

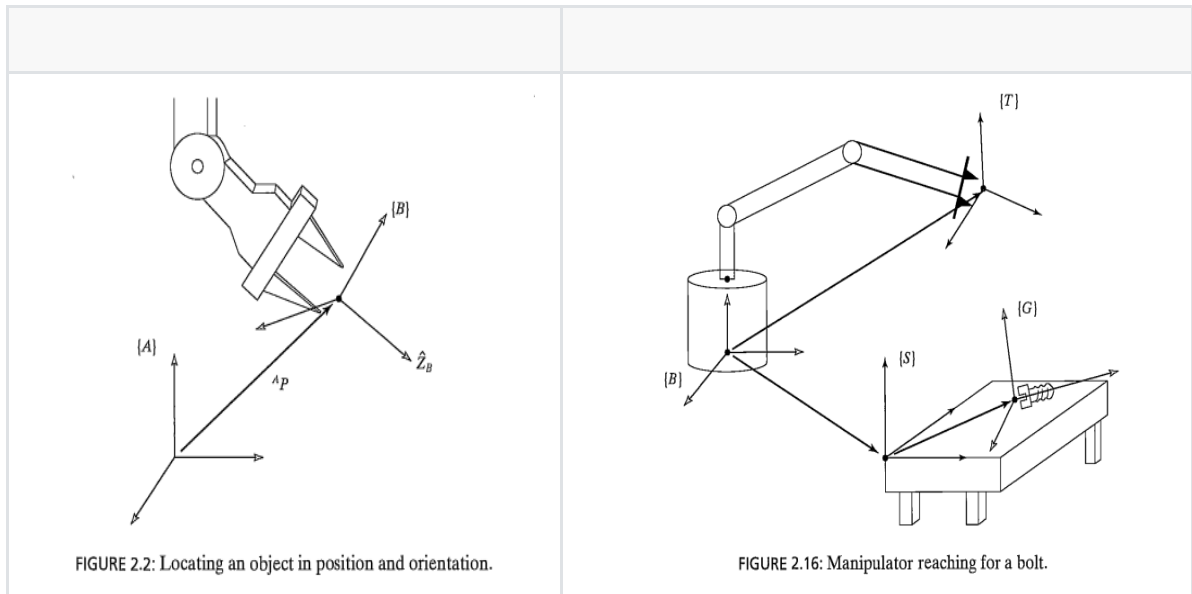
# Introduction to Robotics

[Introduction to Robotics book PDF](#), Third Edition. John J. Craig,

 **Youtube** : 고려대학교 송재복 교수님

## Chapter 1. Spatial descriptions and Transformations

### 1-1. Descriptions: Pose, Position, Orientation



- **Pose = position(위치) + orientation(방위, 자세, ...)**

- example : [ROS Pose Message](#)

- **Position**

- **Description of a position**
  - ${}^A P$  : position vector of  $P$  written in  $\{A\}$

$${}^A P = \begin{bmatrix} p_x \\ p_y \\ p_z \end{bmatrix}$$

## - Orientation

- Description of a orientation

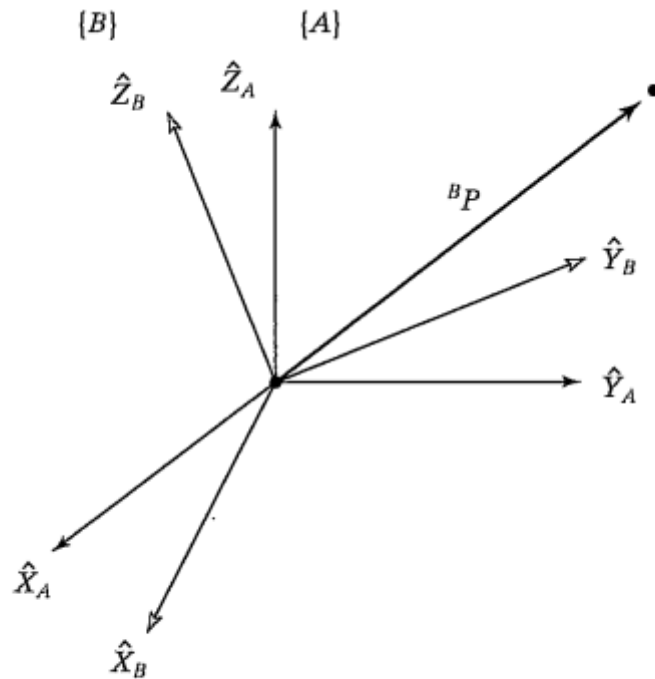
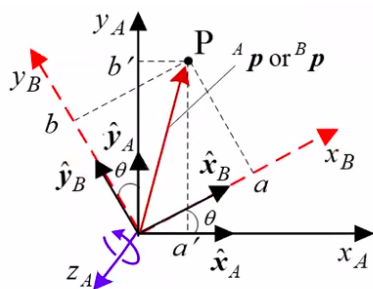


FIGURE 2.5: Rotating the description of a vector.



$${}^A p = a' \hat{x}_A + b' \hat{y}_A \quad \& \quad {}^B p = a \hat{x}_B + b \hat{y}_B$$

$$\begin{aligned} {}^A p &= ({}^B p \cdot \hat{x}_A) \hat{x}_A + ({}^B p \cdot \hat{y}_A) \hat{y}_A \\ &= [(a \hat{x}_B + b \hat{y}_B) \cdot \hat{x}_A] \hat{x}_A + [(a \hat{x}_B + b \hat{y}_B) \cdot \hat{y}_A] \hat{y}_A \\ &= [a \hat{x}_B \cdot \hat{x}_A + b \hat{y}_B \cdot \hat{x}_A] \hat{x}_A + [a \hat{x}_B \cdot \hat{y}_A + b \hat{y}_B \cdot \hat{y}_A] \hat{y}_A \end{aligned}$$

$${}^A p = \begin{bmatrix} a' \\ b' \end{bmatrix} = \begin{bmatrix} \hat{x}_B \cdot \hat{x}_A & \hat{y}_B \cdot \hat{x}_A \\ \hat{x}_B \cdot \hat{y}_A & \hat{y}_B \cdot \hat{y}_A \end{bmatrix} \begin{bmatrix} a \\ b \end{bmatrix} = \begin{bmatrix} \hat{x}_B \cdot \hat{x}_A & \hat{y}_B \cdot \hat{x}_A \\ \hat{x}_B \cdot \hat{y}_A & \hat{y}_B \cdot \hat{y}_A \end{bmatrix} {}^B p$$

- ${}^A \hat{X}_B$ : the vector whose components are the projections of that vector onto the unit directions of its reference frame.

$${}^A R_B = [{}^A \hat{X}_B \quad {}^A \hat{Y}_B \quad {}^A \hat{Z}_B] = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix}$$

$${}^A R_B = [{}^A \hat{X}_B \quad {}^A \hat{Y}_B \quad {}^A \hat{Z}_B] = \begin{bmatrix} \hat{X}_B \cdot \hat{X}_A & \hat{Y}_B \cdot \hat{X}_A & \hat{Z}_B \cdot \hat{X}_A \\ \hat{X}_B \cdot \hat{Y}_A & \hat{Y}_B \cdot \hat{Y}_A & \hat{Z}_B \cdot \hat{Y}_A \\ \hat{X}_B \cdot \hat{Z}_A & \hat{Y}_B \cdot \hat{Z}_A & \hat{Z}_B \cdot \hat{Z}_A \end{bmatrix}$$

- Physical meaning of rotation matrix

- ${}^A R_B$ : rotation matrix from the coordinates of P relative to {B} to coordinates relative to {A}

$${}^A P = {}^A R_B {}^B P.$$

Figure 2.6 shows a frame  $\{B\}$  that is rotated relative to frame  $\{A\}$  about  $\hat{Z}$  by 30 degrees. Here,  $\hat{Z}$  is pointing out of the page.

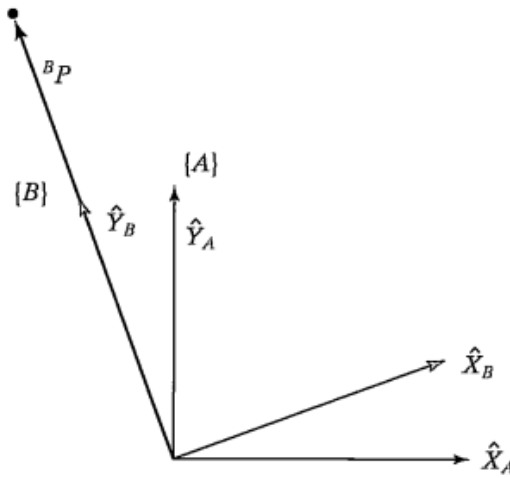


FIGURE 2.6:  $\{B\}$  rotated 30 degrees about  $\hat{Z}$ .

Given,  ${}^B P = \begin{bmatrix} 0.0 \\ 2.0 \\ 0.0 \end{bmatrix}$

we obtain

$${}^A R_B = \begin{bmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} 0.866 & -0.500 & 0.000 \\ 0.500 & 0.866 & 0.000 \\ 0.000 & 0.000 & 1.000 \end{bmatrix}$$

we calculate  ${}^A P$  as

$${}^A P = {}^A R_B {}^B P = \begin{bmatrix} -1.000 \\ 1.732 \\ 0.000 \end{bmatrix}$$

- **Properties of a rotation matrix**

**orthonormal matrix(직교 행렬)**

$${}^A R_B = {}^B R_A^{-1} = {}^B R_A^T.$$

$${}^A P = {}^A R_B {}^B P$$

$${}^B P = {}^B R_A {}^A P$$

$${}^A P = {}^A R_B {}^B R_A {}^A P$$

$${}^A R_B {}^B R_A = I$$

Indeed, from linear algebra, we know that the inverse of a matrix with orthonormal columns is equal to its transpose.

- Orthogonality conditions

$$\hat{x} \cdot \hat{y} = 0, \hat{y} \cdot \hat{z} = 0, \hat{z} \cdot \hat{x} = 0$$

- Unit length conditions

$$|\hat{x}| = 1, |\hat{y}| = 1, |\hat{z}| = 1$$

Only 3 components are independent among 9 components of a rotation matrix because 6 conditions are imposed.]

즉, 3개의 파라미터만 결정을 하면 orientation이 정해진다는 의미입니다.

## 1-2. Operators: Translation, Rotation, and Transformation

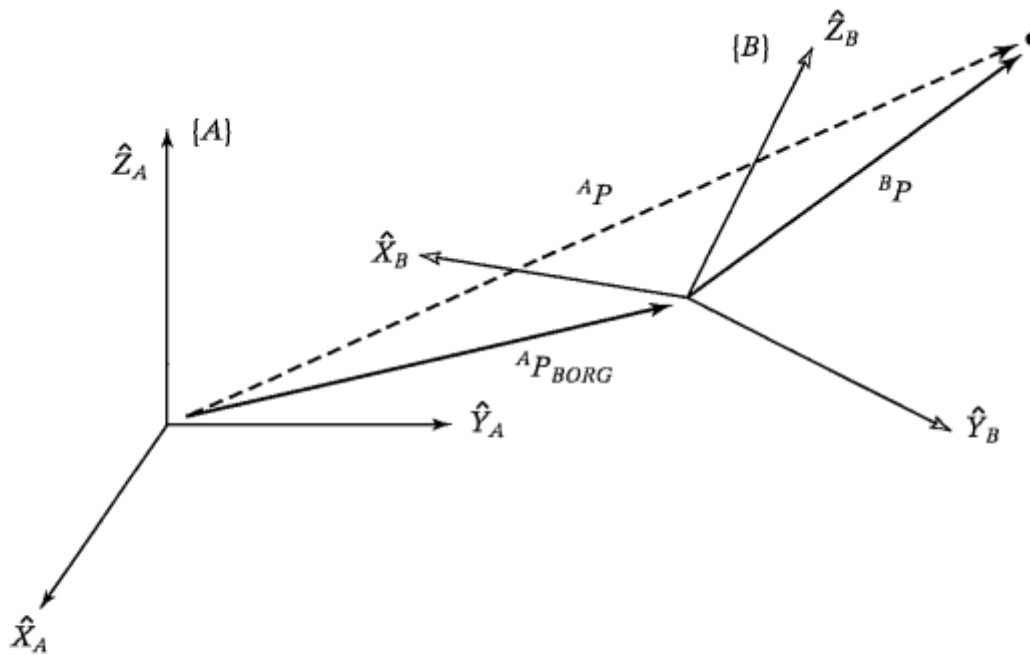


FIGURE 2.7: General transform of a vector.

$${}^A P = {}^A R {}^B P + {}^A P_{BORG}.$$

$$\begin{bmatrix} {}^A P \\ 1 \end{bmatrix} = \begin{bmatrix} {}^A R & | & {}^A P_{BORG} \\ \hline 0 & 0 & 0 & | & 1 \end{bmatrix} \begin{bmatrix} {}^B P \\ 1 \end{bmatrix},$$

- Homogeneous transform (동차변환)

4 x 4 matrix

$$H = \begin{bmatrix} R(3X3) & T(3X1) \\ 0(1X3) & 1(1X1) \end{bmatrix}$$

- Pure translation

$$Trans(Px, Py, Pz) = \begin{bmatrix} 1 & 0 & 0 & Px \\ 0 & 1 & 0 & Py \\ 0 & 0 & 1 & Pz \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

- Pure Rotation (Elementary rotation)

- General rotation : a suitable sequence of three elementary rotations on condition that two successive rotations are not made about parallel axes.

- Fixed angle representation (12 sets)

Rotation with respect to the fixed axes 🖱️ Absolute transforms

Typically, XYZ fixed angles (roll, pitch, yaw angles)

- [Euler angle](#) representation (12 sets)

Rotation with respect to the current axes (or body-fixed axes) 🖱️ Relative transforms

XYZ, ZXY, XZX, XYX, YXZ, YZX, YXY, YZY, ZXY, ZYZ, ZXZ, ZYX

Typically, ZYX Euler angles and ZYZ Euler angles

- 각도 계산 시 [arctan2](#)를 이용

arctan : range  $[-\pi/2, \pi/2]$

arctan2 : range  $[-\pi, \pi]$ ,  $\text{arctan2}(y, x) = \text{arctan2}(\sin(\theta), \cos(\theta))$

```
result_arctan = np.arctan([-1/-1]) * 180 / np.pi
>>> [45.]
result_arctan2 = np.arctan2([-1], [-1]) * 180 / np.pi
>>> [-135.]
```

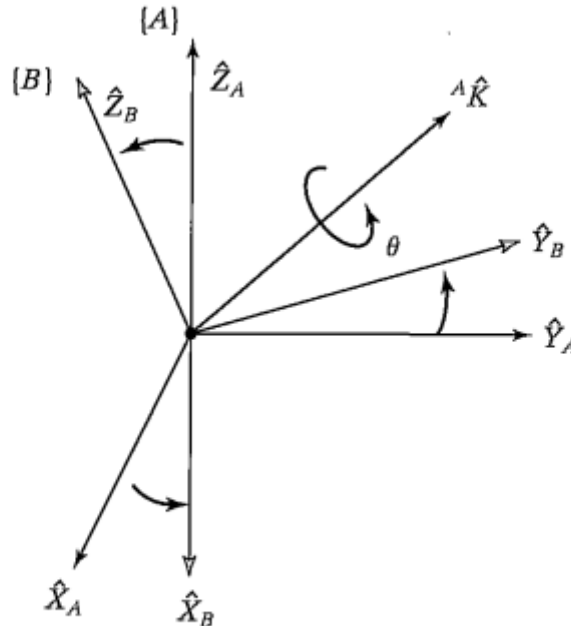


FIGURE 2.19: Equivalent angle-axis representation.

$R_x(\theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\theta) & -\sin(\theta) \\ 0 & \sin(\theta) & \cos(\theta) \end{bmatrix}$	$R_y(\theta) = \begin{bmatrix} \cos(\theta) & 0 & \sin(\theta) \\ 0 & 1 & 0 \\ -\sin(\theta) & 0 & \cos(\theta) \end{bmatrix}$	$R_z(\theta) = \begin{bmatrix} \cos(\theta) & -\sin(\theta) & 0 \\ \sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}$
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- Homogeneous transform

H = Translation x Rotation,

H = TR

$$H = \begin{bmatrix} R & T \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} I & T \\ 0 & 1 \end{bmatrix} \begin{bmatrix} R & 0 \\ 0 & 1 \end{bmatrix}$$

${}^A T_B^{-1}$ : Inverse transform matrix

$${}^A P = {}^A P_{BORG} + {}^A R_B {}^B P$$

$${}^A R_B^T {}^A P = {}^A R_B^T {}^A P_{BORG} + {}^A R_B^T {}^A R_B {}^B P = {}^A R_B^T {}^A P_{BORG} + {}^B P$$

$${}^B P = {}^A R_B^T {}^A P - {}^A R_B^T {}^A P_{BORG}$$

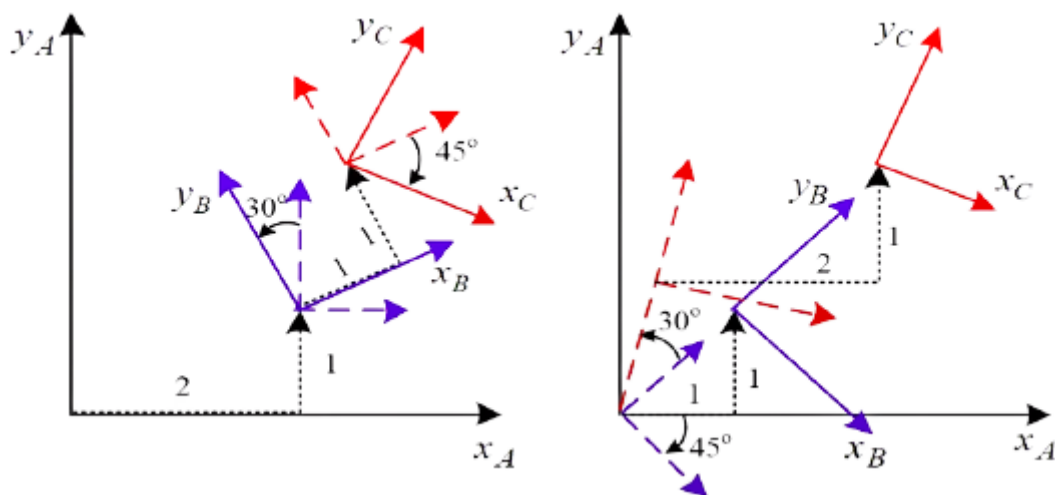
$${}^B_A T = \left[ \begin{array}{ccc|c} {}^A R_B^T & & & -{}^A R_B^T {}^A P_{BORG} \\ 0 & 0 & 0 & 1 \end{array} \right].$$

$${}^A T_B^{-1} = {}^B_A T$$

## 1-3. Relative transform and Absolute transform

- Relative transform
  - Translation relative to the current frame ==> Rotation relative to the current frame
  - Each transform is performed relative to the current frame.
  - The final frame is computed by **post-multiplying** (left -> right) the corresponding transformation matrices successively.
- Absolute transform
  - Rotation relative to the fixed frame -> Translation relative to the fixed frame
  - Each transform is performed relative to the fixed(reference) frame.
  - The final frame is computed by **pre-multiplying** (right -> left) the corresponding transformation matrices successively.

$${}^A T_B = \begin{bmatrix} \cos 30^\circ & -\sin 30^\circ & 0 & 2 \\ \sin 30^\circ & \cos 30^\circ & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, {}^B T_C = \begin{bmatrix} \cos(-45^\circ) & -\sin(-45^\circ) & 0 & 1 \\ \sin(-45^\circ) & \cos(-45^\circ) & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



$$H = T1 * R1 * T2 * R2$$

Relative transform

- (Translation of A -> B) ---> (Rotation of A -> B) ---> (Translation of B -> C) ---> (Rotation of B->C)

Absolute transform

- (Translation of A -> B) <--- (Rotation of A -> B) <--- (Translation of B -> C) <--- (Rotation of B->C)

## 1-4. Transform Equations

### Examples

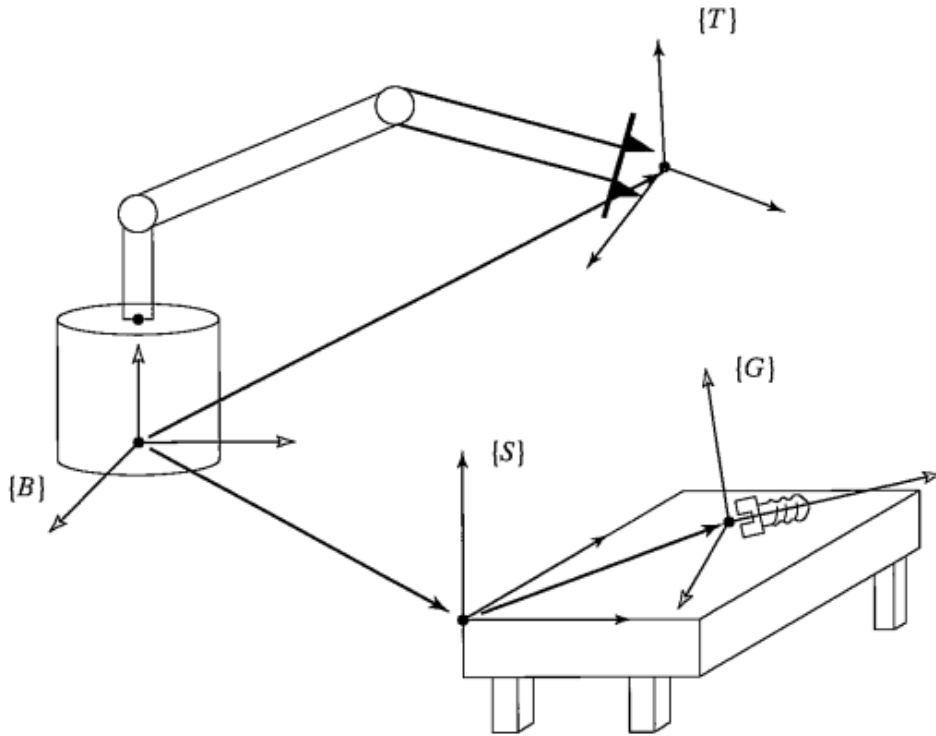


FIGURE 2.16: Manipulator reaching for a bolt.

### EXAMPLE 2.6

Assume that we know the transform  ${}^B_T T$  in Fig. 2.16, which describes the frame at the manipulator's fingertips  $\{T\}$  relative to the base of the manipulator,  $\{B\}$ , that we know where the tabletop is located in space relative to the manipulator's base (because we have a description of the frame  $\{S\}$  that is attached to the table as shown,  ${}^B_S T$ ), and that we know the location of the frame attached to the bolt lying on the table relative to the table frame—that is,  ${}^S_G T$ . Calculate the position and orientation of the bolt relative to the manipulator's hand,  ${}^T_G T$ .

Guided by our notation (and, it is hoped, our understanding), we compute the bolt frame relative to the hand frame as

$${}^T_G T = {}^B_T T^{-1} {}^B_S T {}^S_G T. \quad (2.55)$$



## 1-5. More on representation of Orientation

### - Inverse XYZ Fixed angles, ZYX Euler angles, ZYZ Euler angles problem

- XYZ fixed angles

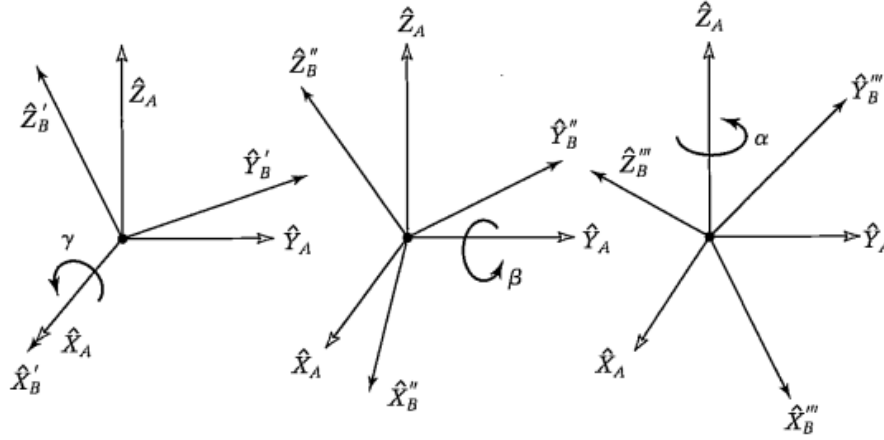


FIGURE 2.17: X–Y–Z fixed angles. Rotations are performed in the order  $R_X(\gamma)$ ,  $R_Y(\beta)$ ,  $R_Z(\alpha)$ .

$${}^A_B R_{XYZ}(\gamma, \beta, \alpha) = R_Z(\alpha) R_Y(\beta) R_X(\gamma)$$

$$= \begin{bmatrix} c\alpha & -s\alpha & 0 \\ s\alpha & c\alpha & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c\beta & 0 & s\beta \\ 0 & 1 & 0 \\ -s\beta & 0 & c\beta \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & c\gamma & -s\gamma \\ 0 & s\gamma & c\gamma \end{bmatrix}, \quad (2.63)$$

$${}^A_B R_{XYZ}(\gamma, \beta, \alpha) = \begin{bmatrix} c\alpha c\beta & c\alpha s\beta s\gamma - s\alpha c\gamma & c\alpha s\beta c\gamma + s\alpha s\gamma \\ s\alpha c\beta & s\alpha s\beta s\gamma + c\alpha c\gamma & s\alpha s\beta c\gamma - c\alpha s\gamma \\ -s\beta & c\beta s\gamma & c\beta c\gamma \end{bmatrix}. \quad (2.64)$$

$${}^A_B R_{XYZ}(\gamma, \beta, \alpha) = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix}.$$

- if  $\cos(\beta) \neq 0$

$$\beta = \text{Atan2}(-r_{31}, \sqrt{r_{11}^2 + r_{21}^2}),$$

$$\alpha = \text{Atan2}(r_{21}/c\beta, r_{11}/c\beta),$$

$$\gamma = \text{Atan2}(r_{32}/c\beta, r_{33}/c\beta),$$

we always compute the single solution for which  $-90.0^\circ \leq \beta \leq 90.0^\circ$

- If  $\beta = 90.0^\circ$

$$\alpha - \gamma = \text{atan2}(-r_{12}, r_{22})$$

$$\beta = 90.0^\circ,$$

$$\alpha = 0.0,$$

$$\gamma = \text{Atan2}(r_{12}, r_{22}).$$

- If  $\beta = -90.0^\circ$

$$\alpha + \gamma = \text{atan2}(-r_{12}, r_{22})$$

$$\beta = -90.0^\circ,$$

$$\alpha = 0.0,$$

$$\gamma = -\text{Atan2}(r_{12}, r_{22}).$$

In those cases, only the sum or the difference of  $\alpha$  and  $\gamma$  can be computed.

-> **Infinitely many solution for  $\alpha$  and  $\gamma$**

Not able to distinguish the rotation  $\alpha$  and  $\gamma$

-> **Representation singularity** (1 자유도 상실)

- **ZYX Euler angles**

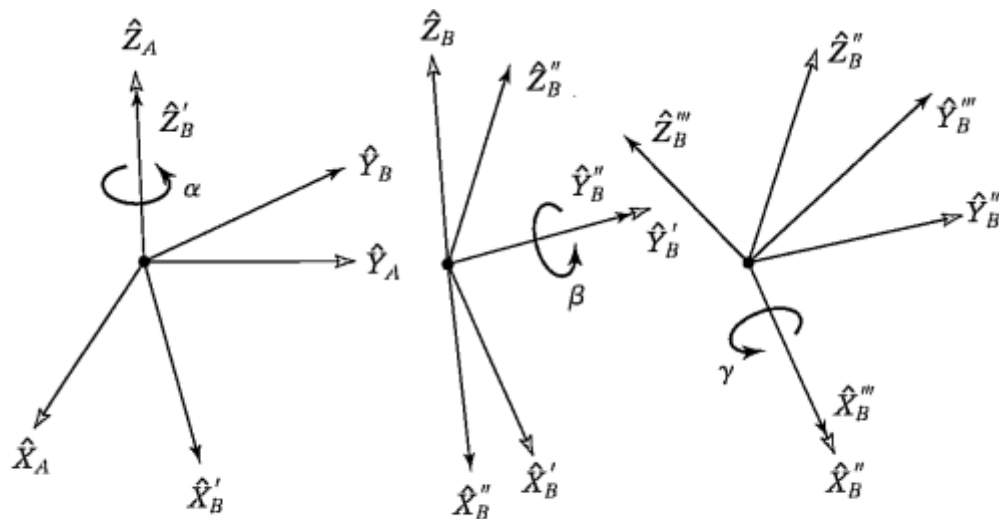


FIGURE 2.18: Z-Y-X Euler angles.

three rotations taken about fixed axes yield the same final orientation as the same three rotations taken in opposite order about the axes of the moving frame.

- **ZYZ Euler angles**

we always compute the single solution for which  $0^\circ \leq \beta \leq 180.0^\circ$

If  $\beta = 0.0$  or  $\beta = 180.0$ ,

In those cases, only the sum or the difference of  $\alpha$  and  $\gamma$  can be computed.

Not able to distinguish the rotation  $\alpha$  and  $\gamma$

-> **Representation singularity** (1 자유도 상실)

## 1-6. Equivalent angle-axis representation

[wikipedia](https://en.wikipedia.org/wiki/Axis-angle_representation)

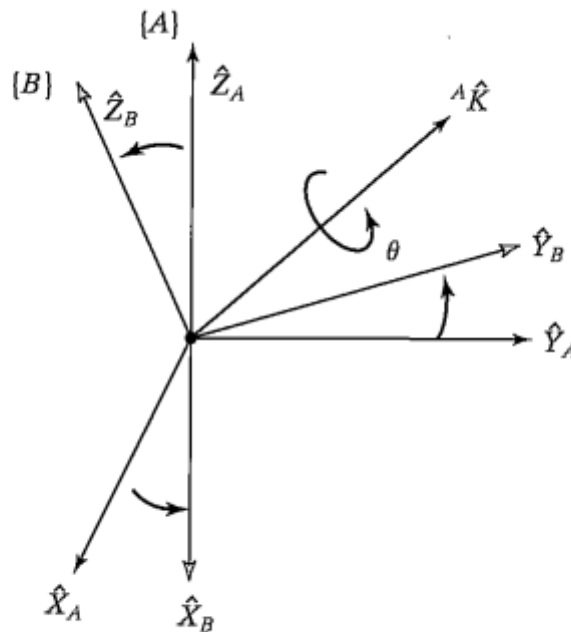


FIGURE 2.19: Equivalent angle-axis representation.

$$R_K(\theta) = \begin{bmatrix} k_x k_x v \theta + c \theta & k_x k_y v \theta - k_z s \theta & k_x k_z v \theta + k_y s \theta \\ k_x k_y v \theta + k_z s \theta & k_y k_y v \theta + c \theta & k_y k_z v \theta - k_x s \theta \\ k_x k_z v \theta - k_y s \theta & k_y k_z v \theta + k_x s \theta & k_z k_z v \theta + c \theta \end{bmatrix}$$

$${}^A_B R_K(\theta) = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix},$$

$$\theta = \text{Acos} \left( \frac{r_{11} + r_{22} + r_{33} - 1}{2} \right)$$

$$\hat{K} = \frac{1}{2 \sin \theta} \begin{bmatrix} r_{32} - r_{23} \\ r_{13} - r_{31} \\ r_{21} - r_{12} \end{bmatrix}$$

**Singularity :** The solution given by fails if  $\theta = 0^\circ$  or  $\theta = 180^\circ$

## 1-7. Unit Quaternion

[wikipedia](#)

- Euler parameters.

$$\epsilon_1 = k_x \sin \frac{\theta}{2},$$

$$\epsilon_2 = k_y \sin \frac{\theta}{2},$$

$$\epsilon_3 = k_z \sin \frac{\theta}{2},$$

$$\epsilon_4 = \cos \frac{\theta}{2}.$$

$$\epsilon_1^2 + \epsilon_2^2 + \epsilon_3^2 + \epsilon_4^2 = 1 \quad , \text{ Only three parameters are independent.}$$

$$R_\epsilon = \begin{bmatrix} 1 - 2\epsilon_2^2 - 2\epsilon_3^2 & 2(\epsilon_1\epsilon_2 - \epsilon_3\epsilon_4) & 2(\epsilon_1\epsilon_3 + \epsilon_2\epsilon_4) \\ 2(\epsilon_1\epsilon_2 + \epsilon_3\epsilon_4) & 1 - 2\epsilon_1^2 - 2\epsilon_3^2 & 2(\epsilon_2\epsilon_3 - \epsilon_1\epsilon_4) \\ 2(\epsilon_1\epsilon_3 - \epsilon_2\epsilon_4) & 2(\epsilon_2\epsilon_3 + \epsilon_1\epsilon_4) & 1 - 2\epsilon_1^2 - 2\epsilon_2^2 \end{bmatrix}.$$

$$\epsilon_1 = \frac{r_{32} - r_{23}}{4\epsilon_4},$$

$$\epsilon_2 = \frac{r_{13} - r_{31}}{4\epsilon_4},$$

$$\epsilon_3 = \frac{r_{21} - r_{12}}{4\epsilon_4},$$

$$\epsilon_4 = \frac{1}{2} \sqrt{1 + r_{11} + r_{22} + r_{33}}.$$

not Singularity

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next  [forward kinematics](#)

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