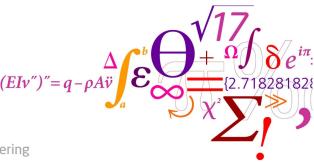


Composites and materials indices

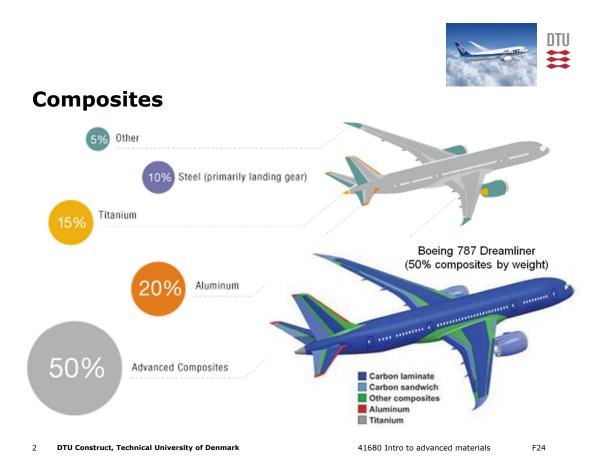
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DTU Construct

Department of Civil and Mechanical Engineering





Composites

- Combination of two or more materials
- Aim: achievement of desired properties
- Artificial multiphase materials
- Phase 1: continuous matrix
- Phase 2: discontinuously distributed in matrix
- Types

MMC	PMC	СМС		
Metal	Polymer	Ceramic		
Matrix Composite				

• Natural multiphase material, e.g. eutectics

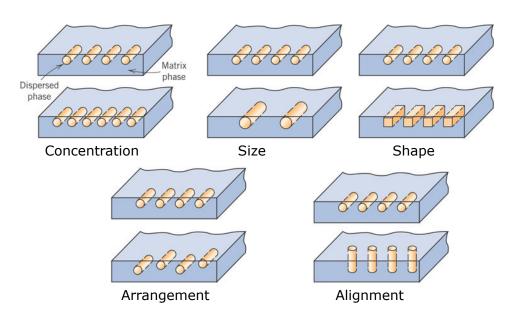
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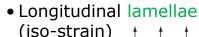


Composites

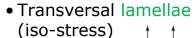




Elastic properties of laminar composites



(iso-strain)
$$\uparrow$$
 \uparrow \uparrow $\varepsilon_c = \varepsilon_m = \varepsilon_f$ $\sigma_{c\parallel} = f_m \sigma_m + f_f \sigma_f$



(iso-stress)
$$\uparrow \uparrow \uparrow$$

$$\sigma_c = \sigma_m = \sigma_f$$

$$\varepsilon_{c\perp} = f_m \varepsilon_m + f_f \varepsilon_f$$

Rule of mixture for stress

$$E_{c||} = f_m E_m + f_f E_f$$

- Voigt model
- Upper bond
- Volume fractions $f_{\rm m}$, $f_{\rm f}$

Rule of mixture for strain

$$\frac{1}{E_{c\perp}} = f_m \frac{1}{E_m} + f_f \frac{1}{E_f}$$

- $E_{c||} > E_{c\perp}$ Reuss model Lower bond

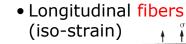
 - Volume fractions $f_{\rm m}$, $f_{\rm f}$

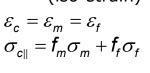
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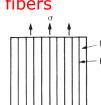
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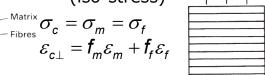
Elastic properties of fiber composites (formulae same as for laminar composites)





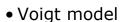


 Transversal fibers (iso-stress)





- Rule of mixture for stress
 - $E_{c} = f_m E_m + f_f E_f$





- Upper bond
- Volume fractions $f_{\rm m}$, $f_{\rm f}$

• Rule of mixture for strain

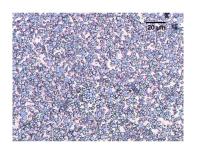
$$\frac{1}{E_{c\perp}} = f_m \frac{1}{E_m} + f_f \frac{1}{E_f}$$

- Volume fractions $f_{\rm m}$, $f_{\rm f}$



Properties of particulate composites

- Particles (p) dispersed in matrix (m)
- Example
 W particles (blue)
 in Cu matrix (red)



Volume fractions

$$f_m + f_p = 1$$

• Rule of mixture

$$X_c = f_m X_m + f_p X_p$$

• Mass density

$$\rho_{c} = f_{m}\rho_{m} + f_{p}\rho_{p}$$

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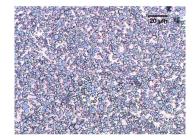
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Elastic properties of particulate composites

- Particles (p) dispersed in matrix (m)
- Example
 W particles (blue)
 in Cu matrix (red)



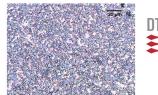
- Young's modulus
- Upper limit (Voigt)

$$\boldsymbol{E}_{c} = \boldsymbol{f}_{m}\boldsymbol{E}_{m} + \boldsymbol{f}_{p}\boldsymbol{E}_{p}$$

• Lower limit (Reuss)

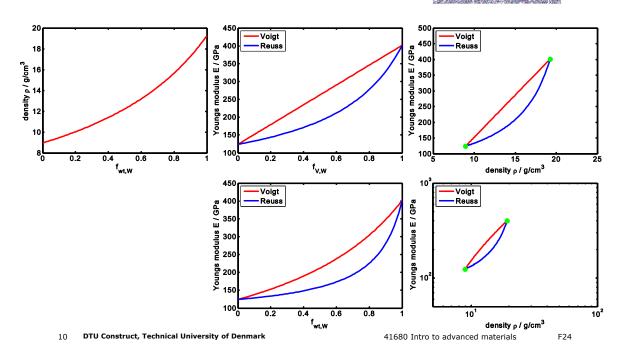
$$\frac{1}{E_c} = f_m \frac{1}{E_m} + f_p \frac{1}{E_p}$$
350
Upper bound
150
Lower bound

Tungsten concentration (vol%)





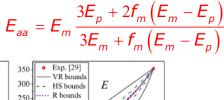
Tungsten copper composites

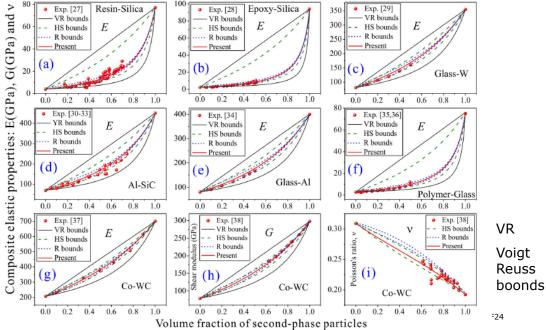


Elastic properties of particulate composites

Analytical approximation

(Zhang et al., Phys. Rev. B (2017))

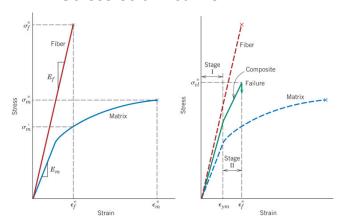






Mechanical properties of fiber composites **Continuous aligned fibers**

Stress strain curve



• Tensile stress (iso-strain)

$$\sigma(\varepsilon) = f_m \sigma_m(\varepsilon) + f_f \sigma_f(\varepsilon)$$

$$= f_m \sigma_m (\varepsilon) + f_f E_f \varepsilon$$
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Yield strength

$$\sigma_{y,c} = f_m \sigma_{y,m} + f_f E_f \varepsilon_{y,m}$$

• Tensile strength

$$\sigma^* = f_m \sigma_m \left(\varepsilon_f^* \right) + f_f \sigma_f^*$$
$$= f_m \sigma_m' + f_f \sigma_f^*$$

• Fracture strength of fibers

• Strain to failure of fibers

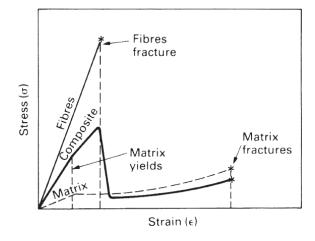
$$\varepsilon_f^* < \varepsilon_m^*$$

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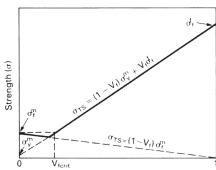
Mechanical properties of fiber composites **Continuous aligned fibers**

• What happens after the fracture of the fibers?



- Fibers are not under stress
- Deformation continues in matrix
- Strain at matrix fracture ε_m^*
- Reduced tensile strength

$$\sigma = \mathbf{f}_{m}\sigma_{m}\left(\varepsilon_{m}^{*}\right) = \mathbf{f}_{m}\sigma_{m}^{*}$$



Volume fraction of fibres (V_f)



Applications of ANSYS Granta EduPack

- Selection for specific purposes
 - Materials indices
- Design of new materials
 - Composites (synthesizer tool)

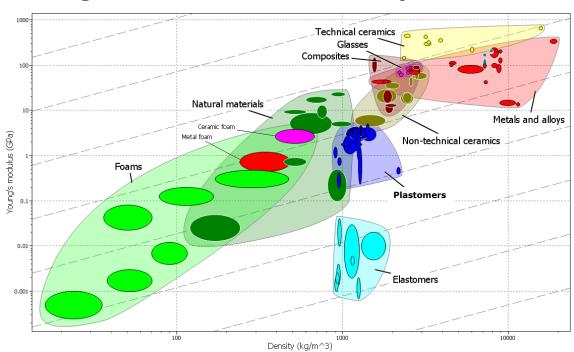


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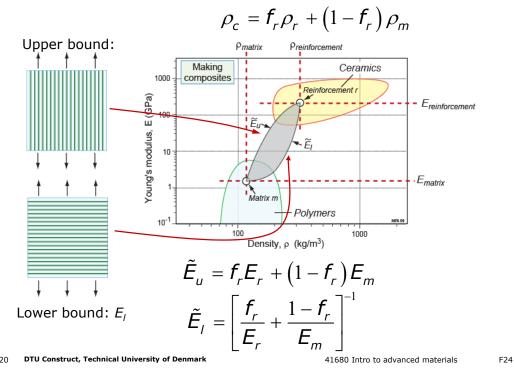
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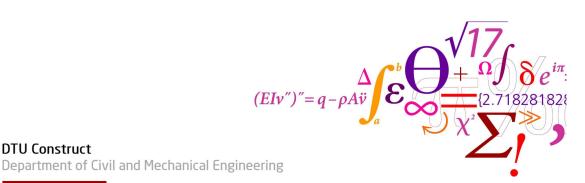
General composites: reinforcement in matrix



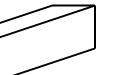


Materials indices

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Design: minimize weight of a light, stiff member





• Force

$$F = \sigma A$$

• Elongation

$$\Delta L = \varepsilon L$$

Elastic behavior

$$\sigma = E\varepsilon$$

• Stiffness of member

$$S = \frac{F}{\Delta L} = \frac{\sigma A}{\varepsilon L} = \frac{EA}{L}$$

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- Requirements: specified stiffness S fixed length L
- Mass

$$m = \rho AL = \frac{\rho}{E} SL^2$$

 Minimizing mass means maximizing ratio

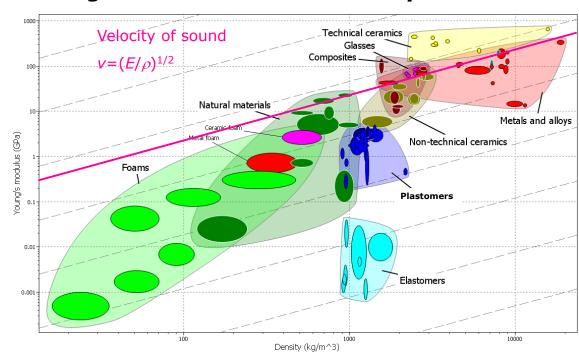
$$E/\rho$$

• Selection line in ANSYS GRANTA EduPack

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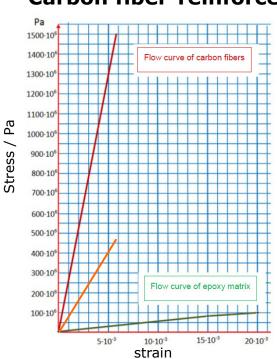




Group exercises

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Carbon fiber-reinforced PMC



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· Young's modulus of the composite (Voigt)

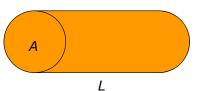
$$E_c = f_f E_f + f_m E_m = 80 \text{ GPa}$$

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- Fracture strength of epoxy $\sigma_{\rm m}^{~*}$ = 100 MPa
- Stress in matrix, when carbon fibers crack $\sigma_{\rm m}'$ = 30 MPa
- fracture strength of composite

$$\boldsymbol{\sigma}_{c}^{*} = f_{f} \boldsymbol{\sigma}_{f}^{*} + f_{m} \boldsymbol{\sigma}_{m}^{\prime} = 471 \text{ MPa}$$





DTU

 Requirements: fixed length L specified load F before yield

Mass

$$m = \rho AL = FL \frac{\rho}{\sigma_y}$$

• Force at yield

$$F = \sigma_{y}A$$

 Minimizing mass means maximizing ratio

$$\sigma_{_{\mathtt{y}}}/
ho$$

• Selection line in ANSYS GRANTA EduPack

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Material indices (light weight structures)

Member		Loading	Index
Beam	Stiffness	Tension / compression	E/ ho
		Torsion	${\it G}/ ho$
		Bending	$E^{1/3}/\rho E^{1/2}/\rho$
	Buckling	Compression	${\it E}^{\scriptscriptstyle 1/2}/ ho$
Panel	Stiffness	Bending	$E^{1/3}/\rho$
Beam	Strength*	Tension / compression	$\sigma_{_{Y}}/ ho$
	Strength*	Bending	$\sigma_{\scriptscriptstyle V}^{\scriptscriptstyle 2/3}/ ho$
Panel	Strength*	Bending	$\sigma_{y}^{^{1/2}}/ ho$
Spring	Resilience		$\sigma_y^2/E\rho$

^{*} Either yield strength or failure strength



Material property chart Young's modulus vs. mass density

