

**Supersonic Flow  
Over a  
Diamond Shape Airfoil**

1/**INVISCID** run:  $\alpha = 0$  and  $\alpha = 3$

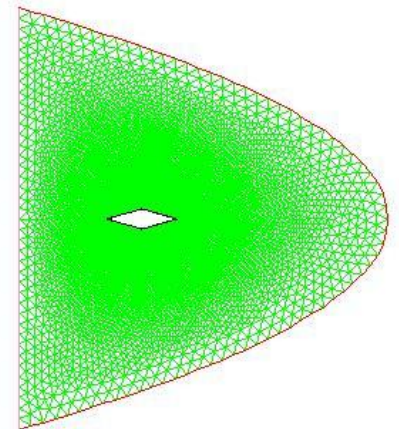
$\left\{ \begin{array}{l} \text{-Mach} = 1.3 \\ \text{-Mach} = 2 \rightarrow \text{compare solutions with oblique-shock theory} \end{array} \right.$

2/**VISCOUS** run

-Grid sensitivity study

-Comparison turbulence models: Spalart-Allmaras/k- $\epsilon$  model

3/Comparison **VISCOUS/INVISCID**



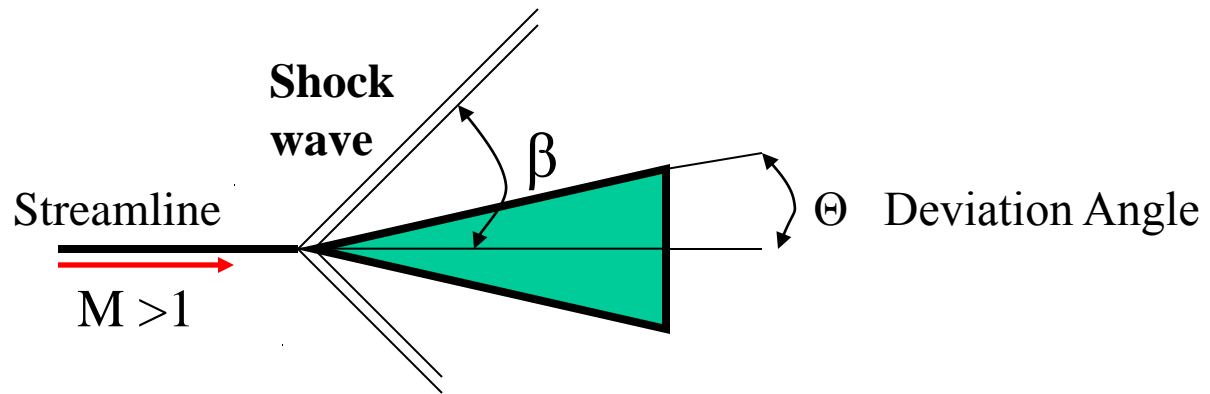
# INVISCID RUN

## Oblique Shock Theory

For any mach number there is a maximum angle of deflection  $\theta$ .

In our case  $\theta = 16^\circ \implies \text{Mach} < 1.65$  Detached Shock (**M = 1.3**)

Mach  $> 1.65$  Attached shock (**M = 2**)



### Shock angle and flow conditions behind the shock

**M1 = 2 and  $\theta = 16^\circ$**

$\beta = 47^\circ$  weak shock solution

$\beta = 79^\circ$  strong shock solution

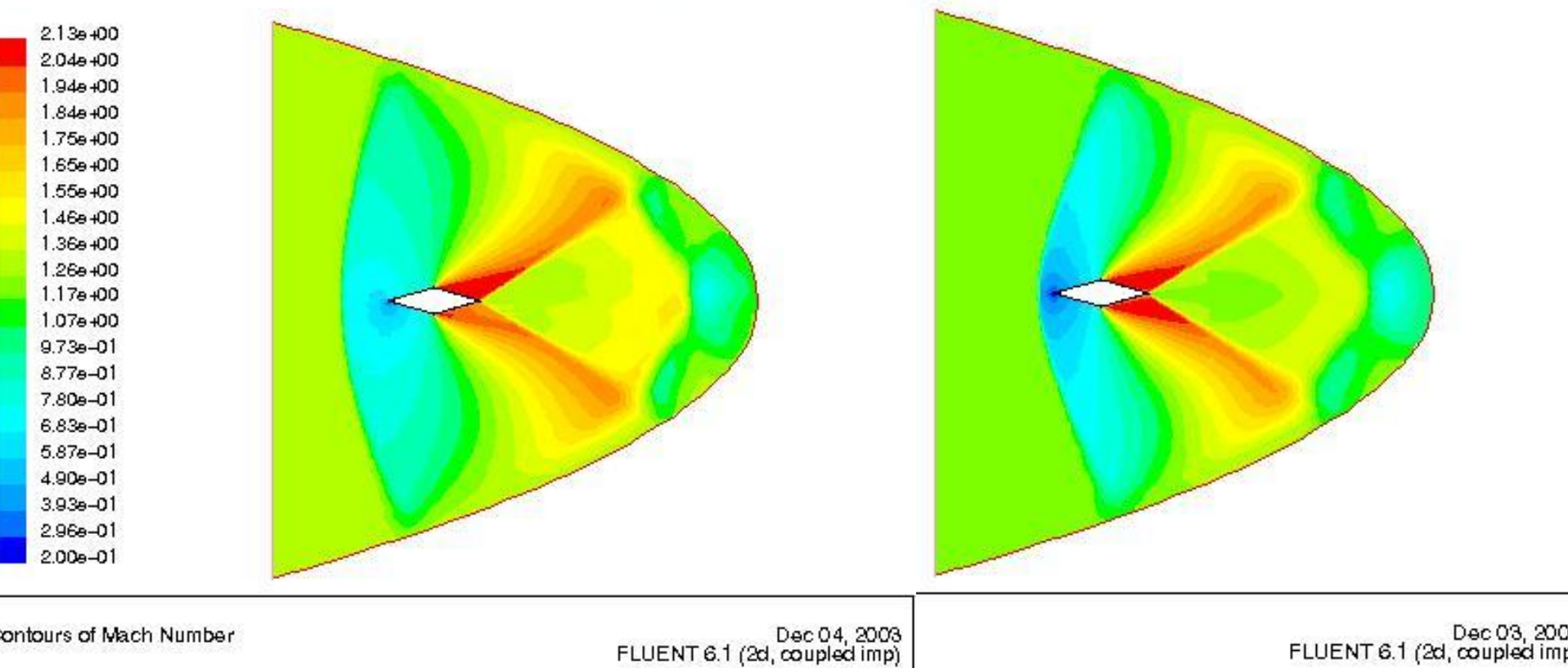
Normal mach :  $M_{n1} = M_1 \sin \beta$       **$M_{n1} = 1.46$**

From  $M_{n1}$  we get  $P_2/P_1$ ,  $T_2/T_1$ ,  $M_{n2}$  from the shock tables:

**$P_2 = 60320 \text{ Pa}$**

**$T_2 = 288.77 \text{ K}$**

**$M_2 = 1.39$**

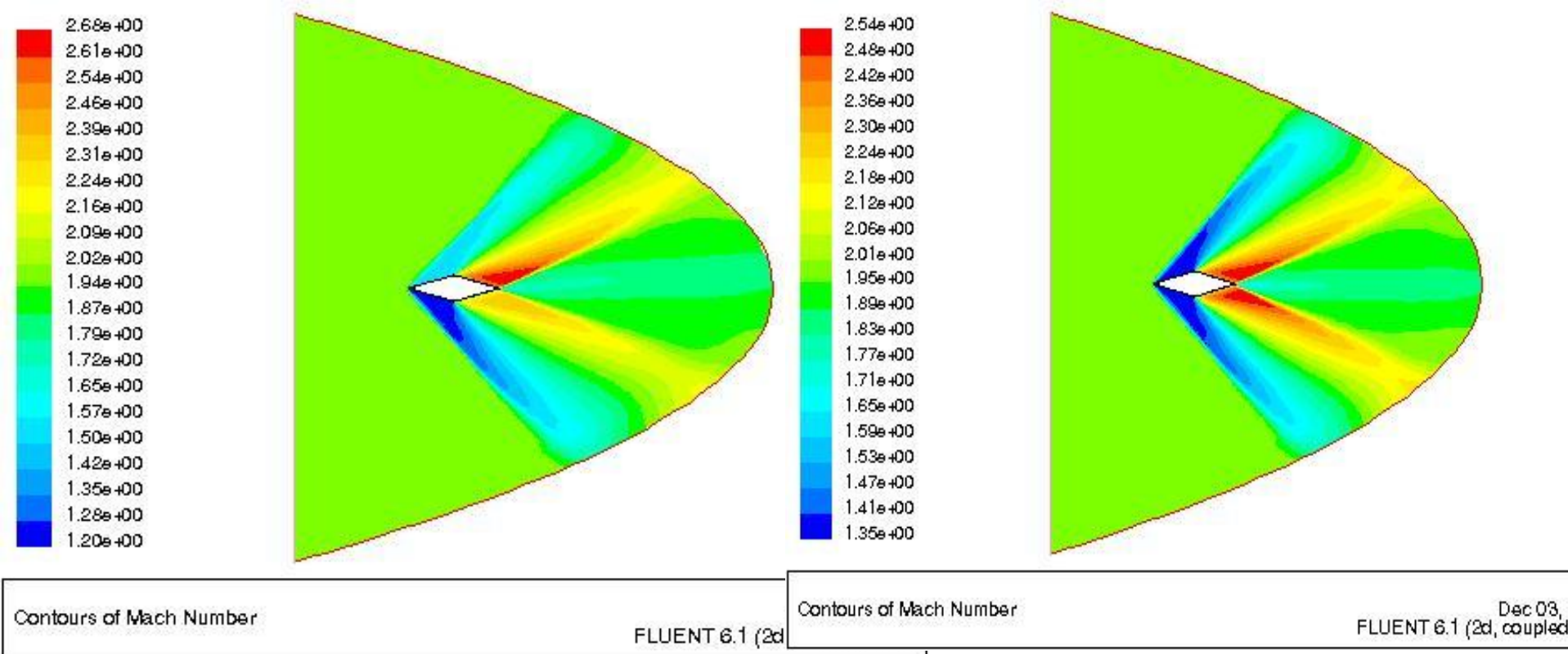


INVISCID **alpha=3**  
2<sup>nd</sup> order upwind

INVISCID **alpha=0**  
2<sup>nd</sup> order upwind

Detached shock **M=1.3**

**MACH NUMBER DISPLAY**



INVISCID **alpha=3**  
2<sup>nd</sup> order upwind

INVISCID **alpha=0**  
2<sup>nd</sup> order upwind

Attached shock **M=2**

**MACH NUMBER DISPLAY**

**ALPHA = 0°**

**Pressure contours**

**expansion fan : 39 °**

**M2=1.39**

**P2=60320 Pa**

**$\beta = 47^\circ$**

**T2=288 K**

**M3=2.55**

**P3=10246 Pa**

**T3=174 K**

**$\Theta = 32^\circ$**

**$\Theta = 16^\circ$**

**M1=2**

**P1=26000 Pa**

**T1 = 223K**

6.05e+04  
5.79e+04  
5.54e+04  
5.29e+04  
5.03e+04  
4.78e+04  
4.53e+04  
4.27e+04  
4.02e+04  
3.77e+04  
3.51e+04  
3.26e+04  
3.01e+04  
2.75e+04  
2.50e+04  
2.25e+04  
1.99e+04  
1.74e+04  
1.49e+04  
1.23e+04  
9.79e+03



**ALPHA = 3°**

**Pressure contours**

$\beta = 43^\circ$

**expansion fan : 36 °**

**M2=1.514**

**P2=51766 Pa**

**T2=274 K**

$\theta = 13^\circ$

$\theta = 32^\circ$

**M3=2.75**

**P3=7718 Pa**

**T3 = 159K**

$\theta = 19^\circ$

$\theta = 32^\circ$

**M3=2.450**

**P3=11935 Pa**

**T3 = 183K**

**M2=1.28**

**P2=69498 Pa**

**T2=303K**

$\beta = 51^\circ$

**M1=2**

**P1=26000 Pa**

**T1 = 223K**

**expansion fan : 59 °**

7.02e+04  
6.71e+04  
6.40e+04  
6.09e+04  
5.78e+04  
5.47e+04  
5.16e+04  
4.84e+04  
4.53e+04  
4.22e+04  
3.91e+04  
3.60e+04  
3.29e+04  
2.98e+04  
2.67e+04  
2.36e+04  
2.05e+04  
1.73e+04  
1.42e+04  
1.11e+04  
8.01e+03

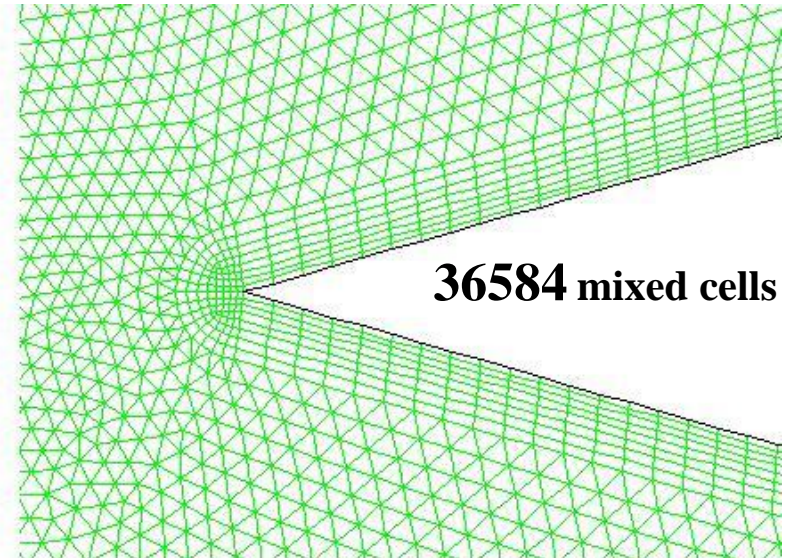
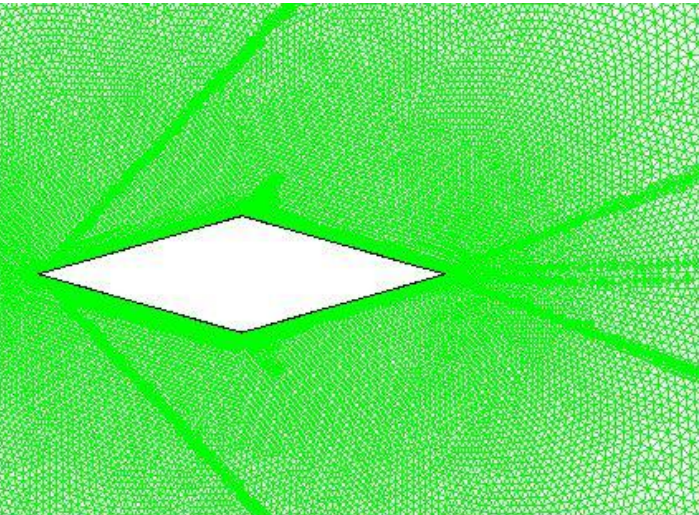
# VISCOUS RUN

## GRID SENSITIVITY STUDY

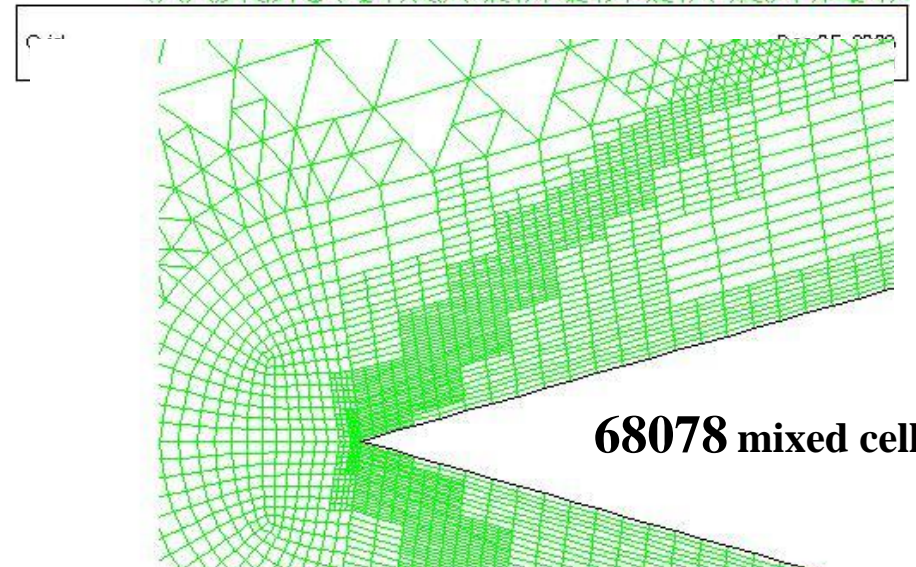
Original Grid: **27402** triangular cells

Final refined grid : **68078** mixed cells

- Pressure gradient adaptation
- Boundary Layer adaptation



**36584** mixed cells

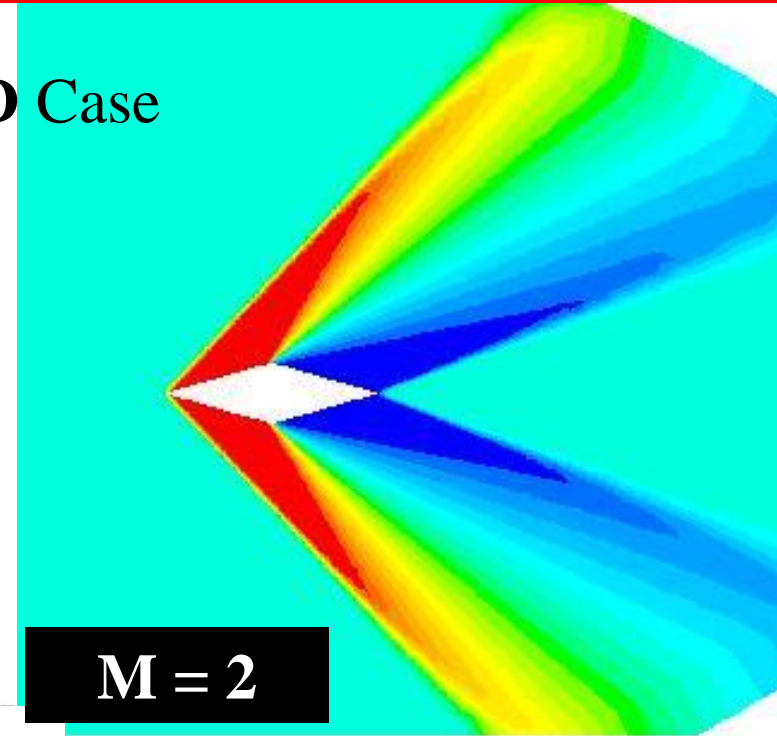
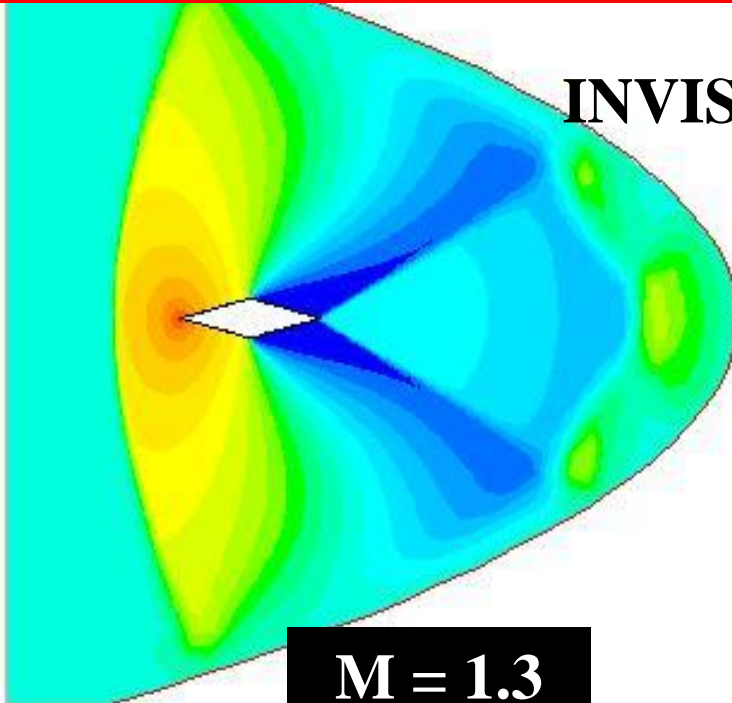


**68078** mixed cells



# INVISCID / VISCOUS

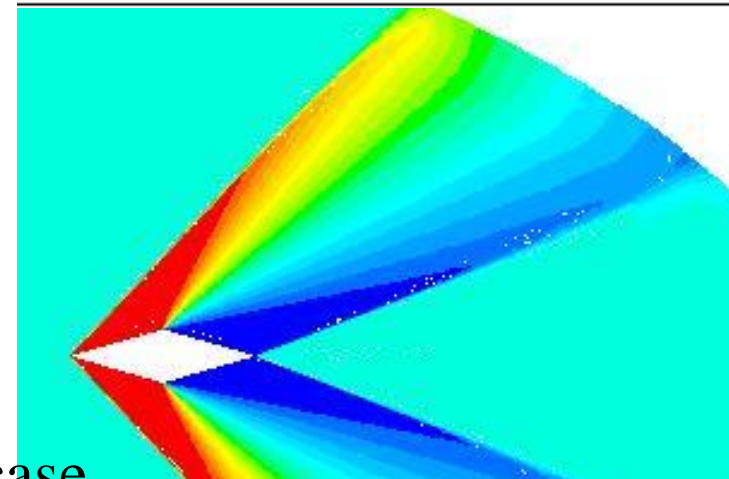
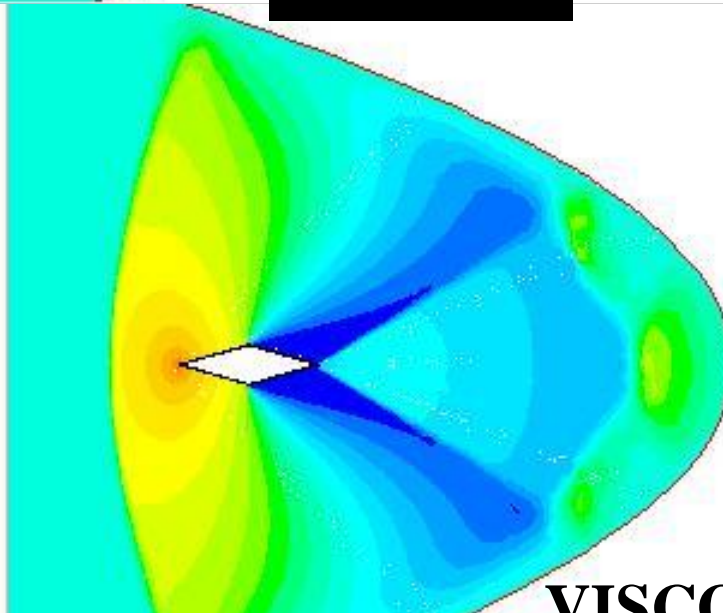
6.18e+04  
5.91e+04  
5.63e+04  
5.36e+04  
5.09e+04  
4.82e+04  
4.54e+04  
4.27e+04  
4.00e+04  
3.72e+04  
3.45e+04  
3.18e+04  
2.90e+04  
2.63e+04  
2.36e+04  
2.09e+04  
1.81e+04  
1.54e+04  
1.27e+04  
9.94e+03  
7.21e+03



ure (pascal)

FLUENT 6.1 (2d

6.56e+04  
6.27e+04  
5.98e+04  
5.68e+04  
5.39e+04  
5.10e+04  
4.81e+04  
4.51e+04  
4.22e+04  
3.93e+04  
3.63e+04  
3.34e+04  
3.05e+04  
2.76e+04  
2.46e+04  
2.17e+04  
1.88e+04  
1.58e+04



VISCOUS case