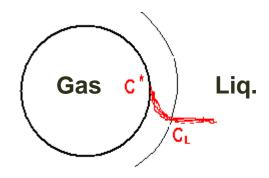


Oxygen transfer rate (OTR)

Oxygen transfer from gas to liquid



- OTR [mg O₂ / L / h]
- k_L: oxygen transfer coefficient (cm/h)
- a : gas-liquid interfacial area per unit vol. (cm²/cm³)
- k_L a : volumetric oxygen transfer coefficient (1/h)
- C* : saturated DO concentration (mg/L)
- C_L: DO concentration in the broth (mg/L)



Oxygen uptake rate (OUR)

OUR from liquid to cell

OUR =
$$q_{O2} X = (\mu X) / Y_{X/O2}$$

- OUR [mg O₂ / L / h]
- q_{O2}: specific rate of oxygen consumption (mg O₂/g cell/h)
- Y_{X/O2}: oxygen yield coefficient (g cell/g O₂)

When oxygen transfer is the rate-limiting step,

OTR
$$(\rightarrow)$$
 = OUR (\rightarrow)
 k_L a $(C^* - C_L)$ = $(\mu X) / Y_{X/O2}$ Gas Liquid \rightarrow Cell
 $Y_{X/O2}$ k_L a $(C^* - C_L)$ = dX / dt
 $Y_{X/O2} \cdot OTR$ = cell growth rate



Modeling cell growth; Monod equation

Similar to Michaelis-Menten Kinetics

Assumes that a single enzyme system is responsible for the uptake of substrate (S), and that S is limited (growth-dependent variable). This is the most common kinetic model for cell growth.

$$\mu = \frac{\mu_{\rm m} S}{K_{\rm S} + S}$$

 μ = specific cell growth rate (hr⁻¹)

 $\mu_{\rm m}$ = maximum specific cell growth rate (hr⁻¹)

S = substrate concentration (g/L)

 K_S = Saturation constant (g/L) = S when μ = 1/2 μ_m .



Batch culture growth model

$$X(t) = ?$$

$$\mu = \frac{1}{X} \frac{dX}{dt} = \frac{\mu_{\rm m} S}{K_{\rm s} + S} \quad \cdots (1)$$

We relate changes in S to changes in X through Y_{X/S}

$$X - X_o = Y_{X/S} (S_o - S), \text{ or } S = S_o + X_o / Y_{X/S} - X / Y_{X/S} \cdots (2)$$

 $Y_{X/S}$ = cell mass yield (g dcw/g S consumed) X_o , S_o = initial concentrations of cells and substrate

Combine (1) and (2), and rearrange

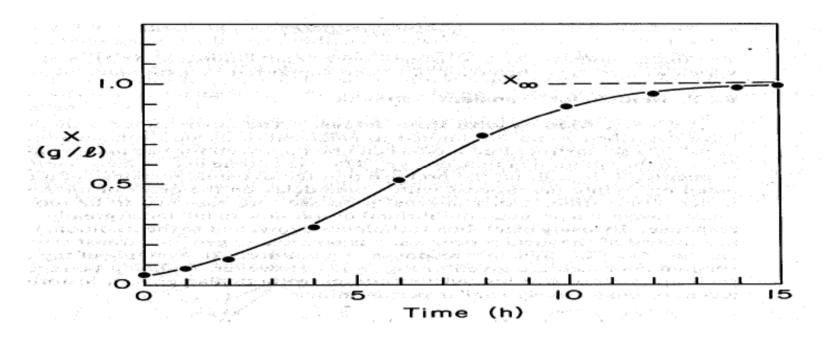
$$\frac{dX}{dt} = \frac{\mu_{\rm m} (S_{\rm o} Y_{\rm X/S} + X_{\rm o} - X)}{(K_{\rm S} Y_{\rm X/S} + S_{\rm o} Y_{\rm X/S} + X_{\rm o} - X)} X \quad ; \quad \text{at } t = 0, X = X_{\rm o}$$



Batch culture growth model (cont.)

Logistic Equation

$$\frac{(K_{\rm S}Y_{\rm X/S}+S_{\rm o}Y_{\rm X/S}+X_{\rm o})}{(S_{\rm o}Y_{\rm X/S}+X_{\rm o})} \ln\!\left(\!\frac{\rm X}{\rm X_{\rm o}}\!\right) - \frac{K_{\rm S}Y_{\rm X/S}}{(S_{\rm o}Y_{\rm X/S}+X_{\rm o})} \ln\!\left\{\!(S_{\rm o}Y_{\rm X/S}+X_{\rm o}-X)S_{\rm o}Y_{\rm X/S}\!\right\} \! = \ \mu_{\rm m} \ t$$



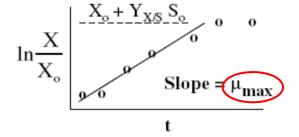


How to determine Monod parameters, K_s and μ_{max}

$$\mu = \frac{1}{X} \frac{dX}{dt}$$

$$\mu t = \ln \left(\frac{X}{X_o} \right)$$

 K_S is determined differently. K_S is equal to S when μ = 1/2 μ_{max}



μ = 1/X dX/dt needs to be determined from available data, especially data at low S concentrations.

$$\mu = \frac{1}{X} \frac{dX}{dt} \begin{bmatrix} \frac{\mu_{\text{max}}}{\sigma} & \sigma & \sigma & \sigma \\ \frac{\sigma}{\sigma} & \mu = 1/2 & \mu_{\text{max}} \end{bmatrix}$$
Basic Concepts K_{α} S

"Bioprocess Engineering: Basic Concepts Shuler and Kargi. Prentice Hall. 2002

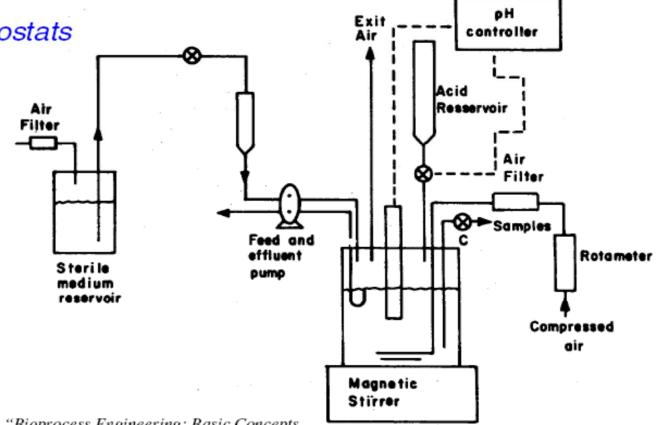


Cell growth in continuous culture

Automated Chemostats

→ control of pH, temp. agitation, dissolved oxygen

→ sterilization required



"Bioprocess Engineering: Basic Concepts Shuler and Kargi, Prentice Hall, 2002



Chemostat as a tool

- \rightarrow evaluate $K_S,\,\mu_{\text{max}},\,Y_{\text{X/S}}$ and other system parameters
- → study changes in environment and effects on cell physiology
- → select for cells with desired metabolic capabilities (e.g. selection for cells capable of degrading a toxic compound)



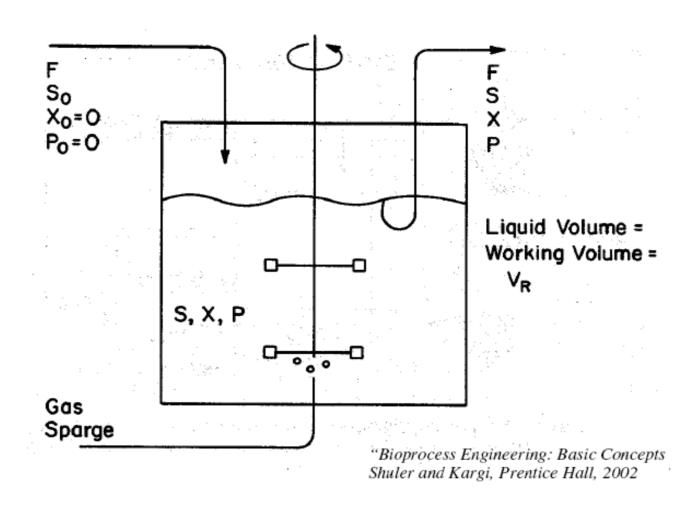
Chemostat mass balance

Why derive mass balance equation?

- Describe dynamics of cell growth, substrate utilization, and product formation.
- Useful for control of bioreactors.
- 3. Evaluate kinetic and yield parameters. $(Y_{x/s}, K_s, \mu_{max})$
- Determine the optimum values for bioreactor operating parameters.



Continuous-stirred tank reactor (CSTR), chemostat





Cell mass balance in CSTR to get S

or

$$FX_o - FX + V_R \mu X - V_R k_d X = V_R \frac{dX}{dt}$$

F = in and out volumetric flow rate (L/hr)

X = bioreactor and outlet cell mass concentration (g/L)

 X_0 = inlet cell mass concentration (g/L) = 0

 μ = specific cell growth rate neglecting endogenous metabolism (hr⁻¹)

 k_d = endogenous cell loss rate constant (hr⁻¹)



Steady state and sterile feed

Chemostats are normally operated at steady-state, d/X/dt = 0. Assume a sterile feed ($X_o = 0$), and k_d is so small that is neglected, $k_d = 0$.

The cell mass balance equations becomes,

$$\begin{bmatrix} \text{mass rate} \\ \text{of cells out} \\ \text{of bioreactor} \end{bmatrix} = \begin{bmatrix} \text{mass rate of cell} \\ \text{growth without} \\ \text{endogenous} \\ \text{metabolism} \end{bmatrix} \qquad \frac{F}{V_R} = \mu \quad \text{or} \quad D = \mu \\ \text{where} \quad \frac{F}{V_R} = D, \text{ dilution rate} \\ \text{where} \quad \frac{F}{V_R} = D, \text{ dilution rate} \\ \end{bmatrix}$$

D [sec-1]; how many times of rxtor vol. flow per second



Substrate concentration in CSTR when $k_d = 0$

Using the Monod Equation, we can predict the bioreactor and outlet stream concentration of Substrate.

$$\mu = \frac{\mu_{\text{max}} S}{K_s + S} = D$$
rearranging,
$$S = \frac{K_s D}{\mu_{\text{max}} - D}$$



"Washout" for CSTR

$$\begin{split} X &= Y_{x/s}(S_o - S) \\ &= Y_{x/s}(S_o - \frac{DK_s}{\mu_{max} - D}) \\ @ D &= D_{w.o.}, \quad X = 0 \\ 0 &= S_o - \frac{D_{w.o.}K_s}{\mu_{max} - D_{w.o.}} \end{split}$$

There is an upper limit on D, or the cells will washed out of the bioreactor.

$$D \le \frac{\mu_{\text{max}} S_{\text{o}}}{K_{\text{S}} + S_{\text{o}}}$$



Substrate concentration in CSTR when $k_d \neq 0$

From cell mass balance

$$FX = V_R \mu X - V_R k_d X$$

$$F = V_R (\mu - k_d)$$

$$D = \mu - k_d$$

$$\mu = \frac{\mu_{\text{max}} S}{K_S + S} = D + k_d$$

$$S = \frac{K_s(D + k_d)}{\mu_{max} - D - k_d}$$

 \rightarrow S is higher than the case when $k_d = 0$



Substrate mass balance in CSTR to get X

How is X affected by D? A similar mass balance <u>equation for S</u> in the absence of endogenous metabolism is written to answer this question.

$$FS_{o} - FS - V_{R} \mu X \frac{1}{Y_{X/S}^{M}} - V_{R} q_{p} X \frac{1}{Y_{P/S}} = V_{R} \frac{dS}{dt}$$

S = bioreactor and outlet substrate concentration (g/L)

 S_o = inlet substrate concentration (g/L)

 $Y_{X/S}^{M}$ = maximum cell yield coefficient (g cells/g substrate)

 $Y_{P/S}$ = product yield coefficient (g product/g substrate)

 q_P = specific rate of extracellular product formation $\left(\frac{g P}{g \text{ cells } \cdot \text{hr}}\right)$



Cell concentration in CSTR

For the simple case of no product formation ($q_p=0$), steady-state (dS/dt=0), and no endogenous metabolism, $k_d=0$.

$$D(S_o - S) = \frac{\mu X}{Y_{x/s}^M}$$

at steady-state, $\mu = D$, and solving for X,

$$X = Y_{X/S}^{M}(S_o - S)$$

or

$$X = Y_{X/S}^{M}(S_o - \frac{K_S D}{\mu_{max} - D})$$



when $k_d \neq 0$

Thus far, the substrate balance eqn. Has been written assuming

that $Y_{\text{X/S}}$ is a constant at $Y_{\text{X/S}}^{\mathrm{M}}$.

With endogenous metabolism, $\mu = D + k_d$ and with no extracellular product formation, the substrate mass balance is at steady-state,

where
$$m_S = \frac{k_d}{Y_{X/S}^M}$$

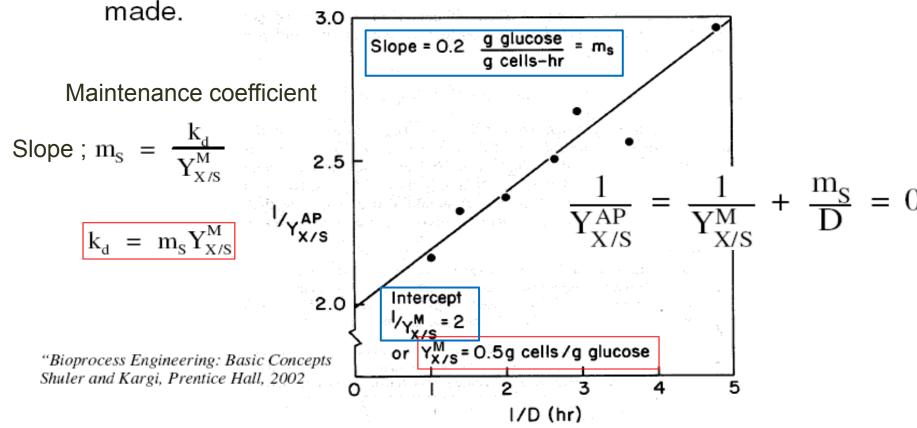
maintenance coefficient based on S.

$$\begin{split} D\frac{(S_o - S)}{X} - \frac{(D + k_d)}{Y_{X/S}^M} &= 0 \\ rearranging, \\ D\frac{(S_o - S)}{X} - \frac{D}{Y_{X/S}^M} - \frac{k_d}{Y_{X/S}^M} &= 0 \\ and \\ \frac{D}{Y_{X/S}^{AP}} - \frac{D}{Y_{X/S}^M} - \frac{k_d}{Y_{X/S}^M} &= 0 \\ \frac{1}{Y_{X/S}^{AP}} &= \frac{1}{Y_{X/S}^M} + \frac{m_S}{D} &= 0 \end{split}$$



Measurement of maximum cell yield and maintenance using a chemostat

From measurements of X, S, S_o, and D in a chemostat experiment at different D values, a double reciprocal plot can be





Determination of μ_{max} and K_s using a chemostat

From data collected using a chemostat, we can obtain the Monod Equation kinetic parameters.

Data include S at several Dilution Rates (D), Recall that,

$$D = \mu - k_d \quad \text{(when } k_d \neq 0\text{)}$$

$$D = \frac{\mu_{\text{max}} S}{K_S + S} - k_d \qquad \frac{1}{D + k_d}$$

rearranging

$$\frac{1}{D+k_d} = \frac{1}{\mu_{max}} + \frac{K_S}{\mu_{max}} \frac{1}{S}$$

slope =
$$\frac{K_S}{\mu_{\text{max}}}$$

intercept = $\frac{1}{\mu_{\text{max}}}$



Productivity of a chemostat

Cell production rate in CSTR [g/h] = FX

 $Pr_X = productivity for cell production = DX = FX / V$

 Pr_{p} = productivity for product formation = DP

The dilution rate (D) which maximizes productivity is found by taking dPr/dD = 0 and solving for D ($D_{optimum}$).

For example, $D_{optimum}$ for X with $k_d = 0$ and $q_P = 0$

$$X = Y_{x/s}^{M}(S_{o} - \frac{K_{S}D}{\mu_{max} - D}) \quad \Rightarrow \quad DX = Y_{x/s}^{M}D(S_{o} - \frac{K_{S}D}{\mu_{max} - D})$$

take
$$\frac{d(DX)}{dD} = 0$$
 and solve for D (D_{opt})

$$D_{opt} = \mu_{max} (1 - \sqrt{\frac{K_S}{K_S + S_o}})$$

$$D_{opt} = \mu_{max} (1 - \sqrt{\frac{K_S}{K_S + S_o}})$$

$$K_S \text{ is usually } << S$$
so $D_{opt} \sim \mu_{max}$ (washout point)



Product mass balance

$$FP_o - FP + V_R q_P X = V_R \frac{dP}{dt}$$

at steady - state, dP / dt = 0 and for $P_0 = 0$

$$DP = q_p X \text{ or } P = \frac{q_p X}{D}$$

for $k_d = 0$, no endogenous metabolism

$$S = \frac{K_s D}{\mu_{max} - D}$$
 from X mass balance

$$X = Y_{X/S}^{M}(S_o - S) \frac{D}{(D + q_p \frac{Y_{X/S}^{M}}{Y_{P/S}})}$$
 from S mass balance



Product mass balance

for $k_d \neq 0$, with endogenous metabolism

$$S = \frac{K_s (D + k_d)}{(\mu_{max} - D - k_d)}$$
 from X mass balance

$$X = Y_{X/S}^{M}(S_o - S) \frac{D}{(D + k_d + q_P \frac{Y_{X/S}^{M}}{Y_{P/S}})}$$
 from S mass balance

to determine D for optimum P formation,

$$\frac{d(DP)}{dD} = 0$$
 \Rightarrow solve for D_{opt}



Chemstat response to D

