

DELFT UNIVERSITY OF TECHNOLOGY

SYSTEMS AND CONTROL
SC42075

Modeling and Control of Hybrid Systems Assignment

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Introduction

This report contains the results and findings of the assignment that is part of the course SC42075 Modelling and Control of Hybrid Systems at Delft University of Technology. The goal of this assignment is twofold.

In the first part of the assignment, a self-chosen real-life system that can be considered as a hybrid system was described and represented as a hybrid automaton. The chosen system is a roller coaster in a theme park.

In the second part of the assignment, the energy management of microgrids is considered. The microgrid is connected to the main powergrid. The microgrid consists of several subsystems, being the diesel generator and its fuel tanks, two batteries and an energy management system. It is assumed that the energy management system has an accurate prediction of the load in the microgrid and that it is able to communicate without delay with the diesel generator and the two batteries. Furthermore, it is assumed that the electrical connection between the main power grid and the microgrid is not physically limited, meaning that the power balance can always be maintained. The power balance describes that the amount of power used by the two charging batteries and the load is equal to the power provided by the discharging batteries, the power grid and the diesel generator. The microgrid is represented in figure 3 below.

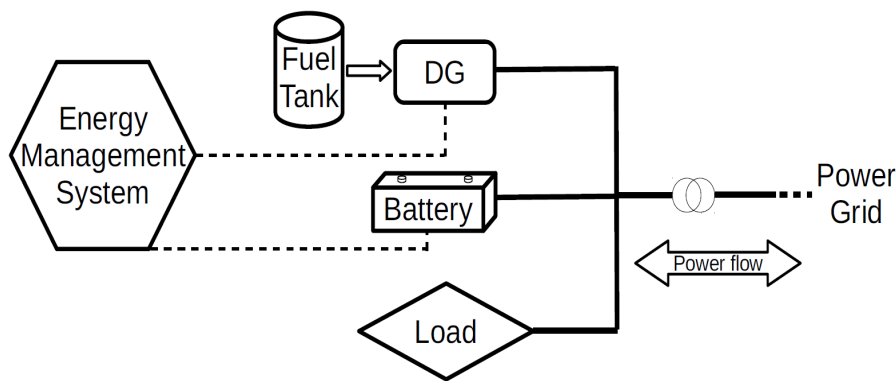


Figure 1: Schematic representation of the considered microgrid

The aim of this assignment is to minimize the operational cost of the microgrid, by designing a hybrid model predictive controller for the energy management system. A price is defined for the exchanged energy per kWh between the microgrid and the power grid. Hence, whenever electrical power is imported from the main power grid, additional operational costs arise because of the price of importing energy. On the other hand, revenue is made whenever energy is exported to the power grid. The energy management system is able to control the operation of the diesel generators and batteries and can in this way influence the costs that are made by the microgrid.

Part 1: Hybrid System Example

Step 1.1

A hybrid system that can be described by an automaton is the waiting line for the *Python*, a roller coaster located in the Dutch theme park *Efteling*.



Figure 2: The Python roller coaster

Variables

The dynamics of the system are defined by two variables $x(t)$ and $y(t)$. Here, $x(t)$ equals time [min] elapsed since a train has been placed or removed on the track, or since the initial condition. $y(t)$ represents the length of the waiting line [m]. Both variables are continuous. There is also one discrete variable, denoted by $P(t)$, which is the status of the Python. When $P(t) = on$, the Python is operational, meaning that visitors can ride the rollercoaster. When $P(t) = off$, the Python is non-operational, meaning that visitors cannot ride the rollercoaster. The second continuous variable, $y(t)$, is described by discontinuous dynamics which can be seen in the automaton in section 1.2.

Dynamics of the system

The initial state is $x(t) = 0$, $y(t) = 0$ and when there is one train on the roller coaster. The initial state is in the first node. The waiting line length grows at the rate of $\dot{y} = a - b_1$ per second. This means the waiting line grows larger by constant a per time, because of people joining the waiting line to get on the roller coaster. The length of the line also decreases by constant b_1 per time, because people get on the train. In reality, the decrease of the waiting line is not continuous over time, because the waiting line only decreases when a train has finished the track of the roller coaster. However, for simplicity, the time average is taken as a continuous decrease.

When the waiting line reaches a length of 20m, a second train should be placed such that the waiting line will decrease faster over time when the two trains are operational. Hence, the guard to node 2 will become active and the system will be described by the dynamics of node 2. The time is then reset and a train is placed, which takes 10 minutes. In those 10 minutes, $\dot{y} = a$ and thus the waiting line length only increases. This is because the Python is non-operational whenever a train is placed/removed and hence no visitors can ride the roller coaster.

When $x(t) \geq 10$, the guard to node 3 becomes active, meaning that the placement/removal of the train is finished. When the Python is operational with two trains, the waiting line length decreases faster than in node 1 because more people get on the roller coaster on average: $\dot{y}(t) = a - b_2$, for $b_2 > b_1$. Finally, when the length of the line gets beneath the 20m again, the process is reversed: a train is removed, which again takes 10 minutes, and the system is described by the dynamics of node 1 again.

Step 1.2

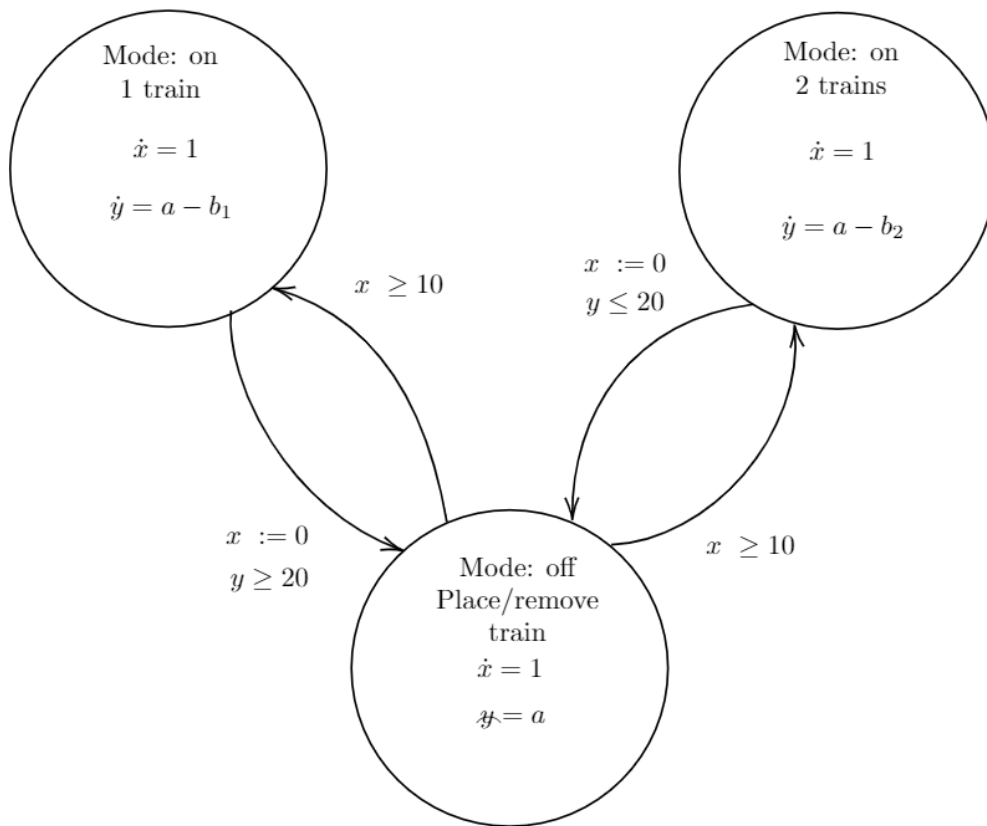


Figure 3: Hybrid automaton for the waiting line for the Python in the Efteling

Part 2: Energy Management of Microgrids

Step 2.1

The discrete-time piecewise affine (PWA) model of the battery is:

$$x_b(k+1) = \begin{cases} x_b(k) - \eta_d T_s u_b(k) & \text{if } s_b = 0 \text{ (discharged)} \\ x_b(k) - \eta_c T_s u_b(k) & \text{if } s_b = 1 \text{ (charged)} \end{cases}$$

$$y_b(k) = u_b(k)$$

Here, x_b is the stored energy in the battery [kWh], u_b the exchanged power [kW], s_b [-] the operational mode (charge / discharge) and η_c, η_d [-] the charging and discharging efficiency respectively. The sampling time of the system is $T_s = 0.20$ [h]. Because the behaviour of the model is described in discrete time (at a certain time instant k), the sampling time is incorporated in the difference equation. In this way, also the units of the equation are correctly used.

The charging/discharging is considered from the grid side. This means that when the battery is charged (discharged), $s_b(k) = 1$ and $u_b(k) \leq 0$ ($s_b(k) = 0$ and $u_b(k) > 0$).

Step 2.2

Looking at the given constraints, and making use of binary variable $s_b(k)$, the following two formulations are constructed:

$$\begin{aligned} [s_b(k) = 1] &\iff [u_b(k) \leq 0] \\ [s_b(k) = 0] &\iff [u_b(k) > 0] \end{aligned}$$

These can be summarized as follows, for ϵ a small tolerance, typically the machine precision:

$$[s_b(k) = 1] \iff [u_b(k) \leq 0] \quad \text{true if and only if:} \quad \begin{cases} u_b(k) \leq \overline{u}_b(1 - s_b(k)) \\ u_b(k) \geq \epsilon + (\underline{u}_b - \epsilon)s_b(k) \end{cases} \quad (1)$$

Then, introducing $z_b(k) = s_b(k)u_b(k)$, the following linear constraints are obtained:

$$z_b(k) \leq \overline{u}_b s_b(k) \quad (2)$$

$$z_b(k) \geq \underline{u}_b s_b(k) \quad (3)$$

$$z_b(k) \leq u_b(k) - \underline{u}_b(1 - s_b(k)) \quad (4)$$

$$z_b(k) \geq u_b(k) - \overline{u}_b(1 - s_b(k)) \quad (5)$$

Looking at the minimum and maximum given in the assignment, another two constraints can be set up:

$$0 \leq x_b(k) \quad (6)$$

$$x_b(k) \leq \overline{x}_b \quad (7)$$

For $u_b(k)$, a maximum and minimum $\overline{u}_b, \underline{u}_b$ is defined as well. However, these constraints are not taken into account in the same way that the maximum and minimum for $x_b(k)$ is defined in constraints 6, 7, because the constraints for $u_b(k)$ are indirectly already given in the linear constraints 2 to 5.

Rewriting the PWA from step 2.1 to get one equation:

$$x_b(k+1) = -s_b(k)\eta_c T_s u_b(k) + \eta_d T_s u_b(k)(s_b(k) - 1) + x_b(k)$$

The battery can be written as a MLD system given by:

$$x_b(k+1) = A^b x_b(k) + B_1^b u_b(k) + B_2^b \delta_b(k) + B_3^b z_b(k) + B_4^b \quad (8)$$

$$x_b(k+1) = \underbrace{1}_{A^b} x_b(k) + \underbrace{-T_s \eta_d}_{B_1^b} u_b(k) + \underbrace{T_s(\eta_d - \eta_c)}_{B_3^b} z_b(k) \quad (9)$$

Where $A^b = 1, B_1^b = -T_s\eta_d, B_2^b = 0, B_3^b = T_s(\eta_d - \eta_c), B_4^b = 0$.

This equation 9 is subjected to the constraints 2 to 5, which together with constraints 1, constraint 6 and constraint 7 form all the constraints to the MLD problem. Firstly, these constraints are rewritten to equations in the right form. Secondly, the constraints are rewritten to matrix representation for the MLD formulation. The following constraints in correct form are obtained:

- (1) $u_b(k) + \overline{u_b}s_b(k) \leq \overline{u_b}$
- (2) $(\underline{u_b} - \epsilon)s_b(k) - u_b(k) \leq -\epsilon$
- (3) $-x_b(k) \leq 0$
- (4) $x_b(k) \leq \overline{x_b}$
- (5) $z_b(k) - \overline{u_b}s_b(k) \leq 0$
- (6) $\underline{u_b}s_b(k) - z_b(k) \leq 0$
- (7) $z_b(k) - u_b(k) - \underline{u_b}s_b(k) \leq -\underline{u_b}$
- (8) $u_b(k) - z_b(k) + \overline{u_b}s_b(k) \leq \overline{u_b}$

The following constraint equation and constraint matrices for the battery are obtained:

$$E_1^b x_b(k) + E_2^b u_b(k) + E_3^b s_b(k) + E_4^b z_b(k) \leq g_5^b \quad (10)$$

$$\underbrace{\begin{bmatrix} 0 \\ 0 \\ -1 \\ 1 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}}_{E_1^b} x_b(k) + \underbrace{\begin{bmatrix} 1 \\ -1 \\ 0 \\ 0 \\ 0 \\ 0 \\ -1 \\ 1 \end{bmatrix}}_{E_2^b} u_b(k) + \underbrace{\begin{bmatrix} \overline{u_b} \\ \underline{u_b} - \epsilon \\ 0 \\ 0 \\ -\underline{u_b} \\ \underline{u_b} \\ -\underline{u_b} \\ \overline{u_b} \end{bmatrix}}_{E_3^b} s_b(k) + \underbrace{\begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 1 \\ -1 \\ 1 \\ -1 \end{bmatrix}}_{E_4^b} z_b(k) \leq \underbrace{\begin{bmatrix} \overline{u_b} \\ -\epsilon \\ 0 \\ \overline{x_b} \\ 0 \\ 0 \\ -\underline{u_b} \\ \underline{u_b} \end{bmatrix}}_{g_5^b} \quad (11)$$

For $E_1^b, E_2^b, E_3^b, E_4^b, g_5^b \in \mathbb{R}^{8 \times 1}$.

Step 2.3

The fuel consumption of the diesel generator is given by the following function:

$$f(u_d(k)) = \begin{cases} u_d^2(k) + 4 \\ 4u_d(k) \\ -9.44u_d^3(k) + 166.06u_d^2(k) - 948.22u_d(k) + 1790.28 \\ -11.78u_d(k) + 132.44 \\ 4.01(u_d(k) - 10.47)^2 + 17.79 \end{cases}$$

With $f(u_d(k))$ the consumed fuel of the diesel generator at time step k in [kg/h] and $u_d(k)$ the output power of the diesel generator at time step k in [kW].

This nonlinear function will be approximated with the PWA function $\hat{f} : [0, \overline{u_d}] \rightarrow \mathbb{R}$, which is divided in the following four regions:

$$\hat{f}(u_d(k)) = \begin{cases} a_1 + b_1 u_d(k) & \text{if } 0 \leq u_d(k) < u_1 \\ a_2 + b_2 u_d(k) & \text{if } u_1 \leq u_d(k) < u_2 \\ a_3 + b_3 u_d(k) & \text{if } u_2 \leq u_d(k) < u_3 \\ a_4 + b_4 u_d(k) & \text{if } u_3 \leq u_d(k) \leq 15 \end{cases}$$

The parameters a_i and b_i for $i \in 1, 2, 3, 4$ in the PWA approximation \hat{f} are determined by minimizing the squared area between f and \hat{f} , or equivalently:

$$\int_0^{\bar{u}_d} (f(u_d) - \hat{f}(u_d))^2 du_d$$

To minimize, this integral is divided into the four PWA approximation regions: 0 to $u_1 = 5$, u_1 to $u_2 = 6.5$, u_2 to $u_3 = 11$ and u_3 to 15:

$$\begin{aligned} (1) & \int_0^2 (u_d^2(k) + 4 - a_1 - b_1 u_d(k))^2 du_d + \int_2^5 (4u_d(k) - a_1 - b_1 u_d(k))^2 du_d \\ (2) & + \int_5^{6.5} (-9.44u_d^3(k) + 166.06u_d^2(k) - 948.22u_d(k) + 1790.28 - a_2 - b_2 u_d(k))^2 du_d \\ (3) & + \int_{6.5}^7 (-9.44u_d^3(k) + 166.06u_d^2(k) - 948.22u_d(k) + 1790.28 - a_3 - b_3 u_d(k))^2 du_d \\ & + \int_7^9 (-11.78u_d(k) + 132.44 - a_3 - b_3 u_d(k))^2 du_d + \int_9^{11} (4.01(u_d(k) - 10.47)^2 + 17.79 - a_3 - b_3 u_d(k))^2 du_d \\ (4) & + \int_{11}^{15} (4.01(u_d(k) - 10.47)^2 + 17.79 - a_4 - b_4 u_d(k))^2 du_d \end{aligned}$$

To minimize this squared area, the integrals are solved analytically. The four regions are minimized separately by first calculating the partial derivatives to a_i and b_i . Secondly, these partial derivatives are set equal to 0 and solved. For example, defining the two integrals in region 1 as a function f_1 , $\nabla f_1(a_1, b_1) = 0$ is computed and the minimized values for a_1 and b_1 are obtained. Following this procedure, this results in the following values for a_i, b_i :

	Precise value	Approximate value		Precise value	Approximate value
a_1	$\frac{136}{75}$	1.813	b_1	$\frac{436}{125}$	3.488
a_2	$\frac{-22732801477233947}{247390116249600}$	-91.891	b_2	$\frac{1357800653035933}{61847529062400}$	21.954
a_3	$\frac{3591809146630509439}{32061759065948160}$	112.028	b_3	$\frac{-1472321153042095969}{160308795329740800}$	-9.184
a_4	$\frac{-121019335510265749}{562949953421312}$	-21.4974	b_4	$\frac{11422592324890509}{562949953421312}$	20.291

To compare the approximated function with the real function for the fuel consumption, the PWA approximation with values found for a_i, b_i is plotted against the real function, see figure 4.

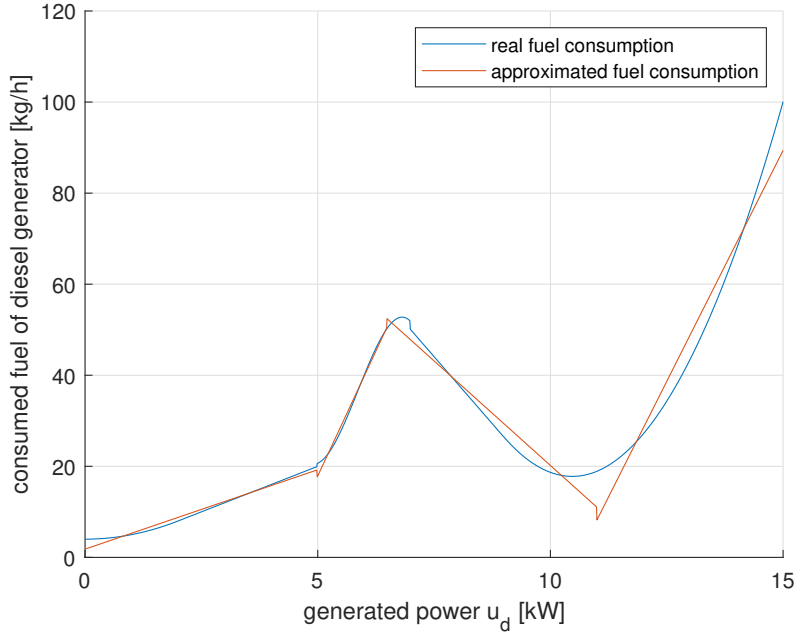


Figure 4: Comparison of real with approximated fuel consumption [kg/h], for optimal values of a_i, b_i for $i = 1, 2, 3, 4$

Step 2.4

The PWA approximation derived in step 2.3 is now recalculated, only now with the bounds u_i of the four PWA approximation regions not fixed but variable. Now, the objective is to minimize:

$$\int_0^{\bar{u}_d} \left(f(u_d) - \hat{f}(u_d) \right)^2 du_d$$

The function should be minimized over 11 variables: a_i, b_i, u_1, u_2, u_3 for $i = 1, 2, 3, 4$. Both functions, $f(u_d(k))$ and $\hat{f}(u_d(k))$, are first discretized on the interval $u_d(k) \in [0 \ 15]$ with step size 0.001. The values that should be estimated are stored in vector x and the objective function to minimize is created. The integral from the objective is calculated using trapezoidal numerical integration. Using the algorithm `fmincon` in MATLAB, the optimal vector x is found. The algorithm finds the minimum of a constrained nonlinear multivariable function, where the constraints are given by:

- (1) $u_3 \leq \bar{u}_d$
- (2) $u_1 - u_2 \leq 0$
- (3) $u_2 - u_3 \leq 0$
- (4) $-u_1 \leq 0$

These can be summarized as $Ax \leq b$, where the matrices and vector are defined as:

$$x = \begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \\ b_1 \\ b_2 \\ b_3 \\ b_4 \\ u_1 \\ u_2 \\ u_3 \end{bmatrix} \quad A = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & -1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & -1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -1 & 0 & 0 \end{bmatrix} \quad b = \begin{bmatrix} \bar{u}_d \\ 0 \\ 0 \\ 0 \end{bmatrix} \quad (12)$$

To make sure the algorithm does not get stuck in a local minimum, 21 different initial vectors x_0 are defined as a starting point, with values close to the estimated values from step 2.3. The minimum value found for the objective function is 118.5073 [kg/h], for the following values for the variables:

	Approximate value
a_1	1.8108
a_2	-86.7707
a_3	102.9772
a_4	-229.6789

	Approximate value
b_1	3.4880
b_2	20.9957
b_3	-8.1265
b_4	21.3577

	Approximate value
u_1	4.9860
u_2	6.8700
u_3	11.3019

To compare the approximated function with the real function for the fuel consumption, the PWA approximation with values found for a_i, b_i, u_1, u_2, u_3 is plotted against the real function, see figure 5.

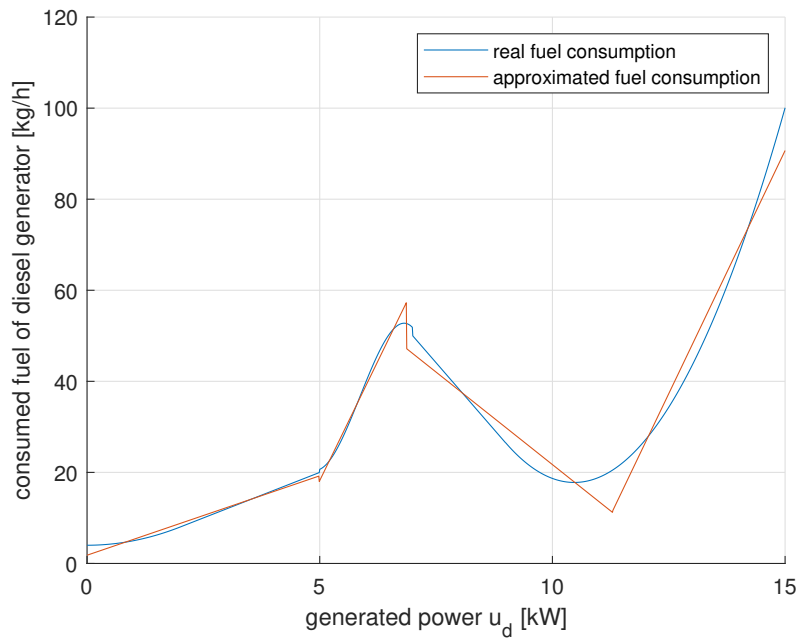


Figure 5: Comparison of real with approximated fuel consumption [kg/h], for optimal values of a_i, b_i, u_1, u_2, u_3 for $i = 1, 2, 3, 4$

Finally, the Root Mean Square Error (RMSE) between the real and approximated fuel consumption function is computed, which equals 2.8145 [kg/h]. The RMSE is calculated as well for step 2.3, where the approximation was done without optimizing u_1, u_2, u_3 . The RMSE for step 2.3 equals 2.9046 kg/h. Thus, in step 2.4, a 3.10% lower error than in step 2.3 is obtained. Therefore, it can be concluded that the values obtained in this step are more optimal.

Step 2.5

The PWA model for the diesel generator is given below, with $\hat{f}(u_d(k))$ the PWA approximation of the consumed fuel of the diesel generator as calculated in step 2.3:

$$x_d(k+1) = \begin{cases} x_d(k) + R_f T_s - \hat{f}(u_d(k)) T_s & \text{if } s_d(k) = 1 \\ x_d(k) + R_f T_s & \text{if } s_d(k) = 0 \end{cases}$$

Filling in $\hat{f}(u_d(k))$, the PWA model for the diesel generator becomes:

$$x_d(k+1) = \begin{cases} x_d(k) + R_f T_s - a_1 T_s - b_1 T_s u_d(k) & \text{if } s_d(k) = 1, \quad 0 \leq u_d(k) \leq u_1 \\ x_d(k) + R_f T_s - a_2 T_s - b_2 T_s u_d(k) & \text{if } s_d(k) = 1, \quad u_1 \leq u_d(k) \leq u_2 \\ x_d(k) + R_f T_s - a_3 T_s - b_3 T_s u_d(k) & \text{if } s_d(k) = 1, \quad u_2 \leq u_d(k) \leq u_3 \\ x_d(k) + R_f T_s - a_4 T_s - b_4 T_s u_d(k) & \text{if } s_d(k) = 1, \quad u_3 \leq u_d(k) \leq \bar{u}_d \\ x_d(k) + R_f T_s & \text{if } s_d = 0 \end{cases} \quad (13)$$

Here, $x_d(k)$ is the fuel level in the tank, or the remaining fuel of the generator [kg], $u_d(k)$ the generated power by the generator [kW], $s_d(k)$ [-] the operational mode (on / off) of the generator and R_f [kg/h] the filling rate of the fuel tank. R_f can be considered a constant and the value of $\bar{u}_d = 15$.

Step 2.6

The objective is to construct a MLD model of the diesel generator.

Constraints

First, a binary variable $s_d(k)$ is introduced, which indicates whether the generator is switched on or off:

$$\begin{aligned} [s_d(k) = 1] &\iff [u_d(k) > 0] \\ [s_d(k) = 0] &\iff [u_d(k) = 0] \end{aligned}$$

For the battery, it holds that $s_b(k) = \delta_b(k)$ and $z(k) = s_b(k)u_b(k)$. However, for the diesel generator, four new binary variables are introduced, such that the $\delta_d(k)$ and $z_d(k)$ vectors are defined as follows:

$$\delta_d(k) = \begin{bmatrix} \delta_1(k) \\ \delta_2(k) \\ \delta_3(k) \\ \delta_4(k) \end{bmatrix} \quad z_d(k) = \begin{bmatrix} z_1(k) \\ z_2(k) \\ z_3(k) \\ z_4(k) \end{bmatrix} = \begin{bmatrix} \delta_1(k)u_d(k) \\ \delta_2(k)u_d(k) \\ \delta_3(k)u_d(k) \\ \delta_4(k)u_d(k) \end{bmatrix}$$

For these new binary variables, the following is desired:

$$\begin{aligned} [\delta_1 = 1] &\text{ if } [0 \leq u_d(k) < u_1] \text{ else } [\delta_1 = 0] \\ [\delta_2 = 1] &\text{ if } [u_1 \leq u_d(k) < u_2] \text{ else } [\delta_2 = 0] \\ [\delta_3 = 1] &\text{ if } [u_2 \leq u_d(k) < u_3] \text{ else } [\delta_3 = 0] \\ [\delta_4 = 1] &\text{ if } [u_3 \leq u_d(k) < 15] \text{ else } [\delta_4 = 0] \end{aligned}$$

This gives rise to equality constraint:

$$\delta_1(k) + \delta_2(k) + \delta_3(k) + \delta_4(k) = s_d(k)$$

Which can be rewritten to the first inequality constraint:

$$\delta_1(k) + \delta_2(k) + \delta_3(k) + \delta_4(k) \leq 1 \quad (14)$$

Update equation

With the newly defined vectors $\delta_d(k)$, $z_d(k)$, the PWA from step 2.5, equation 13, should be rewritten to obtain one update equation:

$$\begin{aligned} x_d(k+1) &= x_d(k) + T_s R_f - T_s a_1 \delta_1(k) - T_s a_2 \delta_2(k) - T_s a_3 \delta_3(k) - T_s a_4 \delta_4(k) - T_s b_1 \delta_1(k) u_d(k) - T_s b_2 \delta_2(k) u_d(k) \\ &\quad - T_s b_3 \delta_3(k) u_d(k) - T_s b_4 \delta_4(k) u_d(k) \\ &= x_d(k) + T_s R_f - T_s a_1 \delta_1(k) - T_s a_2 \delta_2(k) - T_s a_3 \delta_3(k) - T_s a_4 \delta_4(k) - T_s b_1 z_1(k) - T_s b_2 z_2(k) \\ &\quad - T_s b_3 z_3(k) - T_s b_4 z_4(k) \end{aligned} \quad (15)$$

This equation can be summarized as follows:

$$x_d(k+1) = A^d x_d(k) + B_1^d u_d(k) + B_2^d \delta_d(k) + B_3^d z_d(k) + B_4^d \quad (16)$$

Here, the matrices are defined as:

$$\begin{aligned} A^d &= 1 & B_1^d &= 0 & B_2^d &= [-T_s a_1 & -T_s a_2 & -T_s a_3 & -T_s a_4] \\ B_3^d &= [-T_s b_1 & -T_s b_2 & -T_s b_3 & -T_s b_4] & B_4^d &= T_s R_f \end{aligned} \quad (17)$$

For the following vectors:

$$\delta_d(k) = \begin{bmatrix} \delta_1(k) \\ \delta_2(k) \\ \delta_3(k) \\ \delta_4(k) \end{bmatrix} \quad z_d(k) = \begin{bmatrix} z_1(k) \\ z_2(k) \\ z_3(k) \\ z_4(k) \end{bmatrix} = \begin{bmatrix} \delta_1(k)u_d(k) \\ \delta_2(k)u_d(k) \\ \delta_3(k)u_d(k) \\ \delta_4(k)u_d(k) \end{bmatrix}$$

Constraints

Looking at the minimum and maximum given in the assignment, another two constraints can be set up:

$$\underline{x}_d \leq x_d(k) \implies -x_d(k) \leq -\underline{x}_d \quad (18)$$

$$x_d(k) \leq \bar{x}_d \quad (19)$$

$$\underline{u}_d \leq u_d(k) \implies -u_d(k) \leq -\underline{u}_d \quad (20)$$

$$u_d(k) \leq \bar{u}_d \quad (21)$$

The linear inequalities that rise from writing the nonlinear system as a linear system are written for each $\delta_i(k), z_i(k)$ separately:

$$z_1(k) \leq u_1 \delta_1(k) \implies -u_1 \delta_1(k) + z_1(k) \leq 0 \quad (22)$$

$$z_1(k) \geq 0 \cdot \delta_1(k) \implies -z_1(k) \leq 0 \quad (23)$$

$$z_1(k) \leq u_d(k) - 0 \cdot (1 - \delta_1(k)) \implies -u_d(k) + z_1(k) \leq 0 \quad (24)$$

$$z_1(k) \geq u_d(k) - u_1(1 - \delta_1(k)) \implies u_d(k) + u_1 \delta_1(k) - z_1(k) \leq u_1 \quad (25)$$

$$z_2(k) \leq u_2 \delta_2(k) \implies -u_2 \delta_2(k) + z_2(k) \leq 0 \quad (26)$$

$$z_2(k) \geq u_1 \delta_2(k) \implies u_1 \delta_2(k) - z_2(k) \leq 0 \quad (27)$$

$$z_2(k) \leq u_d(k) - u_1(1 - \delta_2(k)) \implies -u_d(k) - u_1 \delta_2(k) + z_2(k) \leq 0 \quad (28)$$

$$z_2(k) \geq u_d(k) - u_2(1 - \delta_2(k)) \implies u_d(k) + u_2 \delta_2(k) - z_2(k) \leq u_2 \quad (29)$$

$$z_3(k) \leq u_3 \delta_3(k) \implies -u_3 \delta_3(k) + z_3(k) \leq 0 \quad (30)$$

$$z_3(k) \geq u_2 \delta_3(k) \implies u_2 \delta_3(k) - z_3(k) \leq 0 \quad (31)$$

$$z_3(k) \leq u_d(k) - u_2(1 - \delta_3(k)) \implies -u_d(k) - u_2 \delta_3(k) + z_3(k) \leq -u_2 \quad (32)$$

$$z_3(k) \geq u_d(k) - u_3(1 - \delta_3(k)) \implies u_d(k) + u_3 \delta_3(k) - z_3(k) \leq u_3 \quad (33)$$

$$z_4(k) \leq \bar{u}_d \delta_4(k) \implies -\bar{u}_d \delta_4(k) + z_4(k) \leq 0 \quad (34)$$

$$z_4(k) \geq u_3 \delta_4(k) \implies u_3 \delta_4(k) - z_4(k) \leq 0 \quad (35)$$

$$z_4(k) \leq u_d(k) - u_3(1 - \delta_4(k)) \implies -u_d(k) - u_3 \delta_4(k) + z_4(k) \leq -u_3 \quad (36)$$

$$z_4(k) \geq u_d(k) - \bar{u}_d(1 - \delta_4(k)) \implies u_d(k) + \bar{u}_d \delta_4(k) - z_4(k) \leq \bar{u}_d \quad (37)$$

$$(38)$$

Next, the binary variables are related to the fuel consumption, for ϵ a small tolerance, typically the machine precision. This relation, for the first binary variable only, is as follows:

$$[\delta_1 = 1] \iff [u_d(k) \geq 0]$$

true if and only if

$$u_d(k) \geq \epsilon \delta_1(k) \implies -u_d(k) + \epsilon \delta_1(k) \leq 0 \quad (39)$$

$$u_d(k) - (\bar{u}_d - \underline{u}_d + \epsilon) \delta_1(k) \leq u_1 - \epsilon \implies u_d(k) - (\bar{u}_d - \underline{u}_d + \epsilon) \leq \underline{u}_d - \epsilon \quad (40)$$

$$(41)$$

$$[\delta_2 = 1] \iff [u_d(k) \geq u_1]$$

true if and only if

$$u_d(k) \geq u_1\delta_2(k) \implies -u_d(k) + u_1\delta_2(k) \leq 0 \quad (42)$$

$$-(\bar{u}_d - u_1 + \epsilon)\delta_2(k) \leq -(u_d - u_1) - \epsilon \implies u_d(k) - (\bar{u}_d - u_1 + \epsilon)\delta_2(k) \leq u_1 - \epsilon \quad (43)$$

$$(44)$$

$$[\delta_3 = 1] \iff [u_d(k) \geq u_2]$$

true if and only if

$$u_d(k) \geq u_2\delta_3(k) \implies -u_d(k) + u_2\delta_3(k) \leq 0 \quad (45)$$

$$-(\bar{u}_d - u_2 + \epsilon)\delta_3(k) \leq -(u_d(k) - u_2) - \epsilon \implies u_d(k) - (\bar{u}_d - u_2 + \epsilon)\delta_3(k) \leq u_2 - \epsilon \quad (46)$$

$$(47)$$

$$[\delta_4 = 1] \iff [u_d(k) \geq u_3]$$

true if and only if

$$u_d(k) \geq u_3\delta_4(k) \implies -u_d(k) + u_3\delta_4(k) \leq 0 \quad (48)$$

$$-(\bar{u}_d - u_3 + \epsilon)\delta_4(k) \leq -(u_d(k) - u_3) - \epsilon \implies u_d(k) - (\bar{u}_d - u_3 + \epsilon)\delta_4(k) \leq u_3 - \epsilon \quad (49)$$

$$(50)$$

The final constraints that arise in the MLD model of the diesel generator are given by constraints 14, 18, 21, linear constraints 22 to 37 and binary constraints 39 to 49:

$$(1) \delta_1(k) + \delta_2(k) + \delta_3(k) + \delta_4(k) \leq 1$$

$$(2) -x_d(k) \leq -\underline{x}_d$$

$$(3) x_d(k) \leq \bar{x}_d$$

$$(4) -u_1\delta_1(k) + z_1(k) \leq 0$$

$$(5) -z_1(k) \leq 0$$

$$(6) -u_d(k) + z_1(k) \leq 0$$

$$(7) u_d(k) + u_1\delta_1(k) - z_1(k) \leq u_1$$

$$(8) -u_d(k) + \epsilon\delta_1(k) \leq 0$$

$$(9) u_d(k) - (\bar{u}_d - \underline{u}_d + \epsilon) \leq \underline{u}_d - \epsilon$$

$$(10) -u_2\delta_2(k) + z_2(k) \leq 0$$

$$(11) u_1\delta_2(k) - z_2(k) \leq 0$$

$$(12) -u_d(k) - u_1\delta_2(k) + z_2(k) \leq -u_1$$

$$(13) u_d(k) + u_2\delta_2(k) - z_2(k) \leq u_2$$

$$(14) -u_d(k) + u_1\delta_2(k) \leq 0$$

$$(15) u_d(k) - (\bar{u}_d - u_1 + \epsilon)\delta_2(k) \leq u_1 - \epsilon$$

$$(16) -u_3\delta_3(k) + z_3(k) \leq 0$$

$$(17) u_2\delta_3(k) - z_3(k) \leq 0$$

$$(18) -u_d(k) - u_2\delta_3(k) + z_3(k) \leq -u_2$$

$$(19) u_d(k) + u_3\delta_3(k) - z_3(k) \leq u_3$$

$$(20) \quad -u_d(k) + u_2\delta_3(k) \leq 0$$

$$(21) \quad u_d(k) - (\bar{u}_d - u_2 + \epsilon)\delta_3(k) \leq u_2 - \epsilon$$

$$(22) \quad -\bar{u}_d\delta_4(k) + z_4(k) \leq 0$$

$$(23) \quad u_3\delta_4(k) - z_4(k) \leq 0$$

$$(24) \quad -u_d(k) - u_3\delta_4(k) + z_4(k) \leq -u_3$$

$$(25) \quad u_d(k) + \bar{u}_d\delta_4(k) - z_4(k) \leq \bar{u}_d$$

$$(26) \quad -u_d(k) + u_3\delta_4(k) \leq 0$$

$$(27) \quad u_d(k) - (\bar{u}_d - u_3 + \epsilon)\delta_4(k) \leq u_3 - \epsilon$$

These constraints can be summarized in the following equation:

$$E_1^d x_d(k) + E_2^d u_d(k) + E_3^d \delta_d(k) + E_4^d z_d(k) \leq g_5^d \quad (51)$$

Here, for $E_1^d, E_2^d, g_5^d \in \mathbb{R}^{27 \times 1}$ and $E_3^d, E_4^d \in \mathbb{R}^{27 \times 4}$, the matrices are defined as:

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Step 2.7

See MATLAB file in the Appendix.

Step 2.8

MPC Problem

The goal is to recast the MPC optimization problem as a mixed-integer linear programming (MILP) problem. The MPC problem is given by the following three update and constraint equations.

Update equations

$$x_{b,1}(k+1) = A^{b,1}x_{b,1}(k) + B_1^{b,1}u_{b,1}(k) + B_3^{b,1}z_{b,1}(k) \quad (53)$$

$$x_{b,2}(k+1) = A^{b,2}x_{b,2}(k) + B_1^{b,2}u_{b,2}(k) + B_3^{b,2}z_{b,2}(k) \quad (54)$$

$$x_d(k+1) = A^d x_d(k) + B_1^d u_d(k) + B_2^d \delta_d(k) + B_3^d z_d(k) + B_4^d \quad (55)$$

For:

$$z_{b,1}(k) = s_{b,1}(k)u_{b,1}(k) \quad z_{b,2}(k) = s_{b,2}(k)u_{b,2}(k) \quad \delta_d(k) = \begin{bmatrix} \delta_1(k) \\ \delta_2(k) \\ \delta_3(k) \\ \delta_4(k) \end{bmatrix} \quad z_d(k) = \begin{bmatrix} \delta_1(k)u_d(k) \\ \delta_2(k)u_d(k) \\ \delta_3(k)u_d(k) \\ \delta_4(k)u_d(k) \end{bmatrix} \quad (56)$$

Constraint equations

$$E_1^{b,1}x_{b,1}(k) + E_2^{b,1}u_{b,1}(k) + E_3^{b,1}\delta_{b,1}(k) + E_4^{b,1}z_{b,1}(k) \leq g_5^{b,1} \quad (57)$$

$$E_1^{b,2}x_{b,2}(k) + E_2^{b,2}u_{b,2}(k) + E_3^{b,2}\delta_{b,2}(k) + E_4^{b,2}z_{b,2}(k) \leq g_5^{b,2} \quad (58)$$

$$E_1^d x_d(k) + E_2^d u_d(k) + E_3^d \delta_d(k) + E_4^d z_d(k) \leq g_5^d \quad (59)$$

For:

$$\delta_{b,1}(k) = s_{b,1}(k) \quad \delta_{b,2}(k) = s_{b,2}(k)$$

Writing MPC problem in explicit form

The update and inequality equations should be written in explicit form. This is done for the batteries and diesel generator separately. Afterwards, both the update and inequality equations can be taken together to get two expressions.

Batteries

First, the following vectors are defined, where i denotes either 1 or 2, referring to the first and second battery respectively. Furthermore, N_p denotes the control horizon. All vectors have dimension $\mathbb{R}^{N_p \times 1}$:

$$\begin{aligned} \tilde{\delta}_{b,i}(k) &= \begin{bmatrix} \hat{\delta}_{b,i}(k|k) \\ \vdots \\ \hat{\delta}_{b,i}(k+N_p-1|k) \end{bmatrix} & \tilde{u}_{b,i}(k) &= \begin{bmatrix} u_{b,i}(k) \\ \vdots \\ u_{b,i}(k+N_p-1) \end{bmatrix} & \tilde{z}_{b,i}(k) &= \begin{bmatrix} \hat{z}_{b,i}(k|k) \\ \vdots \\ \hat{z}_{b,i}(k+N_p-1|k) \end{bmatrix} \\ \tilde{x}_{b,i}(k) &= \begin{bmatrix} \hat{x}_{b,i}(k+1|k) \\ \vdots \\ \hat{x}_{b,i}(k+N_p|k) \end{bmatrix} \end{aligned}$$

Second, all components of vector $\tilde{x}_{b,i}(k)$, $\tilde{\delta}_{b,i}(k)$ and $\tilde{z}_{b,i}(k)$ are expressed as a function of $x(k)$ and of all components in vector $u(k)$. To achieve this, the inequality equations 57, 58 are rewritten to determine $\hat{\delta}(k|k)$, $\hat{z}(k|k)$:

$$E_1^{b,1}x_{b,1}(k) + E_2^{b,1}u_{b,1}(k) + E_3^{b,1}\hat{\delta}_{b,1}(k|k) + E_4^{b,1}\hat{z}_{b,1}(k|k) \leq g_5^{b,1} \quad (60)$$

$$E_1^{b,2}x_{b,2}(k) + E_2^{b,2}u_{b,2}(k) + E_3^{b,2}\hat{\delta}_{b,2}(k|k) + E_4^{b,2}\hat{z}_{b,2}(k|k) \leq g_5^{b,2} \quad (61)$$

Then, update equations 53, 54 are used to determine components of $\hat{x}_{b,i}(k+1|k)$:

$$\hat{x}_{b,1}(k+1|k) = A^{b,1}x_{b,1}(k) + B_1^{b,1}u_{b,1}(k) + B_3^{b,1}\hat{z}_{b,1}(k|k) \quad (62)$$

$$\hat{x}_{b,2}(k+1|k) = A^{b,2}x_{b,2}(k) + B_1^{b,2}u_{b,2}(k) + B_3^{b,2}\hat{z}_{b,2}(k|k) \quad (63)$$

Again, inequality equations 57, 58 are used to determine $\hat{\delta}_{b,i}(k+1|k)$, by looking at time step $k+1$:

$$\begin{aligned} E_1^{b,1}\hat{x}_{b,1}(k+1|k) + E_2^{b,1}u_{b,1}(k+1) + E_3^{b,1}\hat{\delta}_{b,1}(k+1|k) + E_4^{b,1}\hat{z}_{b,1}(k+1|k) &\leq g_5^{b,1} \\ E_1^{b,2}\hat{x}_{b,2}(k+1|k) + E_2^{b,2}u_{b,2}(k+1) + E_3^{b,2}\hat{\delta}_{b,2}(k+1|k) + E_4^{b,2}\hat{z}_{b,2}(k+1|k) &\leq g_5^{b,2} \end{aligned}$$

Here, $\hat{x}_{b,i}(k+1|k)$ can be eliminated using equations 62 and 63:

$$E_1^{b,1}A^{b,1}x_{b,1}(k) + E_1^{b,1}B_1^{b,1}u_{b,1}(k) + E_2^{b,1}u_{b,1}(k+1) + E_1^{b,1}B_3^{b,1}\hat{z}_{b,1}(k|k) + E_4^{b,1}\hat{z}_{b,1}(k+1|k) + E_3^{b,1}\hat{\delta}_{b,1}(k+1|k) \leq g_5^{b,1} \quad (64)$$

$$E_1^{b,2}A^{b,2}x_{b,2}(k) + E_1^{b,2}B_1^{b,2}u_{b,2}(k) + E_2^{b,2}u_{b,2}(k+1) + E_1^{b,2}B_3^{b,2}\hat{z}_{b,2}(k|k) + E_4^{b,2}\hat{z}_{b,2}(k+1|k) + E_3^{b,2}\hat{\delta}_{b,2}(k+1|k) \leq g_5^{b,2} \quad (65)$$

Then, we use update equations 53 and 54 again to determine the next time step $\hat{x}_{b,i}(k+2|k)$:

$$\hat{x}_{b,1}(k+2|k) = A^{b,1}\hat{x}_{b,1}(k+1|k) + B_1^{b,1}u_{b,1}(k+1) + B_3^{b,1}\hat{z}_{b,1}(k+1|k)$$

$$\hat{x}_{b,2}(k+2|k) = A^{b,2}\hat{x}_{b,2}(k+1|k) + B_1^{b,2}u_{b,2}(k+1) + B_3^{b,2}\hat{z}_{b,2}(k+1|k)$$

Here, $\hat{x}_{b,i}(k+1|k)$ can be eliminated using equations 62 and 63:

$$\hat{x}_{b,1}(k+2|k) = (A^{b,1})^2x_{b,1}(k) + A^{b,1}B_1^{b,1}u_{b,1}(k) + B_1^{b,1}u_{b,1}(k+1) + A^{b,1}B_3^{b,1}\hat{z}_{b,1}(k|k) + B_3^{b,1}\hat{z}_{b,1}(k+1|k) \quad (66)$$

$$\hat{x}_{b,2}(k+2|k) = (A^{b,2})^2x_{b,2}(k) + A^{b,2}B_1^{b,2}u_{b,2}(k) + B_1^{b,2}u_{b,2}(k+1) + A^{b,2}B_3^{b,2}\hat{z}_{b,2}(k|k) + B_3^{b,2}\hat{z}_{b,2}(k+1|k) \quad (67)$$

When continuing this way, the update and inequality equations for $\hat{x}_{b,i}(k+3|k)$ can be determined and when continuing even further, the update and inequality equations for $\hat{x}_{b,i}(k+N_p|k)$. The general form of the equations is the following:

$$\begin{aligned} E_1^{b,i}(A^{b,i})^\ell x_{b,i}(k) + E_1^{b,i}(A^{b,i})^{\ell-1}B_1^{b,i}u_{b,i}(k) + E_1^{b,i}(A^{b,i})^{\ell-2}B_1^{b,i}u_{b,i}(k+1) + \dots + E_1^{b,i}B_1^{b,i}u_{b,i}(k+\ell-1) \\ + E_2^{b,i}u_{b,i}(k+\ell) + E_1^{b,i}(A^{b,i})^{\ell-1}B_3^{b,i}\hat{z}_{b,i}(k|k) + E_1^{b,i}(A^{b,i})^{\ell-2}B_3^{b,i}\hat{z}_{b,i}(k+1|k) + \dots \\ + E_1^{b,i}B_3^{b,i}\hat{z}_{b,i}(k+\ell-1|k) + E_4^{b,i}\hat{z}_{b,i}(k+\ell|k) + E_3^{b,i}\hat{\delta}_{b,i}(k+\ell|k) \leq g_5^{b,i} \end{aligned} \quad (68)$$

$$\begin{aligned} \hat{x}_{b,i}(k+\ell+1|k) = (A^{b,i})^{\ell+1}x_{b,i}(k) + (A^{b,i})^\ell B_1^{b,i}u_{b,i}(k) + (A^{b,i})^{\ell-1}B_1^{b,i}u_{b,i}(k+1) + \dots + A^{b,i}B_1^{b,i}u_{b,i}(k+\ell-1) \\ + B_1^{b,i}u_{b,i}(k+\ell) + (A^{b,i})^\ell B_3^{b,i}\hat{z}_{b,i}(k|k) + (A^{b,i})^{\ell-1}B_3^{b,i}\hat{z}_{b,i}(k+1|k) + \dots \\ + A^{b,i}B_3^{b,i}\hat{z}_{b,i}(k+\ell-1|k) + B_3^{b,i}\hat{z}_{b,i}(k+\ell|k) \end{aligned} \quad (69)$$

for $\ell = 0, \dots, N_p - 1$.

Diesel generator

For the diesel generator, first the following vectors are defined. Vectors $\tilde{u}_d(k), \tilde{x}_d(k)$ have dimension $\mathbb{R}^{N_p \times 1}$, while vectors $\tilde{\delta}_d(k), \tilde{z}_d(k)$ have dimension $\mathbb{R}^{4N_p \times 1}$ (as can be seen in equation 56, each δ_d, z_d has length 4):

$$\begin{aligned} \tilde{\delta}_d(k) &= \begin{bmatrix} \hat{\delta}_d(k|k) \\ \vdots \\ \hat{\delta}_d(k+N_p-1|k) \end{bmatrix} & \tilde{u}_d(k) &= \begin{bmatrix} u_{b,i}(k) \\ \vdots \\ u_d(k+N_p-1) \end{bmatrix} & \tilde{z}_d(k) &= \begin{bmatrix} \hat{z}_d(k|k) \\ \vdots \\ \hat{z}_d(k+N_p-1|k) \end{bmatrix} \\ & & \tilde{x}_d(k) &= \begin{bmatrix} \hat{x}_d(k+1|k) \\ \vdots \\ \hat{x}_d(k+N_p|k) \end{bmatrix} \end{aligned}$$

Next, the derivation of the update and inequality equations for each time step was executed in the same way as for the batteries. The general form of the expressions which is then obtained, is the following:

$$\begin{aligned}
& E_1^d(A^d)^\ell x_d(k) + E_1^d(A^d)^{\ell-1} B_1^d u_d(k) + E_1^d(A^d)^{\ell-2} B_1^d u_d(k+1) + \dots + E_1^d B_1^d u_d(k+\ell-1) + E_2^d u_d(k+\ell) \\
& + E_1^d(A^d)^{\ell-1} B_3^d \hat{z}_d(k|k) + E_1^d(A^d)^{\ell-2} B_3^d \hat{z}_d(k+1|k) + \dots + E_1^d B_3^d \hat{z}_d(k+\ell-1|k) + E_4^d \hat{z}_d(k+\ell|k) \\
& + E_1^d(A^d)^{\ell-1} B_2^d \hat{\delta}_d(k|k) + E_1^d(A^d)^{\ell-2} B_2^d \hat{\delta}_d(k+1|k) + \dots + E_1^d B_2^d \hat{\delta}_d(k+\ell-1|k) + E_3^d \hat{\delta}_d(k+\ell|k) \quad (70) \\
& + E_1^d \sum_{n=0}^{\ell} (A^d)^{n-1} B_4^d \leq g_5^d
\end{aligned}$$

$$\begin{aligned}
\hat{x}_d(k+\ell+1|k) = & (A^d)^{\ell+1} x_d(k) + (A^d)^\ell B_1^d u_d(k) + (A^d)^{\ell-1} B_1^d u_d(k+1) + \dots + A^d B_1^d u_d(k+\ell-1) \\
& + B_1^d u_d(k+\ell) + (A^d)^\ell B_3^d \hat{z}_d(k|k) + (A^d)^{\ell-1} B_3^d \hat{z}_d(k+1|k) + \dots + A^d B_3^d \hat{z}_d(k+\ell-1|k) \\
& + B_3^d \hat{z}_d(k+\ell|k) + (A^d)^\ell B_2^d \hat{\delta}_d(k|k) + (A^d)^{\ell-1} B_2^d \hat{\delta}_d(k+1|k) + \dots + A^d B_2^d \hat{\delta}_d(k+\ell-1|k) \\
& + B_2^d \hat{\delta}_d(k+\ell|k) + \sum_{n=0}^{\ell} (A^d)^n B_4^d \quad (71)
\end{aligned}$$

for $\ell = 0, \dots, N_p - 1$. Inequality expression 70 does not hold for $\ell = 0$ and should only be used for all expressions $\ell > 1$.

Batteries and diesel generator together

The estimate vector $\tilde{V}(k)$ is defined as follows:

$$\tilde{V}(k) = \begin{bmatrix} \tilde{V}_{b,1}(k) \\ \tilde{V}_{b,2}(k) \\ \tilde{V}_d(k) \end{bmatrix} \quad (72)$$

Where the submatrices are given by:

$$\begin{aligned}
\tilde{V}_{b,1}(k) = & \begin{bmatrix} \hat{\delta}_{b,1}(k|k) \\ \hat{\delta}_{b,1}(k+1|k) \\ \vdots \\ \hat{\delta}_{b,1}(k+N_p-1|k) \\ u_{b,1}(k|k) \\ u_{b,1}(k+1|k) \\ \vdots \\ u_{b,1}(k+N_p-1|k) \\ \hat{z}_{b,1}(k|k) \\ \hat{z}_{b,1}(k+1|k) \\ \vdots \\ \hat{z}_{b,1}(k+N_p-1|k) \end{bmatrix} & \tilde{V}_{b,2}(k) = & \begin{bmatrix} \hat{\delta}_{b,2}(k|k) \\ \hat{\delta}_{b,2}(k+1|k) \\ \vdots \\ \hat{\delta}_{b,2}(k+N_p-1|k) \\ u_{b,2}(k|k) \\ u_{b,2}(k+1|k) \\ \vdots \\ u_{b,2}(k+N_p-1|k) \\ \hat{z}_{b,2}(k|k) \\ \hat{z}_{b,2}(k+1|k) \\ \vdots \\ \hat{z}_{b,2}(k+N_p-1|k) \end{bmatrix} & \tilde{V}_d(k) = & \begin{bmatrix} \hat{\delta}_d(k|k) \\ \hat{\delta}_d(k+1|k) \\ \vdots \\ \hat{\delta}_d(k+N_p-1|k) \\ u_d(k|k) \\ u_d(k+1|k) \\ \vdots \\ u_d(k+N_p-1|k) \\ \hat{z}_d(k|k) \\ \hat{z}_d(k+1|k) \\ \vdots \\ \hat{z}_d(k+N_p-1|k) \end{bmatrix} \quad (73)
\end{aligned}$$

Here, $\tilde{V}_{b,1}(k), \tilde{V}_{b,2}(k) \in \mathbb{R}^{3N_p \times 1}$ and $\tilde{V}_d(k) \in \mathbb{R}^{9N_p \times 1}$. Furthermore, $x(k), \tilde{x}(k)$ are described by:

$$x(k) = \begin{bmatrix} x_{b,1}(k) \\ x_{b,2}(k) \\ x_d(k) \end{bmatrix} \quad \tilde{x}(k) = \begin{bmatrix} \hat{x}_{b,1}(k+1|k) \\ \vdots \\ \hat{x}_{b,1}(k+N_p|k) \\ \hat{x}_{b,2}(k+1|k) \\ \vdots \\ \hat{x}_{b,2}(k+N_p|k) \\ \hat{x}_d(k+1|k) \\ \vdots \\ \hat{x}_d(k+N_p|k) \end{bmatrix} \quad (74)$$

For $x(k) \in \mathbb{R}^{3 \times 1}$ and $\tilde{x}(k) \in \mathbb{R}^{3N_p \times 1}$. With $\tilde{V}(k), x(k), \tilde{x}(k)$ and the equations and inequalities obtained in the previous part, the expressions can be written in a more compact form. This compact form, including the notation of the matrices, is given in the following two subsections: ‘Update equations MILP’ and ‘Constraint equations MILP’.

Update equations MILP

The update equations, given by 69 and 71 for the batteries and diesel generator respectively, can be summarized as follows:

$$\tilde{x}(k) = M_1 \tilde{V}(k) + M_2 x(k) + M_3 \quad (75)$$

Here, the following holds for the matrices:

$$M_1 = \begin{bmatrix} M_1^{b,1} & 0 & 0 \\ 0 & M_1^{b,2} & 0 \\ 0 & 0 & M_1^d \end{bmatrix} \quad M_2 = \begin{bmatrix} M_2^{b,1} & 0 & 0 \\ 0 & M_2^{b,2} & 0 \\ 0 & 0 & M_2^d \end{bmatrix} \quad M_3 = \begin{bmatrix} M_3^{b,1} \\ M_3^{b,2} \\ M_3^d \end{bmatrix}$$

$$M_1^d = \begin{bmatrix} M_1^d(\hat{\delta}_d) & M_1^d(u_d) & M_1^d(\hat{z}_d) \end{bmatrix} \quad (76)$$

The dimensions of the submatrices of M_1 are given by $M_1^{b,1}, M_1^{b,2} \in \mathbb{R}^{N_p \times 3N_p}$ and $M_1^d \in \mathbb{R}^{N_p \times 9N_p}$. The submatrices of M_1 can be found somewhat further in the report. For M_2 , the submatrices all have same size $M_2^{b,1}, M_2^{b,2}, M_2^d \in \mathbb{R}^{N_p \times 1}$. Finally, for M_3 , the same holds, thus $M_3^{b,1}, M_3^{b,2}, M_3^d \in \mathbb{R}^{N_p \times 1}$. The submatrices are defined as:

$$M_2^{b,1} = \begin{bmatrix} (A^{b,1}) \\ (A^{b,1})^2 \\ (A^{b,1})^3 \\ \vdots \\ (A^{b,1})^{(l+1)} \\ \vdots \\ (A^{b,1})^{N_p} \end{bmatrix} \quad M_2^{b,2} = \begin{bmatrix} (A^{b,2}) \\ (A^{b,2})^2 \\ (A^{b,2})^3 \\ \vdots \\ (A^{b,2})^{(l+1)} \\ \vdots \\ (A^{b,2})^{N_p} \end{bmatrix} \quad M_2^d = \begin{bmatrix} (A^d) \\ (A^d)^2 \\ (A^d)^3 \\ \vdots \\ (A^d)^{(l+1)} \\ \vdots \\ (A^d)^{N_p} \end{bmatrix} \quad (77)$$

$$M_1^d(\hat{\delta}_d) = \begin{bmatrix} B_2^d & 0 & 0 & \dots & 0 \\ (A^d)B_2^d & B_2^d & 0 & \dots & 0 \\ (A^d)^2 B_2^d & (A^d)B_2^d & B_2^d & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ (A^d)^l B_2^d & (A^d)^{(l-1)} B_2^d & (A^d)^{(l-2)} B_2^d & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & 0 \\ (A^d)^{(N_p-1)} B_2^d & (A^d)^{(N_p-2)} B_2^d & (A^d)^{(N_p-3)} B_2^d & \dots & B_2^d \end{bmatrix} \quad (78)$$

$$M_1^d(u_d) = \begin{bmatrix} B_1^d & 0 & 0 & \dots & 0 \\ (A^d)B_1^d & B_1^d & 0 & \dots & 0 \\ (A^d)^2 B_1^d & (A^d)B_1^d & B_1^d & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ (A^d)^l B_1^d & (A^d)^{(l-1)} B_1^d & (A^d)^{(l-2)} B_1^d & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & 0 \\ (A^d)^{(N_p-1)} B_1^d & (A^d)^{(N_p-2)} B_1^d & (A^d)^{(N_p-3)} B_1^d & \dots & B_1^d \end{bmatrix} \quad (79)$$

$$M_1^d(\hat{z}_d) = \begin{bmatrix} B_3^d & 0 & 0 & \dots & 0 \\ (A^d)B_3^d & B_3^d & 0 & \dots & 0 \\ (A^d)^2 B_3^d & (A^d)B_3^d & B_3^d & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ (A^d)^l B_3^d & (A^d)^{(l-1)} B_3^d & (A^d)^{(l-2)} B_3^d & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & 0 \\ (A^d)^{(N_p-1)} B_3^d & (A^d)^{(N_p-2)} B_3^d & (A^d)^{(N_p-3)} B_3^d & \dots & B_3^d \end{bmatrix} \quad (80)$$

$$M_1^{b,1} = \begin{bmatrix} 0 & \dots & 0 & B_1^{b,1} & 0 & \dots & 0 & B_3^{b,1} & 0 & \dots \\ 0 & \dots & 0 & (A^{b,1})B_1^{b,1} & B_1^{b,1} & \dots & 0 & (A^{b,1})B_3^{b,1} & B_3^{b,1} & \dots \\ \vdots & \ddots & \vdots & (A^{b,1})^2 B_1^{b,1} & B_1^{b,1} & \ddots & 0 & (A^{b,1})^2 B_3^{b,1} & B_3^{b,1} & \ddots \\ \vdots & \ddots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \vdots & \ddots \\ 0 & \dots & 0 & (A^{b,1})^l B_1^{b,1} & (A^{b,1})^{(l-1)} B_1^{b,1} & \dots & 0 & (A^{b,1})^{(l-1)} B_3^{b,1} & (A^{b,1})^{(l-2)} B_3^{b,1} & \dots \\ \vdots & \ddots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \vdots & \ddots \\ 0 & \dots & 0 & (A^{b,1})^{(N_p-1)} B_1^{b,1} & (A^{b,1})^{(N_p-2)} B_1^{b,1} & \dots & 0 & (A^{b,1})^{(N_p-2)} B_3^{b,1} & (A^{b,1})^{(N_p-3)} B_3^{b,1} & \dots \end{bmatrix} \quad (81)$$

$$M_1^{b,2} = \begin{bmatrix} 0 & \dots & 0 & B_1^{b,2} & 0 & \dots & 0 & B_3^{b,2} & 0 & \dots \\ 0 & \dots & 0 & (A^{b,2})B_1^{b,2} & B_1^{b,2} & \dots & 0 & (A^{b,2})B_3^{b,2} & B_3^{b,2} & \dots \\ \vdots & \ddots & \vdots & (A^{b,2})^2 B_1^{b,2} & B_1^{b,2} & \ddots & 0 & (A^{b,2})^2 B_3^{b,2} & B_3^{b,2} & \ddots \\ \vdots & \ddots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \vdots & \ddots \\ 0 & \dots & 0 & (A^{b,2})^l B_1^{b,2} & (A^{b,2})^{(l-1)} B_1^{b,2} & \dots & 0 & (A^{b,2})^{(l-1)} B_3^{b,2} & (A^{b,2})^{(l-2)} B_3^{b,2} & \dots \\ \vdots & \ddots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \vdots & \ddots \\ 0 & \dots & 0 & (A^{b,2})^{(N_p-1)} B_1^{b,2} & (A^{b,2})^{(N_p-2)} B_1^{b,2} & \dots & 0 & (A^{b,2})^{(N_p-2)} B_3^{b,2} & (A^{b,2})^{(N_p-3)} B_3^{b,2} & \dots \end{bmatrix} \quad (82)$$

$$M_3^{b,1} = \begin{bmatrix} 0 \\ \vdots \\ 0 \end{bmatrix} \quad M_3^{b,2} = \begin{bmatrix} 0 \\ \vdots \\ 0 \end{bmatrix} \quad M_3^d = \begin{bmatrix} B_4^d \\ B_4^d(1 + A^d) \\ B_4^d(1 + A^d + (A^d)^2) \\ \vdots \\ B_4^d(1 + A^d + (A^d)^2 + \dots + (A^d)^{N_p-1}) \end{bmatrix} \quad (83)$$

Constraint equations MILP

The constraint equations, given by 68 and 70 for the batteries and diesel generator respectively, can be summarized as follows:

$$F_1 \tilde{V}(k) \leq F_2 + F_3 x(k) \quad (84)$$

Here, the following holds for the matrices:

$$F_1 = \begin{bmatrix} F_1^{b,1} & 0 & 0 \\ 0 & F_1^{b,2} & 0 \\ 0 & 0 & F_1^d \end{bmatrix} \quad F_2 = \begin{bmatrix} F_2^{b,1} \\ F_2^{b,2} \\ F_2^d \end{bmatrix} \quad F_3 = \begin{bmatrix} F_3^{b,1} & 0 & 0 \\ 0 & F_3^{b,2} & 0 \\ 0 & 0 & F_3^d \end{bmatrix}$$

The dimensions of the submatrices of F_1 are given by $F_1^{b,1}, F_1^{b,2} \in \mathbb{R}^{8N_p \times 3N_p}$ and $F_1^d \in \mathbb{R}^{27N_p \times 9N_p}$. For F_2 , the submatrices are of size $F_2^{b,1}, F_2^{b,2} \in \mathbb{R}^{8N_p \times 1}$ and $F_2^d \in \mathbb{R}^{27N_p \times 1}$. Finally, for F_3 : $F_3^{b,1}, F_3^{b,2} \in \mathbb{R}^{8N_p \times 1}$ and $F_3^d \in \mathbb{R}^{27N_p \times 1}$. The submatrices are defined as:

$$F_2^{b,1} = \begin{bmatrix} g_5^{b,1} \\ \vdots \\ g_5^{b,1} \end{bmatrix} \quad F_2^{b,2} = \begin{bmatrix} g_5^{b,2} \\ \vdots \\ g_5^{b,2} \end{bmatrix} \quad F_2^d = \begin{bmatrix} g_5^d \\ \vdots \\ g_5^d \end{bmatrix} - \begin{bmatrix} 0 \\ E_1^d B_4^d \\ E_1^d B_4^d(1 + A^d) \\ E_1^d B_4^d(1 + A^d + (A^d)^2) \\ \vdots \\ E_1^d B_4^d(1 + A^d + (A^d)^2 + \dots + (A^d)^{N_p-2}) \end{bmatrix} \quad (85)$$

$$F_3^{b,1} = \begin{bmatrix} -E_1^{b,1} \\ -E_1^{b,1} A^{b,1} \\ -E_1^{b,1} (A^{b,1})^2 \\ \vdots \\ -E_1^{b,1} (A^{b,1})^{N_p-1} \end{bmatrix} \quad F_3^{b,2} = \begin{bmatrix} -E_1^{b,2} \\ -E_1^{b,2} A^{b,2} \\ -E_1^{b,2} (A^{b,2})^2 \\ \vdots \\ -E_1^{b,2} (A^{b,2})^{N_p-1} \end{bmatrix} \quad F_3^d = \begin{bmatrix} -E_1^d \\ -E_1^d A^d \\ -E_1^d (A^d)^2 \\ \vdots \\ -E_1^d (A^d)^{N_p-1} \end{bmatrix} \quad (86)$$

$$F_1^{b,1} = \begin{bmatrix} E_3^{b,1} & 0 & 0 & 0 & \dots & 0 & E_2^{b,1} & 0 & \dots & 0 & E_4^{b,1} & 0 & \dots & 0 \\ 0 & E_3^{b,1} & 0 & 0 & \dots & 0 & E_2^{b,1} & E_2^{b,1} & 0 & \dots & E_4^{b,1} & E_4^{b,1} & 0 & 0 \\ 0 & 0 & E_3^{b,1} & 0 & \dots & 0 & E_1^{b,1} A^{b,1} B_1^{b,1} & E_1^{b,1} B_1^{b,1} & E_2^{b,1} & 0 & E_1^{b,1} A^{b,1} B_3^{b,1} & E_1^{b,1} B_3^{b,1} & E_4^{b,1} & 0 \\ \vdots & \vdots & \vdots & \ddots & & & \vdots & \vdots & \ddots & & \vdots & \vdots & \ddots & \\ 0 & 0 & \dots & E_3^{b,1} & & E_1^{b,1} (A^{b,1})^{N_p-2} B_1^{b,1} & E_1^{b,1} (A^{b,1})^{N_p-3} B_1^{b,1} & E_2^{b,1} & & E_1^{b,1} (A^{b,1})^{N_p-2} B_3^{b,1} & E_1^{b,1} (A^{b,1})^{N_p-3} B_3^{b,1} & \ddots & E_4^{b,1} \end{bmatrix} \quad (87)$$

$$F_1^{b,2} = \begin{bmatrix} E_3^{b,2} & 0 & 0 & 0 & \dots & 0 & E_2^{b,2} & 0 & \dots & 0 & E_4^{b,2} & 0 & \dots & 0 \\ 0 & E_3^{b,2} & 0 & 0 & \dots & 0 & E_1^{b,2} B_1^{b,2} & E_2^{b,2} & 0 & \dots & E_4^{b,2} & E_4^{b,2} & 0 & 0 \\ 0 & 0 & E_3^{b,2} & 0 & \dots & 0 & E_1^{b,2} A^{b,2} B_1^{b,2} & E_1^{b,2} B_1^{b,2} & E_2^{b,2} & 0 & E_1^{b,2} A^{b,2} B_3^{b,2} & E_1^{b,2} B_3^{b,2} & E_4^{b,2} & 0 \\ \vdots & \vdots & \vdots & \ddots & & & \vdots & \vdots & \ddots & & \vdots & \vdots & \ddots & \\ 0 & 0 & \dots & E_3^{b,2} & & E_1^{b,2} (A^{b,2})^{N_p-2} B_1^{b,2} & E_1^{b,2} (A^{b,2})^{N_p-3} B_1^{b,2} & E_2^{b,2} & & E_1^{b,2} (A^{b,2})^{N_p-2} B_3^{b,2} & E_1^{b,2} (A^{b,2})^{N_p-3} B_3^{b,2} & \ddots & E_4^{b,2} \end{bmatrix} \quad (88)$$

$$F_1^d = \begin{bmatrix} E_3^d & 0 & 0 & 0 & \dots & 0 & E_2^d & 0 & \dots & 0 & E_4^d & 0 & \dots & 0 \\ E_1^d B_2^d & E_3^d & 0 & 0 & \dots & 0 & E_2^d & 0 & \dots & 0 & E_1^d B_3^d & E_4^d & 0 & 0 \\ E_1^d A^d B_2^d & E_1^d B_2^d & E_3^d & 0 & \dots & 0 & E_2^d & 0 & \dots & 0 & E_1^d A^d B_3^d & E_1^d B_3^d & E_4^d & 0 \\ \vdots & \vdots & \vdots & \ddots & & & \vdots & \vdots & \ddots & & \vdots & \vdots & \ddots & \\ E_1^d (A^d)^{N_p-2} B_2^d & E_1^d (A^d)^{N_p-3} B_2^d & E_1^d (A^d)^{N_p-2} B_3^d & E_1^d (A^d)^{N_p-3} B_3^d & \dots & E_2^d & E_1^d (A^d)^{N_p-2} B_3^d & E_1^d (A^d)^{N_p-3} B_3^d & \dots & E_4^d \end{bmatrix} \quad (89)$$

Cost function

The cost function of the microgrid at time step k is given by:

$$J(k) = \sum_{j=0}^{N_p-1} \left(\sum_{i=1}^{N_b} W_{b,i} |\Delta s_{b,i}(k+j)| + W_d |\Delta s_d(k+j)| \right) - W_{\text{fuel}} (x_d(k+N_p) - x_d(k)) \quad (90)$$

$$- W_e \sum_{i=1}^{N_b} (x_{b,i}(k+N_p) - x_{b,i}(k)) + \sum_{j=0}^{N_p-1} P_{\text{imp}}(k+j) C_e(k+j) \quad (91)$$

Here, $P_{\text{imp}}(k)$ is defined by:

$$P_{\text{imp}}(k+j) = P_{\text{load}}(k+j) - u_d(k+j) - \sum_{i=1}^{N_b} u_{b,i}(k+j), \quad \forall j \quad (92)$$

The values of $\tilde{C}_e, \tilde{P}_{\text{load}}$ are known and given by the vectors:

$$\tilde{C}_e(k) = \begin{bmatrix} C_e(k) & \dots & C_e(k+N_p-1) \end{bmatrix}^T$$

$$\tilde{P}_{\text{load}}(k) = \begin{bmatrix} P_{\text{load}}(k) & \dots & P_{\text{load}}(k+N_p-1) \end{bmatrix}^T$$

The cost function can be rewritten in terms of the estimate vector $\tilde{V}(k)$ (given by equations 72,73), $\tilde{x}(k)$, $x(k)$ (given by equations 74) and vectors $\tilde{C}_e, \tilde{P}_{\text{imp}}$:

$$J(k) = W_1 |\tilde{V}(k)| + W_3 \tilde{x}(k) + W_4 x(k) + \sum_{j=0}^{N_p-1} P_{\text{imp}}(k+j) C_e(k+j) \quad (93)$$

Here, the weights W_1 to W_4 , with the exception of W_2 , are defined as follows:

$$W_1 = [W_{b,1} \dots W_{b,1} \ 0 \mid W_{b,2} \dots W_{b,2} \ 0 \mid W_d \dots W_d \ 0] \quad (94)$$

$$W_3 = [0 \dots 0 \ -W_e \mid 0 \dots 0 \ -W_e \mid 0 \dots 0 \ -W_{\text{fuel}}] \quad (95)$$

$$W_4 = [W_e \ W_e \ W_{\text{fuel}}] \quad (96)$$

For $W_1 \in \mathbb{R}^{1 \times 3N_p}$, $W_3 \in \mathbb{R}^{1 \times 3N_p}$ and $W_4 \in \mathbb{R}^{1 \times 3}$.

For W_2 , the following holds:

$$W_2 = \begin{bmatrix} W_2^{b,1} & 0 & 0 \\ 0 & W_2^{b,2} & 0 \\ 0 & 0 & W_2^d \end{bmatrix} \quad (97)$$

$$W_2^{b,1} = \begin{bmatrix} 1 & 0 & \dots & 0 & 0 & \dots & 0 & 0 & \dots & 0 \\ -1 & 1 & \dots & 0 & 0 & \dots & 0 & 0 & \dots & 0 \\ & \ddots & \ddots & & 0 & \dots & 0 & 0 & \dots & 0 \\ 0 & \dots & -1 & 1 & 0 & \dots & 0 & 0 & \dots & 0 \end{bmatrix} \quad W_2^{b,2} = \begin{bmatrix} 1 & 0 & \dots & 0 & 0 & \dots & 0 & 0 & \dots & 0 \\ -1 & 1 & \dots & 0 & 0 & \dots & 0 & 0 & \dots & 0 \\ & \ddots & \ddots & & 0 & \dots & 0 & 0 & \dots & 0 \\ 0 & \dots & -1 & 1 & 0 & \dots & 0 & 0 & \dots & 0 \end{bmatrix} \quad (98)$$

$$W_2^d = \begin{bmatrix} 1 & 1 & 1 & 1 & 0 & 0 & 0 & 0 & \dots & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ -1 & -1 & -1 & -1 & 1 & 1 & 1 & 1 & \dots & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ & & & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots \\ 0 & \dots & & -1 & -1 & -1 & -1 & & & 1 & 1 & 1 & 1 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad (99)$$

Here, $W_2 \in \mathbb{R}^{3N_p \times 15N_p}$ and the submatrices are $W_2^{b,1}, W_2^{b,2} \in \mathbb{R}^{N_p \times 3N_p}$ and $W_2^d \in \mathbb{R}^{N_p \times 9N_p}$.

Next, the estimate vector $\tilde{V}(k)$ is expanded with term P_{imp} as follows:

$$\tilde{V}_{\text{new}}(k) = \begin{bmatrix} \tilde{V}_{b,1}(k) \\ \tilde{V}_{b,2}(k) \\ \tilde{V}_d(k) \\ P_{\text{imp}}(k) \\ \vdots \\ P_{\text{imp}}(k + N_p) \end{bmatrix} \quad (100)$$

The submatrices $\tilde{V}_{b,1}(k)$, $\tilde{V}_{b,2}(k)$, $\tilde{V}_d(k)$ are still given by equation 73.

Substituting the update equation found for $\tilde{x}(k)$ and using the new defined vector $\tilde{V}_{\text{new}}(k)$, the cost function expression 93 can be simplified to:

$$\begin{aligned} J(k) &= W_1 |W_2 \tilde{V}(k)| + W_3 (M_1 \tilde{V}(k) + M_2 x(k) + M_3) + W_4 x(k) + \sum_{j=0}^{N_p-1} P_{\text{imp}}(k+j) C_e(k+j) \\ &= W_1 |W_2 \tilde{V}(k)| + W_3 M_1 \tilde{V}(k) + (W_3 M_2 + W_4) x(k) + W_3 M_3 + \sum_{j=0}^{N_p-1} P_{\text{imp}}(k+j) C_e(k+j) \\ &= W_1 |W_{2,\text{new}} \tilde{V}_{\text{new}}(k)| + S_1 \tilde{V}_{\text{new}}(k) + S_2 x(k) + W_3 M_3 \end{aligned}$$

The new matrices are defined as:

$$W_{2,\text{new}} = \left[\begin{array}{ccc|ccc} W_2^{b,1} & 0 & 0 & 0 & \dots & 0 \\ 0 & W_2^{b,2} & 0 & 0 & \dots & 0 \\ 0 & 0 & W_2^d & 0 & \dots & 0 \end{array} \right] \quad (101)$$

The zero-matrix added is of size $3N_p \times N_p$ and is multiplied with the P_{imp} terms in the $\tilde{V}_{\text{new}}(k)$ vector. Thus, $W_2 \in \mathbb{R}^{3N_p \times 16N_p}$. The two S matrices are given by:

$$S_1 = \begin{bmatrix} W_3 M_1 & \tilde{C}_e(k) & 0 \end{bmatrix} \quad S_2 = W_3 M_2 + W_4 \quad (102)$$

Here, $S_1 \in \mathbb{R}^{1 \times 16N_p}$ and $S_2 \in \mathbb{R}^{1 \times 3}$.

As a final step, the definition of P_{imp} given by equation 92 should be added to the constraints as follows:

$$\begin{aligned} P_{\text{imp}}(k+j) &\leq P_{\text{load}}(k+j) - u_d(k+j) - \sum_{i=1}^{N_b} u_{b,i}(k+j), \quad \forall j \\ P_{\text{imp}}(k+j) &\geq P_{\text{load}}(k+j) - u_d(k+j) - \sum_{i=1}^{N_b} u_{b,i}(k+j), \quad \forall j \end{aligned}$$

Rewriting these constraints:

$$u_d(k+j) + \sum_{i=1}^{N_b} u_{b,i}(k+j) + P_{\text{imp}}(k+j) \leq P_{\text{load}}(k+j), \quad \forall j \quad (103)$$

$$-u_d(k+j) - \sum_{i=1}^{N_b} u_{b,i}(k+j) - P_{\text{imp}}(k+j) \leq -P_{\text{load}}(k+j), \quad \forall j \quad (104)$$

These two constraints are added to the general inequality expression to obtain a new constraint equation:

$$F_{1,\text{new}} \tilde{V}_{\text{new}}(k) \leq F_{2,\text{new}} + F_{3,\text{new}} x(k) \quad (105)$$

$$\begin{aligned}
F_{1,new} &= \left[\begin{array}{ccc|ccc} F_1^{b,1} & 0 & 0 & 0 & \dots & 0 \\ 0 & F_1^{b,2} & 0 & 0 & \dots & 0 \\ 0 & 0 & F_1^d & 0 & \dots & 0 \\ \hline F_{11}^{b,1} & F_{11}^{b,2} & F_{11}^d & & & I \\ -F_{11}^{b,1} & -F_{11}^{b,2} & -F_{11}^d & & & -I \end{array} \right] & F_{2,new} &= \begin{bmatrix} F_2^{b,1} \\ F_2^{b,2} \\ F_2^d \\ \hline P_{\text{load}}(k) \\ \vdots \\ P_{\text{load}}(k + N_p) \\ -P_{\text{load}}(k) \\ \vdots \\ -P_{\text{load}}(k + N_p) \end{bmatrix} & F_{3,new} &= \begin{bmatrix} F_3^{b,1} & 0 & 0 \\ 0 & F_3^{b,2} & 0 \\ 0 & 0 & F_3^d \\ \hline 0 & \dots & 0 \\ \vdots & & \vdots \\ 0 & \dots & 0 \end{bmatrix}
\end{aligned} \tag{106}$$

The dimensions of the submatrices in the left upper corner of $F_{1,new}$ are given by $43N_p \times 15N_p$, the zeros in the right upper corner by $43N_p \times N_p$, the matrix in the corner left down by $2N_p \times 15N_p$ and finally, the identity matrices are both $N_p \times N_p$.

For $F_{2,new}$, the upper half is of size $43N_p \times 1$. The $+P_{\text{load}}$ and $-P_{\text{load}}$ vectors are both N_p long.

Finally, for $F_{3,new}$, the upper half is of size $43N_p \times 3$ and the zero matrix beneath it has dimension $2N_p \times 3$.

The submatrices F_{11} located in the $F_{1,new}$ matrix, for $F_{11}^{b,1} = F_{11}^{b,2} \in \mathbb{R}^{N_p \times 9N_p}$ and $F_{11}^d \in \mathbb{R}^{N_p \times 15N_p}$, are given by:

$$F_{11}^{b,1} = F_{11}^{b,2} = \begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \dots & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & \dots & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & \dots & 0 \\ & & & & & & \ddots & \ddots & \ddots & & & \\ 0 & & & \dots & & & 0 & & 0 & 1 & 0 \end{bmatrix} \tag{107}$$

$$F_{11}^d = \begin{bmatrix} 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \dots & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \dots & 0 \\ & & & & & & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & \ddots & & \\ 0 & & & \dots & & & & & & & & 0 & & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \tag{108}$$

When minimizing this cost function, subjected to the constraints as defined above, the absolute value lines should be removed. This is done by making use of the following proposition from the course *Optimization in Systems and Control*:

Proposition 8.2 Consider $A \in \mathbb{R}^{m \times n}$, $b \in \mathbb{R}^m$ and $w \in \mathbb{R}^n$. If $w_i > 0$ for all i , then the following problems are equivalent:

$$\begin{aligned}
& \min_{x \in \mathbb{R}^n} \sum_{i=1}^n w_i |x_i| \quad \text{subject to } Ax \leq b \\
& \min_{x, \alpha \in \mathbb{R}^n} \sum_{i=1}^n w_i \alpha_i \quad \text{subject to } Ax \leq b, \alpha \geq x \text{ and } \alpha \geq -x
\end{aligned}$$

With this proposition, the first part of the cost function can be rewritten. Note that the sizes of the vectors are $\tilde{V}_{\text{new}}(k) \in \mathbb{R}^{16N_p \times 1}$, $\tilde{H}(k) \in \mathbb{R}^{3N_p \times 1}$, $x(k) \in \mathbb{R}^{3 \times 1}$.

$$\begin{aligned}
& \min_{\tilde{V}_{\text{new}}(k)} W_1 |\tilde{V}_{\text{new}}(k)| \\
& \text{subject to} \\
& F_{1,new} \tilde{V}_{\text{new}}(k) \leq F_{2,new} + F_{3,new} x(k)
\end{aligned}$$

Equals:

$$\begin{aligned}
& \min_{\tilde{V}_{\text{new}}(k), \tilde{H}(k)} W_1 \tilde{H}(k) \\
& \text{subject to} \\
& F_{1,new} \tilde{V}_{\text{new}}(k) \leq F_{2,new} + F_{3,new} x(k) \\
& -\tilde{H}(k) \leq W_{2,new} \tilde{V}_{\text{new}}(k) \leq \tilde{H}(k)
\end{aligned}$$

For the final minimization problem, the constant term $W_3 M_3$ is omitted, as well as $S_2 x(k)$. The current states $x(k)$ do not appear in the cost function since it is a known value at time step k . Therefore, it is not an optimization variable. $x(k)$ does appear in the inequality constraints, since the constraints on the optimization variables depend on the current state. With the extra constraints added and the constant terms omitted, the final minimization problem becomes:

$$\begin{aligned}
 & \min_{\tilde{V}_{\text{new}}(k), \tilde{H}(k)} W_1 \tilde{H}(k) + S_1 \tilde{V}_{\text{new}}(k) \\
 & \text{subject to} \\
 & F_{1,\text{new}} \tilde{V}_{\text{new}}(k) \leq F_{2,\text{new}} + F_{3,\text{new}} x(k) \\
 & -\tilde{H}(k) \leq W_{2,\text{new}} \tilde{V}_{\text{new}}(k) \leq \tilde{H}(k)
 \end{aligned} \tag{109}$$

Result

For both of the batteries and the diesel generator, the following result is found for the optimal states:

	Battery 1	Battery 2		Diesel generator
$\hat{\delta}_b$ [-]	0	0	$\hat{\delta}_d$ [-]	$\begin{bmatrix} 0 & 0 & 0 & 0 \end{bmatrix}^T$
u_b [kW]	0	0	u_d [kW]	0
\hat{z}_b [kW]	1	0	\hat{z}_d [kW]	$\begin{bmatrix} 1 & 0 & 0 & 0 \end{bmatrix}^T$

All $\hat{\delta}$ are equal to zero, which means that both of the batteries are on operational mode discharging, and the diesel generator is on operational mode off. As a consequence, the exchanged power of the batteries is 0 kW and the generated power by the diesel generator is 0 kW as well. \hat{z} gives an odd result for battery 1 and for the diesel generator: both values contain a 1. Since z is defined as $u\delta$ and δ is 0 for both batteries and the diesel generator, z can never become 1. Therefore, it can be concluded that the optimization algorithm with the constraints and cost function as defined before, does not perform as it should.

Step 2.9

In this section, the closed-loop behaviour of the system is simulated using the receding horizon approach. This means that at each time step k the optimal MPC control input will be computed following the steps of section 2.8. The result of the MPC optimization procedure at time step k is the optimal vector as given by 72.

At the time instant k , the $\delta_{b,1}(k)$, $\delta_{b,2}(k)$, $\delta_d(k)$, $u_{b,1}(k)$, $u_{b,2}(k)$, $u_d(k)$ and $z_{b,1}(k)$, $z_{b,2}(k)$ and $z_d(k)$ from 72 will be implemented in the update equations for the batteries and diesel generator 53, 54 and 55. Hereafter, the optimal MPC control input is recalculated for the next time-step $k+1$ with the updated states $x_{b,1}$, $x_{b,2}$ and x_d in the optimization problem. This procedure can be repeated up until the desired time-step.

The results, plotted over 36 hours, are shown below in figures 6 and 7. States $x_{b,1}$ and $x_{b,2}$ only decrease with a small amount. State x_d decreases at first, and then switches between two values close to each other. This is not an optimal result. Furthermore, figure 7 shows no control input for all time steps. Thus, it can be concluded no optimal solution is found and that there is an issue with the code.

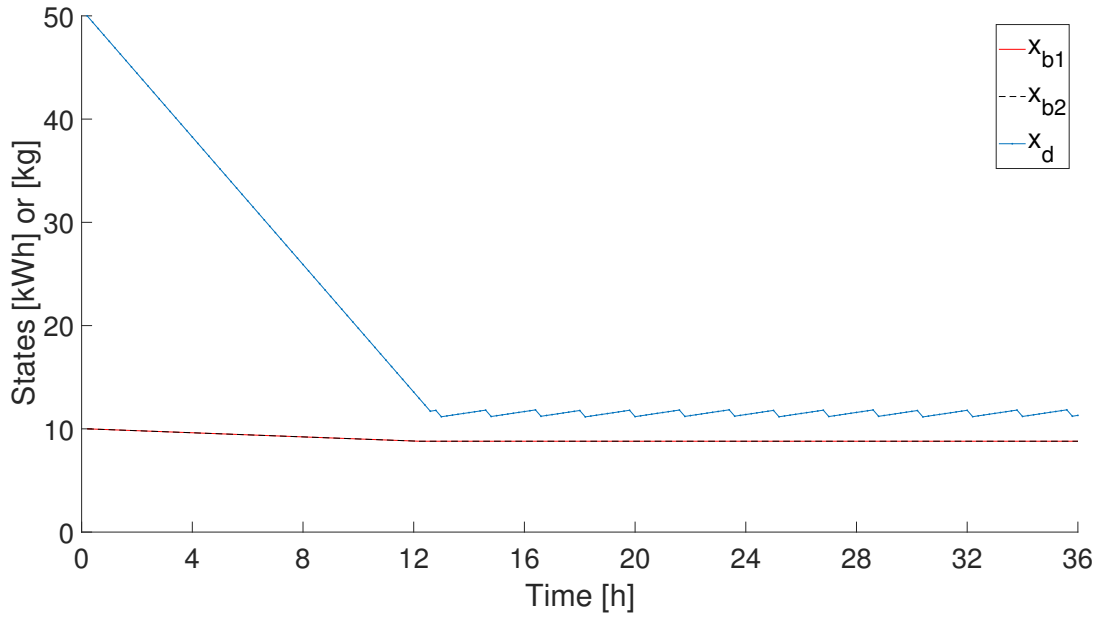


Figure 6: States $x_{b,1}$ [kWh] (red line) $x_{b,2}$ [kWh] (black striped line) and x_d [kg] (blue dotted line), plotted against time [h] for 36 hours

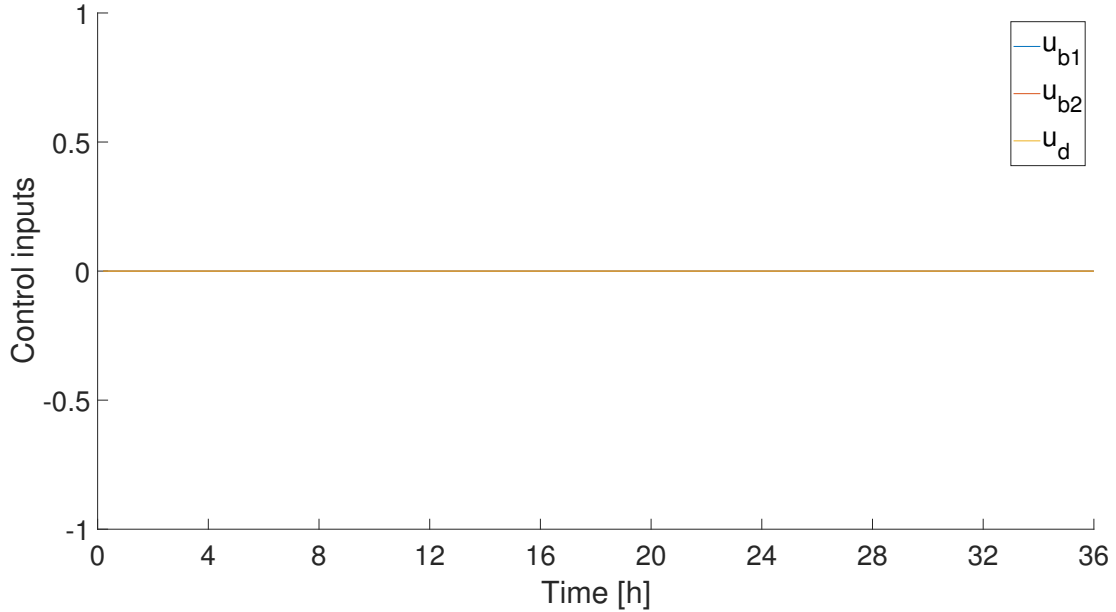


Figure 7: Control inputs $u_{b,1}, u_{b,2}, u_d$ [kW], plotted against time [h] for 36 hours

Step 2.10

The time step T_s is assumed to be 0.20 [h], as defined in step 2.7. Furthermore, it is assumed that at time step $x(1)$ the time is 0.20 hours after 12AM, and thus initial value x_0 starts at 12AM. There is a constraint added on the batteries every time it is either 12AM or 12PM. Therefore, for every $k = 60, 120, 180, \dots$, the constraint on $x_{b,1}$ and $x_{b,2}$ becomes as follows:

$$x_{b,i} \geq 0.2\bar{x}_{b,i} \longrightarrow -x_{b,i} \leq -0.2\bar{x}_{b,i} \quad (110)$$

Which equals the following additions to the constraint matrices:

$$E_1^{b,i,\text{addition}} = -1 \quad E_2^{b,i,\text{addition}} = 0 \quad E_3^{b,i,\text{addition}} = 0 \quad E_4^{b,i,\text{addition}} = 0 \quad g_5^{b,i,\text{addition}} = -0.2\bar{x}_d \quad (111)$$

The algorithm in MATLAB is the same as in 2.7, however, it is expanded with an if-loop such that whenever $k = 60, 120, 180, \dots$, the extra constraints are added.

MATLAB gives an infeasible result. Constraint 110 can never be met: $\bar{x}_{b,1} = 48$ and $\bar{x}_{b,2} = 64$, thus $0.2\bar{x}_{b,1} = 9.6$ and $0.2\bar{x}_{b,2} = 12.8$. Before time step $k = 60$ is reached, the states are already below these lower bounds, see figure 6. Therefore, MATLAB can not give a feasible result. For this reason, in Appendix ??, the piece of code that should be implemented for this exercise is commented out.

Conclusion

While working on this assignment, several skills were learned and insights obtained. Also, several aspects of the implementation could be done differently if this assignment would be done again. This will be briefly outlined below.

Insights

The first main insight is the way to use an optimizer for Mixed Integer Linear Programming (MILP) problems. For Systems & Control, optimization and minimization algorithms have been worked with before, in the course *Optimization in Systems and Control* for example. However, the optimizer *Gurobi* was never used, which works with MILP problems. Rewriting a PWA into a MILP problem required a new approach to setting up constraints and with this new approach, knowledge was gained. The fact that there were many constraints, made it an insightful job to set them up, check them, and check if there might be two constraints that are equal, such that only one of them is needed. Furthermore, the size of the matrices in the update equations, inequality constraints and weights in the cost function was extremely large due to the many constraints and the prediction horizon. Therefore, stacking of submatrices was needed. This required very precise definition of all matrices, both on paper as well as in MATLAB. A lot of consistency was needed when checking the values and variables in the matrices - finding a smart way to check the matrices on paper with the MATLAB matrices and checking the matrices on errors, was also informative.

Another main insight that was obtained during this assignment, is how to use binary variables in describing system dynamics. The description of system dynamics in the piecewise affine (PWA) form is quite straightforward, however, to rewrite the equations to the mixed logical dynamic (MLD) form, binary variables arise to be able to describe the switching between the system modes, where each mode exhibits different dynamical behaviour. Along with the binary variables, many constraints arise, to assign when the binary variables should be turned on or off. The rewriting of these constraints so that they can be used in a linear programming algorithm proved to be a fundamental point of the exercise.

The last main insight that will be highlighted is the size of the system description that was obtained during the assignment. The microgrid consists of only 3 subsystems; the diesel generator and the two batteries. In the full system description of the microgrid, as stated above, many large matrices were obtained. 11 matrices arise in the MLD update equations for the subsystems and 15 matrices arise in the MLD constraint equations. Furthermore, for the implementation in the optimization algorithm another 7 matrices emerged, each of which consisted of multiple matrices, of which the submatrices again are made up of the multiple MLD matrices. When the systems and matrices are described and noted clearly, everything stays comprehensible. However, many different hybrid system model types exist and it could be interesting to consider other hybrid system descriptions whenever the system includes more subsystems or the subsystems behave according to more complex switching patterns.

Discussion

The first time the MATLAB code ran for step 2.8, it gave infinite bounds and thus an infeasible solution. For a few days, multiple methods were tried and an attempt was made to find mistakes in either the code or in the stacking of the matrices. Now, the code does run, but the solution it gives is not a logical one. It is not clear what the issue is exactly. Although the attempts to solve the problem were very insightful, because mistakes were found, for a next time, it would be recommended to rewrite the code from the start instead of looking for mistakes. Also, the model formulation could be adjusted, such as defining vectors differently or adding extra constraints, such that the system might work.

Appendix

Exercise 2.3

```

1 %% SC4160 MODELLING AND CONTROL OF HYBRID SYSTEMS
2 % Step 2.3
3 % Jessie van Dam (4395832) and Miranda van Duijn (4355776)
4 clear all; close all; clc;
5
6 % Region 1
7 syms a1 b1 ud1
8 fun11 = (ud1^2 + 4 - a1 - b1*ud1).^2;
9 fun12 = (4*ud1 - a1 - b1*ud1).^2;
10 int11 = int(fun11,ud1,0,2);
11 int12 = int(fun12,ud1,2,5);
12 g1 = matlabFunction(int11+int12);
13
14 pdiff1a = diff(g1,a1);
15 pdiff1b = diff(g1,b1);
16
17 sol1 = solve(pdiff1a,pdiff1b);
18
19 parD.a1 = double(sol1.a1);
20 parD.b1 = double(sol1.b1);
21
22 % Region 2
23 syms a2 b2 ud2
24 fun2 = (-9.44*ud2^3 + 166.06*ud2^2 -948.22*ud2 + 1790.28 - a2 - b2*ud2).^2;
25 int2 = int(fun2,ud2,5,6.5);
26 g2 = matlabFunction(int2);
27
28 pdiff2a = diff(g2,a2);
29 pdiff2b = diff(g2,b2);
30
31 sol2 = solve(pdiff2a,pdiff2b);
32
33 parD.a2 = double(sol2.a2);
34 parD.b2 = double(sol2.b2);
35
36 % Region 3
37 syms a3 b3 ud3
38 fun31 = (-9.44*ud3^3 + 166.06*ud3^2 -948.22*ud3 + 1790.28 - a3 - b3*ud3).^2;
39 fun32 = (-11.78*ud3 + 132.44 - a3 - b3*ud3).^2;
40 fun33 = (4.01*(ud3-10.47).^2 + 17.79 - a3 - b3*ud3).^2;
41 int31 = int(fun31,ud3,6.5,7);
42 int32 = int(fun32,ud3,7,9);
43 int33 = int(fun33,ud3,9,11);
44 g3 = matlabFunction(int31 + int32 + int33);
45
46 pdiff3a = diff(g3,a3);
47 pdiff3b = diff(g3,b3);
48
49 sol3 = solve(pdiff3a,pdiff3b);
50
51 parD.a3 = double(sol3.a3);
52 parD.b3 = double(sol3.b3);
53
54 % Region 4
55 syms a4 b4 ud4
56 fun4 = (4.01 * (ud4-10.47).^2 + 17.79 - a4 - b4*ud4).^2;
57 int4 = int(fun4,ud4,11,15);
58 g4 = matlabFunction(int4);
59
60 pdiff4a = diff(g4,a4);
61 pdiff4b = diff(g4,b4);
62
63 sol4 = solve(pdiff4a,pdiff4b);
64
65 parD.a4 = double(sol4.a4);
66 parD.b4 = double(sol4.b4);
67

```

```

68 save('parD.mat','parD');
69
70 %% Plot real function together with approximation
71 % real function
72 step = 0.01;
73 ud = 0:step:15;
74
75 for i = 1:length(ud);
76     if i < round(2/step)
77         funreal(i) = ud(i)^2+4;
78     elseif i < round(5/step)
79         funreal(i) = 4*ud(i);
80     elseif i < round(7/step)
81         funreal(i) = -9.44*ud(i)^3+166.06*ud(i)^2-948.22*ud(i)+1790.28;
82     elseif i ≤ round(9/step)
83         funreal(i) = -11.78*ud(i) + 132.44;
84     elseif i > round(9/step)
85         funreal(i) = 4.01*(ud(i)-10.47)^2+17.79;
86     end
87 end
88
89 % approximate function
90 for i = 1:length(ud);
91     if i < round(5/step)
92         funapprox(i) = parD.a1+parD.b1*ud(i);
93     elseif i < round(6.5/step)
94         funapprox(i) = parD.a2+parD.b2*ud(i);
95     elseif i ≤ round(11/step)
96         funapprox(i) = parD.a3+parD.b3*ud(i);
97     elseif i > round(11/step)
98         funapprox(i) = parD.a4+parD.b4*ud(i);
99     end
100 end
101
102 figure;
103 hold on; grid on;
104 plot(ud,funreal);
105 plot(ud,funapprox);
106 xlabel('generated power u_d [kW]');
107 ylabel('consumed fuel of diesel generator [kg/h]');
108 legend('real fuel consumption', 'approximated fuel consumption');
109
110 % compute RMSE
111 rmse = rms(funreal-funapprox);

```

Exercise 2.4

```

1 %% SC4160 MODELLING AND CONTROL OF HYBRID SYSTEMS
2 % Step 2.4
3 % Jessie van Dam (4395832) and Miranda van Duijn (4355776)
4 clear all; close all; clc;
5 load('parD.mat');
6
7 % creating constraints
8 A = [0 0 0 0 0 0 0 0 0 0 0 1
9       0 0 0 0 0 0 0 0 0 1 -1 0
10      0 0 0 0 0 0 0 0 0 0 1 -1
11      0 0 0 0 0 0 0 0 -1 0 0 0];
12
13 b = [15; 0; 0; 0];
14
15 % minimizing integral for several initial values
16 % input vector x = [a1; a2; a3; a4; b1; b2; b3; b4; u1; u2; u3]
17 x = zeros(20,11);
18 x0 = zeros(1,11);
19 for i = 1:21
20     x0 = [parD.a1+(i-11) parD.a2+(i-11) parD.a3+(i-11) parD.a4+(i-11) parD.b1+(i-11) ...
21           parD.b2+(i-11) parD.b3+(i-11) parD.b4+(i-11) ...
22           4+((i-11)/10) 6.5+((i-11)/10) 11+((i-11)/10)];
23     x(i,:) = fmincon(@PWAapprox,x0,A,b);

```

```

23     fun_int(i) = PWAapprox(x(i,:));
24 end
25
26 fun_min = find(fun_int == min(fun_int(:)));
27 x_min = x(fun_min,:);
28
29 %% Plot real function together with approximation
30 % real function
31 step = 0.01;
32 ud = 0:step:15;
33
34 for i = 1:length(ud);
35     if i ≤ round(2/step)
36         funreal(i) = ud(i)^2+4;
37     elseif i ≤ round(5/step)
38         funreal(i) = 4*ud(i);
39     elseif i ≤ round(7/step)
40         funreal(i) = -9.44*ud(i)^3+166.06*ud(i)^2-948.22*ud(i)+1790.28;
41     elseif i ≤ round(9/step)
42         funreal(i) = -11.78*ud(i) + 132.44;
43     elseif i > round(9/step)
44         funreal(i) = 4.01*(ud(i)-10.47)^2+17.79;
45     end
46 end
47
48 % approximate function
49 for i = 1:length(ud);
50     if i ≤ round(x_min(9)/step)
51         funapprox(i) = x_min(1)+x_min(5)*ud(i);
52     elseif i ≤ round(x_min(10)/step)
53         funapprox(i) = x_min(2)+x_min(6)*ud(i);
54     elseif i ≤ round(x_min(11)/step)
55         funapprox(i) = x_min(3)+x_min(7)*ud(i);
56     elseif i > round(x_min(11)/step)
57         funapprox(i) = x_min(4)+x_min(8)*ud(i);
58     end
59 end
60
61 figure;
62 hold on; grid on;
63 plot(ud,funreal);
64 plot(ud,funapprox);
65 xlabel('generated power u_d [kW]');
66 ylabel('consumed fuel of diesel generator [kg/h]');
67 legend('real fuel consumption', 'approximated fuel consumption');
68
69 % compute RMSE
70 rmse = rms(funreal-funapprox);

```

Exercise 2.7

```

1 %% SC4160 MODELLING AND CONTROL OF HYBRID SYSTEMS
2 % Step 2.7
3 % Jessie van Dam (4395832) and Miranda van Duijn (4355776)
4 clear all; close all; clc;
5 addpath C:\Users\Miranda\hysdel-2.0.6-MINGW32_NT-5.1-i686
6 addpath(genpath('C:\Documenten\TU Delft\MSc Systems and Control\Q4\Modelling and Control of ...
    Hybrid Systems\Project\Modelling_and_Control_of_Hybrid_Systems'))
7
8 % Define parameters
9 parB.eta_c = [0.9 0.95];
10 parB.eta_d = [0.8 0.77];
11 parB.x_up = [48 64];
12 parB.u_low = [-3 -4];
13 parB.u_up = [2 3];
14 parB.A = 1;
15 parB.x0 = 10;
16
17 save('parB.mat', 'parB')
18

```

```

19 %%
20 load parD.mat
21 parD.x_low = 10;
22 parD.x_up = 120;
23 parD.u_up = 15;
24 parD.u_low = 0;
25 parD.Rf = 0.4;
26 parD.x0 = 50;
27
28 parD.u1 = 5;
29 parD.u2 = 6.5;
30 parD.u3 = 11;
31
32 save('parD.mat', 'parD')
33
34 %%
35 dim.Ts = 0.20; % in [h]
36 dim.t = 10;
37 dim.Np = 25; % prediction horizon
38 dim.Nc = 25; % control horizon
39 dim.Wb1 = 3; % weight in cost function battery 1
40 dim.Wb2 = 4; % weight in cost function battery 2
41 dim.Wd = 10; % weight in cost function diesel generator
42 dim.Wfuel = 4; % weight in cost function fuel
43 dim.We = 0.4; % weight in cost function e?
44
45 save('dim.mat', 'dim')
46
47 %% Defining battery with matrices
48 % Defining MLD matrices battery 1
49 MLDB1.A = 1;
50 MLDB1.B1 = -dim.Ts*parB.eta_d(1);
51 MLDB1.B2 = 0;
52 MLDB1.B3 = dim.Ts*(parB.eta_d(1)-parB.eta_c(1));
53 MLDB1.B4 = 0;
54
55 MLDB1.E1 = [0; 0; 0; 0; -1; 1; 0; 0; 0; 0]; % E1 matrix battery 1
56 MLDB1.E2 = [1; -1; 1; -1; 0; 0; 0; 0; -1; 1]; % E2 matrix battery 1
57 MLDB1.E3 = [0; 0; parB.u_up(1); parB.u_low(1)-eps; 0; 0; -parB.u_up(1); parB.u_low(1); ...
    -parB.u_low(1); parB.u_up(1)]; % E3 matrix battery 1
58 MLDB1.E4 = [0; 0; 0; 0; 0; 0; 1; -1; 1; -1]; % E4 matrix battery 1
59 MLDB1.g5 = [parB.u_up(1); -parB.u_low(1); parB.u_up(1); -eps; 0; parB.x_up(1); 0; 0; ...
    -parB.u_low(1); parB.u_up(1)]; % g5 matrix battery 1
60
61 save('MLDB1.mat', 'MLDB1')
62
63 % Defining MLD matrices battery 2
64 MLDB2.A = 1;
65 MLDB2.B1 = -dim.Ts*parB.eta_c(1);
66 MLDB2.B2 = 0;
67 MLDB2.B3 = dim.Ts*(parB.eta_d(1)-parB.eta_c(1));
68 MLDB2.B4 = 0;
69
70 MLDB2.E1 = [0; 0; 0; 0; -1; 1; 0; 0; 0; 0]; % E1 matrix battery 2
71 MLDB2.E2 = [1; -1; 1; -1; 0; 0; 0; 0; -1; 1]; % E2 matrix battery 2
72 MLDB2.E3 = [0; 0; parB.u_up(2); parB.u_low(2)-eps; 0; 0; -parB.u_up(2); parB.u_low(2); ...
    -parB.u_low(2); parB.u_up(2)]; % E3 matrix battery 2
73 MLDB2.E4 = [0; 0; 0; 0; 0; 0; 1; -1; 1; -1]; % E4 matrix battery 2
74 MLDB2.g5 = [parB.u_up(2); -parB.u_low(2); parB.u_up(2); -eps; 0; parB.x_up(2); 0; 0; ...
    -parB.u_low(2); parB.u_up(2)]; % g5 matrix battery 2
75
76 save('MLDB2.mat', 'MLDB2')
77
78 %% Defining MLD system diesel generator Jordan
79 MLDD.A = 1;
80 MLDD.B1 = zeros(1,1);
81 MLDD.B2 = dim.Ts*[-parD.a1 -parD.a2 -parD.a3 -parD.a4];
82 MLDD.B3 = dim.Ts*[-parD.b1 -parD.b2 -parD.b3 -parD.b4];
83 MLDD.B4 = dim.Ts*parD.Rf;
84
85 % Constraint matrices diesel generator
86 MLDD.E1 = [0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0];
87 MLDD.E2 = [1 -1 0 0 0 0 -1 1 -1 1 0 0 -1 1 -1 1 0 0 -1 1 -1 1 1];

```



```

88 MLDD.E3 = [0 0 1 0 0 -parD.u_up parD.u_low -parD.u_low parD.u_up eps -(parD.u1-eps)+parD.u_up ...
            0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0;
89            0 0 1 0 0 0 0 0 0 0 0 -parD.u_up parD.u_low -parD.u_low parD.u_up parD.u1 ...
            -(parD.u2-eps)+parD.u_up 0 0 0 0 0 0 0 0 0 0 0;
90            0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 -parD.u_up parD.u_low -parD.u2 parD.u3 parD.u2 ...
            -(parD.u3-eps)+parD.u_up 0 0 0 0 0 0;
91            0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -parD.u_up parD.u_low -parD.u_low ...
            parD.u_up parD.u3 -parD.u_up]';
92 MLDD.E4 = [0 0 0 0 0 1 -1 1 -1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0;
93            0 0 0 0 0 0 0 0 0 0 0 0 1 -1 1 -1 0 0 0 0 0 0 0 0 0 0;
94            0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 -1 1 -1 0 0 0 0 0 0;
95            0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 -1 1 -1 0 0]';
96 MLDD.g5 = [parD.u_up; eps; 1; -parD.x_low; parD.x_up; 0; 0; -parD.u_low; parD.u_up; 0; ...
            parD.u_up; 0; 0; -parD.u_low; parD.u_up; 0; ...
97            parD.u_up; 0; 0; -parD.u_low; parD.u_up; 0; parD.u_up; 0; 0; -parD.u_low; ...
            parD.u_up; 0; 0];
98
99 save('MLDD.mat', 'MLDD')

```

Exercise 2.8 & 2.9 & 2.10

```

1 %% SC4160 MODELLING AND CONTROL OF HYBRID SYSTEMS
2 % Step 2.8 2.9 and 2.10
3 % Jessie van Dam (4395832) and Miranda van Duijn (4355776)
4 clear all; close all; clc;
5 addpath(genpath('C:\Documenten\TU Delft\MSc Systems and Control\Q4\Modelling and Control of ...
    Hybrid Systems\Project\Modelling_and_Control_of_Hybrid_Systems'));
6 addpath c:\gurobi811\win64\matlab\
7
8 %% Loading and defining parameters and data
9 load dim.mat; load MLDB1.mat; load MLDB2.mat; load MLDD.mat; load parB.mat; load parD.mat;
10 load M1.mat; load M2.mat; load M3.mat; load F1.mat; load F2.mat; load F3.mat;
11 load W1.mat; load W2.mat; load W3.mat; load W4.mat; load W5.mat; load S1.mat; load S2.mat;
12 load Ce.mat;
13
14 parB.x0 = 10;
15 parD.x0 = 50;
16 dim.Tend = 180; % Number of timesteps to optimize for
17
18 xb1 = zeros(1,dim.Tend);
19 xb2 = zeros(1,dim.Tend);
20 xd = zeros(1,dim.Tend);
21 xb1(1) = parB.x0;
22 xb2(1) = parB.x0;
23 xd(1) = parD.x0;
24 x = [xb1; xb2; xd];
25 x(:,1) = [xb1(1); xb2(1); xd(1)];
26
27 %% Defining Pload
28 for k = 1:dim.Tend
29     if k ≤ 20
30         Pload(k) = 0;
31     elseif k ≥ 21 && k ≤ 50
32         Pload(k) = 30+2*k;
33     elseif k ≥ 51
34         Pload(k) = 45;
35     end
36 end
37
38 %%
39 % Constructing matrices when it's not 12AM 12PM
40 [W1,W2,W3,F1,F2,F3,S1,S2] = constructMatrices(dim,parB,parD,MLDB1,MLDB2,MLDD,Pload,Ce);
41
42 % Constructing matrices when it's 12AM 12PM
43 MLDB1noon = MLDB1;
44 MLDB2noon = MLDB2;
45
46 MLDB1noon.E1 = [MLDB1.E1; -1];
47 MLDB1noon.E2 = [MLDB1.E2; 0];
48 MLDB1noon.E3 = [MLDB1.E3; 0];

```

```

49 MLDB1noon.E4 = [MLDB1.E4; 0];
50 MLDB1noon.g5 = [MLDB1.g5; -0.2*parB.x_up(1,1)];
51
52 MLDB2noon.E1 = [MLDB1.E1; -1];
53 MLDB2noon.E2 = [MLDB1.E2; 0];
54 MLDB2noon.E3 = [MLDB1.E3; 0];
55 MLDB2noon.E4 = [MLDB1.E4; 0];
56 MLDB2noon.g5 = [MLDB1.g5; -0.2*parB.x_up(1,2)];
57
58 [W1noon,W2noon,W3noon,F1noon,F2noon,F3noon,S1noon,S2noon] = ...
    constructMatrices(dim,parB,parD,MLDB1noon,MLDB2noon,MLDD,Fload,Ce);
59
60
61 %% Simulating closed-loop behaviour of the system
62
63 for k = 1:dim.Tend
64
65     if k == 60 | k == 120
66         k
67         % Minimize
68         %     W1 H + S1new Vnew
69         % Subject to
70         %     F1new Vnew ≤ F2new + F3new*x(k)
71         %     -H - W2new Vnew ≤ 0
72         %     -H + W2new Vnew ≤ 0
73
74         % names = {'H'; 'V'};
75
76         % Cost function to minimize
77         model.obj = [W1noon.W1 S1noon.S1new];
78         model.modelsense = 'min';
79         model.vtype = [repmat('C',3*dim.Np,1); ...
80             repmat('B',dim.Np,1); repmat('C',dim.Np,1); ...
repmat('S',dim.Np,1); repmat('B',dim.Np,1); repmat('C',dim.Np,1); ...
81             repmat('S',dim.Np,1); repmat('B',4*dim.Np,1); ...
repmat('C',dim.Np,1); repmat('S',4*dim.Np,1); repmat('C',dim.Np,1)];
82
83         % Constraints
84         model.A = sparse([zeros(size(F1noon.F1new,1),size(W1noon.W1,2)) F1noon.F1new; ...
85             -eye(size(W2noon.W2new,1)) -W2noon.W2new; ...
86             -eye(size(W2noon.W2new,1)) W2noon.W2new ]);
87         model.rhs = [F2noon.F2new+F3noon.F3new*x(:,k); zeros(size(W2noon.W2new,1),1); ...
zeros(size(W2noon.W2new,1),1)];
88         model.sense = repmat('<',size(F2noon.F2new,1)+2*size(W2noon.W2new,1),1);
89
90         % Gurobi Solve
91         gurobi_write(model, 'mip1.lp');
92         params.outputflag = 0;
93         result = gurobi(model, params);
94         disp(result);
95
96     elseif ~(k == 60*i) % if it is not 12AM or 12PM
97         % Minimize
98         %     W1 H + S1new Vnew
99         % Subject to
100        %     F1new Vnew ≤ F2new + F3new*x(k)
101        %     -H - W2new Vnew ≤ 0
102        %     -H + W2new Vnew ≤ 0
103
104        % names = {'H'; 'V'};
105
106        % Cost function to minimize
107        model.obj = [W1.W1 S1.S1new];
108        model.modelsense = 'min';
109        model.vtype = [repmat('C',3*dim.Np,1); ...
110            repmat('B',dim.Np,1); repmat('C',dim.Np,1); repmat('S',dim.Np,1); ...
repmat('B',dim.Np,1); repmat('C',dim.Np,1); ...
111            repmat('S',dim.Np,1); repmat('B',4*dim.Np,1); ...
repmat('C',dim.Np,1); repmat('S',4*dim.Np,1); ...
repmat('C',dim.Np,1)];
112
113        % Constraints
114        model.A = sparse([zeros(size(F1.F1new,1),size(W1.W1,2)) F1.F1new; ...

```

```

115             -eye(size(W2.W2new,1)) -W2.W2new; ...
116             -eye(size(W2.W2new,1)) W2.W2new ]);
117     model.rhs = [F2.F2new+F3.F3new*x(:,k); zeros(size(W2.W2new,1),1); ...
118                 zeros(size(W2.W2new,1),1)];
119     model.sense = repmat('<',size(F2.F2new,1)+2*size(W2.W2new,1),1);
120
121     % Gurobi Solve
122     gurobi_write(model, 'mip1.lp');
123     params.outputflag = 0;
124     result = gurobi(model, params);
125     disp(result);
126
127     % Optimized vector
128     x_opti(:,k) = result.x;
129
130     % Cost function at time step k
131     J(k) = result.objval + S2.S2*x(:,k) + W3.W3*M3.M3;
132
133     % Update equation
134     xb1(:,k+1) = MLDB1.A*xb1(:,k) + MLDB1.B1*result.x(dim.Np+1) + ...
135                 MLDB1.B3*result.x(2*dim.Np+1);
136     xb2(:,k+1) = MLDB2.A*xb2(:,k) + MLDB2.B1*result.x(dim.Np+1) + ...
137                 MLDB2.B3*result.x(2*dim.Np+1);
138     xd(:,k+1) = MLDD.A*xd(:,k) + MLDD.B2*result.x(6*dim.Np+1:6*dim.Np+4) + ...
139                 MLDD.B3*result.x(11*dim.Np+1:11*dim.Np+4) + MLDD.B4;
140
141     x(:,k+1) = [xb1(:,k+1);
142                 xb2(:,k+1);
143                 xd(:,k+1)];
144
145 %     end
146
147 end
148
149 %%
150 close all;
151
152 figure; hold on;
153 plot(xb1(1,:), 'r')
154 plot(xb2(1,:), '—k')
155 plot(xd(1,:), '—')
156 xticks([0 20 40 60 80 100 120 140 160 180])
157 xticklabels({'0','4','8','12','16','20','24','28','32','36'})
158 xlim([0 180])
159 xlabel('Time [h]'); ylabel('States [kWh] or [kg]')
160 set(gca, 'FontSize', 31)
161 lgd = legend('x_{b1}', 'x_{b2}', 'x_d')
162 lgd.FontSize = 31;
163 hold off;
164
165 figure; hold on;
166 plot(x_opti(dim.Np+1,:));
167 plot(x_opti(4*dim.Np+1,:));
168 plot(x_opti(10*dim.Np+1,:));
169 xticks([0 20 40 60 80 100 120 140 160 180])
170 xticklabels({'0','4','8','12','16','20','24','28','32','36'})
171 xlim([0 180])
172 xlabel('Time [h]'); ylabel('Control inputs')
173 set(gca, 'FontSize', 31)
174 lgd = legend('u_{b1}', 'u_{b2}', 'u_d')
175 lgd.FontSize = 31;
176 hold off;
177
178 %%
179 x_optimal = [x_opti(1,1); x_opti(dim.Np+1,1); x_opti(2*dim.Np+1,1)
180             x_opti(3*dim.Np+1,1); x_opti(4*dim.Np+1,1); x_opti(5*dim.Np+1,1)
181             x_opti(6*dim.Np+1:6*dim.Np+4,1); x_opti(10*dim.Np+1,1); ...
182             x_opti(11*dim.Np+1:11*dim.Np+4,1)];

```

Function for optimization matrices

```

1 function [ W1,W2,W3,F1,F2,F3,S1,S2 ] = constructMatrices( ...
    dim,parB,parD,MLDB1,MLDB2,MLDD,Pload,Ce)
2 %constructMatrices Summary of this function goes here
3 % Detailed explanation goes here
4
5 % Constructing M matrices for update equation MILP
6 % M1.M1 matrix for the diesel generator
7 M1.M1_d_Δ = zeros(dim.Np*size(MLDD.A,1),dim.Np*size(MLDD.B2,2));
8 M1.M1_d_u = zeros(dim.Np,dim.Np);
9 M1.M1_d_zd = zeros(dim.Np*size(MLDD.A,1),dim.Np*size(MLDD.B3,2));
10
11 for np1 = 1:dim.Np % over columns
12     for np2 = 1:dim.Np % over rows
13         M1.M1_d_Δ(1+(np2-1)*size(MLDD.A,1),1+(np1-1)*size(MLDD.B2,2):np1*size(MLDD.B2,2)) = ...
            MLDD.A^(np2-1)*MLDD.B2;
14         M1.M1_d_u(1+(np2-1)*size(MLDD.A,1),1+(np1-1):np1*size(MLDD.B1,2)) ...
            = MLDD.A^(np2-1)*MLDD.B1;
15         M1.M1_d_zd(1+(np2-1)*size(MLDD.A,1),1+(np1-1)*size(MLDD.B3,2):np1*size(MLDD.B3,2)) ...
            = MLDD.A^(np2-1)*MLDD.B3;
16     end
17 end
18 clear np1
19
20 for i = 1:dim.Np
21     for j = 1:4*dim.Np
22         if j > 4*i
23             M1.M1_d_Δ(i,j) = 0;
24             M1.M1_d_zd(i,j) = 0;
25         end
26     end
27 end
28 clear i j
29
30 M1.M1_d = [M1.M1_d_Δ M1.M1_d_u M1.M1_d_zd];
31
32 % M1.M1 matrix for the batteries
33 M1.M1_b1_Δ = zeros(dim.Np,dim.Np);
34 M1.M1_b1_u = zeros(dim.Np,dim.Np);
35 M1.M1_b1_zd = zeros(dim.Np,dim.Np);
36 M1.M1_b1 = zeros(dim.Np,3*dim.Np);
37
38 M1.M1_b2_Δ = zeros(dim.Np,dim.Np);
39 M1.M1_b2_u = zeros(dim.Np,dim.Np);
40 M1.M1_b2_zd = zeros(dim.Np,dim.Np);
41 M1.M1_b2 = zeros(dim.Np,3*dim.Np);
42
43 for np1 = 1:dim.Np % over columns
44     for np2 = 1:dim.Np % over rows
45         M1.M1_b1_Δ(1+(np2-1)*size(MLDB1.A,1),1+(np1-1)*size(MLDB1.B2,2):np1*size(MLDB1.B2,2)) ...
            = MLDB1.A^(np2-1)*MLDB1.B2;
46         M1.M1_b1_u(1+(np2-1)*size(MLDB1.A,1),1+(np1-1)*size(MLDB1.B3,2):np1*size(MLDB1.B3,2)) ...
            = MLDB1.A^(np2-1)*MLDB1.B1;
47         M1.M1_b1_zd(1+(np2-1)*size(MLDB1.A,1),1+(np1-1)*size(MLDB1.B1,2):np1*size(MLDB1.B1,2)) ...
            = MLDB1.A^(np2-1)*MLDB1.B3;
48
49         M1.M1_b2_Δ(1+(np2-1)*size(MLDB2.A,1),1+(np1-1)*size(MLDB2.B2,2):np1*size(MLDB2.B2,2)) ...
            = MLDB2.A^(np2-1)*MLDB2.B2;
50         M1.M1_b2_u(1+(np2-1)*size(MLDB2.A,1),1+(np1-1)*size(MLDB2.B3,2):np1*size(MLDB2.B3,2)) ...
            = MLDB2.A^(np2-1)*MLDB2.B1;
51         M1.M1_b2_zd(1+(np2-1)*size(MLDB2.A,1),1+(np1-1)*size(MLDB2.B1,2):np1*size(MLDB2.B1,2)) ...
            = MLDB2.A^(np2-1)*MLDB2.B3;
52     end
53 end
54 clear np1 np2
55
56 for i = 1:dim.Np
57     for j = 1:dim.Np
58         if j > i
59             M1.M1_b1_Δ(i,j) = 0;
60             M1.M1_b1_u(i,j) = 0;
61             M1.M1_b1_zd(i,j) = 0;
62
63             M1.M1_b2_Δ(i,j) = 0;

```

```

64         M1.M1_b2_u(i,j)      = 0;
65         M1.M1_b2_zd(i,j)      = 0;
66     end
67 end
68 end
69 clear i j
70
71 M1.M1_b1 = [M1.M1_b1_Δ M1.M1_b1_u M1.M1_b1_zd];
72 M1.M1_b2 = [M1.M1_b2_Δ M1.M1_b2_u M1.M1_b2_zd];
73
74 % Total M1.M1 matrix
75 M1.M1 = [M1.M1_b1 zeros(dim.Np,size(M1.M1_b2,2)) zeros(dim.Np,size(M1.M1_d,2)); ...
          zeros(dim.Np,size(M1.M1_b1,2)) M1.M1_b2 zeros(dim.Np,size(M1.M1_d,2)); ...
          zeros(dim.Np,size(M1.M1_b1,2)) zeros(dim.Np,size(M1.M1_b2,2)) M1.M1_d];
76
77 % M2.M2 matrix
78 M2.M2_b1 = zeros(dim.Np,size(MLDB1.A,2));
79 M2.M2_b2 = zeros(dim.Np,size(MLDB2.A,2));
80 M2.M2_d  = zeros(dim.Np,size(MLDD.A,2));
81
82 for np = 1:dim.Np
83     M2.M2_b1(np,:) = (MLDB1.A)^np;
84     M2.M2_b2(np,:) = (MLDB2.A)^np;
85     M2.M2_d(np,:)  = (MLDD.A)^np;
86 end
87 clear np
88
89 M2.M2 = [M2.M2_b1 zeros(size(M2.M2_b1,1),size(M2.M2_b2,2)) ...
          zeros(size(M2.M2_b1,1),size(M2.M2_d,2)); ...
          zeros(size(M2.M2_b2,1),size(M2.M2_b1,2)) M2.M2_b2 ...
          zeros(size(M2.M2_b2,1),size(M2.M2_d,2)); ...
          zeros(size(M2.M2_d,1),size(M2.M2_b1,2)) zeros(size(M2.M2_d,1),size(M2.M2_b2,2)) ...
          M2.M2_d];
90
91
92
93 % M3.M3 matrix
94 M3.M3_b1 = zeros(dim.Np*size(MLDD.B4,1),size(MLDD.B4,2));
95 M3.M3_b2 = zeros(dim.Np*size(MLDD.B4,1),size(MLDD.B4,2));
96 M3.M3_d  = zeros(dim.Np*size(MLDD.B4,1),size(MLDD.B4,2));
97
98 for nd = 1:dim.Np
99     if nd == 1
100         M3.M3_d(1,1) = MLDD.B4;
101     end
102
103     if nd > 1
104         M3.M3_d(1+(nd-1)*size(MLDD.B4,1):nd*size(MLDD.B4,1),1:size(MLDD.B4,2)) = ...
            M3.M3_d(nd-1,:) + MLDD.B4*(MLDD.A)^(nd-1);
105     end
106 end
107 clear nd
108
109 % Concatenating submatrices into complete M3.M3 matrix
110 M3.M3 = [M3.M3_b1; M3.M3_b2; M3.M3_d];
111
112 % Constructing F1.F1 matrix for MILP constraint equation
113 F1.F1b1_Δ = zeros(dim.Np*size(MLDB1.E3,1),dim.Np*size(MLDB1.E3,2));
114 F1.F1b1_u = zeros(dim.Np*size(MLDB1.E2,1),dim.Np*size(MLDB1.E2,2));
115 F1.F1b1_zd = zeros(dim.Np*size(MLDB1.E4,1),dim.Np*size(MLDB1.E4,2));
116
117 F1.F1b2_Δ = zeros(dim.Np*size(MLDB2.E3,1),dim.Np*size(MLDB2.E3,2));
118 F1.F1b2_u = zeros(dim.Np*size(MLDB2.E2,1),dim.Np*size(MLDB2.E2,2));
119 F1.F1b2_zd = zeros(dim.Np*size(MLDB2.E4,1),dim.Np*size(MLDB2.E4,2));
120
121 F1.F1d_Δ = zeros(dim.Np*size(MLDD.E3,1),dim.Np*size(MLDD.E3,2));
122 F1.F1d_u = zeros(dim.Np*size(MLDD.E2,1),dim.Np*size(MLDD.E2,2));
123 F1.F1d_zd = zeros(dim.Np*size(MLDD.E3,1),dim.Np*size(MLDD.E4,2));
124
125 for np1 = 1:dim.Np % over columns
126     for np2 = 1:dim.Np % over rows
127         if np1 == np2
128             % For battery 1
129             F1.F1b1_Δ(1+(np2-1)*size(MLDB1.E3,1):np2*size(MLDB1.E3,1), ...
130                 1+(np1-1)*size(MLDB1.E3,2):np1*size(MLDB1.E3,2)) = MLDB1.E3;

```

```

131         F1.F1b1_u(1+(np2-1)*size(MLDB1.E2,1):np2*size(MLDB1.E2,1),...
132             1+(np1-1)*size(MLDB1.E2,2):np1*size(MLDB1.E2,2)) = MLDB1.E2;
133         F1.F1b1_zd(1+(np2-1)*size(MLDB1.E4,1):np2*size(MLDB1.E4,1),...
134             1+(np1-1)*size(MLDB1.E4,2):np1*size(MLDB1.E4,2)) = MLDB1.E4;
135
136         % For battery 2
137         F1.F1b2_u(1+(np2-1)*size(MLDB2.E3,1):np2*size(MLDB2.E3,1),...
138             1+(np1-1)*size(MLDB2.E3,2):np1*size(MLDB2.E3,2)) = MLDB2.E3;
139         F1.F1b2_u(1+(np2-1)*size(MLDB2.E2,1):np2*size(MLDB2.E2,1),...
140             1+(np1-1)*size(MLDB2.E2,2):np1*size(MLDB2.E2,2)) = MLDB2.E2;
141         F1.F1b2_zd(1+(np2-1)*size(MLDB2.E4,1):np2*size(MLDB2.E4,1),...
142             1+(np1-1)*size(MLDB2.E4,2):np1*size(MLDB2.E4,2)) = MLDB2.E4;
143
144         % For the diesel generator
145         F1.F1d_u(1+(np2-1)*size(MLDD.E3,1):np2*size(MLDD.E3,1),...
146             1+(np1-1)*size(MLDD.E3,2):np1*size(MLDD.E3,2)) = MLDD.E3;
147         F1.F1d_u(1+(np2-1)*size(MLDD.E2,1):np2*size(MLDD.E2,1),...
148             1+(np1-1)*size(MLDD.E2,2):np1*size(MLDD.E2,2)) = MLDD.E2;
149         F1.F1d_zd(1+(np2-1)*size(MLDD.E4,1):np2*size(MLDD.E4,1),...
150             1+(np1-1)*size(MLDD.E4,2):np1*size(MLDD.E4,2)) = MLDD.E4;
151     end
152
153     if np2 > np1 % to fill only below the block diagonal
154         % NOTE: algemener maken voor F1.F1_bi_u?
155         % For battery 1
156         F1.F1b1_u(1+(np2-1)*size(MLDB1.E2,1):np2*size(MLDB1.E2,1),...
157             1+(np1-1)*size(MLDB1.E2,2):np1*size(MLDB1.E2,2)) = ...
158             MLDB1.E1*MLDB1.A^(np2-2)*MLDB1.B1;
159         F1.F1b1_zd(1+(np2-1)*size(MLDB1.E4,1):np2*size(MLDB1.E4,1),...
160             1+(np1-1)*size(MLDB1.E4,2):np1*size(MLDB1.E4,2)) = ...
161             MLDB1.E1*MLDB1.A^(np2-2)*MLDB1.B3;
162
163         % For battery 2
164         F1.F1b2_u(1+(np2-1)*size(MLDB2.E2,1):np2*size(MLDB2.E2,1),...
165             1+(np1-1)*size(MLDB2.E2,2):np1*size(MLDB2.E2,2)) = ...
166             MLDB2.E1*MLDB2.A^(np2-2)*MLDB2.B1;
167         F1.F1b2_zd(1+(np2-1)*size(MLDB2.E4,1):np2*size(MLDB2.E4,1),...
168             1+(np1-1)*size(MLDB2.E4,2):np1*size(MLDB2.E4,2)) = ...
169             MLDB2.E1*MLDB2.A^(np2-2)*MLDB2.B3;
170
171         % For the diesel generator
172         F1.F1d_u(1+(np2-1)*size(MLDD.E3,1):np2*size(MLDD.E3,1),...
173             1+(np1-1)*size(MLDD.E3,2):np1*size(MLDD.E3,2)) = ...
174             MLDD.E1*MLDD.A^(np2-2)*MLDD.B2;
175         F1.F1d_zd(1+(np2-1)*size(MLDD.E4,1):np2*size(MLDD.E4,1),...
176             1+(np1-1)*size(MLDD.E4,2):np1*size(MLDD.E4,2)) = ...
177             MLDD.E1*MLDD.A^(np2-2)*MLDD.B3;
178     end
179 end
180 clear np1 np2
181
182 % Concatenating all submatrices
183 F1.F1b1 = [F1.F1b1_u F1.F1b1_zd];
184 F1.F1b2 = [F1.F1b2_u F1.F1b2_zd];
185 F1.F1d = [F1.F1d_u F1.F1d_zd];
186 F1.F1 = [F1.F1b1 zeros(size(F1.F1b1,1),size(F1.F1b2,2)) ...
187         zeros(size(F1.F1b1,1),size(F1.F1d,2));
188         zeros(size(F1.F1b2,1),size(F1.F1b1,2)) F1.F1b2 zeros(size(F1.F1b2,1),size(F1.F1d,2))
189         zeros(size(F1.F1d,1),size(F1.F1b1,2)) zeros(size(F1.F1d,1),size(F1.F1b2,2)) F1.F1d];
190
191 % Constructing F1 matrices for Pimp
192 F1.F11b1 = zeros(dim.Np,3*dim.Np);
193 F1.F11d = zeros(dim.Np,9*dim.Np);
194
195 % F1 for the batteries
196 diag = [0 1 0];
197 F1.F11b1 = kron(eye(dim.Np),diag);
198 F1.F11b2 = F1.F11b1;
199
200 % F1 for the diesel generator
201 diagd = [0 0 0 0 1 0 0 0 0];
202 F1.F11d = kron(eye(dim.Np),diagd);

```

```

197
198     F1.F1new = [F1.F1 zeros(size(F1.F1,1),dim.Np);
199               F1.F1b1 F1.F1b2 F1.F1d eye(dim.Np);
200               -F1.F1b1 -F1.F1b2 -F1.F1d -eye(dim.Np)];
201
202     % Constructing F2.F2 matrix for MILP constraint equation
203     F2.F2b1 = zeros(dim.Np*size(MLDB1.g5,1),size(MLDB1.g5,2));
204     F2.F2b2 = zeros(dim.Np*size(MLDB2.g5,1),size(MLDB2.g5,2));
205     F2.F2d_1 = zeros(dim.Np*size(MLDD.g5,1),size(MLDD.g5,2));
206     F2.F2d_2 = zeros(dim.Np*size(MLDD.g5,1),size(MLDD.g5,2));
207
208     for n = 1:dim.Np
209         F2.F2b1(1+(n-1)*size(MLDB1.g5,1):n*size(MLDB1.g5,1),1:size(MLDB1.g5,2)) = MLDB1.g5;
210         F2.F2b2(1+(n-1)*size(MLDB2.g5,1):n*size(MLDB2.g5,1),1:size(MLDB2.g5,2)) = MLDB2.g5;
211         F2.F2d_1(1+(n-1)*size(MLDD.g5,1):n*size(MLDD.g5,1),1:size(MLDD.g5,2)) = MLDD.g5;
212
213         if n == 2
214             F2.F2d_2(1+(n-1)*size(MLDD.E1):n*size(MLDD.E1,1),1:size(MLDD.g5,2)) = ...
215                 MLDD.E1*MLDD.B4;
216         end
217
218         if n > 2
219             F2.F2d_2(1+(n-1)*size(MLDD.E1):n*size(MLDD.E1,1),1:size(MLDD.g5,2)) = ...
220                 F2.F2d_2(1+(n-2)*size(MLDD.E1,1):(n-1)*size(MLDD.E1,1)) + ...
221                 MLDD.E1*MLDD.B4*(MLDD.A)^(n-2);
222         end
223     end
224     clear n
225
226     % Concatenating submatrices into complete F2.F2 matrix
227     F2.F2d = F2.F2d_1 - F2.F2d_2;
228     F2.F2 = [F2.F2b1; F2.F2b2; F2.F2d];
229
230     F2.F2new = [F2.F2;
231                Pload(1:dim.Np)';
232                -Pload(1:dim.Np)'];
233
234     % Constructing F3.F3 matrix for MILP constraint equation
235     F3.F3b1 = zeros(dim.Np*size(MLDB1.E1,1),size(MLDB1.E1,2));
236     F3.F3b2 = zeros(dim.Np*size(MLDB2.E1,1),size(MLDB2.E1,2));
237     F3.F3d = zeros(dim.Np*size(MLDD.E1,1),size(MLDD.E1,2));
238
239     for n = 1:dim.Np
240         F3.F3b1(1+(n-1)*size(MLDB1.E1,1):n*size(MLDB1.E1,1),1:size(MLDB1.E1,2)) = ...
241             -MLDB1.E1*MLDB1.A^(n-1);
242         F3.F3b2(1+(n-1)*size(MLDB2.E1,1):n*size(MLDB2.E1,1),1:size(MLDB2.E1,2)) = ...
243             -MLDB2.E1*MLDB2.A^(n-1);
244         F3.F3d(1+(n-1)*size(MLDD.E1,1):n*size(MLDD.E1,1),1:size(MLDD.E1,2)) = ...
245             -MLDD.E1*MLDD.A^(n-1);
246     end
247     clear n
248
249     F3.F3 = [F3.F3b1 zeros(size(F3.F3b1,1),size(F3.F3b2,2)) ...
250             zeros(size(F3.F3b1,1),size(F3.F3d,2));
251             zeros(size(F3.F3b2,1),size(F3.F3b1,2)) F3.F3b2 zeros(size(F3.F3b2,1),size(F3.F3d,2))
252             zeros(size(F3.F3d,1),size(F3.F3b1,2)) zeros(size(F3.F3d,1),size(F3.F3b2,2)) F3.F3d];
253
254     F3.F3new = [F3.F3;
255                zeros(2*dim.Np,3)];
256
257     % Constructing W matrices for optimization
258     W1.W1b1 = [dim.Wb1*ones(1,dim.Np-1) 0];
259     W1.W1b2 = [dim.Wb2*ones(1,dim.Np-1) 0];
260     W1.W1d = [dim.Wd*ones(1,dim.Np-1) 0];
261     W1.W1 = [ W1.W1b1 W1.W1b2 W1.W1d ];
262
263     % W2 matrices again using submatrices
264     W2.W2b1 = zeros(dim.Np,3*dim.Np);
265     W2.W2b2 = zeros(dim.Np,3*dim.Np);
266     W2.W2d = zeros(dim.Np,9*dim.Np);
267
268     for nr = 1:dim.Np

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```

264     for nc = 1:3*dim.Np
265         if nr == nc
266             if nc ≤ dim.Np
267                 W2.W2b1(nr,nc) = 1;
268                 W2.W2b2(nr,nc) = 1;
269             end
270         end
271
272         if nr == nc+1
273             W2.W2b1(nr,nc) = -1;
274             W2.W2b2(nr,nc) = -1;
275         end
276     end
277
278     for nc = 1:9*dim.Np
279         if nc == 1+(nr-1)*4
280             W2.W2d(nr,nc:nc+3) = 1;
281         end
282     end
283
284
285     for nc = 1:9*dim.Np-1
286         if nc == 1+(nr-1)*4
287             W2.W2d(nr+1,nc:nc+3) = -1;
288         end
289     end
290
291 end
292
293 W2.W2d = W2.W2d(1:end-1,:);
294
295 W2.W2 = [W2.W2b1 zeros(size(W2.W2b1,1),size(W2.W2b2,2)) ...
296         zeros(size(W2.W2b1,1),size(W2.W2d,2)); ...
297         zeros(size(W2.W2b2,1),size(W2.W2b1,2)) W2.W2b2 ...
298         zeros(size(W2.W2b2,1),size(W2.W2d,2)); ...
299         zeros(size(W2.W2d,1),size(W2.W2b1,2)) zeros(size(W2.W2d,1),size(W2.W2b2,2)) W2.W2d];
300
301 % W3 matrices
302 W3.W3b1 = [zeros(1,dim.Np-1) -dim.We];
303 W3.W3b2 = [zeros(1,dim.Np-1) -dim.We];
304 W3.W3d = [zeros(1,dim.Np-1) -dim.Wfuel];
305 W3.W3 = [W3.W3b1 W3.W3b2 W3.W3d];
306
307 % W4 matrices
308 W4.W4b1 = dim.We;
309 W4.W4b2 = dim.We;
310 W4.W4d = dim.Wfuel;
311 W4.W4 = [W4.W4b1 W4.W4b2 W4.W4d];
312
313 % W5 matrices
314 W5.W5b1 = [zeros(1,dim.Np) -Ce(1,1:dim.Np-1) 0 zeros(1,dim.Np)];
315 W5.W5b2 = [zeros(1,dim.Np) -Ce(1,1:dim.Np-1) 0 zeros(1,dim.Np)];
316 W5.W5d = [zeros(1,4*dim.Np) -Ce(1,1:dim.Np-1) 0 zeros(1,4*dim.Np)];
317
318 W5.W5 = [W5.W5b1 W5.W5b2 W5.W5d];
319
320 % S matrices
321 S1.S1b1 = W3.W3b1*M1.M1_b1+W5.W5b1;
322 S1.S1b2 = W3.W3b2*M1.M1_b2+W5.W5b2;
323 S1.S1d = W3.W3d*M1.M1_d+W5.W5d;
324
325 S1.S1 = W3.W3*M1.M1+W5.W5;
326
327 S1.S1b1new = [W3.W3b1*M1.M1_b1 Ce(1:dim.Np-1) 0];
328 S1.S1b2new = [W3.W3b2*M1.M1_b2 Ce(1:dim.Np-1) 0];
329 S1.S1dnew = [W3.W3d*M1.M1_d Ce(1:dim.Np-1) 0];
330
331 S1.S1new = [W3.W3*M1.M1+W5.W5 Ce(1:dim.Np-1) 0];
332
333 S2.S2b1 = W3.W3b1*M2.M2_b1+W4.W4b1;
334 S2.S2b2 = W3.W3b2*M2.M2_b2+W4.W4b2;

```



```
335      S2.S2d  = W3.W3d*M2.M2_d*W4.W4d;  
336      S2.S2   = W3.W3*M2.M2+W4.W4;  
337  
338  end
```