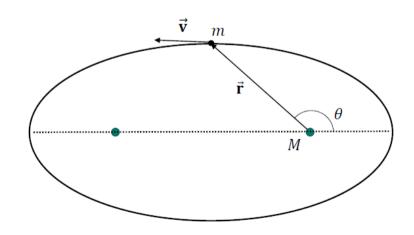
## **Orbit Description**

- It is sufficient to describe an orbit in terms of the orbital state vectors (or Cartesian vectors), position,  $\vec{\mathbf{r}}(t)$ , and velocity,  $\vec{\mathbf{v}}(t)$ , and a given time, t
- We have found the equations of motion for the object: (a coupled system of second order ODES)

$$\dot{\vec{\mathbf{r}}} = \vec{\mathbf{v}}, \qquad \vec{\mathbf{r}}(0) = \vec{\mathbf{r}}_0$$

$$\dot{\vec{\mathbf{v}}} = -\frac{\mu}{r^3}\vec{\mathbf{r}}, \qquad \vec{\mathbf{v}}(0) = \vec{\mathbf{v}}_0$$

 For convenience, other sets of elements are used to describe orbits, let's look at the six:
 "classical orbital elements"





#### **Review of Frames**

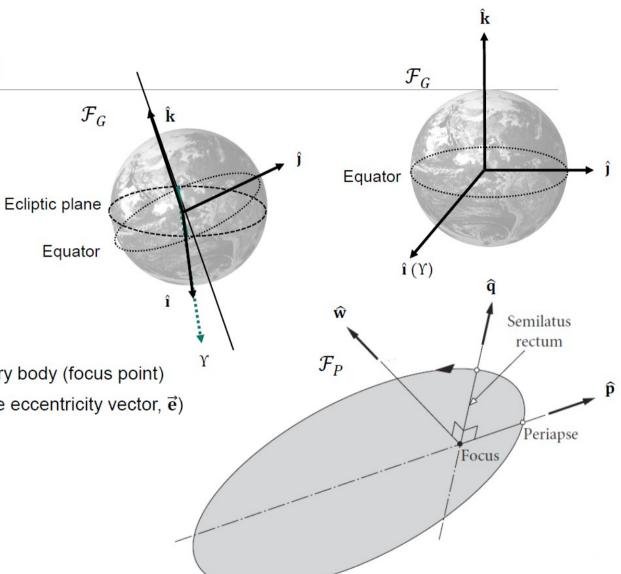
Geocentric-Equatorial Frame  $(\mathcal{F}_G)$ 

- Origin,  $O_G$ , at Earth's center of mass
- $\hat{\mathbf{g}}_1$  in the direction of the vernal equinox  $(\Upsilon)$
- ĝ<sub>3</sub> towards Earth's north pole
- $\hat{\mathbf{g}}_2$  completes the right-hand rule

#### Perifocal Frame $(\mathcal{F}_P)$

- Origin, O<sub>P</sub>, at the center of mass of the primary body (focus point)
- $\widehat{p}_1$  towards the orbit's periapsis (parallel to the eccentricity vector,  $\overrightarrow{e}$ )
- $\hat{\mathbf{p}}_3$  normal to the orbit's plane (parallel to  $\vec{\mathbf{h}}$ )





The last three parameters also define a set of 3-1-3 Euler angles

# **Classical Orbital Elements**

#### Classical Orbital Elements (COEs)

Specific angular momentum, h (or semi-major axis, a)

Eccentricity, e

True anomaly,  $\theta$  (also, sometime  $\nu$ ) (or sometimes epoch)

 $0^{\circ} < \theta < 360^{\circ}$ 

Right ascension of the ascending node,  $\Omega$ (RAAN)  $0^{\circ} \leq \Omega < 360^{\circ}$ 

Inclination, i

 $0^{\circ} < i < 180^{\circ}$ 

Argument of perigee,  $\omega$  0°  $\leq \omega < 360^{\circ}$ 

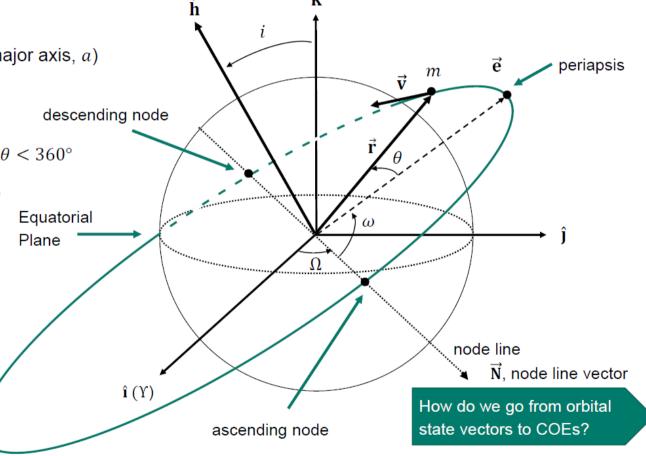
 $i = 0^{\circ} \text{ or } 180^{\circ} \rightarrow \text{Equatorial}$ 

 $i < 90^{\circ} \rightarrow \text{Prograde}$ 

 $i = 90^{\circ} \rightarrow Polar$ 

 $i > 90^{\circ} \rightarrow \text{Retrograde}$ 

Clarkson [De Ruiter, Ch. 3; Curtis, Ch. 4]



#### Algorithm: COEs from State Vectors

$$\vec{\mathbf{r}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$$
$$\vec{\mathbf{v}} = v_x\hat{\mathbf{i}} + v_y\hat{\mathbf{j}} + v_z\hat{\mathbf{k}}$$

#### 1. Calculate the distance:

$$r = \sqrt{\vec{\mathbf{r}} \cdot \vec{\mathbf{r}}}$$
$$r = \sqrt{x^2 + y^2 + z^2}$$

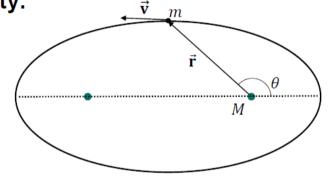
### 2. Calculate the speed:

$$v = \sqrt{\vec{\mathbf{v}} \cdot \vec{\mathbf{v}}}$$
$$v = \sqrt{v_x^2 + v_y^2 + v_z^2}$$

Clarkson [De Ruiter, Ch. 3; Curtis, Ch. 4]

# 3. Calculate the radial velocity:

$$v_r = \frac{\vec{\mathbf{v}} \cdot \vec{\mathbf{r}}}{r}$$
$$v_r = \frac{(xv_x + yv_y + zv_z)}{r}$$

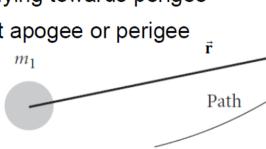


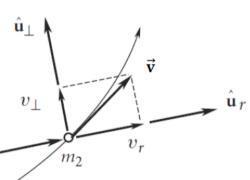
Note:

 $v_r > 0 \leftarrow$  Flying away from perigee

 $v_r < 0 \leftarrow$  Flying towards perigee

 $v_r = 0 \leftarrow \text{At apogee or perigee}$ 





# Algorithm: COEs from State Vectors (cont.)

$$\vec{\mathbf{r}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$$
$$\vec{\mathbf{v}} = v_x\hat{\mathbf{i}} + v_y\hat{\mathbf{j}} + v_z\hat{\mathbf{k}}$$

# 4. Calculate the specific angular momentum:

$$\vec{h} = \vec{r} \times \vec{v}$$

$$\vec{\mathbf{h}} = \begin{vmatrix} \hat{\mathbf{i}} & \hat{\mathbf{j}} & \hat{\mathbf{k}} \\ x & y & z \\ v_x & v_y & v_z \end{vmatrix}$$

$$\mathbf{\dot{h}} = (yv_z - zv_y)\mathbf{\hat{i}} + (zv_x - xv_z)\mathbf{\hat{j}} + (xv_y - yv_x)\mathbf{\hat{k}}$$

$$\mathbf{\dot{h}} = h_x\mathbf{\hat{i}} + h_y\mathbf{\hat{j}} + h_z\mathbf{\hat{k}}$$

Clarkson [De Ruiter, Ch. 3; Curtis, Ch. 4]

# 5. Calculate the magnitude of the specific angular momentum:

$$h = \sqrt{\vec{\mathbf{h}} \cdot \vec{\mathbf{h}}}$$

$$h = \sqrt{h_x^2 + h_y^2 + h_z^2} \leftarrow$$
First orbital element

# Algorithm: COEs from State Vectors (cont.)

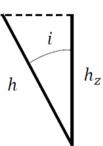
$$\vec{\mathbf{r}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$$
$$\vec{\mathbf{v}} = v_x\hat{\mathbf{i}} + v_y\hat{\mathbf{j}} + v_z\hat{\mathbf{k}}$$

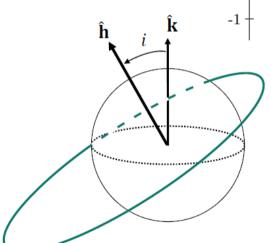
#### 6. Calculate the inclination

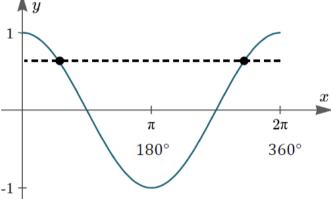
$$\mathbf{\dot{h}} = h_x \mathbf{\hat{i}} + h_y \mathbf{\hat{j}} + h_z \mathbf{\hat{k}}$$

$$\cos i = \frac{h_z}{h}$$

$$i = \cos^{-1}\left(\frac{h_z}{h}\right) \leftarrow \underline{\text{Second orbital element}}$$







Recall,  $0^{\circ} \le i \le 180^{\circ}$ So, no quadrant ambiguity

 $i = 0^{\circ} \text{ or } 180^{\circ} \rightarrow \text{Equatorial}$  $i < 90^{\circ} \rightarrow \text{Prograde}$  $i = 90^{\circ} \rightarrow \text{Polar}$ 

 $i > 90^{\circ} \rightarrow \text{Retrograde}$ 

Clarkson [De Ruiter, Ch. 3; Curtis, Ch. 4; "Graphs of...", https://www.intmath.com/trigonometric-graphs/1-graphs-sine-cosine-amplitude.php , 2018]

# Algorithm: COEs from State Vectors (cont.)

$$\vec{\mathbf{r}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$$
$$\vec{\mathbf{v}} = v_x\hat{\mathbf{i}} + v_y\hat{\mathbf{j}} + v_z\hat{\mathbf{k}}$$

#### 7. Calculate the node line vector:

$$\vec{N} = \hat{k} \times \vec{h}$$

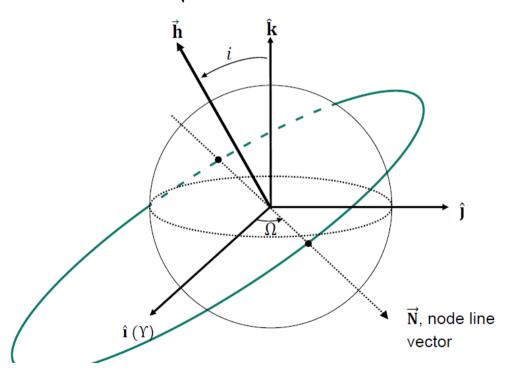
$$\vec{\mathbf{N}} = \begin{vmatrix} \hat{\mathbf{i}} & \hat{\mathbf{j}} & \hat{\mathbf{k}} \\ 0 & 0 & 1 \\ h_x & h_y & h_z \end{vmatrix}$$

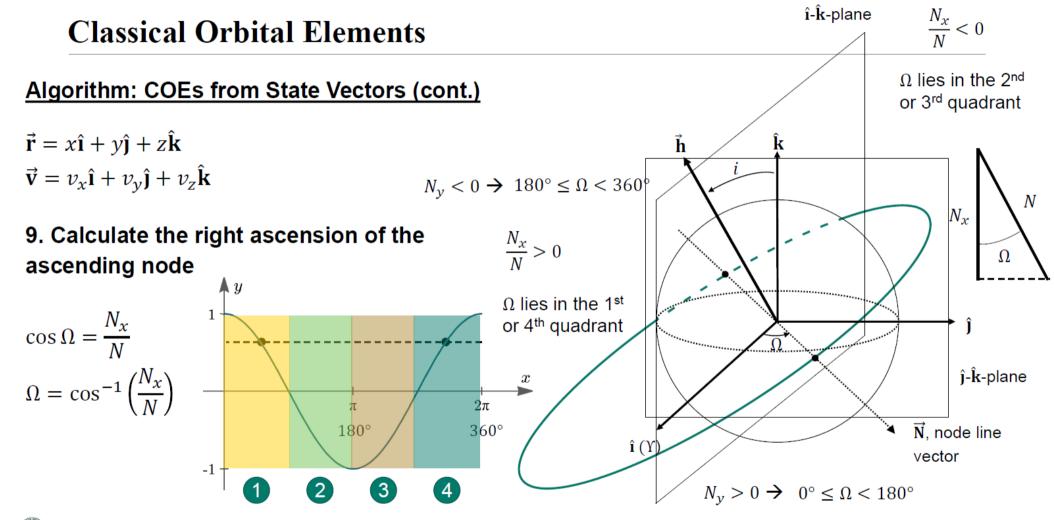
$$\vec{\mathbf{N}} = (-h_y)\hat{\mathbf{i}} + (h_x)\hat{\mathbf{j}} + (0)\hat{\mathbf{k}} = N_x\hat{\mathbf{i}} + N_y\hat{\mathbf{j}}$$

Clarkson [De Ruiter, Ch. 3; Curtis, Ch. 4]

# 8. Calculate the magnitude of the node line vector:

$$N = \sqrt{\overrightarrow{\mathbf{N}} \cdot \overrightarrow{\mathbf{N}}} = \sqrt{N_x^2 + N_y^2}$$





Clarkson [De Ruiter, Ch. 3; Curtis, Ch. 4; "Graphs of…", https://www.intmath.com/trigonometric-graphs/1-graphs-sine-cosine-amplitude.php , 2018]

 $\frac{N_x}{N} < 0$ 

î-k-plane

 $\Omega$  lies in the 2<sup>nd</sup> or 3<sup>rd</sup> quadrant

# Algorithm: COEs from State Vectors (cont.)

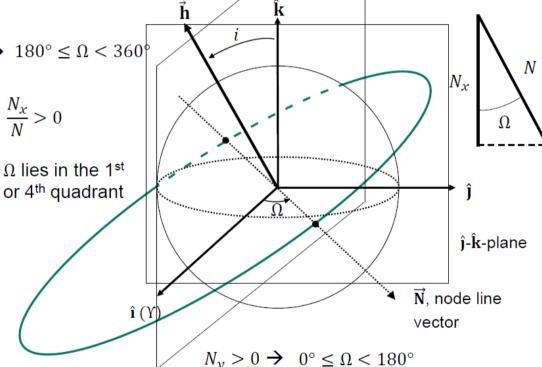
$$\vec{\mathbf{r}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$$
$$\vec{\mathbf{v}} = v_x\hat{\mathbf{i}} + v_y\hat{\mathbf{j}} + v_z\hat{\mathbf{k}}$$

# $N_y < 0 \rightarrow 180^\circ \le \Omega < 360^\circ$

# 9. Calculate the right ascension of the ascending node

$$\Omega = \begin{cases} \cos^{-1}\left(\frac{N_x}{N}\right), & (N_y \ge 0) \\ 360^{\circ} - \cos^{-1}\left(\frac{N_x}{N}\right) & (N_y < 0) \end{cases}$$

Third orbital element



(Clarkson [De Ruiter, Ch. 3; Curtis, Ch. 4; "Graphs of…", https://www.intmath.com/trigonometric-graphs/1-graphs-sine-cosine-amplitude.php, 2018]

# Algorithm: COEs from State Vectors (cont.)

$$\vec{\mathbf{r}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$$
$$\vec{\mathbf{v}} = v_x\hat{\mathbf{i}} + v_y\hat{\mathbf{j}} + v_z\hat{\mathbf{k}}$$

# 10. Calculate the eccentricity vector:

$$\vec{\mathbf{e}} = \frac{1}{\mu} \left[ \vec{\mathbf{v}} \times \vec{\mathbf{h}} - \mu \frac{\vec{\mathbf{r}}}{r} \right] = \frac{1}{\mu} \left[ \vec{\mathbf{v}} \times (\vec{\mathbf{r}} \times \vec{\mathbf{v}}) - \mu \frac{\vec{\mathbf{r}}}{r} \right]$$

$$\vec{\mathbf{e}} = \frac{1}{\mu} \left[ \vec{\mathbf{v}} \times (\vec{\mathbf{r}} \times \vec{\mathbf{v}}) - \mu \frac{\vec{\mathbf{r}}}{r} \right] = \frac{1}{\mu} \left[ \vec{\mathbf{r}} v^2 - \vec{\mathbf{v}} (\vec{\mathbf{r}} \cdot \vec{\mathbf{v}}) - \mu \frac{\vec{\mathbf{r}}}{r} \right]$$

$$\vec{\mathbf{e}} = \frac{1}{\mu} \left[ \left( v^2 - \frac{\mu}{r} \right) \vec{\mathbf{r}} - r v_r \vec{\mathbf{v}} \right]$$
 Vector Triple Product:  $\mathbf{a} \times (\mathbf{b} \times \mathbf{c}) = \mathbf{b} (\mathbf{a} \cdot \mathbf{c}) - \mathbf{c} (\mathbf{a} \cdot \mathbf{b})$ 

$$\mathbf{a} \times (\mathbf{b} \times \mathbf{c}) = \mathbf{b}(\mathbf{a} \cdot \mathbf{c}) - \mathbf{c}(\mathbf{a} \cdot \mathbf{b})$$

$$v_r = \frac{\vec{\mathbf{v}} \cdot \vec{\mathbf{r}}}{r}$$

## 11. Calculate the eccentricity:

$$e = \sqrt{\vec{\mathbf{e}} \cdot \vec{\mathbf{e}}}$$

$$e = \sqrt{e_x^2 + e_y^2 + e_z^2}$$

Or, we can find in terms of scalars:

$$e = \frac{1}{\mu} \sqrt{(2\mu - rv^2)rv_r^2 + (\mu - rv^2)^2}$$

Fourth orbital element

 $\vec{\mathbf{N}} \cdot \vec{\mathbf{e}} < 0$ 

 $\Omega$  lies in the 2<sup>nd</sup>

or 3<sup>rd</sup> quadrant

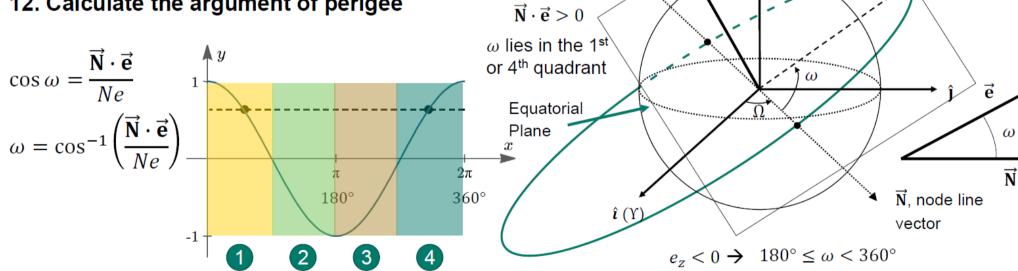
 $\widehat{\it N}_{\perp}$ -plane

 $e_z > 0 \rightarrow 0^{\circ} \le \omega < 180^{\circ}$ 

# Algorithm: COEs from State Vectors (cont.)

$$\vec{\mathbf{r}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$$
$$\vec{\mathbf{v}} = v_x\hat{\mathbf{i}} + v_y\hat{\mathbf{j}} + v_z\hat{\mathbf{k}}$$

# 12. Calculate the argument of perigee



Clarkson [De Ruiter, Ch. 3; Curtis, Ch. 4; "Graphs of...", https://www.intmath.com/trigonometric-graphs/1-graphs-sine-cosine-amplitude.php, 2018]

 $\vec{\mathbf{N}} \cdot \vec{\mathbf{e}} < 0$ 

# Algorithm: COEs from State Vectors (cont.)

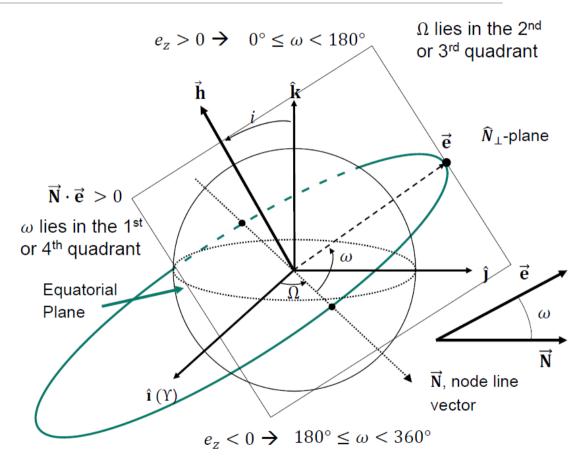
$$\vec{\mathbf{r}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$$

$$\vec{\mathbf{v}} = v_x\hat{\mathbf{i}} + v_y\hat{\mathbf{j}} + v_z\hat{\mathbf{k}}$$

## 12. Calculate the argument of perigee

$$\omega = \begin{cases} \cos^{-1}\left(\frac{\vec{\mathbf{N}} \cdot \vec{\mathbf{e}}}{Ne}\right), & (e_z \ge 0) \\ 360^{\circ} - \cos^{-1}\left(\frac{\vec{\mathbf{N}} \cdot \vec{\mathbf{e}}}{Ne}\right) & (e_z < 0) \end{cases}$$

Fifth orbital element



Clarkson [De Ruiter, Ch. 3; Curtis, Ch. 4; "Graphs of...", https://www.intmath.com/trigonometric-graphs/1-graphs-sine-cosine-amplitude.php, 2018]

Flying away from perigee

 $v_r \ge 0, \, 0^{\circ} \le \theta < 180^{\circ}$ 

 $\vec{\mathbf{e}} \cdot \vec{\mathbf{r}} > 0$ 

 $v_r < 0$ ,

 $180^{\circ} \le \theta < 360^{\circ}$ 

 $\theta$  lies in the 1st or 4th quadrant

# Classical Orbital Elements

# Algorithm: COEs from State Vectors (cont.)

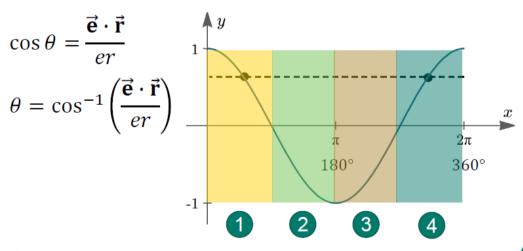
$$\vec{\mathbf{r}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$$
$$\vec{\mathbf{v}} = v_x\hat{\mathbf{i}} + v_y\hat{\mathbf{j}} + v_z\hat{\mathbf{k}}$$

 $\theta$  lies in the 2<sup>nd</sup> or 3<sup>rd</sup> quadrant

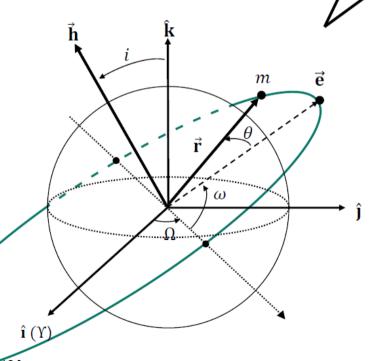
 $\vec{\mathbf{e}} \cdot \vec{\mathbf{r}} < 0$ 

Flying towards perigee

# 13. Calculate the true anomaly



Clarkson [De Ruiter, Ch. 3; Curtis, Ch. 4; "Graphs of...", https://www.intmath.com/trigonometric-graphs/1-graphs-sine-cosine-amplitude.php



Flying away from perigee 4

 $v_r \ge 0$ ,  $0^{\circ} \le \theta < 180^{\circ}$ 

#### $\vec{\mathbf{e}} \cdot \vec{\mathbf{r}} > 0$

 $\theta$  lies in the 1st or 4th quadrant

# **Classical Orbital Elements**

# Algorithm: COEs from State Vectors (cont.)

$$\vec{\mathbf{r}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$$
$$\vec{\mathbf{v}} = v_x\hat{\mathbf{i}} + v_y\hat{\mathbf{j}} + v_z\hat{\mathbf{k}}$$

# $\vec{\mathbf{e}} \cdot \vec{\mathbf{r}} < 0$ $\theta$ lies in the 2<sup>nd</sup> or 3<sup>rd</sup> quadrant

# Flying towards perigee

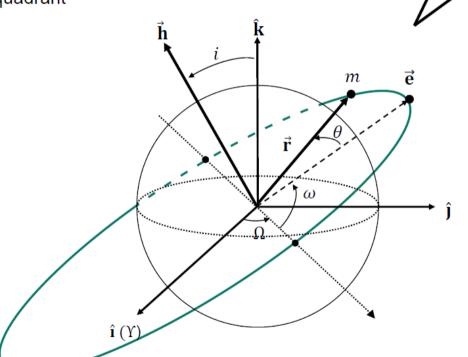
 $v_r < 0$ ,

 $180^{\circ} \le \theta < 360^{\circ}$ 

# 13. Calculate the true anomaly

$$\theta = \begin{cases} \cos^{-1}\left(\frac{\vec{\mathbf{e}} \cdot \vec{\mathbf{r}}}{er}\right), & (v_r \ge 0) \\ 360^{\circ} - \cos^{-1}\left(\frac{\vec{\mathbf{e}} \cdot \vec{\mathbf{r}}}{er}\right) & (v_r < 0) \end{cases}$$

Sixth orbital element



Clarkson [De Ruiter, Ch. 3; Curtis, Ch. 4; "Graphs of...",

https://www.intmath.com/trigonometric-graphs/1-graphs-sine-cosine-amalitude.phr

Algorithm: COEs from State Vectors (cont.)

$$\vec{\mathbf{r}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$$

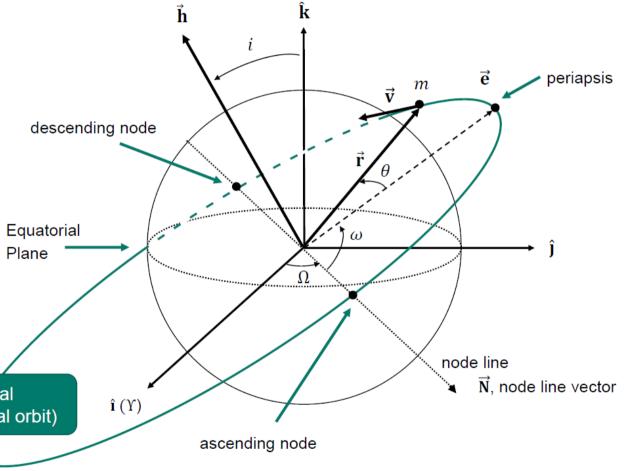
$$\vec{\mathbf{v}} = v_x \hat{\mathbf{i}} + v_y \hat{\mathbf{j}} + v_z \hat{\mathbf{k}}$$

#### Classical Orbital Elements (COEs)

- Specific angular momentum, h
- Eccentricity, e
- True anomaly,  $\theta$
- Right ascension of the ascending node, Ω
- Inclination, i
- Argument of perigee, ω

N.B. special cases exist that need special consideration (e.g., circular orbits or equatorial orbit)



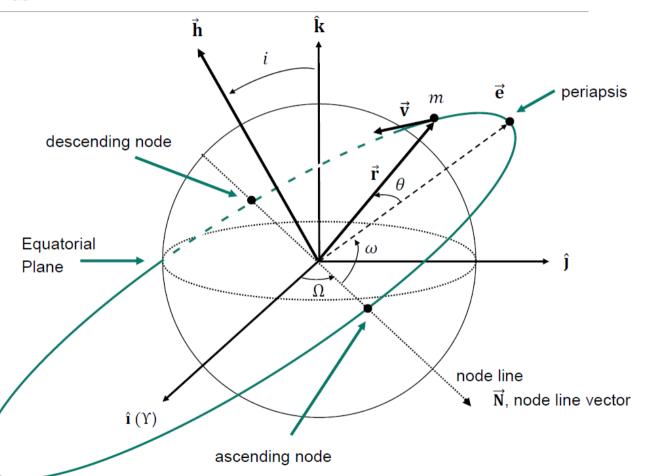


# N.B. special cases exist that need special consideration (e.g., circular orbits or equatorial orbit)

# **Classical Orbital Elements**

Cases where not all elements are defined:

- Circular orbit
  - No periapsis, so  $\omega$  is undefined
  - Instead argument of latitude,  $u \equiv \theta + \omega$  (angle from ascending node) is used
- Elliptical equatorial orbit
  - No line of nodes, so  $\Omega$  is undefined
  - Instead longitude of periapsis,  $\Pi \equiv \Omega + \omega \text{ (angle between periapsis and vernal equinox) is used}$
- Circular equatorial orbit
  - No periapsis or node line, so  $\omega$  and  $\Omega$  are undefined, as is  $\Pi$
  - True longitude,  $l = \theta + \Pi = \theta + \Omega + \omega$  (angle from the vernal equinox) may be used

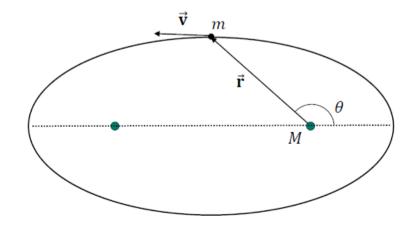




- As mentioned previously, it is sufficient to describe an orbit in terms of the orbital state vectors, position,  $\vec{\mathbf{r}}(t)$ , and velocity,  $\vec{\mathbf{v}}(t)$  and a given time, t
- If we have the classical orbital elements, we can also solve for the state vectors
- The first step is recognizing the relationship between the perifocal frame and the ECI frame

$$\dot{\vec{\mathbf{r}}} = \vec{\mathbf{v}}, \qquad \vec{\mathbf{r}}(0) = \vec{\mathbf{r}}_0$$

$$\dot{\vec{\mathbf{v}}} = -\frac{\mu}{r^3} \vec{\mathbf{r}}, \qquad \vec{\mathbf{v}}(0) = \vec{\mathbf{v}}_0$$

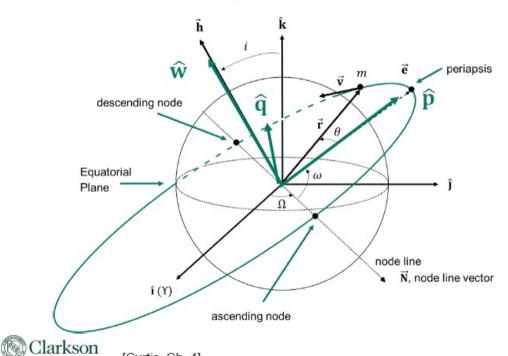


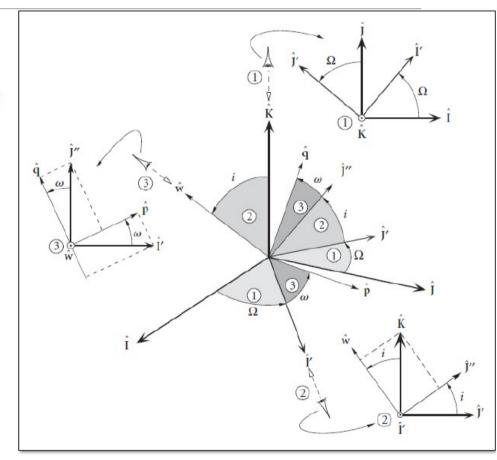


[Curtis, Ch. 4]

Transform between the **Geocentric-Equatorial Frame**  $(\mathcal{F}_G)$  to the **Perifocal Frame**  $(\mathcal{F}_P)$ 

 Rotation matrix can be represented in terms of principal axis rotations and Euler angles





 $\widehat{K} = \widehat{K}'$ 

Transform between the **Geocentric-Equatorial Frame**  $(\mathcal{F}_G)$  to the **Perifocal Frame**  $(\mathcal{F}_P)$ 

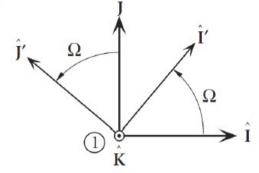
Rotation matrix can be represented in terms of principal axis
 rotations and Fuler angles.

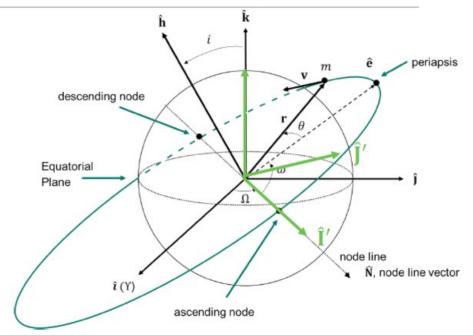
rotations and Euler angles

① Rotation about 3-axis  $(\widehat{\mathbf{K}})$ 

$$\mathbf{C}_3(\theta) = \begin{bmatrix} \cos \theta & \sin \theta & 0 \\ -\sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{C}_{3}(\Omega) = \begin{bmatrix} \cos \Omega & \sin \Omega & 0 \\ -\sin \Omega & \cos \Omega & 0 \\ 0 & 0 & 1 \end{bmatrix}$$





 $\widehat{K} = \widehat{K}'$ 

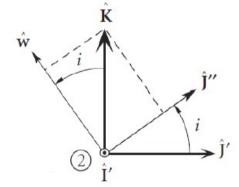
Transform between the **Geocentric-Equatorial Frame**  $(\mathcal{F}_G)$  to the **Perifocal Frame**  $(\mathcal{F}_P)$ 

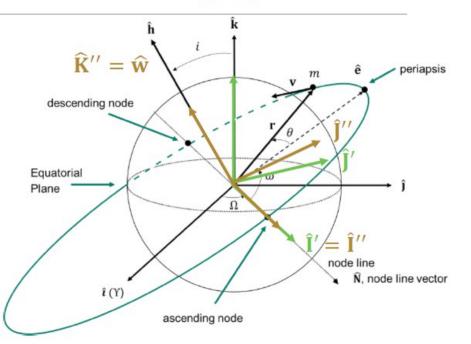
 Rotation matrix can be represented in terms of principal axis rotations and Euler angles

### ② Rotation about 1-axis $(\hat{\mathbf{l}}')$

$$\mathbf{C}_{1}(\theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & \sin \theta \\ 0 & -\sin \theta & \cos \theta \end{bmatrix}$$

$$\mathbf{C_1}(i) \equiv \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos i & \sin i \\ 0 & -\sin i & \cos i \end{bmatrix}$$



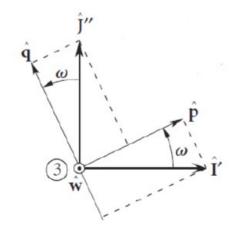


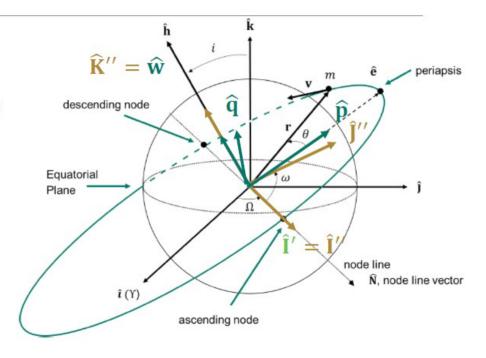
Transform between the **Geocentric-Equatorial Frame**  $(\mathcal{F}_{\mathcal{G}})$  to the **Perifocal Frame**  $(\mathcal{F}_{\mathcal{P}})$ 

- Rotation matrix can be represented in terms of principal axis rotations and Euler angles
- ③ Rotation about 3-axis  $(\hat{\mathbf{K}})$

$$\mathbf{C}_3(\theta) = \begin{bmatrix} \cos \theta & \sin \theta & 0 \\ -\sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{C}_{3}(\omega) = \begin{bmatrix} \cos \omega & \sin \omega & 0 \\ -\sin \omega & \cos \omega & 0 \\ 0 & 0 & 1 \end{bmatrix}$$





Transform between the **Geocentric-Equatorial Frame** ( $\mathcal{F}_G$ ) to

Rotation matrix can be represented in terms of principal axis rotations and Euler angles

$$\mathbf{C}_{PG} = \mathbf{C}_3(\omega)\mathbf{C}_1(i)\mathbf{C}_3(\Omega)$$

the Perifocal Frame  $(\mathcal{F}_{P})$ 

$$\mathbf{C}_{PG} = \begin{bmatrix} \cos \omega & \sin \omega & 0 \\ -\sin \omega & \cos \omega & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos i & \sin i \\ 0 & -\sin i & \cos i \end{bmatrix} \begin{bmatrix} \cos \Omega & \sin \Omega & 0 \\ -\sin \Omega & \cos \Omega & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{C}_{PG} = \begin{bmatrix} c_{\Omega}c_{\omega} - s_{\Omega}c_{i}s_{\omega} & s_{\Omega}c_{\omega} + c_{\Omega}c_{i}s_{\omega} & s_{i}s_{\omega} \\ -c_{\Omega}s_{\omega} - s_{\Omega}c_{i}c_{\omega} & -s_{\Omega}s_{\omega} + c_{\Omega}c_{i}c_{\omega} & s_{i}c_{\omega} \\ s_{\Omega}s_{i} & -c_{\Omega}s_{i} & c_{i} \end{bmatrix}$$

$$\mathbf{r}_G = \mathbf{C}_{GP} \mathbf{r}_P$$
 $\mathbf{v}_G = \mathbf{C}_{GP} \mathbf{v}_P$ 
 $\overrightarrow{\mathcal{F}}_G = \mathbf{C}_{GP} \overrightarrow{\mathcal{F}}_P$ 

(S) Clarkson

$$\mathbf{C}_{GP} = \mathbf{C}_{PG}^{\mathrm{T}}$$

$$\mathbf{r}_{G} = \mathbf{C}_{GP} \mathbf{r}_{P}$$

$$\mathbf{v}_{G} = \mathbf{C}_{GP} \mathbf{v}_{P}$$

$$\vec{\mathcal{F}}_{G} = \mathbf{C}_{GP} \vec{\mathcal{F}}_{P}$$

$$\mathbf{C}_{GP} = \mathbf{C}_{PG}^{\mathsf{T}}$$

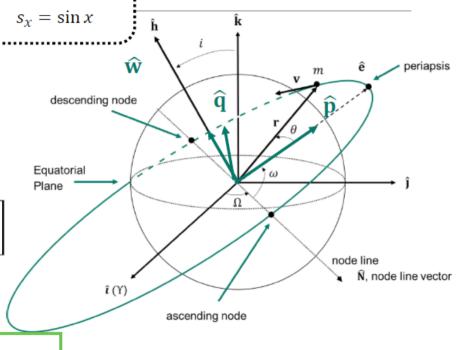
$$\mathbf{C}_{GP} = \mathbf{C}_{PG}^{\mathsf{T}}$$

$$\mathbf{C}_{GP} = \mathbf{C}_{PG}^{\mathsf{T}}$$

$$\mathbf{C}_{GP} = \begin{bmatrix} c_{\Omega} c_{\omega} - s_{\Omega} c_{i} s_{\omega} & -c_{\Omega} s_{\omega} - s_{\Omega} c_{i} c_{\omega} & s_{\Omega} s_{i} \\ s_{\Omega} c_{\omega} + c_{\Omega} c_{i} s_{\omega} & -s_{\Omega} s_{\omega} + c_{\Omega} c_{i} c_{\omega} & -c_{\Omega} s_{i} \\ s_{i} s_{\omega} & s_{i} c_{\omega} & c_{i} \end{bmatrix}$$
Clarkson

Remember!

 $C_{RA} = C_{AR}^{-1} = C_{AR}^{T}$ 



For simplicity:

 $c_x = \cos x$ 

[De Ruiter, Ch. 3; Curtis, Ch. 4]

$$\vec{\mathbf{r}} = \overrightarrow{\boldsymbol{\mathcal{F}}}_{G}^{T} \mathbf{r}_{G} \qquad \overrightarrow{\boldsymbol{\mathcal{F}}}_{G}^{T} = \begin{bmatrix} \hat{\mathbf{i}} & \hat{\mathbf{j}} & \hat{\mathbf{k}} \end{bmatrix}$$
$$\vec{\mathbf{v}} = \overrightarrow{\boldsymbol{\mathcal{F}}}_{G}^{T} \mathbf{v}_{G}$$

Now, given our orbital elements  $(h, e, i, \Omega, \omega, \text{ and } \theta)$  we can compute the state vectors  $(\mathbf{r}_G \text{ and } \mathbf{v}_G)$  in the ECI frame:

1. Find the position vector in  $\mathcal{F}_{p}$ :  $\overrightarrow{\mathcal{F}}_{p}^{T} = [\widehat{\mathbf{p}} \ \widehat{\mathbf{q}} \ \widehat{\mathbf{w}}]$ 

$$\overrightarrow{\boldsymbol{\mathcal{F}}}_{P}^{\mathrm{T}} = [\widehat{\mathbf{p}} \quad \widehat{\mathbf{q}} \quad \widehat{\mathbf{w}}]$$

$$\vec{\mathbf{r}} = \vec{\mathcal{F}}_p^{\mathrm{T}} \mathbf{r}_p$$

$$\mathbf{r}_p = [r \cos \theta \quad r \sin \theta \quad 0]^{\mathrm{T}}$$

$$r = \frac{h^2/\mu}{1 + e\cos\theta}$$

2. Find the velocity vector in  $\mathcal{F}_p$ :

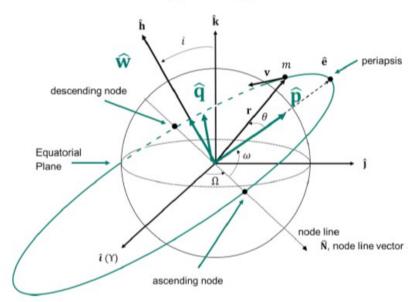
$$\vec{\mathbf{v}} = \vec{\mathcal{F}}_{P}^{\mathrm{T}} \mathbf{v}_{P}$$

$$\mathbf{v}_{P} = \begin{bmatrix} -\frac{\mu}{h} \sin \theta & \frac{\mu}{h} (e + \cos \theta) & 0 \end{bmatrix}^{\mathrm{T}}$$

3. Find the rotation matrix  $C_{GP}$ :

$$\mathbf{C}_{GP} = \begin{bmatrix} c_{\Omega}c_{\omega} - s_{\Omega}c_{i}s_{\omega} & -c_{\Omega}s_{\omega} - s_{\Omega}c_{i}c_{\omega} & s_{\Omega}s_{i} \\ s_{\Omega}c_{\omega} + c_{\Omega}c_{i}s_{\omega} & -s_{\Omega}s_{\omega} + c_{\Omega}c_{i}c_{\omega} & -c_{\Omega}s_{i} \\ s_{i}s_{\omega} & s_{i}c_{\omega} & c_{i} \end{bmatrix} \qquad \mathbf{r}_{G} = \mathbf{C}_{GP}\mathbf{r}_{P}$$

$$\mathbf{v}_{G} = \mathbf{C}_{GP}\mathbf{v}_{P}$$



4. Solve for  $\mathbf{r}_G$  and  $\mathbf{v}_G$ :

$$\mathbf{r}_G = \mathbf{C}_{GP} \mathbf{r}_P$$
$$\mathbf{v}_G = \mathbf{C}_{GP} \mathbf{v}_P$$

[Curtis, Ch. 4]

#### Example

For a given earth orbit, the elements are:  $h = 70,000 \text{ km}^2/\text{s}$ , e = 0.74,  $i = 63.4^\circ$ ,  $\Omega = 40^\circ$ ,  $\omega = 270^\circ$  and  $\theta = 30^\circ$ . Find the state vectors ( $\mathbf{r}_G$  and  $\mathbf{v}_G$ ) in the ECI frame.

1. Find the position vector in  $\mathcal{F}_P$ :

$$\vec{\mathbf{r}} = \vec{\mathcal{F}}_{p}^{T} \mathbf{r}_{p}$$

$$\mathbf{r}_{p} = [r \cos \theta \quad r \sin \theta \quad 0]^{T}$$

$$\mathbf{r}_{p} = [(7492 \text{ km}) \cos 30^{\circ} \quad (7492 \text{ km}) \sin 30^{\circ} \quad 0]^{T}$$

$$\mathbf{r}_{p} = [6488 \text{ km} \quad 3746 \text{ km} \quad 0]^{T}$$

2. Find the velocity vector in  $\mathcal{F}_p$ :

$$\vec{\mathbf{v}} = \vec{\mathbf{F}}_{P}^{T} \mathbf{v}_{P}$$

$$\mathbf{v}_{P} = \left[ -\frac{\mu}{h} \sin \theta - \frac{\mu}{h} (e + \cos \theta) - 0 \right]^{T} = \left[ -\frac{(398,600 \text{ km}^{3}/\text{s}^{2})}{(70,000 \text{ km}^{2}/\text{s})} \sin 30^{\circ} - \frac{(398,600 \text{ km}^{3}/\text{s}^{2})}{(70,000 \text{ km}^{2}/\text{s})} ((0.74) + \cos 30^{\circ}) - 0 \right]^{T}$$

$$\mathbf{v}_{P} = [-2.847 \text{ km/s} - 9.145 \text{ km/s} - 0]^{T}$$



[Curtis, Ch. 4]

#### **Example**

For a given Earth orbit, the elements are:  $h = 70,000 \text{ km}^2/s$ , e = 0.74,  $i = 63.4^\circ$ ,  $\Omega = 40^\circ$ ,  $\omega = 270^\circ$  and  $\theta = 30^\circ$ . Find the state vectors ( $\mathbf{r}_G$  and  $\mathbf{v}_G$ ) in the ECI frame.

#### 3. Find the rotation matrix $C_{GP}$ :

$$\mathbf{C}_{GP} = \begin{bmatrix} c_{\Omega}c_{\omega} - s_{\Omega}c_{i}s_{\omega} & -c_{\Omega}s_{\omega} - s_{\Omega}c_{i}c_{\omega} & s_{\Omega}s_{i} \\ s_{\Omega}c_{\omega} + c_{\Omega}c_{i}s_{\omega} & -s_{\Omega}s_{\omega} + c_{\Omega}c_{i}c_{\omega} & -c_{\Omega}s_{i} \\ s_{i}s_{\omega} & s_{i}c_{\omega} & c_{i} \end{bmatrix}$$

$$\mathbf{C}_{GP} = \begin{bmatrix} s_{11}c_{32} & s_{11}c_{13} & s_{11}c_{13} & s_{11}c_{13} & s_{11}c_{13} & s_{11}c_{13} \\ s_{12}c_{32} & -s_{12}s_{33} & -c_{12}s_{33} & -c_{12}s_{33} \\ s_{13}c_{32} & s_{12}c_{33} & -c_{12}s_{33} & c_{12}s_{33} \\ s_{13}c_{32}c_{270}c_{270}c_{340}c_{63,4}c_{270}c_{33}c_{270}c_{340}c_{63,4}c_{270}c_{270}c_{340}c_{63,4}c_{270}c_{270}c_{340}c_{63,4}c_{270}c_{33}c_{33}c_{33}c_{270}c_{33}c_{33}c_{270}c_{33}c_{33}c_{270}c_{33}c_{33}c_{270}c_{33}c_{33}c_{270}c_{33}c_{33}c_{270}c_{33}c_{33}c_{270}c_{33}c_{33}c_{270}c_{33}c_{33}c_{270}c_{33}c_{33}c_{33}c_{270}c_{33}c_{33}c_{33}c_{270}c_{33}c_{33}c_{33}c_{270}c_{33}c_{33}c_{33}c_{270}c_{33}c_{3$$

$$\mathbf{C}_{GP} = \begin{bmatrix} 0.2878 & 0.766 & 0.5748 \\ -0.343 & 0.6428 & -0.685 \\ -0.8942 & 0 & 0.4477 \end{bmatrix}$$

# (Clarkson

[Curtis, Ch. 4]

#### 4. Solve for $\mathbf{r}_G$ and $\mathbf{v}_G$ :

$$\mathbf{r}_G = \mathbf{C}_{GP}\mathbf{r}_P$$

$$\mathbf{r}_{G} = \begin{bmatrix} 0.2878 & 0.766 & 0.5748 \\ -0.343 & 0.6428 & -0.685 \\ -0.8942 & 0 & 0.4477 \end{bmatrix} \begin{bmatrix} 6488 \text{ km} \\ 3746 \text{ km} \\ 0 \end{bmatrix}$$

$$\mathbf{r}_G = [4737 \, \text{km} \, 182 \, \text{km} \, -5802 \, \text{km}]^{\mathrm{T}}$$

$$\mathbf{v}_G = \mathbf{C}_{GP} \mathbf{v}_P$$

$$\mathbf{v}_G = \begin{bmatrix} 0.2878 & 0.766 & 0.5748 \\ -0.343 & 0.6428 & -0.685 \\ -0.8942 & 0 & 0.4477 \end{bmatrix} \begin{bmatrix} -2.847 \text{ km/s} \\ 9.145 \text{ km/s} \\ 0 \end{bmatrix}$$

$$\mathbf{v}_G = [6.186 \text{ km/s} \quad 6.855 \text{ km/s} \quad 2.546 \text{ km/s}]^T$$

#### Example

For a given Earth orbit, the elements are:  $h=70,000~\mathrm{km^2/s}$ , e=0.74,  $i=63.4^\circ$ ,  $\Omega=40^\circ$ ,  $\omega=270^\circ$  and  $\theta=30^\circ$ . Find the

state vectors ( $\mathbf{r}_G$  and  $\mathbf{v}_G$ ) in the ECI frame.

What does this orbit look like?

r = 7492 km $r_{\bigoplus} = 6371 \text{ km}$ 

Altitude: 1121 km

#### Molniya Orbit

[HOMA, Online Space Orbit Simulator, <a href="http://en.homasim.com/orbitsimulation.php">http://en.homasim.com/orbitsimulation.php</a>, 2020]



