2 e_1 = -ie_1 \\ \widehat{je}_0 &= 0 \\ \widehat{je}_{-1} &= ie_{-1} \end{aligned} \quad (124)$$

We then expand Eq. (122) and separate the orbital and quaternion parts to leading order:

$$\Delta_\theta = \langle F_\theta, H_0 \rangle - \frac{\partial F_\theta}{\partial \theta} + V_\theta \quad (125a)$$

$$\delta_\theta = h_0 f_\theta - f_\theta h_0 - H_0 \cdot \nabla f_\theta + \underbrace{F_\theta \cdot \nabla h_0}_{=0} \quad (125b)$$

We now set the orbital part  $\Delta_\theta$  and spin part  $\delta_\theta$  to zero and later in §15.6.1 discuss whether or not that was foolish. Using Eq. (125a) we get:

---


$$F_{m,n,k}^{1,2} = \frac{-V_{m,n,k}^{1,2}}{-ik + i \left( m - n + (-1)^{1,2} \right) v_1 + \frac{1}{2\pi} (m + n + 1) \alpha_1} \quad (126a)$$

$$f_{m,n,k}^\ell = \frac{-v_{m,n,k}^\ell}{-ik + i (m - n) v_1 + (m + n) \frac{\alpha_1}{2\pi} - i\ell v} \quad (126b)$$

We can easily guess the general case with  $N$  degrees of freedom by introducing a sum over tunes and damping.

$$F_{m,n,k}^j = \frac{-V_{m,n,k}^j}{-ik + \sum_{j=1,N} i \left( m_j - n_j + (-1)^j \right) v_j + \frac{1}{2\pi} (m_j + n_j + 1) \alpha_j} \quad (127a)$$

$$f_{m,n,k}^\ell = \frac{-v_{m,n,k}^\ell}{-ik - i\ell v + \sum_{j=1,N} \left\{ i (m_j - n_j) v_j + (m_j + n_j) \frac{\alpha_j}{2\pi} \right\}} \quad (127b)$$

## 15.6 Types of normal forms

There are broadly two types of normal form: into a rotation or one resonance is left. Damping complicates the situation a little bit.

### 15.6.1 Rotation and sink

In Eq. (127a), we notice that if

$$k = 0 \text{ and } \alpha_j = 0 \quad \sum_{j=1,N} \left| m_j - n_j + (-1)^j \right| = 0 \quad (128)$$

then the denominator vanishes. In that case, these terms cannot be removed from  $H_\theta$ . These are the so-called tune shifts with amplitude. They are uniquely defined and do not depend on the canonical transformation.

If damping is present, one can remove **everything** and the normal form is simply  $H_0$ — a sink. Whether or not this is a good thing to do is a matter of discussion. If there are resonances or large amount of damping (Van der Pol oscillator for example), we may want to keep tune shift and amplitude dependent terms in the Hamiltonian.

In the case of the quaternions, if

$$\ell = k = 0 \text{ and } \alpha_j = 0 \quad \sum_{j=1,N} \left| m_j - n_j \right| = 0 \quad (129)$$

then the quaternion Hamiltonian is proportional to  $e_0 = j$  and the coefficient of proportionality depends on the invariants of the transverse plane.

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### 15.6.2 One-resonance orbital: simple case to illustrate

Let us assume that the tune is dangerously close to a third order resonance:

$$3\nu_1 = p + \epsilon \quad (130)$$

where  $\epsilon$  is a small number. Then, we have:

$$\begin{aligned} \text{if } k = p \quad F_{m,n,k}^j &= \frac{-V_{m,n,k}^j}{-ik + \sum_{j=1,N} i(p + \epsilon) + \frac{1}{2\pi} (m_j + n_j + 1) \alpha_j} \\ &\underbrace{=}_{\text{if } k=p} \frac{-V_{m,n,k}^j}{i\epsilon + \sum_{j=1,N} \frac{1}{2\pi} (m_j + n_j + 1) \alpha_j} = \text{big} \end{aligned} \quad (131)$$

Therefore we leave the resonant term in the Hamiltonian and do not attempt the inversion of Eq. (131). The resulting normalized Hamiltonian operator has the form:

$$\begin{aligned} \hat{K}_\theta &= \sum_{a=1,3} \nu_a(\vec{J}) \frac{\partial}{\partial \Phi_a} + \frac{1}{2} \nu_{\text{spin}}(\vec{J}) \hat{j} \\ &+ : V(\vec{J}) \exp(i\{p\theta - 3\Phi_1\}) : + : \bar{V}(\vec{J}) \exp(-i\{p\theta - 3\Phi_1\}) : \end{aligned} \quad (132)$$

In the above equation,  $: V :$  denotes the usual Poisson bracket operator of Dragt ( $: V : f = [V, f]$ ).

The  $\theta$  dependence of this Hamiltonian can be removed by another transformation, a rotation, of the form:

$$\mathcal{B} = \exp\left(\frac{\#}{\#} - \alpha\theta J_{1\frac{\#}{\#}}\right) = \exp\left(\frac{\#}{\#} \alpha\theta \frac{\partial}{\partial \Phi_1} \frac{\#}{\#}\right) \quad (133)$$

We then use Eq. (120b) to compute the effect of  $\mathcal{B}$  on the Hamiltonian of Eq. (134):

$$\begin{aligned} \mathcal{B}\hat{K}_\theta &= \sum_{a=1,3} \nu_a(\vec{J}) \frac{\partial}{\partial \Phi_a} + \frac{1}{2} \nu_{\text{spin}}(\vec{J}) \hat{j} \\ &+ : V(\vec{J}) \exp(i\{p\theta - 3(\Phi_1 + \alpha\theta)\}) : + : \bar{V}(\vec{J}) \exp(-i\{p\theta - 3(\Phi_1 + \alpha\theta)\}) : \\ &- \sum_{n=1}^{\infty} \frac{\frac{\#}{\#} \alpha\theta \frac{\partial}{\partial \Phi_1} \frac{\#}{\#}^{n-1}}{n!} \frac{\partial}{\partial \theta} : \alpha\theta \frac{\partial}{\partial \Phi_1} : \end{aligned} \quad (134)$$

We choose  $\alpha$  to get rid of the  $\theta$  (time) dependence. Clearly the result is:

$$\alpha = p/3 \quad (135)$$

---

As for the last term in the transformation, only the derivative survives since the higher order terms commute with  $\frac{\partial}{\partial \Phi_1}$ . Therefore the final result is:

$$\begin{aligned} \mathcal{BK}_\theta &= \sum_{a=1,3} \nu_a(\vec{J}) \frac{\partial}{\partial \Phi_a} + \frac{1}{2} \nu_{\text{spin}}(\vec{J}) \hat{j} \\ &+ :V(\vec{J}) \exp(-i3\Phi_1): + : \bar{V}(\vec{J}) \exp(i3\Phi_1): - \frac{p}{3} \frac{\partial}{\partial \Phi_1} \end{aligned} \quad (136)$$

If we separate the linear part of the tune shift from the nonlinear tunes shift terms, we get the famous co-moving operator form:

$$\begin{aligned} \mathcal{BK}_\theta &= \left\{ \nu + \underbrace{\Delta_1(\vec{J})}_{\nu_1(\vec{J}) - \nu} \right\} \frac{\partial}{\partial \Phi_1} + \sum_{a=2,3} \nu_a(\vec{J}) \frac{\partial}{\partial \Phi_a} + \frac{1}{2} \nu_{\text{spin}}(\vec{J}) \hat{j} \\ &+ :V(\vec{J}) \exp(-i3\Phi_1): + : \bar{V}(\vec{J}) \exp(i3\Phi_1): - \frac{p}{3} \frac{\partial}{\partial \Phi_1} \\ &= \left\{ \underbrace{\frac{\epsilon}{3}}_{\nu - p/3} + \underbrace{\Delta_1(\vec{J})}_{\nu_1(\vec{J}) - \nu} \right\} \frac{\partial}{\partial \Phi_1} + \sum_{a=2,3} \nu_a(\vec{J}) \frac{\partial}{\partial \Phi_a} + \frac{1}{2} \nu_{\text{spin}}(\vec{J}) \hat{j} \\ &+ :V(\vec{J}) \exp(-i3\Phi_1): + : \bar{V}(\vec{J}) \exp(i3\Phi_1): \end{aligned} \quad (137)$$

Eq. (137) is the final one-resonance normal form in the Hamiltonian frame work. Since it is time independent it is clear that the following objects are invariants:

1. Because  $\mathcal{BK}_\theta$  is  $\theta$  independent, it is an invariant.
2. The actions in the planes perpendicular to the resonance, commute with  $\mathcal{BK}_\theta$ , they are also invariants.

**The one-resonance Hamiltonian is not unique. Moreover, the results will always be different from the one-resonance calculation done on a one-turn map. This can be seen on the analytical calculation done in appendix D of reference [15]. In a map calculation all the terms proportional to  $\cos(3\Phi_1)$  are kept. Of course any result expressed in the original variables  $x, p_x$  is unique including the invariants in the original space.**

For coupled resonances, the theory is messier but do not differ in its formal complexity from the one-turn map based theory. The spin resonance theory is intrisically coupled and is discussed in the next section.

### 15.6.3 One-resonance spin

**I need to take a rest and relax before surgery.... so this is blank.**

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