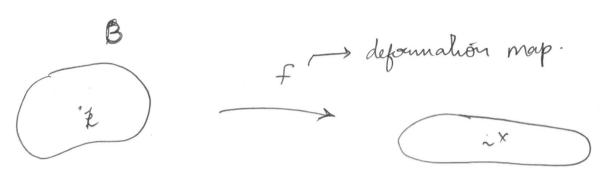
## Infinitesimal strain

Recall the different deformation and strain tensous me discussed so far:



$$F_{iJ}(p) = \frac{\partial f_i}{\partial p_J} = \nabla f$$
 deformation gradient

$$C(p) := F^T F(p)$$
 C-G deformation tensons
$$B(p) := F F^T(p)$$

$$E(f) := \frac{C(p)-I}{(C(p)-I)/2} - Lagrangian Arain tenson.$$

Introduce a new field called the displacement tield  $u: B \to V$  defined as

which describes the displacement of particle p from reference to current/deformed configuration.

$$F_{iJ}(t) := \frac{\partial f_i}{\partial p_J}(t)$$

$$= \frac{\partial}{\partial p_J}(u_i(t) + p_i)$$

$$= S_{iJ} + \frac{\partial u_i}{\partial p_J}(t)$$

$$\iff \boxed{F(p) = I + Vu(p)}$$

Displacement gradient.

Whiting the Lagrangian strain in terms of the displacement gradient, we have

$$2E(\beta) = FF - I$$

$$= (I + Vu) (I + VuT) - I$$

$$= I + VuT + Vu + VuVuT - I$$

$$= VuT + Vu + VuVuT - I$$

If the derivatives  $\frac{\partial u_i}{\partial x_j}$  are small, then the Lagrangian strain can be approximated by

Notation: We are breaking our notational convention here as & is a greek letter and it is being used to describe From O, we have

$$E = \underset{\approx}{\varepsilon} + \underbrace{\nabla u \nabla u^{\mathsf{T}}}_{\mathsf{Z}} - (2)$$

Note: E in linear in the gradients of y, i.e. if we have two displacement maps y, and V2 then for  $u = y_1 + y_2$ , the consumponding  $\xi$  is given E = VU+ PUT

$$= \underbrace{\xi_i}_{\approx} + \underbrace{\xi_i}_{\approx} \quad \text{where} \quad \underbrace{\xi_i}_{\approx} = \underbrace{\frac{\sqrt{u_i}}{\sqrt{u_i}}}_{\approx} + \underbrace{\frac{\sqrt{u_i}}{\sqrt{u_i}}}_{\approx}$$

Caution: Approximating E by & is reasonable only

under 'small' displacement gradients. In fiture lectives, we will discuss the uses of infinitesimal strain. For now, we note that if Dui are not small, then E can sometimes be imphysical.

Example t: Consider a rigid deformation map f(p) = Qp,  $Q \in Orthot$ .

Calculate the coversponding Lagrangian and infitesimal strains.

Since F(p) = Q, it follows that  $E(p) = \frac{FF-I}{2} = Q$ . On the other hand,

 $\underset{\approx}{\mathcal{E}}(p) = \underline{\nabla u + \nabla u^7}$ 

 $= \frac{Q + Q^{T}}{2} - I \qquad \left( \begin{array}{ccc} u = Q + Q - 1 \\ \hline vu = Q - I \end{array} \right)$ 

For the purpose, of discussion let's assume be basis to be oriented such that Q is a clockwise rotation of angle O about the z-axis =>

$$\hat{Q} = \begin{bmatrix}
\cos \theta & \sin \theta & 0 \\
-\sin \theta & \cos \theta & 0 \\
0 & 0 & 1
\end{bmatrix}$$

Therefore
$$\frac{\varepsilon}{z} = \begin{bmatrix}
\cos\theta - 1 & 0 & 0 \\
0 & \cos\theta - 1 & 0
\end{bmatrix}$$

For |Small 0|, |Small 0|, |Small 0|, |Small 0|, |Small 0|.

Fou large rotations, infinitesimal strain can be quite large!

Example 2: In this example, we ask ourselves are there any displacement / deformation maps for which E = 0 while  $E \neq 0$ .

For a given  $W \in Skw$ , consider a displacement map U(p) = Wp = Wp + p

The deformation gradient F(p) = W + I, and  $\nabla u = W + I$ 

 $\Rightarrow \frac{\varepsilon}{z} = \frac{W + W^{T}}{2} = 0$ 

On the other hand

$$E(p) = \frac{(W+I)^{T}(W+I) - I}{2}$$

$$= \frac{WW + W^{T} + W}{2}$$

$$= \frac{W^{T}W}{2}$$

$$= \frac{1}{2} \begin{bmatrix} \beta + \gamma^2 - \alpha \beta & -\alpha \gamma \\ -\alpha \beta & \gamma^2 + \alpha^2 - \beta \gamma \\ -\alpha \gamma & -\beta \gamma & \alpha^2 + \beta^2 \end{bmatrix}, \text{ where } W = \begin{bmatrix} 0 & -\gamma \beta \\ \gamma & 0 & -\alpha \\ -\beta & \alpha & 0 \end{bmatrix}$$

If  $\alpha=\beta=0$ , then

$$E(p) = \frac{1}{2} \begin{bmatrix} r^2 & 0 & 0 \\ 0 & r^2 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

The map  $u(p) \neq Wp$  is called infinitesimal rigid displacement.