

PSSE PV and QV Analysis Study Report

Jessla Varaparambil Abdul Kadher

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Chapter 1

Performing PV and QV Analyses

1.1 Introduction

The PV/QV analyses are designed for studies of low voltage stability, which could be analyzed as a steady-state problem. They are power flow based analyses used to assess voltage variations with active and reactive power change. Two methods are used to determine the loading limits imposed by voltage stability under the steady-state conditions. The PV/QV analyses do not provide solutions to specific problem but function as tools that can be directed by the user to perform analyses in the solution of problems associated with the steady-state voltage stability of power systems.

The objective of a PV and QV curves is to determine the ability of a power system to maintain voltage stability at all the buses in the system under normal and abnormal steady-state operating conditions. They are useful, for example:

- To show the voltage collapse point of the buses in the power system network.
- To study the maximum transfer of power between buses before voltage collapse point.
- To size the reactive power compensation devices required at relevant buses to prevent voltage collapse.
- To study the influence of generators, loads and reactive power compensation devices on the network.

The PV and QV curves are obtained through a series of ac power flow solutions. The PV curve is a representation of voltage change as a result of increased power transfer between two systems, and the QV curve is a representation of reactive power demand by a bus or buses as voltage level changes.

1.2 Description for System Under Study

The following section describes the system and system conditions for which PV and QV analysis is carried out. The focus of this study is to carry out PV and QV analysis on Bus 3005 in area 5 (WORLD) of the savnw system. The Figure 1.1 shows the Bus 3005 considered for the analysis.

The bus 3005 connections are as follows

- to bus 3003 by two lines
- to bus 3008 by two lines
- to bus 3006 by a single line
- to bus 3004 by a 2-winding transformer
- to load of magnitude $102+j51.0$

Following contingencies at the bus 3005 are considered for conducting the analysis.

- Single open line 1 3005-3003(1)
- Single open line 2 3005-3003(2)

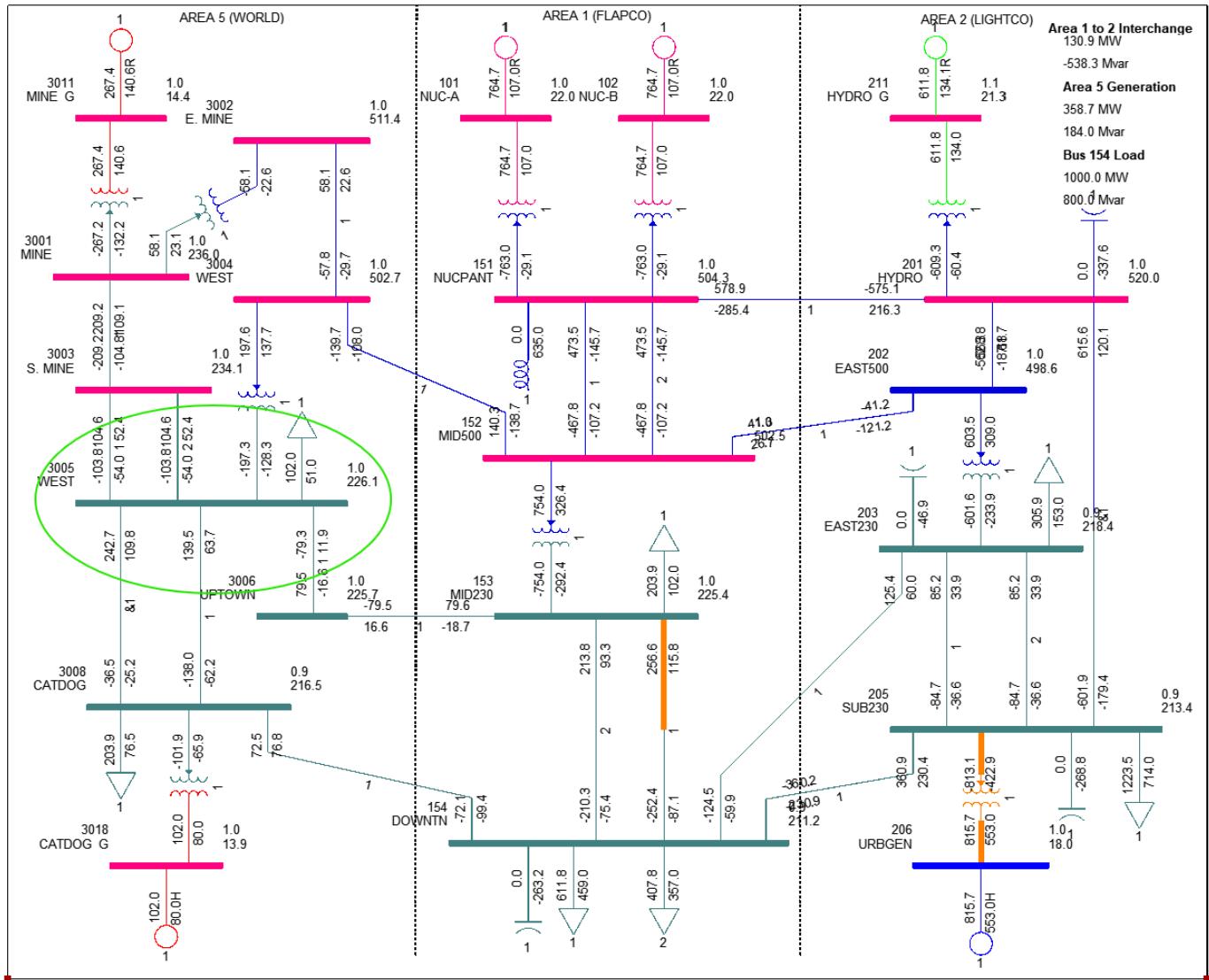


Figure 1.1: System/Bus for conducting PV and QV Analysis

- Single open line 3 3005-3004(1)
 - Single open line 4 3005-3006(1)
 - Single open line 5 3005-3008(&1)
 - Single open line 3 3005-3008(1)

The various loads for which the analysis is carried out are

- $41+j30.6$ (PF = 0.80 lagging)
 - $20+j10$ (PF = 0.89 lagging)
 - $32+j6.4$ (PF = 0.98 lagging)
 - $40+j0$ (PF = UPF)
 - $41-j30.6$ (PF = 0.80 leading)
 - $20-j10$ (PF = 0.89 leading)
 - $32-j6.4$ (PF = 0.98 leading)

The PV analysis is carried out for loads of various power factors to determine the incremental transfers possible from the defined source subsystem to the sink subsystem. The QV analysis is carried out to size the reactive power supporting elements that will be required to maintain a desired voltage at the studied Bus 3005. The configuration files (.sub, .mon and .con) for creating the distribution factor file for this study is as shown in Figure 1.2.

Subsystem Definition	Monitored Element
SUBSYSTEM SOURCE BUS 3011 BUS 3008 END	MONITOR VOLTAGE RANGE SUBSYSTEM MON 0.950 1.050 END END
SUBSYSTEM SINK BUS 3005 END	
SUBSYSTEM CON BUS 3005 END	Contingency Definition
SUBSYSTEM MON BUS 3005 END	SINGLE LINE FROM BUS 3005 END END

Figure 1.2: System/Bus for conducting QV Analysis

Chapter 2

PV Analysis

2.1 Introduction

PV curves are parametric study involving a series of ac power flows that monitor the changes in one set of power flow variables with respect to another in a systematic fashion. This approach is a powerful method for determining transfer limits that account for voltage and reactive flow effects. As power transfer is increased, voltage decreases at some buses on or near the transfer path. The transfer capacity where voltage reaches the low voltage criterion is the low voltage transfer limit. Transfer can continue to increase until the solution identifies a condition of voltage collapse; this is the voltage collapse transfer limit.

PV curves are typically used for the knee curve analysis. It is as named because of its distinctive shape at the point of voltage collapse as the power transfer increases. Depending on the transfer path, different buses have different knee point. The buses closer to the transfer path will normally exhibit a more discernible knee point.

Voltage instability occurs at the knee point of the PV curve where the voltage drops rapidly with an increase in the transfer power flow. The power flow solution will not converge beyond this limit, indicating voltage instability. Operation at or near the stability limit is impractical and a satisfactory operating condition must be ensured to prevent voltage collapse.

In PSSE, the PV curves are generated by selecting two subsystems where the power transfer between the subsystems is incremented in a defined step size for a series of ac power flow calculations while the bus voltages, generator outputs and the branch flows of the system are monitored. When the bus voltages are plotted as a function of the incremental power transfer the PV curves are obtained. One of the subsystems in the study must be defined as the study (source) system and another as the opposing (sink) system. The power flows from the study subsystem to the opposing subsystem.

In this chapter PV analysis is analysed to determine the maximum power that can be transmitted at any load factor. In the previous chapter the various load factors that will be considered for this analysis was listed.

2.2 PV Analysis in PSSE

The PV analysis is carried out for loads of various power factors to determine the incremental transfers possible from the defined source subsystem of generators connected in Bus 3011 and Bus 3018 to the sink subsystem of Bus 3005. By conducting PV analysis for the defined source and sink subsystem, the goal of this study is to determine the maximum power transfer possible for each of the considered cases and loads. Figure 2.1 shows the PV analysis parameters considered for this study.

Figure 2.2 shows the PV curves of a bus 3005 in an example network under normal and various contingency conditions for a load factor of 0.89 lagging. The maximum transfer limit for this bus in base case is approximately 400 MW. The maximum transfer limit decreases under contingency conditions. The response shown is expected because under network contingencies the loading of the line will increase. These curves can be used to set transfers or local generation dispatch so that the system will not fall below the knee point following a disturbance (i.e. loss of lines).

The complete results of PV analysis for each MW incremental transfer of every case and load obtained from PSSE is given in the Appendix A of this document.

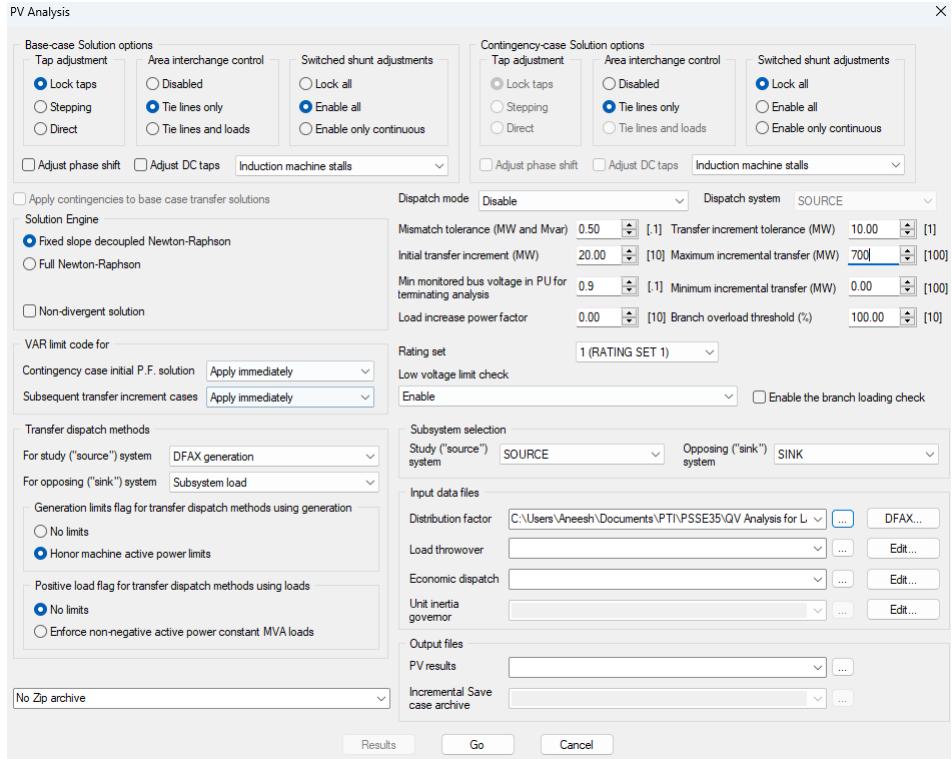


Figure 2.1: PV Analysis Study Parameters

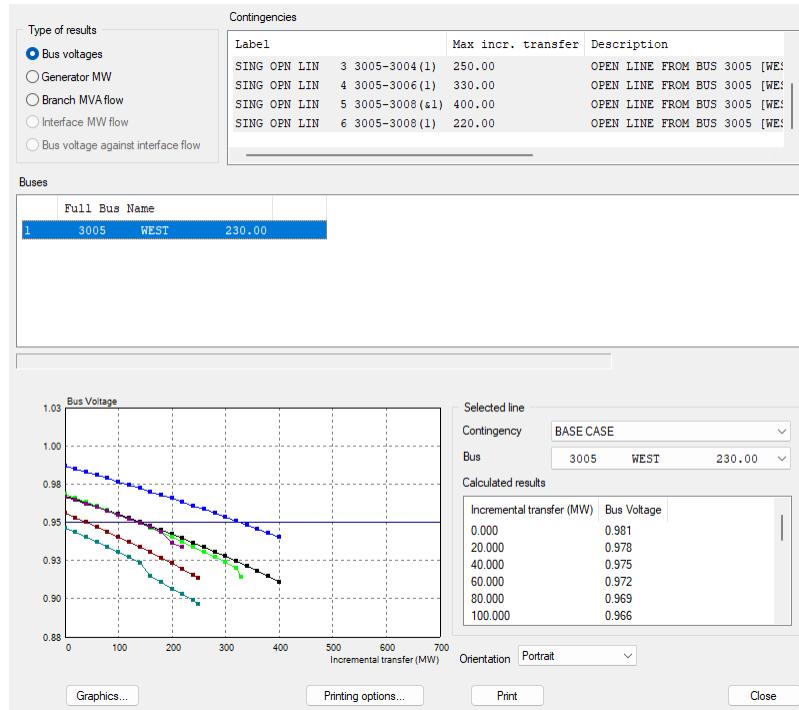


Figure 2.2: PV Curves Voltage and Incremental Power Transfer Characteristics for Bus 3005 under Different Network Conditions

2.3 Analysis of PV Solution for Different Network Conditions

As previously mentioned in Chapter 1 there are 7 contingency cases and 7 load factors considered for this analysis. Each of these loads are started with a low magnitude and the PV analysis scales these loads in MWs of 20 to give

corresponding voltages at Bus 3005. Table 2.1 tabulates the maximum incremental transfers to the bus for base case and contingencies for each considered load factor.

Study Case	Load	Load Factor	Maximum incr. transfer	Voltage (PU)
BASE CASE	32-j6.4	0.98 leading	680	0.976
	20-j10	0.89 leading	700	1.021
	41-j30.6	0.8 leading	680	1.054
	40+j0	UPF	660	0.943
	32+j6.4	0.98 lagging	620	0.914
	20+j10	0.89 lagging	400	0.913
	41+j30.6	0.8 lagging	280	0.912
SING OPN LIN 1 3005-3003(1)	32-j6.4	0.98 leading	680	0.946
	20-j10	0.89 leading	700	1.003
	41-j30.6	0.8 leading	680	1.044
	40+j0	UPF	540	0.922
	32+j6.4	0.98 lagging	380	0.918
	20+j10	0.89 lagging	250	0.916
	41+j30.6	0.8 lagging	170	0.914
SING OPN LIN 2 3005-3003(2)	32-j6.4	0.98 leading	680	0.946
	20-j10	0.89 leading	700	1.003
	41-j30.6	0.8 leading	680	1.044
	40+j0	UPF	540	0.922
	32+j6.4	0.98 lagging	380	0.918
	20+j10	0.89 lagging	250	0.916
	41+j30.6	0.8 lagging	170	0.914
SING OPN LIN 3 3005-3004(1)	32-j6.4	0.98 leading	680	0.941
	20-j10	0.89 leading	700	0.999
	41-j30.6	0.8 leading	680	1.041
	40+j0	UPF	580	0.902
	32+j6.4	0.98 lagging	380	0.899
	20+j10	0.89 lagging	250	0.896
	41+j30.6	0.8 lagging	160	0.897
SING OPN LIN 4 3005-3006(1)	32-j6.4	0.98 leading	680	0.976
	20-j10	0.89 leading	700	1.026
	41-j30.6	0.8 leading	680	1.063
	40+j0	UPF	660	0.939
	32+j6.4	0.98 lagging	520	0.918
	20+j10	0.89 lagging	330	0.917
	41+j30.6	0.8 lagging	280	0.908
SING OPN LIN 5 3005-3008(&1)	32-j6.4	0.98 leading	680	1.01
	20-j10	0.89 leading	700	1.051
	41-j30.6	0.8 leading	680	1.092
	40+j0	UPF	660	0.98
	32+j6.4	0.98 lagging	620	0.954
	20+j10	0.89 lagging	400	0.948
	41+j30.6	0.8 lagging	280	0.945
SING OPN LIN 6 3005-3008(1)	32-j6.4	0.98 leading	680	0.975
	20-j10	0.89 leading	700	1.021
	41-j30.6	0.8 leading	680	1.056
	40+j0	UPF	600	0.942
	32+j6.4	0.98 lagging	370	0.94
	20+j10	0.89 lagging	220	0.94
	41+j30.6	0.8 lagging	140	0.939

Table 2.1: Maximum power transfer for considered study cases and load factors

From Table 2.1, looking at the results of base case and the contingency case of single open line 1 3005 - 3003 (1), the following inferences are derived.

For the base case, the maximum power transfer of 700 MW is achieved for a load factor of 0.89 leading at a bus voltage of 1.021 PU, which is below the upper limit of 1.05 PU. Besides the above case, the load factor 0.98 leading also has the maximum transfer of 680 MW achieved at a bus voltage of 0.976 PU. All other load factors considered have their maximum power transfers achieved outside of the normal operating limit of 0.95 PU to 1.05 PU.

For the single open line 1 3005 - 3003 (1), the maximum power transfer of 700 MW is achieved for a load factor of 0.89 leading at a bus voltage of 1.003 PU, which is below the upper limit of 1.05 PU. Besides the above case, the load factor 0.8 leading also has the maximum transfer of 680 MW achieved within the normal operating limit at a bus voltage of 1.044 PU. Similar to the Base Case all other load factors considered have their maximum power transfers achieved outside of the normal operating limit of 0.95 PU to 1.05 PU.

Chapter 3

QV Analysis

3.1 Introduction

QV (Reactive Power - Voltage) curve analysis focuses on reactive power support required to maintain voltage within acceptable limits at the studied bus. By injecting or absorbing reactive power at specified buses and observing voltage changes, it reveals the system's voltage sensitivity and strength. Together, these analyses provide a comprehensive view of voltage stability, guiding decisions on reactive power compensation and system reinforcements.

The QV analysis process does a series of power flow solutions with unlimited reactive power support at some bus and the estimated quantity is the bus voltage at the bus. Bus reactive support comes in two (2) ways

- Capacitive - increases bus voltage (supplying VARs to the system)
- Inductive - decreases bus voltage (absorbing VARs from the system)

QV in PSSE can be used to determine how many VARs are needed at the studied bus to maintain certain range of bus voltages defined (for both normal and outage conditions) QV curves are used to determine the reactive power injection required at a bus in order to vary the bus voltage to the required value. The curve is obtained through a series of ac power flow calculations. Starting with the specified maximum per unit voltage setpoint at the study bus, the reactive power injections can be computed for a series of power flows as the voltage setpoint is decreased in steps, until the power flow demonstrates convergence difficulties as the system approaches the voltage collapse point.

The bottom of the QV curve, where the change of reactive power, Q , with respect to voltage, V (or derivative dQ/dV) is equal to zero, represents the voltage stability limit. Because all reactive power compensator devices are designed to operate satisfactorily when an increase in Q is accompanied by an increase in V , the operation on the right side of the QV curve is stable, whereas the operation on the left side is unstable. Also, voltage on the left side may be so low that the protective devices may be activated. The bottom of the QV curves, in addition to identifying the stability limit, defines the minimum reactive power requirement for the stable operation. Hence, the QV curve can be used to examine the type and size of compensation needed to provide voltage stability. This can be performed by super-imposing the QV characteristic curves of the compensator devices on that of the system. For instance the capacitor characteristic can be drawn over the system's QV curves.

3.2 Analysis of QV Analysis Solution Using PSSE

QV analysis on the system is carried out to determine the reactive power support that would be required to maintain the voltage range of 0.90 PU to 1.10 PU at bus 3005 for the network conditions as well as for the load factors listed in Chapter 1. From the Figure 1.1, it can be seen that at present the bus does not have any reactive supporting elements connected to it. Bus 3005 has a load connected to it. There are 5 lines connecting the bus to other buses and a transformer branch to bus 3004. The normal voltage limit of operation for the system is 0.95 PU to 1.05 PU.

The goal of this study is to conduct analysis on obtained QV analysis results for various loads to determine the reactive power support needed to maintain the set voltage of 1.0 PU at bus 3005 for single line contingencies at Bus 3005. Figure 3.1 shows the QV analysis parameters considered for this study.

Figure 3.2 shows the QV curves of a bus 3005 in an example network under normal and various contingency conditions for a load of $32+j6.4$ with a power factor of 0.98 lagging. To maintain a voltage of 1.0 PU at the studied

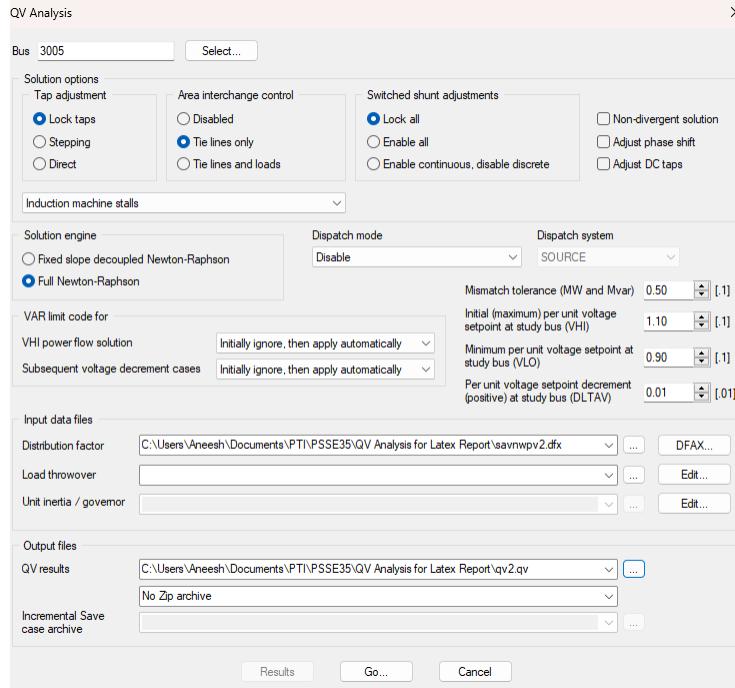


Figure 3.1: QV Analysis Study Parameters

bus, for the base case a reactive power support of 90.92 MVAR is required. For the same load under contingency condition - single open line of the transformer branch from 3005 to 3004, a reactive power support of 171.96 MVAR is required. Similarly for other contingency cases the reactive power support required to maintain 1.0 PU of voltage at the Bus 3005 can be determined.

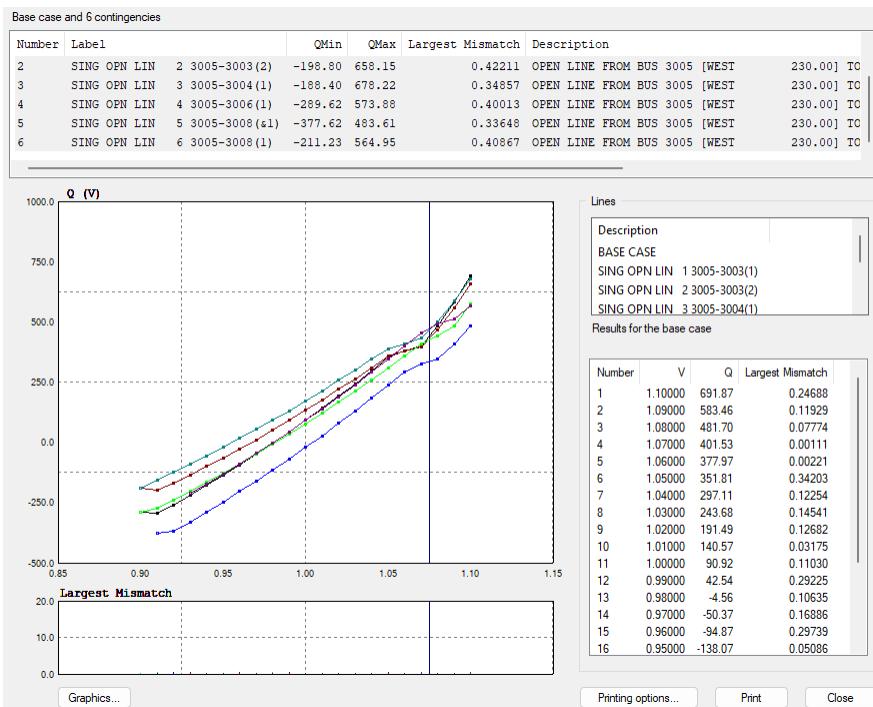


Figure 3.2: QV Curves showing Reactive power support needed for set bus voltages for Bus 3005 under Different Network Conditions for a load of $32+j6.4$

The complete results of QV analysis results for every case and load obtained from PSSE is given in the Appendix B of this document.

3.3 Analysis of QV Solution for Different Network Conditions

As previously mentioned there are 7 contingency cases and 7 loads considered for this analysis. For each of the 7 network conditions for each load, the reactive power support required to maintain a voltage of 1.0 PU at the Bus 3005 is derived from the QV analysis. Table 3.1 tabulates the reactive power support required to maintain a

Study Case	Load	Load Factor	Voltage (PU)	Reactive Power (MVAR)
BASE CASE	32-j6.4	0.98 leading	1.0	78.117
	20-j10	0.89 leading	1.0	72.911
	41-j30.6	0.80 leading	1.0	55.152
	40+j0	UPF	1.0	85.613
	32+j6.4	0.98 lagging	1.0	90.917
	20+j10	0.89 lagging	1.0	92.911
	41+j30.6	0.80 lagging	1.0	116.352
SING OPN LIN 1 3005-3003(1)	32-j6.4	0.98 leading	1.0	119.204
	20-j10	0.89 leading	1.0	113.63
	41-j30.6	0.80 leading	1.0	96.524
	40+j0	UPF	1.0	126.953
	32+j6.4	0.98 lagging	1.0	132.004
	20+j10	0.89 lagging	1.0	133.63
	41+j30.6	0.80 lagging	1.0	157.724
SING OPN LIN 2 3005-3003(2)	32-j6.4	0.98 leading	1.0	119.204
	20-j10	0.89 leading	1.0	113.63
	41-j30.6	0.80 leading	1.0	96.524
	40+j0	UPF	1.0	126.953
	32+j6.4	0.98 lagging	1.0	132.004
	20+j10	0.89 lagging	1.0	133.63
	41+j30.6	0.80 lagging	1.0	157.724
SING OPN LIN 3 3005-3004(1)	32-j6.4	0.98 leading	1.0	159.165
	20-j10	0.89 leading	1.0	153.601
	41-j30.6	0.80 leading	1.0	136.47
	40+j0	UPF	1.0	166.901
	32+j6.4	0.98 lagging	1.0	171.965
	20+j10	0.89 lagging	1.0	173.601
	41+j30.6	0.80 lagging	1.0	197.67
SING OPN LIN 4 3005-3006(1)	32-j6.4	0.98 leading	1.0	63.669
	20-j10	0.89 leading	1.0	58.437
	41-j30.6	0.80 leading	1.0	40.724
	40+j0	UPF	1.0	71.183
	32+j6.4	0.98 lagging	1.0	76.469
	20+j10	0.89 lagging	1.0	78.437
	41+j30.6	0.80 lagging	1.0	101.924
SING OPN LIN 5 3005-3008(&1)	32-j6.4	0.98 leading	1.0	-34.077
	20-j10	0.89 leading	1.0	-38.488
	41-j30.6	0.80 leading	1.0	-57.639
	40+j0	UPF	1.0	-27.111
	32+j6.4	0.98 lagging	1.0	-21.277
	20+j10	0.89 lagging	1.0	-18.488
	41+j30.6	0.80 lagging	1.0	3.561
SING OPN LIN 6 3005-3008(1)	32-j6.4	0.98 leading	1.0	77.924
	20-j10	0.89 leading	1.0	72.736
	41-j30.6	0.80 leading	1.0	54.946
	40+j0	UPF	1.0	85.409
	32+j6.4	0.98 lagging	1.0	90.724
	20+j10	0.89 lagging	1.0	92.736
	41+j30.6	0.80 lagging	1.0	116.146

Table 3.1: Reactive power support required to maintain 1.0 PU at Bus 3005 for considered study cases and loads

voltage of 1.0 PU at the bus 3005 for the base case and contingencies for each considered load.

From Table 3.1, looking at the results of base case and the contingency case of single open line 1 3005 - 3008

(1), the following inferences are derived.

For the base case, to maintain a voltage of 1.0 PU at the study bus for the UPF load of $40+j0$, a reactive power support of 85.613 MVAR is needed. When the load connected is having a lagging power factor, the reactive power support needed would be more than that for the UPF and when the load connected has a leading power factor, the reactive power required to maintain the 1.0 PU will be less than that is needed for the UPF load. When the $41-j30.6$, 0.80 leading pf load is connected to the bus 3005, the reactive power support needed to maintain 1.0 PU is 55.152 MVAR (less than UPF load requirement) and when the load connected is $41+j30.6$, 0.8 lagging pf, the reactive power support needed to maintain 1.0 PU is 116.352 MVAR (more than UPF load requirement).

For the contingency case of single open line 1 3005 - 3008 (1), to maintain a voltage of 1.0 PU at the study bus for the UPF load of $40+j0$, a reactive power support of 85.409 MVAR is needed.. When the $41-j30.6$, 0.80 leading pf load is connected to the bus 3005, the reactive power support needed to maintain 1.0 PU is 54.946 MVAR (less than UPF load requirement) and when the load connected is $41+j30.6$, 0.8 lagging pf, the reactive power support needed to maintain 1.0 PU is 116.146 MVAR (more than UPF load requirement).

Chapter 4

Conclusion

The PV and QV analysis are carried out for various network conditions for Bus 3005. The Chapter 1 described the study system and the various network conditions considered (single line contingencies on Bus 3005 and loads of various power factors) to carry out the PV and QV analysis. In Chapter 2 the maximum incremental power that can be transferred to the sink bus 3005 was analyzed for various network conditions and load factors. In Chapter 3 the reactive power support required to maintain a voltage of 1.0 PU at the bus 3005 was analyzed for various network conditions and load factors.

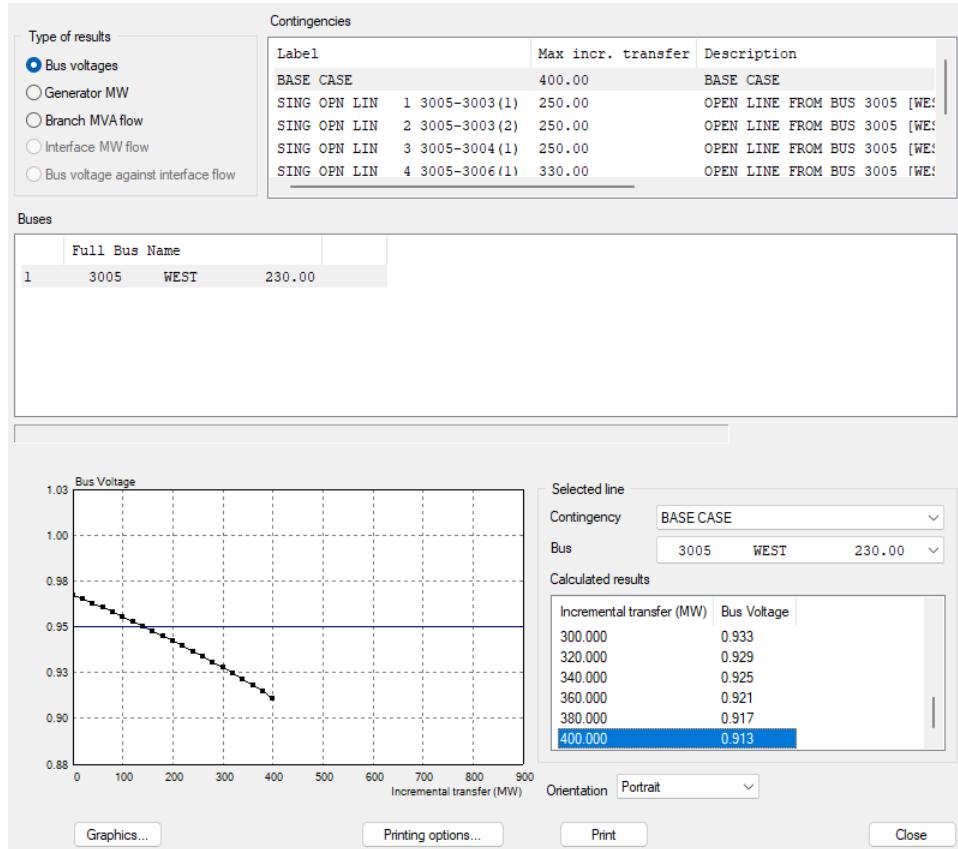


Figure 4.1: PV Results for Load Factor 0.89

To conclude this study, a special case is considered where the maximum power transfer obtained from PV analysis for a load factor of 0.89 lagging is used to estimate the load MVAR for a fictitious load. When this load is connected to the system, a QV analysis is carried out to estimate the reactive power support needed to maintain the Bus voltage of 1.0 PU for normal operating conditions. Figure 4.1 shows the PV Result obtained for the load factor of 0.89 lagging.. It can be seen that a maximum incremental transfer of 400 MW is possible from the present operating conditions. For the incremental transfer of 400 MW, the voltage at the bus is 0.913 PU, which is less than the normal operating voltage. If the 400 MW of power needed to be transferred to the system, there needs to be

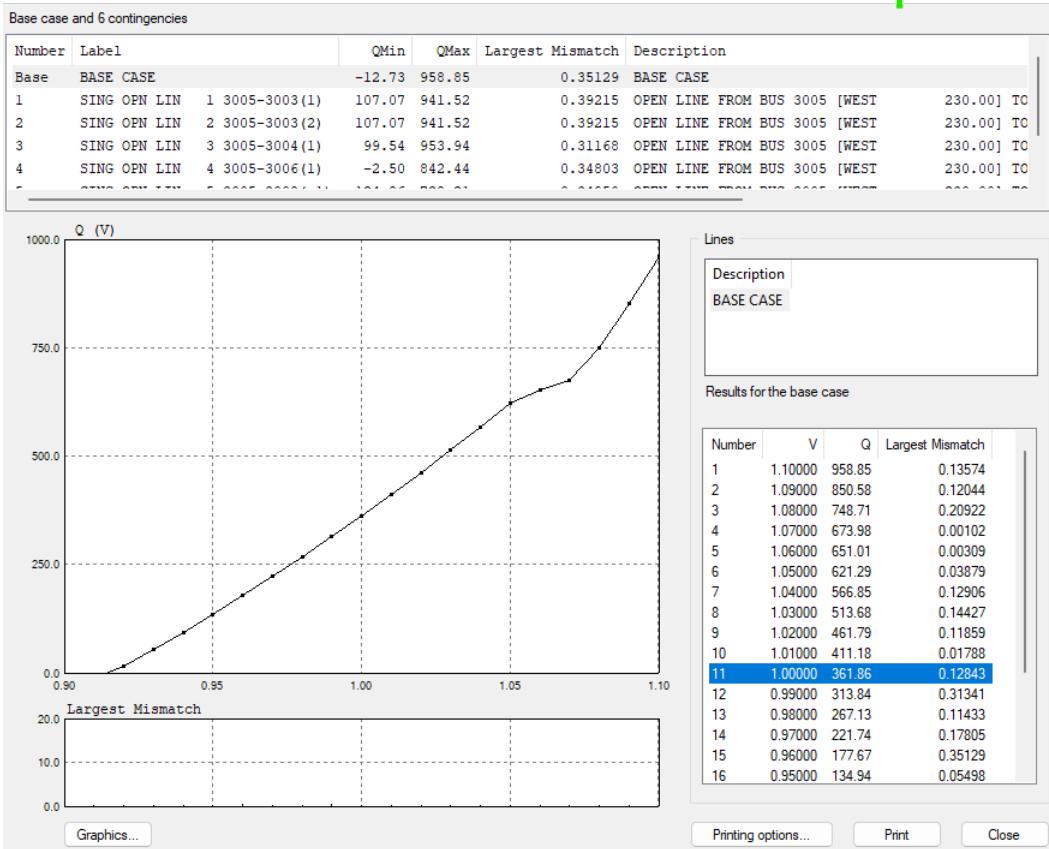


Figure 4.2: QV Results corresponding to a load of $400+j204.9$ at Bus 3005

a reactive power supporting device connected at the bus. If the desired bus voltage at the bus for this transfer is chosen as 1.0 PU, a QV analysis can be carried out on the system connected with a load of 400 MW with a load factor of 0.89 lagging connected to size the reactive power supporting equipment to be connected at the bus.

BUS	3005	WEST	230.00	CKT	MW	MVAR	MVA	%	0.9160PU	-11.99	X---	LOSSES	--X	X----	AREA	--X	X----	ZONE	--X	3005
TO LOAD-PQ					400.0	204.9	449.4		210.69KV											
TO 3003	S. MINE	230.00	1	-209.7	-88.5	227.6					3.66	32.91	5	WORLD				5	FIFTH	
TO 3003	S. MINE	230.00	2	-209.7	-88.5	227.6					3.66	32.91	5	WORLD				5	FIFTH	
TO 3004	WEST	500.00	1	-263.1	-178.0	317.7	40	1.0000UN			0.48	19.54	5	WORLD				5	FIFTH	
TO 3006	UPTOWN	230.00	1	-86.9	-25.1	90.5					0.34	2.88	5	WORLD				5	FIFTH	
TO 3008	CATDOG	230.00	&1	236.4	111.2	261.2					2.51	20.93	5	WORLD				5	FIFTH	
TO 3008	CATDOG	230.00	1	133.0	64.0	147.6					1.61	13.38	5	WORLD				5	FIFTH	

Figure 4.3: Load flow results without reactive power support

BUS	3005	WEST	230.00	CKT	MW	MVAR	MVA	%	1.0000PU	-11.07	X---	LOSSES	--X	X----	AREA	--X	X----	ZONE	--X	3005
TO LOAD-PQ					400.0	204.9	449.4		230.00KV											
TO SHUNT					0.0	-361.8	361.8													
TO 3003	S. MINE	230.00	1	-206.8	-15.3	207.3					2.57	23.15	5	WORLD				5	FIFTH	
TO 3003	S. MINE	230.00	2	-206.8	-15.3	207.3					2.57	23.15	5	WORLD				5	FIFTH	
TO 3004	WEST	500.00	1	-270.2	-81.5	282.2	35	1.0000UN			0.32	12.94	5	WORLD				5	FIFTH	
TO 3006	UPTOWN	230.00	1	-91.4	47.6	103.1					0.38	3.29	5	WORLD				5	FIFTH	
TO 3008	CATDOG	230.00	&1	239.5	133.7	274.3					2.39	19.91	5	WORLD				5	FIFTH	
TO 3008	CATDOG	230.00	1	135.6	87.7	161.5					1.63	13.59	5	WORLD				5	FIFTH	

Figure 4.4: Load flow results with reactive power support at Bus 3005

QV results obtained by connecting a load of $400+j204.9$ at the Bus 3005 is as shown in Figure 4.2. It can be seen that in order to maintain voltage of 1.0 PU at the bus a reactive power support of 361.86 MVAR is needed.

The power flow solution obtained at the Bus 3005 is shown with(Figure 4.3) and without(Figure 4.4 the reactive power support. It can be seen that the added reactive power support has helped to achieve the desired voltage of 1.0 PU at Bus 3005.

Appendix A

Complete PV Results

Here, the complete PV Result obtained for various load factors and network conditions are shown for reference. The maximum power transfer information shared on Table 2.1 is obtained from collating the PV result obtained for these various cases.

Load Factor 0.8 Lagging															
CONTINGENCY: BASE CASE							Voltage (pu)								
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	220.000	240.000	260.000	280.000
3005 WEST 230.00	0.975	0.972	0.968	0.964	0.959	0.955	0.951	0.946	0.942	0.937	0.933	0.928	0.923	0.918	0.912
CONTINGENCY: SING OPN LIN 1 3005-3003(1) Voltage (pu)															
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000	170.000					
3005 WEST 230.00	0.961	0.956	0.951	0.945	0.940	0.935	0.929	0.923	0.917	0.914					
CONTINGENCY: SING OPN LIN 2 3005-3003(2) Voltage (pu)															
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000	170.000					
3005 WEST 230.00	0.961	0.956	0.951	0.945	0.940	0.935	0.929	0.923	0.917	0.914					
CONTINGENCY: SING OPN LIN 3 3005-3004(1) Voltage (pu)															
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000						
3005 WEST 230.00	0.949	0.944	0.938	0.933	0.927	0.916	0.909	0.910	0.897						
CONTINGENCY: SING OPN LIN 4 3005-3006(1) Voltage (pu)															
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	220.000	240.000	260.000	270.000
3005 WEST 230.00	0.976	0.972	0.967	0.963	0.958	0.953	0.948	0.944	0.938	0.933	0.928	0.922	0.917	0.911	0.908
CONTINGENCY: SING OPN LIN 5 3005-3008(41) Voltage (pu)															
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	220.000	240.000	260.000	280.000
3005 WEST 230.00	0.999	0.996	0.992	0.989	0.985	0.982	0.978	0.974	0.970	0.966	0.962	0.958	0.954	0.950	0.945
CONTINGENCY: SING OPN LIN 6 3005-3008(1) Voltage (pu)															
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000							
3005 WEST 230.00	0.975	0.971	0.967	0.963	0.958	0.954	0.944	0.939							

Figure A.1: PV Results corresponding to a base case load of 41+j30.6 and load factor of 0.8 lagging at Bus 3005

Load Factor 0.89 Lagging

		Voltage (pu)																			
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	220.000	240.000	260.000	280.000	300.000	320.000	340.000	360.000	380.000	400.000
3005 WEST 230.00	0.981	0.978	0.975	0.972	0.969	0.966	0.963	0.960	0.957	0.954	0.951	0.947	0.944	0.940	0.937	0.933	0.929	0.925	0.921	0.917	0.913
		CONTINGENCY: SING OPN LIN 1 3005-3003(1) Voltage (pu)																			
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	220.000	240.000	250.000							
3005 WEST 230.00	0.987	0.963	0.960	0.956	0.952	0.949	0.945	0.941	0.936	0.932	0.928	0.923	0.918	0.916							
		CONTINGENCY: SING OPN LIN 2 3005-3003(2) Voltage (pu)																			
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	220.000	240.000	250.000							
3005 WEST 230.00	0.987	0.963	0.960	0.956	0.952	0.949	0.945	0.941	0.936	0.932	0.928	0.923	0.918	0.916							
		CONTINGENCY: SING OPN LIN 3 3005-3004(1) Voltage (pu)																			
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	220.000	240.000	250.000							
3005 WEST 230.00	0.985	0.962	0.948	0.944	0.940	0.936	0.932	0.928	0.918	0.913	0.908	0.904	0.898	0.896							
		CONTINGENCY: SING OPN LIN 4 3005-3006(1) Voltage (pu)																			
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	220.000	240.000	260.000	280.000	300.000	320.000	330.000			
3005 WEST 230.00	0.982	0.979	0.975	0.972	0.969	0.966	0.962	0.959	0.955	0.952	0.948	0.944	0.940	0.937	0.932	0.928	0.924	0.917			
		CONTINGENCY: SING OPN LIN 5 3005-3008(41) Voltage (pu)																			
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	220.000	240.000	260.000	280.000	300.000	320.000	340.000	360.000	380.000	400.000
3005 WEST 230.00	1.004	1.001	0.999	0.997	0.994	0.992	0.989	0.987	0.984	0.981	0.978	0.976	0.973	0.970	0.967	0.964	0.961	0.958	0.955	0.951	0.948
		CONTINGENCY: SING OPN LIN 6 3005-3008(1) Voltage (pu)																			
MW TRANSFER->	0.000	20.000	40.000	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	220.000									
3005 WEST 230.00	0.980	0.977	0.974	0.971	0.968	0.965	0.962	0.959	0.956	0.952	0.944	0.940									

Figure A.2: PV Results corresponding to a to a base case load of 20+j10 and load factor of 0.89 lagging at Bus 3005

Load Factor 0.98 Lagging

Figure A.3: PV Results corresponding to a base case load of 32+j6.4 and a load factor of 0.98 lagging at Bus 3005

20

UPF Load Factor										
CONTINGENCY: BASE CASE										
NO TRANSFER ->	0.000	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
3005 WEST 230 ->	0.982	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
CONTINGENCY: SING OPEN LIN	1	3005-5-3003(1)	Voltage (pu)							
NO TRANSFER ->	0.000	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
3005 WEST 230 ->	0.982	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
CONTINGENCY: SING OPEN LIN	2	3005-5-3003(2)	Voltage (pu)							
NO TRANSFER ->	0.000	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
3005 WEST 230 ->	0.982	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
CONTINGENCY: SING OPEN LIN	3	3005-5-3004(1)	Voltage (pu)							
NO TRANSFER ->	0.000	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
3005 WEST 230 ->	0.982	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
CONTINGENCY: SING OPEN LIN	4	3005-5-3006(1)	Voltage (pu)							
NO TRANSFER ->	0.000	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
3005 WEST 230 ->	0.982	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
CONTINGENCY: SING OPEN LIN	5	3005-5-3008(61)	Voltage (pu)							
NO TRANSFER ->	0.000	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
3005 WEST 230 ->	0.982	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
CONTINGENCY: SING OPEN LIN	6	3005-5-3008(1)	Voltage (pu)							
NO TRANSFER ->	0.000	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000
3005 WEST 230 ->	0.982	20.000	41.000	60.000	89.000	100.000	120.000	140.000	160.000	200.000

Figure A-4: PV Results corresponding to a base case load of $40+jo$ and a UPF load factor at Bus 3005

Figure A.5: PV Results corresponding to a base case load of 41:30.6 and load factor of 0.8 leading at Bus 3005

Load Factor 0.89 Leading											
MM TRANSFER->											
3005 WEST 230-00	0.945	0.996	40.000	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000
CONTINGENCY: SING CEN LINN 1 3(05-3003)(1)											
3005 WEST 230-00	0.920	0.990	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	240.000
MM TRANSFER->											
3005 WEST 230-00	0.972	0.974	60.977	60.977	0.979	0.980	0.982	0.983	0.984	0.985	0.987
CONTINGENCY: SING CEN LINN 2 3(05-3003)(2)											
3005 WEST 230-00	0.920	0.974	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	240.000
MM TRANSFER->											
3005 WEST 230-00	0.920	0.974	60.975	60.975	0.977	0.979	0.980	0.982	0.984	0.985	0.987
CONTINGENCY: SING CEN LINN 3 3(05-3004)(1)											
3005 WEST 230-00	0.961	0.964	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	240.000
MM TRANSFER->											
3005 WEST 230-00	0.961	0.963	60.964	60.964	0.966	0.968	0.970	0.972	0.973	0.975	0.977
CONTINGENCY: SING CEN LINN 4 3(05-3006)(1)											
3005 WEST 230-00	0.960	0.960	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	240.000
MM TRANSFER->											
3005 WEST 230-00	0.986	0.988	60.990	60.991	0.991	0.993	0.995	0.998	0.999	0.999	0.999
CONTINGENCY: SING CEN LINN 5 3(05-3008)(6)											
3005 WEST 230-00	1.018	1.010	60.000	80.000	100.000	120.000	140.000	160.000	180.000	200.000	240.000
MM TRANSFER->											
3005 WEST 230-00	1.013	1.011	1.013	1.015	1.015	1.018	1.021	1.021	1.021	1.024	1.025
CONTINGENCY: SING CEN LINN 6 3(05-3008)(1)											
3005 WEST 230-00	0.984	0.986	60.988	60.989	0.990	0.991	0.992	0.993	0.994	0.995	0.996

Figure A.6: PV Results corresponding to a base case load of 20-j10 and to a load factor of 0.89 leading at Bus 3005

Figure A.7: PV Results corresponding to a base case load of 32-j6.4 and to a load factor of 0.98 leading at Bus 3005

Appendix B

Complete QV Results

Here, the complete QV Result obtained for various loads and network conditions are shown for reference. The reactive power required to maintain a voltage of 1 PU at the Bus 3005 information shared on Table 2.1 is obtained from collating the QV result obtained for these various cases.

Load 41+j30.6																									
CONTINGENCY: BASE CASE		Plant (MVAR)																							
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	717.271	608.655	507.084	427.011	403.464	377.230	322.541	269.103	216.922	166.003	116.352	67.976	20.682	-24.920	-69.423	-112.614	-154.484	-195.019	-234.204	-268.236	-263.134				
CONTINGENCY: SING OPN LIN 1	3005-3003(1) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	683.802	583.548	489.767	419.358	403.254	383.249	335.910	289.683	244.573	200.584	157.724	115.999	75.417	35.986	-2.285	-39.385	-75.302	-110.023	-143.534	-172.833	-162.632				
CONTINGENCY: SING OPN LIN 2	3005-3003(2) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	683.802	583.548	489.767	419.358	403.254	383.249	335.910	289.683	244.573	200.584	157.724	115.999	75.417	35.986	-2.285	-39.385	-75.302	-110.023	-143.534	-172.833	-162.632				
CONTINGENCY: SING OPN LIN 3	3005-3004(1) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	703.828	611.862	524.314	457.827	431.999	412.105	370.392	325.708	282.024	239.343	197.670	157.007	117.359	78.730	41.126	4.551	-30.988	-65.484	-98.930	-131.318	-162.632				
CONTINGENCY: SING OPN LIN 4	3005-3006(1) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	599.307	509.022	464.846	434.272	383.610	334.005	285.458	237.973	191.554	146.205	101.924	58.721	16.599	-24.437	-64.381	-103.225	-140.972	-177.604	-213.115	-247.497	-263.928				
CONTINGENCY: SING OPN LIN 5	3005-3008(41) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	508.471	431.611	372.350	348.894	315.291	260.354	206.605	154.046	102.682	52.519	3.561	-44.187	-90.716	-136.021	-180.093	-222.923	-264.501	-304.815	-343.851	-352.717					
CONTINGENCY: SING OPN LIN 6	3005-3008(1) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	590.325	539.088	516.452	479.973	424.321	369.885	316.669	264.680	213.925	164.411	116.146	69.140	23.403	-21.053	-64.214	-106.066	-146.593	-185.773							

Figure B.1: QV Results corresponding to a load of 41+j30.6, load factor of 0.8 lagging at Bus 3005

Load 20+j10																									
CONTINGENCY: BASE CASE		Plant (MVAR)																							
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	693.917	585.498	483.747	403.455	379.891	353.812	299.120	245.679	193.493	142.568	92.911	44.527	-2.575	-48.388	-92.901	-136.105	-177.989	-218.538	-257.740	-292.034	-386.997				
CONTINGENCY: SING OPN LIN 1	3005-3003(1) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	659.868	559.609	465.851	395.076	378.944	359.195	311.851	265.618	220.499	176.501	133.630	91.893	51.297	11.851	-26.436	-63.554	-99.491	-134.234	-167.769	-197.496	-217.392				
CONTINGENCY: SING OPN LIN 2	3005-3003(2) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	659.868	559.609	465.851	395.076	378.944	359.195	311.851	265.618	220.499	176.501	133.630	91.893	51.297	11.851	-26.436	-63.554	-99.491	-134.234	-167.769	-197.496	-217.392				
CONTINGENCY: SING OPN LIN 3	3005-3004(1) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	679.982	588.006	500.490	434.012	407.561	387.620	346.348	301.659	257.969	215.282	173.601	132.930	93.273	54.634	17.019	-19.568	-55.120	-89.631	-123.093	-155.498	-186.836				
CONTINGENCY: SING OPN LIN 4	3005-3006(1) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	575.073	485.592	441.158	410.813	360.149	310.541	261.992	214.503	168.079	122.725	78.437	35.227	-6.903	-47.948	-87.903	-126.761	-164.517	-201.161	-236.687	-271.085	-307.954				
CONTINGENCY: SING OPN LIN 5	3005-3008(41) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	486.366	409.522	350.151	326.693	293.193	238.266	184.525	131.975	80.620	30.464	-18.488	-66.230	-112.754	-158.055	-202.124	-244.951	-286.527	-326.840	-365.877	-374.915					
CONTINGENCY: SING OPN LIN 6	3005-3008(1) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0											

Load 32+j6.4																									
CONTINGENCY: BASE CASE		Plant (MVAR)																							
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	691.875	582.458	481.695	401.527	377.973	351.805	297.115	243.676	191.492	140.571	90.917	42.537	-4.560	-50.367	-94.874	-138.072	-179.948	-220.489	-259.681	-293.827	-288.753				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	658.153	557.897	464.125	393.557	377.441	357.547	310.206	263.976	218.862	174.869	132.004	90.273	49.685	10.247	-28.031	-65.138	-101.064	-135.795	-169.317	-198.802	-188.643				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	658.153	557.897	464.125	393.557	377.441	357.547	310.206	263.976	218.862	174.869	132.004	90.273	49.685	10.247	-28.031	-65.138	-101.064	-135.795	-169.317	-198.802	-188.643				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	678.221	586.251	498.716	432.233	406.135	386.220	344.699	300.012	256.325	213.642	171.965	131.298	91.646	53.013	15.404	-21.176	-56.721	-91.224	-124.677	-157.072	-188.400				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	573.876	483.593	439.305	408.831	358.168	308.561	260.013	212.526	166.105	120.753	76.469	33.263	-8.862	-49.902	-89.852	-128.704	-166.453	-203.090	-238.608	-272.997	-289.618				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	483.610	406.757	347.448	323.991	290.433	235.500	181.754	129.199	77.839	27.678	-21.277	-69.022	-115.550	-160.853	-204.924	-247.753	-289.331	-329.644	-368.681	-377.622					
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	564.950	513.612	490.966	454.564	398.912	344.475	291.257	239.267	188.509	138.992	90.724	43.715	-2.026	-46.486	-89.653	-131.511	-172.044	-211.231							

Figure B.3: QV Results corresponding to a load of 32+j6.4, load factor of 0.98 lagging at Bus 3005

Load 40+j0																									
CONTINGENCY: BASE CASE		Plant (MVAR)																							
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	686.597	578.121	476.351	396.267	372.719	346.452	291.003	239.366	186.184	135.265	85.613	37.237	-9.857	-55.660	-100.163	-143.355	-185.226	-225.761	-264.947	-298.992	-293.893				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	653.040	552.785	459.005	388.578	372.473	352.480	305.142	258.914	213.803	169.914	126.953	85.228	44.645	8.213	-33.059	-70.159	-106.077	-140.800	-174.312	-203.632	-219.436				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	653.040	552.785	459.005	388.578	372.473	352.480	305.142	258.914	213.803	169.914	126.953	85.228	44.645	8.213	-33.059	-70.159	-106.077	-140.800	-174.312	-203.632	-219.436				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	673.071	581.104	493.557	427.071	401.213	381.316	339.625	294.940	251.256	208.575	166.901	126.238	86.589	47.960	10.355	-26.220	-61.759	-96.256	-121.703	-162.092	-193.413				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	568.569	478.284	434.055	403.533	352.871	303.265	254.718	207.234	160.814	115.468	71.183	27.980	-14.142	-55.179	-96.124	-133.572	-171.716	-208.348	-243.860	-278.243	-294.656				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	477.797	400.937	341.671	318.214	284.617	229.680	175.931	123.373	72.010	21.847	-27.111	-74.888	-121.388	-166.933	-210.765	-253.595	-295.172	-335.486	-374.522	-383.397					
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	559.594	508.345	485.708	449.237	393.586	339.149	285.933	233.944	183.189	133.674	85.409	38.402	-7.335	-51.791	-94.963	-136.806	-177.333	-216.514							

Figure B.4: QV Results corresponding to a load of 40+j0, UPF load factor at Bus 3005

Load 41-j30.6																									
CONTINGENCY: BASE CASE		Plant (MVAR)																							
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	656.071	547.655	445.884	365.811	342.264	316.030	261.341	207.903	155.722	104.803	55.152	6.776	-40.318	-86.120	-130.623	-173.814	-215.684	-256.219	-295.404	-325.436	-324.334				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	622.602	522.348	428.567	388.158	342.054	322.049	274.710	228.483	183.373	139.304	96.524	54.799	14.217	-25.214	-63.485	-100.585	-136.502	-171.223	-204.734	-234.033	-223.832				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	642.628	550.662	463.114	396.627	370.799	350.905	309.192	264.509	220.924	176.143	136.470	95.807	56.159	17.530	-20.074	-56.649	-92.188	-126.684	-160.130	-192.518	-223.838				
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.00	447.271	370.411	311.150	287.694	254.091</td																				

Figure B.6: QV Results corresponding to a load of 20-j10, load factor of 0.89 leading at Bus 3005

Load 32-j6.4																									
		Plant (MVAR)																							
CONTINGENCY: BASE CASE		Plant (MVAR)																							
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.0	679.075	570.658	468.895	388.727	365.173	339.005	284.315	230.876	178.692	127.771	78.117	25.737	-17.360	-63.167	-107.674	-150.872	-192.748	-233.289	-272.481	-306.627	-301.553				
	CONTINGENCY: SING OPN LIN 1 3005-3003(1) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.0	645.353	545.097	451.325	380.757	364.641	344.747	297.406	251.176	206.062	162.069	119.304	77.473	36.885	-2.553	-40.831	-77.938	-113.864	-148.595	-182.117	-211.602	-201.443				
	CONTINGENCY: SING OPN LIN 2 3005-3003(2) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.0	645.353	545.097	451.325	380.757	364.641	344.747	297.406	251.176	206.062	162.069	119.304	77.473	36.885	-2.553	-40.831	-77.938	-113.864	-148.595	-182.117	-211.602	-201.443				
	CONTINGENCY: SING OPN LIN 3 3005-3004(1) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.0	665.421	573.451	485.516	419.433	389.335	373.420	331.899	287.212	243.525	200.842	159.165	118.498	78.046	40.213	2.604	-33.796	-69.521	-104.024	-137.477	-169.872	-201.200				
	CONTINGENCY: SING OPN LIN 4 3005-3006(1) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.0	561.076	470.793	426.505	396.031	345.368	295.761	247.213	195.726	153.305	107.953	63.669	20.463	-21.662	-62.702	-102.652	-141.504	-175.253	-215.880	-251.408	-285.797	-302.418				
	CONTINGENCY: SING OPN LIN 5 3005-3008(41) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.0	470.811	393.957	334.648	311.151	277.633	222.700	189.554	146.399	105.078	64.039	34.077	-81.822	-128.350	-173.653	-217.724	-260.553	-302.130	-342.444	-381.481	-390.422					
	CONTINGENCY: SING OPN LIN 6 3005-3008(1) Plant (MVAR)																								
VOLTAGE SETPOINT->	1.100	1.090	1.080	1.070	1.060	1.050	1.040	1.030	1.020	1.010	1.000	0.990	0.980	0.970	0.960	0.950	0.940	0.930	0.920	0.910	0.900				
3005 WEST 230.0	552.150	500.812	478.166	441.764	386.112	331.674	278.457	246.467	175.709	126.192	77.924	30.915	-14.826	-59.286	-102.453	-144.311	-184.844	-224.031							

Figure B.7: QV Results corresponding to a load of 32-j6.4, load factor of 0.98 leading at Bus 3005