Dynamic Modeling of the Human Coagulation Cascade using Reduced Order Effective Kinetic Models

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Running Title: Modeling blood coagulation

To be submitted: Processes

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Abstract

Keywords: Coagulation, Mathematical modeling, Systems Biology

Introduction

Developing mathematical models of biochemical networks is a significant facet of systems biology. Modeling approaches differ in their degree of detail, but the choice of approach is often determined by prior knowledge, or model requirements [1]. Ordinary differential equation (ODE) models are a common tool for modeling biochemical systems because of their ability to capture dynamics. However, ODE models typically come with difficult (or sometimes impossible) parameter identification problems. For example, Gadkar et al., showed that even with near-perfect information, it was often impossible to identify all the parameters in typical signal transduction models [2]. However, Bailey suggested more than a decade ago, that achieving qualitative or even quantitative understanding of biological systems should not require complete structural and parametric knowledge [3]. Since Bailey's complex biology with no parameters hypothesis, Sethna and coworkers showed that model performance is typically sensitive to only a few parameter combinations, a characteristic seemingly universal to multi-parameter models referred to as sloppiness [4]. Thus, reasonable predictions from sloppy models may be possible, de-15 spite parametric uncertainty, if a few critical components are well understood. Perhaps a 16 more important issue is that ODE models also require significant mechanistic information, 17 thereby limiting their utility in poorly understood systems. Data-driven [5] or logical model 18 approaches [6] are emerging modeling paradigms that constrain model structure by the 19 availability of experimental data. These are interesting techniques because the data nat-20 urally informs model structure, thereby limiting the identification challenge. Although not 21 always mechanistic, these models can simulate surprisingly rich system responses in the absence of mechanism [REFHERE]. However, modeling dynamics using logical models is not straightforward. Thus, a potential third approach could be a combination of ODEs and logical models, where mechanistic information was used when available, and missing or incomplete knowledge encoded using causal local rules.

In this study, we developed a hybrid approach which combined ODEs and logical rules 27 to model a well studied biochemical network, the human coagulation system. Coagulation is an archetype proteolytic cascade involving both positive and negative feedback [7–9]. Coagulation is mediated by a family proteases in the circulation, called factors and a key group of blood cells, called platelets. The central process in coagulation is the conver-31 sion of prothrombin (fII), an inactive coagulation factor, to the master protease thrombin (FIIa). Thrombin generation involves three phases, initiation, amplification and termina-33 tion [10, 11]. Initiation requires a trigger event, for example vessel injury, which leads to 34 the activation of factor VII (FVIIa). Two converging pathways, the extrinsic and intrinsic 35 cascades, then process and amplify this initial coagulation signal. The extrinsic cascade is generally believed to be the main mechanism of thrombinogenesis in the blood [12-37 14]. Initially, thrombin is produced upon cleavage of prothrombin by fluid phase activated 38 factor X (FXa), which itself has been activated by FVIIa [7]. Picomolar amounts of thrombin then activate the cofactors factors V and VIII (fV and fVIII) and platelets, leading to the formation of the tenase and prothrombinase complexes on activated platelets. These complexes amplify the early coagulation signal by further activating FXa, and directly converting prothrombin to thrombin. There are several control points in the cascade that inhibit thrombin formation, and eventually terminate thrombin generation. Tissue Factor Pathway Inhibitor (TFPI) inhibits FXa formation catalyzed by TF/FVIIa, while antithrombin III (ATIII) neutralizes several of the proteases generated during coagulation, including thrombin. Thrombin itself also inadvertently plays a role in its own inhibition; thrombin, through interaction with thrombomodulin, protein C and endothelial cell protein C receptor (EPCR), converts protein C to activated protein C (APC) which attenuates the coagulation response by proteolytic cleavage of fV/FVa and fVIII/FVIIIa. Termination occurs after either prothrombin is consumed, or thrombin formation is neutralized by inhibitors such as 51 activated protein C (APC) or antithrombin III (ATIII).

Coagulation models in the literature have typically been formulated as systems of non-53 linear ordinary differential equations, often using mass-action kinetics to describe the rates of biochemical conversions [REFHERE]. Previous ODE coagulation models from our laboratory [15, 16], were built upon the earlier studies of Jones and Mann [17], and 56 later Hockin et al. [18], who developed and then refined highly mechanistic models of ex-57 trinsic coagulation. Other laboratories have also expanded upon Hockin et al., for example including the intrinsic pathway, and thrombin mediated clot formation [19]. Other biochem-59 ical or biophysical aspects of coagulation have also been modeled, such as platelet bio-60 chemistry [20], multi-scale models of clot formation [21, 22], and transport inside growing 61 clots [23]. However, most of these previous studies were based upon detailed mechanistic knowledge. Such a description is possible because blood, while enormously complex, 63 can be systematically interrogated. However, other systems, such as the intracellular 64 networks which mediate cancer, are more difficult to experimentally probe and model. Towards this unmet need, we have formulated a hybrid modeling approach which combines ODEs and logical rules to model biochemical processes for which mechanistic information 67 is difficult or impossible to obtain. We have used this approach to model the coagulation cascade because of the wealth of training and validation data available for this system. We proposed a reduced order coagulation model that consisted of five differential equations augmented with several logical rules. We identified the reduced order coagulation model parameters from in vitro extrinsic coagulation data sets, in the presence of ATIII, with and without the protein C pathway. We then validated the model using thrombin data sets from multiple laboratories, for both normal and hemophilic coagulation. Flux and sensitivity analysis identified which parameter or parameters combinations were critical to 75 model performance in several conditions. The reduced order hybrid approach produced a surprisingly predictive coagulation model, suggesting this framework could potentially be 77 used to model other biochemical networks important to human health.

79 Results

Formulation of reduced order coagulation models. We developed a reduced order coagulation model to test our hybrid kinetic rule based modeling approach (Fig. 1). A 81 trigger event initiates thrombin formation (FIIa) from prothrombin (fII) through a lumped 82 initiation step. This step loosely represents the initial fluid phase activation of thrombin by 83 activated FXa. Once activated, thrombin catalyzes its own formation (amplification step), and inhibition via the conversion of protein C to activated protein C (APC). APC and tissue factor pathway inhibitor (TFPI) inhibit initiation, while antithrombin III (ATIII) inhibits amplification. All initiation and inhibition processes, as well as the dependence of amplification upon other coagulation factors, was approximated using our rule-based approach (Fig. 2). Individual regulatory contributions to the activity of pathway enzymes were integrated 89 into control coefficients using an integration rule. These control coefficients then modified the rates of model processes at each time step. Hill-like transfer functions $0 \le f(\mathcal{Z}) \le 1$ 91 quantified the influence of components upon a target process. Components were either individual inhibitor or activator levels or some function of levels, e.g., the product of factor 93 levels. In this study, $\mathcal Z$ corresponded to the abundance of individual inhibitors or acti-94 vators, with the exception of the dependence of amplification upon specific coagulation 95 factors (modeled as the product of factors). When a process was potentially sensitive to 96 multiple inputs, logical integration rules were used to select which transfer functions influ-97 enced the process at any given time. In our proof of concept model, we used a winner 98 takes all strategy; the maximum or minimum transfer function was selected at any given 99 time step. However, other integration rules are certainly possible. Taken together, while 100 the reduced order coagulation model encodes significant biological complexity, it is highly 101 compact, consisting of only five differential equations. Thus, it will serve as an excellent 102 proof of principle example to study the reduction of a highly complex human subsystem.

Identification of model parameters using particle swarm optimization. A critical challenge for any dynamic model is the estimation of kinetic parameters. We estimated 105 kinetic and control parameters simultaneously from eight in vitro time-series coagulation 106 data sets with and without the protein C pathway. The residual between model simula-107 tions and experimental measurements was minimized using particle swarm optimization 108 (PSO). A population of particles (N = 20) was initialized with randomized kinetic and con-109 trol parameters and allowed to search for parameter vectors that minimized the residual. 110 However, not all parameters were varied simultaneously. We partitioned the parame-111 ter estimation problem into two subproblems based upon the biological organization of 112 the training data; (i) estimation of parameters associated with thrombin formation in the 113 absence of the protein C pathway and (ii) estimation of parameters associated with the 114 protein C pathway. Only those parameters associated with each subproblem were varied 115 during the optimization procedure for that subproblem e.g., thrombin parameters were not 116 varied during the protein C subproblem. The PSO procedure was run for 20 generations 117 for each subproblem, where each generation was 1200 iterations. The best particle from 118 each generation was used to generate the particle population for the next generation. We 119 rotated the subproblems, starting with subproblem 1 in the first generation. 120

The reduced order coagulation model captured the role of initial prothrombin abundance, and the decay of the thrombin signal following from ATIII activity (Fig. 3). However, we systematically under-predicted the thrombin peak and the strength of ATIII inhibition in this training data set. On the other hand, with fixed thrombin parameters, we captured peak thrombin values and the decay of the thrombin signal (at least for the 150% fII case) in the presence of both ATIII and the protein C pathway (Fig. 4). Lastly, we were unable to capture global differences in initiation time *across* separate data sets with a single ensemble of model parameters. These differences likely result from normal experimental variability. For example different thrombin generation experiments within our training data

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(at the same physiological factor levels) have significantly different initiation times (supplemental results). However, this also highlights a potential shortcoming of the initiation 131 module within the model. To capture the variability in initiation time across training data 132 sets, we included a constant time-delay parameter (T_D) for each data group. The delay 133 parameter was constant within a data set, but allowed to vary across training data sets. 134 Introduction of the delay parameter allowed the model to simulate multiple training data 135 sets using a single ensemble of model parameters. Taken together, the model identifica-136 tion results suggested that our kinetic-rules based approach could reproduce a panel of 137 thrombin generation data sets conducted at physiological factor and inhibitors concentra-138 tions. However, it was unclear whether the reduced order model could predict new data, 139 without updating the model parameters. 140

Validation of the reduced order coagulation model. We tested the predictive power of the reduced order coagulation model with validation data sets not used during model 142 training. Two validation data sets were used, thrombin generation for various prothrombin 143 and ATIII concentrations with the protein C pathway, and thrombin generation in normal 144 versus hemophilic plasma in the presence of the protein C pathway. Lastly, we compared 145 the qualitative output of the model to rFVIIa addition in the presence of hemophilia. The 146 hemophilia case was an especially difficult test as it was taken from a different study 147 which used a plasma-based in vitro assay involving platelets instead of phospholipid vesi-148 cles (PCPS). All kinetic and control parameters were fixed for the validation simulations. 149 The only globally adjustable parameter T_D , was fixed within each validation data set but 150 allowed to vary between data sets. The reduced order model predicted the thrombin 151 generation profile for ratios of prothrombin and ATIII in the absence of the protein C path-152 way (Fig. 5). Simulations near the physiological range (fII,ATIII) = (100%, 100%) or 153 (125%,75%) tracked the measured thrombin values (Fig. 5B and C). On the other hand, 154 predictions for factors levels outside of the physiological range (fII,ATIII) = (50%, 150%) or (150%, 50%), while qualitatively consistent with measured thrombin values, did show significant deviation from the measurements (Fig. 5A and D). Likewise, simulations of thrombin generation in normal versus hemophilia (missing both fVIII and fIX) were consistent with measured thrombin values (Fig. 6). We modeled the dependence of thrombin amplification on factor levels using a product rule ($\mathcal{Z} = fV \times fX \times fVIII \times fIX$), which was then was integrated using a min integration rule into the control variable governing amplification. Thus, in the absence of fVIII or fIX, the amplification control variable evaluated to zero, and the only thrombin produced was from initiation (Fig. 6B). However, the decay of the thrombin signal was underpredicted in the normal case (Fig. 6A), while the activated thrombin level was overpredicted in hemophilia simulations, although thrombin generation was far less than normal (Fig. 6B). Taken together, the reduced order model performed well in the physiological range of factors, even with unmodeled components such as platelet activation in the hemophilia data set. Thus, our kinetic-rules framework predicted the output of a physiologically important cascades such as coagulation, despite significant unmodeled components.

The model ensemble predicted a direct correlation between thrombin generation and rFVIIa addition in hemophilia (Fig. 7). In the current model, we cannot distinguish between different initiation sources, e.g., TF/FVIIa and rFVIIa, as we have only a single lumped initiation source (trigger). Thus, we simulated the addition of rFVIIa in hemophilia by removing fVIII and fIX from the model, and modulating the initial level of trigger. Simulations with a baseline level of trigger were consistent with the previous hemophilia simulations, where the only thrombin being produced was from initiation (Fig. 7, 1× trigger). As we increased the strength of the trigger event, the thrombin peak time and the maximum value of thrombin increased (Fig. 7, 50× trigger). However, as the trigger strength increased, the thrombin generated quickly decayed. For example, for the highest trigger strength simulated (50×trigger), 95% of the thrombin was gone by 20 min after initiation. We per-

formed flux analysis to understand how the reduced order coagulation model balanced initiation, amplification and inhibition of thrombin formation for normal coagulation and 183 hemophilia. Analysis of the reaction flux through the reduced order network for thrombin 184 generation in normal, hemophilia and rFVIIa-treated hemophilia identified three distinct 185 operational modes (Fig. 8). The reduced order network includes four lumped reactions, 186 initiation, amplification, thrombin-induced APC generation and total thrombin inhibition (in-187 cluding both APC and ATIII action). Directly after the addition of a trigger (e.g., TF/FVIIa or 188 rFVIIa), the lumped initiation flux was the largest for all three cases. However, within a few 189 minutes enough thrombin was generated by the initiation mechanism to induce the am-190 plification stage. During amplification, thrombin catalyzes its own formation and inhibition 191 by generating activated protein C (APC), a potent inhibitor of the coagulation cascade. 192 For normal coagulation, amplification and thrombin inhibition are the dominate reactions 193 by 6 min after initiation (Fig. 8, left). After 10 min, the dominate reaction has shifted to 194 thrombin inhibition (both ATIII and APC action). In the current proof-of-principle model, 195 APC inhibits upstream of amplification thus APC activity will slow the rate of thrombin 196 formation directly from the initiation trigger. On the other hand, ATIII inhibits thrombin di-197 rectly, as well as upstream coagulation factors. In hemophilia (missing both fVIII and fIX), the amplification reaction does not occur and the only thrombin produced is from initiation (Fig. 8, center). Initiation is quickly inhibited by APC, and the thrombin level stabilizes and eventually decays because of ATIII activity. Lastly, when 50×rFVIIa is used to induce 201 thrombin formation in hemophilia (absence of fVIII/fIX), initiation mechanisms dominate 202 for up to 6 min following initiation (Fig. 8, right). However, similar to hemophilia alone, 203 without amplification the thrombin signal is quickly extinguished by the combined action 204 of ATIII and APC generated by thrombin. 205

Global sensitivity analysis of the reduced order coagulation model. We conducted a global sensitivity analysis to estimate which parameters controlled the performance of the reduced order model. We calculated the sensitivity of the time to maximum thrombin 208 (peak time) and the thrombin exposure (area under the thrombin curve) for different levels of prothrombin, and protein C (Fig. 9). Globally, 41% of the parameters shifted in impor-210 tance between the (fII,PC) = (50%, 0%) and (150%,100%) cases for the peak thrombin time (Fig. 9A). The majority of these shifts were involved increased prothrombin and the 212 protein C pathway, while only 5% were directly associated with increased prothrombin 213 alone. The rate constant for thrombin amplification was the most important parameter 214 controlling the peak thrombin time. While this parameter was differentially important for 215 different prothrombin levels, and in the presence or absence of the activated protein C 216 pathway, it's sensitivity was consistently above all other parameters in the model. The 217 saturation constant governing thrombin amplification was the second most important pa-218 rameter, followed by the initiation control gain parameter. Other important parameters 219 influencing the thrombin peak time included the control gain for activated protein C for-220 mation, as well as the rate constant controlling ATIII inhibition of thrombin activity. On the other hand, only 27% of the model parameters were differentially sensitive between the 222 (%fII,%PC) (50%, 0%) and (150%,100%) cases for the thrombin exposure (Fig. 9B). Of these parameters, all of the shifts were associated the interplay between thrombin formation and the protein C pathway. The rate constant controlling ATIII inhibition was the most important parameter controlling the thrombin exposure. While this parameter was less 226 important in the presence of protein C for 150% prothrombin levels, it was significantly above all other parameters. Similar to the peak time, for 150% prothrombin, the control 228 gain for activated protein C formation was differentially important along with the rate con-229 stant controlling amplification. However, the influence of the amplification parameter was 230 much less in the thrombin exposure case versus peak time.

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Discussion

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In this study, we developed a reduced order model of the human coagulation cascade. 233 We chose coagulation because it is well studied, has a complex architecture, and has an 234 abundance of experimental data available for model identification and validation. How-235 ever, coagulation was just a proof-of concept; the proposed framework could also be 236 used to dynamically model other biochemical networks, including intracellular metabolic 237 networks, gene expression programs or potentially even cell free metabolic systems. The 238 model consisted of five differential equations augmented with several logical rules de-239 scribing regulatory connections between model components, and unmodeled interactions in the network. We estimated model parameters from in vitro extrinsic coagulation data sets, in the presence of ATIII, with and without the protein C pathway. To estimate pa-242 rameters, the residual between model simulations and experimental measurements was minimized using particle swarm optimization (PSO). However, not all of the model pa-244 rameters were uniquely identifiable, given the training data. Instead, we estimated an 245 ensemble of likely parameter sets (N = 20) from eight in vitro time-series coagulation data 246 sets with and without the protein C pathway. We validated the ensemble using thrombin 247 data sets taken from multiple laboratories for a variety of experimental conditions not used 248 during training. The ensemble predicted thrombin trajectories for conditions not used for 249 model training, including thrombin generation for normal and hemophilic coagulation in the 250 presence of platelets (a significant unmodeled component). We then used flux analysis 251 to understand how the network operated in a variety of conditions, and global sensitivity 252 analysis to identify which parameters controlled the performance of the network. Taken 253 together, the reduced order hybrid approach produced a surprisingly predictive model, 254 suggesting this approach could potentially be used to model other biochemical networks 255 important to human health. 256

Malfunctions in coagulation can have potentially fatal consequences. For example,

aggressive clotting involved with Coronary Artery Diseases (CADs), collectively accounts for 38% of all deaths in North America [24]. Coagulation management during surgery can 259 also be challenging, particularly because of the increasing clinical use of antithrombotic 260 drugs [25]. Insufficient coagulation due to genetic disorders such as hemophilia can also 261 result in recurrent bleeding. The coagulation factors VIII (fVIII) and IX (fIX) are deficient 262 in Hemophilia A and B, respectively [26-28]. People with mild hemophilia have 5-40% of 263 the normal clotting factor levels while severe hemophiliacs have <1% [28]. Hemophilia 264 can be controlled with regular infusions of the deficient clotting factors. However, clotting 265 factor replacement sometimes leads to the formation of fVIII and fIX inhibitors in-vivo [29]. 266 Alternatively, recombinant factor VIIa (rFVIIa) has been used to treat bleeding disorders 267 [30, 31] including hemophilia with and without factor VIII/IX inhibitors [32]. However, rFVIIa 268 requires frequent administration (every 2-3 hr) because of its short half-life in the circula-269 tion. Many questions also remain about the mechanism of action of rFVIIa, its effective 270 dose range [29], and its overall utility for the treatment trauma-associated hemorrhage 271 [33]. In the current proof of concept model, we did not model rFVIIa directly. Rather we 272 modeled a broad class of trigger materials which initiated the extrinsic coagulation cas-273 cade. Since we identified the model using TF/FVIIa, inherent to our rFVIIa simulations 274 was the presence of TF. However, even with this complication, the model generated potentially useful insight into the rFVIIa mechanism of action, and its possible shortcomings especially for the treatment of hemophilia. Addition of rFVIIa directly activated thrombin through the fluid phase initiation pathway. However, in the presence of ATIII and the pro-278 tein C pathway but without fVIII or fIX, this initial thrombin signal was quickly extinguished 279 by inhibition, as thrombin amplification could not occur. As the dose of rFVIIa increased, 280 the peak thrombin time decreased, eventually saturating. Butenas et al., performed an 281 extensive study of rFVIIa induced thrombin generation in hemophilia [34]. 282

Although the performance of the proof of principle coagulation model was impressive

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given its size, there were several mathematical and biological questions that can be explored further. First, the choice of max/min integration rules, or the particular form of the 285 transfer functions could be generalized to include other rule types and functions. Theo-286 retically, an integration rule is simply a function whose domain is a set of transfer function 287 inputs, and whose range is $v \in [0,1]$. Thus, integration rules other than max/min could be 288 used, such as the mean or the product, assuming the range of the transfer functions is 289 always $f \in [0,1]$. Alternative integration rules such the mean would have different prop-290 erties which could influence model identification or performance. For example, a mean or 291 product integration rule would be differentiable, which allows derivative based optimiza-292 tion approaches to be used. The particular form of the transfer function could also be 293 explored. We choose a hill-like function because of its prominence in the systems and 294 synthetic biology community. However, the only mathematical requirement for a transfer 295 function is that it must map a non-negative continuous or categorical variable into the 296 range $f \in [0,1]$. Thus, many function types are possible. There are several additional 297 biological modules that can be added to the core model presented here. First, we need 298 to update the model to included thrombin induced platelet activation. While we were able 299 to capture thrombin generation data in the presence of platelets, the initial shape of the 300 activation curve and the time-scale of activation was not always consistent with the data. 301 Platelets are activated by thrombin through the cleavage of the extracellular domain of protease-activated receptors (PARs) on the platelet surface. Next, we should add the 303 intrinsic or contact thrombin activation pathway to the model. The intrinsic coagulation 304 pathway is triggered by contact activation of the plasma protease factor XII (fXII) by nega-305 tively charged surfaces. The activation of fXII is followed by proteolytic activation of factor 306 XI (fXI) and the activation of downstream factors like fIX [35]. It has also been suggested 307 that activated platelets can release polyphosphate which directly activates fXII [36]. Lastly, 308 to make the model more clinically relevant, we should include the biochemical processes 309

responsible for clot formation, and clot dissolution (fibrinolysis). Clot formation is driven by thrombin activity, while fibrinolysis is driven by plasmin activity, a key enzyme that cleaves 311 fibrin (one of the main materials in a clot). Similar to coagulation, fibrinolysis is managed by several activating and inhibitory factors which control the balance between clot forma-313 tion and dissolution. Tissue plasminogen activator (t-PA) and urokinase activate plasmin, 314 along with contact pathway factors such fXIa. On the other hand, thrombin activatable 315 fibrinolysis inhibitor (TAFI) inhibits the degradation of fibrin by plasmin. Also similar to 316 coagulation, there is considerable fibrinolysis and contact pathway data sets that can be 317 used to train the model. 318

Materials and Methods

Formulation and solution of the model equations. We used ordinary differential equations (ODEs) to model the time evolution of proteins (x_i) in our reduced order coagulation model:

$$\frac{dx_i}{dt} = \sum_{j=1}^{\mathcal{R}} \sigma_{ij} r_j \left(\mathbf{x}, \epsilon, \mathbf{k} \right) \qquad i = 1, 2, \dots, \mathcal{M}$$
 (1)

where \mathcal{R} denotes the number of reactions, \mathcal{M} denotes the number of protein species in the model. The quantity $r_j(\mathbf{x}, \epsilon, \mathbf{k})$ denotes the rate of reaction j. Typically, reaction jis a non-linear function of biochemical species abundance, as well as unknown kinetic parameters \mathbf{k} ($\mathcal{K} \times 1$). The quantity σ_{ij} denotes the stoichiometric coefficient for species iin reaction j. If $\sigma_{ij} > 0$, species i is produced by reaction j. Conversely, if $\sigma_{ij} < 0$, species iis consumed by reaction j, while $\sigma_{ij} = 0$ indicates species i is not connected with reaction j. The system material balances were subject to the initial conditions $\mathbf{x}(t_o) = \mathbf{x}_o$, which were specified by the experimental setup.

Each reaction rate was written as the product of two terms, a kinetic term (\bar{r}_j) and a regulatory term (v_j) :

$$r_i(\mathbf{x}, \epsilon, \mathbf{k}) = \bar{r}_i v_i \tag{2}$$

We used multiple saturation kinetics to model the reaction term \bar{r}_j :

$$\bar{r}_j = k_j^{max} \epsilon_i \left(\prod_{s \in m_j^-} \frac{x_s}{K_{js} + x_s} \right) \tag{3}$$

where k_j^{max} denotes the maximum rate for reaction j, ϵ_i denotes the scaled enzyme activity which catalyzes reaction j, and K_{js} denotes the saturation constant for species s in reaction j. The product in Eqn. (3) was carried out over the set of *reactants* for reaction j (denoted as m_j^-).

The control term v_i depended upon the combination of factors which influenced the 338 activity of enzyme i. For each enzyme, we used a rule-based approach to select from 339 competing control factors (Fig. 2). If an enzyme was activated by m metabolites, we 340 modeled this activation as:

$$v_i = \max\left(f_{1i}\left(\mathcal{Z}\right), \dots, f_{mi}\left(\mathcal{Z}\right)\right) \tag{4}$$

where $0 \leq f_{ij}\left(\mathcal{Z}\right) \leq 1$ was a regulatory transfer function that calculated the influence of metabolite i on the activity of enzyme j. Conversely, if enzyme activity was inhibited by a 343 m metabolites, we modeling this inhibition as: 344

$$v_{j} = 1 - \max\left(f_{1j}\left(\mathcal{Z}\right), \dots, f_{mj}\left(\mathcal{Z}\right)\right) \tag{5}$$

Lastly, if an enzyme had both m activating and n inhibitory factors, we modeled the regulatory term as: 346

$$v_i = \min\left(u_i, d_i\right) \tag{6}$$

where:

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$$u_{j} = \max_{j^{+}} \left(f_{1j} \left(\mathcal{Z} \right), \dots, f_{mj} \left(\mathcal{Z} \right) \right) \tag{7}$$

$$d_{j} = 1 - \max_{j^{-}} \left(f_{1j} \left(\mathcal{Z} \right), \dots, f_{nj} \left(\mathcal{Z} \right) \right)$$
 (8)

The quantities j^+ and j^- denoted the sets of activating and inhibitory factors for enzyme j. If a process has no modifying factors, we set $v_j=1$. There are many possible functional 349 forms for $0 \leq f_{ij}\left(\mathcal{Z}\right) \leq 1$. However, in this study, each individual transfer function took the 350 form: 351

$$f_i(\mathbf{x}) = \frac{\kappa_{ij}^{\eta} \mathcal{Z}_j^{\eta}}{1 + \kappa_{ij}^{\eta} \mathcal{Z}_j^{\eta}} \tag{9}$$

where \mathcal{Z}_j denotes the abundance of the j factor (e.g., metabolite abundance), and κ_{ij} and η are control parameters. The κ_{ij} parameter was species gain parameter, while η was a 353 cooperativity parameter (similar to a Hill coefficient). Applying the general framework to 354 the reduced coagulation network resulted in five ordinary differential equations: 355

$$\frac{dx_1}{dt} = -(r_{init}v_{init} + r_{amp}v_{amp})$$

$$\frac{dx_2}{dt} = r_{amp}v_{amp} + r_{init}v_{init} - r_{inh,ATIII}v_{inh,ATIII}$$
(11)

$$\frac{dx_2}{dt} = r_{amp}v_{amp} + r_{init}v_{init} - r_{inh,ATIII}v_{inh,ATIII}$$
(11)

$$\frac{dx_3}{dt} = -r_{apc}v_{apc} \tag{12}$$

$$\frac{dx_3}{dt} = -r_{apc}v_{apc}$$

$$\frac{dx_4}{dt} = r_{apc}v_{apc}$$

$$\frac{dx_5}{dt} = -r_{inh,ATIII}v_{inh,ATIII}$$
(12)

$$\frac{dx_5}{dt} = -r_{inh,ATIII}v_{inh,ATIII} \tag{14}$$

where $\mathbf{x} = (fII, FIIa, PC, APC, ATIII)^T$. The terms r_*v_* in the balance equations denote corrected kinetic expressions for initiation, amplification and inhibition processes. 357 The rate of initiation \bar{r}_{init} was modeled as:

$$\bar{r}_{init} = k_{init} \left(trigger \right) \frac{x_1}{K_{init,fII} + x_1} \tag{15}$$

where k_{init} , $K_{init,fII}$ are the rate and saturation constants governing initiation, respectively. The rate of initiation was modified by v_{init} , the control parameter governing initiation. 360 Initiation was sensitive to level of trigger (activator), and TFPI (inhibitor):

$$v_{init} = \min \left(f_{init}^{-} \left(TFPI \right), f_{init}^{+} \left(trigger \right) \right) \tag{16}$$

where the transfer functions f took the form of Eqn (9). The rate of thrombin amplification was given by:

$$\bar{r}_{amp} = k_{amp} (x_2) \frac{x_1}{K_{amp,fII} + x_1}$$
 (17)

where k_{amp} , $K_{amp,fII}$ denote the rate and saturation constants governing amplification, respectively. The amplification control term, which modified amplification rate, was modeled as a combination of multiple inhibition terms and one activation term:

$$v_{amp} = \min \left(f_{amp}^{-}(TFPI), f_{amp}^{-}(x_4), f_{amp}^{+}(\mathcal{Z}_{amp}) \right)$$
 (18)

where $\mathcal{Z}_{amp} = fV \times fX \times fVIII \times fIX$. Although, $f^+_{amp} \left(\mathcal{Z}_{amp} \right)$ is an activating term, we included it in the min integration rule; the factors in \mathcal{Z}_{amp} were essential for amplification (if any of these factors was missing the amplification reaction would not occur). Thus, the factors in \mathcal{Z}_{amp} were required components, a classification that we implemented by the min selection rule. The rate activated protein C formation was given by:

$$\bar{r}_{apc} = k_{APC,formation} (TM) \frac{x_3}{K_{formation,PC} + x_3}$$
(19)

where $k_{APC,formation}$, $K_{formation,PC}$ denote the rate and saturation constants governing activated protein C formation, respectively and TM denotes the thrombomodulin abundance. We modeled the control term which governed APC formation as a single thrombin dependent activation term:

$$v_{apc} = \max\left(f_{apc}^{+}\left(x_{2}\right)\right) \tag{20}$$

Lastly, we included direct irreversible inhibition of FIIa by ATIII:

$$\bar{r}_{inh,ATIII} = k_{ATIII,inhibition} \left(x_5 x_2^{\gamma} \right)$$
 (21)

where γ was estimated to be $\gamma=1.26$. For ATIII inhibition of FIIa, the control variables $v_{inh,ATIII}$ was taken to be unity. The model equations were encoded using the Python programming language and solved using the ODEINT routine of the SciPy module [37].

The model files can be downloaded from http://www.varnerlab.org.

Estimation of model parameters from experimental data. Model parameters were estimated by minimizing the difference between simulations and experimental thrombin measurements (squared residual):

$$\min_{\mathbf{k}} \sum_{\tau=1}^{\mathcal{T}} \sum_{j=1}^{\mathcal{S}} \left(\frac{\hat{x}_{j}(\tau) - x_{j}(\tau, \mathbf{k})}{\omega_{j}(\tau)} \right)^{2}$$
(22)

where $\hat{x}_{j}\left(\tau\right)$ denotes the measured value of species j at time τ , $x_{j}\left(\tau,\mathbf{k}\right)$ denotes the 384 simulated value for species j at time τ , and $\omega_{j}(\tau)$ denotes the experimental measure-385 ment variance for species j at time τ . The outer summation is respect to time, while 386 the inner summation is with respect to state. We minimized the model residual using 387 Particle swarm optimization (PSO) [38]. PSO uses a swarming metaheuristic to explore 388 parameter spaces. A strength of PSO is its ability to find the global minimum, even in the 389 presence of potentially many local minima, by communicating the local error landscape 390 experienced by each particle collectively to the swarm. Thus, PSO acts both as a local 391 and a global search algorithm. For each iteration, particles in the swarm compute their 392 local error by evaluating the model equations using their specific parameter vector real-393 ization. From each of these local points, a globally best error is identified. Both the local 394 and global error are then used to update the parameter estimates of each particle using 395 the rules: 396

$$\Delta_i = \theta_1 \Delta_i + \theta_2 \mathbf{r}_1 \left(\mathcal{L}_i - \mathbf{k}_i \right) + \theta_3 \mathbf{r}_2 \left(\mathcal{G} - \mathbf{k}_i \right)$$
 (23)

$$\mathbf{k}_i = \mathbf{k}_i + \mathbf{\Delta}_i \tag{24}$$

where $(\theta_1, \theta_2, \theta_3)$ are adjustable parameters, \mathcal{L}_i denotes local best solution found by particle i, and \mathcal{G} denotes the best solution found over the entire population of particles.

The quantities r_1 and r_2 denote uniform random vectors with the same dimension as the number of unknown model parameters ($\mathcal{K} \times 1$). In thus study, we used $(\theta_1, \theta_2, \theta_3) =$ 400 (1.0, 0.05564, 0.02886). The quality of parameter estimates was measured using good-401 ness of fit (model residual). The particle swarm optimization routine was implemented in 402 the Python programming language. All plots were made using the Matplotlib module of 403 Python [39]. The optimization code can be downloaded from http://www.varnerlab.org. 404 Global sensitivity analysis of model performance. We conducted a global sensitiv-405 ity analysis to estimate which parameters controlled the performance of the reduced or-406 der model. We computed the total sensitivity index of each parameter relative to two 407 performance objectives, the peak thrombin time and the area under the thrombin curve 408 (thrombin exposure). [FINISH ME].

410 Acknowledgements

This study was supported by an award from the Army Research Office (ARO #59155-LS).

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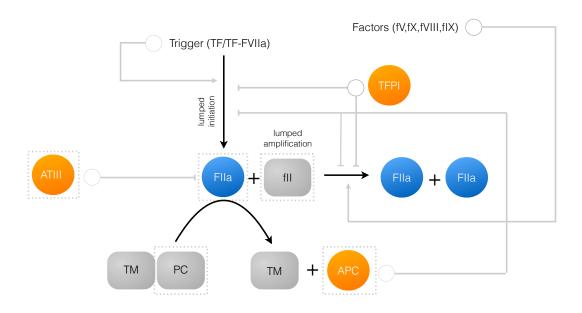


Fig. 1: Schematic of the connectivity of the reduced order coagulation model. A trigger compound e.g., TF/FVIIa initiates thrombin production (FIIa) from prothrombin (fII). Once activated, thrombin catalyzes its own activation (amplification step), as well as its own inhibition via the conversion of protein C to activated protein C (APC). APC and tissue factor pathway inhibitor (TFPI) inhibit initiation and amplification, while antithrombin III (ATIII) directly inhibits thrombin. All inhibition steps, and trigger-induced initiation were modeled using a rule-based approach. Likewise, the dependence of amplification on other coagulation factors was also modeled using a rule-based approach. The abundance of the highlighted species (in the dashed boxes) was governed by an ordinary differential equation. All other species were assumed to be constant.

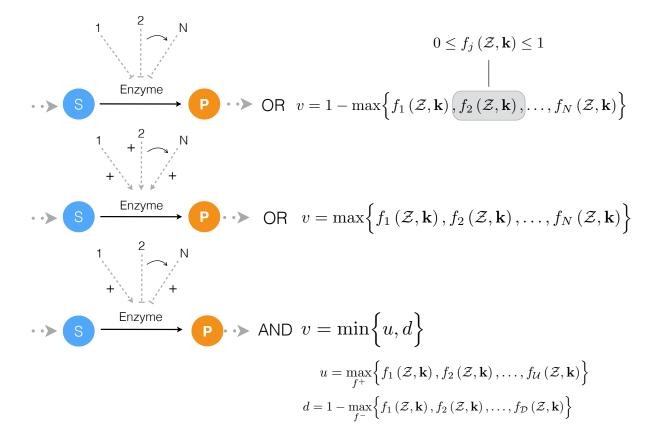


Fig. 2: Schematic of rule based effective control laws. Traditional enzyme kinetic expressions e.g., Michaelis-Menten or multiple saturation kinetics are multiplied by an enzyme activity control variable $0 \le v_j \le 1$. Control variables are functions of many possible regulatory factors encoded by arbitrary functions of the form $0 \le f_j(\mathcal{Z}) \le 1$. At each simulation time step, the v_j variables are calculated by evaluating integration rules such as the max or min of the set of factors f_1, \ldots, f_n influencing the activity of enzyme E_j .

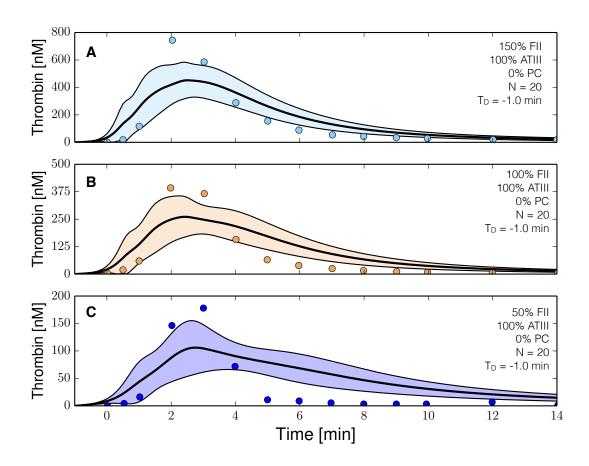


Fig. 3: Reduced order coagulation model training simulations. Reduced order coagulation model parameters were estimated using particle swarm optimization (PSO) with and without the protein C pathway as a function of prothrombin. Solid lines denote the simulated mean value of the thrombin profile for N = 20 independent particles, points denote experimental data. The shaded region denotes the 99% confidence estimate of the mean simulated thrombin value (uncertainty in the model simulation). (A,B,C) training results for 150%, 100% and 50% of physiological prothrombin levels in the absence of the protein C pathway. Thrombin generation was initiated using 5 pmol/L FVIIa-TF in the presence of 200 μ mol/L of phospholipid vesicles (PCPS). All factors and control proteins were at their physiological concentration unless others denoted. The experimental training data was reproduced from the study of Butenas et al. [40].

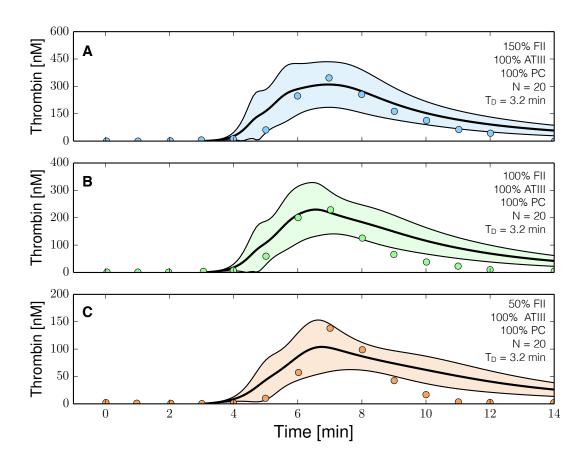


Fig. 4: Reduced order coagulation model training simulations. Reduced order coagulation model parameters were estimated using particle swarm optimization (PSO) with and without the protein C pathway as a function of prothrombin. Solid lines denote the simulated mean value of the thrombin profile for N = 20 independent particles, points denote experimental data. The shaded region denotes the 99% confidence estimate of the mean simulated thrombin value (uncertainty in the model simulation). (A,B,C) training results for 150%, 100% and 50% of physiological prothrombin levels in the presence of the protein C pathway. Only APC pathway parameters were allowed to vary in the simulations on the right. Thrombin generation was initiated using 5 pmol/L FVIIa-TF in the presence of 200 μ mol/L of phospholipid vesicles (PCPS). All factors and control proteins were at their physiological concentration unless others denoted. The experimental training data was reproduced from the study of Butenas et al. [40].

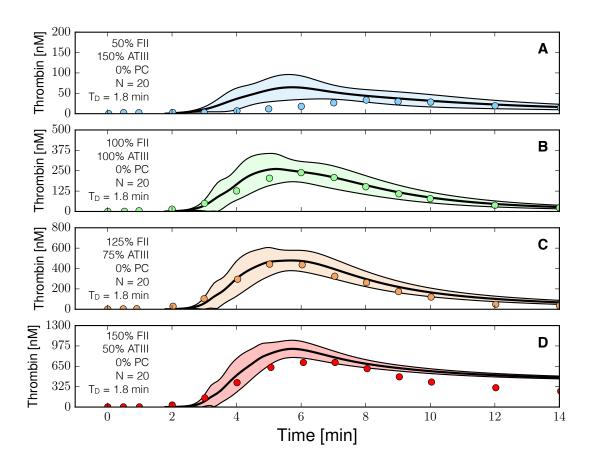


Fig. 5: Reduced order coagulation model predictions versus experimental data for normal coagulation. The reduced order coagulation model parameter estimates were tested against data not used during model training. Simulations of different levels of prothrombin and ATIII were compared with experimental data in the absence of the protein C pathway. Solid lines denote the simulated mean value of the thrombin profile for N = 20 independent particles, points denote experimental data. The shaded region denotes the 99% confidence estimate of the mean simulated thrombin value (uncertainty in the model simulation). (A,B,C,D) prediction results for (FII,ATIII): (50%,150%), (100%, 100%), (125%, 75%) and (150%, 50%) of physiological prothrombin and ATIII levels in the absence of the protein C pathway. Thrombin generation was initiated using 5 pmol/L FVIIa-TF in the presence of 200 μ mol/L of phospholipid vesicles (PCPS). All factors and control proteins were at their physiological concentration unless others denoted. The experimental validation data was reproduced from the study of Butenas et al. [40]

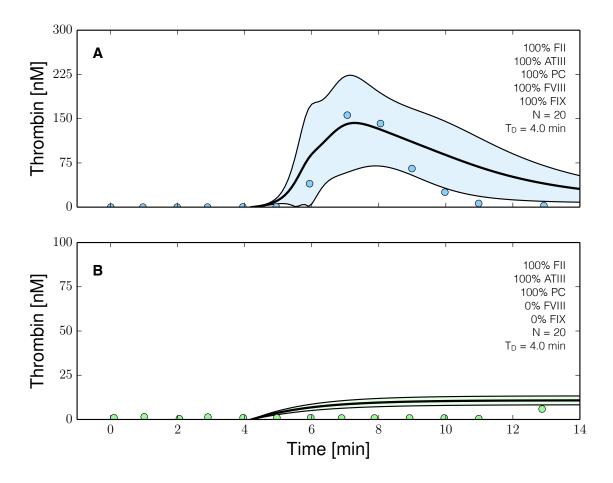


Fig. 6: Reduced order coagulation model predictions versus experimental data with and without FVIII and FIX. The reduced order coagulation model parameter estimates were tested against data not used during model training. Simulations of normal thrombin formation with ATIII and the protein C pathway were compared with thrombin formation in the absence of fVIII and fIX. Solid lines denote the simulated mean value of the thrombin profile for N = 20 independent particles, points denote experimental data. The shaded region denotes the 99% confidence estimate of the mean simulated thrombin value (uncertainty in the model simulation). (A,B) prediction results for normal thrombin generation and thrombin generation in hemophilia. All factors and control proteins were at their physiological concentration unless others noted. The experimental validation data was reproduced from the study of Allen et al. [41].

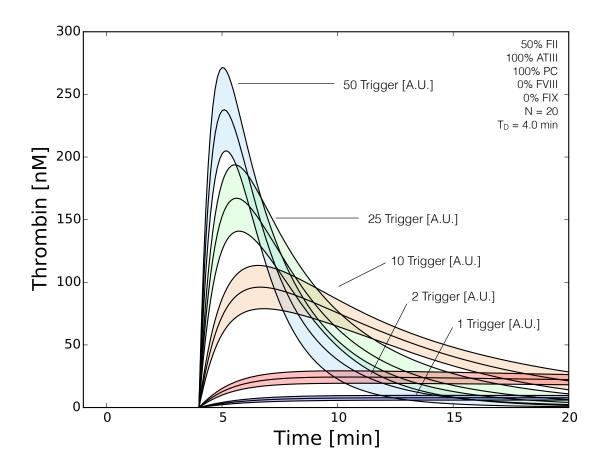


Fig. 7: Reduced order coagulation model predictions of rFVIIa administration. Simulations of thrombin formation in the presence of ATIII and the protein C pathway were conducted for a range of trigger values (1x - 50x) in the absence of fVIII and fIX. Solid lines denote the simulated mean value of the thrombin profile for N = 20 independent particles. The shaded region denotes the 99% confidence estimate of the mean simulated thrombin value (uncertainty in the model simulation). All factors and control proteins were at their physiological concentration unless others noted.

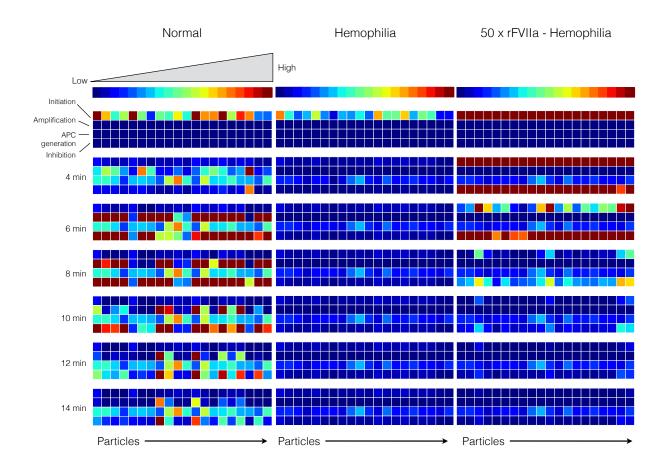


Fig. 8: Reaction flux distribution as a function of time for thrombin generation under normal (left), hemophilia (center) and rFVIIa treated hemophilia (right). Reaction flux was calculated for each particle at T=0,4,6,8,10,12,14 min after the initiation of coagulation. Reaction fluxes were calculated for each particle in the parameter ensemble (N = 20). Blue colors denote low flux values while red colors denote high flux values.

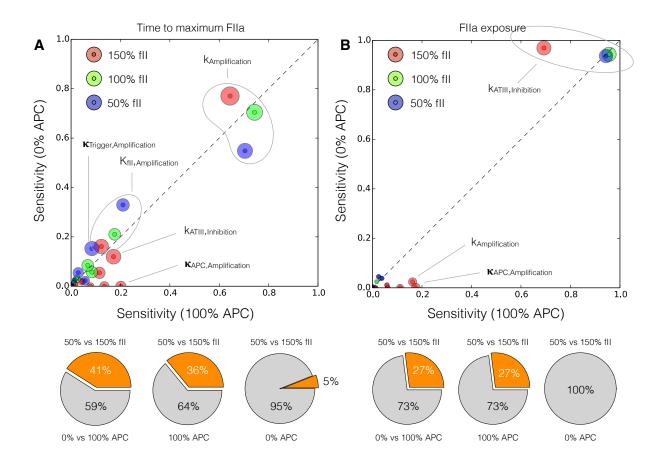


Fig. 9: Global sensitivity analysis of the reduced order coagulation model with with respect to the model parameters. A: Sensitivity analysis of the thrombin peak time for different prothrombin levels (150%,100% and 50% of the physiological value) as a function of activated protein C. B: Sensitivity analysis of the thrombin exposure for different prothrombin levels (150%,100% and 50% of the physiological value) as a function of activated protein C. Points denote the mean total sensitivity value, while the area around each point denotes the uncertainty in the sensitivity value. The gray dashed line denotes the 45° degree diagonal, if sensitivity values are equal for different conditions they will lie on the diagonal. Sensitivity values significantly above or below the diagonal indicate differentially important model parameters.